

MARCH 2021 QUARTERLY ACTIVITIES REPORT

DATELINE RESOURCES LIMITED

(ACN 149 105 653)

ASX Code: DTR

CAPITAL STRUCTURE

Share Price (26.4.21) \$0.004
 Shares on issue 8,831 million
 Market Cap \$35.3 million

MAJOR SHAREHOLDERS

Southern Cross Exploration NL 27.1%
 Mr. Mark Johnson AO 19.0%
 National Nominees Ltd 14.9%

DIRECTORS & MANAGEMENT

Mark Johnson AO
 Chairman
 Stephen Baghdadi
 Managing Director
 Greg Hall
 Non-Executive Director
 Tony Ferguson
 Non-Executive Director
 Bill Lannen
 Non-Executive Director
 John Smith
 Company Secretary

CONTACT
 John Smith
 Phone: +61 2 9375 2353
 Postal Address: P.O. Box 553
 South Hurstville NSW 2221
 Email: info@datelineresources.com.au

Dateline Resources Limited (ASX: DTR) (Dateline or the Company) is pleased to provide an update on its activities for the March 2021 quarter. The Company’s focus during the period was the acquisition of the Colosseum Gold Mine (Colosseum) in California and securing an approximate A\$9.0M working capital facility to advance the Gold Links Project in Colorado.

Acquisition of Colosseum Gold Mine – California USA

Dateline has entered into a binding Agreement with LAC Minerals (USA) LLC, a wholly owned subsidiary of Barrick Gold Corporation, for the acquisition of 100% of Colosseum and will acquire 83 mining claims that host the Colosseum Gold Mine and surrounding areas, totalling approximately 1,600 acres¹.

The Colosseum is located in the southern section of the Walker Lane Trend in California USA. The Walker Lane Trend hosts numerous substantial discoveries including the Corvus Gold owned 1.7 million ounce Mother Lode deposit and the 6.5 million ounce Castle Mountain gold mine owned by Equinox Gold (located 50km to the South East of Colosseum). America’s only rare earths mine, the MP Materials owned Mountain Pass Mine is located 10km from the Colosseum.



Figure 1: Colosseum location relative to other operating mines and significant discoveries

The Colosseum produced approximately 344,000 ounces of gold between 1988 and 1993 from a BP Minerals calculated mining reserve of 700,000 ounces. Mining reserve calculations by BP Minerals used a 1.0g/t gold cutoff grade and estimated a 2.5g/t gold head grade. Mineralisation is primarily hosted in breccia pipes and is reported to be open at depth.

Dateline is currently reviewing the historical exploration data and is planning a drill program designed to test the extent of mineralisation within the breccia pipes below the previously drilled depth of 333 metres (1,000 feet) and the possibility that the separate pipes join up and/or link to a larger feeder system.

Post quarter end, Dateline deposited US\$500,000 into the nominated escrow account completing the first financial obligation of the acquisition².

¹ ASX release – 15 March 2021 - Colosseum Gold Mine Acquisition

² ASX release – 7 April 2021 - Colosseum Transaction Update

Gold Links – Colorado USA 100% Owned

During the quarter, Dateline secured a US\$6,843,000 (approximately A\$9,000,000) long term working capital facility to advance Gold Links into production³. The funds were received in full and will finance an extensive work program to be carried out at Gold Links over the year. The work program includes:

- Underground and surface drilling to increase the current resource base;
- Underground development to enable the extraction of the resource (expected Q3 CY21); and
- Processing of the extracted resource at the company’s Lucky Strike Mill (expected Q4 CY21).

Gold Links hosts a swarm of high-grade narrow gold veins over more than 5km strike length and a kilometre across strike. Historical mapping and drilling coupled with the Company’s own exploration work has confirmed mineralisation is extensive throughout the Project. Dateline’s 100% owned Lucky Strike Mill will be used to process material from the Gold Links Mine.

The Company’s website hosts an informative video on the Gold Links Project, found on the Gold Links Project page.

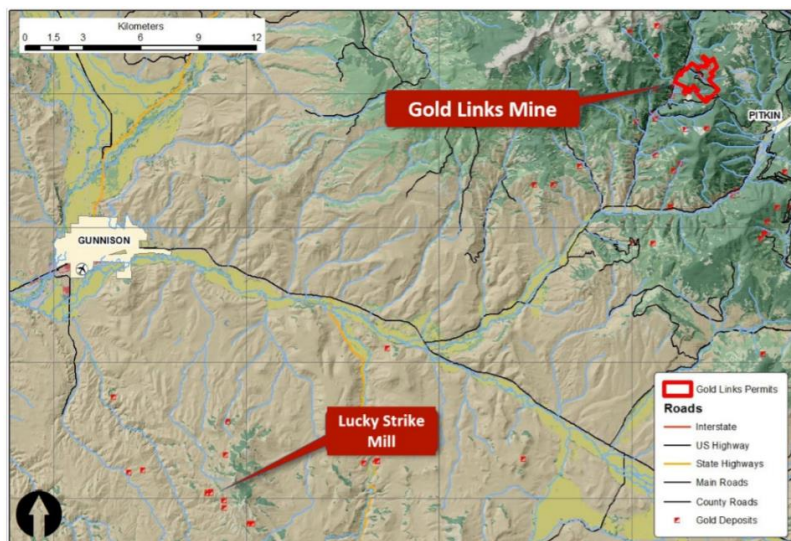


Figure 2: Location map of Gold Links Mine and the Lucky Strike Mill, Colorado USA

Delineated Mineral Resource

Dateline has delineated the following JORC compliant resource as described in the table below and in the attached JORC Table:

Zone	Category	Tons	Average Grade (Au g/t)	Total Ounces Au
2150 vein “Above” (9900ft elevation)	Indicated	9,033	14.73	3,879
	Inferred	4,134	7.32	882
2150 vein “Below” (9450ft elevation)	Inferred	21,026	10.52	6,453
Sacramento	Inferred	110,780	3.21	10,378

Table 1 – JORC compliant resource

³ ASX release – 24 March 2021 – Long Term Working Capital Facility Secured

Corporate

At the end of the quarter, the Company's cash balance was \$9.323 million.

Post quarter end, the Company announced a Notice of General Meeting, to be held on 21 May 2021. The purpose of the General Meeting is, amongst other matters, to replace the Constitution, a share consolidation through the conversion of every 25 shares held by a Shareholder into 1 share and the ratification of prior and new share issues. More information can be found on the ASX release dated 21 April 2021.

Authorised by the Dateline Board.

For more information, please contact:

Stephen Baghdadi

Managing Director

+61 2 9375 2353

www.datelineresources.com.au

Follow Dateline on Twitter:



https://twitter.com/Dateline_DTR

About Dateline Resources Limited

Dateline Resources Limited (ASX: DTR) is an Australian publicly listed company focused on gold mining and exploration in North America. The Company owns 100% of the Colosseum Gold Mine in California as well as the Gold Links and Green Mountain Projects in Colorado, USA.

Colosseum Gold Mine is located in the Walker Lane Trend in East San Bernardino County, California and produced approximately 344,000 ounces of gold at a head grade of 2.5g/t (see ASX release 15 March 2021).

Gold Links is comprised of several contiguous historic gold mines that have been consolidated by the Company. Gold Links has produced up to 150,000 ounces of high-grade gold (see ASX release 8 February 2019).

Mineralisation can be traced on surface and underground for almost 6km from the Northern to the Southern sections of the project. Well documented records indicate that there are large areas that remain untested at surface and little to no exploration has been done below the valley floor.

Green Mountain Project hosts the Lucky Strike and Mineral Hill permitted gold properties as well as a recommissioned gold processing plant (Lucky Strike Mill). Gold Links and the Lucky Strike Mill are 50km apart.

Appendix 1. Drill Hole Configuration Information

Gold Links Vein System REY Drilling Program - Part A RELEV & DEPT in feet as originally recorded								
HOLE	NORT	EAST	RELEV	INCL	AZIM	DEPT	TYPE	AREA
REY-001	1292167.88	2694413.74	9933.27	0	259	137.7	DD-HQ	Reynolds Decline
REY-002	1292077.99	2694366.59	9935.19	-3	256	183	DD-NQ	Reynolds Decline
REY-003	1292069.15	2694358.33	9932.97	-10	226	139	DD-NQ	Reynolds Decline
REY-004	1291976.03	2694274.35	9912.68	12	263	123	DD-DD-NQ2	Reynolds Decline
REY-005	1291975.44	2694278.47	9922.98	52	265	66	DD-NQ2	Reynolds Decline
REY-006	1291971.9	2694268.75	9911.86	-8	259	100	DD-NQ2	Reynolds Decline
REY-007	1291971.02	2694270.22	9916	10	260	84.7	DD-NQ2	Reynolds Decline
REY-008	1291973.08	2694274.35	9920.34	34	239	65	DD-NQ2	Reynolds Decline
REY-009	1291974.26	2694278.18	9922.64	53	245	66	DD-NQ2	Reynolds Decline
REY-010	1291969.84	2694274.94	9911.26	-6.5	227.5	131	DD-NQ2	Reynolds Decline
REY-011	1291974.26	2694271.4	9915.51	17	270	74.2	DD-NQ2	Reynolds Decline
REY-012	1291974.26	2694274.35	9919.06	40	263	62	DD-NQ2	Reynolds Decline
REY-013	1291876.42	2694212.46	9901.57	-20	306	154	DD-NQ3/2	Reynolds Decline
REY-014	1291876.42	2694212.46	9903.07	-11	312	86	DD-NQ2	Reynolds Decline
REY-015	1291876.13	2694212.16	9905.87	21	309	51	DD-NQ3	Reynolds Decline
REY-016	1291874.36	2694213.93	9913.57	81	312	77	DD-NQ2	Reynolds Decline
REY-017	1291873.18	2694208.04	9900.27	-26	261	112	DD-NQ2	Reynolds Decline
REY-018	1291872.3	2694207.45	9902.86	-8	258	110	DD-NQ2	Reynolds Decline
REY-019	1291873.77	2694209.22	9906.3	22	264	97	DD-NQ2	Reynolds Decline
REY-020	1291874.36	2694212.16	9912.43	76	313	82	DD-NQ2	Reynolds Decline
REY-025	1291808.94	2694178.57	9888.45	-15	283	203	DD-NQ2	Reynolds Decline
REY-027	1291808.35	2694179.16	9895.23	32	275	92	DD-NQ2	Reynolds Decline
REY-028	1291806.87	2694183.28	9899.65	77	254	103	DD-NQ2	Reynolds Decline
REY-030	1291806.28	2694177.68	9891.04	7	247	98	DD-NQ2	Reynolds Decline
REY-038	1291726.42	2694144.97	9876.15	-16	268	123	DD-NQ2	Reynolds Decline
REY-039	1291726.42	2694144.68	9878.23	2	267	49	DD-NQ2	Reynolds Decline
REY-040	1291726.42	2694145.56	9884.7	45	287	57	DD-NQ2	Reynolds Decline
REY-041	1291726.13	2694147.92	9886.13	82	221	99	DD-NQ2	Reynolds Decline
REY-042	1291724.65	2694144.09	9876.39	-7	251	133	DD-NQ2	Reynolds Decline
REY-043	1291724.65	2694144.09	9878.01	10	260	103	DD-NQ2	Reynolds Decline
REY-044	1291725.24	2694145.27	9881.19	39	263	74	DD-NQ2	Reynolds Decline
REY-045	1291725.54	2694147.04	9886.05	65	249	112	DD-NQ2	Reynolds Decline
REY-046	1291725.83	2694149.1	9887.15	86	130	128	DD-NQ2	Reynolds Decline
REY-047	1291645.67	2694113.15	9863.08	-1	301	114	DD-NQ2	Reynolds Decline
REY-048	1291645.97	2694112.26	9866.68	17	305	109	DD-NQ2	Reynolds Decline
REY-049	1291645.67	2694113.44	9871.89	49	304	108	DD-NQ2	Reynolds Decline
REY-050	1291643.32	2694116.09	9872.73	81	306	97	DD-NQ2	Reynolds Decline
REY-051	1291643.32	2694111.97	9862.76	-6	272	99	DD-NQ2	Reynolds Decline
REY-052	1291643.61	2694111.08	9865.25	17	280	99	DD-NQ2	Reynolds Decline
REY-053	1291643.02	2694112.56	9871.33	51	276	97	DD-NQ2	Reynolds Decline
REY-054	1291642.43	2694115.8	9872.64	77	230	103	DD-NQ2	Reynolds Decline
REY-056	1291641.84	2694110.49	9866.57	16	268	188	DD-NQ2	Reynolds Decline
REY-057	1291641.55	2694111.38	9869.27	62	253	91	DD-NQ2	Reynolds Decline
REY-058	1291641.55	2694114.03	9872.1	84	235	89	DD-NQ2	Reynolds Decline
REY-074	1291971.9	2694268.75	9910.54	-19	268	16	DD-NQ2	Reynolds Decline
REY-075	1291972.49	2694269.93	9915.29	25	269	75	DD-NQ2	Reynolds Decline
REY-076	1291972.79	2694270.51	9918.24	46	264	70	DD-NQ2	Reynolds Decline
REY-078	1292009.33	2694302.64	9924.43	38	310	67	DD-NQ3	Reynolds Decline
REY-079	1292007.56	2694304.7	9927.16	54	296	56	DD-NQ3	Reynolds Decline

**Gold Links Vein
System REY Drilling
Program - Part B
RELEV & DEPT in feet as originally recorded**

HOLE	NORT	EAST	RELEV	INC L	AZIM	DEPT	TYPE	AREA
REY-080	1292004.61	2694308.53	9923.82	75	302	60	DD-NQ3	Reynolds Decline
REY-081	1291945.97	2694257.55	9907.08	-18	285	91.3	DD-NQ3	Reynolds Decline
REY-082	1291945.97	2694257.55	9907.54	-12	285	87.4	DD-NQ3	Reynolds Decline
REY-083	1291945.97	2694257.55	9907.83	-2	285	77	DD-NQ3	Reynolds Decline
REY-084	1291937.42	2694250.48	9908.27	10	293	68	DD-NQ3	Reynolds Decline
REY-085	1291937.13	2694250.77	9909.85	23	291	60	DD-NQ3	Reynolds Decline
REY-086	1291936.83	2694251.95	9911.87	39	288	58	DD-NQ3	Reynolds Decline
REY-087	1291936.24	2694253.13	9914.34	56	293	55	DD-NQ3	Reynolds Decline
REY-088	1291935.66	2694254.31	9916.42	68	287	58.5	DD-NQ3	Reynolds Decline
REY-089	1291934.48	2694256.66	9916.55	85	309	69	DD-NQ3	Reynolds Decline
REY-090	1291921.51	2694238.1	9903.87	-16	281	106.5	DD-NQ3	Reynolds Decline
REY-091	1291921.51	2694238.39	9904.3	-12	281	93	DD-NQ3	Reynolds Decline
REY-092	1291921.22	2694238.98	9905.14	-1	281	83	DD-NQ3	Reynolds Decline
REY-093	1291920.63	2694241.04	9908.23	35	284	83	DD-NQ3	Reynolds Decline
REY-094	1291920.63	2694241.04	9911.15	43	282	66	DD-NQ3	Reynolds Decline
REY-095	1291920.33	2694241.04	9913.56	53	280	15	DD-NQ3	Reynolds Decline
REY-096	1291921.51	2694238.1	9903.47	-20	280	118	DD-NQ3	Reynolds Decline
REY-097	1291921.51	2694238.1	9903.22	-24	282	58	DD-NQ3	Reynolds Decline
REY-098	1291992.24	2694282.01	9914.17	-9	289	132	DD-NQ3	Reynolds Decline
REY-099	1291991.06	2694283.48	9914.98	-5	288	118	DD-NQ3	Reynolds Decline
REY-100	1291990.76	2694282.89	9915.63	-1	278	48	DD-NQ3	Reynolds Decline
REY-101	1291990.76	2694282.3	9917.1	4	275	88	DD-NQ3	Reynolds Decline
REY-102	1291990.47	2694285.54	9918.15	15	279	76	DD-NQ3	Reynolds Decline
REY-103	1291990.47	2694283.19	9918.37	25	274	67	DD-NQ3	Reynolds Decline
REY-104	1291990.17	2694283.78	9923.55	43	272	57.5	DD-NQ3	Reynolds Decline
REY-105	1291990.17	2694285.25	9923.57	48	273	58	DD-NQ3	Reynolds Decline
REY-106	1291989.88	2694286.43	9926.41	67	308	6	DD-NQ3	Reynolds Decline
REY-107	1291989.59	2694289.67	9926.71	74	264	62	DD-NQ3	Reynolds Decline
REY-108	1291864.34	2694204.8	9901.81	-1	300	104	DD-NQ3	Reynolds Decline
REY-109	1291875.83	2694212.16	9903.49	-3	310	68	DD-NQ3	Reynolds Decline
REY-110	1291875.54	2694212.16	9901.61	-18	311	114	DD-NQ3	Reynolds Decline
REY-111	1291875.54	2694211.87	9901.91	-13	311	107	DD-NQ3	Reynolds Decline
REY-112	1291875.54	2694211.87	9901.21	-20	310	119	DD-NQ3	Reynolds Decline
REY-113	1291873.77	2694208.63	9901.01	-10	258	44	DD-NQ3	Reynolds Decline
REY-114	1291874.06	2694209.22	9898.81	-26	260	112	DD-NQ3	Reynolds Decline
REY-115	1292118.37	2694344.78	9935.01	-20	297	68	DD-NQ3	Reynolds Decline
REY-116	1292118.37	2694344.19	9937.41	-1	296	45	DD-NQ3	Reynolds Decline
REY-117	1292115.72	2694347.73	9945.21	58	299	45	DD-NQ3	Reynolds Decline
REY-118	1291728.19	2694145.56	9878.49	4	260	62	DD-NQ3	Reynolds Decline
REY-119	1291728.19	2694145.56	9876.91	-18	268	59	DD-NQ3	Reynolds Decline
REY-120	1291759.43	2694175.33	9882.38	-14	106	914.7	DD-NQ3	Reynolds Decline
REY-121	1291576.42	2694071.89	9850.09	0	264	109	DD-HQ	Reynolds Decline
REY-122	1291576.42	2694071.59	9851.56	-1	263	65.7	DD-HQ	Reynolds Decline
REY-123	1291621.8	2694102.54	9858.15	-14	260	28	DD-HQ	Reynolds Decline
REY-124	1291621.21	2694102.54	9864.13	21	260	17	DD-HQ	Reynolds Decline
REY-125	1291874.95	2694211.28	9901.2	-28	285	129	DD-HQ	Reynolds Decline
REY-126	1291874.95	2694210.99	9901.65	-24	277	104	DD-HQ	Reynolds Decline
REY-127	1291874.95	2694210.69	9902.22	-9	283	99.7	DD-HQ	Reynolds Decline
REY-128	1291875.24	2694210.1	9903.18	-1	290	80	DD-HQ	Reynolds Decline

**Gold Links Vein
System REY Drilling
Program - Part A
(FROM-TO-LENGTH in feet; GOLD>1 ppm; G x L in ft-ppm)
(Significant Values in Bold)**

HOLE	SAMP	FROM	TO	LENG	GOLD	G x L	TYPE	NOTES	AREA
REY-001	P359119	36.0	41.0	5.0	1.47	7.35	Core	No Information	Reynolds Decline
REY-003	P359131	110.0	113.0	3.0	2.81	8.43	Core	FW 2150 vein	Reynolds Decline
REY-003	P359132	113.0	118.5	5.5	20.20	111.10	Core	2150 vein	Reynolds Decline
REY-004	P358481	77.0	79.0	2.0	34.00	68.00	Core	2150 vein	Reynolds Decline
REY-005	P358492	48.5	51.0	2.5	40.50	101.25	Core	2150 vein	Reynolds Decline
REY-005	P358494	53.0	55.5	2.5	1.54	3.85	Core	HW 2150 vein	Reynolds Decline
REY-006	P359136	79.2	81.0	1.8	86.50	155.70	Core	2150 vein	Reynolds Decline
REY-006	P359141	89.0	91.0	2.0	90.60	181.20	Core	2150 vein	Reynolds Decline
REY-007	P358498	59.0	61.0	2.0	27.30	54.60	Core	2150 vein	Reynolds Decline
REY-007	P358499	61.0	63.0	2.0	9.60	19.20	Core	2150 vein	Reynolds Decline
REY-007	P358500	63.0	66.0	3.0	12.30	36.90	Core	2150 vein	Reynolds Decline
REY-007	P358401	66.0	68.0	2.0	11.10	22.20	Core	2150 vein	Reynolds Decline
REY-008	P359148	49.0	51.0	2.0	3.39	6.78	Core	2150 vein	Reynolds Decline
REY-008	P359149	51.0	53.0	2.0	8.84	17.68	Core	2150 vein	Reynolds Decline
REY-008	P359150	53.0	55.0	2.0	2.09	4.18	Core	HW 2150 vein	Reynolds Decline
REY-009	P358466	49.0	52.0	3.0	4.56	13.68	Core	2150 vein	Reynolds Decline
REY-009	P358467	52.0	54.0	2.0	50.90	101.80	Core	2150 vein	Reynolds Decline
REY-009	P358469	54.0	56.0	2.0	8.57	17.14	Core	2150 vein	Reynolds Decline
REY-011	P358457	57.0	59.2	2.2	21.20	46.64	Core	2150 vein	Reynolds Decline
REY-012	P358473	41.0	45.0	4.0	2.85	11.40	Core	2150 vein	Reynolds Decline
REY-012	P358476	49.0	51.0	2.0	5.49	10.98	Core	2150 vein	Reynolds Decline
REY-014	P358417	76.6	78.0	1.4	116.00	162.40	Core	2150 vein	Reynolds Decline
REY-015	P358410	30.7	32.7	2.0	3.05	6.10	Core	Veinlets	Reynolds Decline
REY-018	P358444	49.5	52.5	3.0	1.65	4.95	Core	HW 2150 vein	Reynolds Decline
REY-038	P358577	40.0	42.0	2.0	2.81	5.62	Core	2150 vein	Reynolds Decline
REY-039	P358558	41.2	44.6	3.4	5.69	19.35	Core	2150 vein	Reynolds Decline
REY-075	P358607	49.6	52.5	2.9	1.89	5.48	Core	2150 vein	Reynolds Decline
REY-076	P358610	38.6	40.6	2.0	288.00	576.00	Core	FW 2150 vein	Reynolds Decline
REY-076	P358611	40.6	43.6	3.0	327.00	981.00	Core	2150 vein	Reynolds Decline
REY-076	P358612	43.6	46.6	3.0	85.00	255.00	Core	2150 vein	Reynolds Decline
REY-076	P358614	46.6	49.6	3.0	123.00	369.00	Core	2150 vein	Reynolds Decline
REY-076	P358615	49.6	52.5	2.9	41.10	119.19	Core	2150 vein	Reynolds Decline
REY-076	P358616	52.5	54.5	2.0	297.00	594.00	Core	HW 2150 vein	Reynolds Decline
REY-078	P358618	47.6	49.6	2.0	10.40	20.80	Core	2150 vein	Reynolds Decline
REY-079	P358621	49.0	54.0	5.0	8.81	44.05	Core	2150 vein	Reynolds Decline
REY-081	P358623	82.5	85.3	2.8	14.70	41.16	Core	2150 vein	Reynolds Decline
REY-081	P358624	85.3	88.5	3.2	6.38	20.42	Core	2150 vein	Reynolds Decline
REY-082	P358629	73.3	76.0	2.7	32.80	88.56	Core	2150 vein	Reynolds Decline
REY-083	P358676	61.0	64.0	3.0	32.10	96.30	Core	2150 vein	Reynolds Decline
REY-084	P358680	44.7	47.5	2.8	3.15	8.82	Core	2150 vein	Reynolds Decline
REY-084	P358681	47.5	49.0	1.5	48.20	72.30	Core	2150 vein	Reynolds Decline
REY-085	P358687	37.0	38.2	1.2	3.15	3.78	Core	2150 vein	Reynolds Decline
REY-085	P358689	40.0	42.0	2.0	1.78	3.56	Core	2150 vein	Reynolds Decline
REY-085	P358690	42.0	46.5	4.5	3.94	17.73	Core	2150 vein	Reynolds Decline
REY-086	P358703	39.0	43.5	4.5	20.00	90.00	Core	2150 vein	Reynolds Decline
REY-087	P358723	39.0	41.0	2.0	2.64	5.28	Core	HW 2150 vein	Reynolds Decline
REY-087	P358724	41.0	43.5	2.5	10.90	27.25	Core	HW 2150 vein	Reynolds Decline
REY-087	P358725	43.5	45.5	2.0	3.09	6.18	Core	HW 2150 vein	Reynolds Decline
REY-088	P358712	29.0	32.5	3.5	2.57	9.00	Core	FW 2150 vein	Reynolds Decline

Appendix 2. Drill Hole Significant Intersections

Gold Links Vein System REY Drilling Program - Part A (FROM-TO-LENGTH in feet; GOLD>1 ppm; G x L in ft-ppm)(Significant Values in Bold)									
HOLE	SAMP	FROM	TO	LENG	GOLD	G x L	TYPE	NOTES	AREA
REY-088	P358716	43.0	48.4	5.4	5.52	29.81	Core	2150 vein	Reynolds Decline
REY-088	P358717	48.4	49.3	0.9	9.08	8.17	Core	2150 vein	Reynolds Decline
REY-089	P358706	39.5	44.5	5.0	30.10	150.50	Core	2150 vein	Reynolds Decline
REY-089	P358708	44.5	49.0	4.5	2.19	9.86	Core	2150 vein	Reynolds Decline
REY-089	P358711	64.5	67.0	2.5	25.80	64.50	Core	Vein	Reynolds Decline
REY-090	P358634	78.0	83.0	5.0	3.84	19.20	Core	2150 vein	Reynolds Decline
REY-090	P358636	83.0	85.8	2.8	35.50	99.40	Core	2150 vein	Reynolds Decline
REY-091	P358645	67.7	70.6	2.9	3.29	9.54	Core	Gouge	Reynolds Decline
REY-091	P358646	70.6	72.0	1.4	7.10	9.94	Core	2150 vein	Reynolds Decline
REY-091	P358647	72.0	75.0	3.0	2.81	8.43	Core	2150 vein	Reynolds Decline
REY-091	P358649	75.0	76.7	1.7	62.90	106.93	Core	2150 vein	Reynolds Decline
REY-092	P358655	50.3	53.2	2.9	13.70	39.73	Core	2150 vein	Reynolds Decline
REY-092	P358656	53.2	58.0	4.8	2.88	13.82	Core	2150 vein	Reynolds Decline
REY-092	P358658	58.0	62.0	4.0	9.50	38.00	Core	2150 vein	Reynolds Decline
REY-093	P358660	31.0	33.0	2.0	1.92	3.84	Core	2150 vein	Reynolds Decline
REY-093	P358662	35.0	37.0	2.0	1.06	2.12	Core	Clay	Reynolds Decline
REY-093	P358663	37.0	39.8	2.8	2.33	6.52	Core	2150 vein	Reynolds Decline
REY-093	P358666	47.2	48.2	1.0	205.00	205.00	Core	Limonite Qtz	Reynolds Decline
REY-094	P358672	32.4	34.2	1.8	52.00	93.60	Core	2150 vein	Reynolds Decline
REY-094	P358673	34.2	37.7	3.5	20.90	73.15	Core	2150 vein	Reynolds Decline
REY-096	P358693	102.0	105.0	3.0	4.24	12.72	Core	2150 vein	Reynolds Decline
REY-099	P358731	95.0	97.0	2.0	36.00	72.00	Core	2150 vein	Reynolds Decline
REY-101	P358736	61.8	64.6	2.8	2.63	7.36	Core	2150 vein	Reynolds Decline
REY-102	P358741	58.7	61.3	2.6	2.19	5.69	Core	2150 vein	Reynolds Decline
REY-103	P358748	53.0	54.0	1.0	2.02	2.02	Core	2150 vein	Reynolds Decline
REY-104	P358751	43.6	46.8	3.2	8.60	27.52	Core	2150 vein	Reynolds Decline
REY-107	P358756	45.7	48.0	2.3	24.30	55.89	Core	2150 vein	Reynolds Decline
REY-107	P358758	50.0	53.0	3.0	2.43	7.29	Core	2150 vein	Reynolds Decline
REY-109	P358762	46.1	48.0	1.9	6.41	12.18	Core	2150 vein	Reynolds Decline
REY-109	P358763	48.0	50.0	2.0	3.70	7.40	Core	2150 vein	Reynolds Decline
REY-109	P358764	50.0	52.4	2.4	7.61	18.26	Core	2150 vein	Reynolds Decline
REY-109	P358765	52.4	54.4	2.0	24.30	48.60	Core	2150 vein	Reynolds Decline
REY-110	P358768	96.8	99.0	2.2	95.70	210.54	Core	2150 vein	Reynolds Decline
REY-110	P358770	99.0	102.4	3.4	1.10	3.74	Core	2150 vein	Reynolds Decline
REY-111	P358775	81.0	83.0	2.0	1.92	3.84	Core	FW 2150 vein	Reynolds Decline
REY-111	P358776	83.0	85.0	2.0	62.10	124.20	Core	2150 vein	Reynolds Decline
REY-111	P358778	85.0	87.0	2.0	73.50	147.00	Core	2150 vein	Reynolds Decline
REY-111	P358779	87.0	89.5	2.5	82.80	207.00	Core	2150 vein	Reynolds Decline
REY-111	P358781	89.5	92.5	3.0	1.85	5.55	Core	HW 2150 vein	Reynolds Decline
REY-116	P358800	3.0	4.0	1.0	13.30	13.30	Core	Limonite Qtz	Reynolds Decline
REY-116	P358802	19.6	22.0	2.4	1.13	2.71	Core	2150 vein	Reynolds Decline
REY-117	P358811	14.8	16.8	2.0	5.73	11.46	Core	Limonite Qtz	Reynolds Decline
REY-118	P358813	39.0	41.2	2.2	3.70	8.14	Core	Sulphide Qtz Vein	Reynolds Decline
REY-118	P358817	54.0	56.0	2.0	1.54	3.08	Core	2150 vein	Reynolds Decline
REY-118	P358818	56.0	58.0	2.0	23.00	46.00	Core	2150 vein	Reynolds Decline
REY-118	P358819	58.0	60.0	2.0	5.66	11.32	Core	2150 vein	Reynolds Decline
REY-119	P358822	39.0	41.5	2.5	1.30	3.25	Core	Sulphide Qtz Vein	Reynolds Decline
REY-125	P358827	116.6	119.0	2.4	20.40	48.96	Core	2150 vein	Reynolds Decline
REY-126	P358830	93.0	96.8	3.8	18.40	69.92	Core	2150 vein	Reynolds Decline

**Gold Links Vein
System C-CRG-GL-
SAC Drilling
Programs
(FROM-TO-LENGTH in feet; GOLD>1 ppm; G x L
in ft-ppm)(Significant Values in Bold)**

HOLE	SAMP	FROM	TO	LENG	GOLD	G x L	TYPE	NOTES	AREA
C-08-2018	P358851	445.0	449.0	4.0	38.40	153.60	Core	2150 vein	Reynolds SF
C-08-2018	P358852	449.0	451.0	2.0	198.00	396.00	Core	2150 vein	Reynolds SF
C8-16-1	P358155	512.0	514.0	2.0	3.37	6.74	Core	Vein	Reynolds SF
CRG-17-1	P358184	206.0	208.0	2.0	2.30	4.60	Core	No Information	Reynolds Main UG
CRG-17-1	P358187	254.8	255.8	1.0	1.37	1.37	Core	No Information	Reynolds Main UG
CRG-17-1	P358188	267.4	269.0	1.6	7.61	12.18	Core	No Information	Reynolds Main UG
CRG-17-3	P358252	116.5	119.0	2.5	3.81	9.53	Core	No Information	Reynolds Main UG
CRG-17-3	P358254	122.0	124.4	2.4	1.03	2.47	Core	No Information	Reynolds Main UG
CRG-17-3	P358257	161.6	164.4	2.8	1.41	3.95	Core	No Information	Reynolds Main UG
CRG-17-3	P358266	202.7	203.7	1.0	7.77	7.77	Core	Vein	Reynolds Main UG
GL01	P359238	170.5	171.8	1.3	2.02	2.63	Core	No Information	Reynolds SF
GL02	P359525	210.0	215.0	5.0	1.20	6.00	Chips	No Information	Reynolds SF
GL03	P359444	574.1	575.0	0.9	151.00	135.90	Core	Sulphide Alteration	Reynolds SF
GL03	P359445	575.0	575.8	0.8	1.71	1.37	Core	Gouge	Reynolds SF
GL03	P359446	575.8	577.2	1.4	1.47	2.06	Core	Sulphide Gouge	Reynolds SF
GL03	P359447	577.2	578.9	1.7	3.87	6.58	Core	Sulphide Vein	Reynolds SF
GL03	P359803	636.4	637.3	0.9	1.61	1.45	Core	No Information	Reynolds SF
GL04	P359462	664.0	665.0	1.0	6.96	6.96	Core	Sulphide Vein	Reynolds SF
GL04	P359464	666.5	667.8	1.3	4.83	6.28	Core	Sulphide Vein	Reynolds SF
GL04	P359468	670.4	671.6	1.2	3.70	4.44	Core	Sulphide Fault	Reynolds SF
GL05	P359476	637.5	638.5	1.0	7.82	7.82	No Info	No Information	Reynolds SF
GL05	P359480	641.8	643.5	1.7	7.20	12.24	No Info	Vein	Reynolds SF
GL05	P359481	643.5	645.0	1.5	1.27	1.91	No Info	No Information	Reynolds SF
GL05	P359483	646.6	648.4	1.8	6.52	11.74	No Info	No Information	Reynolds SF
GL06	P359491	702.2	703.9	1.7	3.05	5.19	Core	No Information	Reynolds SF
GL06	P359496	718.0	718.9	0.9	6.92	6.23	Core	No Information	Reynolds SF
GL08	P359664	216.3	217.7	1.4	71.90	100.66	Core	No Information	Reynolds SF
GL08	P359753	540.9	542.2	1.3	1.13	1.47	Core	Gouge	Reynolds SF
GL09	P359820	672.1	672.4	0.3	1.13	0.34	Core	No Information	Reynolds SF
GL09	P359825	690.4	692.0	1.6	7.34	11.74	Core	No Information	Reynolds SF
GL09	P359852	699.7	700.8	1.1	1.20	1.32	Core	No Information	Reynolds SF
GL11	P359550	360.0	365.0	5.0	4.56	22.80	Chips	No Information	Reynolds SF
GL11	P359586	365.0	370.0	5.0	1.06	5.30	Chips	No Information	Reynolds SF
GL17	P359939	250.0	255.0	5.0	1.89	9.45	Chips	No Information	Reynolds SF
SAC06	P359317	275.5	277.0	1.5	14.00	21.00	Core	No Information	Sacramento SF
SAC06	P359319	278.5	280.0	1.5	1.71	2.57	Core	No Information	Sacramento SF
SAC07	P359342	275.0	280.0	5.0	4.08	20.40	Chips	No Information	Sacramento SF
SAC09	P359436	360.3	361.2	0.9	6.00	5.40	Core	Gouge	Sacramento SF
SAC12	P359425	307.9	309.8	1.9	2.16	4.10	Core	Gouge	Sacramento SF
SAC12	P359426	309.8	310.6	0.8	8.12	6.50	Core	Sulphide Vein	Sacramento SF
SAC13	P359414	294.7	296.1	1.4	80.10	112.14	Core	Limonite Breccia	Sacramento SF
SAC13	P359415	296.1	297.6	1.5	9.80	14.70	Core	Limonite Breccia	Sacramento SF
SAC13	P359416	297.6	300.0	2.4	2.06	4.94	Core	Lim Breccia	Sacramento SF
SAC15	p359518	295.0	300.0	5.0	2.91	14.55	Chips	No Information	Sacramento SF
SAC16	P359430	95.9	98.0	2.1	18.10	38.01	Core	No Information	Sacramento SF
SAC17	P359736	290.0	295.0	5.0	5.45	27.25	Chips	No Information	Sacramento SF
SAC17	P359737	295.0	300.0	5.0	1.27	6.35	Chips	No Information	Sacramento SF
SAC18	P359743	380.0	385.0	5.0	4.42	22.10	Chips	No Information	Sacramento SF
SAC18	P359744	385.0	390.0	5.0	7.75	38.75	Chips	No Information	Sacramento SF
SAC22	P359979	280.0	285.0	5.0	4.59	22.95	Chips	No Information	Sacramento SF

JORC Code, 2012 Edition – Table 1 report

SECTION 1 SAMPLING TECHNIQUES AND DATA

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information. 	<ul style="list-style-type: none"> A total of 7,390.5 m of drilling in 147 holes comprising 1,229.9 m of core and 4,625.6 m of reverse circulation (RC) chips. Whole NQ core samples were collected for the REY program and half HQ core samples for the C8-16, CRG, SAC, and GL programs. Quarter and half NQ core samples were collected for the C-08-2018 historic hole. Core sample boundaries were defined by changes in lithology, alteration, and mineralization noted in logging. Core samples varied from 0.09 m to 2.44 m and averaged 0.64 m with a median length of 0.61 m. Core remaining after sampling was stored in wax coated cardboard core trays. RC chips were obtained from a 10 cm diameter drilling rod, collected in a cyclone for each 1.5 m interval, passed through a splitter to reduce the sample size to about 6 kg, and then bagged for assaying. A small amount of RC chips were collected separately in chip trays for logging. RC reject samples remaining after sampling were stored for reference.
Drilling techniques	<ul style="list-style-type: none"> Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc). 	<ul style="list-style-type: none"> Drilling comprised diamond coring and reverse circulation (RC) methods. Surface diamond drilling used a Longyear LF90 rig with wireline core barrels, bottom discharge bits, split inner tubes, and HQ or NQ core sizes. Underground diamond drilling used Atlas Copco Diamec U6 and First Drilling UMC02 rigs with wireline core barrels, bottom discharge bits, split inner tubes for the U6 rig, and NQ or HQ core sizes. Surface RC drilling used Multi-Power Products Scout and Discovery II rigs with 10 cm diameter face sampling percussion hammers.
Drill sample recovery	<ul style="list-style-type: none"> Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to 	<ul style="list-style-type: none"> Core was recovered using split inner tubes for all surface holes and about half of the underground holes; each drilled core run was measured for recovered length Core recovery was calculated as a percentage for each drilled interval. Most core was competent with recoveries at or close to 100 % in fresh rock and generally 95 to 100 % in mineralized zones, but could

Criteria	JORC Code explanation	Commentary
	<p><i>preferential loss/gain of fine/coarse material.</i></p>	<p>be lower within fault or gouge zones due to the crumbly nature of the rock.</p> <ul style="list-style-type: none"> • Bottom discharge bits allow the water to bypass the core and minimize erosion of soft materials. Split inner tubes provide better core recovery in soft and/or highly fractured rock, and core is able to be examined with minimal disturbance before placing in trays for permanent storage. • No quantitative analysis of sample weights, sample condition, recovery, or repeatability was done. • No assessment of sample recovery and grade was done.
<p><i>Logging</i></p>	<ul style="list-style-type: none"> • <i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i> • <i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i> • <i>The total length and percentage of the relevant intersections logged.</i> 	<ul style="list-style-type: none"> • Core and RC samples were geologically logged. • Lithology, veining, alteration, mineralization, and weathering were recorded in database tables. • Core trays were photographed dry and wet. • Geotechnical logging was done for rock quality. • Geological logging of core / RC chips is qualitative. • Geotechnical logging of core is quantitative and includes measuring RQD and planar features.
<p><i>Sub-sampling techniques and sample preparation</i></p>	<ul style="list-style-type: none"> • <i>If core, whether cut or sawn and whether quarter, half or all core taken.</i> • <i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i> • <i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i> • <i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i> • <i>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</i> • <i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i> 	<ul style="list-style-type: none"> • Core was cut along the long axis using a diamond saw, half-core was sampled, and half stored for reference. • Sample intervals were marked with a permanent marker in the core trays and sample number tags were attached to each interval. • Samples were placed in sample bags that were labeled with sample numbers using a permanent marker, sample number tags were stapled to bags and/or sample tags were placed inside bags, and sample bags sealed with zip ties. • RC chips were split using a rig-mounted rotary splitter to produce a sample of approximately 6 kg in weight. • The splitter was cleaned at the end of each 1.5 m drill rod to minimize contamination, or as needed.
<p><i>Quality of assay data and laboratory tests</i></p>	<ul style="list-style-type: none"> • <i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i> • <i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations</i> 	<ul style="list-style-type: none"> • New drilling samples were sent to Hazen Research, Golden, Colorado, for sample preparation and assaying. • Historical core samples were sent to ALS Geochemistry, Reno, Nevada. • Samples were dried, weighed, crushed and split to obtain 100 to 150 g, pulverized to

Criteria	JORC Code explanation	Commentary
	<p><i>factors applied and their derivation, etc.</i></p> <ul style="list-style-type: none"> • <i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i> 	<p>90% minus 75 microns, blended on brown Kraft paper, packaged in Kraft bags,</p> <ul style="list-style-type: none"> • 29.17 g subsamples were weighed, and analyzed using a standard fire assay for gold and silver. • Routine QAQC samples were inserted in the sample batches at a rate of 6 % for commercial CRMs and 6 % for BLKs comprising barren granodiorite. • Based on the author's observations and data provided, the author is of the opinion that the sample preparing and gold assaying have been conducted in an appropriate manner, which ensures the final data are representative of the original material sampled in the field.
<p><i>Verification of sampling and assaying</i></p>	<ul style="list-style-type: none"> • <i>The verification of significant intersections by either independent or alternative company personnel.</i> • <i>The use of twinned holes.</i> • <i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i> • <i>Discuss any adjustment to assay data.</i> 	<ul style="list-style-type: none"> • Verification work was conducted by Mr. Dale A. Sketchley, who is independent of the Company. • Crushed and pulverized reject samples were submitted to ALS Reno for gold check assays to compare to the original gold assays from Hazen Research. • Screen metallics and gold particle size distribution assays were compared to the original gold assays to check on variability of results. • Assays were manually compiled and checked against the original laboratory certificates.
<p><i>Location of data points</i></p>	<ul style="list-style-type: none"> • <i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i> • <i>Specification of the grid system used.</i> • <i>Quality and adequacy of topographic control.</i> 	<ul style="list-style-type: none"> • Drill hole collars were surveyed by a Colorado Licensed Professional Surveyor using differential GPS survey equipment. • The positions are accurate to within 10 cm x-y and height (z) to +/- 20 cm. • The holes are surveyed in the Colorado State Plane, UTM zone 12, NAD 1983 coordinate system. • Down hole surveys using a Reflex EZ_TRAC were done on all diamond drill holes.
<p><i>Data spacing and distribution</i></p>	<ul style="list-style-type: none"> • <i>Data spacing for reporting of Exploration Results.</i> • <i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. Whether sample compositing has been applied.</i> 	<ul style="list-style-type: none"> • Drill hole spacing for the REY program is appropriate for inferred resources, and in some locations where holes are closer spaced, for indicated resources. • Drill hole spacing for the SAC, GL, CRG, and C programs is appropriate only for inferred resources.

Criteria	JORC Code explanation	Commentary
<i>Orientation of data in relation to geological structure</i>	<ul style="list-style-type: none"> Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material. 	<ul style="list-style-type: none"> Mineralized structures and veins trend north-northeast at about 30 degrees and dip to the west-northwest at about 60 degrees. Drill holes typically intersected the veins at 40 to 90 degrees, which is roughly equivalent to 65 % to 100 % of the true thicknesses of the veins.
<i>Sample security</i>	<ul style="list-style-type: none"> The measures taken to ensure sample security. 	<ul style="list-style-type: none"> Samples were taken by Company personnel who maintained custody until shipping. Samples were sent by courier or delivered by Company personnel to labs. All samples followed a strict Chain of Custody.
<i>Audits or reviews</i>	<ul style="list-style-type: none"> The results of any audits or reviews of sampling techniques and data. 	<ul style="list-style-type: none"> QAQC procedures, including sampling techniques, were developed by Dale A. Sketchley, M.Sc., P.Geo. of Acuity Geoscience Ltd. Mr. Sketchley visited the project site in late 2016 for 7 days, in late 2017 for 8 days, and in early 2018 for 25 days. Mr. Sketchley has inspected ALS Geochemistry laboratory in Reno, Nevada. Mr. Hollenbeck visited the project site in August 2020 for four days.

SECTION 2 REPORTING OF EXPLORATION RESULTS

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
<i>Mineral tenement and land tenure status</i>	<ul style="list-style-type: none"> Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area. 	<ul style="list-style-type: none"> All claims are 100% owned by Dateline Resources Limited, or a wholly owned subsidiary, and there exists production-based royalties as previously disclosed to ASX.
<i>Exploration done by other parties</i>	<ul style="list-style-type: none"> Acknowledgment and appraisal of exploration by other parties. 	<ul style="list-style-type: none"> All previous work undertaken by other parties is non-JORC compliant.
<i>Geology</i>	<ul style="list-style-type: none"> Deposit type, geological setting and style of mineralisation. 	<ul style="list-style-type: none"> Gold Links Property is underlain by granitic and metamorphic rocks of the Early to Middle Proterozoic age, which are partly overlain by a thin cover of Paleozoic strata. Both the Proterozoic and Paleozoic rocks are intruded by Tertiary rhyolite porphyry dykes and plutons.

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> The property is characterized by multiple, semi-parallel, polymetallic mineralized structures occurring over an area of approximately 4 km by 2 km on the east side of Gold Creek. Individual mineralized structures are characterized by masses of quartz varying from fine to coarse-grained, which pinch and swell along shears resulting in a distinct segmented geometry. Ore shoots are typically 30 to 150 m long with vertical extents of over 100 m, which are more common in areas of structural complexity, splitting, and larger flexures along structures.
<p><i>Drill hole Information</i></p>	<ul style="list-style-type: none"> A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length. If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case. 	<ul style="list-style-type: none"> See Appendix 1 within this report for drill hole configuration information.
<p><i>Data aggregation methods</i></p>	<ul style="list-style-type: none"> In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated. 	<ul style="list-style-type: none"> See Appendix 2 within this report for drill hole significant intersections. Drill hole significant intersections are presented as received from the assaying laboratories.
<p><i>Relationship between mineralisation widths and intercept lengths</i></p>	<ul style="list-style-type: none"> These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known'). 	<ul style="list-style-type: none"> Mineralized structures and veins trend north-northeast at about 30 degrees and dip to the west-northwest at about 60 degrees. Drill holes typically intersected the veins at 40 to 90 degrees, which is roughly equivalent to 65 % to 100 % of the true thicknesses of the veins. Assays are presented as down hole lengths.

Criteria	JORC Code explanation	Commentary
<i>Diagrams</i>	<ul style="list-style-type: none"> • <i>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</i> 	
<i>Balanced reporting</i>	<ul style="list-style-type: none"> • <i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i> 	
<i>Other substantive exploration data</i>	<ul style="list-style-type: none"> • <i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i> 	
<i>Further work</i>	<ul style="list-style-type: none"> • <i>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</i> • <i>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i> 	

SECTION 3 ESTIMATION AND REPORTING OF MINERAL RESOURCES

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database Integrity	<ul style="list-style-type: none"> Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. Data validation procedures used. 	<ul style="list-style-type: none"> Data from core logging up to early 2019 were entered directly into a spreadsheet template with individual tabs for various types of geological data. Manual verification methods were used for data entry. In mid-2019, data was entered directly onsite into dedicated logging software and then transferred to an offsite database. Historical drill hole data were transferred to the offsite database and automated verification methods used. The offsite database was queried to derive data for exporting into required formats for importing into software for checking assay QC, geological modelling, geological interpretation, and resource estimation. Assays were manually compiled and checked against the original laboratory certificates for resource estimation work.
Site Visits	<ul style="list-style-type: none"> Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is the case. 	<ul style="list-style-type: none"> Mr. Sketchley visited the project site in late 2016 for 7 days, in late 2017 for 8 days, and in early 2018 for 25 days. QAQC procedures previously initiated were confirmed and re-emphasized. Mr. Hollenbeck visited the project site in August 2020 for four days.
Geological interpretation	<ul style="list-style-type: none"> Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. Nature of the data used and any assumptions made. The effect, if any, of alternative interpretations on Mineral Resource estimation. The use of geology in guiding and controlling Mineral Resource estimation. The factors affecting continuity both of grade and geology. 	<ul style="list-style-type: none"> The geological model was made using all recent data available, as well as a mixture of historic data types of varying detail and completeness. No alternative geological interpretations were done at this time; refinements to the vein model are planned for future work to enhance detail of vein complexities. The vein shapes crated for the geologic model were the primary constraining volumes for the resource estimations.
Dimensions	<ul style="list-style-type: none"> The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral resource 	<ul style="list-style-type: none"> 9900 Reynolds Decline Zone = 380 x165 x 4 ft Sub-9600 Zone = 450 x 245 x 3 ft Sacramento Zone = 975 x 550 x 5 ft

Criteria	JORC Code explanation	Commentary
<i>Estimation and modelling techniques</i>	<ul style="list-style-type: none"> • <i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i> • <i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i> • <i>The assumptions made regarding recovery of by- products.</i> • <i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i> • <i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i> • <i>Any assumptions behind modelling of selective mining units.</i> • <i>Any assumptions about correlation between variables.</i> • <i>Description of how the geological interpretation was used to control the resource estimates.</i> • <i>Discussion of basis for using or not using grade cutting or capping.</i> • <i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i> 	<ul style="list-style-type: none"> • The use of the Radial Basis Function (RBF) estimator for all mineralized areas was selected due to its flexibility for the varying number of available samples. • Where a larger pool of samples was available in the 9900 area, Ordinary Krige, Inverse Distance, and Nearest Neighbor estimations were done in addition to the RBF estimation for comparative purposes. • Previous estimates or mine production records were not taken into account at this time. • No assumptions were made regarding the recovery of by-products; only gold was estimated at this time. • Deleterious elements were not estimated at this time, pending a more thorough metallurgical study. • The sub-block size of 2x2x2ft was selected to capture as much detail within the veins as possible while keeping the block model a reasonable file size. SMUs were not considered for the block size as it was not intended to be an engineering model. • In addition to using the vein boundaries as mineralization domains, indicator shells were created in Leapfrog Geo software as additional lateral constraints within the vein domains. This was to prevent grade “blow-outs” into areas of minimal drilling data. • Grades were not capped due to the general erratic nature of the veins, and a general cap was deleterious to those areas of expected high-grade. Spatial limitations were set on high-grade samples to limit their influence to a short range adjacent to the sample in question, thereby reducing the overall influence of the high-grade samples while still maintaining some representation of their existence • Block model validation was done visually, as well as through the use of general statistics and histograms for data distribution, along with swath plots in the X, Y, and Z directions comparing composites against block grades.
<i>Moisture</i>	<ul style="list-style-type: none"> • <i>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of</i> • <i>determination of the moisture content.</i> 	<ul style="list-style-type: none"> • The tonnages are estimated based on an assumed dry material weight.

Criteria	JORC Code explanation	Commentary
<i>Cut-off parameters</i>	<ul style="list-style-type: none"> <i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i> 	<ul style="list-style-type: none"> No cut-off grades were used for reporting at this time
<i>Mining factors or assumptions</i>	<ul style="list-style-type: none"> <i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i> 	<ul style="list-style-type: none"> The material is assumed to be an underground mining target. Waste and diluting material has not been quantified or factored into the model for the purposes of this report.
<i>Metallurgical factors or assumptions</i>	<ul style="list-style-type: none"> <i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i> 	<ul style="list-style-type: none"> It was assumed that recoveries will meet 100% of the assayed value. No other metallurgical assumptions were made during the estimation process.
<i>Environmental factors or assumptions</i>	<ul style="list-style-type: none"> <i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i> 	<ul style="list-style-type: none"> No assumptions were made regarding waste and process residue disposal, as waste and residual material was not factored into the model at this time.
<i>Bulk Density</i>	<ul style="list-style-type: none"> <i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i> <i>The bulk density for bulk material must have been measured by methods that</i> 	<ul style="list-style-type: none"> Fifty-three core and rock samples were submitted to Hazen Research for specific gravity determination; twelve were by the stereopycnometer method and forty-one were by the water immersion method. Eight samples were submitted to ALS Geochemistry for specific gravity and bulk

Criteria	JORC Code explanation	Commentary
	<p><i>adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i></p> <ul style="list-style-type: none"> • <i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i> 	<p>density determination by water immersion methods.</p> <ul style="list-style-type: none"> • Water immersion method samples weighed between 0.4 and 1.0 kg; pycnometer samples were less than 100g. • Bulk density measurements were similar to specific gravity measurements as the samples had negligible pore spaces.
<p><i>Classification</i></p>	<ul style="list-style-type: none"> • <i>The basis for the classification of the Mineral Resources into varying confidence categories.</i> • <i>Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i> • <i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i> 	<ul style="list-style-type: none"> • The classification for the Mineral Resources is all Inferred with exception of the 9900 Level ore zone, which has been categorized as Indicated as well as Inferred. • The Indicated material was based on the number of samples used in the estimation, the distance to the nearest sample, and the Krige variance in a given block. • Measured blocks were not assigned due to the lack of QAQC duplicates for those drill holes used in the 9900 estimation. • Overall the estimation results are reasonable for the deposit, and should be considered representative of the identified ore material.
<p><i>Audits or Reviews</i></p>	<ul style="list-style-type: none"> • <i>The results of any audits or reviews of Mineral Resource estimates.</i> 	<ul style="list-style-type: none"> • No audits or reviews have been done at this time.
<p><i>Discussion of relative accuracy/ confidence</i></p>	<ul style="list-style-type: none"> • <i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i> • <i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i> • <i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i> 	<ul style="list-style-type: none"> • The relative accuracy should be considered moderate to high for the 9900 mineralized zone, and low for the sub-9600 and Sacramento zones, which is reflected in their respective categorizations. • The visual and statistical analyses of the estimations are the basis for the confidence levels. More data is required to bring up the level of confidence in all locations. • Modern production data is not currently available for any of the zones from which to draw conclusions around accuracy or confidence.