

Far West Development On Track To Increase Thalanga Production

Highlights:

- Decline has advanced to 90m vertical depth and ore production is scheduled to commence in Q1 2019. Ore from Far West will augment West 45 ore, and increase production at Thalanga
- Recent drilling has indicated potential to extend upper levels of Far West. Highlights include:
 - TH854: 13.45m @ 13.7% Zn Eq. from 193.40m down hole including 4.20m @ 31.1% Zn Eq. from 193.40m down hole plus 6.12m @ 11.8% Zn Eq. from 218.90m down hole
 - TH844: 3.30m @ 10.5% Zn Eq. from 42.00m down hole
 - TH845: 4.95m @ 19.2% Zn Eq. from 49.35m down hole
 - TH855: 4.00m @ 11.3% Zn Eq. from 230.00m down hole
- Far West has a current JORC Reserve of 1.5Mt @ 12.0% Zinc Equivalent and a mine life to 2025

Figure 1 Far West Development



Red River Managing Director Mel Palancian said: "The Far West deposit will extend production at Thalanga Operations for at least the next five years. Production from Far West is on track to start in Q1 2019 and we are planning further drilling to target extensions of the high-grade mineralisation in early 2019"



Far West Development Progress

To date, over 660m of lateral development has been completed in Far West, including 552m of total decline development. The decline is currently at 90m vertical depth and at the 920 ore drive cross-cut access.

The raise-borer has been mobilised to site to commence the Far West return air rise and second means of egress with completion and ventilation fan installation expected in the March quarter 2019.



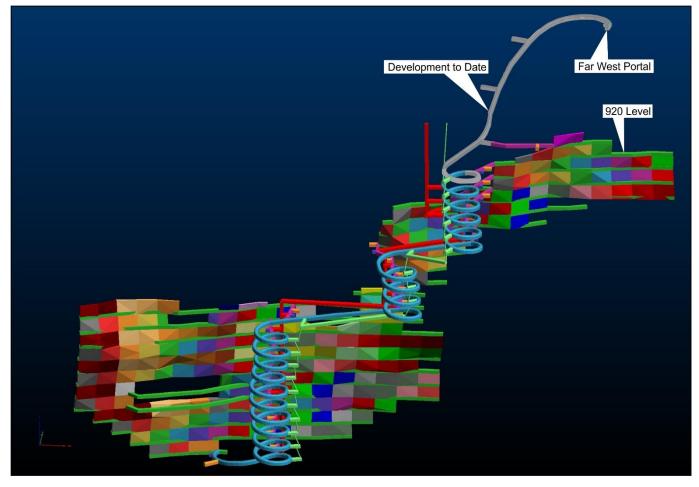




Figure 3 Far West Return Air Rise Site Preparation



Figure 4 Far West Return Air Rise Site Preparation (Raise Borer located on Emergency Egress Pad)





1. Far West Resource Extension Drilling Activities

The current Far West drilling program has been completed, with the drill rig stood down for the wet season. This program consisted of 11 holes completed for a total of 1,568 metres. The program objective was to target extensions to the Far West mineralisation outside of the currently designed stoping blocks. The program was a success, with the following material intersections returned (Table 1).

Hole ID	From (m)	To (m)	Intersection (m) ⁽¹⁾	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)	Zn Eq. (%)
TH841	102.40	104.35	1.95	1.4	0.0	0.4	0.1	6	5.3
TH842	90.40	92.40	2.00	0.8	0.3	0.8	0.1	32	4.5
TH843	143.00	146.00	3.00	0.1	0.2	0.8	0.0	5	1.4
TH844	42.00	45.30	3.30 ⁽²⁾	0.9	2.9	8.7	0.5	68	10.5(3)
TH845	49.35	54.30	4.95	2.0	3.8	7.0	0.4	77	19.2
TH854	193.40	206.85	13.45	1.3	2.0	6.3	0.2	47	13.7
inc.	193.40	197.60	4.20	0.9	6.1	19.6	0.3	118	31.1
and	218.90	225.02	6.12	3.3	0.0	0.6	0.1	6	11.8
TH855	230.00	234.00	4.00	2.8	0.1	1.4	0.1	12	11.3
	ole width								

Table 1 Far West Drilling Program Material Assay Summary, Thalanga Operation

2. Includes 0.3m of core loss (43.20m to 45.30m). Core loss assigned zero grade in assay calculation

3. Zn Eq. calculation based on Transitional Calculation Factors

Figure 5 Far West Long Section

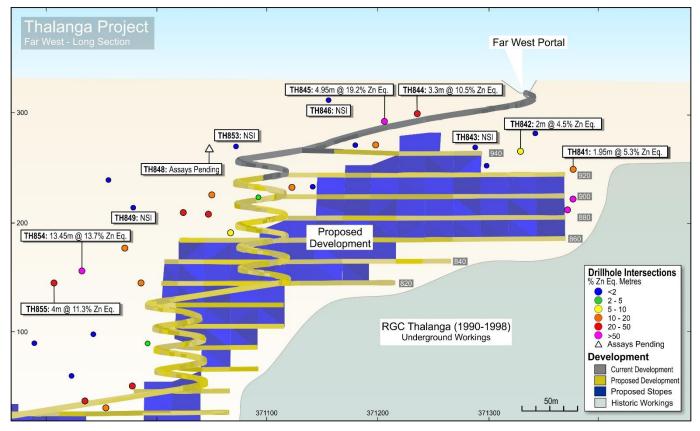




Figure 6 TH854 (4.20m @ 0.9% Cu, 6.1% Pb, 19.6% Zn, 0.3 g/t Au & 118 g/t Ag (31.1% Zn Eq.) from 193.40m to 197.60m down hole)



Table 2 Far West Drilling Program Drillhole Details, Thalanga Operation

Hole ID	Dip	Final Depth	Azi (MGA)	East (MGA)	North (MGA)	RL (MGA)	Lease ID	Hole Status
TH841	-51	113.07	34.8	371340	7750496	329	ML1531	Complete
TH842	-45	133.6	41.8	371286	7750517	329	ML1531	Complete
TH843	-45	157.7	2.8	371286	7750517	330	ML1531	Complete
TH844	-45	103.5	15.8	371229	7750548	330	ML1531	Complete
TH845	-45	78.3	14.8	371198	7750548	330	ML1531	Complete
TH846	-45	33.3	16.8	371152	7750570	331	ML1531	Complete
TH848	-55	124.8	13.8	371035	7750581	333	ML1531	Assays Pending
TH849	-58	181.9	12.8	370962	7750574	334	ML1531	Complete
TH853	-46	148.7	16.8	371056	7750552	332	ML1531	Complete
TH854	-61	241.9	5.8	370926	7750568	334	ML1531	Complete
TH855	-58	251	352.8	370927	7750568	335	ML1531	Complete

The drilling results received indicate the potential to extend planned ore drives and possibly add additional level(s) above. These results also confirm that the orebody is not closed off and further drilling is planned to start after the wet season in early 2019 to target further extensions of the high grade mineralisation in TH854 and TH855.



Table 3 Far West Ore Reserve (>6 % Zn Eq.)

Reserve Class	Tonnage (kt)	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)	Zn Eq. (%)
Proved	48	1.3	1.0	4.4	0.0	27	10.1
Probable	1,486	1.3	1.6	5.0	0.2	46	12.1
Total	1,534	1.3	1.6	5.0	0.2	45	12.0

Source: Far West Ore Reserve and Mineral Resource Update Extends Thalanga Mine Life (RVR ASX Release, 21 November 2017) Tonnages and grades are rounded. Discrepancies in totals may exist due to rounding.

Zinc equivalent (Zn Eq.) has been calculated using the metal selling prices, recoveries and other assumptions contained in Appendices of this announcement. It is Red River's opinion that all elements included in the metal equivalent calculation have a reasonable potential to be recovered and sold. Proved and Probable Reserves are included within (and not in addition to) the Thalanga Far West Mineral Resource estimate

Table 4 Far West Mineral Resource (>5% Zn Eq.)

Resource Class	Tonnage (kt)	Cu (%)	Pb (%)	Zn (%)	Au (g/t)	Ag (g/t)	Zn Eq. (%)
Measured	52	1.4	1.3	5.3	0.0	32	12.0
Indicated	1,491	1.7	2.2	6.6	0.2	61	15.7
Measured + Indicated	1,543	1.7	2.1	6.6	0.2	60	15.6
Inferred	150	1.4	2.3	6.5	0.1	53	14.6
Total	1,693	1.6	2.1	6.5	0.2	59	15.5

Source: Updated Resource Estimation of the Thalanga Far West Deposit (Mining One Consultants, 9 November 2017).

Tonnages and grades are rounded. Discrepancies in totals may exist due to rounding.

Zinc equivalent (Zn Eq.) has been calculated using the metal selling prices, recoveries and other assumptions contained in Appendices of this announcement. It is Red River's opinion that all elements included in the metal equivalent calculation have a reasonable potential to be recovered and sold.



About Red River Resources (ASX: RVR)

RVR is the leading ASX base metal producer, with its key asset being the Thalanga Operation in Northern Queensland. RVR commenced copper, lead and zinc concentrate production at the Thalanga Operation in September 2017 and RVR is focused on maximising returns from the Operation by increasing plant throughput and extending mine life through increasing Mineral Resources and Ore Reserves at deposits currently in the mine plan (West 45, Far West and Waterloo), by potentially converting Mineral Resources into Ore Reserves at Liontown and Orient and by continuing to aggressively explore our growing pipeline of high quality targets within the surrounding area.

On behalf of the Board,

Mel Palancian Managing Director Red River Resources Limited

For further information please visit Red River's website or contact:

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COMPETENT PERSONS STATEMENT

Exploration Results

The information in this report that relates to Exploration Results is based on information compiled by Mr Steven Harper who is a member of The Australasian Institute of Mining and Metallurgy, and a full time employee of Red River Resources Ltd., and who has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activities being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting Exploration Results, Mineral Resources and Ore Reserves' (JORC Code).

Mr Harper consents to the inclusion in this report of the matters based on the information in the form and context in which it appears.

Far West Mineral Resource

The information in this report that relates to the estimation and reporting of the Thalanga Far West Mineral Resource is based on and fairly represents, information and supporting documentation compiled by Mr Stuart Hutchin who is a Member of The Australasian Institute of Mining and Metallurgy, Member of the Australian Institute of Geoscientists and a full time employee of Mining One Consultants Pty Ltd.

Mr Hutchin has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'.

Mr Hutchin consents to the inclusion in the report of the matters based on the information in the form and context in which it appears. The information in this report that relates to database compilation, geological interpretation and mineralisation wireframing, project parameters and costs and overall supervision and direction of the Thalanga Far West Mineral Resource estimation is based on and fairly represents, information and supporting documentation compiled under the overall supervision and direction of Mr Hutchin.

Far West Ore Reserve

The information in this report that relates to the estimation and reporting of the Far West Ore Reserve is based on and fairly represents, information and supporting documentation compiled by Mr Mel Palancian who is a Member of The Australasian Institute of Mining and Metallurgy and a full time employee of Red River Resources.

Mr Palancian has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'.

Mr Palancian consents to the inclusion in the report of the matters based on the information in the form and context in which it appears.



Zinc Equivalent Calculation

The net smelter return zinc equivalent (Zn Eq.) calculation adjusts individual grades for all metals included in the metal equivalent calculation applying the following modifying factors: metallurgical recoveries, payability factors (concentrate treatment charges, refining charges, metal payment terms, net smelter return royalties and logistic costs) and metal prices in generating a zinc equivalent value for copper (Cu), lead (Pb), zinc (Zn), gold (Au) and silver (Ag).

Red River has selected to report on a zinc equivalent basis, as zinc is the metal that contributes the most to the net smelter return zinc equivalent (Zn Eq.) calculation. It is the view of Red River Resources that all the metals used in the Zn Eq. formula are expected to be recovered and sold.

Where:

Metallurgical Recoveries are derived from historical metallurgical recoveries from test work carried out the Thalanga deposit. The Far West deposit is related to and of a similar style of mineralisation to the Thalanga Operations and it is appropriate to apply similar recoveries. The Metallurgical Recovery for each metal is shown below in Table 1.

Metal Prices and Foreign Exchange assumptions are set as per internal Red River price forecasts and are shown below in Table 1.

Metal	Metallurgical Recoveries (Fresh Sulphide)	Metallurgical Recoveries (Transitional Sulphide)	Price
Copper	80%	58%	US\$3.00/lb
Lead	75%	0%	US\$0.90/lb
Zinc	89%	76%	US\$1.00/lb
Gold	47%	30%	US\$1,200/oz
Silver	65%	58%	US\$17.00/oz
FX Rate: A\$0.75	:US\$1		

Table 1 Metallurgical Recoveries and Metal Prices

Payable Metal Factors are calculated for each metal and make allowance for concentrate treatment charges, transport losses, refining charges, metal payment terms and logistic costs. It is the view of Red River that three separate saleable base metal concentrates will be produced at Thalanga. Payable metal factors are detailed below in Table 2.

Table 2 Payable Metal Factors

Metal	Payable Metal Factor
Copper	Copper concentrate treatment charges, copper metal refining charges copper metal payment terms (in copper concentrate), logistic costs and net smelter return royalties
Lead	Lead concentrate treatment charges, lead metal payment terms (in lead concentrate), logistic costs and net smelter return royalties
Zinc	Zinc concentrate treatment charges, zinc metal payment terms (in zinc concentrate), logistic costs and net smelter return royalties
Gold	Gold metal payment terms (in copper and lead concentrates), gold refining charges and net smelter return royalties
Silver	Silver metal payment terms (in copper, lead and zinc concentrates), silver refining charges and net smelter return royalties



The zinc equivalent grade is calculated as per the following formula:

Fresh Sulphide Zn Eq. =	(Zn%*1.0) + (Cu%*3.3) + (Pb%*0.9) + (Au ppm*0.5) + (Ag ppm*0.025)
Transitional Sulphide Zn Eq. =	(Zn%*0.84) + (Cu%*2.5) + (Pb%*0.0) + (Au ppm*0.4) + (Ag ppm*0.01)

The following metal equivalent factors used in the zinc equivalent grade calculation has been derived from metal price x Metallurgical Recovery x Payable Metal Factor and have then been adjusted relative to zinc (where zinc metal equivalent factor = 1).

Table 3 Metal Equivalent Factors

Metal	Copper	Lead	Zinc	Gold	Silver
Metal Equivalent Factor (Fresh)	3.3	0.9	1.0	0.5	0.025
Metal Equivalent Factor (Transitional)	2.5	0.0	0.84	0.4	0.01



APPENDIX 1 – DRILLHOLE ASSAY DETAILS

Hole ID	From (m)	To (m)	Int (m) ⁽¹⁾	Cu%	Pb%	Zn%	Au g/t	Ag g/t	Zn Eq. %
TH841	99.38	99.78	0.40	0.0	0.0	0.1	0.0	1	0.2
TH841	99.78	100.50	0.72	0.0	0.0	0.1	0.0	0	0.1
TH841	100.50	101.00	0.50	0.0	0.0	0.1	0.0	0	0.1
TH841	101.00	101.90	0.90	0.1	0.0	0.2	0.0	1	0.5
TH841	101.90	102.40	0.50	0.1	0.0	0.2	0.0	1	0.5
TH841	102.40	103.30	0.90	0.6	0.0	0.2	0.0	5	2.5
TH841	103.30	103.80	0.50	3.8	0.0	0.9	0.3	10	13.7
TH841	103.80	104.35	0.55	0.5	0.1	0.2	0.0	5	2.1
TH841	104.35	104.70	0.35	0.1	0.0	0.0	0.0	2	0.5
TH841	104.70	105.50	0.80	0.0	0.0	0.0	0.0	0	0.1
TH841	105.50	106.35	0.85	0.0	0.0	0.0	0.0	0	0.0
TH841	106.35	107.00	0.65	0.0	0.0	0.0	0.0	1	0.1
TH841	107.00	108.00	1.00	0.0	0.0	0.2	0.0	1	0.3
TH841	108.00	108.60	0.60	0.0	0.1	0.2	0.0	2	0.3
TH842	90.00	90.40	0.40	0.1	0.4	0.7	0.0	5	1.6
TH842	90.40	91.30	0.90	1.0	0.6	1.0	0.1	59	6.5
TH842	91.30	91.57	0.27	0.3	0.2	0.4	0.1	22	2.4
TH842	91.57	92.40	0.83	0.7	0.0	0.6	0.1	6	3.0
TH842	92.40	93.00	0.60	0.0	0.0	0.0	0.0	0	0.1
TH842	93.00	94.00	1.00	0.0	0.0	0.0	0.0	0	0.0
TH842	94.00	95.00	1.00	0.0	0.0	0.0	0.0	0	0.0
TH842	95.00	95.70	0.70	0.0	0.0	0.0	0.0	0	0.1
TH842	95.7	97.00	1.3	0.0	0.0	0.0	0.0	1	0.1
TH843	140.00	141.00	1.00	0.0	0.1	0.3	0.0	2	0.5
TH843	141.00	142.00	1.00	0.0	0.1	0.3	0.0	4	0.6
TH843	142.00	143.00	1.00	0.0	0.1	0.2	0.0	2	0.4
TH843	143.00	144.00	1.00	0.1	0.2	0.8	0.0	4	1.3
TH843	144.00	145.00	1.00	0.1	0.3	0.7	0.0	6	1.4
TH843	145.00	146.00	1.00	0.1	0.2	0.8	0.0	4	1.4
TH843	146.00	147.00	1.00	0.0	0.1	0.4	0.0	2	0.6
1110-15	147.00	148.00	1.00	0.1	0.2	0.7	0.0	3	1.2

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Hole ID	From (m)	To (m)	Int (m) ⁽¹⁾	Cu%	Pb%	Zn%	Au g/t	Ag g/t	Zn Eq. % ⁽²⁾
TH844	33.50	34.50	1.00	0.0	0.0	0.1	0.0	1	0.1
TH844	34.50	35.40	0.90	0.0	0.0	0.3	0.0	2	0.3
TH844	35.40	36.10	0.70	0.1	0.1	0.2	0.1	40	0.8
TH844	36.10	36.80	0.70	0.0	0.1	0.2	0.0	16	0.4
TH844	36.80	37.20	0.40						core loss
TH844	37.20	37.80	0.60	0.1	1.9	2.2	0.2	19	2.4
TH844	37.80	38.70	0.90	0.2	5.6	9.6	0.2	87	9.6
TH844	38.70	39.50	0.80	0.5	4.7	7.5	0.4	97	8.6
TH844	39.50	40.00	0.50	0.3	1.4	1.6	0.1	34	2.4
TH844	40.00	40.30	0.30						core loss
TH844	40.30	40.80	0.50	0.2	0.7	3.2	0.3	81	4.1
TH844	40.80	41.40	0.60	0.2	0.7	1.3	0.1	58	2.3
TH844	41.40	42.00	0.60	0.6	4.1	5.5	0.3	120	7.4
TH844	42.00	42.70	0.70	0.5	4.1	9.4	0.5	108	10.4
TH844	42.70	43.20	0.50	0.8	3.8	8.5	0.4	77	10.0
TH844	43.20	43.50	0.30						core loss
TH844	43.50	44.00	0.50	1.3	2.2	9.7	1.0	103	12.7
TH844	44.00	44.50	0.50	0.6	1.4	8.3	0.1	26	8.9
TH844	44.50	45.30	0.80	1.9	3.9	11.0	0.6	57	14.7
TH844	45.30	45.90	0.60	0.8	0.3	0.8	0.1	10	2.7
TH844	45.90	46.30	0.40						core loss
TH844	46.30	47.10	0.80	0.1	0.0	0.4	0.0	2	0.7
TH844	47.10	48.00	0.90	0.3	1.0	0.1	0.1	61	1.5
TH844	48.00	49.00	1.00	0.2	0.7	0.6	0.1	73	1.8
TH844	49.00	49.70	0.70	0.1	1.4	1.8	0.1	46	2.4
TH844	49.70	50.50	0.80	0.1	0.6	0.9	0.1	23	1.2
TH844	50.50	51.00	0.50	0.0	0.2	0.3	0.0	8	0.4
TH844	51.00	52.00	1.00	0.1	0.2	0.5	0.0	13	0.8
TH844	52.00	53.00	1.00	0.0	0.0	0.1	0.0	2	0.1
TH844	53.00	54.00	1.00	0.0	0.1	0.3	0.0	5	0.4
1. Downhole width									
2. Zn Eq. calculation	based on Trans	tional Calculatio	n						



16.00			Pb%	Zn%	Au g/t	Ag g/t	Zn Eq. %
	1.00	0.0	0.0	0.1	0.0	1	0.2
17.00	1.00	0.0	0.0	0.1	0.0	1	0.1
18.00	1.00	0.0	0.0	0.4	0.0	5	0.5
18.65	0.65	0.0	0.0	0.4	0.0	5	0.6
19.35	0.70	0.1	0.0	0.2	0.0	3	0.5
50.00	0.65	1.6	12.2	15.0	0.4	173	35.7
50.60	0.60	1.4	5.4	11.4	0.4	94	23.4
51.30	0.70	1.1	1.2	6.7	0.6	35	12.4
51.85	0.55	1.5	1.2	1.6	0.3	39	8.8
52.60	0.75	7.0	6.0	9.3	1.0	175	42.8
53.00	0.40	1.0	0.9	4.4	0.2	29	9.3
53.70	0.70	0.8	0.0	1.1	0.1	8	4.0
54.30	0.60	0.5	1.9	5.4	0.2	28	9.5
55.20	0.90	0.0	0.1	0.2	0.0	3	0.4
56.10	0.90	0.0	0.0	0.1	0.0	1	0.2
57.05	0.95	0.0	0.0	0.1	0.0	7	0.3
58.00	0.95	0.0	0.0	0.0	0.0	1	0.1
228.00	1.00	0.1	0.4	0.8	0.0	3	1.7
228.85	0.85	0.1	0.1	0.2	0.0	2	0.6
229.50	0.65	0.4	0.0	0.1	0.1	1	1.3
230.00	0.50	0.9	0.0	0.1	0.0	2	3.2
231.00	1.00	1.3	0.0	0.2	0.1	4	4.6
231.50	0.50	1.4	0.0	0.2	0.1	7	5.0
232.30	0.80	10.7	0.0	6.0	0.2	21	41.8
232.90	0.60	0.1	0.0	0.0	0.0	1	0.2
233.47	0.57	0.0	0.0	0.0	0.0	1	0.2
234.00	0.53	1.6	0.8	1.4	0.2	42	8.5
234.50	0.50	0.6	0.0	0.1	0.0	4	2.0
235.00	0.50	0.0	0.0	0.0	0.0	1	0.1
236.00	1.00	0.0	0.0	0.0	0.0	1	0.1
)	35.00	35.00 0.50	35.00 0.50 0.0	35.00 0.50 0.0 0.0	35.00 0.50 0.0 0.0 0.0	35.00 0.50 0.0 0.0 0.0 0.0	35.00 0.50 0.0 0.0 0.0 0.0 1



Hole ID	From (m)	To (m)	Int (m) ⁽¹⁾	Cu%	Pb%	Zn%	Au g/t	Ag g/t	Zn Eq. %
TH854	189.00	190.00	1.00	0.0	0.0	0.0	0.0	1	0.2
TH854	190.00	191.00	1.00	0.0	0.0	0.0	0.0	0	0.0
TH854	191.00	192.10	1.10	0.0	0.0	0.0	0.0	0	0.1
TH854	192.10	193.40	1.30	0.2	0.1	0.2	0.0	8	1.3
TH854	193.40	194.32	0.92	1.3	5.7	8.2	0.1	95	20.0
TH854	194.32	195.20	0.88	0.6	6.5	18.0	0.2	82	27.8
TH854	195.20	196.40	1.20	1.2	9.2	19.4	0.3	178	36.1
TH854	196.40	197.60	1.20	0.5	3.0	29.7	0.5	104	37.0
TH854	197.60	198.60	1.00	1.8	0.7	1.5	0.3	70	9.8
TH854	198.60	199.60	1.00	1.5	0.1	0.2	0.1	13	5.6
TH854	199.60	200.55	0.95	1.7	0.0	0.1	0.1	9	6.0
TH854	200.55	201.50	0.95	0.0	0.0	0.0	0.0	1	0.2
TH854	201.50	202.00	0.50	0.3	0.0	0.0	0.1	3	1.3
TH854	202.00	202.75	0.75	2.0	0.0	0.1	0.2	7	7.0
TH854	202.75	203.50	0.75	1.4	0.1	0.1	0.2	16	5.2
TH854	203.50	204.25	0.75	0.8	0.0	0.1	0.0	4	2.7
TH854	204.25	205.00	0.75	2.9	0.0	0.1	0.0	7	9.9
TH854	205.00	206.00	1.00	0.3	0.0	0.0	0.0	2	1.1
TH854	206.00	206.85	0.85	4.0	0.1	0.2	0.6	13	14.1
TH854	206.85	208.10	1.25	0.7	0.0	0.1	0.1	3	2.6
TH854	208.10	209.00	0.90	0.2	0.0	0.1	0.0	2	0.7
TH854	209.00	210.00	1.00	0.0	0.0	0.1	0.0	1	0.3
TH854	210.00	211.00	1.00	0.0	0.0	0.0	0.0	1	0.1
TH854	211.00	212.00	1.00	0.0	0.1	0.3	0.0	2	0.4
TH854	212.00	212.33	0.33	0.0	0.0	0.0	0.0	0	0.1
TH854	212.33	212.95	0.62	0.1	0.0	0.3	0.0	1	0.7
TH854	212.95	214.00	1.05	0.2	0.4	0.3	0.0	14	1.9
TH854	214.00	215.00	1.00	1.0	0.2	0.1	0.0	14	3.9
TH854	215.00	216.00	1.00	0.0	0.0	0.1	0.0	1	0.1
TH854	216.00	217.00	1.00	0.0	0.0	0.1	0.0	0	0.1
TH854	217.00	218.33	1.33	0.0	0.0	0.0	0.0	0	0.1
TH854	218.33	218.90	0.57	0.5	0.1	0.4	0.0	4	2.3
TH854	218.90	219.40	0.50	4.2	0.0	0.6	0.2	6	14.7
TH854	219.40	220.00	0.60	3.8	0.0	2.8	0.1	6	15.7
TH854	220.00	221.00	1.00	4.6	0.0	0.5	0.1	7	16.1
TH854	221.00	222.00	1.00	2.1	0.0	0.4	0.1	5	7.4
TH854	222.00	223.00	1.00	2.2	0.0	0.3	0.1	4	7.8
TH854	223.00	224.00	1.00	4.7	0.0	0.4	0.1	8	16.2
TH854	224.00	225.02	1.02	2.2	0.0	0.2	0.1	7	7.6
TH854	225.02	225.55	0.53	0.0	0.0	0.0	0.0	0	0.1
TH854	225.55	226.90	1.35	0.3	0.0	0.0	0.0	2	1.1
TH854	226.90	228.00	1.10	0.0	0.1	0.0	0.0	2	0.2
TH854	228.00	229.20	1.20	0.0	0.0	0.0	0.0	0	0.1
TH854	229.20	229.90	0.70	0.1	0.0	0.1	0.0	1	0.5
TH854	229.90	230.50	0.60	0.0	0.0	0.0	0.0	0	0.0
TH854	230.50	231.60	1.10	0.0	0.0	0.0	0.0	0	0.1
TH854	231.60	232.63	1.03	0.7	0.1	0.2	0.0	4	2.7
TH854	232.63	233.98	1.35	0.0	0.0	0.1	0.0	2	0.3
TH854	233.98	235.00	1.02	0.1	0.0	0.0	0.0	1	0.5
1. Downhole width									



JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	 Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information. 	 Diamond drilling was used to obtain core samples Samples consist of half NQ2 drill core Sample intervals were selected by company geologists based on visual mineralisation Intervals ranged from 0.5 to 1.45m based on geological boundaries Samples were sawn if half using an onsite core saw and sent to Intertek Genalysis laboratories Townsville. Samples were crushed to sub 6mm, split and pulverised to sub 75µm in order to produce a representative sub-sample for analysis. Analysis consisted of a four acid digest and Inductively Coupled Plasma Optical Emission Spectrometry (ICP-OES) for the following elements; Ag, As, Ba, Bi, Ca, Cu, Fe, K, Mg, Mn, Na, Pb, S, Sb, Ti, Zn, & Zr. A selection of samples was also assayed for Au using a 30g Fire Assay technique
Drilling techniques	• Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	 Drilling techniques consist of; HQ3 diamond core drilling until in competent ground typically from 8 to 18m down hole NQ2 diamond core drilling for the remainder of the drill holes.
Drill sample recovery	 Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material. 	 Core is measured every meter with recovery and RQD taken over the meter interval Sample recovery is measured and recorded by company trained geology technicians and geologists Any issues with recovery is always checked against drillers run sheet. Good ground conditions have been encountered to date
Logging	• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining	 Holes are logged to a level of detail that will support mineral resource estimation. Qualitative logging includes lithology, alteration, structures and textures

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Criteria	JORC Code explanation	Commentary
	 studies and metallurgical studies. Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. The total length and percentage of the relevant intersections logged. 	 Quantitative logging includes sulphide and gangue mineral percentages All drill core was photographed All drill holes have been logged in full
Sub- sampling techniques and sample preparation	 If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. Whether sample sizes are appropriate to the grain size of the material being sampled. 	 Core was sawn and half core sent for analysis Sample preparation is industry standard, occurring at an independent commercial laboratory Samples were crushed to sub 6mm, split and pulverised to sub 75µm in order to produce a representative sub-sample for analysis Laboratory certified standards were used in each sample batch The sample sizes are considered to be appropriate to correctly represent the mineralisation style
Quality of assay data and laboratory tests	 The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established. 	 The assay methods employed are considered appropriate for near total digestion Laboratory certified standards were used in each sample batch Certified standards returned results within an acceptable range
Verification of sampling and assaying	 The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes. Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. Discuss any adjustment to assay data. 	 Laboratory results are reviewed by Company geologists and laboratory technicians
Location of data points	 Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. 	 Collars surveyed by Company surveyor Down hole surveys conducted with magnetic multi- shot digital camera Coordinate system used is MGA94 Zone 55 Topographic control is based on a detailed 3D Digital



Criteria	JORC Code explanation	Commentary
	 Specification of the grid system used. Quality and adequacy of topographic control. 	Elevation Model
Data spacing and distribution	 Data spacing for reporting of Exploration Results. Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. Whether sample compositing has been applied. 	 The drilling has been designed on approximately 40m x 40m spacing This data spacing and distribution is sufficient to establish a degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedures applied. No sample compositing has been applied
Orientation of data in relation to geological structure	 Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material. 	 Drill holes are orientated perpendicular to the perceived strike of the host lithologies Drill holes are drilled at a dip based on logistics and dip of anomaly to be tested The orientation of the drilling is designed to not bias sampling
Sample security	• The measures taken to ensure sample security.	• Samples have been overseen by company geologists during transport from site to Intertek Genalysis laboratories, Townsville.
Audits or reviews	 The results of any audits or reviews of sampling techniques and data. 	 No audits or reviews have been carried out at this point



Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	 Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area. 	 The drilling was conducted on Mining Lease ML1531 ML1531 is held by Cromarty Pty Ltd. (a wholly owned subsidiary of Red River Resources) and form part of Red River's Thalanga Zinc Project No Native Title exists over ML1531 The Mining Leases are in good standing
Exploration done by other parties	• Acknowledgment and appraisal of exploration by other parties.	Historic Exploration was carried out by PanContinental Mining & RGC Exploration. This included drilling and geophysics
Geology	• Deposit type, geological setting and style of mineralisation.	 The exploration model is Volcanic Hosted Massive Sulphide (VHMS) base metal mineralisation The regional geological setting is the Mt Windsor Volcanic Sub-province, consisting of Cambro- Ordovician marine volcanic and volcano- sedimentary sequences
Drill hole Information	 A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes, including, easting and northing, elevation or RL, dip and azimuth, down hole length, interception depth and hole length. If the exclusion of this information is justified the Competent Person should clearly explain why this is the case. 	 See Table 3 – Drill Hole Details See Appendix 1 – Assay Details
Data aggregation methods	 In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated. 	 Interval length weighted assay results are reported Significant Intercepts are chosen based on the context of the results, for example significant intercepts relating to resource definition are generally > 5% Zn Equivalents. Refer to Appendix 1 for metal equivalent calculation methodology



Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	 These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known'). 	 The mineralisation is interpreted to be steeply dipping. Drill holes have been angled to intercept the mineralisation as close to perpendicular as possible. Down hole intercepts are reported. True widths are likely to be 60-70% of the down hole widths.
Diagrams	 Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plans and sections. 	Refer to plans and sections within report
Balanced reporting	• Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	 The accompanying document is considered to represent a balanced report
Other substantive exploration data	• Other exploration data, if meaningful and material, should be reported.	All meaningful and material data is reported
Further work	• The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).	 Further drilling is planned based on the results of this current program