Consolidated Tin Mines Limited

ANNOUNCEMENT

11 June 2014

ASX/MEDIA RELEASE

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Snapshot:

Current CSD Share Price: **$0.056**

Current LME Tin Price: **US$23,130**

Detailed information at
www.csdtin.com.au

Final assay results from large scale drill program at Gillian Deposit at Mt Garnet Tin Project

Key points:

- Consolidated Tin completed a 6,481 metre drill program at Gillian deposit as part of the Mt Garnet Tin Project
- Results from this program will be included in a JORC Resource Review as part of the Gillian Deposit DFS
- Final results from this drill program have now been received and include the final 25 reverse circulation holes and 12 diamond core holes. Highlight results include:

Highlight intersection results

HD670	**76.0 metres downhole**	**7.8m**	**@ 0.99% Sn**
HD671	**107.7 metres downhole**	**5.1m**	**@ 0.84% Sn**
HD672	**90.6 metres downhole**	**11.0m**	**@ 0.89% Sn**
HD673	**104.2 metres downhole**	**23.9m**	**@ 1.05% Sn**
HD675	**128.8 metres downhole**	**7.7m**	**@ 0.98% Sn**
HD703	**113.6 metres downhole**	**6.4m**	**@ 0.90% Sn**
HD705	**88.1 metres downhole**	**10.6m**	**@ 0.72% Sn**
H662	**43.0 metres downhole**	**6.0m**	**@ 0.83% Sn**
H662	**53.0 metres downhole**	**5.0m**	**@ 0.75% Sn**
H678	**43.0 metres downhole**	**12.0m**	**@ 0.94% Sn**

ASX CODE: CSD

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ABOUT CSD

Consolidated Tin Mines Limited is an Australian Listed tin focused company developing a large scale tin project at Mt Garnet in the lower Herberton Tinfield in north Queensland

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CAPITAL STRUCTURE

Snow Peak	16.3%
Ralph De Lacey	7.3%
Beacon Minerals	6.6%
Geocrystal	4.0%
John Sainsbury	3.5%

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OBJECTIVE

To become Australia's premier tin producing company

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STRATEGY

To develop and establish tin production by end 2014 and focus on increasing mine life and production profile by developing other tin production opportunities within the broader Mt Garnet Tin Project area

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Drilling Program Overview

Australian tin exploration and development company, Consolidated Tin Mines Limited (**ASX:CSD**) ("CSD" or "the Company") is pleased to announce final assay results from the final 37 holes from the drilling on the Gillian deposit within the Mt Garnet Tin Project in North Queensland (see Attachment 1). The first stage results from this drill program were released in the ASX announcement on 17 December 2013.

The drill program consisted of a total of 6,481 metres, with the final stage completed in the first quarter 2014. The total drill program comprised of:

- Resource drilling – 4,240 metres reverse circulation (RC) and 954.1 metres diamond core (DC)
- Metallurgical drilling – 202.4 metres DC
- Geotechnical drilling – 1,087 metres DC

The drill program was designed to add further confidence to the Gillian JORC Resource released in June 2013 (Attachment 2) with the majority being infill drilling. A JORC Resource review is underway with completion expected mid-year.

The final stage of the drilling targeted geotechnical and hydro-geological data for mine pit design and optimisation. Test results from geotechnical samples have been provided to geotechnical consultants for evaluation to assist in the design of the deposit's open cut pit and optimise the production schedule. Drill samples also provided a representative run-of-mine ore body sample for final flotation and reduction roast/tin fuming pilot test work.

Final Assay Results

The final assay results presented here are from the final 25 reverse circulation holes and 12 diamond core holes.

The latest drilling was an infill drill program which confirmed increased confidence in the resource and the structures targeted.

The Company plans to develop this project into a significant hard rock open pit tin mining operation. The Company's current priority is to complete the Definitive Feasibility Study (DFS) for the Gillian deposit.

Gillian will be the first deposit to be mined at the Mt Garnet Tin Project with the first processing of tin ore expected in 2015.

Metallurgical Testwork Update

The Company completed commissioning a pilot scale trial reduction roasting/tin fuming plant at the Ansac facility at Bunbury, Western Australia, in mid-May 2014. This commissioning phase provided preliminary technical information for processing the Gillian ore, and following some modifications to the Ansac plant, further trials will follow in June/July to develop additional technical data and design details.

Consolidated Tin Mines' Managing Director, John Banning, said:

"Completion of the final Gillian drilling program and commissioning of the pilot scale reduction roasting plant are major milestones for the Mt Garnet Tin Project. Drilling results at the Gillian Deposit have continued to confirm significant intersections and improve confidence in the resource, and will be used to update the resource model over the coming month as part of the Definitive Feasibility Study. We expect completion of the Gillian resource update towards the end of the second quarter, leading to a positive DFS completion in the first half of the coming financial year."

ENDS

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Attachments

Attachment 1: Detailed Results

- Appendix 1: Drill Collar Locations
- Appendix 2: Gillian Significant Intercepts
- Appendix 3: Gillian Assays Above 0.2%Sn

Attachment 2: JORC Resource Table (ASX release 26 June 2013)

Attachment 3: Key Project Map

About Consolidated Tin Mines

Consolidated Tin Mines is an emerging ASX-listed (ASX:CSD) tin explorer and developer. Its major project is the Mt Garnet Tin Project approximately 180km south west of Cairns in northern Queensland, comprised of the Gillian, Pinnacles and Windermere deposits (refer to Key Project Map in Attachment 3). The project is located in an established mining area, in close proximity to mining and concentrating infrastructure. Consolidated Tin's objective is to develop the project into a major low cost, open pit mining operation processing 1Mt per annum to produce approximately 5,000 tonnes of tin in concentrate per annum, commencing with key deposits, Gillian and Pinnacles. With completion of the favourable PFS, Consolidated Tin's strategy is to develop and establish tin production in 2015 and focus on increasing mine life and production profile by developing other tin production opportunities within the broader Mt Garnet Tin Project area.

Attachment 1: Detailed Results

JORC Table 1

SECTION 1 SAMPLING TECHNIQUES AND DATA

Criteria	Commentary
Sampling techniques	The Gillian deposit was sampled using Reverse Circulation (RC) and HQ triple tube diamond (DD) drill holes. The Gillian deposit was drilled on nominal 20 m x 20 m grid spacing. A total of 233 RC and 47 DD holes were drilled for 12,742 m and 3,769.2 m respectively. Holes were drilled at varying angles to optimally intersect the mineralised zones.
	Collar locations for 60% of holes at Gillian were surveyed by CSD using RTK-DGPS providing a horizontal accuracy of +/- 0.01m and vertical accuracy of +/- 0.02m; the remainder was recorded using a standard Differential GPS with 0.6m to 1m horizontal accuracy. RC drilling was used to delineate the resource, with DD used to validate the interpretation, while at the deeper eastern end of the deposit, DD was used to ensure intersections where achieved and sample quality was maximized. The RC samples were collected by riffle splitter. Diamond core was used to obtain high quality samples that were logged for lithology, structure, density and other attributes. Sampling was carried out under CSD protocols and QAQC procedures.
	RC drilling was used to obtain 1 m samples, which were split using a 3 tier riffle splitter below the cyclone of the drill rig to obtain a 12.5% representative sample. Diamond core was HQ size, sampled from a minimum width of 0.2m and maximum of 1.2m within lithological boundaries, and cut by CSD into half core by manual core saw, sent to lab, which was then crushed and if above 3kg was riffle split at the lab. 0.5 gram sample and 8 grams of flux containing 80% 12:22 X-ray flux (12 parts lithium tetraborate and 22 parts lithium tetraborate) and 20% sodium nitrate is mixed in a platinum crucible and roasted in a muffle furnace at 700oC for 20 minutes. Sample is then fused at 1100oC and poured into a platinum mould (40mm diameter) where the mixture cools to create a solid disc. This disc is then determined by sequential XRF calibrated with a mixture of CRMs and synthetic discs fused the same way. Samples were crushed, dried and pulverized (total prep) to produce a sub sample for analysis. Tin and iron were assayed using fused bead preparations with XRF determination, or a sodium peroxide fusion with ICP-MS determination.
Drilling techniques	Diamond drilling accounts for 20% of the drilling in the resource area and comprises HQ sized triple tube core. DD hole depths range from 13 m to 158m. Core orientation using a Reflex orientation tool has been completed on all seven geotechnical DD holes. RC drilling accounts for 80% of the total drilling and comprises 120-140 mm diameter face sampling hammer drilling. RC drill hole depths range from 4 m to 124 m.
Drill sample recovery	RC sample recovery and quality data was logged for approximately 40% of all RC holes. Minimal evidence of smearing has been noted and intersections where it is noted have been excluded from the database. DD drilling recoveries were logged and where core loss occurred, it has been entered into the database. Where core loss has occurred, intervals are marked as 'not sampled', providing an overall slight dilution to grade of the intersection.
	Driller used appropriate measures to maximise RC recovery such as SuperFoam. Triple Tube was used in DD holes to maximise recovery. Depths are checked against the depth given on the core blocks and rod counts are routinely carried out by the drillers and CSD Geologist. RC samples were visually checked for recovery, moisture and contamination. Where poor sample return occurred, or sample was unable to be kept dry, the hole was stopped and diamond tails drilled if necessary.

Criteria	Commentary
	RC sample recovery and quality data was logged for approximately 40% of all RC holes. Minimal evidence of smearing has been noted and intersections where it is noted have been excluded from the database. DD drilling recoveries were logged and where core loss occurred, it has been entered into the database. Where core loss has occurred, intervals are marked as 'not sampled', providing an overall slight dilution to grade of the intersection. Small amounts (< 20cm) of core loss was commonly encountered at the start of drill runs due to the soft nature of the core.
Logging	Geological logging was carried out on all diamond drill holes, with weathering, lithology, mineralogy, alteration, texture, mineralisation, structure, RQD and veining all recorded. Geological logging was also carried out on chip samples from reverse circulation drilling, with primary lithology, mineralogy and alteration recorded. 7 DD holes have been completed and logged for geotechnical purposes. These holes used PQ3 coring and samples were collected and sent for geotechnical testing.
	DD core was photographed after mark up, before sampling with both Dry and Wet photos recorded. Logging of diamond core and RC samples recorded primary lithology, mineralogy, mineralisation, structural (DD only), weathering, and other features of the samples.
	All drill holes were logged in full.
Sub-sampling techniques and sample preparation	Core was cut in half onsite using a manual core saw. Where core was competent, and orientation allowed, samples were collected from the same side of the core.
	RC samples were collected on the rig using 1 in 4 splitters below the cyclone cone. In general, mineralised samples were dry. Where the sample return could not be kept dry, holes were stopped and diamond tails were used to complete the holes.
	The sample preparation of diamond core follows industry best practice in sample preparation involving logging of sample weights, oven drying, and coarse crushing of the half core sample down to ~ 10 mm. Samples weighing <3.3kg undergo pulverisation of the entire sample (total prep) using Essa LM5 grinding mills to a grind size of 85% passing 75 micron. Samples weighing >3.3kg are riffle split, typically in half, with a split size between 1.65 and 3.3kg undergoing pulverization using Essa LM5 grinding mills to a grind size of 85% passing 75 micron. The sample preparation for RC samples is identical, without the coarse crush stage.
	Field QC procedures involve the use of industry certified blanks and standards, along with field duplicates and lab checks. QAQC samples represented approximately 8% of all samples sent to lab.
	RC field duplicates and lab checks were taken on 1m samples, using a riffle splitter. Statistical analysis of duplicate sample data for tin shows a high level of repeatability and a lack of bias between the original and duplicate sample data.
	The sample sizes are considered to be appropriate to correctly represent the mineralisation at Mount Garnet based on: the style of mineralisation (skarn related mineralisation), the thickness and consistency of the intersections, the sampling methodology and percent value assay ranges for the primary elements.

Criteria	Commentary
Quality of assay data and laboratory tests	The analytical techniques for tin and iron were fused bead preparations with XRF determination. This assay technique is considered a "total" assay technique – that is, the assay technique is considered to extract and measure the entire element contained within the sample.
	No geophysical tools were used to determine any element concentrations used in this resource estimate. Portable XRF was only used to assist in logging and all results reported are for lab analysis.
	Grind size checks were performed by the labs and reported as part of their due diligence. QAQC procedures involve the use of industry certified blanks and standards, along with field duplicates and lab checks. QAQC samples represented approximately 8% of all samples sent to lab. Statistical analysis of duplicate sample data for tin shows a high level of repeatability and a lack of bias between the original and duplicate sample data. Results for blanks and industry certified standards show no significant variation across all samples analysed.
Verification of sampling and assaying	No independent verification of significant intersections has been carried out for the most recent RC and diamond drill program; however Optiro did carry out an independent verification of previous drill intersections in June 2013.
	DD was used to twin a number of RC holes as part of the most recent drill program at Gillian. There is a good correlation between the DD twin holes and initial RC holes.
	Data is collected by qualified geologists and entered into spreadsheets with pre-determined lookup fields. An internally developed database system is in use at Mount Garnet with backups and audit records stored. Validation rules are in place to ensure no data entry errors occur. Data is loaded into the database by CSD staff and is reviewed by supervisors.
	No adjustments or calibrations were made to any assay data in this announcement.
Location of data points	Collar locations for 60% of holes at Gillian were surveyed by CSD using RTK-DGPS providing a horizontal accuracy of +/- 0.01m and vertical accuracy of +/- 0.02m; the remainder was recorded using a standard Differential GPS with 0.6m to 1m horizontal accuracy. No local grids are in use, with MGA Zone 55 and AHD grids used. A combination of Eastman camera shots and digital downhole surveys has been used. Total magnetic field is reviewed for each survey to ensure accurate representation of the drillhole bearing.
	The grid system is GDA 1994 MGA zone 55.
	Topographic contours were collected via Airborne LiDAR over entire project area. 4 samples points taken per square meter.
Data spacing and distribution	Drill hole spacing across the orebody is 20 m (northing) by 20 m (easting).
	The mineralised domains have demonstrated sufficient continuity in both geological and grade continuity to support the definition of Mineral Resource and Reserves, and the classifications applied under the 2012 JORC Code.
	Samples have been composited to one metre lengths, and adjusted where necessary to ensure that no residual sample lengths have been excluded (best fit).
Orientation of data in relation to geological structure	Wireframes are modelled around significant intercepts and to outcrop identifying that holes are generally near perpendicular to structures. The data is generally drilled in angles that intersect the mineralised domains perpendicularly, or nearly perpendicular. The

Criteria	Commentary
	orientation of the drill holes across the Mount Garnet Project is varied in order to achieve the best orientation relative to the domain being drilled.
	No orientation based sampling bias has been identified in the data at this point.
Sample security	Chain of custody is managed by CSD. Samples are stored on site, and are collected from site by Toll Ipec for transport and deliver to the assay laboratory. Sample bags are sealed for storage and transport.
Audits or reviews	A review of the sampling data from previous drill programs was carried out by Optiro as part of the 2013 resource estimate. No review has been completed on the data specific to this release.

SECTION 2 REPORTING OF EXPLORATION RESULTS

Criteria	Commentary
Mineral tenement and land tenure status	MDL38 Gillian is 100% owned by Consolidated Tin Mines Limited, situated on a free hold block, west of Mount Garnet. The deposit sits within freehold land and no native title or other interests exist.
Exploration done by other parties	No other parties have been involved in exploration on this site.
Geology	The deposit is a tin/iron skarn; geological setting is altered limestone beds within the Chillagoe Formation intruded by granites. Mineralisation is fine grained Cassiterite, Magnetite and Goethite.
Drill hole information	A table showing collar locations, elevations, dip and azimuth, and down hole lengths is shown in Appendix 1.
Data aggregation methods	For all results, a cut off of 0.2% Sn has been used for data reported.
	Intercepts are separated into two or more mineralised lenses, where a gap of at least 2m of non-mineralised material (i.e. less than 0.2% Sn) occurs. In a broad intercept, individual metres of low grade material may be incorporated into the overall 'minable intersection'. Where significant intercepts with high grade results have been highlighted in the summary and on the accompanying diagram, data has been aggregated using weighted average grades across the full length of the intercept. Significant intercepts are broadly defined as having lengths of greater than 5 metres and grades greater than 0.7% tin. For example, hole HD675 returned the following results:

Sample No.	From (m)	To (m)	% Sn
63654	128.8	129.7	0.67
63655	129.7	130.5	2.84
63656	130.5	131.0	1.59
63657	131.0	132.0	0.75
63658	132.0	133.0	0.64
63659	133.0	133.2	2.12
63661	133.2	133.9	1.08
63662	133.9	134.5	0.66
63663	134.5	135.5	0.48
63664	135.5	136.5	0.47
Total length of intercept		7.7m	
Weighted Average Sn Grade			0.98

The tin equivalent calculation uses the PFS recovery value of 75% for iron and a price of AU$20,000/t for Tin, which is slightly

Criteria	Commentary
	lower than the 5 year mean. The price of AU$150/t for Iron is based on the 5 year mean and therefore will remain. The metal equivalent formula is: Sn(Eq)=(Sn%)+(Fe%*0.75*(150/20,000))
Relationship between mineralisation widths and intercept lengths	Drill holes in this program were designed to intersect the mineralised domains perpendicularly, or nearly perpendicular. Dip and strike of holes was designed precisely to allow accurate pierce points within the orebody. In general the orientation of the drill holes across the Gillian deposit is varied in order to achieve the best orientation relative to the domain being drilled. Due to surface accessibility restrictions some drill hole intersections are not representative of true width of the mineralized zone. Modelling of these zones however is representative of the mineralised zones.
Diagrams	Significant intercepts are shown in the diagram in Appendix 2.
Balanced Reporting	Holes that do not intersect mineralisation are used to close off mineralised envelopes for modelling purposes. Drilling results are shown in Appendix 3.
Other substantive exploration data	A 15 tonne bulk sample was collected during the RC drill program from various zones of tin mineralisation across the orebody (from three ore types being primarily Magnetite, Goethite and other). This bulk sample will be used for final metallurgical testing work which is currently underway.
Further Work	No further resource definition work is planned. Ongoing work includes activities for DFS studies including reviewing the Fluorine content of the deposit for metallurgical testwork, geotechnical reporting, geochemical waste studies, hydrogeological studies, environmental monitoring, mine planning, pit optimization and metallurgical testwork.

Competent Person Statements

The information contained in this announcement that relates to Exploration Results is based on information compiled by Michael Hicks (BScHons, MAIG). Michael Hicks is a geologist of 20 years' experience and has sufficient experience which is relevant to the type of mineralisation under consideration, and to the exploration activities being undertaken, to qualify as a Competent Person as defined by the Australasian Code for Reporting of Exploration Results - JORC Code, 2012 Edition. Michael Hicks is a full time employee of Consolidated Tin Mines Limited and has consented to the inclusion of this information in the form and context in which it appears.

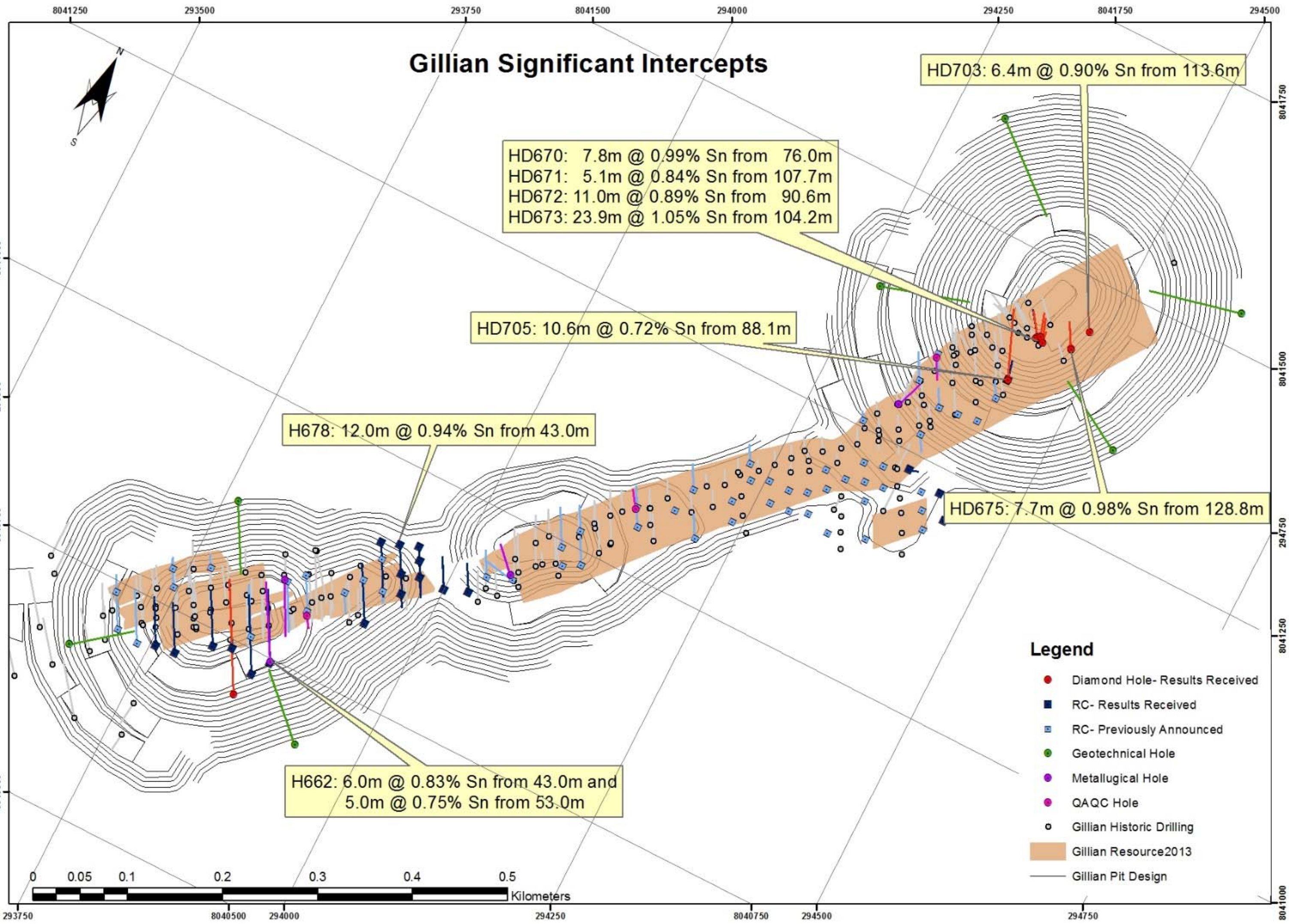
Where the Company refers to the Mt Garnet Mineral Resource in this report (referencing the release made to the ASX on 26 June 2013), it confirms that it is not aware of any new information or data that materially affects the information included in that announcement and all material assumptions and technical parameters underpinning the resource estimate with that announcement continue to apply and have not materially changed.

Appendix 1: Drill Collar Locations

Hole	Easting	Northing	Elevation	Length	Azimuth	Dip
H658	293,747	8,040,716	743	105	333.7	-61
H659	293,776	8,040,707	745	108	330.6	-60
H660	293,810	8,040,733	748	115	329.1	-61
H661	293,828	8,040,739	749	110	332.3	-53
H662	293,859	8,040,728	749	100	332.3	-53
H665	293,918	8,040,912	738	124	159.4	-62
H676	293,963	8,040,873	753	28	155.1	-59
H677	293,953	8,040,891	748	72	148.9	-74
H678	293,941	8,040,914	739	98	157.6	-60
H679	293,973	8,040,897	748	43	150.6	-59
H680	294,023	8,040,909	763	45	330.7	-44
H681	294,430	8,041,363	689	76	336.5	-54
H683	294,438	8,041,418	685	54	322.4	-54
H684	294,436	8,041,416	685	58	315.1	-83
H686	294,441	8,041,421	685	91	330.9	-63
H687	294,439	8,041,199	705	25	0	-90
H688	294,423	8,041,226	705	25	0	-90
H690	294,026	8,040,906	763	65	328.7	-61
H691	294,000	8,040,898	752	50	331.2	-49

Hole	Easting	Northing	Elevation	Length	Azimuth	Dip
H692	294,001	8,040,898	752	60	332	-59
H693	293,967	8,040,910	744	40	152	-43
H694	293,967	8,040,911	744	45	155.9	-59
H695	293,959	8,040,925	740	64	151.3	-60
H696	294,474	8,041,423	686	114	330.9	-45
H682	294,430	8,041,365	689	66	343.8	-69
HD666	293,853	8,040,698	747	102.6	330.9	-50
HD669	294,438	8,041,414	685	101.7	322.1	-82
HD670	294,438	8,041,416	685	94.8	315.9	-52
HD671	294,441	8,041,418	685	145.9	354.1	-62
HD672	294,441	8,041,417	685	109.9	344.9	-50
HD673	294,442	8,041,418	685	137	365.3	-75
HD674	294,475	8,041,425	686	128	335.4	-45
HD675	294,475	8,041,424	686	158	336.6	-60
HD702	294,476	8,041,424	686	153.5	340.5	-75
HD703	294,483	8,041,447	689	150.3	328.8	-58
HD704	294,431	8,041,366	689	81.5	346.4	-70
HD705	294,431	8,041,366	689	104	343.1	-57

Appendix 2: Gillian Significant Intercepts



Appendix 3: Final Gillian Assays Above 0.2%Sn

Hole	Sample	From	To	Sn %	Fe %
H658	59878	81	82	0.91	35.30
H658	59879	82	83	0.70	41.50
H658	59885	91	92	0.35	18.10
H658	59886	92	93	0.36	14.20
H658	59887	93	94	0.33	13.75
H659	59892	79	80	1.98	25.50
H659	59893	80	81	4.21	43.90
H659	59894	81	82	4.40	46.40
H659	59901	89	90	0.34	17.05
H659	59902	90	91	0.43	11.45
H659	59903	91	92	0.43	23.90
H661	59921	36	37	0.56	19.70
H661	59922	37	38	0.30	13.70
H662	59926	43	44	0.41	10.95
H662	59927	44	45	0.84	23.30
H662	59928	45	46	0.80	23.20
H662	59929	46	47	1.03	23.40
H662	59930	47	48	1.58	22.70
H662	59931	48	49	0.35	8.32
H662	59936	53	54	0.38	30.40
H662	59937	54	55	0.72	43.20
H662	59938	55	56	0.54	16.65
H662	59939	56	57	0.74	31.00
H662	59941	57	58	1.35	49.30
H665	63064	45	46	0.42	11.80
H665	63066	47	48	0.35	12.80
H665	63067	48	49	0.27	12.90
H665	63075	56	57	0.60	15.75
H665	63091	69	70	0.36	19.35
H665	63092	70	71	0.38	17.20
H665	63109	105	106	0.23	12.65
H665	63110	106	107	0.20	14.70
H665	63113	109	110	0.21	15.95
H665	63114	110	111	0.26	16.80
H665	63115	111	112	0.68	14.15
H665	63116	112	113	0.41	13.20
H665	63117	113	114	0.39	13.70
H665	63118	114	115	0.45	14.55

Hole	Sample	From	To	Sn %	Fe %
H676	63123	4	5	0.23	17.65
H676	63124	5	6	0.53	17.50
H676	63125	6	7	1.03	20.60
H676	63127	7	8	0.36	6.15
H677	63142	1	2	0.40	21.10
H677	63145	8	9	0.70	24.30
H677	63146	9	10	0.35	20.60
H677	63149	12	13	0.63	22.80
H677	63150	13	14	0.32	16.70
H677	63151	14	15	0.21	9.97
H677	63153	16	17	0.23	9.79
H677	63157	20	21	0.34	21.50
H677	63158	21	22	0.29	17.50
H677	63159	22	23	0.31	19.35
H677	63161	23	24	0.48	24.30
H677	63233	66	67	0.24	12.10
H677	63235	68	69	0.22	12.15
H678	63170	35	36	0.66	18.35
H678	63171	36	37	0.51	15.25
H678	63176	40	41	0.38	16.15
H678	63177	41	42	0.49	18.95
H678	63178	42	43	0.67	19.65
H678	63179	43	44	0.85	20.10
H678	63181	44	45	0.92	19.35
H678	63182	45	46	0.91	22.50
H678	63183	46	47	1.12	23.80
H678	63184	47	48	1.01	23.10
H678	63185	48	49	0.84	25.00
H678	63186	49	50	1.16	29.90
H678	63187	50	51	1.05	26.40
H678	63188	51	52	0.69	28.70
H678	63189	52	53	1.14	26.10
H678	63190	53	54	0.86	26.00
H678	63191	54	55	0.80	22.90
H678	63192	55	56	0.65	21.70
H678	63193	56	57	0.81	20.30
H678	63194	57	58	0.53	19.85
H678	63195	58	59	0.21	17.55

Hole	Sample	From	To	Sn %	Fe %
H678	63201	63	64	0.52	17.55
H678	63202	64	65	0.56	19.50
H678	63203	65	66	0.73	20.40
H678	63204	66	67	0.66	18.55
H678	63205	67	68	0.38	13.60
H678	63206	68	69	0.59	17.20
H678	63208	70	71	0.30	18.55
H678	63209	71	72	0.45	18.35
H678	63210	72	73	0.52	17.75
H678	63211	73	74	0.46	18.35
H678	63212	74	75	0.47	15.05
H678	63214	76	77	0.44	15.80
H678	63218	82	83	0.42	11.80
H678	63222	85	86	0.67	15.65
H678	63223	86	87	0.70	19.30
H680	63252	27	28	0.81	22.20
H680	63253	28	29	1.01	23.50
H680	63254	29	30	1.01	20.00
H680	63255	30	31	0.30	18.95
H680	63256	31	32	0.26	17.40
H681	63263	55	56	0.28	10.35
H681	63268	60	61	0.24	11.80
H681	63269	61	62	0.24	27.60
H681	63273	66	67	0.20	17.85
H681	63274	67	68	0.20	11.60
H681	63279	71	72	0.36	43.20
H681	63284	75	76	0.67	50.00
H687	63299	14	15	0.70	13.70
H687	63301	15	16	0.78	22.30
H687	63302	16	17	0.66	21.90
H687	63303	17	18	0.57	17.75
H688	63307	17	18	0.35	4.72
H688	63308	18	19	1.00	30.10
H692	63325	26	27	0.21	13.80
H692	63327	27	28	0.25	13.90
H692	63328	28	29	0.30	14.15
H692	63329	29	30	0.43	14.40
H692	63332	39	40	0.23	9.51
H692	63341	52	53	0.28	13.10

Hole	Sample	From	To	Sn %	Fe %
H693	63348	20	21	0.24	8.99
H693	63349	21	22	0.33	12.00
H693	63350	22	23	0.22	11.80
H694	63358	27	28	0.20	18.00
H695	63365	8	9	0.23	3.89
HD666	63381	72.3	72.8	0.23	16.60
HD666	63382	72.9	73.7	0.88	36.10
HD666	63383	74.3	75.3	0.69	25.00
HD666	63384	75.3	75.9	1.15	50.80
HD669	63409	70.2	71.2	0.40	10.55
HD669	63410	71.2	71.7	0.29	17.35
HD669	63411	71.7	72.6	0.24	9.13
HD669	63412	72.6	73.5	0.61	15.45
HD669	63414	74.2	75	0.73	18.00
HD669	63421	79.7	80	2.43	31.90
HD669	63428	85.1	86.2	0.38	13.65
HD669	63429	86.2	86.8	0.31	14.15
HD669	63432	88.6	89.6	0.23	20.70
HD669	63439	93.1	93.9	0.89	58.50
HD669	63441	94	94.9	0.95	51.60
HD669	63442	95	95.4	0.46	41.10
HD669	63443	95.4	96.1	0.57	29.30
HD669	63444	96.1	97	1.00	35.40
HD670	63449	69.7	70.7	0.31	42.70
HD670	63450	70.7	71.8	0.99	50.70
HD670	63451	72.4	73.4	0.61	23.40
HD670	63452	73.4	73.9	0.77	52.60
HD670	63453	74	74.4	0.29	55.50
HD670	63454	74.5	75.2	0.53	44.50
HD670	63456	76	77	0.59	48.90
HD670	63457	77	78.1	0.89	39.90
HD670	63458	78.1	79.1	1.20	42.80
HD670	63459	79.1	80.1	1.55	50.20
HD670	63461	80.1	80.8	0.82	29.40
HD670	63462	80.8	81.5	1.04	36.70
HD670	63463	81.5	82.4	1.37	44.30
HD670	63464	82.4	83.4	0.63	39.00
HD670	63465	83.4	83.8	0.61	21.60
HD670	63466	83.8	84.8	0.38	15.45

Hole	Sample	From	To	Sn %	Fe %
HD670	63467	84.8	85.4	0.52	17.05
HD670	63468	85.4	86	0.38	12.80
HD670	63469	86	87	0.50	14.20
HD670	63470	87	88	0.58	16.10
HD670	63471	88	89	0.51	15.10
HD670	63472	89	89.7	0.29	11.20
HD671	63482	103.2	103.8	0.40	29.70
HD671	63483	103.8	104.5	0.36	19.85
HD671	63484	104.5	105.2	0.38	21.90
HD671	63485	105.2	106.2	0.58	37.70
HD671	63486	106.2	107.2	0.31	48.10
HD671	63487	107.2	107.7	0.35	31.40
HD671	63488	107.7	108.4	0.56	33.50
HD671	63489	108.4	109.3	0.44	49.90
HD671	63490	109.3	109.6	1.00	45.30
HD671	63491	109.6	110.6	0.95	51.80
HD671	63492	110.6	111	1.73	35.30
HD671	63493	111	111.6	1.15	57.90
HD671	63494	111.6	112.2	0.86	62.60
HD671	63495	112.2	112.8	0.63	49.40
HD671	63496	112.8	113.9	0.49	46.70
HD671	63497	113.9	115	0.38	41.10
HD671	63498	115	115.9	0.57	36.70
HD671	63499	115.9	116.8	0.57	35.30
HD671	63501	116.8	117.7	0.36	51.80
HD671	63502	117.7	118.6	0.52	34.10
HD671	63503	118.6	119.4	0.51	35.90
HD671	63504	119.4	120.4	0.48	37.90
HD671	63505	120.4	121.4	0.22	21.80
HD671	63506	121.4	122	0.35	19.70
HD672	63511	86.2	86.6	0.20	45.00
HD672	63512	86.6	87.2	0.42	34.60
HD672	63517	89.4	90	0.23	31.10
HD672	63518	90	90.6	0.34	41.50
HD672	63519	90.6	91.3	0.79	47.40
HD672	63521	91.3	92.3	0.75	57.40
HD672	63522	92.3	92.9	0.32	63.70
HD672	63523	92.9	93.3	1.15	49.70
HD672	63524	93.3	93.8	2.18	42.80
HD672	63526	93.8	94.2	1.37	37.70
HD672	63527	94.2	95	1.09	23.90
HD672	63528	95	95.5	1.02	28.00
HD672	63529	95.5	96	1.59	22.00
HD672	63530	96	96.8	0.95	22.90
HD672	63531	96.8	97.5	1.31	23.90
HD672	63532	97.5	98.3	0.55	41.30
HD672	63533	98.3	99	0.56	36.30
HD672	63535	100	100.6	1.03	22.00
HD672	63536	100.6	101.6	0.70	27.60
HD672	63537	101.6	102.6	0.41	11.40
HD672	63539	103.3	104.3	0.37	11.75
HD673	63554	88	88.4	1.47	60.10
HD673	63555	88.4	89.4	1.66	54.10
HD673	63556	89.4	90.1	1.53	47.00
HD673	63557	90.1	90.5	0.24	46.40
HD673	63566	94.9	95.4	1.37	26.10
HD673	63567	95.4	96.5	1.35	50.90
HD673	63568	96.5	97.5	0.71	29.90
HD673	63574	101.9	103	0.26	21.90
HD673	63575	103	104.1	0.54	54.30
HD673	63577	104.2	104.7	0.65	61.10
HD673	63578	104.7	105.3	0.73	54.40
HD673	63579	105.3	106	0.55	55.10
HD673	63581	106	106.8	1.38	51.60
HD673	63582	106.8	107.3	1.34	48.80
HD673	63583	107.3	108	0.62	17.30
HD673	63584	108.4	109.5	1.74	55.30
HD673	63585	109.5	110.4	1.18	55.80
HD673	63586	110.4	111	1.64	43.30
HD673	63587	111	112	1.66	44.70
HD673	63588	112	113	1.65	39.00
HD673	63589	113	114	1.51	42.90
HD673	63591	114.7	115.5	0.26	47.50
HD673	63592	115.5	116.2	1.05	35.80
HD673	63593	116.2	117.3	1.91	36.20
HD673	63594	117.5	118	2.16	30.70
HD673	63595	118	118.8	0.59	54.90
HD673	63596	118.9	119.1	0.46	42.70

Hole	Sample	From	To	Sn %	Fe %
HD673	63597	119.1	120.3	0.87	54.60
HD673	63598	120.3	121.1	0.78	53.50
HD673	63599	121.1	122.3	1.05	52.00
HD673	63601	122.3	123.4	1.26	49.40
HD673	63602	123.4	124.4	1.12	59.30
HD673	63603	124.4	125	1.01	54.70
HD673	63604	125	126	0.88	56.50
HD673	63605	126.2	127	0.99	45.70
HD673	63606	127	128.1	0.50	31.50
HD673	63610	79.9	80.6	0.61	15.05
HD674	63613	108.4	108.7	0.26	11.85
HD674	63614	108.7	108.9	0.46	28.10
HD674	63615	108.9	109.1	0.89	52.00
HD674	63616	109.1	109.5	0.48	54.60
HD674	63617	109.5	110	0.42	50.40
HD674	63619	110.5	110.8	0.46	9.16
HD674	63621	110.8	111	0.50	16.85
HD674	63622	111	111.7	0.41	21.50
HD674	63623	111.7	112.2	0.83	36.90
HD674	63624	112.2	112.9	0.63	47.40
HD674	63627	113.4	114	0.49	48.00
HD674	63628	114	114.4	0.36	26.40
HD674	63629	114.4	115	0.92	59.50
HD674	63630	115	115.4	0.59	61.70
HD674	63631	115.4	116	0.73	54.20
HD674	63632	116	117	0.46	44.30
HD674	63633	117	117.3	0.67	22.00
HD674	63634	117.3	117.8	0.47	31.30
HD674	63635	117.8	118.3	0.36	42.70
HD674	63636	118.3	119	0.48	27.50
HD674	63637	119	120	0.53	19.35
HD674	63638	120	120.4	0.59	18.25
HD675	63645	121.3	122	0.56	22.30
HD675	63648	123.7	124.6	0.23	56.40
HD675	63649	124.6	125.2	0.30	40.50
HD675	63650	125.2	126	0.30	60.40
HD675	63651	126	127	0.22	59.90
HD675	63652	127	128	0.24	58.00
HD675	63653	128	128.8	0.21	61.30

Hole	Sample	From	To	Sn %	Fe %
HD675	63654	128.8	129.7	0.67	61.00
HD675	63655	129.7	130.5	2.84	56.30
HD675	63656	130.5	131	1.59	43.20
HD675	63657	131	132	0.75	38.10
HD675	63658	132	133	0.64	51.80
HD675	63659	133	133.2	2.12	31.20
HD675	63661	133.2	133.9	1.08	29.40
HD675	63662	133.9	134.5	0.66	47.60
HD675	63663	134.5	135.5	0.48	48.30
HD675	63664	135.5	136.5	0.47	54.10
HD675	63665	136.5	137.3	0.57	40.80
HD675	63666	137.3	137.9	0.49	37.50
HD675	63667	137.9	139	0.27	14.95
HD675	63671	141.8	142.5	0.29	32.70
HD675	63672	142.5	143.5	0.32	39.70
HD675	63673	143.5	144	0.31	42.90
HD675	63677	145.3	146	0.37	20.50
HD675	63678	146	147	0.57	26.40
HD675	63679	147	148	0.49	28.20
HD675	63681	148	149	0.30	26.90
HD675	63682	149	149.6	0.36	22.30
HD675	63683	149.6	150.6	0.55	16.50
HD675	63684	150.6	150.9	0.62	18.80
HD702	63696	120	121	0.39	12.45
HD702	63697	121	122	0.24	15.10
HD702	63698	122	123	0.21	16.95
HD702	63701	124	125	0.55	16.15
HD702	63702	125	126	0.21	14.55
HD702	63723	142.6	143.5	0.53	46.20
HD702	63724	143.5	144	0.42	49.20
HD702	63725	144	144.4	0.23	37.80
HD702	63727	144.4	145	0.50	53.70
HD702	63728	145	146	0.86	53.40
HD702	63729	146	146.6	0.54	50.30
HD702	63730	146.6	147	0.55	30.70
HD702	63731	147	147.5	0.45	32.20
HD702	63732	147.5	148	0.80	37.20
HD702	63733	148	148.5	0.38	50.40
HD702	63734	148.5	149	0.66	49.20

Hole	Sample	From	To	Sn %	Fe %
HD702	63735	149	149.3	0.30	14.40
HD702	63736	149.3	150	0.67	29.90
HD702	63737	150	150.6	1.12	39.60
HD702	63738	150.6	151.3	0.73	43.30
HD703	63743	111	111.8	0.27	42.00
HD703	63744	111.8	112.8	0.43	46.40
HD703	63745	112.8	113.2	0.21	21.60
HD703	63746	113.2	113.6	0.30	36.60
HD703	63747	113.6	114	1.20	59.40
HD703	63748	114	114.8	1.21	54.30
HD703	63749	114.8	115.5	0.57	23.10
HD703	63750	115.5	116.2	0.59	20.10
HD703	63751	116.2	116.5	0.90	28.10
HD703	63752	116.6	117	0.44	29.70
HD703	63753	117	117.6	0.43	24.50
HD703	63754	117.6	118.5	1.49	47.60
HD703	63755	118.5	119	1.11	49.40
HD703	63756	119	119.5	0.91	46.90
HD703	63757	119.5	120	0.94	41.70
HD703	63761	122	123	0.38	56.30
HD703	63762	123	123.9	0.32	33.50
HD703	63763	123.9	124.5	0.26	23.70
HD703	63764	124.5	125.5	0.41	26.40
HD703	63765	125.5	126.1	0.55	48.40
HD703	63766	126.1	126.6	0.27	46.20
HD703	63767	126.6	127	0.34	46.40
HD703	63768	127	127.7	0.21	15.65
HD703	63769	127.7	128.4	0.23	14.25
HD703	63772	130	130.8	1.23	33.50
HD703	63773	131	132	0.43	33.40
HD703	63774	132	133	0.21	11.40
HD703	63776	133	134	0.25	11.95
HD703	63781	137	137.5	0.29	13.10

Hole	Sample	From	To	Sn %	Fe %
HD703	63782	137.5	138	0.34	7.87
HD704	63791	70.5	70.9	0.36	53.20
HD704	63792	70.9	71.7	0.44	48.40
HD704	63793	71.7	72.1	0.52	51.40
HD704	63794	72.1	72.7	1.48	50.40
HD704	63795	72.7	73.2	0.61	21.00
HD704	63796	73.2	74	0.92	24.60
HD704	63797	74	75	0.41	21.40
HD704	63798	75	75.8	0.76	24.30
HD704	63799	75.8	76.4	0.73	25.50
HD704	63801	76.4	77	0.36	14.55
HD704	63802	77	77.7	0.25	11.80
HD705	63808	72.5	73.6	0.22	9.37
HD705	63816	78.1	78.5	0.21	53.60
HD705	63819	79.7	80	0.41	53.40
HD705	63823	81.7	82.6	0.30	50.70
HD705	63824	82.6	83.6	0.60	54.00
HD705	63829	86.8	87.6	0.20	56.50
HD705	63831	88.1	89	1.05	44.90
HD705	63832	89	90.1	0.89	51.50
HD705	63833	90.5	91	0.84	59.90
HD705	63834	91	92	0.79	59.90
HD705	63835	92	93	0.72	62.70
HD705	63836	93	94	0.70	54.40
HD705	63837	94	95	0.57	56.90
HD705	63838	95	96	0.48	60.80
HD705	63839	96	97	0.91	44.90
HD705	63841	97	98	0.69	42.70
HD705	63842	98	98.7	0.67	39.10
HD705	63843	98.7	99.1	0.32	20.90
HD705	63844	99.1	99.7	0.22	15.45
HD705	63846	100.2	101.2	0.21	12.85

Attachment 2: JORC Resource Table (ASX release 26 June 2013)

TIN (Sn)	Cut-off Sn_EQ %	Measured tonnes	Grade Sn%	Indicated tonnes	Grade Sn%	Inferred tonnes	Grade Sn%	Total tonnes	Grade Sn%
Gillian	0.2	1,105,000	0.73	1,563,000	0.62	930,000	0.61	**3,599,000**	**0.65**
Pinnacles	0.33	-	-	5,461,000	0.30	1,575,000	0.30	**7,035,000**	**0.30**
Deadmans Gully	0.18	-	-	444,000	0.34	-	-	**444,000**	**0.34**
Windermere	0.25	-	-	829,000	0.26	1,211,000	0.27	**2,040,000**	**0.27**
TOTAL		**1,105,000**	**0.73**	**8,296,000**	**0.36**	**3,716,000**	**0.37**	**13,118,000**	**0.39**

IRON (Fe)	Cut-off Sn_EQ %	Measured tonnes	Grade Fe%	Indicated tonnes	Grade Fe%	Inferred tonnes	Grade Fe%	Total tonnes	Grade Fe%
Gillian	0.2	1,105,000	32.32	1,563,000	24.50	930,000	28.53	**3,599,000**	**27.95**
Pinnacles	0.33	-	-	5,461,000	19.12	1,575,000	21.04	**7,035,000**	**19.55**
Deadmans Gully	0.18	-	-	444,000	26.70	-	0.00	**444,000**	**26.70**
Windermere	0.25	-	-	829,000	25.79	1,211,000	23.68	**2,040,000**	**24.54**
TOTAL		**1,105,000**	**32.32**	**8,296,000**	**21.21**	**3,716,000**	**23.78**	**13,118,000**	**22.87**

FLUORINE (F)	Cut-off Sn_EQ %	Measured tonnes	Grade F%	Indicated tonnes	Grade F%	Inferred tonnes	Grade F%	Total tonnes	Grade F%
Pinnacles	0.33	-	-	5,461,000	6.28	1,575,000	4.14	**7,035,000**	**5.80**
TOTAL		**-**	**-**	**5,461,000**	**6.28**	**1,575,000**	**4.14**	**7,035,000**	**5.80**

TIN EQUIVALENT (Sn_EQ)	Cut-off Sn_EQ %	Measured tonnes	Sn_EQ %	Indicated tonnes	Sn_EQ %	Inferred tonnes	Sn_EQ %	Total tonnes	Sn_EQ %
Gillian	0.2	1,105,000	0.91	1,563,000	0.75	930,000	0.77	**3,599,000**	**0.81**
Pinnacles	0.33	-	-	5,461,000	0.50	1,575,000	0.47	**7,035,000**	**0.49**
Deadmans Gully	0.18	-	-	444,000	0.49	-	0.00	**444,000**	**0.49**
Windermere	0.25	-	-	829,000	0.40	1,211,000	0.41	**2,040,000**	**0.41**
TOTAL		**1,105,000**	**0.91**	**8,296,000**	**0.54**	**3,716,000**	**0.53**	**13,118,000**	**0.56**

Sn equivalent is based on the following Formula, product pricing and metallurgical recoveries;

Sn%+(Fe%*FeREC*Fe$/t/Sn$/t)+(F%*FREC*F$/t/Sn$/t)
(Sn%)+(Fe%*0.75*(150/20,000))+(F%*0.7*(400/20,000))
Sn = AU$ 20,000/tonne,
Fe = 75% recovery @ AU$ 150/tonne
F = 70% recovery @ AU$ 400/tonne
REC = Recovery

Attachment 3: Key Project Map