# ASX Announcement

June 2021 Quarterly Report

*29 July 2021*

# Highlights

## Paterson Project

**Final diamond drill hole locations for the Apollo, Atlas, Juno and Voyager targets were determined, and sufficient funds allocated to budget in the quarter to drill these targets and more upon receipt of final heritage clearances from the Traditional Owners.**

**As detailed and extensive planning in advance of the Q3/Q4 2021 Paterson drill campaign is now largely complete with the Paterson Central exploration team currently in the pre-mobilisation phase with respect to rig booking and logistical planning in advance of receiving final heritage clearances. Once complete, the Company will then move to immediately commence drilling and intends to drill continuously for the remainder of the calendar year.**

**The Company intends to provide a more detailed update on the proposed final drill program hole locations and site mobilisation start dates in the near future.**

## Carlow Castle Au-Cu-Co Project

**The commencement of the newly planned campaign of drilling for circa 11,000 metres, signals a new phase of exploration and evaluation at the Carlow Castle Project. This drilling is also designed to test the long-awaited Good Luck and Little Fortune Projects, located approximately one kilometre to the south of Carlow Castle.**

**As at 30 of June, a total of 16 holes have been drilled for a total of 3,506 metres of which 2,020 metres was RC and 1,486 metres was diamond.**

**Results for RC holes ARC310 to 313 and ARC315 have been received which focussed on the Carlow Castle Western Zone. These holes returned significant results of:**

- **6m @ 14.97g/t Au, 7.09% Cu, 0.06% Co from 53 metres Hole ARC310**
  - **Including; 3m @ 13.92g/t Au, 5.11% Cu 0.03% Co from 54 metres**
- **6m @ 2.61g/t Au, 0.54% Cu, 0.14% Co from 186 metres Hole ARC311**
  - **Including; 1m @ 6.27g/t Au, 1.07% Cu, 0.05% Co from 187 metres**
- **4m @ 2.09g/t Au, 0.50% Cu, 0.06% Co from 121 metres Hole ARC313**
  - **Including; 1m @ 5.76g/t Au, 1.74% Cu, 0.07% Co from 124 metres**
- **1m @ 9.29g/t Au, 0.67% Cu, 0.17% Co from 114 metres Hole ARC312**

**Diamond drilling results are pending review and RC drilling at Carlow Castle is currently in progress, testing the new interpretation designed to add significant ounces to the project.**

## Carlow Castle Mineral Resource Estimate

**The Mineral Resource report was completed by CSA and submitted in May. The updated Mineral Resource is 14.3 million tonnes at 0.7 g/t Au, 0.4% Cu, and 0.05% Co for 320,000 ounces gold, 53,000 tonnes contained copper, and 7,000 tonnes contained cobalt. The difference in resource numbers occurred due to additional drilling, redefinition and increase in the confidence of the model.**

**The Company is currently reviewing the recent Mineral Resource estimate with a view to approaching the Carlow Castle Project via a new strategy, aiming to increase tonnages and grade by targeting the higher-grade mineralised features, thus allowing for more effective geological control to drive project development. The current Q3 2021 RC drill program has been designed to achieve this objective and combined with the Mineral Resource review should, with success, allow the Company to clearly demonstrate the potential of the project to host a robust and significant gold, copper and cobalt resource.**

## Munni Munni Project

**Drilling at Munni Munni comprised of 15 RC drill holes for 2,740 metres, completed between April and May, with drill holes spread through the entire upper portion of the mineralisation, to a maximum depth of 250 metres.**

**Significant intersections include:**

- **7m @ 2.20g/t 2PGE + Au (1.46g/t Pd, 0.67 g/t Pt, 0.07g/t Au) from 124 metres, 21MMRC005;**
- **7m @ 2.35g/t 2PGE + Au (1.33g/t Pd, 0.84 g/t Pt, 0.18g/t Au), from 96 metres , 21MMRC006;**
- **4m @ 2.45g/t 2PGE + Au (1.31g/t Pd, 0.85g/t Pt, 0.29g/t Au) from 60 metres , 21MMRC007;**
- **5m @ 2.35g/t 2PGE + Au (1.36g/t Pd, 0.68g/t Pt, 0.31g/t Au) from 75 metres , 21MMRC008;**
- **4m @ 2.87g/t 2PGE + Au (1.76g/t Pd, 0.89g/t Pt, 0.22g/t Au) from 115 metres, 2MMRC010.**

**Artemis is pleased to have now executed a full Joint Venture Agreement and associated documents that will proceed to a Joint Venture Agreement for 100% of the Munni Munni Project with Platina Resources Limited in the ratio of beneficial interests, 70% ARV and 30% PGM.**

**Artemis and Platina continue to explore ways to monetise Munni Munni for the benefit of shareholders.**

## Radio Hill FLEM Survey

**A Fixed-Loop Electromagnetic (FLEM) survey was completed in May which detected deep and untested conductor anomaly zones of interest identified from historic deep drilling and follow-up DHEM survey data. From this survey, the Radio Hill Project is still considered prospective for additional Ni-Cu-Co-PGE discoveries. Recommendations for further work at Radio Hill are pending.**

# Whundo GAIP Survey

**A Gradient-Array Induced Polarisation (GAIP) survey was conducted at the Whundo VMS project to identify VMS-style mineralisation along target trends located to the northeast of the main Whundo deposit. Additional work has been recommended post-survey that has identified anomalous trends that will require another GAIP survey and drilling.**

## SUMMARY OF DRILLING AT CARLOW CASTLE

Artemis Resources (ASX: ARV) is pleased to release this June Quarterly, highlighting the achievements gained during the reporting period.

The June Quarterly results include the final assays from the initial holes drilled at the beginning of the circa 11,000m program, which is the follow up program from the 2020 Q4 drilling campaign. This program will continue into Q3.

Drill statistics and completed holes are shown in Table 1 and Figure 1, respectively.

*Table 1: Drill statistics for June Quarterly*

| *Location* | *No of Holes* | *RC (m)* | *Diamond (m)* | *No of Samples* | *No Samples Submitted* | *No Samples Received* | *No of Samples Outstanding* |
|---|---|---|---|---|---|---|---|
| East Zone | 6 | | 1290.7 | 1276 | 1097 | 782 | 494 |
| West Zone | 9 | 2020 | | 2046 | 2046 | 2046 | 0 |
| Cross-Cut | 1 | | 195.3 | 201 | 0 | 0 | 201 |

Several assays from the beginning of the planned drilling program have returned significant results and these have been used to define and update the remaining holes in the program. These are shown in Table 2.

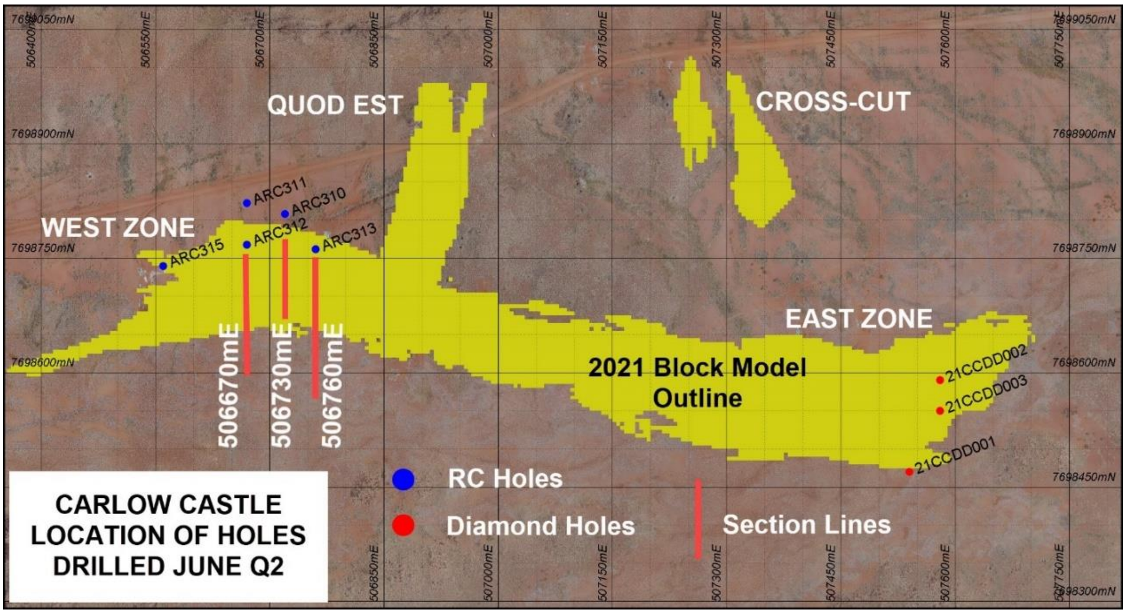


*Figure 1: Location of drill collars drilled during the June Q2 period. Section lines are shown in red with corresponding section co-ordinates.*

The rationale behind the new drilling program was to test the interpreted shallow plunging high-grade gold and copper shoots in and below the Carlow Castle Western Zone, the steeply dipping high-grade shoots on the eastern zone, the steep down-plunging gold shoots at Quod Est and the new interpretation of Cross-Cut.

*Table 2: Carlow Castle drilling assay results averaged over significant drill intercept intervals bases on 1m assay samples, intersections defined by either >0.5g/t Au or >0.5%Cu, max 2m internal dilution. NSI = no significant intercept with values above lower cut off.*

| Hole No | Comment | From | To | Downhole Width (m) | True Width (m) | Au (g/t) | Cu (%) | Co (%) |
|---|---|---|---|---|---|---|---|---|
| ARC310 | | 53 | 59 | 6 | 5.4 | **14.97** | **7.09** | 0.06 |
| | ***Including*** | ***54*** | ***57*** | ***3*** | ***2.7*** | ***13.92*** | ***5.11*** | ***0.03*** |
| | | 112 | 113 | 1 | 0.9 | 1.42 | 0.05 | 0.03 |
| | | 168 | 170 | 2 | 1.8 | 1.61 | 0.16 | **0.13** |
| | | 225 | 226 | 1 | 0.9 | 1.37 | 0.06 | 0.01 |
| ARC311 | | 136 | 142 | 6 | 5.4 | 1.35 | 0.34 | 0.07 |
| | | 154 | 155 | 1 | 0.9 | **2.49** | 0.49 | 0.02 |
| | | 186 | 192 | 6 | 5.4 | **2.61** | 0.54 | **0.14** |
| | ***Including*** | ***187*** | ***188*** | ***1*** | ***0.9*** | ***6.27*** | ***1.07*** | ***0.05*** |
| ARC312 | | 9 | 10 | 1 | 0.9 | 1.61 | **2.33** | 0.05 |
| | | 28 | 34 | 6 | 5.4 | 2.68 | **1.10** | 0.02 |
| | ***Including*** | ***31*** | ***34*** | ***3*** | ***2.7*** | ***4.34*** | ***1.75*** | ***0.01*** |
| | | 56 | 61 | 5 | 4.5 | 1.66 | 0.26 | 0.04 |
| | | 83 | 85 | 2 | 1.8 | 1.15 | 0.19 | 0.03 |
| | | 114 | 115 | 1 | 0.9 | **9.29** | 0.67 | **0.17** |
| | | 144 | 145 | 1 | 0.9 | **2.63** | 0.23 | 0.01 |
| ARC313 | | 35 | 36 | 1 | 0.9 | 1.11 | 0.05 | 0.01 |
| | | 44 | 45 | 1 | 0.9 | 1.21 | 0.28 | 0.03 |
| | | 82 | 83 | 1 | 0.9 | 1.06 | **3.93** | 0.01 |
| | | 105 | 106 | 1 | 0.9 | 1.30 | 0.08 | **0.18** |
| | | 110 | 112 | 2 | 1.8 | **2.07** | 0.44 | **0.31** |
| | | 121 | 125 | 4 | 3.6 | **2.09** | 0.50 | 0.06 |
| | ***Including*** | ***124*** | ***125*** | ***1*** | ***0.9*** | ***5.76*** | ***1.74*** | ***0.07*** |
| | | 147 | 148 | 1 | 0.9 | 1.35 | 0.14 | 0.10 |
| | | 199 | 200 | 1 | 0.9 | **5.17** | **0.38** | 0.01 |
| ARC315 | NSI | | | | | | | |

A reinterpretation of the structural setting and mineralising events have returned high-grade gold, copper and cobalt assays on the main shoots (Figure 2) and is defining the extent of the rich, lower grade gold-copper-cobalt "halo envelop" surrounding the internal high-grade zones.

The Mineral Resource Estimate (MRE) completed by CSA Global and released in May, is being reviewed, considering the updated interpretation of the Carlow Castle system. This information, along with the updated interpretation will be incorporated into the new model and drive future drilling campaigns.

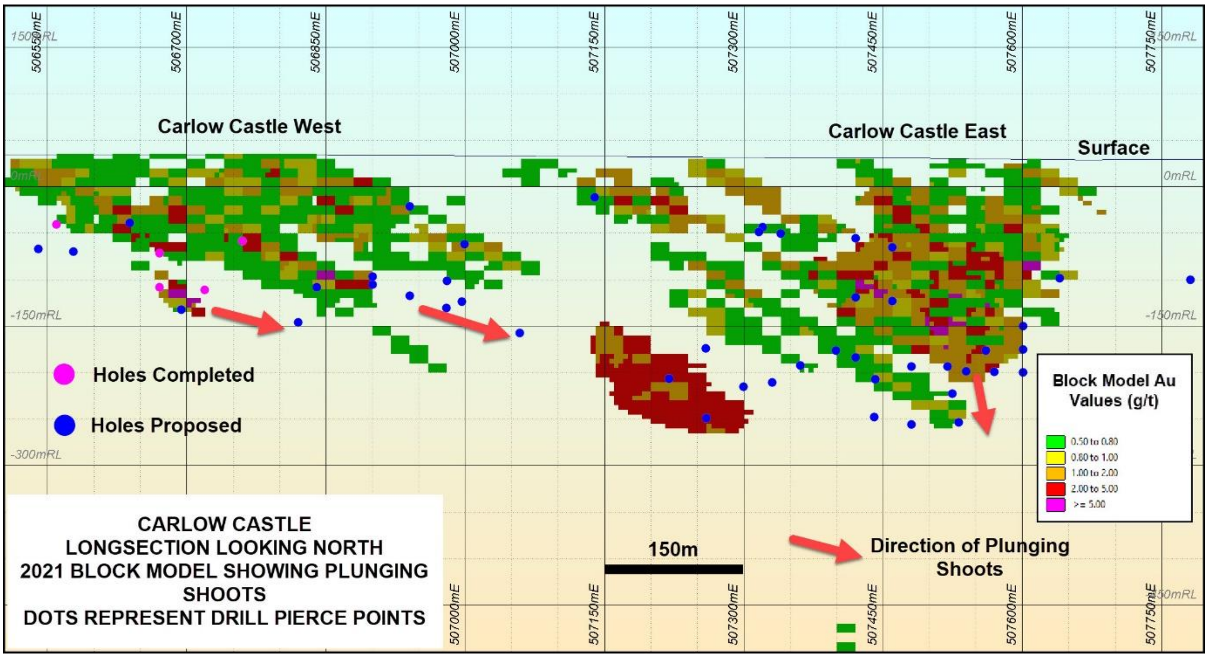


*Figure 2: Longsection of Carlow Castle looking north showing the high-grade trends (hot colours) in the 2021 block model. The dots denote the target pierce points of the drill holes.*

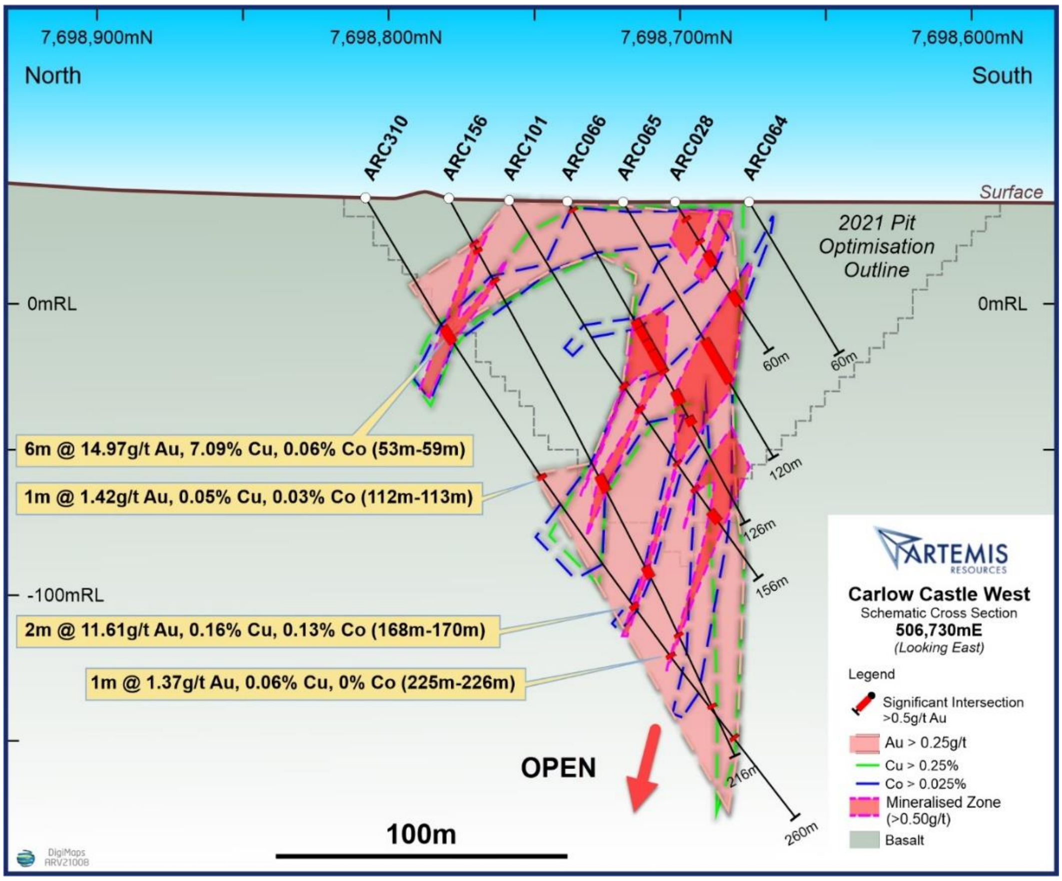


*Figure 3: Section 506730mE, intersections for Hole ARC310. (Refer to Figure 1 for location)*

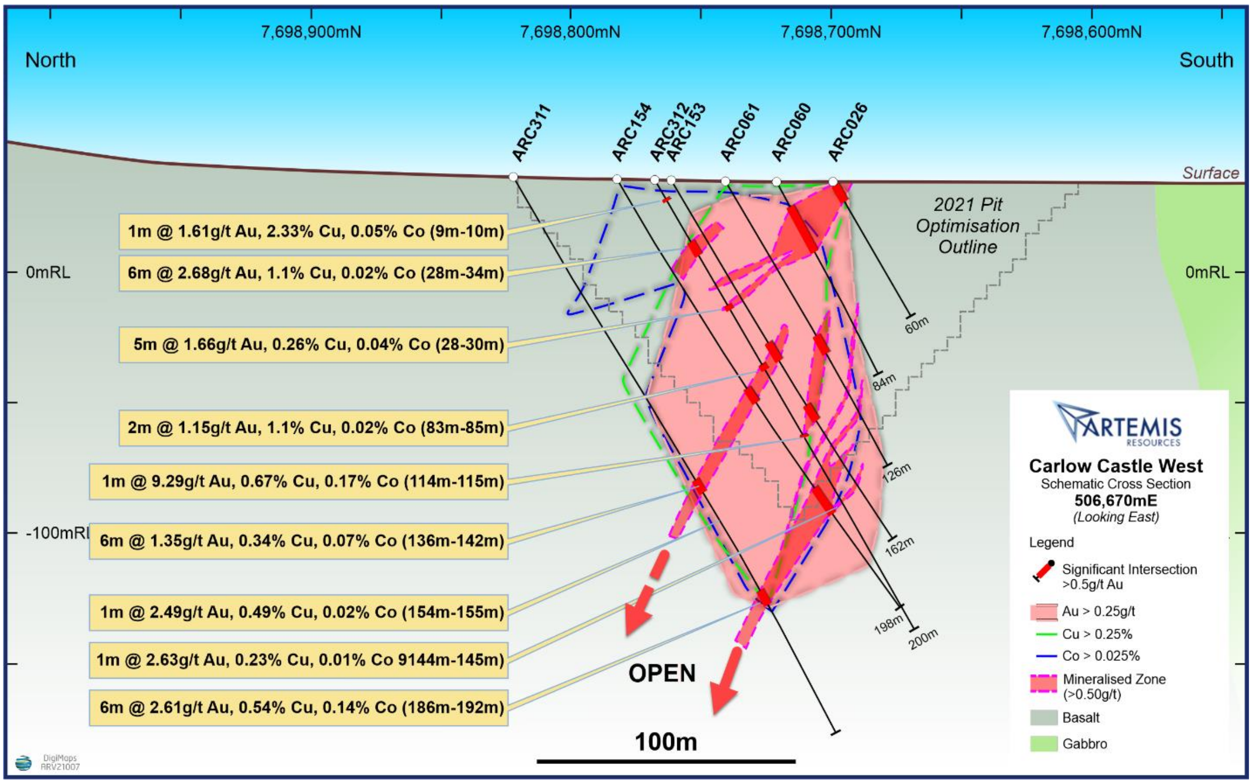


*Figure 4: Section 506670mE showing intersections for holes ARC311 and ARC312 (refer to Figure 1 for location)*

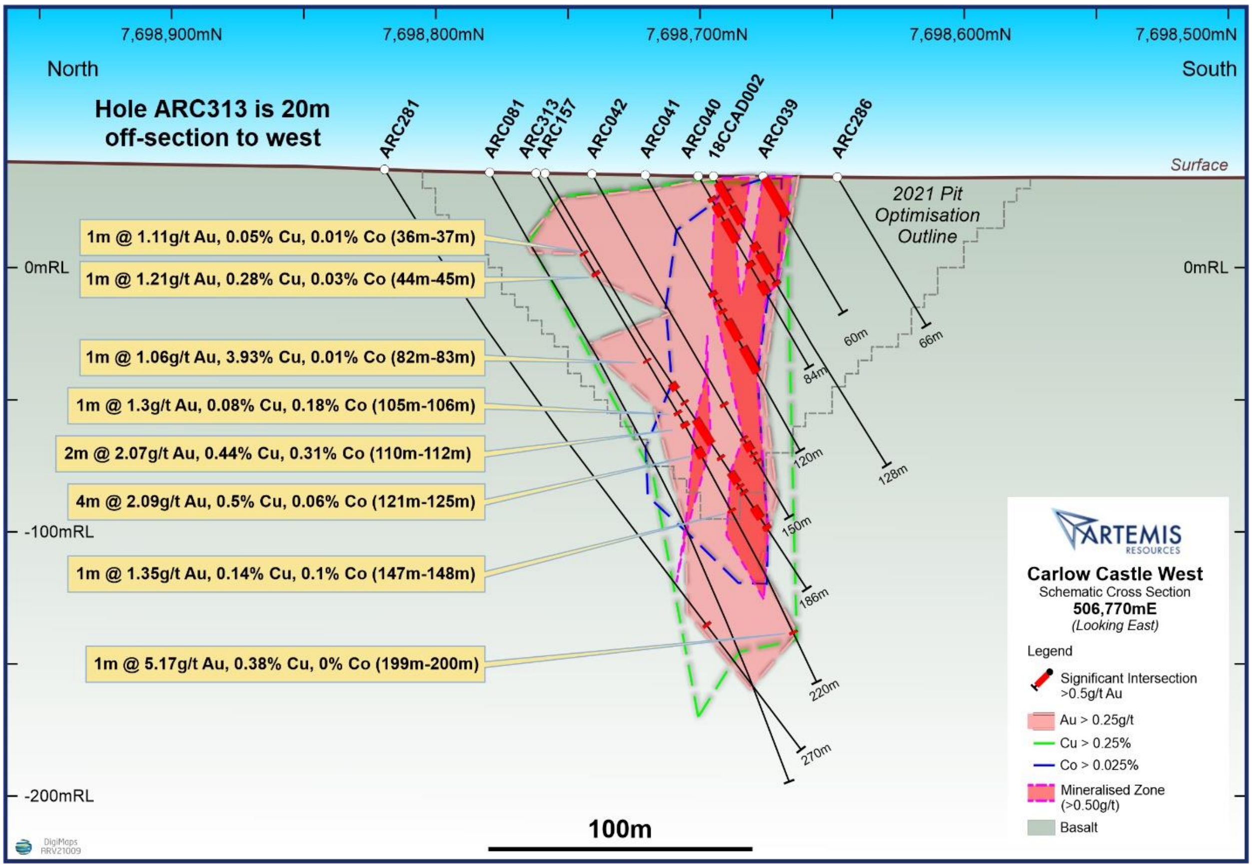


*Figure 5: Section 506770mE showing intersections for hole ARC313 (Refer to Figure 1 for location)*

Along with the potential in the Carlow Castle main zone, the Quod Est System located to the immediate north, is another area developing into a significant gold and copper resource, (refer to Figure 1 for location).

Quod Est mineralisation trends north to northeast, with a steeply dipping mineralisation plunge to the southeast, controlled by a gabbro/basalt contact. Significant results for Quod Est are included in the 23 April 2021 ASX release. Drilling at Quod Est is in progress.

Discovery of the Cross-Cut Zone by testing geophysical targets had intersected several high grade zones associated with north-westerly striking structures, (refer to Figure 1).

A new interpretation has been put forward, using airborne magnetic data and the SAM survey which suggests that Cross-Cut may be a series of *en-echelon* mineralised structures, as shown in Figure 6. Previous drilling had intersected significant copper and gold numbers, which are noted in the 23 April 2021 ASX release. Drilling at Cross-Cut is in progress.

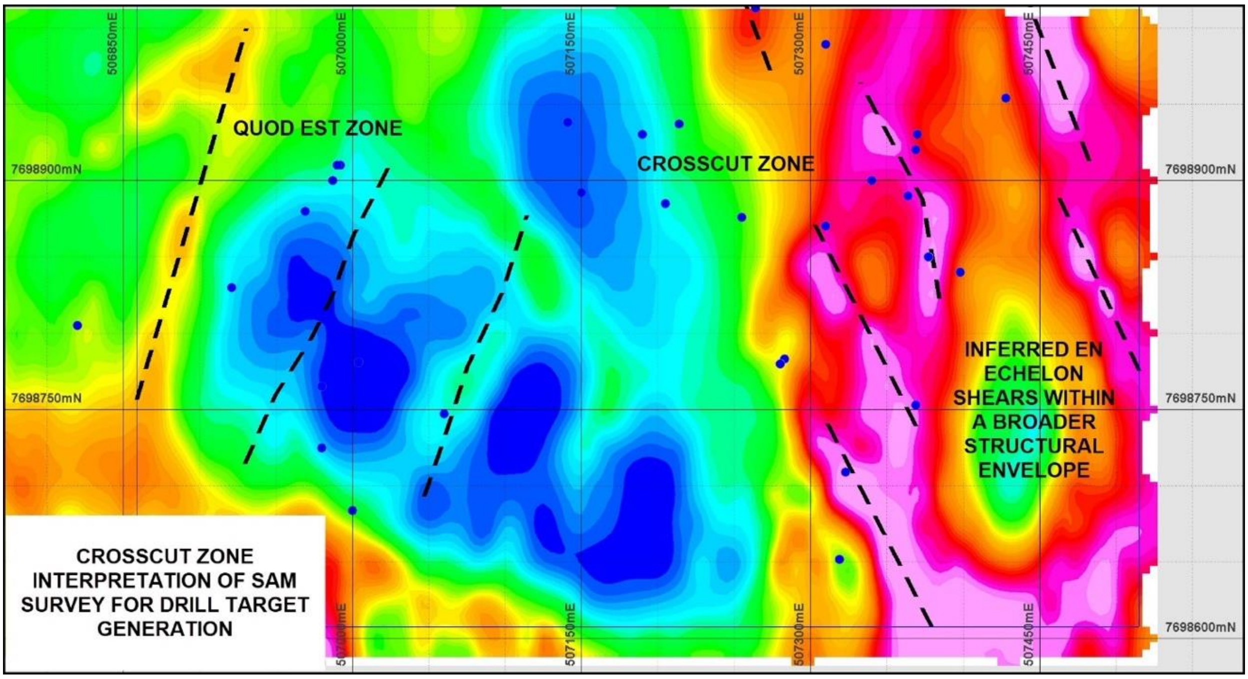


*Figure 6: Updated interpretation (plan view) of the Crosscut Zone showing the potential for repeated mineralised structures of an **en echelon** nature. Holes have been repositioned in the current drill program to test these features. Background image of SAM survey.*

## CARLOW CASTLE MINERAL RESOURCE ESTIMATE

During the quarter, the Mineral Resource for the Carlow Castle Project was updated by CSA Global using all data available as of 19 May 2021; this includes an additional 129 drill holes for 22,395 m since the 2019 Mineral Resource update. The additional drillholes were mainly at the eastern end of the Carlow Main zone and in the newly discovered Cross-Cut zone.

An open pit optimisation was completed to constrain the reported Mineral Resource. The updated Carlow Castle Mineral Resource is 14.3 million tonnes at 0.7 g/t Au, 0.4% Cu, and 0.05% Co for 320,000 ounces gold, 53,000 tonnes contained copper, and 7,000 tonnes contained cobalt.

Table 3 shows the updated resource numbers compared to the 2019 resources numbers.

*Table 3. Comparison between 2021 and 2019 Mineral Resource estimates*

| **Type** | **2021 Inferred** | | | | **2019 Inferred** | | | |
|---|---|---|---|---|---|---|---|---|
| | Tonnes (kt) | Au (g/t) | Cu (%) | Co (%) | Tonnes (kt) | Au (g/t) | Cu (%) | Co (%) |
| Oxide | 4,400 | 0.4 | 0.3 | 0.04 | 5,100 | 2.1 | 0.6 | 0.1 |
| Transitional | 3,100 | 0.7 | 0.5 | 0.06 | - | - | - | - |
| Fresh | 6,900 | 0.9 | 0.4 | 0.06 | 2,800 | 0.7 | 0.6 | 0.05 |
| Total | 14,300 | 0.7 | 0.4 | 0.05 | 8,000 | 1.6 | 0.6 | 0.08 |

The 2021 Mineral Resource is materially different to the previously reported 2019 Mineral Resource, with a significant decrease in Au, Cu, and Co grades, and an increase in resource tonnes. The contained gold decreased by 98,000 ounces, contained copper increased 5,000 tonnes, and contained cobalt was approximately the same (Figures 7 and 8).

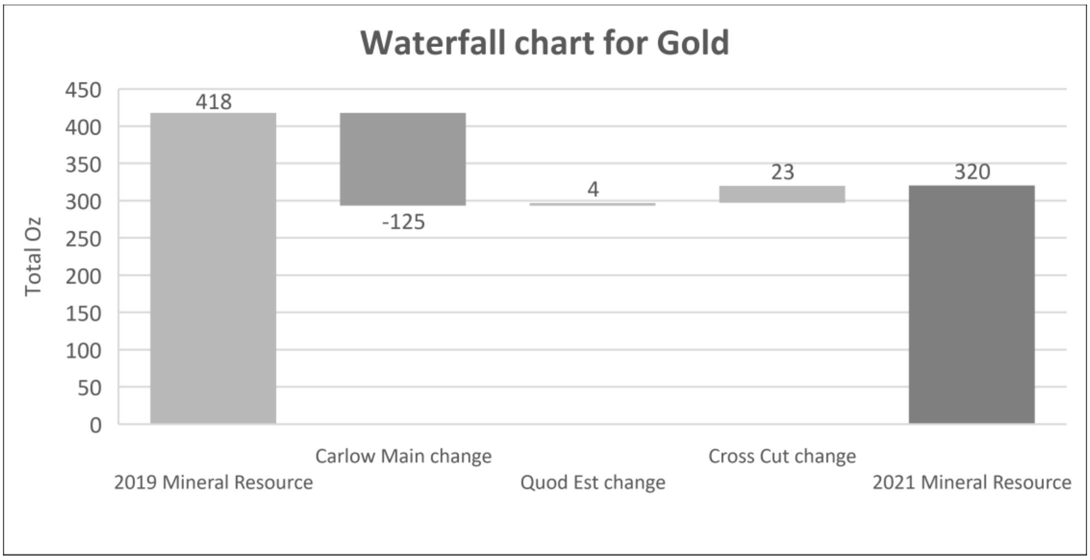


*Figure 7. Waterfall chart of changes in the MRE for contained gold between 2019 and 2021 estimates*

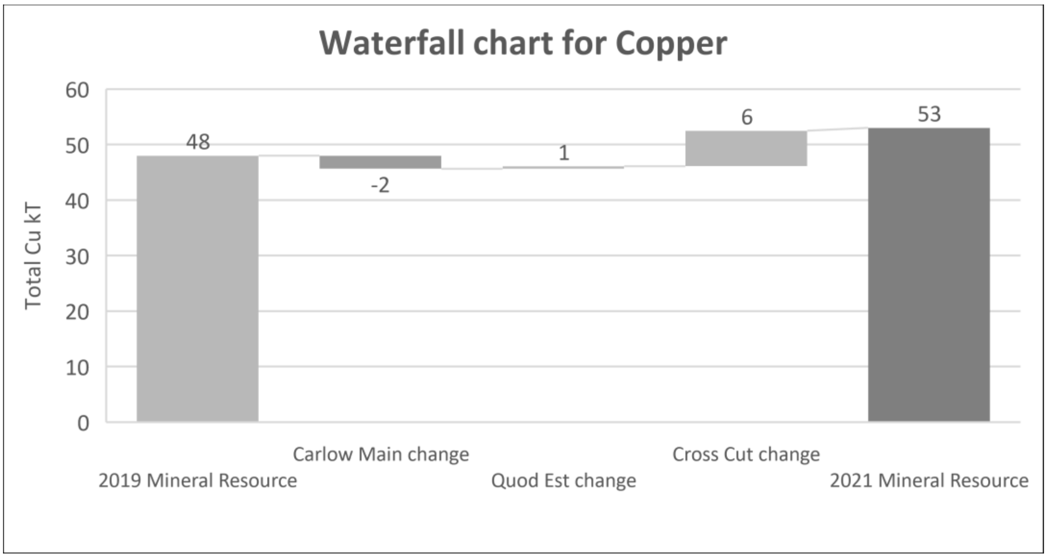


*Figure 8. Waterfall chart of changes in the MRE for contained copper between 2019 and 2021 estimates.*

### ***Comparison between the 2019 and 2021 Mineral Resource***

The 2021 Mineral Resource for Carlow Castle incorporated a significant amount of additional surface RC and diamond drilling. The decrease in resource grades and contained metal is a direct result of increased drilling below the -100mRL (approximately 140m below surface) as shown in Figure 9.

Below -100 mRL, the estimated mean gold grade decreased from 1.25 g/t Au in the 2019 model to 0.5 g/t Au in the 2021 model. Similarly, copper decreased from 0.3% Cu to 0.25% Cu, and cobalt from 0.05% Co to 0.03% Co. Material differences in the data and estimation methodology between the 2019 and 2020 Mineral Resource models are discussed below.

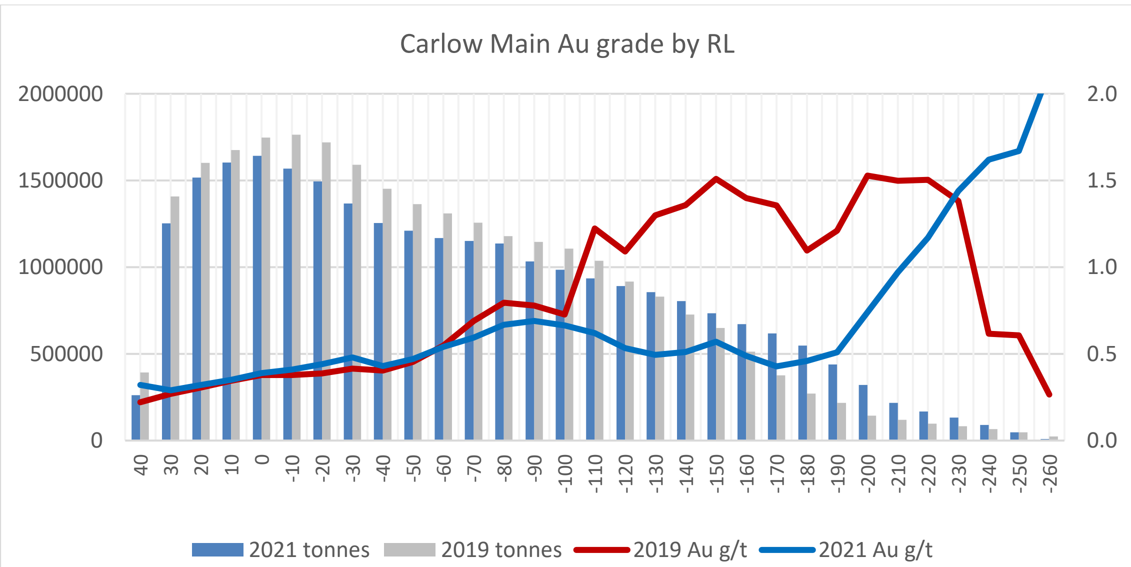


*Figure 9. Carlow Main zone 2019 and 2021 model tonnes and Au grades by RL*

### **Differences in the Input Datasets**

Several very high-grade drill holes were drilled down dip in 2018: ARC133, ARC138, ARC139, and 18CCAD010. The 2021 Mineral Resource included several additional infill drillholes drilled across the mineralisation adjacent to ARC133, ARC138 and ARC139 and 18CCAD010 that reported lower Au, Cu, and Co grades and improved the confidence in the mineralisation interpretation (Figure 10).

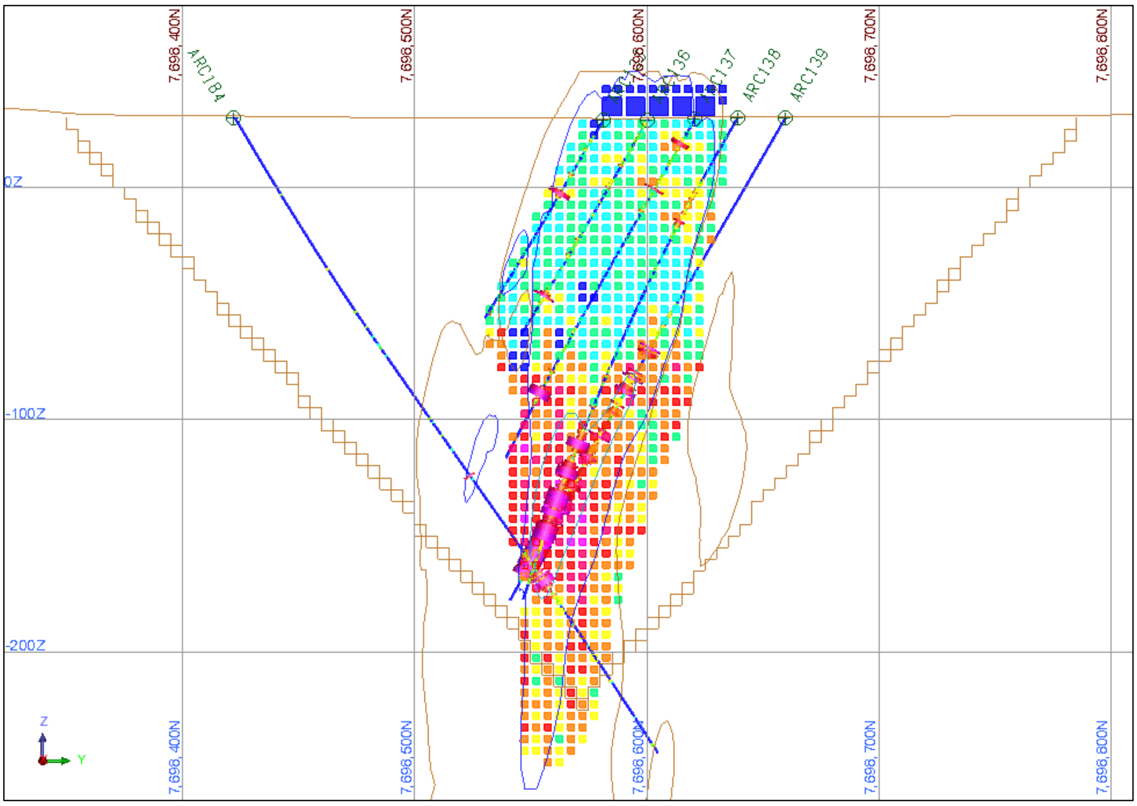


*Figure 10. Cross-section 507 520 mE showing ARC138 and ARC139, 2019 block model, and 2019 Whittle shell*

A comparison of the composite data for the Carlow Main zone showed the mean composite Au grade decreased from 0.60 g/t in 2019 to 0.55 g/t in 2021, while Cu composite grades increased from 2,935 ppm to 3,720 ppm, and Co composite grades stayed approximately the same. The changes in mean grades for Au and Cu are reflected in the Mineral Resource.

### Differences in the Interpretation Approach

The 2019 mineralisation wireframe for Carlow Main used manual sectional interpretation on 40 m spacings at a nominal 500 ppm Cu cut-off. The 2021 model utilised a probabilistic indicator modelling method to model the complex and variable grade and geological continuity effectively. Nested indicator grade shells were generated at 200 ppm Cu, 500 ppm Cu, and 0.5 g/t Au cutoffs.

The additional 0.5 g/t Au sub-domain was created for the 2021 model to constrain the influence of the high-grade down-dip drillholes. In areas with no infill drilling the 500 ppm Cu wireframes in 2019 and 2021 are generally comparable.

**Differences in the Volume Covered**

Infill drilling led to a refinement in the mineralisation interpretation and subsequent decrease in volume below -100 mRL. The decrease in volume was largely driven by infill drilling on four sections (507 380 mE; 507 500 mE; 507 540 mE; and 507 620 mE).

The additional drilling removed poorly constrained volume that had been projected down-dip in 2019, especially on the footwall.

**Differences in the Estimation Parameters**

The two models used different treatments of outlier grades. For the 2019 model, no top cuts were applied; grades above certain thresholds were restricted to a search distance of 10 m, or inside the OK panel in which they were situated. For the 2021 model, a top cut was applied to high grades before estimation.

**Differences in the Open Pit Optimisation Parameters**

Both the 2019 and 2021 models were constrained by a Whittle open pit optimisation to account for the reasonable prospects for eventual economic extraction (RPEEE) test of the JORC Code. The optimisation parameters for both models were identical except for increased commodity prices in 2021.

**Differences in Mineral Resource Classification Approach**

The resource classification followed similar approaches in the 2019 and 2021 models. In the 2019 model, the lower extents of the optimized resource shell were constrained by the extent of the mineralisation wireframe. The 2021 Whittle shell was not limited by the wireframe, but by grade and tonnage of mineralisation. Material below the -220 mRL was left unclassified based on limited drill data.  The Carlow Main zone remains open at depth.

**Differences in the Estimation Method**

The change from a localised uniform conditioning (LUC) estimation method in 2019 to a global ordinary kriging (OK) method in 2021 was based on the improved mineralisation domaining and population statistics with infill drilling.

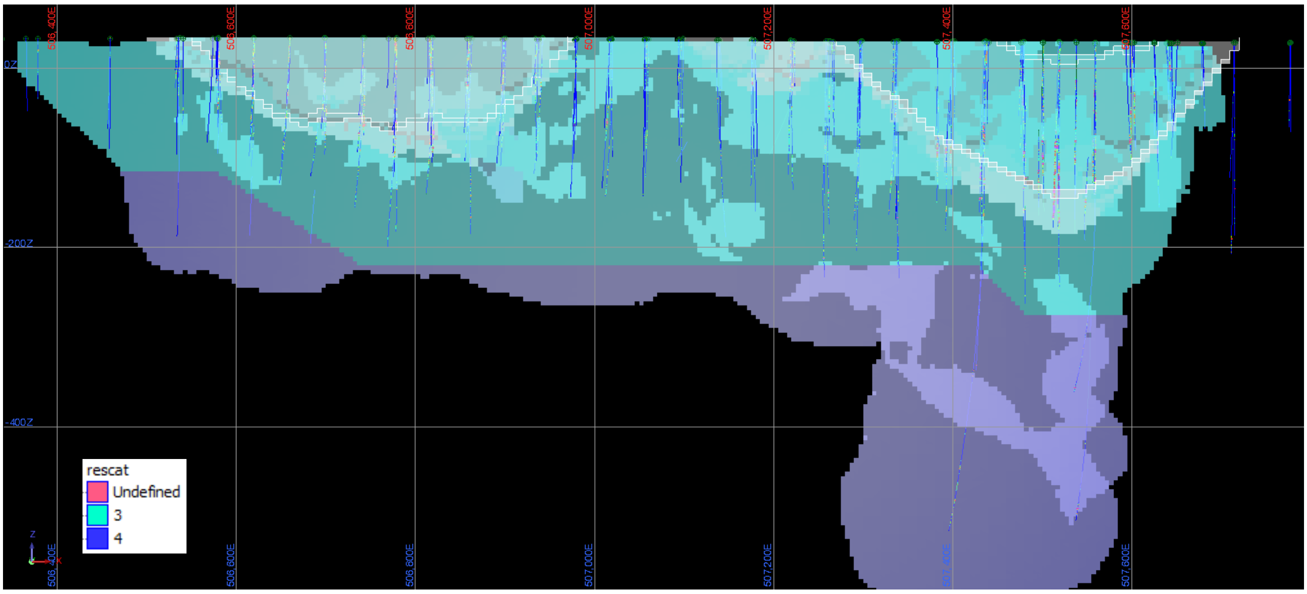


*Figure 11. 2019 block model resource classification (Inferred – 3; Unclassified – 4) with 2019 Whittle shell*

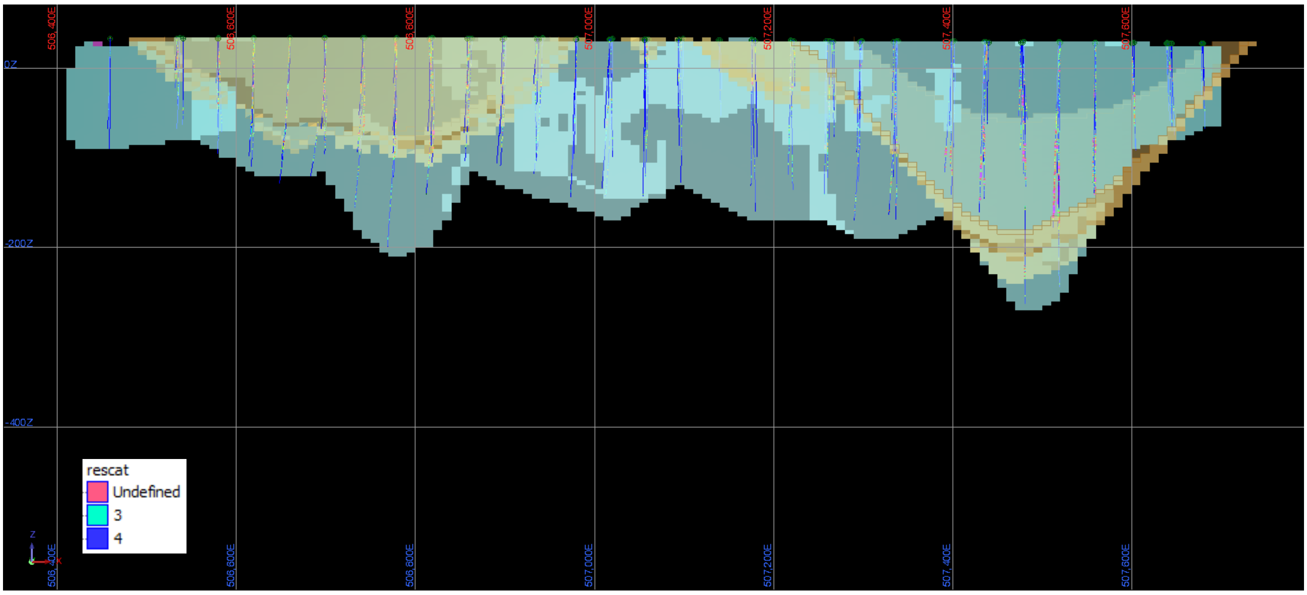


*Figure 12. 2021 block model resource classification (Inferred – 3; Unclassified – 4) with 2021 Whittle shell*

### *Summary of Findings from the 2021 and 2019 Resource Comparisons*

- Some of the 2020 and 2021 drilling has drilled through parts of the 2019 Carlow Main zone resource model.
- This drilling has reduced the volume of the mineralisation and the contained metal below the -100mRL.
- Additional resource has been added in the newly discovered Cross-cut zone.

- The balance of the 2020-2021 drilling has extended the Carlow Main mineralisation at depth; none of this additional mineralisation is reported in the current Mineral Resource as it is below the optimized resource pit shell.
- Three drillholes that were drilled down-dip had a disproportionate effect on the Au grade below -100 mRL in the 2019 model; this has been rectified by the additional infill drilling and revised domaining.
- The change from LUC to OK has not significantly changed the grade-tonnage selectivity prediction, due to the additional data available for the 2021 model.
- The optimisation parameters for the 2021 model are the same as those used in 2019, except for higher commodity prices.
- The 2019 and 2021 Inferred Mineral Resiurce classification is justified given the changes described above.

### *Strategy for Carlow Castle*

Following the Mineral Resource update for Carlow Castle, a detailed review of the current resource and exploration strategy has been conducted.

It is proposed that a structural review and interpretation be completed, and drill targets identified and tested. The new interpretation will include a re-modeling of Carlow Castle using previous drill data, current drilling data, assay results and mineralisation trends.

- Interpretation of the geology and structural setting;
- Remodel and generate additional drill targets;
- Step out drilling to add additional ounces to a currently increasing resource base;
- Regional review to stitch together data from various disciplines and generate new targets.

## MUNNI MUNNI PGE PROJECT H1 DRILL PROGRAM

Reverse Circulation (RC) drilling of 15 drill holes for 2,740 metres has been completed in May, with drill holes spread through the entire upper portion of the mineralisation, to a maximum depth of 250 metres. Samples were processed at ALS Global.

### *Joint Venture Formation with Platina Resources Limited*

Following a period of constructive dialogue, Artemis is pleased to have now executed a full Joint Venture Agreement and associated documents that allow for to formal formation of a Joint Venture over 100% of the Munni Munni Project with Platina Resources Limited in the ratio of beneficial interests, 70% ARV and 30% PGM.

### *Drilling and Multi-elements Results*

The RC drilling program was designed to confirm the PGE horizon located on the northern nose of the >20km long Munni Munni mafic intrusive Complex, on a 50 x 50 metre drill pattern.

A non-JORC resource estimation was calculated using historic holes which had defined the mineralised horizon. The recent drill program was designed to infill the historic drilling.

Holes 2MMRC0014 & 015 were targeted to test mineralisation along the poorly defined eastern side of the mafic intrusive Complex.

As the PGE horizon is essentially a stratigraphic zone, historical drilling has been widely spaced and very selectively assayed; Artemis has undertaken a broad multi-element analytical suite to improve the subtle lithological variations.

Location of Munni Munni tenements and completed drill hole collars are located in Figure 13.

Sections relating to the completed drilling are located in Figures 14 and 15.

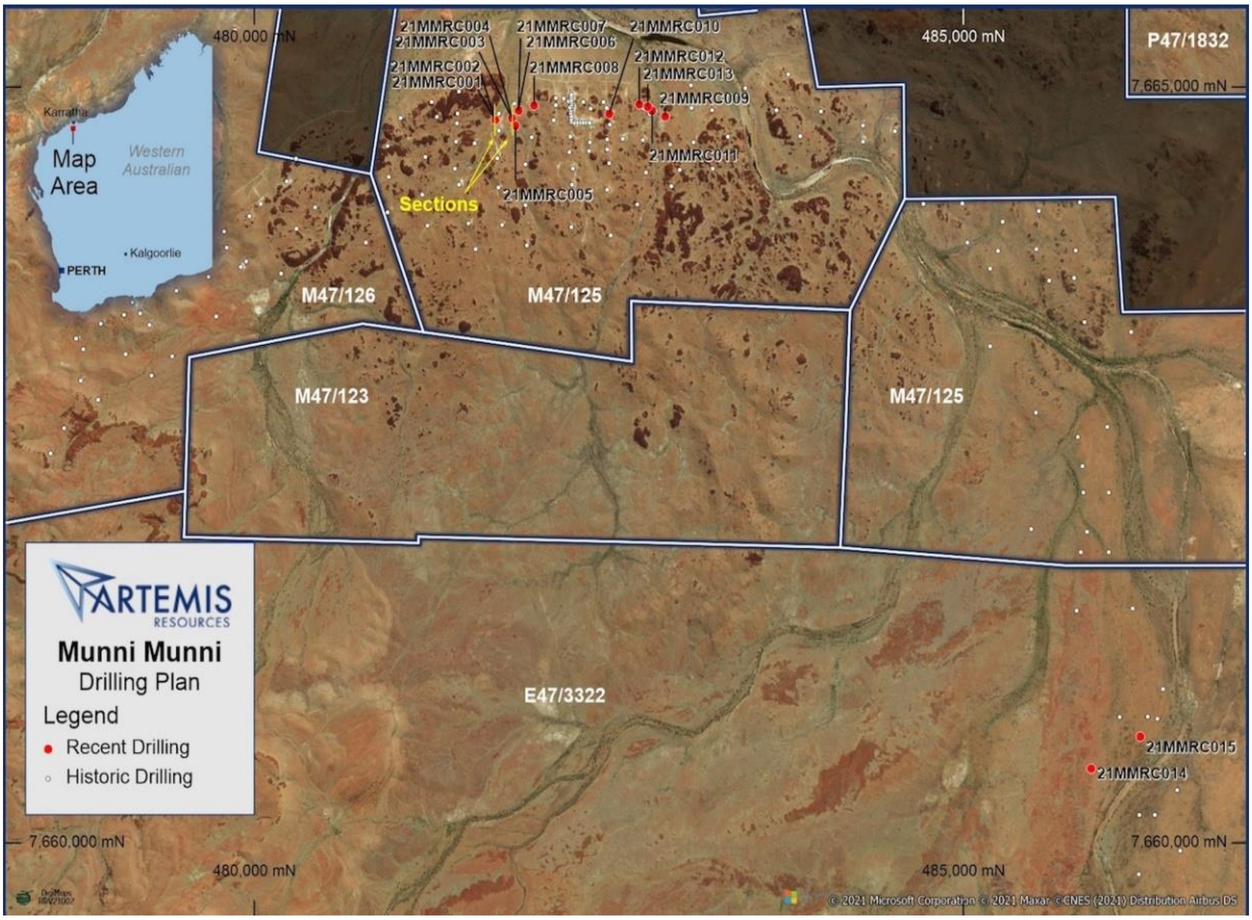


*Figure 13: Munni munni location map highlighting recent drilling in red and section locations in yellow.*

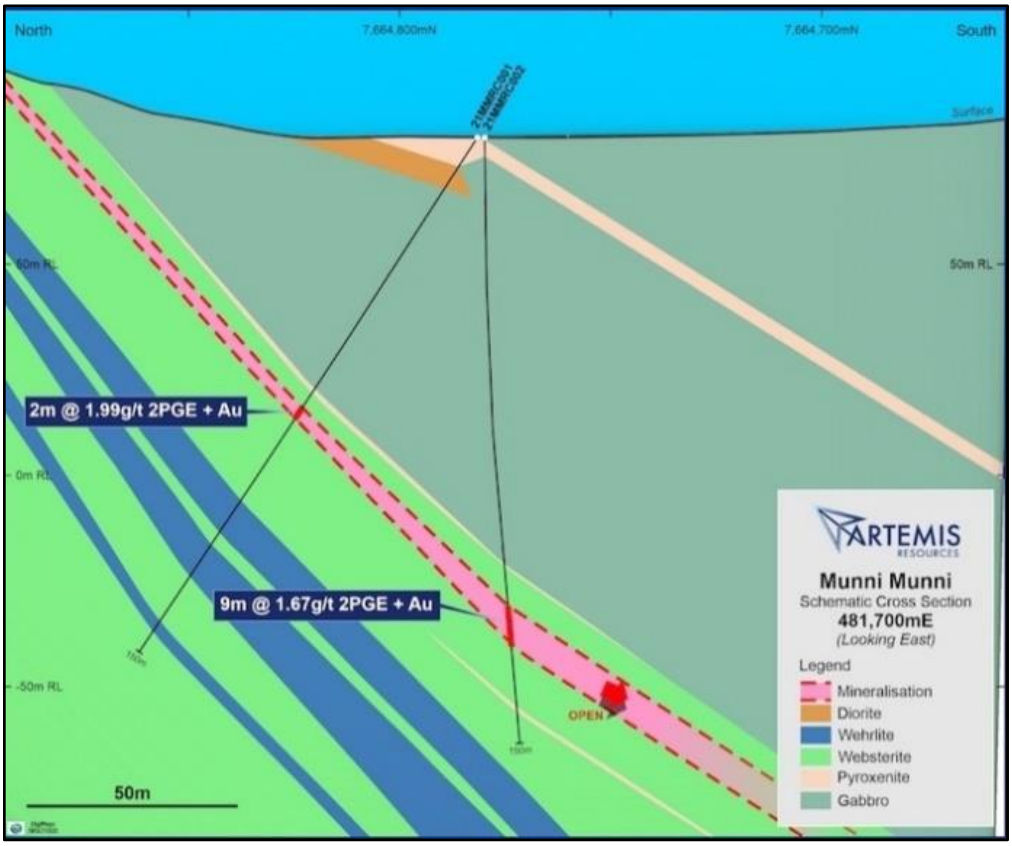


*Figure 14: Section 481800mE – 2PGE + Au intercepts.*

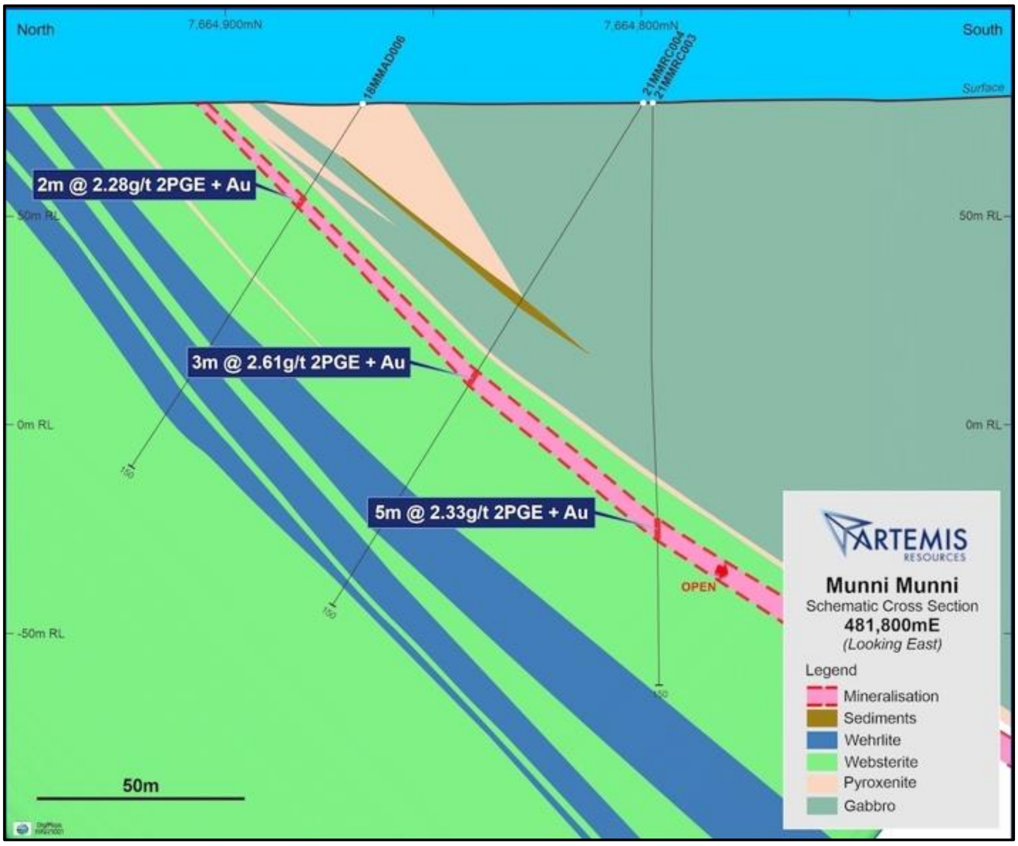


*Figure 15: Section 481700mE – 2PGE + Au intercepts.*

In the diamond drill core from 2018 essentially only gabbros and pyroxenites were recognised, likewise in the RC chips only gabbros, pyroxenites and sediments with various minor intrusive dykes were noted.

Holes 18MMAD006 with 21MMRC003 and 21MMRC004 show the direct correlation of the PGE results and the remarkable continuity and consistency of the lithochemistry.

The RC data shows slightly lower absolute results for the PGE but occurs in the same relative 'stratigraphic' position. Virtually all PGE occur within the websterite lithology with a lesser amount in the pyroxenite due the PGE occurring very close to the contact between the two units.

Significant results from the PGE zone in this drilling program include:

- 7m @ 2.20g/t 2PGE + Au (1.46g/t Pd, 0.67 g/t Pt, 0.07g/t Au) from 124m, 21MMRC005;
- 7m @ 2.35g/t 2PGE + Au (1.33g/t Pd, 0.84 g/t Pt, 0.18g/t Au), from 96m, 21MMRC006;
- 4m @ 2.45g/t 2PGE + Au (1.31g/t Pd, 0.85g/t Pt, 0.29g/t Au) from 60m, 21MMRC007;
- 5m @ 2.35g/t 2PGE + Au (1.36g/t Pd, 0.68g/t Pt, 0.31g/t Au) from 75m, 21MMRC008;
- 4m @ 2.87g/t 2PGE + Au (1.76g/t Pd, 0.89g/t Pt, 0.22g/t Au) from 115m, 2MMRC010.

## RADIO HILL FIXED-LOOP ELECTROMAGNETIC (FLEM) SURVEY

Resource Potentials Pty Ltd (ResPot) completed a high-level review of Radio Hill project tenements M47/161 and M47/337 to determine what geophysical exploration datasets are available, highlight geophysical anomaly zones, identify anomalies and target areas of interest that remain untested, or are under- tested by drilling.

The aim is to provide recommendations for additional geophysical surveying, and then to plan, monitor, process and interpret new geophysical surveys carried out over target areas of interest. FLEM surveying was completed by GAP Geophysics in April 2021.

This study identified deep and untested conductor anomaly zones of interest identified from historic deep drilling and follow-up DHEM survey data and reports, with DHEM targets shown projected to surface on the map in Figure 16.

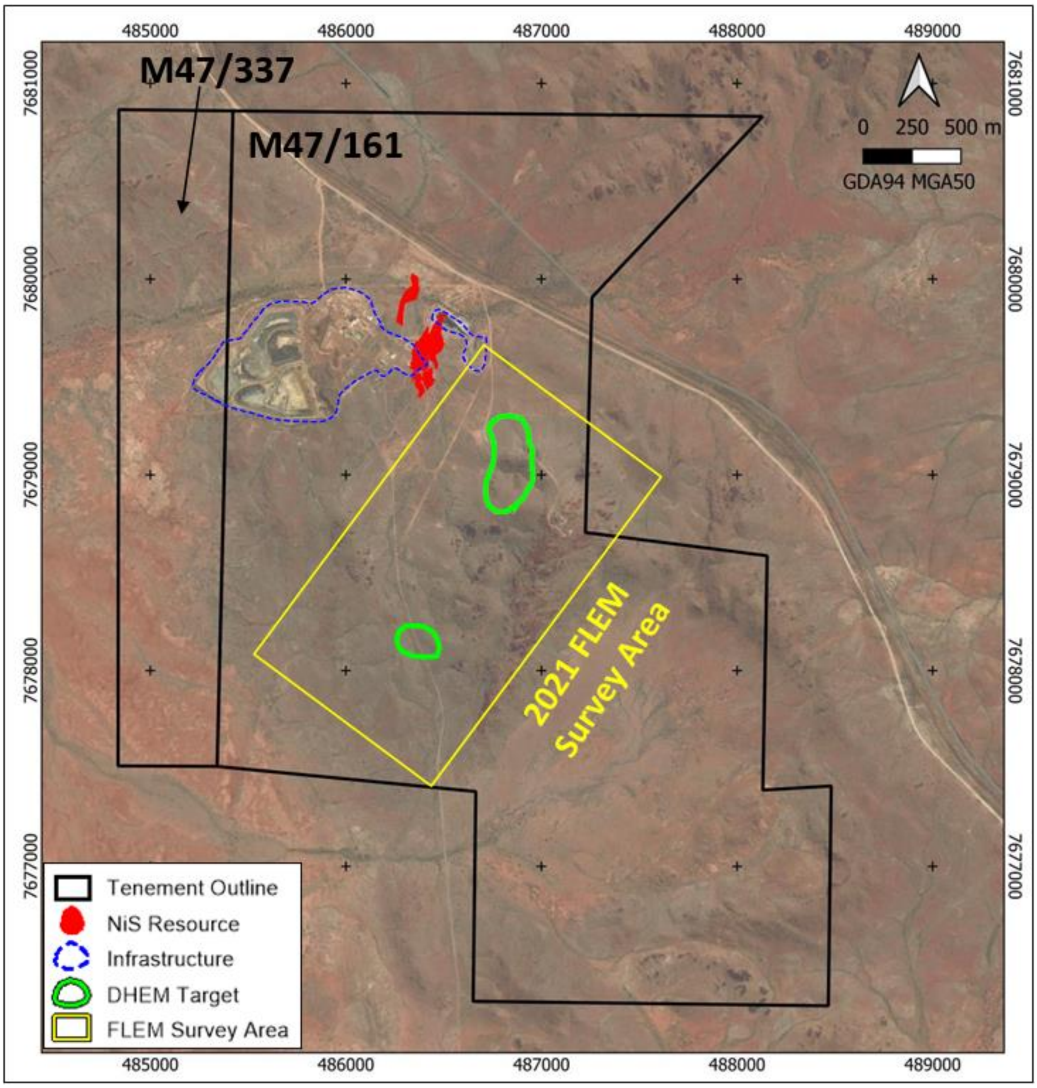


*Figure 16: Radio Hill Project tenements M47/161 and M47/337 (black outlines), mine infrastructure (dashed blue outlines), and the Radio Hill resource wireframes projected to surface (red) over a satellite image. The recent FLEM survey coverage area is outlined in yellow.*

The Radio Hill project area is still considered to hold potential for additional discoveries of Ni-Cu-Co-PGE sulphide deposits at depths >500m and to the south of the mined out NiS deposits, where long conduits likely follow the base of the intrusion. However, additional deposits are most likely located at least 600m below surface based on drilling and DHEM results and are therefore too hard to identify using airborne or surface-based EM survey methods.

Recommendations to this program are pending.

## WHUNDO GRADIENT-ARRAY INDUCED POLARISATION (GAIP) SURVEY

Artemis Resources hold mining rights to the Whundo VMS project tenements, located approximately 45km S of Karratha in Western Australia. The Whundo Zn-Cu-Pb-Ag VMS deposit has been mined in places and is now in care-and-maintenance status. The project area still holds some un-mined deposits and has potential for additional VMS deposits that remain to be discovered.

This study identified VMS mineralisation potential along a target trend located to the NE of the main Whundo deposit and covers the Yannery and Ayshia prospect areas. These prospect areas may host only weakly-conductive base metal mineralisation, such as sphalerite-rich or disseminated sulphide deposits, that were not identified using previous electromagnetic (EM) survey methods. Therefore, a new induced polarisation (IP) survey was planned and carried out over this area to identify chargeable sulphide mineralisation that was not detected by historic EM surveying. This is highlighted in green on Figure 17.

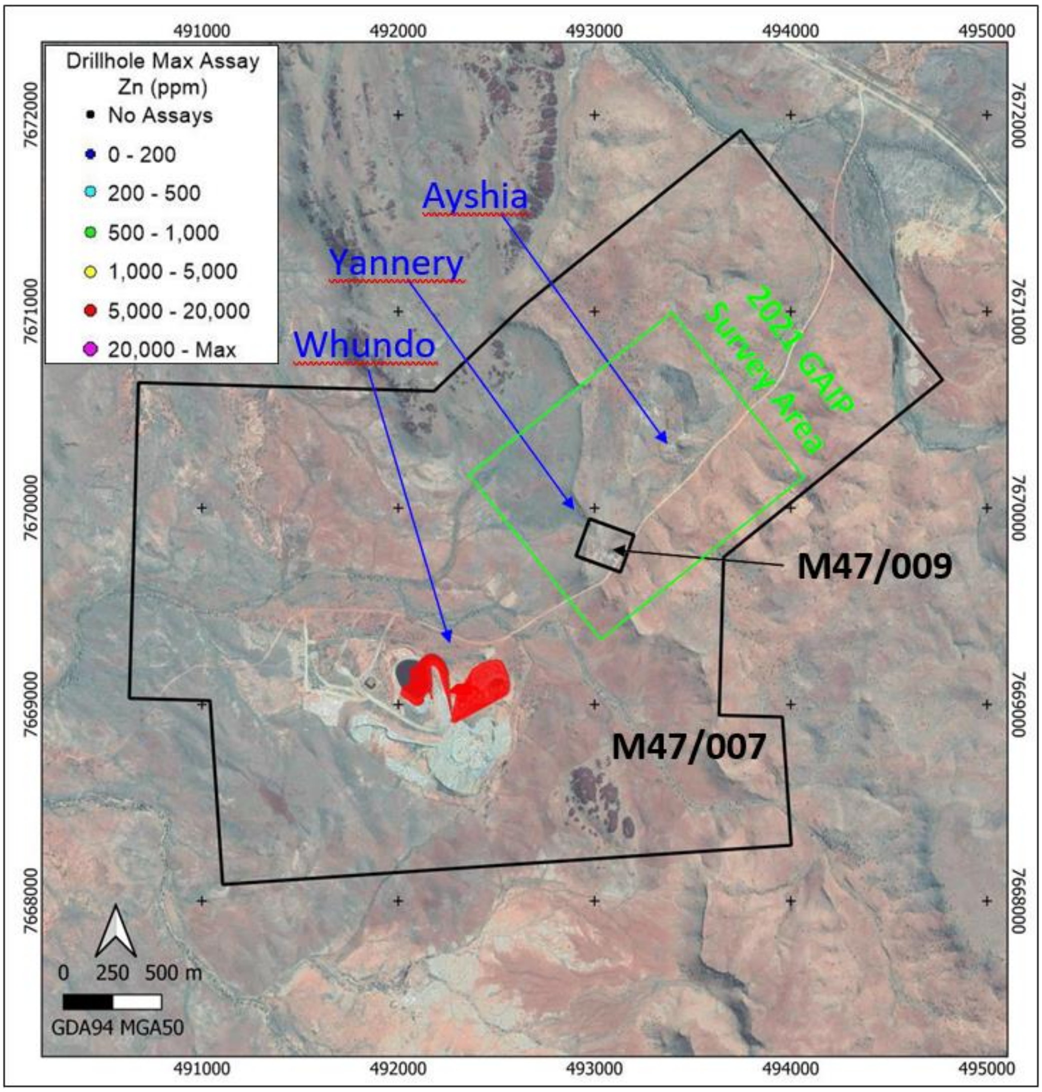


*Figure 17: Whundo Project tenements M47/007 and M47/009 (black outlines), and the Whundo resource wireframe (red) over a satellite image. The recent GAIP survey area is outlined in green, and the known prospect locations are highlighted by blue arrows*

A new GAIP survey area is recommended to be surveyed between the Whundo deposit and the recent GAIP survey area, as highlighted by the yellow square, (Figure 18).

This proposed GAIP survey area will cover a gap in survey coverage between Whundo and Yannery and cover the highest-amplitude chargeability anomaly located in the SW corner of the recent GAIP survey block.

Shallow RC drilling is recommended to test the chargeable and resistive target trend identified between Yannery and Ayshia prospects, as highlighted by the dashed black outline. This anomaly trend can be tested by RC drill transects planned across the trend. Untested VTEM target outlines to the NE and W of Whundo should also be RC drill tested. These targets are shown in Figure 18.

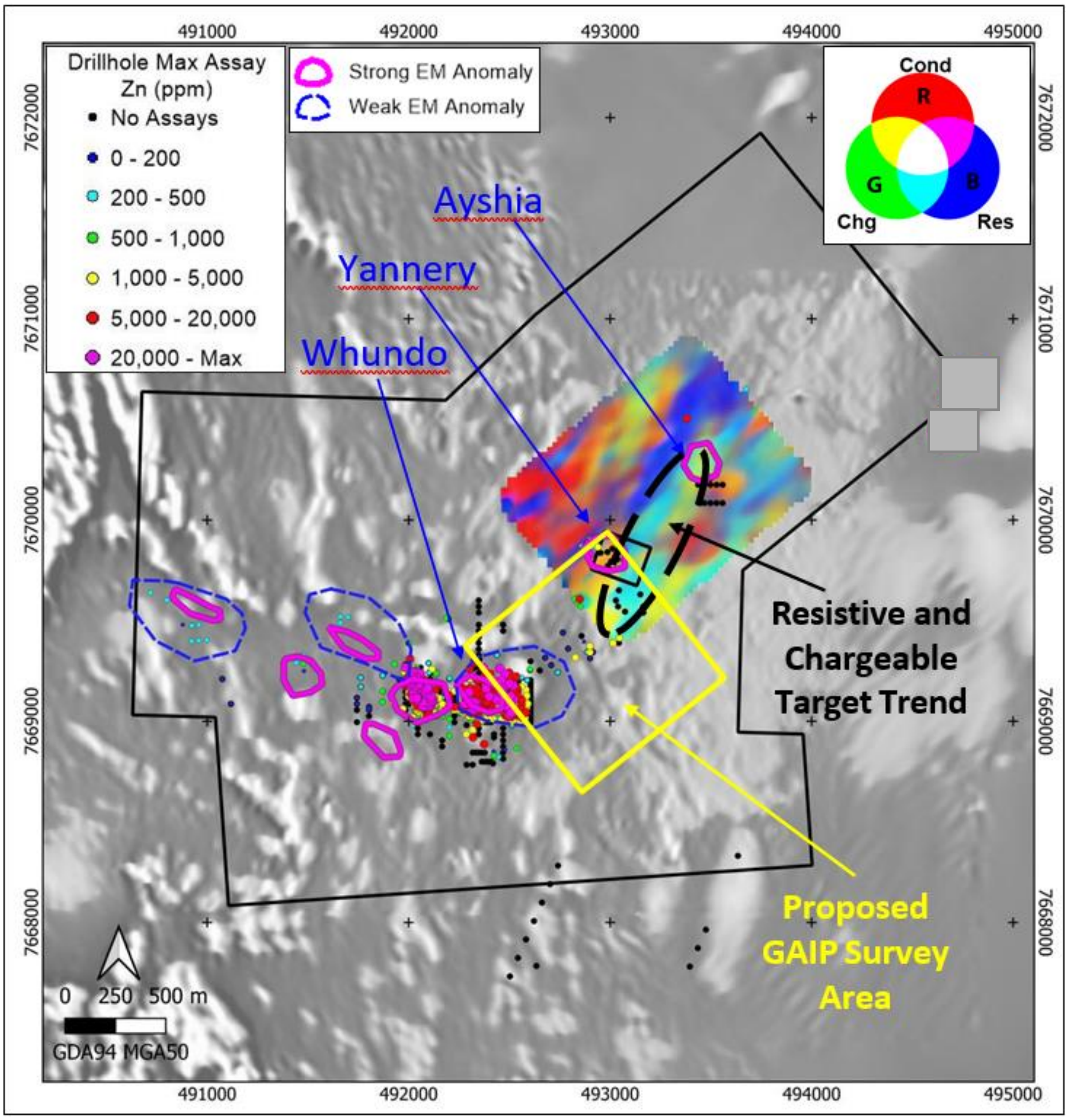


*Figure 18: Whundo Project tenements M47/007 and M47/009 (black outlines), VTEM anomaly outlines from late-time VTEM data (pink), early-time anomalies (dashed blue), historic Whundo drillhole collar locations coloured by max Zn, and a semi-transparent colour GAIP ternary image where conductivity is red, chargeability is green and resistivity is blue, all overlying a greyscale derivative magnetic image background*

## CORPORATE

*Health and Safety*

The Company continues to comply with all State guidelines to ensure the health and safety of its workforce, contractors, and the community in which it operates.

There is currently no significant impact on operations as a result of COVID-19.

Artemis has had no Occupational Health and Safety incidences during the quarter.

The Company ended the Quarter with a cash balance of $9.1m and liquid listed investments of circa $590,000.

*Capital Raising*

The Company raised $7 million at 6 cents a share in early June 2021 issuing 116.7 million new shares. The raise was strongly supported by European and Australian Institutional Investors.

*Board of Directors*

The Board welcomed Dr Simon Dominy as a Director on 1 July 2021. Dr Dominy is Adjunct Professor at the Western Australian School of Mines (WASM), Curtin University, and a Visiting Associate Professor at the Camborne School of Mines (CSM), University of Exeter, UK.

A mining geologist-engineer with over 25 years' experience, Dr Dominy has since 2015 been working with a number of private and listed entities developing/operating gold projects including: MG Gold Ltd; Novo Resources Corporation (TSV: NVO); Scotgold Resources Ltd (AIM: SGZ) and OCX Gold Group.

Between 2004-2014 he was an Executive Consultant/General Manager with the Snowden Group based in Australia and UK, including two years contracted out to LionGold Corporation (SGX: A78).

Simon is a Fellow of the Australasian Institute of Mining and Metallurgy ("FAusIMM") and the Australian Institute of Geoscientists ("FAIG").

Mr Boyd Timler resigned as a director on 24 May 2021.

*Other*

The Company spent ~$1.8 million on exploration in the quarter ended 30 June 2021, principally on the drilling programs at Carlow Castle and Munni Munni, and exploration planning at Paterson's outlined above.

Payments to Directors, related parties and their associates during the quarter amounted to $192,000, being salaries, superannuation and directors' fees.

About Artemis Resources

Artemis Resources (ASX: ARV; FRA: ATY; US: ARTTF) is a Perth-based exploration and development company, led by an experienced team that has a singular focus on delivering shareholder value from its Pilbara gold projects – the Greater Carlow Gold Project in the West Pilbara and the Paterson Central exploration project in the East Pilbara.

For more information, please visit www.artemisresources.com.au

**This report has been approved for release by the Board.**

*COMPETENT PERSONS STATEMENT PATERSONS RANGE:*

The information in this announcement that relates to Exploration Results complies with the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code) and has been compiled and assessed under the supervision of Dr Jayson Meyers, a consultant to Artemis Resources Limited and a Director of Resource Potentials Pty Ltd. Dr Meyers is a Fellow of the Australasian Institute of Geoscientists. He has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the JORC Code. Dr Meyers consents to the inclusion in this announcement of the matters based on his information in the form and context in which it appears. Dr Meyers does not hold securities in the Company.

*COMPETENT PERSONS STATEMENT WEST PILBARA:*

The information in this announcement that relates to Exploration Results is based on information compiled or reviewed by Steve Boda, who is a Member of the Australasian Institute of Geoscientists (AIG). Mr Boda is an employee of Artemis Resources Limited. Mr Boda has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Boda consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears.

*COMPETENT PERSONS STATEMENT MINERAL RESOURCE ESTIMATION (MRE)*

The information in this report that relates to Mineral Resources is based on information compiled by Mr Phil Jankowski, who is a Member of the Australasian Institute of Mining and Metallurgy. Mr Jankowski has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Jankowski consents to the inclusion in this website of the matters based on this information in the form and context in which it appears.

Tenement List - All tenements are located in Western Australia.

| Project | Tenement | Status | Company |
|---|---|---|---|
| Purdy's Reward | L47/782 | Pending | KML No 2 Pty Ltd |
| Carlow Castle | E47/1797 | Live | KML No 2 Pty Ltd |
| Ruth Well | P47/1929 | Live | KML No 2 Pty Ltd |
| | E47/3719 | Live | KML No 2 Pty Ltd |
| | E47/3487[1] | Live | Elysian Resources Pty Ltd |
| | E47/3341[1] | Live | Hard Rock Resources Pty Ltd |
| 47 Patch | E47/3361[1] | Live | Elysian Resources Pty Ltd |
| Elysian / Hard Rock | E47/3564[1] | Live | Elysian Resources Pty Ltd |
| | E47/3340[1] | Live | Hard Rock Resources Pty Ltd |
| | E47/3390[1] | Live | Hard Rock Resources Pty Ltd |
| | P47/1832[1] | Live | Hard Rock Resources Pty Ltd |
| | P47/1881[1] | Live | Hard Rock Resources Pty Ltd |
| | E47/3534[1] | Live | Jindalee Resources Pty Ltd |
| | E47/3535[1] | Pending | Jindalee Resources Pty Ltd |
| | P47/1833[1] | Pending | Jindalee Resources Pty Ltd |
| Whundo | L47/163 | Live | Fox Radio Hill Pty Ltd |
| | M47/7 | Live | Fox Radio Hill Pty Ltd |
| | M47/9 | Live | Fox Radio Hill Pty Ltd |
| Radio Hill | M47/161 | Live | Fox Radio Hill Pty Ltd |
| | M47/337 | Live | Fox Radio Hill Pty Ltd |
| | L47/93 | Live | Fox Radio Hill Pty Ltd |
| Weerianna | M47/223[2] | Live | Western Metals Pty Ltd |
| Silica Hills | L47/781 | Pending | KML No 2 Pty Ltd |

| | | | |
|---|---|---|---|
| | E47/1746 | Live | KML No 2 Pty Ltd |
| Telfer | E45/5276 | Live | Armada Mining Pty Ltd |
| Sing Well | P47/1622 | Live | KML No 2 Pty Ltd |
| | P47/1112 | Live | KML No 2 Pty Ltd |
| Nickol River | P47/1126 | Live | KML No 2 Pty Ltd |
| | P47/1925 | Live | KML No 2 Pty Ltd |
| Munni Munni | E47/3322[5] | Live | Karratha Metals Pty Ltd |
| | M47/123[5] | Live | Platina Resources Ltd |
| | M47/124[5] | Live | Platina Resources Ltd |
| | M47/125[5] | Live | Platina Resources Ltd |
| | M47/126[5] | Live | Platina Resources Ltd |

1– 70% Artemis – Karratha Gold Joint Venture

2 – 80% Artemis

3 – 70% Artemis

4 – 70% Artemis – Joint Venture with Platina Resources

*Table 4:Carlow Drill Collar Survey June Q2 2021 (MGA50 Grid)*

| *HoleID* | *Type* | *Easting GDA94* | *Northing GDA94* | *RL (m)* | *Dip* | *Azimuth Mag* | *Total Depth (m)* |
|---|---|---|---|---|---|---|---|
| ARC310 | RC | 506720 | 7698808 | 37 | -60.71 | 179.89 | 260 |
| ARC311 | RC | 506670 | 7698822 | 37 | -60.53 | 180.39 | 260 |
| ARC312 | RC | 506670 | 7698768 | 36 | -59.99 | 180.03 | 200 |
| ARC313 | RC | 506760 | 7698762 | 36 | -60.65 | 180.05 | 220 |
| ARC315 | RC | 506560 | 7698740 | 35 | -60.14 | 180 | 150 |
| 21CCDD001 | DD | 507540 | 7698470 | 30 | -60.11 | 359.72 | 300.2 |
| 21CCDD002 | DD | 507580 | 7698590 | 30 | -60.27 | 1.92 | 110.6 |
| 21CCDD003 | DD | 507580 | 7698550 | 30 | -60.43 | 359.96 | 177.3 |

*Table 5: Significant results for the Q2 June RC drilling at Carlow Castle. Results are >0.5g/t Au or >0.5% Cu*

| ***Hole No*** | ***From (m)*** | ***To (m)*** | ***Downhole Width (m)*** | ***Au (g/t)*** | ***Cu (%)*** | ***Co (%)*** |
|---|---|---|---|---|---|---|
| ARC310 | 34 | 35 | 1 | 0.300 | 0.014 | 0.042 |
| ARC310 | 40 | 41 | 1 | **0.900** | **1.585** | 0.009 |
| ARC310 | 53 | 54 | 1 | **1.430** | **1.700** | **0.050** |
| ARC310 | 54 | 55 | 1 | **47.300** | **11.250** | **0.065** |
| ARC310 | 55 | 56 | 1 | **26.500** | **9.510** | **0.060** |
| ARC310 | 56 | 57 | 1 | **9.700** | **9.900** | **0.057** |
| ARC310 | 57 | 58 | 1 | **4.350** | **6.900** | **0.050** |
| ARC310 | 58 | 59 | 1 | **0.530** | **3.250** | 0.035 |
| ARC310 | 59 | 60 | 1 | 0.320 | 0.266 | 0.009 |
| ARC310 | 112 | 113 | 1 | **1.420** | 0.053 | 0.027 |
| ARC310 | 113 | 114 | 1 | 0.380 | **0.870** | **0.074** |
| ARC310 | 129 | 130 | 1 | **0.670** | 0.264 | **0.141** |
| ARC310 | 136 | 137 | 1 | 0.320 | 0.145 | 0.007 |
| ARC310 | 137 | 138 | 1 | 0.320 | 0.116 | 0.009 |
| ARC310 | 138 | 139 | 1 | 0.450 | 0.090 | 0.034 |
| ARC310 | 142 | 143 | 1 | 0.370 | **0.640** | 0.036 |
| ARC310 | 143 | 144 | 1 | 0.330 | 0.159 | 0.012 |
| ARC310 | 168 | 169 | 1 | **1.650** | 0.177 | **0.102** |
| ARC310 | 169 | 170 | 1 | **1.570** | 0.136 | **0.155** |
| ARC310 | 204 | 205 | 1 | 0.330 | **0.573** | 0.029 |
| ARC310 | 214 | 215 | 1 | 0.450 | 0.068 | **0.228** |
| ARC310 | 222 | 223 | 1 | 0.300 | 0.211 | 0.011 |
| ARC310 | 225 | 226 | 1 | **1.370** | 0.063 | 0.003 |
| | | | | | | |
| ARC311 | 6 | 7 | 1 | **0.550** | 0.139 | 0.007 |
| ARC311 | 45 | 46 | 1 | **0.570** | 0.180 | 0.021 |
| ARC311 | 53 | 54 | 1 | 0.280 | 0.126 | **0.060** |
| ARC311 | 56 | 57 | 1 | 0.480 | 0.181 | **0.082** |
| ARC311 | 100 | 101 | 1 | **0.540** | 0.214 | **0.066** |
| ARC311 | 109 | 110 | 1 | 0.320 | 0.090 | **0.060** |
| ARC311 | 117 | 118 | 1 | 0.280 | **0.715** | 0.014 |
| ARC311 | 132 | 133 | 1 | 0.330 | 0.047 | 0.010 |
| ARC311 | 136 | 137 | 1 | **2.550** | 0.223 | **0.058** |
| ARC311 | 139 | 140 | 1 | **1.650** | **0.570** | **0.058** |

| Hole No | From (m) | To (m) | Downhole Width (m) | Au (g/t) | Cu (%) | Co (%) |
|---|---|---|---|---|---|---|
| ARC311 | 140 | 141 | 1 | **2.870** | **0.565** | **0.157** |
| ARC311 | 141 | 142 | 1 | **0.690** | 0.269 | **0.072** |
| ARC311 | 154 | 155 | 1 | **2.490** | 0.486 | 0.016 |
| ARC311 | 175 | 176 | 1 | 0.460 | 0.068 | 0.012 |
| ARC311 | 176 | 177 | 1 | **0.570** | 0.099 | 0.016 |
| ARC311 | 181 | 182 | 1 | 0.340 | 0.090 | 0.008 |
| ARC311 | 182 | 183 | 1 | **0.780** | 0.187 | 0.011 |
| ARC311 | 186 | 187 | 1 | **0.650** | 0.155 | 0.024 |
| ARC311 | 187 | 188 | 1 | **6.270** | **1.075** | **0.054** |
| ARC311 | 189 | 190 | 1 | **1.460** | 0.106 | **0.083** |
| ARC311 | 190 | 191 | 1 | **5.930** | **1.630** | **0.610** |
| ARC311 | 191 | 192 | 1 | **1.140** | 0.199 | **0.061** |
| | | | | | | |
| ARC312 | 9 | 10 | 1 | **1.610** | **2.330** | **0.053** |
| ARC312 | 28 | 29 | 1 | **0.860** | 0.340 | 0.025 |
| ARC312 | 29 | 30 | 1 | **0.840** | 0.385 | 0.030 |
| ARC312 | 30 | 31 | 1 | **1.350** | **0.621** | 0.015 |
| ARC312 | 31 | 32 | 1 | **6.950** | **0.570** | 0.011 |
| ARC312 | 32 | 33 | 1 | **1.700** | **0.841** | 0.013 |
| ARC312 | 33 | 34 | 1 | **4.370** | **3.830** | 0.022 |
| ARC312 | 35 | 36 | 1 | 0.320 | 0.297 | 0.011 |
| ARC312 | 46 | 47 | 1 | 0.330 | 0.186 | **0.053** |
| ARC312 | 47 | 48 | 1 | 0.420 | 0.196 | 0.045 |
| ARC312 | 49 | 50 | 1 | 0.290 | 0.282 | 0.026 |
| ARC312 | 53 | 54 | 1 | 0.480 | 0.363 | 0.030 |
| ARC312 | 55 | 56 | 1 | 0.310 | 0.059 | 0.010 |
| ARC312 | 56 | 57 | 1 | **2.440** | 0.125 | 0.015 |
| ARC312 | 57 | 58 | 1 | **1.450** | 0.328 | 0.016 |
| ARC312 | 59 | 60 | 1 | 0.260 | 0.066 | 0.018 |
| ARC312 | 60 | 61 | 1 | **4.010** | **0.713** | **0.118** |
| ARC312 | 66 | 67 | 1 | **0.880** | 0.051 | **0.397** |
| ARC312 | 77 | 78 | 1 | 0.490 | **0.563** | 0.025 |
| ARC312 | 78 | 79 | 1 | 0.480 | **1.410** | 0.018 |
| ARC312 | 83 | 84 | 1 | **0.760** | 0.073 | **0.050** |
| ARC312 | 84 | 85 | 1 | **1.530** | 0.304 | 0.014 |
| ARC312 | 93 | 94 | 1 | 0.300 | **0.664** | 0.013 |
| ARC312 | 105 | 106 | 1 | **0.560** | 0.295 | 0.013 |
| ARC312 | 114 | 115 | 1 | **9.290** | **0.673** | **0.169** |
| ARC312 | 115 | 116 | 1 | 0.380 | 0.098 | 0.014 |
| ARC312 | 116 | 117 | 1 | 0.390 | 0.112 | 0.015 |
| ARC312 | 118 | 119 | 1 | **0.570** | 0.049 | 0.022 |
| ARC312 | 125 | 126 | 1 | 0.370 | 0.221 | 0.030 |
| ARC312 | 134 | 135 | 1 | 0.330 | 0.099 | 0.023 |
| ARC312 | 144 | 145 | 1 | **2.630** | 0.234 | 0.006 |
| ARC313 | 14 | 15 | 1 | 0.460 | 0.058 | 0.010 |
| ARC313 | 35 | 36 | 1 | **1.110** | 0.046 | 0.010 |
| ARC313 | 43 | 44 | 1 | 0.480 | 0.128 | 0.034 |
| ARC313 | 44 | 45 | 1 | **1.210** | 0.283 | 0.028 |
| ARC313 | 82 | 83 | 1 | **1.060** | **3.930** | 0.010 |
| ARC313 | 90 | 91 | 1 | 0.340 | **2.110** | 0.011 |
| ARC313 | 103 | 104 | 1 | 0.320 | 0.222 | 0.030 |
| ARC313 | 105 | 106 | 1 | **1.300** | 0.079 | **0.185** |
| ARC313 | 110 | 111 | 1 | **0.990** | 0.421 | **0.570** |

| Hole No | From (m) | To (m) | Downhole Width (m) | Au (g/t) | Cu (%) | Co (%) |
|---|---|---|---|---|---|---|
| ARC313 | 111 | 112 | 1 | **3.150** | 0.463 | 0.047 |
| ARC313 | 121 | 122 | 1 | **2.170** | 0.018 | **0.083** |
| ARC313 | 122 | 123 | 1 | 0.360 | 0.156 | **0.083** |
| ARC313 | 124 | 125 | 1 | **5.760** | **1.740** | **0.071** |
| ARC313 | 130 | 131 | 1 | 0.370 | 0.050 | 0.007 |
| ARC313 | 140 | 141 | 1 | 0.440 | 0.172 | **0.062** |
| ARC313 | 147 | 148 | 1 | **1.350** | 0.145 | **0.098** |
| ARC313 | 148 | 149 | 1 | 0.360 | 0.091 | 0.046 |
| ARC313 | 151 | 152 | 1 | **0.640** | 0.393 | **0.243** |
| ARC313 | 152 | 153 | 1 | 0.420 | 0.128 | **0.090** |
| ARC313 | 170 | 171 | 1 | 0.280 | **0.574** | 0.013 |
| ARC313 | 195 | 196 | 1 | **0.730** | **2.070** | 0.007 |
| ARC313 | 199 | 200 | 1 | **5.170** | 0.376 | 0.002 |
| | | | | | | |
| ARC315 | NSI | | | | | |

*Table 6: Drill Collar Locations for Munni Munni*

| Hole ID | Type | Easting | Northing | RL | Grid | Azimuth (True) | Dip | Depth |
|---|---|---|---|---|---|---|---|---|
| 18MMAD001 | DDH | 482199.26 | 7664902.04 | 86.73 | MGA-50 | 4.11 | -60.1 | 100.5 |
| 18MMAD002 | DDH | 482660.00 | 7664952.82 | 81.86 | MGA-50 | 5.17 | -60.1 | 101.8 |
| 18MMAD003 | DDH | 482340.74 | 7664909.75 | 89.17 | MGA-50 | 5.77 | -60.2 | 100 |
| 18MMAD004 | DDH | 482454.88 | 7664874.92 | 85.70 | MGA-50 | 4.47 | -59.2 | 120 |
| 18MMAD005 | DDH | 481898.96 | 7664872.90 | 83.68 | MGA-50 | 0 | -70 | 100 |
| 18MMAD006 | DDH | 481796.57 | 7664865.99 | 82.57 | MGA-50 | 0.84 | -60.3 | 108.8 |
| 18MMAD007 | DDH | 482143.34 | 7664922.90 | 94.51 | MGA-50 | 0 | -80 | 110 |
| 18MMAD008 | DDH | 482454.50 | 7664875.00 | 85.70 | MGA-50 | 0 | -80 | 110 |
| 20MMRC001 | RC | 485794.94 | 7661174.67 | 96.57 | MGA-50 | 90 | -60 | 160 |
| 20MMRC002 | RC | 485863.85 | 7662228.67 | 92.18 | MGA-50 | 90 | -60 | 200 |
| 20MMRC003 | RC | 485901.19 | 7662571.11 | 91.25 | MGA-50 | 90 | -60 | 180 |
| 20MMRC004 | RC | 486293.89 | 7663240.68 | 89.82 | MGA-50 | 90 | -60 | 80 |
| 20MMRC005 | RC | 481923.45 | 7664887.17 | 82.84 | MGA-50 | 0 | -60 | 100 |
| 20MMRC006 | RC | 482201.58 | 7664896.23 | 86.94 | MGA-50 | 0 | -90 | 160 |
| 20MMRC007 | RC | 482492.96 | 7664856.56 | 88.47 | MGA-50 | 180 | -80 | 190 |
| 20MMRC008 | RC | 479730.23 | 7664005.47 | 102.58 | MGA-50 | 330 | -70 | 150 |
| 20MMRC009 | RC | 480200.52 | 7663223.59 | 104.73 | MGA-50 | 0 | -90 | 150 |
| 20MMRC010 | RC | 480309.48 | 7662943.32 | 106.57 | MGA-50 | 0 | -90 | 160 |
| 20MMRC011 | RC | 479598.19 | 7663830.25 | 123.01 | MGA-50 | 320 | -60 | 200 |
| 20MMRC012 | RC | 479696.24 | 7663809.66 | 112.06 | MGA-50 | 330 | -60 | 198 |
| 21MMRC001 | RC | 481699.73 | 7664781.70 | 83.18 | MGA-51 | 0.00 | -60 | 150 |
| 21MMRC002 | RC | 481699.72 | 7664779.73 | 83.07 | MGA-52 | 0.00 | -90 | 150 |
| 21MMRC003 | RC | 481814.44 | 7664795.24 | 83.58 | MGA-53 | 0.00 | -90 | 150 |
| 21MMRC004 | RC | 481814.52 | 7664797.22 | 83.51 | MGA-54 | 0.00 | -60 | 150 |
| 21MMRC005 | RC | 481844.03 | 7664739.96 | 84.73 | MGA-55 | 0.00 | -60 | 150 |
| 21MMRC006 | RC | 481862.44 | 7664843.06 | 83.49 | MGA-56 | 0.00 | -90 | 150 |
| 21MMRC007 | RC | 481864.87 | 7664843.26 | 83.67 | MGA-57 | 30.00 | -60 | 150 |
| 21MMRC008 | RC | 481974.29 | 7664875.13 | 86.89 | MGA-58 | 20.00 | -60 | 150 |
| 21MMRC009 | RC | 482895.77 | 7664802.80 | 82.58 | MGA-59 | 0.00 | -60 | 150 |
| 21MMRC010 | RC | 482502.76 | 7664821.49 | 98.79 | MGA-60 | 350.00 | -60 | 150 |
| 21MMRC011 | RC | 482798.12 | 7664827.12 | 82.19 | MGA-61 | 0.00 | -60 | 170 |
| 21MMRC012 | RC | 482713.67 | 7664884.68 | 85.61 | MGA-62 | 0.00 | -60 | 150 |
| 21MMRC013 | RC | 486247.37 | 7660700.45 | 98.29 | MGA-63 | 0.00 | -60 | 150 |
| 21MMRC014 | RC | 485899.50 | 7660489.58 | 99.18 | MGA-64 | 0.00 | -60 | 250 |
| 21MMRC015 | RC | 486247.366 | 7660700.47 | 98.29 | MGA-65 | 0.00 | -60 | 250 |

*Table 7: Significant Intersections for Munni Munni*

| Hole_ID | M From | M To | Width | Sample Type | Pd | Pt | Au | 2PGE+Au | Co | Cu | Ni |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 18MMAD001 | 40.5 | 41 | 0.5 | ASSAY 1/4 | 0.02 | 0.01 | 0.20 | 0.23 | 100 | 2660 | 1320 |
| 18MMAD001 | 41 | 41.5 | 0.5 | ASSAY 1/4 | **0.66** | 0.49 | **0.60** | **1.74** | 130 | 4130 | 1910 |
| 18MMAD001 | 41.5 | 42 | 0.5 | ASSAY 1/4 | **2.00** | **1.85** | 0.40 | **4.25** | 90 | 1430 | 950 |
| 18MMAD001 | 42 | 42.5 | 0.5 | ASSAY 1/4 | **2.13** | **1.34** | 0.08 | **3.55** | 70 | 340 | 530 |
| 18MMAD001 | 42.5 | 43 | 0.5 | ASSAY 1/4 | **1.92** | **0.88** | 0.04 | **2.83** | 70 | 210 | 530 |
| 18MMAD001 | 43 | 43.5 | 0.5 | ASSAY 1/4 | **1.15** | 0.45 | 0.06 | **1.66** | 70 | 320 | 520 |
| 18MMAD001 | 43.5 | 44 | 0.5 | ASSAY 1/4 | **1.34** | 0.36 | 0.24 | **1.93** | 90 | 1070 | 780 |
| 18MMAD001 | 44 | 44.5 | 0.5 | ASSAY 1/4 | **0.73** | 0.14 | 0.04 | 0.91 | 70 | 380 | 540 |
| 18MMAD001 | 44.5 | 45 | 0.5 | ASSAY 1/4 | **0.95** | 0.15 | 0.06 | **1.16** | 60 | 340 | 500 |
| 18MMAD001 | 45 | 45.5 | 0.5 | ASSAY 1/4 | **1.11** | 0.17 | 0.12 | **1.39** | 100 | 1090 | 830 |
| 18MMAD001 | 45.5 | 46 | 0.5 | ASSAY 1/4 | **0.59** | 0.08 | 0.06 | 0.73 | 70 | 520 | 570 |
| 18MMAD001 | 46 | 46.5 | 0.5 | ASSAY 1/4 | 0.38 | 0.06 | 0.02 | 0.45 | 80 | 170 | 550 |
| 18MMAD001 | 46.5 | 47 | 0.5 | ASSAY 1/4 | 0.50 | 0.41 | 0.02 | 0.93 | 80 | 120 | 510 |
| 18MMAD001 | 47 | 47.5 | 0.5 | ASSAY 1/4 | **1.28** | **0.76** | 0.06 | **2.10** | 90 | 420 | 610 |
| 18MMAD001 | 47.5 | 48 | 0.5 | ASSAY 1/4 | 0.01 | 0.01 | 0.01 | 0.03 | 80 | 190 | 530 |
| 18MMAD001 | 98 | 98.5 | 0.5 | ASSAY 1/4 | 0.05 | 0.02 | 0.01 | 0.08 | 170 | 100 | 2260 |
| 18MMAD001 | 98.5 | 99 | 0.5 | ASSAY 1/4 | **0.60** | 0.28 | 0.16 | **1.04** | 140 | 2080 | 2660 |
| 18MMAD001 | 99 | 99.5 | 0.5 | ASSAY 1/4 | 0.01 | 0.00 | 0.00 | 0.01 | 90 | 100 | 1040 |
| | | | | | | | | | | | |
| 18MMAD002 | 22 | 22.5 | 0.5 | ASSAY 1/4 | 0.01 | 0.00 | 0.03 | 0.04 | 110 | 3160 | 1540 |
| 18MMAD002 | 22.5 | 23 | 0.5 | ASSAY 1/4 | **0.59** | 0.41 | **0.72** | **1.71** | 120 | 3430 | 1710 |
| 18MMAD002 | 23 | 23.5 | 0.5 | ASSAY 1/4 | **2.09** | 0.85 | **0.27** | **3.21** | 80 | 1140 | 790 |
| 18MMAD002 | 23.5 | 24 | 0.5 | ASSAY 1/4 | **0.30** | 0.04 | **0.07** | **0.41** | 90 | 890 | 730 |
| | | | | | | | | | | 0.22 | 0.12 |
| 18MMAD003 | 34 | 34.5 | 0.5 | ASSAY 1/4 | **0.01** | 0.01 | **0.24** | **0.26** | 160 | 4400 | 1960 |
| 18MMAD003 | 34.5 | 35 | 0.5 | ASSAY 1/4 | **0.07** | 0.04 | **0.47** | **0.58** | 140 | 3420 | 1620 |
| 18MMAD003 | 35 | 35.5 | 0.5 | ASSAY 1/4 | **2.06** | 2.01 | **0.72** | **4.79** | 180 | 3790 | 2010 |
| 18MMAD003 | 35.5 | 36 | 0.5 | ASSAY 1/4 | **2.71** | 2.53 | **0.22** | **5.46** | 100 | 1250 | 940 |
| 18MMAD003 | 36 | 36.5 | 0.5 | ASSAY 1/4 | **2.14** | 1.40 | **0.29** | **3.83** | 80 | 400 | 650 |
| 18MMAD003 | 36.5 | 37 | 0.5 | ASSAY 1/4 | **1.40** | 0.46 | **0.08** | **1.94** | 80 | 240 | 610 |
| 18MMAD003 | 37 | 37.5 | 0.5 | ASSAY 1/4 | **1.62** | 0.53 | **0.15** | **2.30** | 80 | 430 | 730 |
| 18MMAD003 | 37.5 | 38 | 0.5 | ASSAY 1/4 | **0.92** | 0.29 | **0.04** | **1.25** | 160 | 2290 | 1370 |
| 18MMAD003 | 38 | 38.5 | 0.5 | ASSAY 1/4 | **0.93** | 0.39 | **0.17** | **1.48** | 140 | 2070 | 1190 |
| 18MMAD003 | 38.5 | 39 | 0.5 | ASSAY 1/4 | **0.04** | 0.02 | **0.00** | **0.06** | 80 | 260 | 560 |
| | | | | | | | | | | | |
| 18MMAD004 | 56.7 | 57 | 0.3 | ASSAY 1/4 | **0.11** | 0.07 | **0.02** | **0.20** | 110 | 1160 | 620 |
| 18MMAD004 | 57 | 57.5 | 0.5 | ASSAY 1/4 | **0.75** | 0.22 | **0.07** | **1.05** | 120 | 2090 | 1160 |
| 18MMAD004 | 57.5 | 58 | 0.5 | ASSAY 1/4 | **0.19** | 0.14 | **0.03** | **0.36** | 90 | 580 | 710 |
| | | | | | | | | | | | |
| 18MMAD005 | 34 | 34.5 | 0.5 | ASSAY 1/4 | **0.01** | 0.01 | **0.23** | **0.25** | 100 | 2880 | 1350 |
| 18MMAD005 | 34.5 | 35 | 0.5 | ASSAY 1/4 | **0.12** | 0.09 | **0.40** | **0.60** | 110 | 3100 | 1360 |
| 18MMAD005 | 35 | 35.5 | 0.5 | ASSAY 1/4 | **1.80** | 1.83 | **0.52** | **4.15** | 100 | 2600 | 1250 |
| 18MMAD005 | 35.5 | 36 | 0.5 | ASSAY 1/4 | **1.82** | 1.79 | **0.25** | **3.85** | 80 | 930 | 780 |
| 18MMAD005 | 36 | 36.5 | 0.5 | ASSAY 1/4 | **2.05** | 1.42 | **0.10** | **3.57** | 80 | 460 | 620 |
| 18MMAD005 | 36.5 | 37 | 0.5 | ASSAY 1/4 | **2.24** | 1.34 | **0.06** | **3.64** | 80 | 380 | 620 |
| 18MMAD005 | 37 | 37.5 | 0.5 | ASSAY 1/4 | **1.71** | 0.92 | **0.04** | **2.67** | 70 | 250 | 530 |
| 18MMAD005 | 37.5 | 38 | 0.5 | ASSAY 1/4 | **1.23** | 0.53 | **0.05** | **1.80** | 80 | 340 | 590 |
| 18MMAD005 | 38 | 38.5 | 0.5 | ASSAY 1/4 | **1.57** | 0.37 | **0.16** | **2.10** | 110 | 970 | 920 |
| 18MMAD005 | 38.5 | 39 | 0.5 | ASSAY 1/4 | **1.72** | 0.24 | **0.06** | **2.02** | 80 | 260 | 610 |
| 18MMAD005 | 39 | 39.5 | 0.5 | ASSAY 1/4 | **0.75** | 0.10 | **0.04** | **0.88** | 80 | 180 | 580 |
| 18MMAD005 | 59 | 59.5 | 0.5 | ASSAY 1/4 | **0.01** | 0.00 | **0.00** | **0.01** | 60 | 180 | 330 |
| 18MMAD005 | 59.5 | 60 | 0.5 | ASSAY 1/4 | **0.41** | 0.17 | **0.06** | **0.64** | 120 | 3990 | 1840 |
| 18MMAD005 | 60 | 60.5 | 0.5 | ASSAY 1/4 | **0.61** | 0.35 | **0.10** | **1.05** | 110 | 2770 | 1480 |
| 18MMAD005 | 60.5 | 61 | 0.5 | ASSAY 1/4 | **0.87** | 0.60 | **0.19** | **1.65** | 110 | 3020 | 1680 |
| 18MMAD005 | 61 | 61.5 | 0.5 | ASSAY 1/4 | **0.24** | 0.14 | **0.04** | **0.42** | 90 | 1340 | 1090 |
| | | | | | | | | | | 0.33 | 0.17 |

| Hole_ID | M From | M To | Width | Sample Type | Pd | Pt | Au | 2PGE+Au | Co | Cu | Ni |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 18MMAD005 | 65 | 65.5 | 0.5 | ASSAY 1/4 | **0.01** | 0.00 | **0.00** | **0.01** | 40 | 60 | 200 |
| 18MMAD005 | 65.5 | 66 | 0.5 | ASSAY 1/4 | **0.30** | 0.19 | **0.05** | **0.53** | 50 | 680 | 420 |
| 18MMAD005 | 66 | 66.5 | 0.5 | ASSAY 1/4 | **1.24** | 0.75 | **0.20** | **2.19** | 130 | 3290 | 1880 |
| 18MMAD005 | 66.5 | 67 | 0.5 | ASSAY 1/4 | **1.41** | 0.60 | **0.18** | **2.19** | 140 | 3310 | 2200 |
| 18MMAD005 | 67 | 67.5 | 0.5 | ASSAY 1/4 | **0.21** | 0.11 | **0.04** | **0.36** | 80 | 630 | 1040 |
| 18MMAD005 | 67.5 | 68 | 0.5 | ASSAY 1/4 | **0.35** | 0.18 | **0.05** | **0.58** | 90 | 760 | 1120 |
| 18MMAD005 | 68 | 68.5 | 0.5 | ASSAY 1/4 | **0.18** | 0.10 | **0.03** | **0.31** | 90 | 570 | 1000 |
| 18MMAD005 | 68.5 | 69 | 0.5 | ASSAY 1/4 | **1.09** | 0.63 | **0.10** | **1.82** | 130 | 2320 | 1630 |
| 18MMAD005 | 69 | 69.5 | 0.5 | ASSAY 1/4 | **0.19** | 0.12 | **0.05** | **0.36** | 90 | 380 | 980 |
| | | | | | | | | | | | |
| 18MMAD006 | 27.5 | 28 | 0.5 | ASSAY 1/4 | **0.01** | 0.00 | **0.13** | **0.14** | 120 | 3210 | 1400 |
| 18MMAD006 | 28 | 28.5 | 0.5 | ASSAY 1/4 | **0.76** | 0.69 | **0.33** | **1.78** | 100 | 2330 | 1160 |
| 18MMAD006 | 28.5 | 29 | 0.5 | ASSAY 1/4 | **1.66** | 1.21 | **0.14** | **3.00** | 80 | 420 | 560 |
| 18MMAD006 | 29 | 29.5 | 0.5 | ASSAY 1/4 | **1.49** | 0.77 | **0.06** | **2.32** | 80 | 360 | 540 |
| 18MMAD006 | 29.5 | 30 | 0.5 | ASSAY 1/4 | **1.29** | 0.67 | **0.06** | **2.01** | 80 | 350 | 540 |
| 18MMAD006 | 30 | 30.5 | 0.5 | ASSAY 1/4 | **0.76** | 0.14 | **0.07** | **0.97** | 80 | 440 | 600 |
| 18MMAD006 | 30.5 | 31 | 0.5 | ASSAY 1/4 | **0.48** | 0.09 | **0.02** | **0.59** | 80 | 390 | 580 |
| 18MMAD006 | 31 | 31.5 | 0.5 | ASSAY 1/4 | **1.10** | 0.19 | **0.08** | **1.37** | 70 | 380 | 550 |
| 18MMAD006 | 31.5 | 32 | 0.5 | ASSAY 1/4 | **0.55** | 0.26 | **0.03** | **0.85** | 70 | 260 | 530 |
| 18MMAD006 | 32 | 32.5 | 0.5 | ASSAY 1/4 | **1.16** | 0.25 | **0.11** | **1.51** | 100 | 1070 | 740 |
| 18MMAD006 | 32.5 | 33 | 0.5 | ASSAY 1/4 | **0.32** | 0.17 | **0.04** | **0.53** | 80 | 230 | 540 |
| 18MMAD006 | 33 | 33.5 | 0.5 | ASSAY 1/4 | **0.04** | 0.01 | **0.00** | **0.05** | 70 | 150 | 500 |
| | | | | | | | | | | | |
| 18MMAD007 | 65 | 65.5 | 0.5 | ASSAY 1/4 | **0.06** | 0.03 | **0.36** | **0.45** | 110 | 3440 | 1490 |
| 18MMAD007 | 65.5 | 66 | 0.5 | ASSAY 1/4 | **1.56** | 1.60 | **0.49** | **3.64** | 100 | 2410 | 1160 |
| 18MMAD007 | 66 | 66.5 | 0.5 | ASSAY 1/4 | **1.98** | 1.44 | **0.09** | **3.50** | 90 | 430 | 590 |
| 18MMAD007 | 66.5 | 67 | 0.5 | ASSAY 1/4 | **1.58** | 0.55 | **0.13** | **2.26** | 90 | 770 | 700 |
| 18MMAD007 | 67 | 67.5 | 0.5 | ASSAY 1/4 | **0.91** | 0.16 | **0.14** | **1.21** | 90 | 1320 | 900 |
| 18MMAD007 | 67.5 | 68 | 0.5 | ASSAY 1/4 | **0.55** | 0.12 | **0.04** | **0.71** | 90 | 410 | 590 |
| 18MMAD007 | 68 | 68.5 | 0.5 | ASSAY 1/4 | **0.68** | 0.11 | **0.07** | **0.85** | 80 | 850 | 700 |
| 18MMAD007 | 68.5 | 69 | 0.5 | ASSAY 1/4 | **0.64** | 0.08 | **0.04** | **0.76** | 90 | 440 | 620 |
| 18MMAD007 | 69 | 69.5 | 0.5 | ASSAY 1/4 | **0.71** | 0.23 | **0.05** | **0.98** | 90 | 380 | 620 |
| 18MMAD007 | 69.5 | 70 | 0.5 | ASSAY 1/4 | **0.34** | 0.26 | **0.01** | **0.61** | 80 | 130 | 530 |
| 18MMAD007 | 70 | 70.5 | 0.5 | ASSAY 1/4 | **0.42** | 0.25 | **0.02** | **0.69** | 90 | 240 | 560 |
| 18MMAD007 | 70.5 | 71 | 0.5 | ASSAY 1/4 | **0.02** | 0.01 | **0.00** | **0.03** | 90 | 160 | 550 |
| | | | | | | | | | | | |
| 18MMAD008 | 81.5 | 82 | 0.5 | ASSAY 1/4 | **0.01** | 0.00 | **0.00** | **0.01** | 60 | 260 | 470 |
| 18MMAD008 | 82 | 82.5 | 0.5 | ASSAY 1/4 | **0.67** | 0.25 | **0.07** | **0.99** | 80 | 1520 | 950 |
| 18MMAD008 | 82.5 | 83 | 0.5 | ASSAY 1/4 | **1.46** | 1.03 | **0.33** | **2.81** | 100 | 2080 | 1330 |
| 18MMAD008 | 83 | 83.5 | 0.5 | ASSAY 1/4 | **3.14** | 2.15 | **0.48** | **5.77** | 120 | 2400 | 1690 |
| 18MMAD008 | 83.5 | 84 | 0.5 | ASSAY 1/4 | **2.66** | 2.00 | **0.45** | **5.11** | 150 | 2570 | 2040 |
| 18MMAD008 | 84 | 84.5 | 0.5 | ASSAY 1/4 | **0.74** | 0.72 | **0.21** | **1.67** | 90 | 1890 | 1200 |
| 18MMAD008 | 84.5 | 85 | 0.5 | ASSAY 1/4 | **0.73** | 0.52 | **0.13** | **1.39** | 80 | 990 | 1140 |
| 18MMAD008 | 85 | 85.5 | 0.5 | ASSAY 1/4 | **0.08** | 0.06 | **0.01** | **0.14** | 60 | 190 | 490 |
| 18MMAD008 | 85.5 | 86 | 0.5 | ASSAY 1/4 | **0.66** | 0.47 | **0.11** | **1.24** | 90 | 1940 | 1170 |
| 18MMAD008 | 86 | 86.5 | 0.5 | ASSAY 1/4 | **0.64** | 0.37 | **0.09** | **1.10** | 80 | 1850 | 1040 |
| 18MMAD008 | 86.5 | 87 | 0.5 | ASSAY 1/4 | **0.03** | 0.02 | **0.01** | **0.05** | 60 | 130 | 520 |
| 18MMAD008 | 87 | 87.5 | 0.5 | ASSAY 1/4 | **0.18** | 0.09 | **0.03** | **0.30** | 70 | 340 | 540 |
| 18MMAD008 | 87.5 | 88 | 0.5 | ASSAY 1/4 | **0.69** | 0.57 | **0.18** | **1.44** | 100 | 1580 | 1130 |
| 18MMAD008 | 88 | 89 | 1 | ASSAY 1/4 | **0.14** | 0.08 | **0.02** | **0.24** | 80 | 440 | 670 |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| 20MMRC003 | 133 | 134 | 1 | RC | **0.25** | 0.05 | **0.04** | **0.33** | 62 | 638 | 336 |
| 20MMRC003 | 134 | 135 | 1 | RC | **0.48** | 0.19 | **0.12** | **0.78** | 78 | 1590 | 613 |
| 20MMRC003 | 135 | 136 | 1 | RC | **0.71** | 0.25 | **0.12** | **1.08** | 90 | 2310 | 870 |
| 20MMRC003 | 136 | 137 | 1 | RC | **0.08** | 0.02 | **0.05** | **0.15** | 79 | 356 | 401 |
| | | | | | | | | | | | |
| | | | | | | | | | | | |

| Hole_ID | M From | M To | Width | Sample Type | Pd | Pt | Au | 2PGE+Au | Co | Cu | Ni |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 20MMRC005 | 18 | 19 | 1 | RC | **0.00** | 0.00 | **0.04** | **0.05** | 95 | 1640 | 924 |
| 20MMRC005 | 19 | 20 | 1 | RC | **0.34** | 0.33 | **0.23** | **0.90** | 125 | 2810 | 1350 |
| 20MMRC005 | 20 | 21 | 1 | RC | **1.74** | 1.37 | **0.20** | **3.30** | 96 | 1450 | 981 |
| 20MMRC005 | 21 | 22 | 1 | RC | **1.88** | 1.03 | **0.13** | **3.03** | 85 | 861 | 752 |
| 20MMRC005 | 22 | 23 | 1 | RC | **0.97** | 0.20 | **0.09** | **1.26** | 94 | 887 | 794 |
| 20MMRC005 | 23 | 24 | 1 | RC | **0.50** | 0.09 | **0.04** | **0.63** | 82 | 497 | 616 |
| 20MMRC005 | 24 | 25 | 1 | RC | **0.24** | 0.17 | **0.01** | **0.42** | 82 | 177 | 521 |
| | | | | | | | | | | | |
| 20MMRC006 | 69 | 70 | 1 | RC | **0.03** | 0.01 | **0.10** | **0.15** | 100 | 1275 | 532 |
| 20MMRC006 | 70 | 71 | 1 | RC | **0.62** | 0.60 | **0.30** | **1.51** | 76 | 1520 | 846 |
| 20MMRC006 | 71 | 72 | 1 | RC | **0.85** | 0.61 | **0.06** | **1.52** | 85 | 802 | 423 |
| 20MMRC006 | 72 | 73 | 1 | RC | **0.90** | 0.29 | **0.16** | **1.35** | 96 | 1140 | 669 |
| 20MMRC006 | 73 | 74 | 1 | RC | **0.62** | 0.33 | **0.12** | **1.06** | 105 | 1500 | 695 |
| 20MMRC006 | 74 | 75 | 1 | RC | **0.16** | 0.08 | **0.03** | **0.26** | 81 | 355 | 605 |
| | | | | | | | | | | | |
| 20MMRC006 | 101 | 102 | 1 | RC | **0.00** | 0.00 | **0.00** | **0.01** | 59 | 296 | 143 |
| 20MMRC006 | 102 | 103 | 1 | RC | **0.62** | 0.39 | **0.08** | **1.10** | 131 | 2280 | 937 |
| 20MMRC006 | 103 | 104 | 1 | RC | **0.22** | 0.11 | **0.04** | **0.37** | 87 | 708 | 812 |
| | | | | | | | | | | | |
| 20MMRC007 | 121 | 122 | 1 | RC | **0.01** | 0.01 | **0.14** | **0.16** | 97 | 2280 | 1280 |
| 20MMRC007 | 122 | 123 | 1 | RC | **0.49** | 0.44 | **0.33** | **1.26** | 95 | 2810 | 1280 |
| 20MMRC007 | 123 | 124 | 1 | RC | **1.70** | 1.50 | **0.17** | **3.37** | 89 | 1090 | 736 |
| 20MMRC007 | 124 | 125 | 1 | RC | **1.33** | 0.76 | **0.05** | **2.13** | 81 | 511 | 527 |
| 20MMRC007 | 125 | 126 | 1 | RC | **1.08** | 0.40 | **0.12** | **1.60** | 82 | 874 | 722 |
| 20MMRC007 | 126 | 127 | 1 | RC | **0.57** | 0.17 | **0.05** | **0.80** | 75 | 416 | 572 |
| 20MMRC007 | 127 | 128 | 1 | RC | **0.54** | 0.16 | **0.02** | **0.71** | 76 | 380 | 594 |
| 20MMRC007 | 128 | 129 | 1 | RC | **0.70** | 0.22 | **0.03** | **0.94** | 76 | 260 | 573 |
| 20MMRC007 | 129 | 130 | 1 | RC | **0.09** | 0.04 | **0.01** | **0.14** | 74 | 133 | 528 |
| | | | | | | | | | | | |
| 20MMRC011 | 143 | 144 | 1 | RC | **0.06** | 0.04 | **0.19** | **0.29** | 88 | 1960 | 873 |
| 20MMRC011 | 144 | 145 | 1 | RC | **0.87** | 0.82 | **0.42** | **2.11** | 89 | 2360 | 1050 |
| 20MMRC011 | 145 | 146 | 1 | RC | **0.78** | 0.78 | **0.14** | **1.69** | 77 | 781 | 587 |
| 20MMRC011 | 146 | 147 | 1 | RC | **0.83** | 0.44 | **0.09** | **1.35** | 78 | 829 | 601 |
| 20MMRC011 | 147 | 148 | 1 | RC | **0.95** | 0.17 | **0.07** | **1.20** | 83 | 1460 | 853 |
| 20MMRC011 | 148 | 149 | 1 | RC | **0.64** | 0.08 | **0.04** | **0.76** | 75 | 1200 | 762 |
| 20MMRC011 | 149 | 150 | 1 | RC | **0.48** | 0.15 | **0.05** | **0.68** | 76 | 632 | 576 |
| 20MMRC011 | 150 | 151 | 1 | RC | **0.21** | 0.08 | **0.01** | **0.30** | 74 | 239 | 473 |
| | | | | | | | | | | | |
| 20MMRC012 | 193 | 194 | 1 | RC | **0.01** | 0.01 | **0.14** | **0.15** | 84 | 2710 | 1200 |
| 20MMRC012 | 194 | 195 | 1 | RC | **0.37** | 0.30 | **0.15** | **0.82** | 81 | 1060 | 756 |
| 20MMRC012 | 195 | 196 | 1 | RC | **1.00** | 0.60 | **0.10** | **1.70** | 79 | 909 | 651 |
| 20MMRC012 | 196 | 197 | 1 | RC | **0.80** | 0.37 | **0.06** | **1.23** | 73 | 659 | 544 |
| 20MMRC012 | 197 | 198 | 1 | RC | **0.62** | 0.21 | **0.04** | **0.86** | 73 | 656 | 556 |
| | | | | | | | | | | | |
| 21MMRC001 | 78 | 79 | 1 | RC | **0.01** | 0.01 | **0.17** | **0.19** | 117 | 3380 | 1485 |
| 21MMRC001 | 79 | 80 | 1 | RC | **0.95** | 1.01 | **0.20** | **2.16** | 87 | 1400 | 863 |
| 21MMRC001 | 80 | 81 | 1 | RC | **0.59** | 1.18 | **0.05** | **1.82** | 79 | 350 | 551 |
| 21MMRC001 | 81 | 82 | 1 | RC | **0.17** | 0.39 | **0.02** | **0.58** | 74 | 210 | 519 |
| 21MMRC001 | 82 | 83 | 1 | RC | **0.01** | 0.02 | **0.01** | **0.04** | 78 | 214 | 550 |
| | | | | | | | | | | | |
| 21MMRC002 | 115 | 116 | 1 | RC | **0.01** | 0.01 | **0.19** | **0.21** | 102 | 2470 | 1285 |
| 21MMRC002 | 116 | 117 | 1 | RC | **0.11** | 0.16 | **0.33** | **0.61** | 106 | 2970 | 1400 |
| 21MMRC002 | 117 | 118 | 1 | RC | **1.37** | 1.36 | **0.35** | **3.07** | 102 | 1980 | 1120 |
| 21MMRC002 | 118 | 119 | 1 | RC | **1.20** | 1.68 | **0.11** | **2.99** | 89 | 555 | 672 |
| 21MMRC002 | 119 | 120 | 1 | RC | **1.00** | 1.71 | **0.07** | **2.78** | 89 | 476 | 644 |
| 21MMRC002 | 120 | 121 | 1 | RC | **0.59** | 1.36 | **0.06** | **2.01** | 86 | 462 | 634 |
| 21MMRC002 | 121 | 122 | 1 | RC | **0.16** | 0.77 | **0.08** | **1.01** | 91 | 944 | 801 |
| 21MMRC002 | 122 | 123 | 1 | RC | **0.09** | 0.53 | **0.02** | **0.64** | 91 | 403 | 673 |

| Hole_ID | M From | M To | Width | Sample Type | Pd | Pt | Au | 2PGE+Au | Co | Cu | Ni |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 21MMRC002 | 123 | 124 | 1 | RC | **0.15** | 0.88 | **0.04** | **1.07** | 88 | 359 | 644 |
| 21MMRC002 | 124 | 125 | 1 | RC | **0.07** | 0.35 | **0.02** | **0.43** | 80 | 185 | 574 |
| 21MMRC002 | 125 | 126 | 1 | RC | **0.21** | 0.73 | **0.07** | **1.01** | 90 | 625 | 735 |
| 21MMRC002 | 126 | 127 | 1 | RC | **0.03** | 0.15 | **0.01** | **0.19** | 77 | 155 | 578 |
| | | | | | | | | | | | |
| 21MMRC003 | 107 | 108 | 1 | RC | **0.00** | 0.01 | **0.18** | **0.19** | 98 | 2710 | 1310 |
| 21MMRC003 | 108 | 109 | 1 | RC | **0.54** | 0.61 | **0.61** | **1.76** | 112 | 3550 | 1580 |
| 21MMRC003 | 109 | 110 | 1 | RC | **1.58** | 1.52 | **0.36** | **3.46** | 98 | 1630 | 1020 |
| 21MMRC003 | 110 | 111 | 1 | RC | **1.27** | 1.64 | **0.13** | **3.03** | 85 | 632 | 661 |
| 21MMRC003 | 111 | 112 | 1 | RC | **0.78** | 1.43 | **0.05** | **2.26** | 81 | 376 | 579 |
| 21MMRC003 | 112 | 113 | 1 | RC | **0.26** | 0.80 | **0.08** | **1.14** | 85 | 624 | 687 |
| 21MMRC003 | 113 | 114 | 1 | RC | **0.15** | 0.70 | **0.05** | **0.90** | 94 | 1080 | 865 |
| 21MMRC003 | 114 | 115 | 1 | RC | **0.11** | 0.56 | **0.02** | **0.68** | 72 | 302 | 553 |
| 21MMRC003 | 115 | 116 | 1 | RC | **0.07** | 0.37 | **0.01** | **0.45** | 75 | 178 | 562 |
| 21MMRC003 | 116 | 117 | 1 | RC | **0.06** | 0.38 | **0.01** | **0.46** | 78 | 134 | 566 |
| 21MMRC003 | 117 | 118 | 1 | RC | **0.15** | 0.77 | **0.01** | **0.93** | 83 | 160 | 614 |
| 21MMRC003 | 118 | 119 | 1 | RC | **0.54** | 1.08 | **0.02** | **1.63** | 87 | 131 | 640 |
| 21MMRC003 | 119 | 120 | 1 | RC | **0.03** | 0.10 | **0.00** | **0.13** | 83 | 88 | 599 |
| | | | | | | | | | | | |
| 21MMRC004 | 80 | 81 | 1 | RC | **0.01** | 0.01 | **0.16** | **0.18** | 103 | 3080 | 1305 |
| 21MMRC004 | 81 | 82 | 1 | RC | **0.68** | 0.76 | **0.39** | **1.82** | 94 | 2430 | 1175 |
| 21MMRC004 | 82 | 83 | 1 | RC | **1.38** | 1.44 | **0.26** | **3.08** | 91 | 1300 | 871 |
| 21MMRC004 | 83 | 84 | 1 | RC | **1.28** | 1.49 | **0.16** | **2.92** | 88 | 836 | 726 |
| 21MMRC004 | 84 | 85 | 1 | RC | **0.18** | 0.67 | **0.04** | **0.88** | 84 | 369 | 571 |
| 21MMRC004 | 85 | 86 | 1 | RC | **0.02** | 0.04 | **0.02** | **0.08** | 84 | 187 | 520 |
| | | | | | | | | | | | |
| 21MMRC005 | 122 | 123 | 1 | RC | **0.00** | 0.01 | **0.18** | **0.19** | 102 | 3850 | 1710 |
| 21MMRC005 | 123 | 124 | 1 | RC | **0.17** | 0.19 | **0.38** | **0.74** | 104 | 3130 | 1460 |
| 21MMRC005 | 124 | 125 | 1 | RC | **1.48** | 1.56 | **0.10** | **3.14** | 79 | 836 | 705 |
| 21MMRC005 | 125 | 126 | 1 | RC | **1.07** | 1.73 | **0.06** | **2.86** | 74 | 326 | 543 |
| 21MMRC005 | 126 | 127 | 1 | RC | **0.14** | 0.98 | **0.14** | **1.26** | 95 | 1225 | 876 |
| 21MMRC005 | 127 | 128 | 1 | RC | **0.19** | 0.90 | **0.05** | **1.14** | 86 | 628 | 619 |
| 21MMRC005 | 128 | 129 | 1 | RC | **0.07** | 0.46 | **0.04** | **0.57** | 73 | 245 | 368 |
| 21MMRC005 | 129 | 130 | 1 | RC | **1.45** | 3.67 | **0.12** | **5.23** | 151 | 2610 | 1250 |
| 21MMRC005 | 130 | 131 | 1 | RC | **0.33** | 0.94 | **0.02** | **1.29** | 88 | 638 | 730 |
| 21MMRC005 | 131 | 132 | 1 | RC | **0.17** | 0.56 | **0.02** | **0.75** | 81 | 292 | 635 |
| 21MMRC005 | 132 | 133 | 1 | RC | **0.01** | 0.02 | **0.00** | **0.03** | 79 | 103 | 613 |
| | | | | | | | | | | | |
| 21MMRC006 | 94 | 95 | 1 | RC | **0.00** | 0.00 | **0.03** | **0.03** | 89 | 1560 | 981 |
| 21MMRC006 | 95 | 96 | 1 | RC | **0.13** | 0.21 | **0.50** | **0.84** | 120 | 4040 | 1725 |
| 21MMRC006 | 96 | 97 | 1 | RC | **1.59** | 1.56 | **0.50** | **3.65** | 100 | 2420 | 1250 |
| 21MMRC006 | 97 | 98 | 1 | RC | **1.76** | 1.69 | **0.24** | **3.69** | 85 | 1000 | 824 |
| 21MMRC006 | 98 | 99 | 1 | RC | **1.20** | 1.79 | **0.10** | **3.08** | 76 | 410 | 599 |
| 21MMRC006 | 99 | 100 | 1 | RC | **0.72** | 1.50 | **0.05** | **2.26** | 78 | 319 | 572 |
| 21MMRC006 | 100 | 101 | 1 | RC | **0.31** | 1.27 | **0.22** | **1.80** | 94 | 1010 | 828 |
| 21MMRC006 | 101 | 102 | 1 | RC | **0.12** | 0.53 | **0.07** | **0.72** | 73 | 331 | 587 |
| 21MMRC006 | 102 | 103 | 1 | RC | **0.20** | 0.97 | **0.11** | **1.28** | 78 | 391 | 613 |
| 21MMRC006 | 103 | 104 | 1 | RC | **0.10** | 0.58 | **0.04** | **0.71** | 77 | 295 | 583 |
| 21MMRC006 | 104 | 105 | 1 | RC | **0.06** | 0.33 | **0.01** | **0.40** | 80 | 209 | 587 |
| 21MMRC006 | 105 | 106 | 1 | RC | **0.10** | 0.57 | **0.02** | **0.69** | 81 | 268 | 588 |
| 21MMRC006 | 106 | 107 | 1 | RC | **0.29** | 1.02 | **0.03** | **1.34** | 81 | 302 | 591 |
| 21MMRC006 | 107 | 108 | 1 | RC | **0.04** | 0.11 | **0.00** | **0.16** | 79 | 139 | 575 |
| | | | | | | | | | | | |
| 21MMRC006 | 136 | 137 | 1 | RC | **0.00** | 0.01 | **0.00** | **0.02** | 90 | 310 | 290 |
| 21MMRC006 | 137 | 138 | 1 | RC | **0.19** | 0.45 | **0.07** | **0.71** | 101 | 2060 | 634 |
| 21MMRC006 | 138 | 139 | 1 | RC | **0.03** | 0.07 | **0.01** | **0.11** | 80 | 669 | 596 |
| 21MMRC006 | 139 | 140 | 1 | RC | **0.55** | 1.00 | **0.10** | **1.65** | 88 | 3870 | 939 |
| 21MMRC006 | 140 | 141 | 1 | RC | **0.06** | 0.08 | **0.01** | **0.14** | 105 | 975 | 1535 |

| Hole_ID | M From | M To | Width | Sample Type | Pd | Pt | Au | 2PGE+Au | Co | Cu | Ni |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 21MMRC007 | 59 | 60 | 1 | RC | **0.03** | 0.04 | **0.28** | **0.35** | 121 | 3230 | 1440 |
| 21MMRC007 | 60 | 61 | 1 | RC | **1.81** | 1.76 | **0.32** | **3.89** | 99 | 1900 | 982 |
| 21MMRC007 | 61 | 62 | 1 | RC | **1.25** | 2.02 | **0.69** | **3.96** | 89 | 1010 | 742 |
| 21MMRC007 | 62 | 63 | 1 | RC | **0.19** | 0.95 | **0.14** | **1.28** | 106 | 1470 | 917 |
| 21MMRC007 | 63 | 64 | 1 | RC | **0.14** | 0.52 | **0.01** | **0.67** | 82 | 252 | 584 |
| 21MMRC007 | 64 | 65 | 1 | RC | **0.03** | 0.04 | **0.01** | **0.07** | 89 | 257 | 647 |
| | | | | | | | | | | | |
| 21MMRC008 | 74 | 75 | 1 | RC | **0.00** | 0.00 | **0.00** | **0.01** | 69 | 148 | 509 |
| 21MMRC008 | 75 | 76 | 1 | RC | **0.22** | 0.38 | **0.11** | **0.71** | 86 | 1575 | 838 |
| 21MMRC008 | 76 | 77 | 1 | RC | **0.61** | 1.03 | **0.22** | **1.85** | 99 | 3120 | 1385 |
| 21MMRC008 | 77 | 78 | 1 | RC | **0.75** | 1.48 | **0.33** | **2.55** | 92 | 2960 | 1875 |
| 21MMRC008 | 78 | 79 | 1 | RC | **1.25** | 2.72 | **0.64** | **4.60** | 121 | 4950 | 3110 |
| 21MMRC008 | 79 | 80 | 1 | RC | **0.60** | 1.23 | **0.30** | **2.13** | 90 | 2600 | 1755 |
| 21MMRC008 | 80 | 81 | 1 | RC | **0.09** | 0.18 | **0.03** | **0.30** | 62 | 510 | 691 |
| 21MMRC008 | 81 | 82 | 1 | RC | **0.03** | 0.06 | **0.01** | **0.10** | 70 | 212 | 649 |
| 21MMRC008 | 82 | 83 | 1 | RC | **0.06** | 0.12 | **0.03** | **0.20** | 72 | 392 | 724 |
| 21MMRC008 | 83 | 84 | 1 | RC | **0.16** | 0.31 | **0.08** | **0.56** | 74 | 1105 | 986 |
| 21MMRC008 | 84 | 85 | 1 | RC | **0.18** | 0.36 | **0.08** | **0.62** | 93 | 916 | 1260 |
| 21MMRC008 | 85 | 86 | 1 | RC | **0.02** | 0.04 | **0.01** | **0.07** | 76 | 146 | 788 |
| 21MMRC008 | 86 | 87 | 1 | RC | **0.64** | 1.27 | **0.30** | **2.22** | 114 | 4180 | 2340 |
| 21MMRC008 | 87 | 88 | 1 | RC | **0.35** | 0.80 | **0.17** | **1.32** | 93 | 1930 | 1675 |
| 21MMRC008 | 88 | 89 | 1 | RC | **0.24** | 0.56 | **0.13** | **0.94** | 90 | 1295 | 1445 |
| 21MMRC008 | 89 | 90 | 1 | RC | **0.19** | 0.45 | **0.09** | **0.73** | 90 | 992 | 1380 |
| 21MMRC008 | 90 | 91 | 1 | RC | **0.01** | 0.03 | **0.01** | **0.05** | 71 | 135 | 836 |
| | | | | | | | | | | | |
| 21MMRC009 | NSI | | | | | | | | | | |
| | | | | | | | | | | | |
| 21MMRC010 | 114 | 115 | 1 | RC | **0.02** | 0.10 | **0.27** | **0.39** | 119 | 3490 | 1590 |
| 21MMRC010 | 115 | 116 | 1 | RC | **1.46** | 1.35 | **0.61** | **3.42** | 141 | 3410 | 1735 |
| 21MMRC010 | 116 | 117 | 1 | RC | **1.20** | 2.21 | **0.12** | **3.53** | 73 | 418 | 646 |
| 21MMRC010 | 117 | 118 | 1 | RC | **0.19** | 0.80 | **0.07** | **1.06** | 71 | 361 | 599 |
| 21MMRC010 | 118 | 119 | 1 | RC | **0.73** | 2.66 | **0.10** | **3.49** | 97 | 817 | 925 |
| 21MMRC010 | 119 | 120 | 1 | RC | **0.05** | 0.17 | **0.03** | **0.24** | 77 | 277 | 595 |
| | | | 0 | RC | | | | | | | |
| 21MMRC010 | 131 | 132 | 1 | RC | **0.01** | 0.01 | **0.01** | **0.03** | 76 | 66 | 588 |
| 21MMRC010 | 132 | 133 | 1 | RC | **1.05** | 1.59 | **0.25** | **2.89** | 118 | 2190 | 1300 |
| 21MMRC010 | 133 | 134 | 1 | RC | **0.05** | 0.08 | **0.01** | **0.14** | 77 | 199 | 604 |
| | | | | | | | | | | | |
| 21MMRC010 | 141 | 142 | 1 | RC | **0.05** | 0.09 | **0.01** | **0.15** | 74 | 301 | 653 |
| 21MMRC010 | 142 | 143 | 1 | RC | **0.21** | 0.40 | **0.05** | **0.66** | 93 | 1420 | 1055 |
| 21MMRC010 | 143 | 144 | 1 | RC | **0.01** | 0.02 | **0.01** | **0.03** | 80 | 101 | 795 |
| | | | | | | | | | | | |
| 21MMRC011 | 141 | 142 | 1 | RC | **0.00** | 0.00 | **0.07** | **0.07** | 78 | 1710 | 757 |
| 21MMRC011 | 142 | 143 | 1 | RC | **0.11** | 0.21 | **0.36** | **0.68** | 98 | 3000 | 1260 |
| 21MMRC011 | 143 | 144 | 1 | RC | **1.39** | 1.94 | **0.12** | **3.44** | 82 | 609 | 602 |
| 21MMRC011 | 144 | 145 | 1 | RC | **0.57** | 1.40 | **0.09** | **2.06** | 80 | 533 | 588 |
| 21MMRC011 | 145 | 146 | 1 | RC | **0.06** | 0.27 | **0.04** | **0.37** | 85 | 787 | 726 |
| | | | | | | | | | | | |
| 21MMRC011 | 151 | 152 | 1 | RC | **0.00** | 0.01 | **0.00** | **0.01** | 82 | 154 | 559 |
| 21MMRC011 | 152 | 153 | 1 | RC | **0.31** | 0.74 | **0.11** | **1.16** | 101 | 2180 | 1115 |
| 21MMRC011 | 153 | 154 | 1 | RC | **0.33** | 0.84 | **0.11** | **1.27** | 106 | 3570 | 1255 |
| 21MMRC011 | 154 | 155 | 1 | RC | **0.07** | 0.14 | **0.02** | **0.24** | 76 | 688 | 649 |
| | | | | | | | | | | | |
| 21MMRC012 | 82 | 83 | 1 | RC | **0.01** | 0.10 | **0.01** | **0.12** | 101 | 1220 | 771 |
| 21MMRC012 | 83 | 84 | 1 | RC | **0.31** | 0.39 | **0.10** | **0.80** | 111 | 2180 | 1225 |
| 21MMRC012 | 84 | 85 | 1 | RC | **0.13** | 0.26 | **0.03** | **0.42** | 84 | 556 | 731 |
| 21MMRC012 | 85 | 86 | 1 | RC | **0.08** | 0.26 | **0.02** | **0.36** | 92 | 838 | 782 |
| 21MMRC012 | 86 | 87 | 1 | RC | **0.05** | 0.10 | **0.03** | **0.18** | 84 | 389 | 627 |

| Hole_ID | M From | M To | Width | Sample Type | Pd | Pt | Au | 2PGE+Au | Co | Cu | Ni |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 21MMRC012 | 87 | 88 | 1 | RC | **0.07** | 0.12 | **0.02** | **0.20** | 86 | 302 | 620 |
| 21MMRC012 | 88 | 89 | 1 | RC | **0.13** | 0.31 | **0.04** | **0.47** | 102 | 826 | 775 |
| 21MMRC012 | 89 | 90 | 1 | RC | **0.25** | 0.55 | **0.08** | **0.88** | 99 | 1110 | 849 |
| 21MMRC012 | 90 | 91 | 1 | RC | **0.28** | 0.50 | **0.08** | **0.85** | 91 | 979 | 860 |
| 21MMRC012 | 91 | 92 | 1 | RC | **0.83** | 1.48 | **0.36** | **2.66** | 111 | 3690 | 1980 |
| 21MMRC012 | 92 | 93 | 1 | RC | **1.03** | 2.99 | **0.42** | **4.44** | 118 | 4300 | 2230 |
| 21MMRC012 | 93 | 94 | 1 | RC | **0.22** | 0.47 | **0.06** | **0.76** | 85 | 1100 | 920 |
| 21MMRC012 | 94 | 95 | 1 | RC | **0.01** | 0.04 | **0.00** | **0.05** | 80 | 278 | 594 |
| 21MMRC012 | 95 | 96 | 1 | RC | **0.04** | 0.07 | **0.01** | **0.12** | 91 | 901 | 732 |
| 21MMRC012 | 96 | 97 | 1 | RC | **0.05** | 0.10 | **0.02** | **0.16** | 93 | 891 | 752 |
| 21MMRC012 | 97 | 98 | 1 | RC | **0.14** | 0.19 | **0.06** | **0.40** | 104 | 1865 | 990 |
| 21MMRC012 | 98 | 99 | 1 | RC | **0.04** | 0.09 | **0.02** | **0.14** | 87 | 769 | 736 |
| 21MMRC012 | 99 | 100 | 1 | RC | **0.26** | 0.27 | **0.09** | **0.62** | 105 | 2140 | 1100 |
| 21MMRC012 | 100 | 101 | 1 | RC | **0.21** | 0.25 | **0.07** | **0.53** | 105 | 2220 | 1140 |
| 21MMRC012 | 101 | 102 | 1 | RC | **0.29** | 0.37 | **0.31** | **0.97** | 120 | 2870 | 1370 |
| 21MMRC012 | 102 | 103 | 1 | RC | **0.12** | 0.21 | **0.05** | **0.38** | 118 | 2250 | 1190 |
| 21MMRC012 | 103 | 104 | 1 | RC | **0.19** | 0.30 | **0.07** | **0.56** | 123 | 2530 | 1340 |
| 21MMRC012 | 104 | 105 | 1 | RC | **0.12** | 0.21 | **0.04** | **0.37** | 112 | 1780 | 1130 |
| | | | | | | | | | | | |
| 21MMRC012 | 133 | 134 | 1 | RC | **0.00** | 0.01 | **0.00** | **0.01** | 148 | 34 | 1980 |
| 21MMRC012 | 134 | 135 | 1 | RC | **0.13** | 1.09 | **0.03** | **1.25** | 167 | 1185 | 2350 |
| 21MMRC012 | 135 | 136 | 1 | RC | **0.27** | 1.07 | **0.04** | **1.38** | 148 | 512 | 2370 |
| 21MMRC012 | 136 | 137 | 1 | RC | **0.01** | 0.05 | **0.00** | **0.07** | 150 | 84 | 2040 |
| | | | | | | | | | | | |
| 21MMRC013 | 103 | 104 | 1 | RC | **0.03** | 0.05 | **0.15** | **0.23** | 88 | 2080 | 1000 |
| 21MMRC013 | 104 | 105 | 1 | RC | **1.12** | 1.06 | **0.34** | **2.51** | 88 | 1230 | 808 |
| 21MMRC013 | 105 | 106 | 1 | RC | **0.77** | 1.32 | **0.06** | **2.14** | 81 | 285 | 544 |
| 21MMRC013 | 106 | 107 | 1 | RC | **0.30** | 0.86 | **0.07** | **1.23** | 105 | 839 | 765 |
| 21MMRC013 | 107 | 108 | 1 | RC | **0.15** | 0.67 | **0.06** | **0.88** | 112 | 1090 | 918 |
| 21MMRC013 | 108 | 109 | 1 | RC | **0.03** | 0.05 | **0.02** | **0.10** | 108 | 1730 | 899 |
| 21MMRC013 | 109 | 110 | 1 | RC | **0.04** | 0.21 | **0.03** | **0.28** | 154 | 5250 | 1790 |
| 21MMRC013 | 110 | 111 | 1 | RC | **0.03** | 0.07 | **0.01** | **0.11** | 85 | 1010 | 736 |
| 21MMRC013 | 111 | 112 | 1 | RC | **0.08** | 0.18 | **0.03** | **0.29** | 76 | 517 | 592 |
| 21MMRC013 | 112 | 113 | 1 | RC | **0.19** | 0.41 | **0.10** | **0.70** | 97 | 1040 | 898 |
| 21MMRC013 | 113 | 114 | 1 | RC | **0.16** | 0.36 | **0.07** | **0.59** | 100 | 1260 | 928 |
| 21MMRC013 | 114 | 115 | 1 | RC | **0.00** | 0.02 | **0.01** | **0.03** | 66 | 122 | 466 |
| | | | | | | | | | | | |
| 21MMRC013 | 130 | 131 | 1 | RC | **0.05** | 0.10 | **0.02** | **0.16** | 53 | 274 | 445 |
| 21MMRC013 | 131 | 132 | 1 | RC | **0.23** | 0.49 | **0.09** | **0.82** | 86 | 1180 | 929 |
| 21MMRC013 | 132 | 133 | 1 | RC | **0.01** | 0.03 | **0.00** | **0.04** | 73 | 244 | 527 |
| | | | | | | | | | | | |
| 21MMRC014 | NSI | | | | | | | | | | |
| | | | | | | | | | | | |
| 21MMRC015 | 99 | 100 | 1 | RC | **0.13** | 0.13 | **0.06** | **0.32** | 80 | 1670 | 576 |
| 21MMRC015 | 100 | 101 | 1 | RC | **0.18** | 0.75 | **0.07** | **1.00** | 88 | 1915 | 656 |
| 21MMRC015 | 101 | 102 | 1 | RC | **0.27** | 0.72 | **0.14** | **1.13** | 89 | 3200 | 1100 |
| 21MMRC015 | 102 | 103 | 1 | RC | **0.20** | 0.50 | **0.10** | **0.80** | 92 | 2420 | 915 |
| 21MMRC015 | 103 | 104 | 1 | RC | **0.05** | 0.22 | **0.01** | **0.28** | 94 | 621 | 489 |

## JORC Code, 2012 Edition – Table 1

## SECTION 1 SAMPLING TECHNIQUES AND DATA

(Criteria in this section apply to all succeeding sections.)

| Criteria | | Commentary |
|---|---|---|
| **Sampling techniques** | *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*<br><br>*Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.*<br><br>*Aspects of the determination of mineralisation that are Material to the Public Report.*<br><br>*In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.* | Reverse circulation drilling was used to obtain both 2m composite and one metre samples, using a 5 ¼" face sampling hammer.<br><br>Samples were collected on a 2m composite basis to a prescribed depth predetermined by previous drilling, wireframing and assay data. Once the predetermined depth is achieved, the sampling reverts to one metre sample through the orezone to EOH.<br><br>After composite sample results received, all samples that return a value of >0.1g/t Au will result in the resplitting of the one metre bulk bags at site using a 75:25 jones riffle splitter. These one metre samples are then submitted for analysis.<br><br>All samples are pulverized to produce a 50g charge for fire assay.<br><br>Drilling sampling techniques employed at the Artemis core facility include saw cut HQ (63mm) drill core samples.<br><br>Both RC and HQ wireline core is currently being used to drill out the geological sequences and identify zones of mineralisation that may or may not be used in any Mineral Resource estimations, mining studies or metallurgical testwork.<br><br>Duplicate samples were collected at the rig from a static cone splitter, with the primary and duplicate bag both simultaneously collected from separate chutes.<br><br>For RC, the cyclone was cleared between rod changes to minimise contamination. |
| **Drilling techniques** | *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).* | Reverse Circulation drilling completed by Topdrill.<br><br>Drilling was completed using a truck mounted T685 Schramm rig mounted on 8x8 trucks<br><br>This can produce 1000psi/2700CFM with an axillary booster which is capable of achieving dry samples at depths of around 300m. |
| **Drill sample recovery** | *Method of recording and assessing core and chip sample recoveries and results assessed.*<br><br>*Measures taken to maximise sample recovery and ensure representative nature of the samples.*<br><br>*Whether a relationship exists between sample recovery and grade and whether* | Recoveries are recorded on logging sheets along with encounters with water and whether the samples are dry, moist or wet.<br><br>Drilling recoveries for Reverse Circulation drilling were >80% with some exceptions that maybe caused by loss of return through faults or encounters with water.<br><br>>90% of samples returned dry. |

| Criteria | | Commentary |
| --- | --- | --- |
| | *sample bias may have occurred due to preferential loss/gain of fine/coarse material.* | Statistical analysis shows that no bias of grade exists due to recoveries |
| **Logging** | *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*<br><br>*Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.*<br><br>*The total length and percentage of the relevant intersections logged.* | RC samples were collected from the static cone splitter as two samples, one bulk sample and one primary (analytical) sample.<br><br>The bulk samples are one metre splits.<br><br>These bags are then placed in neat rows of 50 bags each clear of the rig for safety reasons.<br><br>A field technician mixes the bag by hand before taking a sample using a sieve and sieves the sample to remove fines.<br><br>The sieved sample is then transferred to a wet sieve in a bucket of water, and the sample is sieved further until rock fragments are clearly visible.<br><br>These rock fragments are then logged by the site geologist, taking note of colour, grainsize, rock type, alteration if any, mineralisation if any, veining if any, structural information if notable and any other relevant information.<br><br>This information is then written down on pre-printed logging sheets, using codes to describe the attributes of the geology.<br><br>A representative sample is transferred to pre-labelled chip trays into the corresponding depth from where the sample was drilled from.<br><br>The remainder of the sample from the sieve is then transferred into a core tray that has been marked up by depths at metre intervals.<br><br>An identification sheet noting the hole number and from-to depths that correspond to each tray is then written up and placed above the tray and a photograph is taken of the chips.<br><br>The hole is logged in its entirety, hence 100%<br><br>The geological data would be suitable for inclusion in a Mineral Resource Estimation (MRE) |
| **Sub-sampling techniques and sample preparation** | *If core, whether cut or sawn and whether quarter, half or all core taken.*<br><br>*If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.*<br><br>*For all sample types, the nature, quality and appropriateness of the sample preparation technique.*<br><br>*Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.*<br><br>*Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance* | RC samples were collected on the drill rig using a cone splitter. If any mineralised samples were collected wet these were noted in the drill logs and database.<br><br>The RC drilling rig is equipped with a rig-mounted cyclone and static cone splitter, which provided one bulk sample of approximately 20-30 kilograms, and a sub-sample of approximately 2-4 kilograms for every metre drilled.<br><br>Field QC procedures involve the use of Certified Reference Materials (CRM's) as assay standards, along with duplicates and blank samples. The insertion rate of these was approximately 1:20.<br><br>For RC drilling, field duplicates were taken on a routine basis at approximately 1:20 ratio using the |

| Criteria | | Commentary |
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| | *results for field duplicate/second-half sampling.*<br><br>*Whether sample sizes are appropriate to the grain size of the material being sampled.* | same sampling techniques (i.e. cone splitter) and inserted into the sample run.<br><br>Primary and duplicates results have been compared.<br><br>The sample sizes are appropriate, representative and are considered more than adequate to ensure that there are no particle size effects relating to the grain size of the mineralisation. |
| **Quality of assay data and laboratory tests** | *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*<br><br>*For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*<br><br>*Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.* | All samples were assayed by ALS-Chemex (ALS) in Perth, which is a National Association of Testing Authorities (NATA) Australia accredited organisation. The laboratory techniques below are for all samples submitted to ALS and are considered appropriate for the style of mineralisation defined within the Carlow Castle Project area<br><br>The sample preparation followed industry best practice. Fire assay samples were dried, coarse crushing to ~10mm, split to 300g subsample, followed by pulverisation in an LM5 or equivalent pulverising mill to a grind size of 85% passing 75 micron.<br><br>This fraction was split again down to a 50g charge for fire assay<br><br>Both 30g and 50g sample sizes were chosen for analysis of gold, with fire assay (Au-AA26) with ICP finish and determination by AAS. The limit of 100 g/t was not reached for any samples. The larger sample size of 50g was predominantly selected to provide greater confidence in the analyses.<br><br>All samples were dried, crushed, pulverised and split to produce a sub-sample of 50g which is digested and refluxed with hydrofluoric, nitric, hydrochloric and perchloric acid (4 acid digest).<br><br>This digest is considered a total dissolution for most minerals.<br><br>Analytical analysis is performed using ICP-AES Finish (ME-ICP61A) for Ag, Al, As, Ba, Be, Bi, Ca, Cd, Co, Cr, Cu, Fe, Ga, K, La, Mg, Mn, Mo, Na, Ni, P, Pb, S, Sb, Sc, Sr, Th, Ti, Tl, U, V, W, Zn.<br><br>The original assay technique used for copper and cobalt was 0.25 g sample with four acid digest and ICP-AES finish. When the upper limits of the range recommended by the lab were exceeded, a method more appropriate method was used to re-assay another sample of the pulp. For assays that reached the limits of 1% for the 30 g, the laboratory method ME-ICP61A was triggered, using 0.40 g samples with the same liberation and finish techniques.<br><br>Standards are matrix matched by using previous pulps from drilling programs and homogenised using certified laboratories.<br><br>Standards were analysed by round robins to determine grade. |

| Criteria | | Commentary |
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| | | Standards were routinely inserted into the sample run at 1:20.<br><br>Laboratory standards and blank samples were inserted at regular intervals and some duplicate samples were taken for QC checks. |
| **Verification of sampling and assaying** | *The verification of significant intersections by either independent or alternative company personnel.*<br><br>*The use of twinned holes.*<br><br>*Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.*<br><br>*Discuss any adjustment to assay data.* | Sampling was undertaken by field assistants supervised by experienced geologists from Artemis Resources. Significant intercepts were checked by senior personnel who confirmed them as prospective for gold mineralisation.<br><br>No twin holes using RC was completed in this program.<br><br>Electronic data capture on excel spreadsheets which are then uploaded as .csv files and routinely sent to certified database management provider.<br><br>Routine QC checks performed by Artemis senior personnel and by database management consultant.<br><br>PDF laboratory certificates are stored on the server and are checked by the Exploration Manager. |
| **Location of data points** | *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*<br><br>*Specification of the grid system used.*<br><br>*Quality and adequacy of topographic control.* | A Garmin GPSMap62 hand-held GPS was used to define the location of the initial drill hole collars. Standard practice is for the GPS to be left at the site of the collar for a period of 5 minutes to obtain a steady reading. Collar locations are considered to be accurate to within 5m.<br><br>A high-quality downhole north-seeking multi-shot or continuous survey gyro-camera was used to determine the dip and azimuth of the hole at 30m intervals down the hole<br><br>The topographic surface was calculated from the onsite mine survey pickups and subsequently verified by RTK GNSS collar surveys.<br><br>Zone 50 (GDA 94).<br><br>Surface collar coordinates are surveyed via RTK GNSS with 1cm accuracy by a professional surveying contractor. |
| **Data spacing and distribution** | *Data spacing for reporting of Exploration Results.*<br><br>*Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.*<br><br>*Whether sample compositing has been applied.* | In certain areas, current drill hole spacing is variable and dependent on specific geological, and geochemical targets.<br><br>A nominal 40x20m drill spacing is considered adequate to establish the degree of geological and grade continuity appropriate for JORC (2012) classifications applied.<br><br>No sample compositing to date has been used for drilling completed by Artemis. All results reported are the result of 1 metre downhole sample intervals. |

| Criteria | | Commentary |
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| **Orientation of data in relation to geological structure** | *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*<br><br>*If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.* | Drill holes were designed to be perpendicular to the strike of known mineralisation. Due to the structural and geological complexity of the area, mineralisation of unknown orientation can be intersected. |
| **Sample security** | *The measures taken to ensure sample security.* | The chain of custody is managed by the supervising geologist who places calico sample bags in polyweave sacks. Up to 10 calico sample bags are placed in each sack. Each sack is clearly labelled with:<br><br>Artemis Resources Ltd<br><br>Address of laboratory<br><br>Sample range<br><br>Samples were delivered by Artemis personnel to the transport company in Karratha and shrink wrapped onto pallets.<br><br>The transport company then delivers the samples directly to the laboratory. |
| **Audits or reviews** | *The results of any audits or reviews of sampling techniques and data.* | Data is validated upon up-loading into the master database. Any validation issues identified are investigated prior to reporting of results. |

## SECTION 2 REPORTING OF EXPLORATION RESULTS

(Criteria listed in the preceding section also apply to this section.)

| Criteria | | Commentary |
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| **Mineral tenement and land tenure status** | *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*<br><br>*The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.* | Drilling by Artemis was carried out on E47/1797 – 100% owned by Artemis Resources Ltd. This tenement forms a part of a broader tenement package that comprises the West Pilbara Project.<br><br>This tenement is in good standing. |
| **Exploration done by other parties** | *Acknowledgment and appraisal of exploration by other parties.* | The most significant work to have been completed historically in the Carlow Castle area, including the Little Fortune and Good Luck prospects, was completed by Open Pit Mining Limited between 1985 and 1987, and subsequently Legend Mining NL between 1995 and 2008.<br><br>Work completed by Open Pit consisted of geological mapping, geophysical surveying (IP), and RC drilling and sampling. |

| Criteria | | Commentary |
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| | | Work completed by Legend Mining Ltd consisted of geological mapping and further RC drilling.<br><br>Legend also completed an airborne ATEM survey over the project area, with follow up ground-based FLTEM surveying. Re-processing of this data was completed by Artemis and was critical in developing drill targets for the completed RC drilling.<br><br>Compilation and assessment of historic drilling and mapping data completed by both Open Pit and Legend has indicated that this data is compares well with data collected to date by Artemis. Validation and compilation of historic data is ongoing.<br><br>All exploration and analysis techniques conducted by both Open Pit and Legend are considered to have been appropriate for the style of deposit. |
| **Geology** | *Deposit type, geological setting and style of mineralisation.* | The Carlow Castle Co-Cu-Au prospect includes a number of mineralised shear zones, located on the northern margin of the Andover Intrusive Complex. Mineralisation is exposed in numerous workings at surface along quartz-rich shear zones. Both oxide and sulphide mineralisation are evident at surface associated with these shear zones.<br><br>Sulphide mineralisation appears to consist of Chalcopyrite, chalcocite, cobaltite, pyrrhotite and pyrite |
| **Drill hole Information** | *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*<br><br>*easting and northing of the drill hole collar*<br><br>*elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar*<br><br>*dip and azimuth of the hole*<br><br>*down hole length and interception depth*<br><br>*hole length.*<br><br>*If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.* | Drill hole information is contained within this release. |
| **Data aggregation methods** | *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.*<br><br>*Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation* | All intervals reported are composed of 1 metre down hole intervals for Reverse Circulation drilling.<br><br>Aggregated intercepts do include reported lengths of higher-grade internal intercepts.<br><br>No upper or lower cut-off grades have been used in reporting results.<br><br>No metal equivalent calculations are used in this report. |

| Criteria | | Commentary |
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| | *should be stated and some typical examples of such aggregations should be shown in detail.*<br>*The assumptions used for any reporting of metal equivalent values should be clearly stated.* | |
| **Relationship between mineralisation widths and intercept lengths** | *These relationships are particularly important in the reporting of Exploration Results.*<br>*If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.*<br>*If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').* | The mineralisation in the Carlow Castle Western Zone strikes generally E-W and dips to the north at approximately -75 to -80 degrees. The drill orientation was 180 -60 dip. Drilling is believed to be generally perpendicular to strike. Given the angle of the drill holes and the interpreted dip of the host rocks and mineralisation, reported intercepts approximate true width.<br>True thicknesses are calculated from interpretation deriving from orientation of high-grade intervals, orientation of the main mineralised trend and its dip. This is an estimation only and can change according to additional information. |
| **Diagrams** | *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.* | Appropriate plans are shown in the text. |
| **Balanced reporting** | *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.* | This release reports the results of five RC holes. The significant results tabulated in the release are reported at a base grade of >0.5 g/t Au or >0.5% Cu. Internal dilution of up to 2 m may be included in an intersection. |
| **Other substantive exploration data** | *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.* | Targeting for the RC drilling completed by Artemis was based on compilation of historic exploration data, and the surface expression of the targeted mineralised shear zones and associated historic workings. |
| **Further work** | *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).*<br>*Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.* | Further work (RC and diamond drilling) is justified to locate extensions to mineralisation both at depth and along strike. |

## SECTION 3 – Estimation and Reporting of Mineral Resources

| Criteria | JORC Code explanation | Commentary |
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| **Database integrity** | *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* | Geophysical files were uploaded from the data logging device to the contractor's central storage database and then provided in both raw and corrected/filtered format in CSV, LAS and PDF format. This has removed the potential for transcription errors and for reference checks.<br><br>Core logging was completed by Artemis on site using project-specific logging codes and a database management system; DataShed™, with primary key fields and look-up tables. Collar survey, down hole survey and assay files were loaded from source files using templates to load into predefined tables. These measures enforced strict referential integrity and validation rules to prevent corruption errors.<br><br>The Competent Person found no material errors and deemed the database was fit for the purpose of Mineral Resource estimation. |
| | *Data validation procedures used.* | The Competent Person checked the drillhole files for the following errors prior to Mineral Resource estimation:<br>• Absent collar data<br>• Multiple collar entries<br>• Questionable downhole survey results<br>• Absent survey data<br>• Overlapping intervals<br>• Negative sample lengths<br>• Sample intervals which extended beyond the hole depth defined in the collar table.<br>• Assay values reported as negative detection limits were updated to half detection limits. |
| **Site visits** | *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* | The Competent Person has not visited the site, but has relied on information from colleague Mr Matt Clark, Senior Resource Geologist, collected during a site visit in April 2021. |
| | *If no site visits have been undertaken, indicate why this is the case.* | The Competent Person considers that the information provided to him by colleague Mr Matt Clark allows him to appropriately consider the necessary factors in establishing Mineral Resources for the confidence estimated. |
| **Geological interpretation** | *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* | The host lithologies at Carlow Castle are basalt and gabbro, with mineralisation predominantly in basalt with a strong lithological control on mineralisation between basalt and gabbro. The dominant control on mineralisation is by structures potentially far smaller than the drill hole spacing and smaller than which can be explicitly modelled. Therefore, the geological model consisted of waste and mineralisation. |
| | *Nature of the data used and of any assumptions made.* | No material assumptions have been made which affect the MRE reported herein. |
| | *The effect, if any, of alternative interpretations on Mineral Resource estimation.* | The Competent Person is confident any alternative interpretations would result in globally immaterial differences in the Mineral Resource estimate. |
| | *The use of geology in guiding and controlling Mineral Resource estimation.* | Mineralisation generally shows a continuous grade distribution from un-mineralised through to high grade, with minor inflection points within the log-probability plot |

| Criteria | JORC Code explanation | Commentary |
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| | *The factors affecting continuity both of grade and geology.* | for the distribution. One such inflection occurs at 200 ppm Cu, on which definition of mineralisation lodes were based. A second cut-off at 500 ppm correlated with high-grade copper, gold, and cobalt, and also correlated with structural measurements defined by structural logging and modelling.<br><br>The geological model includes a shallow, approximately 3 m thick overburden surface and an oxide horizon that averages 40 m depth. Transitional material is typically 10 to 20 m thick and extends down to 100 m depth in the eastern section of Carlow Main. |
| **Dimensions** | *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.* | The Carlow Main lodes have been modelled as a set of anastomosing fingers extending off and conjoining a major central zone that follows a broad sigmoidal curve whose average centreline at 769,660 mN strikes 1,200m east-west. The anastomosing lodes vary in thickness from 5 m where they pinch to 90 m in the thickest portion. The high-grade 500 ppm copper shell averages 30-40m thick, within the low-grade 200 ppm copper wireframe that extends up to 50 m to the north and south. At the western end, mineralisation dips steeply north, and at the eastern end it dips steeply south. Mineralisation in Carlow Main has been interpreted to a maximum of 630 m below surface, averaging 280 m.<br><br>The Quod Est and Cross Cut mineralisation have been modelled similarly with low-grade 200 ppm copper shell and inner high-grade 500 ppm grade shells. Quod Est and Cross-Cut lodes have been interpreted as a steeply east dipping lodes. The major lode at Quod Est outcrops and strikes NNE, bifurcates at its southern third, and measures about 200 m overall, with maximum depth of 180 m. The Cross Cut mineralisation has been interpreted as two lode structures that strike 150 m NNE and dip steeply east, to a maximum depth of 180 m. |
| **Estimation and modelling techniques** | *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen, include a description of computer software and parameters used* | The Mineral Resources were estimated within nine estimation domains, representing Carlow Castle Main, Quod Est and Cross Cut, formed from the mineralisation model interpreted at nominal cut-offs of 200 ppm and 500 ppm Cu. The domains were further split into overburden, oxide and fresh by the oxidation wireframes. A small volume wireframe was modelled in the eastern section of Carlow Main based on a 0.5 g/t Au cut-off to control the influence of high-grade holes that were drilled subparallel to mineralisation.<br><br>All geological modelling was undertaken using Leapfrog Geo software. Estimation domains were modelled using indicator interpolants and the nominal 200 ppm Cu, 500 ppm Cu, and 0.5 g/t Au cut-off grades.<br><br>Statistics, grade and density estimates, and variography, were undertaken in Supervisor software, and composite selection and block coding, undertaken in Surpac software, used the combined domains as hard boundaries.<br><br>Samples were composited to 1 m intervals based on assessment of the raw drillhole sample interval lengths.<br><br>Quantitative Kriging Neighbourhood Analysis (QKNA) was undertaken using Supervisor software to assess the effect |

| Criteria | JORC Code explanation | Commentary |
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| | | of changing key kriging neighbourhood parameters on block grade and density estimates. Kriging Efficiency and Slope of Regression were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids. A two-pass search ellipse strategy was adopted, whereby the first pass equated to the full range of the relevant variogram model for each domain, with a minimum of 8 samples, maximum of 20 samples and a maximum of 6 samples per hole. The second pass search ellipse was between 2 to 3.5-times the variogram model range, with a minimum of 8 samples, maximum of 16 samples and a maximum of 6 samples per hole. All blocks were filled in the first two passes.<br><br>A 20 mE x 10 mN x 10 mRL parent cell size was constructed covering the full volume of the mineralisation and additional space for mine infrastructure planning. Sub-celling was employed to 5 mE x 5 mN x 5 mRL to improve block volume fitting to the complex wireframe. Mineralisation domains were coded in the block model below the overburden surface, and further coded by oxidation domain.<br><br>High grade cuts were used to constrain outliers in the dataset as described above.<br><br>Grade interpolation for Au, Cu, Co, As, S was completed using ordinary kriging (OK) into the parent block cells. The search employed a dynamic anisotropy to allow the ellipse to rotate along the sinusoidal mineralisation domains. |
| | *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* | Several previous historical resource estimates have been completed previously. These reports were available to the Competent Person. These did not necessarily cover the same area as this Mineral Resource update and were volumetrically smaller in their extent. Further; while these Previous Mineral Resources are quoted below, the approach taken to modelling and estimation differs fundamentally from that of the current estimate Consequently, the models are not directly comparable.<br><br>In 2018, Mr Philip Jones estimated Mineral Resources reported in accordance with the JORC Code for Carlow South using drilling data provided by Artemis to model mineralisation wireframes that were based on a total net smelter return of >$30 using the following metal factors:<br>• Copper: Price: $4.473/lb; Recoveries: 75% (mining and metallurgical recovery)<br>• Gold: Price: $USD1282.10/oz; Recoveries: 90% (mining and metallurgical)<br>• Cobalt: Price: $54,500/t; Recoveries: 75% mining and metallurgical<br><br>In January 2019 Al Maynard & Associates estimated Inferred Mineral Resources at Carlow Castle South and Quod Est of 7.7 Mt @ 0.51% Cu, 1.06 g/t Au and 0.08% Co.<br><br>Four domains, based on the strike of the mineralisation, were used in the modelling. High grade cuts were also applied using mean grades +2SD of copper, gold and cobalt per domain. Grades were interpolated by Inverse Distance Squared ($ID^2$). |

| Criteria | JORC Code explanation | Commentary |
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| | | In November 2019, CSA Global estimated Inferred Mineral Resources at Carlow Castle South and Quod Est of 8 Mt @ 0.6% Cu, 1.6 g/t Au and 0.08% Co, reported above a lower cut-off of 0.3% Cu, and within a theoretical optimised pit shell.<br><br>Two estimation domains for Carlow Main and Quod Est were used in the modelling based on a lower cut-off grade of 500 ppm copper. Grade interpolation was completed initially by ordinary kriging into panels, with post-processing using localised uniform conditioning (LUC) within the panels to derive an estimate at the smaller selective mining unit (SMU) scale. Grade limiting was employed in the panel estimates to restrict the influence of very high grades to 10 m.<br><br>The optimised pit shell used for the Mineral Resource reporting used the following parameters:<br>• 50º overall slope angle<br>• Oxide and Fresh used same recoveries/processing costs<br>• $48.1/t processing cost<br>• 85% copper recovery<br>• 94.8% gold recovery<br>• 73% cobalt recovery<br>• Mining costs $/t incremented by depth ranging from $2.57 through to $5.77 inclusive.<br>• Copper: $9000/t<br>• Gold: $2000/oz<br>• Cobalt: $48,000/t |
| | *The assumptions made regarding recovery of by-products.* | The co-products, gold and cobalt, are assumed to be recoverable within the mineralisation wireframe volumes that have been modelled on a copper grade cut-off. The metallurgical testwork for gold and cobalt may not be representative of the material reported as Mineral Resources. However, the metallurgical testwork results show that gold and cobalt can be recovered. |
| | *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).* | Arsenic and sulphur have been estimated, although it is unknown at this stage of the project if they are deleterious for copper, gold and cobalt. |
| | *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* | The dimensions of the parent block used for estimation represents approximately half the drillhole spacing in the X orientation and one quarter the spacing in the Y orientation. |
| | *Any assumptions behind modelling of selective mining units.* | SMU units were not modelled. The parent block size of 10 m in the Z direction is approximately twice the size of assumed SMU of 5 m high mining benches.<br><br>The assumed SMU has been determined based on the assumption of a production scenario utilising small to medium size earthmoving equipment (for reference; 125 tonne excavator, plus CAT 777 or equivalent haul trucks). In the experience of the Competent Person, this |

| Criteria | JORC Code explanation | Commentary |
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| | | equipment selection may be considered typical for a deposit of the size and style of Carlow Castle. |
| | *Any assumptions about correlation between variables* | No assumptions have been made regarding the correlation of variables. |
| | *Description of how the geological interpretation was used to control the resource estimates.* | Logged geology, alteration and structural controls were used in the interpretation of lodes within the resource model. Hard boundaries were used for estimation between mineralised domains. |
| | *Discussion of basis for using or not using grade cutting or capping.* | For the estimate of grades, high-grade cuts were applied to reduce the influence of extreme outliers. These values, determined by statistical analysis including review of CV values, histograms, log-probability plots and mean-variance plots. |
| | *The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.* | Standard model validation was completed using numerical methods (histogram and swath plots) and validated visually in section and 3D against the input raw drillhole data, composites and blocks. |
| **Moisture** | *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.* | Tonnages have been estimated on a dry basis. |
| **Cut-off parameters** | *The basis of the adopted cut-off grade(s) or quality parameters applied.* | The Mineral Resources were reported at a 0.3 ppm Au.Eq cut-off, within a Whittle™ theoretical optimisation that used the following factors:<br>• 50° overall slope angle<br>• Oxide, Transitional and Fresh used same recoveries / processing costs<br>• $48.1 / tonne processing (includes refining, insurance and G&A)<br>• Recoveries, which in Artemis' opinion have a reasonable potential to be achieved, are:<br>• 85% Cu recovery<br>• 94.8% Au recovery<br>• 73% Co recovery<br>• Mining Costs $ / tonne incremented by depth (coded into each block in the model by RL), ranging from $2.57 through to $5.77 inclusive<br>• Prices:<br>o Cu $9,400 / tonne<br>o Au $2,200 / oz<br>o Co $50,000 / tonne<br>• 2.5% royalty per ounce payable on gold produced. 5% royalties per tonne payable on both copper and cobalt produced.<br>• Au.Eq was calculated from a combined weighted grade of Au, Cu, Co using the same commodity prices and metallurgical recoveries as the optimisation.<br>Au.Eq = Au (ppm) + Cu (%)x1.19 + Co (%) x 5.44 |
| **Mining factors or assumptions** | *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for* | Open pit mining is considered as the appropriate method for future studies, and the Competent Person believes that there are reasonable prospects for eventual economic extraction based on the outputs of the Whittle optimisation completed. |

| Criteria | JORC Code explanation | Commentary |
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| | *eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.* | A minimum mining width of 2 m was applied (downhole composite width). No other mining assumptions were made.<br>Detailed mining assumptions such as dilution and minimum mining widths will be included in any optimisation, detailed mine planning and Life of Mine plan. |
| **Metallurgical factors or assumptions** | *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.* | Preliminary metallurgical testwork was conducted by ALS Metallurgy in 2019 focussing on the metallurgical amenability of selected samples to a conventional gravity gold, cyanide leach and flotation processes.<br>Results are detailed below:<br>Gold<br>• 48% of gold by testwork on metallurgical samples was recovered using gravity separation, and most of the balance of the non-gravity gold is recoverable in sulphide concentrates as a by-product using standard flotation.<br>Copper<br>• Quick floating copper minerals produced a high-grade, premium copper concentrate of approximately 30% Cu.<br>• Deleterious elements including arsenic may be managed with a light concentrate polishing using regrind or blend control. Recoveries depended on mineralogy, with 77–85% copper recoveries achieved.<br>• Unrecovered copper minerals are predominantly represented by non-floating silicates or secondary oxide copper minerals.<br>Cobalt<br>• Cobalt recoveries ranged from 73–79%. Saleable Cobalt concentrate grades ranging 2.3–5.3% Co were produced. Cobaltite (CoAsS) is the dominant cobalt bearing mineral and is therefore intrinsically linked to arsenic affecting its sale price.<br>Artemis believe the gold recovered by metallurgical testwork could be sold in concentrates as a credit or recovered on site using a cyanide leach process.<br>Acid soluble copper testwork has been completed for oxide and transitional ore and estimated in the block model by inverse distance (ID2) to guide additional metallurgical sampling.<br>CSA Global recommend additional metallurgical programs across the Mineral Resource incorporating results from acid soluble copper and multi-element analysis. Further geometallurgical testwork to develop quantitative mineralogy and rock mass studies is also recommended. |
| **Environmental factors or assumptions** | *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the* | No assumptions regarding possible waste and process residue disposal options have been made.<br>Sulphur and arsenic have been estimated into the model to allow the assessment of potentially acid forming minerals and other environmentally sensitive residue. |

| Criteria | JORC Code explanation | Commentary |
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| | *determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered, this should be reported with an explanation of the environmental assumptions made.* | |
| **Bulk density** | *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* | For mineralisation, downhole geophysical gamma density was used to estimate density by OK using the relevant variogram and estimation parameters for each statistical domain.<br><br>Only sample points that had a calliper measurement of not more than 20% of the nominal hole diameter for each hole type were included in the analysis and data for estimation. The gamma density was visually correlated point-by-point to each overlapping water immersion determination of specific gravity on HQ3 core, which found a strong correlation.<br><br>The size and range of lengths of density determinations are considered by the Competent Person to be robust. A correlation of 0.05 was calculated between sample lengths and density determinations, confirming that the sample length has no impact on the density.<br><br>The gamma-density of the RC hole is weakly low-biased compared to the diamond core density, while the gamma-density of the diamond hole is very weakly high-biased.<br><br>Sample points were composited to 1 m length prior to estimation.<br><br>Waste densities were applied from nominal values. |
| | *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.* | The gamma determines a quantitative, in situ measurement of density that accounts for void spaces. The measurements have been calibrated to regular calibration holes in iron ore deposits in the Pilbara, and on materials at the contractor's facility.<br><br>The water immersion method measurements were determined by measuring the weight of part or the entire sample in air and water and then applying the formula bulk density = weight_air/(weight_air-weight_water). Samples of drill core were sealed with a masonry sealant/wax and allowed to dry prior to bulk density determination.<br><br>The estimate of density was undertaken within oxidation domains in the mineralisation. |
| | *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.* | The gamma density data were considered sufficient in number for all material types, quantitative and unbiased when large calliper deviations from the nominal hole diameter were removed. Calibration was undertaken using comparison to other holes and to density measured by water immersion. The approach adopted is considered robust. |
| **Classification** | *The basis for the classification of the Mineral Resources into varying confidence categories.* | The MRE was classified as Inferred based on the level of geological understanding of the mineralisation, quality of samples, density data, drillhole spacing, historical nature of the drilling, detail of metallurgical information available |

| Criteria | JORC Code explanation | Commentary |
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| | | for soluble / insoluble copper speciation and sampling and assaying processes. |
| | *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* | The classification reflects the overall level of confidence in mineralised domain continuity based the mineralisation drill sample data numbers, spacing and orientation. Overall mineralisation trends are reasonably consistent within the various lithotypes over numerous drill sections. |
| | *Whether the result appropriately reflects the Competent Person's view of the deposit.* | The Mineral Resource classifications applied appropriately reflect the view of the Competent Person. |
| **Audits or reviews** | *The results of any audits or reviews of Mineral Resource estimates.* | Internal audits were completed by CSA Global which verified the technical inputs, methodology, parameters and results of the estimate. |
| **Discussion of relative accuracy/ confidence** | *Where appropriate, a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* | The accuracy of the MREs is communicated through the classification assigned to the various parts of the deposits. The MREs have been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this table.<br>The MRE statement relates to a global estimate of in-situ tonnes and grade. |
| | *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* | The accuracy of the MREs is communicated through the Inferred classification assigned to the deposit. The MRE has been classified in accordance with the JORC Code. All factors that have been considered have been adequately communicated in Section 1, Section 2 and Section 3 of this table.<br>The MRE statement relates to a global estimate of in-situ tonnes and grade. |
| | *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.* | No production data are available. |