

## 2021 MINERAL RESOURCES AND ORE RESERVES UPDATE

### MINERAL RESOURCES

- Total Mineral Resources of 44.3Mt @ 1.7g/t for 2.5Moz
  - Total Measured & Indicated Mineral Resources of 25.4Mt @ 1.6g/t for 1.3Moz
- Mt Morgans Gold Operations
  - Total Mineral Resources of 32.4Mt @ 1.8g/t for 1.8Moz
  - Jupiter Mining Area Measured & Indicated of 12.5Mt @ 1.2g/t for 475,000oz
  - Greater Westralia Area Measured & Indicated of 3.4Mt @ 4.1g/t for 454,000oz
- Redcliffe Project
  - Total Mineral Resources of 11.9Mt @ 1.7g/t for 638,000oz
  - Total Measured & Indicated Mineral Resources of 1.6Mt @ 3.1g/t for 154,000oz

### ORE RESERVES

- Total Ore Reserves of 11.3Mt @ 1.1g/t for 385,000oz
- Mt Morgans Gold Operations
  - Total open pit Ore Reserves of 5.5Mt @ 1.2g/t for 215,000oz
  - Total underground Ore Reserves of 0.5Mt @ 4.7g/t for 74,000oz
- Redcliffe Project
  - Indicated Mineral Resources at Hub, GTS and Nambi pending final technical studies prior to assessment as potential additions to Ore Reserves

Dacian Gold Limited (**Dacian Gold or the Company**) (**ASX: DCN**) provides its 2021 Mineral Resources and Ore Reserves estimate as of 30 June 2021. The Company's previous Mineral Resources and Ore Reserves estimates were as of 31 December 2019.

## MINERAL RESOURCES

The total Mineral Resources estimate for the Mt Morgans Gold Operation (Mt Morgans) and Redcliffe Project (Redcliffe) as at 30 June 2021 is shown in **Table 1** below.

**Table 1: Total Mineral Resource estimate as at 30 June 2021 (after mining depletion)**

MINING CENTRE	Deposit/Area	Deposit/Prospect	Cut-off grade (Au g/t)	Measured			Indicated			Inferred			Total Mineral Resource			Reporting date
				Tonnes (kt)	Au g/t	Au Oz	Tonnes (kt)	Au g/t	Au Oz	Tonnes (kt)	Au g/t	Au Oz	Tonnes (kt)	Au g/t	Au Oz	
MT MORGANS	Westralia Mine Corridor	Beresford	2.0	160	4.72	24,000	1,940	4.02	251,000	1,490	3.01	144,000	3,590	3.63	419,000	11/05/2021
		Allanson	2.0	70	4.18	9,000	570	4.50	82,000	900	3.94	114,000	1,530	4.16	205,000	11/05/2021
		Morgans North - Phoenix Ridge	2.0							330	6.66	72,000	330	6.66	72,000	11/05/2021
	Westralia Satellite deposits	Transvaal	2.0				650	3.76	79,000	1,110	3.54	126,000	1,760	3.62	205,000	30/06/2021
		Craic	2.0				30	8.27	9,000	70	5.93	13,000	100	6.67	22,000	30/06/2021
		Ramornie OP & UG	0.5 & >290RL OR 2.0 & <290RL							730	2.53	59,000	730	2.53	59,000	30/06/2021
		McKenzie Well	0.5							950	1.10	34,000	950	1.10	34,000	16/02/2021
	GREATER WESTRALIA MINING AREA	SUBTOTAL	2.0	220	4.56	33,000	3,190	4.10	421,000	5,570	3.14	562,000	8,990	3.51	1,015,000	
	Jupiter OP*	Heffernans*	0.5				1,610	1.16	60,000	-			1,610	1.16	60,000	30/06/2021
		Doublejay*	0.5	3,620	1.46	170,000	3,440	1.02	112,000	340	0.92	10,000	7,400	1.23	292,000	30/06/2021
		Ganymede*	0.5				2,450	0.95	75,000	250	0.99	8,000	2,700	0.95	83,000	30/06/2021
		Mt Marven*	0.5				1,250	1.22	49,000	580	1.42	27,000	1,860	1.26	76,000	30/06/2021
		Jupiter UG**	2.0	10	2.45	1,000	110	2.42	8,000	910	2.69	79,000	1,030	2.66	88,000	30/06/2021
	JUPITER MINING AREA	SUBTOTAL		3,630	1.46	171,000	8,850	1.07	304,000	2,090	1.84	124,000	14,600	1.28	599,000	
	Cameron Well	Cameron Well*	0.5				2,510	1.10	89,000	370	1.30	16,000	2,880	1.10	105,000	31/12/2019
		Maxwells	0.5				170	0.90	5,000	500	0.75	12,000	660	0.79	17,000	30/06/2021
	CAMERON WELL PROJECT AREA	SUBTOTAL					2,680	1.09	94,000	870	0.99	28,000	3,550	1.04	119,000	
REDCLIFFE PROJECT AREA	SOUTHERN ZONE OP & UG	Mine Stockpiles	0	110	1.03	4,000							110	1.03	4,000	30/06/2021
		LG Stockpiles	0	1,680	0.62	34,000							1,680	0.62	34,000	30/06/2021
		Jupiter LG Stockpiles (Dump Leach)	0	3,490	0.51	57,000							3,490	0.51	57,000	30/06/2021
		STOCKPILES		5,280	0.56	95,000							5,280	0.56	95,000	
		TOTAL MMGO		9,130	1.01	298,000	14,720	1.73	819,000	8,530	2.60	713,000	32,410	1.75	1,827,000	
	CENTRAL ZONE OP & UG	GTS	0.5 & >300RL OR 2.0 & <300RL				840	2.00	54,000	1,220	1.20	47,000	2,060	1.53	101,000	30/06/2021
		Hub	0.5 & >300RL OR 2.0 & <300RL				530	4.7	80,000	580	3.2	60,000	1,110	3.91	140,000	30/06/2021
		Bindy	0.5 & >300RL OR 2.0 & <300RL							3,080	1.30	129,000	3,080	1.30	129,000	30/06/2021
		Kelly	0.5 & >300RL OR 2.0 & <300RL							2,350	0.89	67,000	2,350	0.89	67,000	30/06/2021
		SUBTOTAL					1,370	3.04	134,000	7,220	1.30	303,000	8,590	1.58	437,000	
		Nambi	0.5 & >300RL OR 2.0 & <300RL				190	3.30	20,000	1,350	2.70	117,000	1,530	2.77	137,000	30/06/2021
		Redcliffe	0.5 & >300RL OR 2.0 & <300RL							930	1.19	35,000	930	1.19	35,000	30/06/2021
		Mesa / Westlode	0.5 & >300RL OR 2.0 & <300RL							850	1.04	28,000	850	1.04	28,000	30/06/2021
		SUBTOTAL					190	3.30	20,000	3,130	1.80	181,000	3,320	1.88	201,000	
	TOTAL REDCLIFFE	SUBTOTAL					1,560	3.07	154,000	10,350	1.45	484,000	11,910	1.67	638,000	
TOTAL				9,130	1.01	298,000	16,280	1.86	973,000	18,880	1.97	1,197,000	44,320	1.73	2,465,000	

\* reported with a \$2,400 RPEEE pit shell

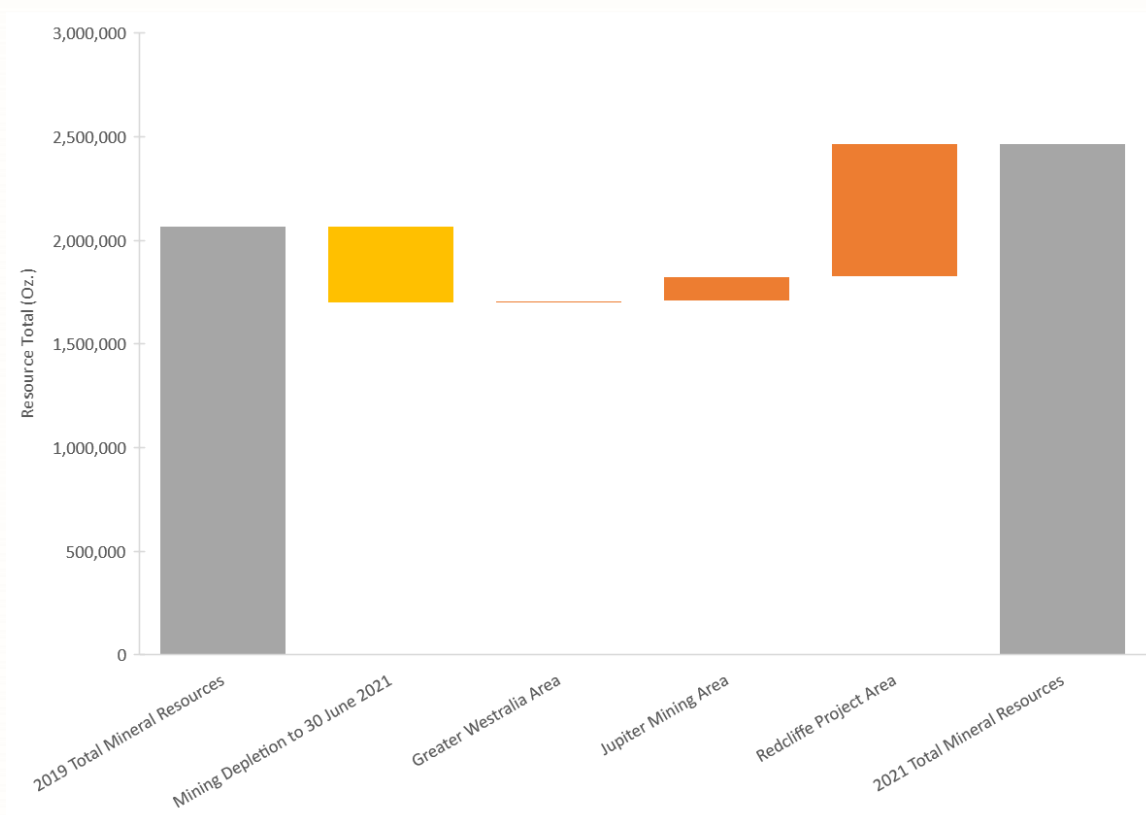
\*\* reported below a \$2,400 RPEEE pit shell

## Key Changes for Mineral Resources

Key changes versus the 2019 Mineral Resource estimate are:

- Updated geological interpretation, estimation parameters, classification, and reporting constraints have been applied to all updated Mineral Resources with the exception of Cameron Well
- Total Mineral Resources increased from 2.1Moz to 2.5Moz
- Total Measured and Indicated (M&I) Mineral Resources reduced from 1.5Moz to 1.3Moz
- Total Inferred Mineral Resources increased from 0.6Moz to 1.2Moz

The significant changes in the Mineral Resources versus the Company's 2019 Mineral Resources estimate are shown in Figure 1.



**Figure 1: Waterfall chart of variances in Mineral Resources from 31 December 2019 to 30 June 2021**

## Mt Morgans

### Jupiter Mining Area

A revised Mineral Resource estimate has been made for Jupiter (which includes Doublejay, Heffernans and Ganymede) and Mt Marven deposits based on additional diamond drilling (DD), reverse circulation (RC) and RC with DD tail drilling. The Jupiter Mining Area Mineral Resources have been depleted for the mined volumes from the Doublejay, Heffernans and Ganymede pits, and for the Mt Marven pit.

## Greater Westralia Area

The Beresford, Allanson, Morgans North and Phoenix Ridge Mineral Resource estimates are unchanged from the 11 May 2021 announcement. Transvaal, Craic, and Ramornie Mineral Resource estimate updates have now been completed. These three deposits were updated incorporating the latest drilling data, reinterpretation of the geology and mineralisation, review of statistics, re-estimation of grades, review and update of the density estimate, reclassification, change to the reporting cut-off grades and spatial constraints.

## Cameron Well Area

The Mineral Resource estimate for Cameron Well has been assessed and remains unchanged from the 2019 Mineral Resource estimate (see ASX announcement dated 27 Feb 2020). The Maxwell Bore Mineral Resource was updated following additional RC drilling.

## Redcliffe Project

The Company has now updated the Mineral Resource estimates for the remainder of the deposits, which include GTS, Kelly, Bindy, Mesa–Westlode, Nambi and Redcliffe. For Bindy, new drilling data was available to assist the Mineral Resource update, while for all deposits including Bindy, the Mineral Resources were updated by reinterpretation of the geology and mineralisation, review of statistics, re-estimation of grades, review and update of the density estimate, reclassification, change to the reporting cut-off grades and spatial constraints.

For further information, refer to Appendix 1 for the explanation of the details of the Mineral Resource updates in accordance with ASX reporting requirement listing rule 5.8, and Appendix 2 for all Table 1 details.

## ORE RESERVES

The Company's total Ore Reserve estimate as of 30 June 2021, after mining depletion is shown in Table 2 below.

**Table 2: Total Ore Reserve estimate as at 30 June 2021**

Deposit	Cut-off Grade	Proved			Probable			Total		
	Au g/t	Tonnes t	Au g/t	Au oz	Tonnes t	Au g/t	Au oz	Tonnes t	Au g/t	Au oz
Jupiter OP	0.5	2,710,000	1.4	124,000	2,848,000	1.0	92,000	5,558,000	1.2	216,000
Westralia UG	*0.4/2.4	40,000	5.8	7,000	453,000	4.6	66,000	492,000	4.7	74,000
Mine Stockpiles	0.5	107,000	1.0	4,000	-	-	-	107,000	1.0	4,000
LG Stockpiles	0.5	5,173,000	0.5	91,000	-	-	-	5,173,000	0.5	91,000
<b>TOTAL ORE RESERVE</b>		<b>8,030,000</b>	<b>0.9</b>	<b>226,000</b>	<b>3,301,000</b>	<b>1.5</b>	<b>158,000</b>	<b>11,330,000</b>	<b>1.1</b>	<b>385,000</b>

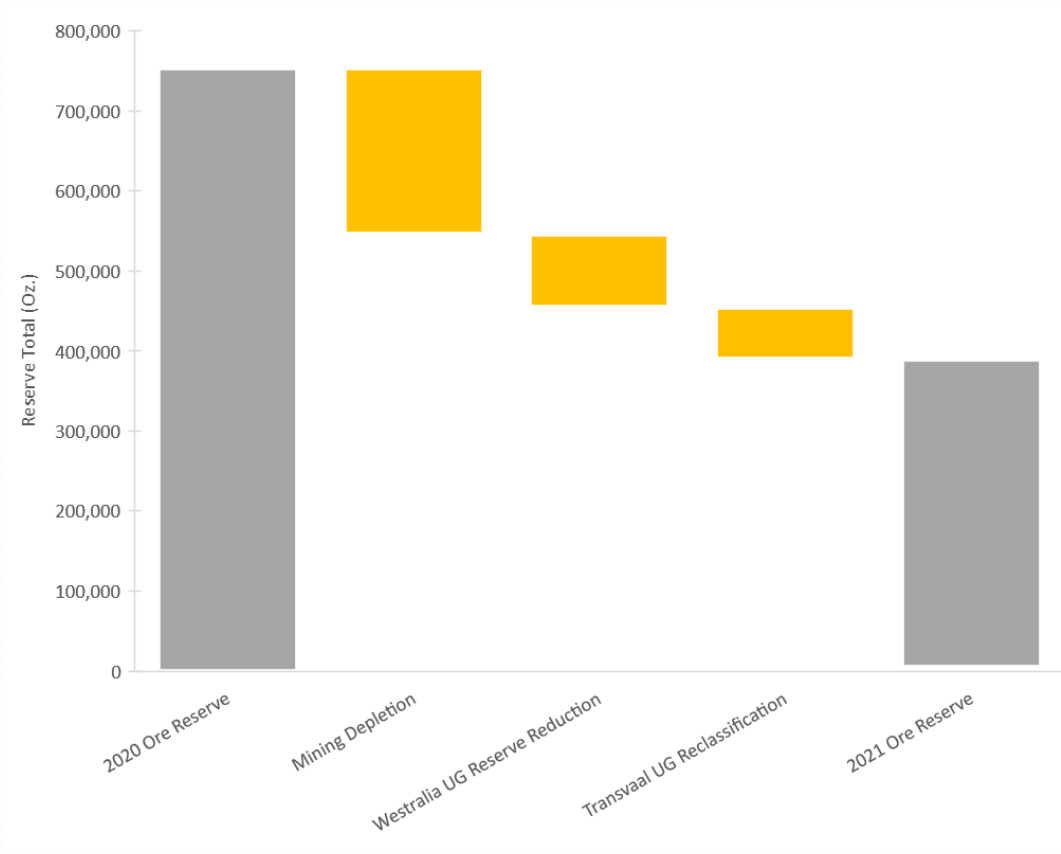
*\*Development and stoping grades respectively. Rounding errors will occur*

Compared to the January 2020 Ore Reserve estimate, the updated Ore Reserves see a decrease in total Ore Reserves from 754,000oz to 385,000oz, predominantly from mining depletion and an updated Ore Reserve for Westralia underground.

## Key Changes for Ore Reserves

The change in the updated Ore Reserve estimate compared to the January 2020 Ore Reserve is shown in Figure 2 and detailed below:

- Mining depletion from January 2020 to June 2021 totals 208,000oz
- Reduction in Ore Reserves for the Westralia underground totalling 91,000oz
- Removal of Transvaal underground from the Ore Reserve estimate totals 65,000oz



**Figure 2: Key variances between 1 January 2020 and 30 June 2021 Ore Reserve estimate**

The majority of the reduction in Ore Reserves was driven by mining depletion across the Jupiter open pits, Mt Marven open pit and the Westralia underground since January 2020 to June 2021 for a total of 208,000oz.

Reduction in Ore Reserves at the Westralia underground is a function of a complete revision of the Mineral Resource estimates for the Beresford and Allanson deposits (see ASX announcement dated 11 May 2021).

The Transvaal underground was removed from Ore Reserves following the updated Mineral Resource estimation and classification. Given the significant remaining Indicated Mineral Resource, technical studies continue to advance and mine dewatering activities have commenced ahead of a resource definition program.

### **Material Assumptions for Ore Reserve Estimate**

The following material assumptions were applied to the June 2021 Ore Reserve update. Assumptions regarding mining method, equipment selection and ore loss and mining dilution have not materially changed from the January 2020 Ore Reserve estimate.

- Gold price of A\$2,100/oz has been applied to check-optimisations for the Jupiter open pits and to estimate cut-off-grade to guide stope optimisations for the Beresford and Allanson deposits at the Westralia underground
- Current operational capital and operating cost structure
- Current operational mining, processing and metallurgical performance

- Geotechnical recommendations based on modelling and site inspections completed by an independent geotechnical engineer

## **Ore Reserve Classification**

The classification of the Jupiter Ore Reserve has been carried out in accordance with the recommendations outlined in the JORC Code (2012). It is based on Mineral Resource classification, the selected mining method and cost estimates.

All Proven and Probable Ore Reserves have been derived from Measured and Indicated Mineral Resources respectively. No Inferred Mineral Resources have been included in the Ore Reserve. No Probable Ore Reserves have been derived from Measured Mineral Resource.

## **Mining Method**

For the Jupiter open pit Ore Reserve, mechanised open pit mining remains the selected mining method.

The Jupiter open pit Ore Reserve estimate is based on detailed pit designs generated using mining software. Mining recovery and dilution was modelled through conversion of the Mineral Resource block model to a regularised Mining Model and estimated by taking into account ore width, orebody dip, excavator size and the grade of the diluent material.

For the Westralia underground Ore Reserve, the underground mining method of top-down long hole open stoping with pillars remains the selected mining method.

The Westralia Ore Reserve estimate is based on the application of detailed three-dimensional mine designs generated using mining software to Mineral Resource block models. Stope designs assumed a minimum mining width of 1.1m as well as a 0.2m of 'dilution skin' applied to the stope hangingwall and footwall. An additional dilution modifying factor ranging from 5-16% was applied to stopes based on operational performance observed by the Company until mining ceased in August 2020. For designed ore drives, a 5% dilution factor was applied at zero grade.

A mining recovery factor of 95% was applied to stopes in addition to allowances made for in-situ rib and sill pillars required to maintain void stability. A 95% mining recovery factor was also applied to ore drives.

## **Processing Method**

Ore mined will be treated through the Mt Morgans CIL Processing Plant. A metallurgical recovery factor of 92.7% has been applied which is based on the average metallurgical recovery achieved treating a blended ore feed from Jupiter, Westralia and historical ore stockpiles since the processing plant was commissioned in March 2018.

Evidence of deleterious elements has not been observed since commissioning of the Processing Plant in March 2018 to the date of this Ore Reserve update as at 30 June 2021 when treating a blended feed of ore mined from the Jupiter open pits and Westralia underground.

## **Cut-off-Grade**

Break-even cut-off grades have been determined by considering gold price, royalties, average metallurgical recoveries achieved for a blended feed at the Mt Morgans processing plant, contractor and owner mining costs, surface ore haulage costs where applicable (Westralia underground) and ore processing costs.

For the Jupiter open pit, a cut-off-grade of 0.5 g/t has been selected and applied in the estimation of the Ore Reserve.

For the Westralia underground, a cut-off grade of 0.4g/t has been applied as an incremental cut-off grade for development ore mined to honour the Ore Reserve stope design. For stoping, a cut-off grade of 2.4g/t has been applied.

## **Estimation Methodology and Mineral Resource Estimate**

Refer to Mineral Resource Estimate section.

## **Material Non-Mining Parameters**

Key non-mining parameters considered in the Ore Reserve Estimate include:

- All mining tenements have been granted, regulatory approvals and permits are in place for mining the Jupiter open pits and Westralia underground.
- All required mining and processing infrastructure is in place.
- Agreements are in place for the transport and sale of gold doré produced from Mt Morgans.

< ENDS >

*This ASX announcement was approved and authorised for release by the Board of Dacian Gold Limited*

For further information please contact:

Leigh Junk Dacian Gold Limited +61 8 6323 9000 info@daciangold.com.au	Phil Russo Dacian Gold Limited +61 8 6323 9000 info@daciangold.com.au
--	--

## **COMPETENT PERSON STATEMENT**

### **MINERAL RESOURCES**

The information in this report that relates to Mineral Resources is based on information compiled by Mr Alex Whishaw, a Competent Person who is a member of the Australasian Institute of Mining and Metallurgy. Mr Whishaw is a full-time employee of Dacian Gold Ltd. Mr Whishaw has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code 2012). Mr Whishaw consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

Where the company refers to the Mineral Resources and Ore Reserves in this report (referencing previous releases made to the ASX including Cameron Well and Hub), it confirms that it is not aware of any new information or data that materially affects the information included in that announcement and all material assumptions and technical parameters underpinning the Mineral Resource estimate and Ore Reserve estimate with that announcement continue to apply and have not materially changed. The Company confirms that the form and context in which the Competent Persons findings are presented have not materially changed from the original announcement.

All information relating to the Mineral Resources and Ore Reserves were prepared and disclosed under the JORC Code 2012.

### **ORE RESERVES**

The information in this report that relates to the Jupiter open pit Ore Reserve is based on information compiled or reviewed by Mr Ross Cheyne. Mr Cheyne has confirmed that he has read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code 2012 Edition). He is a Competent Persons as defined by the JORC Code 2012 Edition, having more than five years' experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity for which they are accepting responsibility. Mr Cheyne is a Fellow of the Australasian Institute of Mining and Metallurgy and an employee of Orelogy Consulting Pty Ltd. He consents to the inclusion in the report of the matters based on their information in the form and context in which it appears.

The information in this report that relates to the Westralia underground Ore Reserve is based on information compiled or reviewed by Mr Andrew Cooper. Mr Cooper has confirmed that he has read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code 2012 Edition). He is a Competent Persons as defined by the JORC Code 2012 Edition, having more than five years' experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity for which they are accepting responsibility. Mr Cooper is a Member of the Australasian Institute of Mining and Metallurgy and an employee of Orelogy Consulting Pty Ltd. He consents to the inclusion in the report of the matters based on their information in the form and context in which it appears.



## APPENDIX 1:

### MINERAL RESOURCE ESTIMATES: TECHNICAL BACKGROUND

#### Jupiter

##### GEOLOGY AND GEOLOGICAL INTERPRETATION

The deposit is Archean lode gold style.

The Jupiter deposit is interpreted to comprise structurally controlled mesothermal gold mineralisation related to syenite intrusions within altered basalt. A majority of mineralisation is associated with large shallow east dipping shears, with significant mineralisation developing where these shears crosscut syenite intrusions or the altered basalt proximal to the syenite intrusions.

The largest, most continuous and generally highest tenor lodes are formed within the Cornwall Shear Zone (CSZ), a deposit-wide structure.

Several small structures in the form of shears, faults and veins dip either steeply to the west, or moderately towards the north-west, north and/or north-east.

The confidence in the geological interpretation around the GC and resource development drilling areas is very high where the drilling density is at 10 m by 10 m out to 20 m by 20 m, and is based on mining exposure as well as a high drilling density. Visual confirmation of lode position and orientations has been observed and mapped in the Mount Marven operating open pit.

Ongoing infill drilling has confirmed geological and grade continuity.

Geological and structural logging and pit mapping have been used to assist identification and delineation of lithology and mineralisation.

All lodes were treated as hard-boundaries for statistics and estimation.

Doublejay geological objects modelled were:

- Lodes: 67 (including two CSZ lodes)
- Syenite intrusive pipes: two (Joanne and Jenny)
- Syenite stocks: 2
- Syenite dykes: 5
- Porphyry dykes or combined intrusive bodies: 2

Heffernans geological objects modelled were:

- Lodes: 61 (including eight CSZ lodes)
- Syenite intrusive pipes: 1
- Syenite dykes: 4
- Porphyry dykes: 5

Ganymede geological objects modelled were:

- Lodes: 41
- Syenite intrusive pipes: 1
- Porphyry dykes: 3

The mineralisation was modelled with a relatively strict gold cut-off of 0.3 g/t Au, which has been confirmed as appropriate for the mining methods and ore markouts. All modelled lodes were treated as hard boundaries for statistics and estimation, although where geological and statistical observations deemed suitable, the lodes were grouped into domains for increased sample counts.

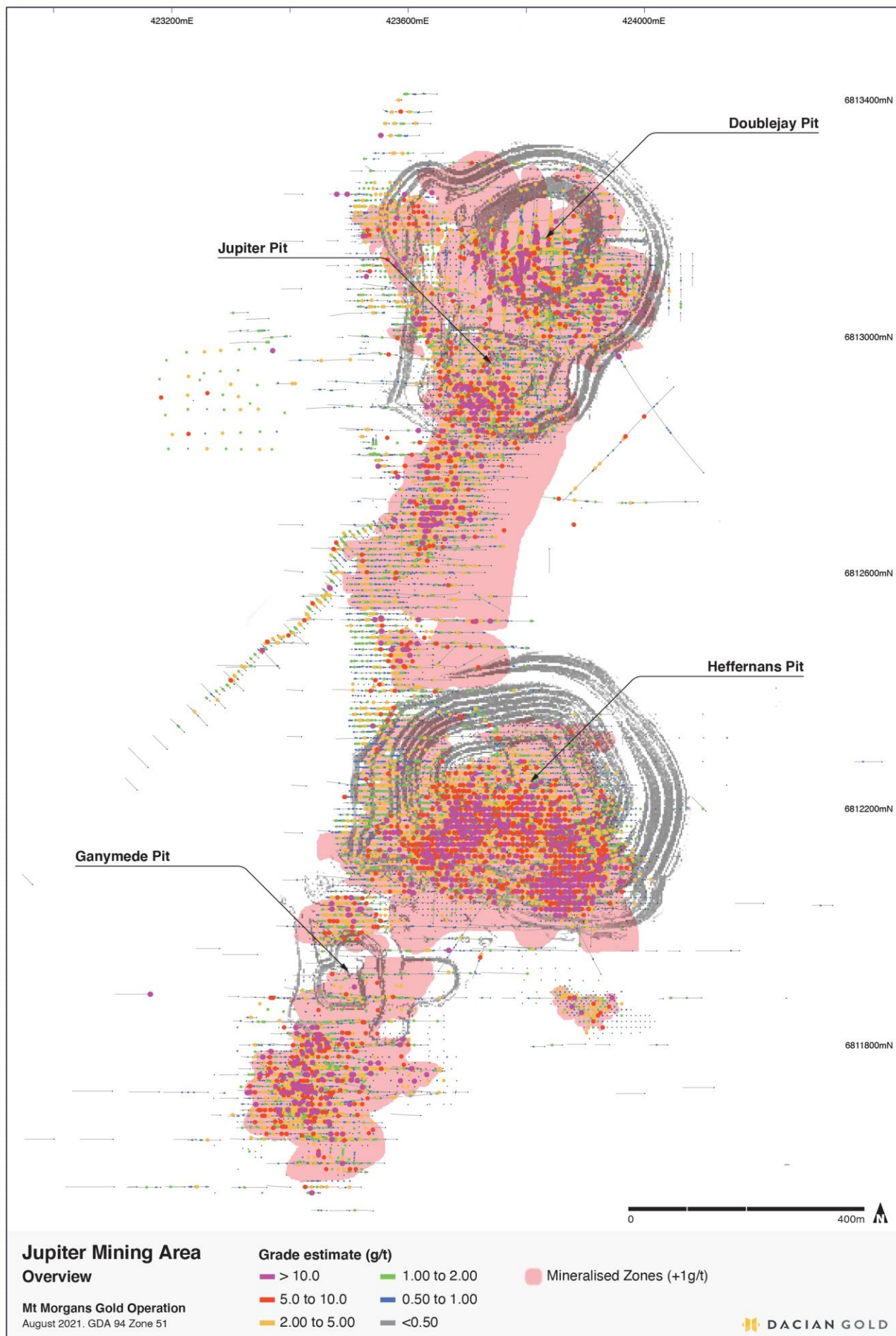
The composited samples within the modelled lode objects were used to estimate the corresponding block object codes with the resource block model.

The lodes show high continuity through the oxidation/weathering profile without dispersion halos. Statistics were reviewed, including grade distributions, and contact analysis, between the oxidation domains, which showed that evidence for boundaries was weak, although almost all lodes do not transect any of the modelled oxidation surfaces. Therefore, no hard boundaries by oxidation domain were applied.

The larger syenite intrusive pipes are the core bodies from which the lodes protrude as flat-lying, stacked, mineralised structures. There is evidence that the syenite stocks and dykes are also associated with higher grade mineralisation.

Contact and continuity statistical analysis confirmed that no or soft boundaries existed for the lodes within and outside the syenites.

A plan of the updated Jupiter Mineral Resource is provided in Figure 3.



**Figure 3: Jupiter plan showing the mineralisation wireframes used to constrain the Jupiter Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**

## DRILLING TECHNIQUES

Drilling that informed the Mineral Resource estimate (MRE) was exclusively surface drilling, which included 9,532 RC holes for 347,462 m, 67 diamond drill (DD) holes for 14,422.81 m, and 49 RC holes with DD tails for 13,684.78 m.

Drilling that intersected modelled mineralisation lodes or other mineralised and modelled geological objects, whose data were used to estimate grades for the Mineral Resource estimate (MRE), included 7,188 RC holes for 272,383 m, of which 6,479 holes for 190,013 m were drilled for grade control (GC) purposes (average of 29 m), 65 diamond drill (DD) holes for 13,473.81 m, and 46 RC holes with DD tails for 12,463.14 m.

98% of holes that intersected modelled mineralisation were drilled by Dacian.

Dominion Mining Limited drilled 93\*, 94\* and 95\* prefixed holes (168 holes) Ausdrill, Robinsons and Drillex RC rigs. 1 m samples were collected using a riffle splitter. Only samples expected to be anomalous were sent to the onsite lab for analysis.

and one Dominion hole were removed from the resource modelling database,

The following number of holes with specified prefixes were ignored or removed from the MRE, as their data were considered unreliable.

- 14 of the 39 “95\*” prefixed holes
- 44 of the 190 “HR\*” prefixed holes
- Five of the “HD\*” prefixed holes

90 of Dacian’s RC GC holes were removed, as their data had not been acquired in time, or were dummy entries in the database that had not been drilled.

The Jupiter area includes many historic drilling types not used in the MRE.

Dacian Diamond drilling was mostly carried out with NQ2 sized equipment, along with minor HQ3 and PQ2, using standard tube. Surface drill core was orientated using a Reflex orientation tool.

Dominion holes (94MCRC and 95MCRC holes) were drilled with RC rigs utilising face-sampling hammers for maximum sample return.

Other than the drill type being RC, nothing is known about the MM historic holes.

## SAMPLING AND SUB-SAMPLING TECHNIQUES AND SAMPLE ANALYSIS METHOD

Surface RC holes were angled to intersect the targeted mineralised zones at optimal angles.

In-pit RC holes were dominantly angled to the west to intersect the prevailing east dip and plunge of the mineralisation, but also vertical to target mineralised zones at optimal angles, and to fit around historic workings.

For historical RC drilling, where available, the original logs and laboratory results that are in the central SQL Server database are retained by Dacian as either original hard copies or as scanned copies.

Dominion Mining Limited drilled 93\*, 94\* and 95\* prefixed holes (168 holes) Ausdrill, Robinsons and Drillex RC rigs. 1 m samples were collected using a riffle splitter. Only samples expected to be anomalous were sent to the onsite lab for analysis.

For Dacian RC holes, face sampling hammer bits with size from 5¼” to 5¾” were used (99% of reverse circulation (RC) holes) except where a 4¾” and 3½” face sampling hammer was used for 98 and 2 holes respectively.

The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data

Dacian surface diamond core was sampled as half core at 1m intervals or to geological contacts. Sampling did not cross geological boundaries. Samples were cut in half, sampled into lengths in sample bags to achieve approximately 3kg, and submitted to a contract laboratory for crushing and pulverising to produce either a 40g or 50g charge for fire assay.

Dacian surface RC holes are sampled over the entire length of hole. Dacian RC drilling was sampled at 1m intervals via an on-board cone splitter to achieve approximately 3kg samples. Samples were then submitted to a contract laboratory for crushing and pulverising to produce either a 40g or 50g charge for fire assay.

Dacian in pit RC holes were sampled over the entire length of hole on 1m intervals via an on-board cone splitter to achieve approximately 3kg samples.

Prior to December, 2020, all samples were submitted to a contract laboratory for crushing and pulverising to produce either a 40 g or 50 g charge for fire assay.

After December, 2020, GC samples were submitted to the on-site laboratory for Pulverise and Leach (PAL) analyses using a 600 g subsample.

#### ESTIMATION METHODOLOGY

Samples were composited to 1 m intervals (“composites”) based on assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.

To model the spatial continuity of gold grades, variography was conducted in Supervisor 8.12. Statistics were length-weighted.

Composite samples were declustered prior to variography for the statistical domains that contained lodes (i.e. not syenite and porphyry domains).

A normal-score transform was applied to continuity analysis data.

After variograms were modelled, a back-transform model was exported with Datamine rotations for use in Datamine parameter files.

Variograms were modelled for each statistical domain where possible, or borrowed from the most geologically related domain. Many statistical domains showed good variograms. Other variograms were coerced into the plane of the lode orientations, and then variograms were constructed with reasonable structures evident for most, although some required variograms to be informed entirely by the lode orientations and geometries guided by modelling of other, better informed statistical domains.

The core-immersion method determinations from Jupiter diamond core number 20,806 on a variety of whole, half and quarter core, approximately 10% of which are from the top 50 m of the hole, although some of these may have been drilled from pit floors or other in-pit platforms.

Material type	Count of sample_type
HALF_BQ	573
HALF_HQ2	828
HALF_HQ3	5,332
HALF_NQ2	10,745
HALF_PQ2	32
QUARTER_HQ2	455
QUARTER_HQ3	99
QUARTER_NQ2	1,590
QUARTER_PQ2	1,150
WHOLE_HQ3	1
WHOLE_NQ2	1
<b>Grand Total</b>	<b>20,806</b>

Quantitative gamma-density measurements were captured on six Ganymede GC holes and four Doublejay resource development holes in February 2021 by Surtech to mitigate the risk of the lack of density determinations in oxide and transitional material.

Void space has been accounted for in the industry-standard, immersion method core density determination process.

The data were adjusted for measured porosity in fresh Ganymede and Doublejay material utilising borehole magnetic resonance (BMR) data. The BMR data quantitatively assesses the porosity of the material logged, from which the percentage of porosity was removed to provide an in-situ, dry bulk density.

A porosity of 5% and 3% was applied to the density of fresh material respectively for Ganymede and Doublejay.

Porosity values of 10% for oxide and 7.5% for transitional were assumed.

### **Doublejay:**

For most lode domains and the syenite and porphyry domains, a short-range (~6 m to ~15 m in the major and semi-major directions, less in the minor direction) and long range structure (20 m to 50 m in the major direction) were modelled.

The CSZ showed longer ranges in all directions for all structures.

Multi-block KNA was undertaken. KNA found that a 10 x 10 x 5 block size gave the best statistics, marginally better than 5 x 5 x 2.5 block size, which was considered more appropriate for the drillhole density across the unmined area of the deposit. The KNA confirmed that the best statistics were for minimum samples of 8 to 10 and maximum samples of between 15–20 inclusive, although for porphyry and syenites the minimum was dropped to 6. Max samples per drillhole were set to 4 for all lodes and domains other than CSZ, which was set to 3. A max of 4 for lodes was selected because. The short-range structure was often very short (11 m to 27 m), so forcing 3 samples per drillhole and with a minimum of 8 samples to achieve a minimum of 3 holes in any estimate was detrimental to the estimates of lode fringes.

The largest short-range modelled was for Syenite domain 6 of 49 m. The full range of any variogram modelled was capped at 5 x the short range if the experimental variography suggested longer.

The best statistics were achieved for a search ellipse size matching the short-range structure in all cases, followed by the full range.

Statistics were invariable for changes in discretization.

Insufficient samples were available to model FW3 (no variogram maps could be calculated), therefore, the variogram modelled for FW2 was borrowed.

An unrotated block model was created in MGA Zone 51 grid to cover the extent of the deposit. The deposit is a subset of the larger Jupiter deposit; therefore, to avoid overlap with the Heffernans MRE, the model is relatively truncated to the mineralisation. However, the mining area has been established, and therefore mining studies do not require infrastructure design elements to be built using the model cells.

A parent block size of 10 m x 10 m x 5 m (X x Y x Z) was chosen, which was supported by drill hole spacing in X and Y directions. Some areas of tighter drilling at grade control density exist, but most of the deposit has been drilled at a density of 20 m x 20 m out to 40 m x 40 m on the fringes. The dominant 1 m sample length and the Jupiter bench height of 5 m support the shorter block height. Nominally spaced 10 m to 20 m pierce points have been achieved, although this is highly variable resulting from the variable hole angles.

Sub-celling to 1/8 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.

Based on statistical analysis that no or soft boundaries existed, the CSZ and lodes were estimated with all corresponding composites for the lode number, inside and outside the syenites.

The estimate employed OK within a 3-pass expanding search ellipse strategy, honouring the anisotropic ratios orthogonally, which was based on KNA results to improve the local grade estimate without unacceptable error, while ensuring a globally unbiased estimate.

Lodes:

Pass 1: 1st short-range structure of the statistical domain variogram with dynamic anisotropy applied.



Pass 2: full range of the variogram, except for CSZ domain 30001, which has three structures, the third being too large for a second pass search ellipse.

Pass 3: typically 5 times the first ellipse volume, but adjusted to 6 x and 7 x for lodes that required larger search volumes to estimate fringe blocks, and 10 x for the deep syenite where it is mostly uninformed by samples. The min and max samples were dropped to 4 and 8 respectively.

To handle the wireframe flexures (and local variability in the lode orientations known from mining to exist), dynamic anisotropy was applied for the 1st pass of mineralisation only.

Density values assigned in the previous MRE, tabulated below, were used to compare against the gamma-density values and provide cross-validation:

Oxidation	Waste (Mafic)	Mineralisation (shear-hosted in mafic)	Syenite
Oxide	1.80	1.80	2.24
Trans	2.83	1.80	2.55
Fresh	2.94	2.86	2.65

The gamma-density values were filtered to be within 20% of the nominal hole diameter, determined by the density caliper arm. The data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging, which was available for:

DJRD\_STG2\_0099 from 100.1 m to 109.02 m

DJRD\_STG2\_0101 from 24.41 m to 79.27 m

The average porosity (assumed to be all fresh) for the data was 3%, which was used to adjust all densities from the gamma.

The gamma-density data could not be extracted by lithological type, but the values were confirmed to be from the following:

Zone	Type	Wireline Geophysics Records (10 cm points)	Metres Logged
	Mafic waste	65,175	6,517.5
10	CSZ	1,300	130
1002	Syenite	50	5
1004	Syenite	25	2.5
1021	Syenite	1,975	197.5
14	CSZ	1,100	110
3046	Mineralisation lode	2,275	227.5
3047	Mineralisation lode	3,750	375
3102	Mineralisation lode	1,875	187.5

The Doublejay Mineral Resources are almost entirely depleted for Oxide and transitional material. Therefore, the gamma-density data are derived from fresh material, and instead of using the data for assignment or estimation, the data were used to validate the core density determinations, with the following observations made:

- A small amount of weathering impact was noted in the immersion-method core densities not noted in the gamma-densities at the same RL.
- The gamma-density data largely correlates with the values for the same depths in the core densities, once the scatter is removed and the banding disregarded for comparison.
- A cluster between 2.8 t/m<sup>3</sup> and 3.1 t/m<sup>3</sup> existed, which provides little indication of a relationship between fresh lithologies and density.
- However, there were distinct bands noted for the (mostly) fresh core densities, which could not be ignored, and therefore the data were coded by zone and oxidation to determine the geological relationships, which were averaged for comparison:

Oxidation	Waste (Mafic)	Mineralisation (shear-hosted in mafic)	Syenite (waste and mineralisation)	Porphyries
Oxide	N/A	N/A	N/A	N/A
Trans	2.94	2.82	N/A	2.76
Fresh	2.94	2.86	2.91	2.84

Although very limited transitional material remained, it was carefully considered. The transitional mineralisation averaged 2.82, but the graphs suggest an assignment of 2.65 is more appropriate. The syenite density values were adjusted to those closer to the analysis defined for the Ganymede quantitative data.

The values assigned for oxide and transitional material by bench are shown below:

Oxidation	Waste (Mafic)	Mineralisation (shear-hosted in mafic)	Syenite (waste and mineralisation)	Porphyries
Oxide	N/A (1.80 used in macro)	N/A (1.80 used in macro)	N/A (2.24 used in macro)	N/A (2.24 used in macro)
Trans	2.82	2.65	2.65	2.76
Fresh	2.94	2.86	2.75	2.84

### **Hefferenans:**

All of the oxide and transitional, and most of the fresh material within the current and RPEEE pit shells have been depleted. The following describes the modelling briefly in context of the grade control model.

The CSZ, hanging-wall showed the best variogram.

For most lode domains and the syenite and porphyry domains, a short-range and longer-range structure were modelled.

All variograms contained a high to very high nugget when back-transformed.

KNA was initially undertaken on a well-informed block within a well-informed area of the CSZ, but the statistics for this block were uninformative. Therefore, multi-block KNA was undertaken. KNA found that a 5 x 5 x 2.5 block size gave the best statistics, which was considered appropriate for the drillhole density for the unmined area of the deposit.

The KNA confirmed that the best statistics were for minimum samples of 8 to 10 and maximum samples of 24 to 28 were appropriate for lodes dependent on the domain, while 6 minimum and 12 maximum. The best statistics were achieved for a search ellipse size matching the short-range structure, followed by the full range. Statistics were invariable for changes in discretization.

Variogram data for CSZ reviewed by DR for orientation, nugget, and modelled structures Anisotropic ratios with application of successive search volumes and influence reviewed.

An unrotated block model was created in MGA Zone 51 grid to cover the extent of the deposit. The deposit is a subset of the larger Jupiter deposit; therefore, to avoid overlap with the Ganymede and Doublejay MREs, the model is relatively truncated to the mineralisation.

A parent block size of 5 m x 5 m x 2.5 m (X x Y x Z) was chosen, which was supported by drill hole spacing in X and Y directions. Some areas of tighter drilling at grade control density exist, most of the remainder of the deposit has been drilled at a density of 10 m by 10 m and 10 m by 8 m out. The dominant 1 m sample length and the Jupiter bench height of 5 m support the shorter block height.

Sub-celling to 1/40 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.

The estimate employed OK within a 3-pass expanding search ellipse strategy, honouring the anisotropic ratios orthogonally, which was based on KNA results to improve the local grade estimate without unacceptable error, while ensuring a globally unbiased estimate.



Gamma-density data were not available at the time of density assignment for these deposits. However, the Mineral Resources for these areas are entirely depleted for Oxide and transitional material. Therefore, core-immersion method determinations were used for the density assignment.

Lithology	Oxidation	Value
Mafic mineralisation	Oxide	1.8
	Transitional	1.8
	Fresh	2.86
Mafic waste	Oxide	1.8
	Transitional	2.83
	Fresh	2.94
Syenite	Oxide	2.24
	Transitional	2.55
	Fresh	2.65
Porphyry	Oxide	2.15
	Transitional	2.61
	Fresh	2.73
Carbonatite	Oxide	N/A
	Transitional	2.6
	Fresh	2.72
Transported sand	All	2.2
Dump fill	All	2.0

### **Ganymede:**

The CSZ, hanging-wall showed the best variogram, followed by the syenite and FW1 and FW2 statistical domains. Other variograms were coerced into the plane of the lode orientations, and then variograms were constructed with reasonable structures evident for most, although some required variograms to be informed entirely by the lode orientations and geometries guided by modelling of other, better informed statistical domains.

For most lode domains and the syenite and porphyry domains, a short-range (~6 m to ~15 m) and longer (but relatively short around 20 m) range structure were modelled. The CSZ also had two spherical structures modelled, but the longer range was much longer than other domains, reflecting the greater size and continuity of the lodes. Variography for two poorly informed supergene statistical domains yielded a single spherical structure.

All variograms contained a high to very high nugget when back-transformed.

KNA was initially undertaken on a well-informed block within a well-informed area of the CSZ, but the statistics for this block were uninformative. Therefore, multi-block KNA was undertaken. KNA found that a 5 x 5 x 2.5 block size gave the best statistics, marginally better than 10 x 10 x 5, which was considered more appropriate for the drillhole density across the partially mined area of the deposit. The KNA confirmed that the best statistics were for minimum samples of 7 to 9 and maximum samples of typically less than 20. The best statistics were achieved for a search ellipse size matching the short-range structure, followed by the full range. Statistics were invariable for changes in discretization.

Variogram data for CSZ reviewed by DR for orientation, nugget, and modelled structures Anisotropic ratios with application of successive search volumes and influence reviewed.

An unrotated block model was created in MGA Zone 51 grid to cover the extent of the deposit. The deposit is a subset of the larger Jupiter deposit; therefore, to avoid overlap with the Heffernans MRE, the model is relatively truncated to the mineralisation. However, the mining area has been established, and therefore mining studies do not require infrastructure design elements to be built using the model cells.

A parent block size of 10 m x 10 m x 5 m (X x Y x Z) was chosen, which was supported by drill hole spacing in X and Y directions. Some areas of tighter drilling at grade control density exist, but most of the deposit has been drilled at a density of 20 m x 20 m out to 40 m x 40 m on the fringes. The dominant 1 m sample length and the Jupiter bench height of 5 m support the shorter block height. Nominally spaced 10 m to 20 m pierce points have been achieved, although this is highly variable resulting from the variable hole angles.

Sub-celling to 1/8 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.

The estimate employed OK within a 3-pass expanding search ellipse strategy, honouring the anisotropic ratios orthogonally, which was based on KNA results to improve the local grade estimate without unacceptable error, while ensuring a globally unbiased estimate.

Lodes:

Pass 1: 1st range structure of the statistical domain variogram with dynamic anisotropy applied. min 7 to 9, max 17 to 23, max per hole 4

Pass 2: full range of the variogram, min 7 to 9, max 17 to 23, max per hole 4

Pass 3: 200 m search ellipse (major); min 3, max 10, max per hole 4

To handle the wireframe flexures (and local variability in the lode orientations known from mining to exist), dynamic anisotropy was applied for the 1st pass of mineralisation only.

For Ganymede, density values assigned in the previous MRE, tabulated below, were used to compare and validate the gamma-density values:

Oxidation	Waste	Mineralisation
Oxide	1.80	1.80
Trans	2.83	1.80
Fresh	2.94	2.86

The updated density estimate was based on the analysis of gamma-density values filtered to be within 20% of the nominal hole diameter, determined by the density caliper arm. The data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging, which was available for only 32 m from surface for one hole, GAGC\_400\_0379. The average density porosity across the 32 m, assumed to be entirely oxide, was calculated as 10% of the mass. Reduced porosities of 7.5% and 5% were assumed for the transitional and fresh materials respectively.

Two clear trends were noted in the final adjusted gamma-density values:

- A vertical alignment of density for fresh mineralisation and waste, i.e. the density is invariable for changes in depth, and has a visual average of 2.9 t/m<sup>3</sup>, which was assigned to the fresh mineralisation and waste.
- A gradational, inverse relationship between density and depth (as the depth decreases, the density increases) for oxide and transitional material. There was no relationship noted between density and lithology. The densities were averaged by depth for the oxide and transitional material to account for the positive relationship between density and depth.

The density assignment was calculated as follows:

- An average for each 5 m bench depth was calculated for the caliper-filtered, porosity-adjusted data.
- An order-relation adjustment that ensured that the average density for each successively shallower bench was equal to or less than the bench below it.
- As no data existed for oxide and transitional syenite, and porphyry material, the proportion from visual fresh values were used to reduce the density against waste and mineralisation, as follows:
  - Syenite: 2.65/2.9
  - Porphyry: 2.75/2.9
- The values assigned for oxide and transitional material by bench
- Caliper filtered, pore and order relation adjusted density averages assigned by bench for oxide and transitional material only are shown below:

bench_top_ 5m	Mineralisation density value assigned	Syenite density value assigned	Porphyry density value assigned
>=400	1.62	1.48	1.54
395	1.70	1.55	1.61
390	1.86	1.70	1.76
385	1.92	1.75	1.82
380	1.93	1.76	1.83
375	1.95	1.78	1.85
370	1.95	1.78	1.85
365	2.08	1.90	1.97
360	2.10	1.92	1.99
355	2.25	2.06	2.13
350	2.25	2.06	2.13
345	2.47	2.26	2.34
340	2.47	2.26	2.34
335	2.47	2.26	2.34
<=330	2.47	2.26	2.34

## CLASSIFICATION

The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:

- Drill density data
- Geological understanding
- Quality of gold assay grades
- Continuity of gold grades
- Economic potential for mining.

For Indicated Mineral Resources, statistical consideration has been employed to assess the grade estimate quality in considering large, contiguous, and coherent zones of blocks form zones where:

- Large areas are formed that have been grade control drilled, but also extending out to where drill hole spacing reaches 20 m to 20 m max.
- Estimation was chiefly undertaken in search passes of 1 and 2.
- Number of samples was predominantly near the optimum.
- Slope of regression formed large volumes of > 0.4 with cores of 0.6.

For Measured Mineral Resources, large contiguous volumes were required that that had reached a GC drill spacing of 10 m by 10 m, or not more than 20 m by 20 m near the GC drilling areas and where very high grade continuity was established.

The remainder of the mineralisation was classified as Inferred.

## CUT-OFF GRADE

The MRE has been reported above a lower cut-off of 0.5 g/t Au above a RPEEE pit optimisation shell, and above a lower cut-off of 2.0 g/t Au below the same RPEEE shell, which has included the following parameters and assumptions:

- Mining by open pit excavation
- Ore loss of 6%
- Mining dilution of 12%
- Processing recovery 92.3% for all material types
- Australian gold price of \$2,400/oz
- Gold royalty of 2.5%
- Mining rates are based on the long-term performance of the currently operating Jupiter gold mine.
- Geotechnical inputs are derived from detailed geotechnical investigations completed by geotechnical consultants.

- The reporting cut-off parameters were selected based on known open pit economic cut-off grades.
- The potential to extract mineralisation via underground mining methods has not been considered due to the depth of drilling and mineralisation.

#### MINING AND METALLURGICAL METHODS AND PARAMETERS

- The ore is being processed at the adjacent Jupiter Processing Facility, part of the MMGO. Recoveries achieved to date are 92.3%.
- Dacian has been mining Jupiter via open pit methods since December 2017. It is assumed that the same mining methods will be applicable for extraction of in-situ material included in this MRE update.
- The ore is processed at the proximal Jupiter Processing Facility, part of the MMGO. Recoveries achieved to date are 92.3%.

## Mt Marven

#### GEOLOGY AND GEOLOGICAL INTERPRETATION

The deposit is Archean lode gold style.

The Mt Marven deposit consists of a series of lode structures within basalt flows and felsic rock intrusions, generally striking north to north-west and dipping approximately 60-75°. Mineralisation is associated with basalt hosted shearing and sheared intrusive contacts. Mineralised intervals typically display a combination of chlorite-carbonate to sericite-albite alteration with increased fine disseminated sulphide (predominantly pyrite with lesser chalcopyrite).

Mineralisation within felsic rock intrusions is associated with quartz-carbonate veining with pyrite-chalcopyrite, and disseminated pyrite-chalcopyrite adjacent to the veins as a selvage. Mineralisation and host rocks within the nearby open pit confirm the geometry of the mineralisation.

There are both visual and non-visual mineralization types at Mount Marven. Some mineralized shear zones are clearly visible within pit exposures and in drill chips, distinguished by goethitic to hematitic red defined zones that correlate with grades greater than 0.3g/t Au. Beneath the oxidized profile, higher gold grades are sometimes associated with higher disseminated pyrite and sometimes associated with silica-sericite +/- albite alteration.

Mount Marven is hosted by massive to pillowed basalts, which are variably altered, sheared, oxidised and mineralised. There are a series of lode structures striking north and dipping at 60° – 75° to the east, shallowing in the east. Mineralised shear zones can be hematite altered in the oxide material and sericite/carbonate altered in fresh rock.

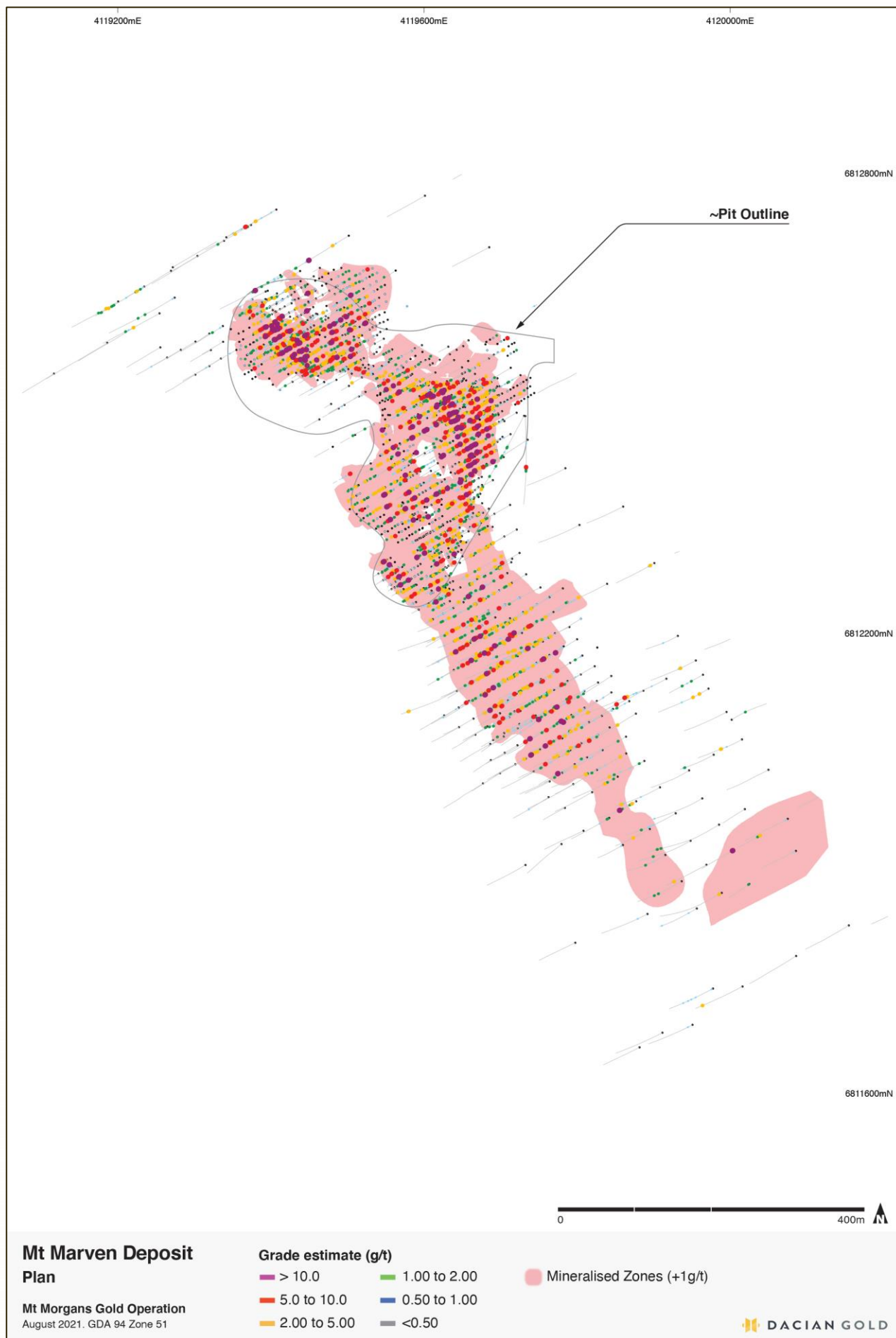
The mineralisation was modelled with a relatively strict gold cut-off of 0.3 g/t Au, which has been confirmed as appropriate for the mining methods and ore markouts.

Porphyry units are also mineralised at times but not visually recognisable as mineralised.

The following objects were modelled that the Competent Person considers adequate to control the MRE.

- Lodes: 67
- Porphyry dykes: 34
- Oxidation/weathering: base of complete oxidation (BOCO), top of fresh (TOFR)

The mineralised lodes at Mount Marven occur within a greater shear corridor and are hosted by both mafic and porphyry units suggesting gold mineralization continued post-intrusion. A WNW structure splits the mineralization between the historic northern and southern pit. Oxidation/weathering: base of complete oxidation (BOCO), top of fresh (TOFR)



**Figure 4: Plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**

## **DRILLING TECHNIQUES**

Drilling that informed the Mineral Resource estimate (MRE) included 1,688 reverse circulation (RC) holes for 75,966 m and 7 surface diamond drill (DD) holes for 1,945.45 m.

Drilling that intersected modelled mineralisation included 1,119 reverse circulation (RC) holes for 44,501 m and 2 diamond drill (DD) holes for 466.35 m.

Rotary Air Blast drilling (RAB) and was used to guide the geological and mineralisation interpretation, but the data were not used in for grade estimation.

For Dacian RC holes, a 5¼" face sampling hammer bit was used except to drill Dacian Mt Marven South holes, where a 5" face sampling hammer was used.

Dacian Diamond drilling was mostly carried out with NQ2 sized equipment, along with minor HQ3 and PQ2, using standard tube. Surface drill core was orientated using a Reflex orientation tool.

Dominion holes (94MCRC and 95MCRC holes) were drilled with RC rigs utilising face-sampling hammers for maximum sample return.

Other than the drill type being RC, nothing is known about the MM historic holes.

## **SAMPLING AND SUB-SAMPLING TECHNIQUES AND SAMPLE ANALYSIS METHOD**

Surface reverse circulation (RC) drilling chips and diamond drilling (DD) core informed the Mt Marven Mineral Resource estimate (MRE) update.

All DD and 80% of RC holes that intersected mineralisation were drilled by Dacian from 2019.

Surface RC holes were angled to intersect the targeted mineralised zones at optimal angles.

In-pit RC holes were variably angled and vertical to target mineralised zones at optimal angles, and to fit around historic workings.

For historical RC drilling, where available the original logs and laboratory results that are in the central SQL Server database are retained by Dacian as either original hard copies or as scanned copies.

94MCRC (107 holes) and 95MCRC holes (29 holes) was undertaken by Dominion Mining Limited using RC rigs from Ausdrill, Robinsons and Drilllex. 1m samples were collected using a riffle splitter. Only samples expected to be anomalous were sent to the onsite lab for analysis.

MM holes (32 holes) were drilled during 1987-1988 by Taurus Resources. No information exists regarding drill contractor or sample methodologies; however, after review of the assay table in the database, all samples were taken at 1m intervals.

The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.

Core was cut in half using an automatic core saw at either 1m intervals or to geological contacts; core samples were collected from the same side of the core where orientations were completed.

Dacian RC samples were collected via on-board cone splitters. Most samples were dry, any wet samples are recorded as wet, this data is then entered into the sample condition field in the drillhole database.

The RC sample was split using the cone splitter to give an approximate 3kg sample. The remainder was collected into a plastic sack as a retention sample. At the grain size of the RC chips, this method of splitting is considered appropriate.

Dominion historical RC samples were collected at the rig using riffle splitters if dry while wet samples were bagged for later splitting. Samples condition was not recorded for a majority of the historic sampling. For historic RC drilling, information on the QAQC programs used is limited but acceptable with original batch reports having been reviewed and retained by Dacian.



The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.

#### ESTIMATION METHODOLOGY

Samples were composited to 1 m intervals (“composites”) based on assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.

High-grade top-cuts ranging from 4.9 – 20g/t Au were applied to the mineralisation domains following statistical analysis completed in Snowden Supervisor™ software.

The top-cuts were kept at around 1% – 2% of the grade distribution for each lode.

To model the spatial continuity of gold grades, variography was conducted in Supervisor 8.12. Statistics were length-weighted.

Composite samples were declustered prior to variography for the statistical domains that contained lodes. A normal-score transform was applied to all data.

In total, there are 62 individual mineralized lodes at Mount Marven. Due to lack of data in some lodes, they were grouped together based on lode orientation, statistics and location. The groups consist of the following:

- Supergene envelope
- NNW-SSE lodes in north-western pit area
- NNW-SSE lodes in southern area
- N-S lodes in southern area
- NW-SE lodes in southern area
- Lode 6 – WNW structure splitting north and south pit
- Lode 25 – large, flat EW lode at northern end

Variograms were modelled for each of the above lode groups – seven in total. The majority of the variograms yielded poor experimental variograms, however, the modelling of short-range and long-range spherical structures was possible.

Two spherical structures were modelled for each lode group.

After variograms were modelled, a back-transform model was exported with Datamine rotations for use in Datamine parameter files. All variograms contained a low nugget when back-transformed, and typically a very high proportion of the variance accounted for in the short-range structure.

Multi-block kriging neighbourhood analysis (KNA) was undertaken using Supervisor™ software to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE), slope of regression (SOR) and negative weights were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids.

KNA found that a 5 x 5 x 5m block size was among the best statistics, and was considered most appropriate considering the drill density. KNA suggested using between 6 and 8 minimum samples and between 16 and 20 maximum samples. The maximum samples allowed per drillhole was set to 3 for all lodes. These parameters were set for the first pass.

The KNA suggested adopting a search ellipse size matching the short-range structure in all cases, followed by the full range. The short range structure was often very short (6m to 28m in the major directions.)

The second pass was the full range of the variogram, from 16.8 m to 57.6 m, and the minimum samples was 10 and maximum was 20. The third pass was 8x to 12x the full range of the variogram, from 60 m to 224 m, and the minimum samples was 4 and maximum was 8.

The major direction was modelled with a ratio of between 1.2x to 2.3x the semi-major direction, and 2.3x 6.8x the minor direction. The latter of 6.8x ratio to the minor is an exception, relating to domain South, which incorporates the elongated lodes drilled to a lower density, and that have almost entirely been classified as Inferred.

Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains. The technique is considered appropriate to allow the geostatistical continuity determined from variography to weight samples during estimation.

Dynamic anisotropy was used only on the first pass to prevent wildly fluctuating large ellipses from weighting samples in high angles to the prevailing orientations of the lodes.

Geological modelling was undertaken in Leapfrog Geo 6.0 software.

Compositing, block modelling and grade estimation were undertaken using Datamine™ RM software.

The estimation technique is appropriate to allow a locally adequate estimate for detailed mine planning and with a globally unbiased estimate per lode.

Density used to estimate tonnages for the MRE update has been determined from 891 core immersion method samples.

Surtech captured quantitative wireline gamma-density data from two holes at Mount Marven in early 2021, entirely within the transitional zone.

A high graphical correlation (compared visually) was shown between the gamma-density and core density determinations.

Density assignments by oxidation type for waste and mineralization, adjusted for porosity are shown below:

Material	Density value (t/m <sup>3</sup> )
Oxide	1.9
Transitional	2.3
Fresh	2.8

Void space has been accounted for in the industry-standard, immersion method core density determination process.

No borehole magnetic resonance data were captured, therefore the data were not porosity or moisture adjusted.

Instead, the data were adjusted for an assumed porosity by using the porosity adjustment by oxidation state for a nearby deposit with a similar weathering profile, Ganymede, which utilised borehole magnetic resonance (BMR) data. The BMR data quantitatively assesses the porosity of the material logged, from which the percentage of porosity was removed to provide an in-situ, dry bulk density.

Porosity values of 10% for oxide, 7.5% for transitional and 5% for fresh were applied to the density.

## CLASSIFICATION

The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:

- Drill density data
- Geological understanding
- Quality of gold assay grades
- Continuity of gold grades
- Economic potential for mining.

Unclassified material:

- Part of lode 74, a flat lying oxide zone, located on the south-eastern extent of the model remained unclassified due to very limited drill density.

Indicated Mineral Resources:

- Statistical consideration has been employed to assess the grade estimate quality in considering large, contiguous and coherent zones of blocks form zones where:
- Large areas are formed that have been grade control drilled, but also extending out to where drill hole spacing reaches 20 m to 20 m max.



- Estimation was chiefly undertaken in search passes of 1 and 2.
- Number of samples was predominantly near the optimum.
- Slope of regression formed large volumes of > 0.4 with cores of 0.6.

The remainder of the mineralisation was classified as Inferred.

#### **CUT-OFF GRADE**

The reporting cut-off parameters were selected based on known open pit economic cut-off grades.

The potential to extract mineralisation via underground mining methods has not been considered due to the depth of drilling and mineralisation.

The MRE has been reported above a lower cut-off of 0.5 g/t Au and within a pit optimisation shell that allows the test of reasonable prospects of eventual economic extraction (RPEEE) for the undepleted MRE, and without the inclusion of dilution and ore loss, as the Competent Person considers these excessive economic modifying factors, whereas the other parameters are based on in-situ material parameters or fixed costs:

- Gold price A\$2,400/oz
- Pit overall slope angles: oxide 44°, transitional, 49° fresh 63°
- Ore loss 0%
- Dilution 0%
- Mining costs (scaled by RL range as per actual rates): 425 m RL: A\$7.06/t – 360 m RL: A\$9.24/t
- Processing recovery 92% (oxide, transitional and fresh)
- Processing costs: oxide: A\$20.50/t; transitional A\$22.50/t; fresh A\$24.50/t
- Refining cost: A\$1.60/oz
- Gold royalty of 2.5%
- Discount rate: 5%

#### **MINING AND METALLURGICAL METHODS AND PARAMETERS**

Dacian began open pit production at Mount Marven in July 2020. It is assumed that the same mining methods will be applicable for extraction of in-situ material included in this MRE update.

The ore is processed at the proximal Jupiter Processing Facility, part of the MMGO. Recoveries achieved to date are 92.3%.

### **Maxwell Bore**

#### **GEOLOGY AND GEOLOGICAL INTERPRETATION**

The deposit is Achaean lode-gold-style, hosted in the Yilgarn Craton, Western Australia.

The gold mineralisation has been deposited in lodes along a BIF-chert ridge, dominantly contained within the BIF-chert units, but also is emplaced along the contacts of the mafic material, forms larger halos around the units, and occasionally obliquely transects the BIF-chert units at low-angles resulting from unmeasured local structural controls.

The BIF-chert units and lodes are dominantly buried beneath an extensive, shallow colluvial cover and laterite to the west, but also outcrop in parts of the central and north

The variably deep weathering/oxidation profile extends 10 m – 50 m to the base of the completely oxidised surface, and ~25 m – 70 m to the top of fresh surface.

Geological logging has been used to assist identification and delineation of lithology, weathering and mineralisation.

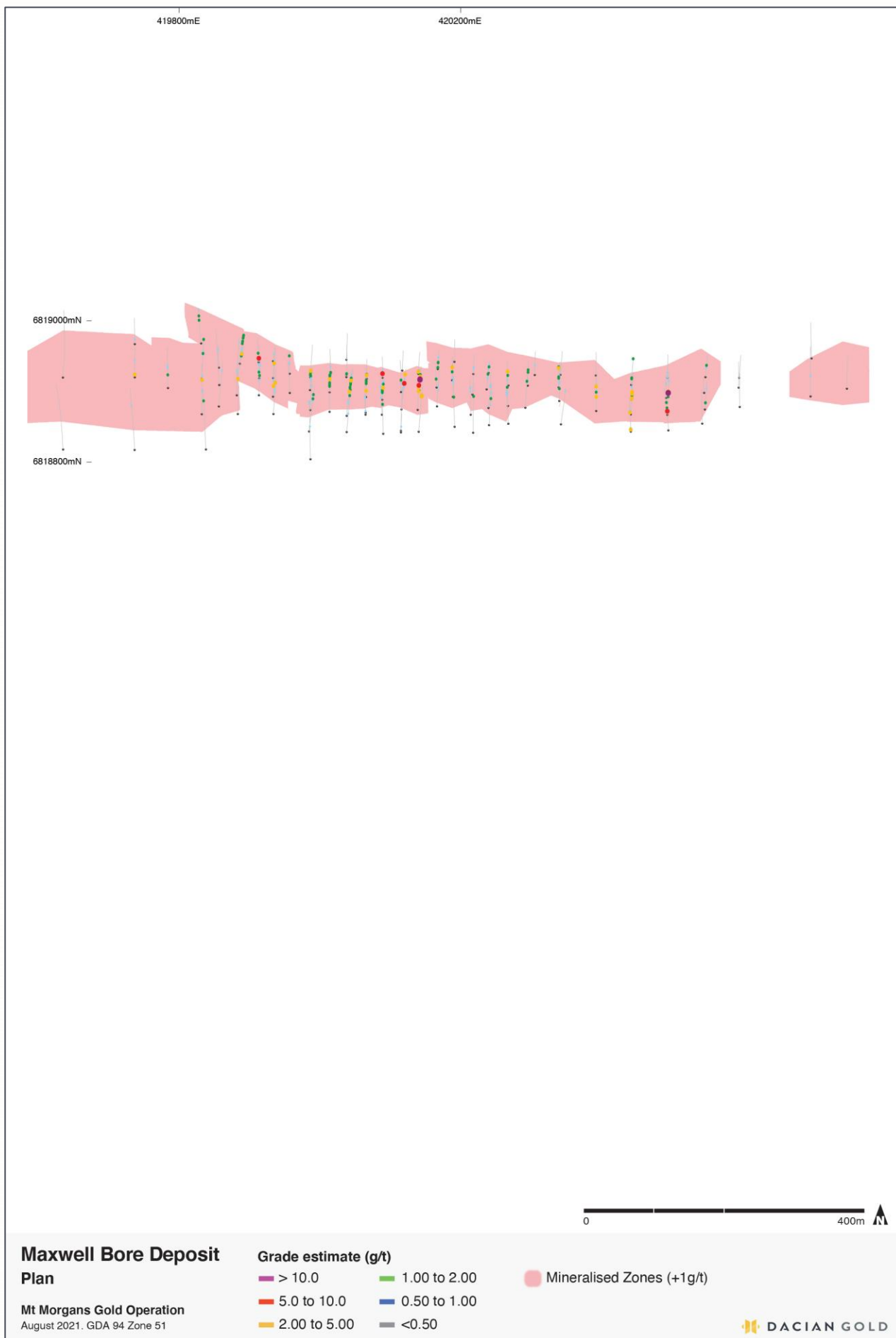
The following mineralisation modelling techniques were incorporated into the modelling, which has formed assumptions regarding the continuity:

- Logging of weathering was used to model base-of-complete-oxidation (BOCO) and top-of-fresh (TOFR) surfaces. Isolated peaks and troughs created by variable logging were ignored for a smoother surface that is assumed to be less likely to be influenced by subjective differences or error in the logging.
- Any internal waste units not assayed across several metres were excluded from mineralisation wireframes to provide coherent geometries.
- All lodes were treated as hard-boundaries for statistics and estimation.
- Porphyry intrusions were modelled predominately in the Ramornie Central area on the same trend of the those modelled at Beresford (Westralia mine corridor).

The deposit has been divided into four domains based on the orientation of the lodes:

- Max\_West
- Max\_NW
- Max\_Central
- Max\_East

Porphyries and meta-sandstone/siltstone and other sedimentary lithologies exist in the stratigraphy, but they are minor or not associated with or proximal to the modelled mineralisation, and so they have not been modelled.



**Figure 5: Plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**

## DRILLING TECHNIQUES

Drilling that informed the modelling area of the MRE included 119 Reverse Circulation (RC) drill holes for 10,170 m, all of which intersected mineralisation and were used to estimate grades, while air core (AC) and rotary air blast (RAB) were used to guide, but not inform, the MRE.

Dacian drilled 97% of the RC holes. The remainder were drilled in 1998 by an unknown company, but Homestake, the company whose drilling dates are closest to the involved in the area drilled RAB and AC in 1999.

For Dacian RC holes, a face sampling hammer bit was used.

Dominion holes were drilled with RC rigs utilising 5¼" to 5 ¾" face-sampling hammer bits for maximum sample return.

## SAMPLING AND SUB-SAMPLING TECHNIQUES AND SAMPLE ANALYSIS METHOD

Surface Reverse Circulation (RC) chips informed both the Mineral Resource estimate (MRE).

RC holes within mineralisation were sampled on 1 m intervals in mineralisation via an on-board cone splitter mounted at the base of the cyclone to achieve a representative split of approximately 3 kg samples.

Dacian samples were submitted to a National Association of Testing Authorities (NATA) certified contract laboratory for drying, crushing and pulverising to produce either a 40 g or 50 g charge for lead collection fire assay and an atomic absorption spectrometry (AAS) finish.

The Dacian RC sample was split using the cone splitter to give an approximate 3kg sample. The remainder of the sample was collected into a plastic sack as a retention sample. At the grain size of the RC chips, this method of splitting is considered appropriate.

Most samples were dry; any wet samples are recorded as wet; this data is then entered into the sample condition field in the drillhole database.

At all times, an attempt was made to keep samples dry. If due to significant groundwater inflow or drilling limitations sample quality became degraded (consecutive intervals of wet sample or poor sample recovery), the RC hole was abandoned.

## ESTIMATION METHODOLOGY

Geological modelling, sample compositing, block modelling and grade estimation were undertaken using Surpac™ software.

Statistical analysis including variography was undertaken in Supervisor™ software.

Samples were composited to 1 m intervals ("composites") based on assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.

Statistical analysis was completed in Snowden Supervisor™ 8.14 software, including modelling of the spatial continuity of gold grades by variography.

Statistics were length-weighted.

Cell de-clustering analysis using cell size combinations of 10 m to 50 m in X, Y and Z directions were undertaken for the Max\_Central domain, as the data were more clustered. A 20 m cube was selected based on the analysis that the declustered mean grade was significantly lower than the naïve mean, while being within the range of other declustered cell sizes and not extremely lower. De-clustering was also analysed for the other domains, but was not applied, as it had immaterial impact on statistics reviewed.

Domains were based on spatial characteristics (location, orientation, and geometry) of lodes.

Visual validation of composite grades was reviewed in Surpac to determine if there were any trends with depth or accumulation on weathering/oxidation boundaries.

Multi-block kriging neighbourhood analysis (KNA) was undertaken to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE), slope of regression

(SOR) and negative weights were determined for a range of block sizes, minimum and maximum samples, search dimensions, and discretisation grids. Statistics were invariable for changes in discretisation.

Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains. The technique is considered appropriate to allow the geostatistical continuity determined from variography to weight samples during estimation and allow a locally adequate estimate for detailed mine planning, while ensuring a globally unbiased estimate per lode.

A three-pass expanding search ellipse strategy was used, honouring the anisotropic ratios from the relevant domain variogram orthogonally, except for the first pass, which employed dynamic anisotropy (DA), and the dynamic orientation of the search ellipse in Surpac causes the major and semimajor directions to be incorrect. DA was employed as local flexures not related to modelled structural offsets (which divided the deposit's modelled objects) were evident.

Search parameters for each pass were as follows:

Pass 1:

- Search ellipse size 44 m, isotropic in the major-semimajor plane, DA
- Minimum samples: 9
- Maximum samples: 22
- Maximum samples per hole: 6
- Discretisation: 3 by 3 by 3

Pass 2:

- Search ellipse size 100% of the full range of the domain variogram (44 m to 118 m)
- Minimum samples: 9
- Maximum samples: 22
- Maximum samples per hole: 6
- Discretisation: 3 by 3 by 3

Pass 3:

- Search ellipse size 300 m
- Minimum samples: 4
- Maximum samples: 10
- Maximum samples per hole: 6
- Discretisation: 3 by 3 by 3

Grades have not been interpolated into the waste, as there is little evidence for a grade halo or mineralisation in other objects.

The wireline gamma-density data logged throughout Mt Morgans by Surtech systems in February 2021 were used to assist the density determination of the MRE, although they were not taken from the Maxwell Bore deposit.

The density for mafic material of differing oxidation states was taken from the density assigned to the Craic deposit, whose style of mineralisation is mafic-hosted. The waste laterite and colluvium was assigned based on the Competent Person's knowledge of similar material throughout Mt Morgans and similar geological settings in the Yilgarn. As the BIF material was frequently logged as chert-rich BIF or chert, the densities applied were lower than those determined by wireline gamma-density and diamond core immersion methods.

The final densities assigned were:

Lithology	Oxidation state	Density value (t/m3)
colluvium	Transported	1.4
laterite	Transported	2.0
BIF-chert	Completely oxidised	1.6
BIF-chert	Transitional	2.2
BIF-chert	Fresh	2.65
mafic	Completely oxidized	1.8
mafic	Transitional	2.3
mafic	Fresh	2.75

## CLASSIFICATION

The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:

- Drill density data
- Geological understanding
- Quality of gold assay grades
- Continuity of gold grades
- Economic potential for mining.
- 

For Indicated Mineral Resources, statistical consideration has been employed to assess the grade estimate quality in considering large, contiguous and coherent zones of blocks form zones where:

- From the 15 total lodes modelled in the deposit, only two lodes each from the Max\_Central and Max\_East domains total that displayed the highest geological confidence were considered.
- Drill hole spacing reached a nominal maximum of 20 m.
- Estimation dominantly was undertaken in search pass 1.
- Number of samples was near the optimum.
- Slope of regression formed large volumes of > 0.4 with cores of 0.6.

Inferred Mineral Resources:

- All other mafic-hosted mineralisation, as the drill hole spacing and pierce was never greater than 80 m within the geological model that is considered robust.

Unclassified material:

- All material outside of the mineralisation model.

## CUT-OFF GRADE

The MRE has been reported above a lower cut-off of 0.5 g/t Au.

A RL was considered for reporting above the MRE at this cut-off; however, as the mineralisation is no more than 140 m depth from surface RPEEE is established for the shallow depths, no RL cut-off was applied.

The reporting cut-off parameters were selected based on known UG economic cut-off grades from Dacian's Westralia UG operation.

## MINING AND METALLURGICAL METHODS AND PARAMETERS

It is assumed that the deposit will be amenable to open pit methods, as has been undertaken for similar deposits in the MMGO project.

The ore is intended to be processed at the Jupiter Processing Facility, part of the Mt Morgans Gold Operation (MMGO). Recoveries achieved to date are 92.3%, which includes ore from the analogous Westralia deposit, which is also part of the MMGO.

## Transvaal and Craic

### GEOLOGY AND GEOLOGICAL INTERPRETATION

The deposit is Archean lode gold style.

Both deposits consist of a series of mineralised structures within greenschist facies altered basalt flows and quartz feldspar porphyry dyke intrusions.

The lodes strike north to NNE, dip steeply east and generally plunge moderately to the north. The porphyry dykes strike NNE to NE, and display a moderate dip to the E or NE, cross-cutting or delineating the mineralised structures into the lodes.

Gold mineralisation is hosted within north-northeast trending shear-hosted lodes. For Transvaal, the anastomosing lode-porphyry bodies are hosted along an extension of the Ramornie Transvaal Shear Zone, whereas the mineralisation of Craic is hosted on a parallel local shear structure east of the Ramornie Transvaal Shear Zone on two dominant mineralised structures.

High-grade accumulations are evident at the contacts within the pre-mineralising porphyry dykes.

The mineralised lodes occur within a greater shear corridor and are hosted by both mafic and porphyry units suggesting gold mineralisation was post-intrusion, but mineralisation preferenced the mafic material.

Mineralised intervals typically display altered and fractured or strained zones in the basalt and an alteration mineral assemblage associated with elevated pyrite-pyrrhotite that is a combination of chlorite-carbonate to sericite-albite alteration. For Transvaal, these alteration zones are distinct, but at Craic they are more subtle and thinner. The alteration zones are generally difficult to model.

Mineralisation is hosted within porphyries across the contacts of the basalt within the planes of the mineralised structures, but the grades rapidly decrease moving into the porphyries, and therefore have not been classified nor reported.

Mineralisation and host rocks within the OP exposures confirm the geometry of the mineralisation.

The oxidation profile for Transvaal is very shallow, with no or sub-metre scale completely oxidized material. The transitional zone extends only 10s of metres.

For Craic, a deeper oxidation profile of 1 m – 5 m completely oxidised and 25 m – 40 m of transitional material.

Grades above 0.5 g/t Au display a high continuity, and therefore this was selected as the mineralisation modelling cut-off.

The mineralised structures are laterally continuous beyond the modelled mineralisation, yet the mineralisation shows sharp cut-offs laterally either where the mafic units are intruded by the porphyries or for other unknown reasons. Therefore, the modelling cut-off has a high influence on the continuity of the grade.

All lodes were treated as hard-boundaries for statistics and estimation.

High-grade accumulations are noted within the porphyries across the contacts of the basalt, and within the planes of the mineralised structures. The samples and volumes within the mineralised structures and in the porphyry volumes have been estimated independently with a hard boundary to the basalt-hosted mineralisation within the same lode. However, the grades rapidly decrease moving into the porphyries where sample density is lower, causing higher-grade clustering within the porphyries near their contacts, so that the grades are likely to have smeared through the thickness of the porphyry volumes without an ability (such as an alteration halo or other geologically confirmed hard boundary) to control the grades from smearing away from the contact into the porphyry volume. Therefore, have not been classified nor reported.

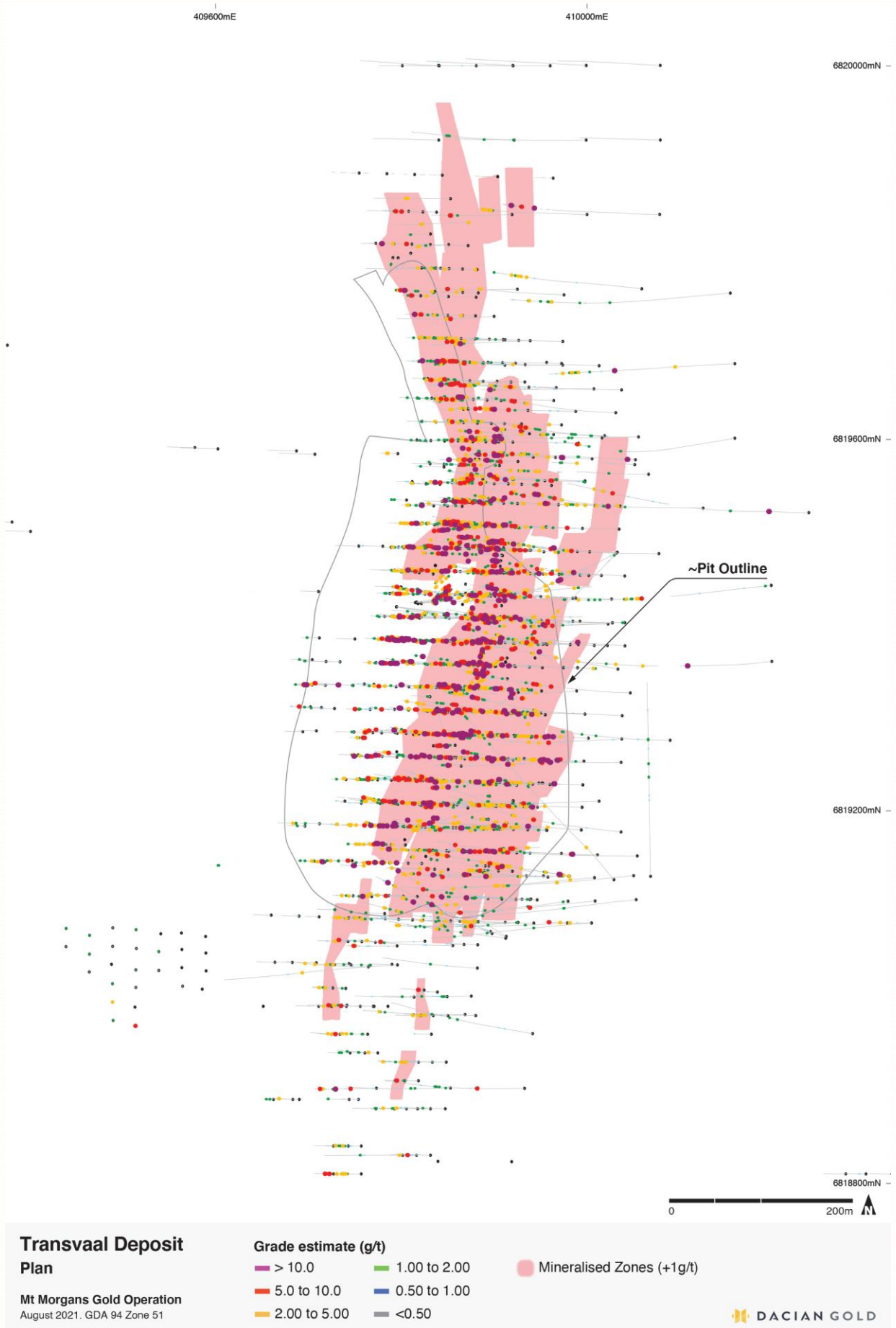
Statistics were reviewed, including grade distributions, contact analysis and variogram continuity, between the oxidation domains, which showed that no boundaries were present, and therefore no hard boundaries by oxidation domain were applied.

Porphyry units are also mineralised at times but not visually recognisable as mineralised. Lodes generally are truncated by the porphyries into discrete lode objects, but where the mineralising structures cross-cut the porphyries, the mineralisation appears to extend sub-metre scale into the porphyries, and therefore the MREs exclude porphyry-hosted mineralisation.

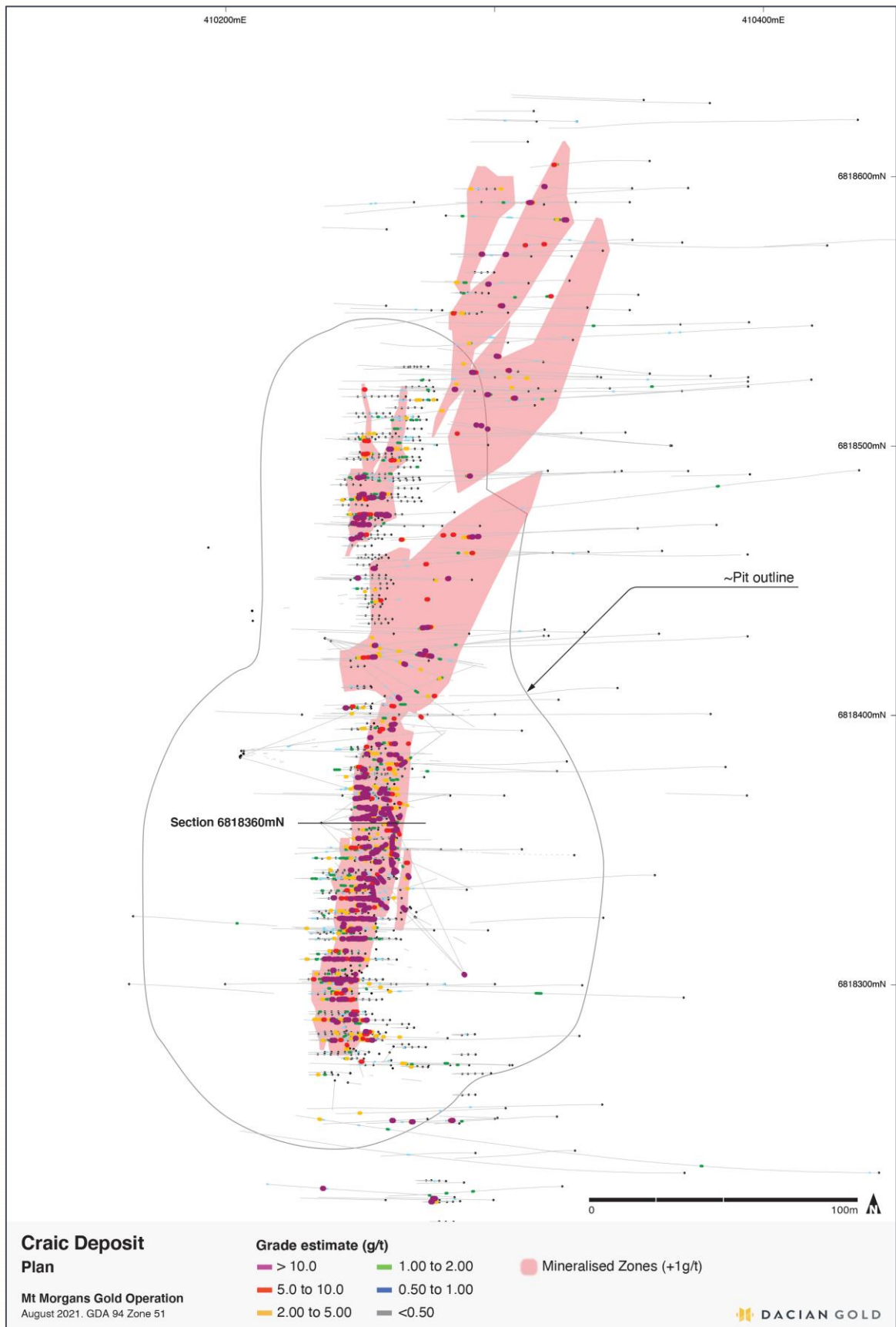
The following objects were modelled that the Competent Person considers adequate to control the MRE.

- Transvaal lodes: 50
- Transvaal porphyry dykes: 22
- Craic lodes: 18
- Craic porphyry dykes: 27
- Transvaal oxidation/weathering: top of fresh (TOFR)
- Craic oxidation/weathering: base of complete oxidation (BOCO), TOFR.





**Figure 6: Transvaal plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**



**Figure 7: Craic plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**

## DRILLING TECHNIQUES

Drilling that informed the Craic MRE included 91 Reverse Circulation (RC) drill holes for 31,344.2 m, 91 diamond (DD) holes for 9,045.17 m, seven RC holes with diamond tails (RCD) for 1,279.2 m and 113 face samples for 427.08 m.

Drilling that informed the Transvaal MRE update included 623 Reverse Circulation (RC) drill holes for 56,640 m, 274 diamond (DD) holes for 18,736.55 m, and 52 RCD holes for 16,851.79 m. Face samples were not included for the Transvaal MRE, as no information was available for them.

Drilling that intersected modelled Transvaal mineralisation and was used to estimate grades for the MRE update, included 1,307 RC drill holes for 17,277.52 m, 654 diamond (DD) holes for 4,983.11 m, and 353 RCD holes for 4,647.29 m.

Drilling that intersected modelled Craic mineralisation and was used to estimate grades for the MRE update, included 498 RC drill holes for 1,707.22 m, 79 diamond (DD) holes for 195.64 m, 6 RCD holes for 23.16 m, and 74 face samples for 147.75 m.

Nearly 100% of holes that intersected Craic mineralisation were drilled since from 1990, 95% since 2000, and 4% by Dacian.

87% of holes that intersected Transvaal mineralisation were drilled since from 1990, 13% since 2000, and 10% by Dacian.

Reverse circulation (RC) drilling and surface diamond drilling informed the Minerals Resource estimate (MRE) for Transvaal and Craic, while face sampling of drives informed the first pass only for Craic.

For Dacian RC holes, a 5¼" to 5¾" face sampling hammer bit was used.

UG DD drilling was mostly sampled whole core with NQ2 sized equipment.

Dacian DD was sampled as half core, mostly HQ3 and PQ3 with minor PQ2.

## SAMPLING AND SUB-SAMPLING TECHNIQUES AND SAMPLE ANALYSIS METHOD

Surface and underground (UG) Diamond (DD) core, surface Reverse Circulation (RC) chips and surface RC chips with DD tail (RCD) core informed both the Transvaal and Craic Mineral Resource estimates (MRE).

Underground drive face samples taken by chipping channels cut into drive faces were also used to inform the Craic MRE within the first pass of the grade estimate.

Quantitative wireline gamma-density data was captured by geophysical sondes in Dacian RC and DD holes for informing the density estimates.

Dacian surface diamond core was sampled as half core at 1m intervals or to geological contacts. To ensure representative sampling, half core samples were always taken from the same side of the core.

Dacian RC holes were sampled over the entire length of hole. Dacian RC drilling was sampled at 1m intervals via an on-board cone splitter.

Face samples were sampled across the full length of the drive face, perpendicular to the lode orientations, and to geological contacts.

Geophysical sondes used in the wireline data capture were calibrated against known density standards and repeat logging of a calibration hole at Mt Morgans.

The wireline gamma-density data were compared to the core density for transitional material, which showed that acceptable correlations existed for inclusion of either dataset in the MRE. RC holes within mineralisation were dominantly sampled on 1 m intervals in mineralisation via either a riffle splitter or on-board cone splitter mounted at the base of the cyclone to achieve a representative split of approximately 3 kg samples.

Diamond core was sampled as half core if drilled from surface or full core if UG on 1 m intervals or to geological contacts, sampled into lengths in sample bags to achieve approximately 3 kg.

Dacian surface RC holes were sampled over the entire length of hole.

Surface samples were submitted to NATA certified contract laboratory for crushing and pulverising to produce either a 40 g or 50 g charge for fire assay with an atomic absorption spectrometry (AAS) finish.

Face samples were collected by Range River on underground drives on 4.5 m – 5.5 m advances across the full width of the face and perpendicular to lode orientations on approximately 1 m lengths or to geological contacts. The samples were collected by cutting channels into the drive face and chipping pieces of the channel into sample bags.

Face samples and UG DD core was submitted to an on-site laboratory for crushing and pulverizing. The sample charge size for fire assay is unknown, but is believed to have been either from 30 g to 50 g, with an atomic absorption spectrometry (AAS) finish.

## **ESTIMATION METHODOLOGY**

Samples were composited to 1 m intervals (“composites”) based on assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.

Statistical analysis was completed in Snowden Supervisor™ 8.14 software, including modelling of the spatial continuity of gold grades by variography. Statistics were length-weighted.

Multi-block kriging neighbourhood analysis (KNA) was undertaken using Supervisor™ software to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE), slope of regression (SOR) and negative weights were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids.

Geological modelling, sample compositing, block modelling and grade estimation were undertaken using Surpac™ software.

Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains. The technique is considered appropriate to allow the geostatistical continuity determined from variography to weight samples during estimation.

The estimation technique is appropriate to allow a locally adequate estimate for detailed mine planning and with a globally unbiased estimate per lode.

### **Transvaal:**

As only 157 Transvaal composites out of 2,510 sat above the top of fresh rock, analysis for the oxidation profile was meaningless. The lodes show strong continuity regardless of the weathering, with no supergene dispersion halo evident. Therefore, the lodes were not split by the oxidation profile.

Multi-block KNA statistics were reviewed for the mineralised mafic domains, using a maximum of 3 samples per drillhole:

Combinations of 5 m, 10 m and 20 m block sizes in X, Y and Z directions were reviewed.

5x by 10y by 5z block size gave among the best statistics and was considered more appropriate for the drillhole density.

A search ellipse size matching the full range structure.

Transvaal experimental semivariograms did not provide coherent anisotropic directions, so the models were coerced into the plane of mineralisation. This ensured that the anisotropic directions made geological sense by forcing the major direction down-plunge with the mineralisation, the semi-major was orthogonal within the plane of mineralisation, and the minor was across strike.

Two spherical structures were modelled for each lode group.

After variograms were modelled, a back-transform model was exported with Datamine rotations for use in Datamine parameter files. All variograms contained a low nugget when back-transformed, and typically a very high proportion of the variance accounted for in the short-range structure.

A hard-boundary for composites and estimation across the oxidation type boundaries was not applied for the following reasons:

Sufficient samples for contact analysis were only available for lode object 4, which included 56 and 128 transitional and fresh samples respectively.

Visual review of the locations of the oxide and transitional samples showed that all oxide most transitional samples within mineralisation have been depleted by the pit surface.

Minor lodes are almost entirely within the transitional or fresh oxidation type.

Minor lodes contain insufficient samples for further splitting by a hard-boundary.

The OK estimate was undertaken in three passes based on KNA:

- A search ellipse size 75% of the full range structure, expanding out to 150% and 250% on passes two and 3.
- Minimum samples of 8 or 9 gave statistics that were at the lower end of acceptable prior to a significant decrease in the quality of statistics, relaxed to two samples in the third pass to allow all blocks to be estimated.
- Between 22 and 24 maximum samples inclusive gave the best statistics before diminishing returns were noted, providing little benefit to the estimate and increasing smoothing and conditional bias; the maximum samples was reduced to 10 on the third pass to ensure previously unestimated fringe blocks would not be informed by samples at extreme distances from the estimated blocks.
- Statistics were invariable for changes in discretisation.

### **Craic**

Face samples, which exist in lodes 1, 12 and 13, were excluded from statistical analysis to prevent their high-grade, selective and clustered sampling from biasing the statistics.

Craic composite samples were declustered prior to variography for the major lodes of the statistical domains that contained lodes. A normal-score transform was applied to all data.

Statistics were invariable for changes in discretisation.

The second pass was the full range of the variogram, from 16.8 m to 57.6 m, and the minimum samples was 10 and maximum was 20. The third pass was 8x to 12x the full range of the variogram, from 60 m to 224 m, and the minimum samples was 4 and maximum was 8.

The major direction was modelled with a ratio of between 1.2x to 2.3x the semi-major direction, and 2.3x 6.8x the minor direction. The latter of 6.8x ratio to the minor is an exception, relating to domain South, which incorporates the elongated lodes drilled to a lower density, and that have almost entirely been classified as Inferred.

Dynamic anisotropy was used only on the first pass to prevent wildly fluctuating large ellipses from weighting samples in high angles to the prevailing orientations of the lodes.

The OK estimate was undertaken in four passes based on KNA:

- The first pass was conducted for lodes 1, 12 and 13 using face samples, using a search ellipse of 14 m, which was approximately 2 x the short range spherical structure of the variogram, as below this estimated too few blocks and above this the face samples had too large an influence.
- A search ellipse size of 20 m was used for the second pass of all lodes, expanding out to 150% for the third pass, after which the fourth pass at 100 m was not required, as all blocks had been estimated in prior passes.
- A minimum of 6 gave statistics that were at the lower end of acceptable prior to a significant decrease in the quality of statistics, relaxed to four samples in the third pass to allow all blocks to be estimated.
- A maximum of 14 samples inclusive gave the best statistics before diminishing returns were noted, providing little benefit to the estimate and increasing smoothing and conditional bias; the maximum samples was reduced to 10 on the third pass to ensure previously unestimated fringe blocks would not be informed by samples at extreme distances from the estimated blocks.

Immersion-method density was determined on diamond core. Quantitative gamma-density measurements were captured in February 2021 by Surtech.

#### **Transvaal:**

Core immersion/Archimedes method data:

- 1,601 half NQ2 core samples were available.
- Samples only taken in fresh rock with no other weathering profile represented.
- Composited to 1 meter across mafics and porphyries then averaged to give density for comparison with the wireline data.

Density values assigned in the previous MRE, tabulated below, were used to compare and validate the gamma-density values:

Oxidation	Porphyry	Mineralisation & Mafic waste
Oxide	N/A	N/A
Trans	N/A	N/A
Fresh	2.72	2.87

The updated density estimate was based on the analysis of gamma-density values filtered to be within 20% of the nominal hole diameter, determined by the density caliper arm. The data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging.

The following observations were made:

- For fresh material, the density was invariable for changes in depth, visually averaged to be 2.9 t/m<sup>3</sup>, which was assigned to the fresh mineralisation and waste.
- A vertical alignment of density for fresh porphyry material, with a visual average of 2.7 t/m<sup>3</sup>.
- There was no influence of RC or DD hole type on the densities.
- A gradational, inverse relationship between density and depth (as the depth decreases, the density increases) for oxide and transitional material. There is no relationship between density and lithology. As the weathering profile is so shallow, which is confirmed by the densities, an estimated visual average was assigned for oxide and transitional densities.
- The gamma-densities for fresh agree with the previous assignment calculated from DD core.

The final densities were applied based on the above.

Oxidation	Porphyry	Mineralisation & Mafic waste
Oxide	N/A	N/A
Trans	2.3	2.6
Fresh	2.7	2.9

#### **Craic:**

Wireline gamma-density data were captured by Surtech on six holes for 886.2 m

The density values were adjusted by borehole magnetic resonance (BMR) imaging, giving a quantitative, porosity-adjusted value (dry-bulk density).

Compared to the oxidation logging and the oxidation model, the gamma-density data show a gradational increase with depth within the shallow oxidation profile to the TOFR, after which the data are stable in a reasonably tight range.

Core immersion/Archimedes method data were captured by Range River on 21 holes surface and underground diamond for 644.02 m

There is no information on the core immersion-method density samples, and therefore the data were not used.



The final density values assigned to the Craic MRE are shown below.

Oxidation type	Porphyry	Mineralisation & Mafic waste
Oxide	1.7	1.7
Transitional	2.3	2.6
Fresh	2.7	2.9

## CLASSIFICATION

The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:

- Drill density data
- Geological understanding
- Quality of gold assay grades
- Continuity of gold grades
- Economic potential for mining.

Indicated Mineral Resources:

- Statistical consideration has been employed to assess the grade estimate quality in considering large, contiguous and coherent zones of blocks form zones where:
- Drill hole spacing reaches a nominal maximum of 25 m.
- Estimation was undertaken in search passes of 1 and 2.
- Number of samples was near the optimum.
- Slope of regression formed large volumes of > 0.4 with cores of 0.6.

Unclassified material:

- Porphyries.
- Single intercept and other poorly informed lodes.
- Remnant material that AW determined failed the RPEEE test from UG depletion.

Inferred Mineral Resources:

- All other mafic-hosted mineralisation.

## CUT-OFF GRADE

- The MRE has been reported above a lower cut-off of 2.0 g/t Au.
- The reporting cut-off parameters were selected based on known UG economic cut-off grades from Dacian's Westralia UG operation.
- Pit optimisations using parameters that the Competent Person deemed appropriate tests for reasonable prospects for eventual economic extraction (RPEEE) were reviewed, which showed that insufficient material was included above the pit to warrant reporting at lower cut-off grades for Mineral Resources in OP mining scenarios.

## MINING AND METALLURGICAL METHODS AND PARAMETERS

Previous operators mined both deposits using the methods currently in use by Dacian. It is assumed that the same mining methods will be applicable for extraction of in-situ material included in this MRE update.

The ore is intended to be processed at the Jupiter Processing Facility, part of the Mt Morgans Gold Operation (MMGO). Recoveries achieved to date are 92.3%.

## Ramornie

### GEOLOGY AND GEOLOGICAL INTERPRETATION

The mineralisation has been formed along three parallel structures to or within the local Ramornie – Transvaal Shear that cross-cuts the Westralia stratigraphy in greenschist facies altered basalt flows.

Gold mineralisation is hosted within north-northeast trending shear-hosted lodes.

The style of mineralisation is less well understood than other deposits, such as the proximal Transvaal and Craic deposits, but as the former lies on the same local Ramornie – Transvaal Shear, the mineralisation style is expected to be equivalent.

Mineralisation and host rocks within the OP exposures confirm the geometry of the mineralisation.

A relatively shallow oxidation profile exists of 5 m – 10 m completely oxidised and ~25 m of transitional material.

The deposit has been divided into three zones based on the three structural corridors hosting the modelled lodes, all of which strike north relative to Grid North (NE in MTM2017); this division forms the “Ramornie Complex” of:

- Ramornie South – a structure that hosts sub-vertical lodes that dip steeply to the NW and SE (MTM2017 grid) which were mined from the Ramornie and Ramornie North pits, and, at the SW end, a discrete mineralised area that has developed four lodes that dip and plunge moderately to the NE across the structure.
- Ramornie Central – a structure that hosts sub-vertical lodes that dip steeply to the SE (MTM2017 grid)
- Ramornie – a structure that hosts sub-vertical lodes that dip steeply to the SE (MTM2017 grid), and which were mined in the Sarah pit.

The porphyry dykes strike NNE to NE, and display a moderate dip to the E or NE, cross-cutting or delineating the mineralised structures into the lodes.

Geological logging has been used to assist identification and delineation of lithology, weathering and mineralisation.

The following mineralisation modelling techniques were incorporated into the modelling, which has formed assumptions regarding the continuity:

- Logging of weathering was used to model base-of-complete-oxidation (BOCO) and top-of-fresh (TOFR) surfaces. Isolated peaks and troughs created by variable logging were ignored for a smoother surface that is assumed to be less likely to be influenced by subjective differences or error in the logging.
- Any internal waste units not assayed across several metres were excluded from mineralisation wireframes to provide coherent geometries.
- All lodes were modelled above a moderately strict cut-off of 0.5g/t, except for the retention of continuity, where lower grades were allowed.
- Boundary strings were utilised to control the strike and down dip extents beyond the last known drill hole data.
- Amorphous blob-shapes were prevented to avoid estimates ‘seeing’ composites across holes and around fluid boundaries.
- All lodes were treated as hard-boundaries for statistics and estimation.

Porphyry intrusions were modelled predominately in the Ramornie Central area on the same trend of the those modelled at Beresford (Westralia mine corridor).

All lodes were treated as hard-boundaries for statistics and estimation.

High-grade accumulations are noted within the porphyries across the contacts of the basalt, and within the planes of the mineralised structures. The samples and volumes within the mineralised structures and in the porphyry volumes have been estimated independently with a hard boundary to the basalt-hosted mineralisation within the same lode. However, the grades rapidly decrease moving into the porphyries



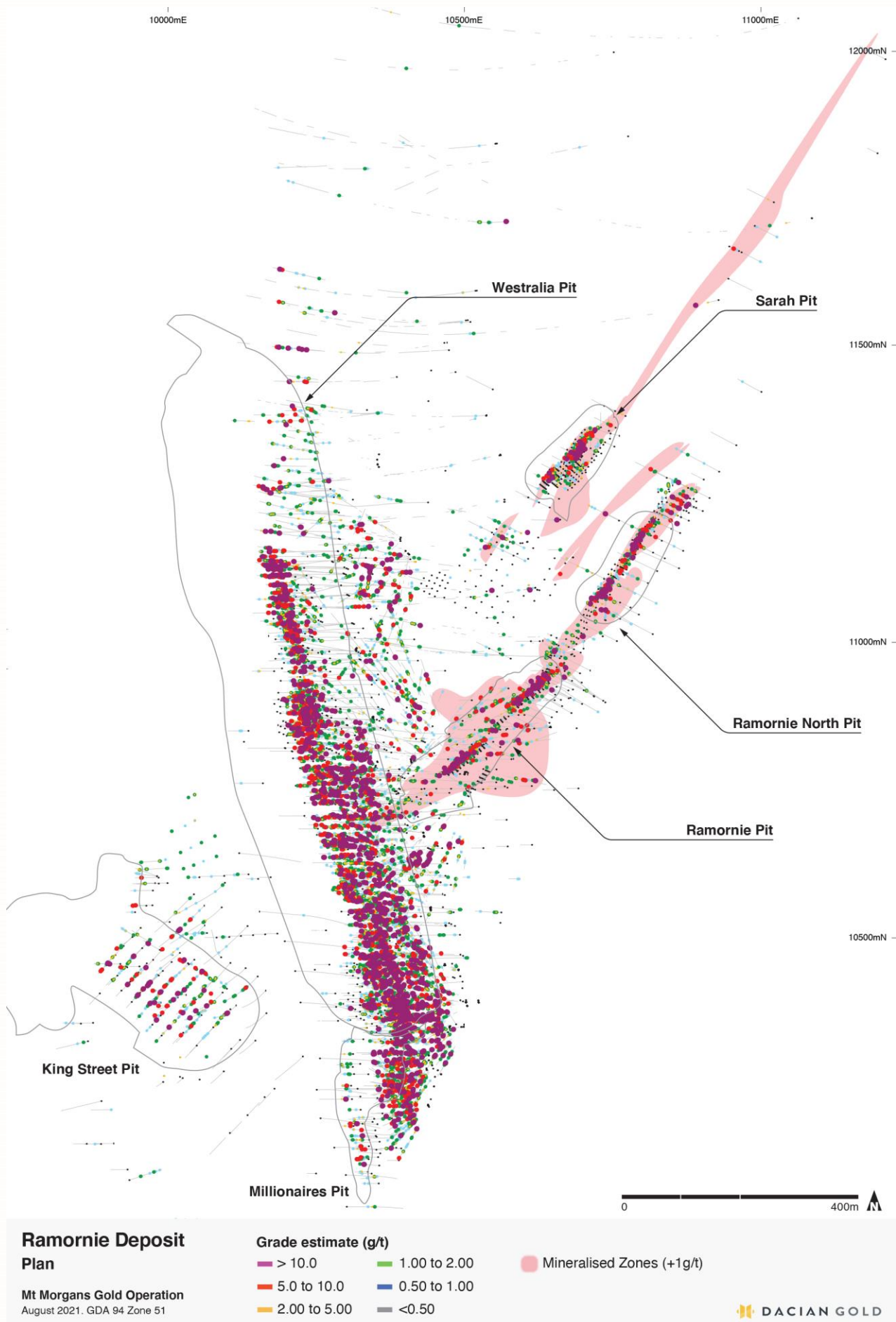
where sample density is lower, causing higher-grade clustering within the porphyries near their contacts, so that the grades are likely to have smeared through the thickness of the porphyry volumes without an ability (such as an alteration halo or other geologically confirmed hard boundary) to control the grades from smearing away from the contact into the porphyry volume. Therefore, have not been classified nor reported,

Statistics were reviewed, including grade distributions, contact analysis and variogram continuity, between the oxidation domains, which showed that no boundaries were present, and therefore no hard boundaries by oxidation domain were applied.

Porphyry units are also mineralised at times but not visually recognisable as mineralised. Lodes generally are truncated by the porphyries into discrete lode objects, but where the mineralising structures cross-cut the porphyries, the mineralisation appears to extend sub-metre scale into the porphyries, and therefore the MREs exclude porphyry-hosted mineralisation.

The following objects were modelled that the Competent Person considers adequate to control the MRE.

- Lodes: 21
- Porphyry dykes: 32
- Oxidation/weathering: base of complete oxidation (BOCO), top of fresh (TOFR)



**Figure 8: Ramornie plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**

## DRILLING TECHNIQUES

Drilling that informed the modelling area of the MRE included 1,258 Reverse Circulation (RC) drill holes for 41,467 m, 380 diamond (DD) holes for 94,366.04 m, and 18 RC holes with diamond tails (RCD) for 11,374.97 m. However, many of these holes were targeted at the Westralia stratigraphy from which the Ramornie structure (host of the modelled mineralisation) intersects in the south.

Drilling that intersected modelled mineralisation and was used to estimate grades for the MRE update included 194 RC drill holes for 704 m, 81 diamond (DD) holes for 303.202 m, and 5 RCD holes for 18 m.

Of the 63% of holes that intersected mineralisation drilled since from 2000, 33% were drilled by Dacian. The remainder were drilled from 1988.

For Dacian RC holes, a 5¼" to 5¾" face sampling hammer bit was used.

UG DD drilling was mostly sampled whole core with NQ2 sized equipment.

Dacian DD was sampled as half core, mostly HQ3 and PQ3 with minor PQ2.

Dominion holes were drilled with RC rigs utilising face-sampling hammers for maximum sample return.

## SAMPLING AND SUB-SAMPLING TECHNIQUES AND SAMPLE ANALYSIS METHOD

RC holes within mineralisation were dominantly sampled on 1 m intervals in mineralisation via either a riffle splitter (historic samples) or on-board cone splitter (Dacian) mounted at the base of the cyclone to achieve a representative split of approximately 3 kg samples.

Diamond core was sampled as half core if drilled from surface or full core if UG on 1 m intervals or to geological contacts, sampled into lengths in sample bags to achieve approximately 3 kg. To ensure representative sampling, half core samples were always taken from the same side of the core.

Dacian surface RC holes were sampled over the entire length of hole.

Surface samples were submitted to NATA certified contract laboratory for drying, crushing and pulverising to produce either a 40 g or 50 g charge for fire assay with an atomic absorption spectrometry (AAS) finish.

The wireline gamma-density data logged throughout Mt Morgans by Surtech systems in February 2021 were used to assist the density determination of the MRE, although they were not taken from the Ramornie deposit.

As the Ramornie mineralisation is proximal to Transvaal and Craic, the lodes lie on extensions from Westralia through to Transvaal, and the geology and mineralisation types are equivalent to Transvaal, the densities applied were selected from Craic and Transvaal data and analysis.

## ESTIMATION METHODOLOGY

Samples were composited to 1 m intervals ("composites") based on assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.

Statistical analysis was completed in Snowden Supervisor™ 8.14 software, including modelling of the spatial continuity of gold grades by variography.

Statistics were length-weighted.

Cell de-clustering analysis using cell size combinations of 5m to 20 m in X, Y and Z directions was undertaken for 10 largest lodes by volume.

Domains were based on spatial characteristics (location, orientation, and geometry) of lodes.

Visual validation of composite grades was reviewed in Surpac to determine if there were any trends with depth or accumulation on weathering/oxidation boundaries.

A final cell de-cluster size of 15m X, 15m Y and 10m Z was used for the estimate.

Composites were split by weathering domains and hole type to review populations requiring separate treatment in the estimate.

A total of 10 composites (out of 1,036) were flagged as mineralisation within porphyry solid volumes used for the estimation. Given the low number and the spatial variation of these composites, the impact on the estimation is considered immaterial.

Insufficient statistics existed above the oxide and transitional surfaces within the lodes. The lodes show continuity regardless of the weathering, with no supergene dispersion halo evident. Therefore, the lodes were not split by the oxidation profile.

Multi-block kriging neighbourhood analysis (KNA) was undertaken using Supervisor™ software to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE), slope of regression (SOR) and negative weights were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids. Statistics were invariable for changes in discretisation.

Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains. The technique is considered appropriate to allow the geostatistical continuity determined from variography to weight samples during estimation.

Geological modelling, sample compositing, block modelling and grade estimation were undertaken using Leapfrog™ software.

The estimation technique is appropriate to allow a locally adequate estimate for detailed mine planning and with a globally unbiased estimate per lode.

A three-pass expanding search ellipse strategy was used, honouring the anisotropic ratios orthogonally. Search parameters for each pass were as follows:

- Pass 1 = 25m
- Pass 2 = 50m
- Pass 3 = 100m

Grades have not been interpolated into the waste, as there is short range continuity of the lodes at Ramornie and little evidence for a grade halo. There were examples of lodes crossing into porphyries however, the mineralisation has been estimated and depleted within these areas.

In each pass, the search ellipse anisotropic ratios and orientations honoured the variogram model.

All Lodes:

1<sup>st</sup> Pass:

- Max samples 16
- Min samples 6
- Max samples per drillhole 6
- Face samples – N/A
- No octants
- Grade Limiting of from 8g/t to 25m

2<sup>nd</sup> pass:

- Max samples 10
- Min samples 2
- Max samples per drillhole 6
- Face samples – N/A
- No octants.
- Grade Limiting from 8g/t to 25m

3<sup>rd</sup> pass:

- Max samples 10
- Min samples 2
- Max samples per drillhole 6
- Face samples – N/A

- No octants.
- Grade Limiting above 8g/t to 25m

Specific gravity (immersion method) determinations number 1,391 from surface drilling and 402 from UG drilling. These were plotted by depth to determine if any relationship exists, notwithstanding the issue that UG depths are not related to the depth from surface. However, the analysis shows that a high proportion of the data fall within a range of  $\sim 2.65 \text{ t/m}^3 - 2.9 \text{ t/m}^3$ .

This data was used to confirm that the gamma density data from the closest and geologically related deposit, Craic, was suitable from which to apply densities. The densities applied to the Ramornie are listed below by lithological and oxidation types.

Oxidation	Porphyry	Mineralisation & Mafic waste
Oxide	1.6 (none)	1.7
Trans	2.3	2.6
Fresh	2.7	2.9

## CLASSIFICATION

The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:

- Drill density data
- Geological understanding
- Quality of gold assay grades
- Continuity of gold grades
- Economic potential for mining.

Unclassified material:

- Mined volumes including mineralisation were set to 0 and insitu set to 1.
- No exploration potential mineralisation was classified, as the drilling density for modelled mineralisation was insufficient to support an Inferred classification.
- Mined areas, chiefly the historical pits and UG workings, were set to AIR min code for depletion purposes.

For Inferred Mineral Resources, the following statistical considerations for the quality of the grade estimate were used to classify large, contiguous, and coherent zones of blocks:

- Drill hole spacing reaches 20 m to 20 m.
- Estimation was undertaken in search passes of 1 and 2.
- Number of samples was used was near the optimum.

## CUT-OFF GRADE

The MRE has been reported above a lower cut-off of 0.5 g/t Au where above the 290 m RL or above a lower cut-off of 2.0 g/t Au where below the 290 m RL.

The RL split for the changes to the cut-off grade were selected by the Competent Person, who considered that the higher-grades were required approximately 150 m from the topographic surface, while above this, the tenor of the mineralisation did not appear to support a deeper RL split.

The reporting cut-off parameters were selected based on known UG economic cut-off grades from Dacian's OP and UG operations.

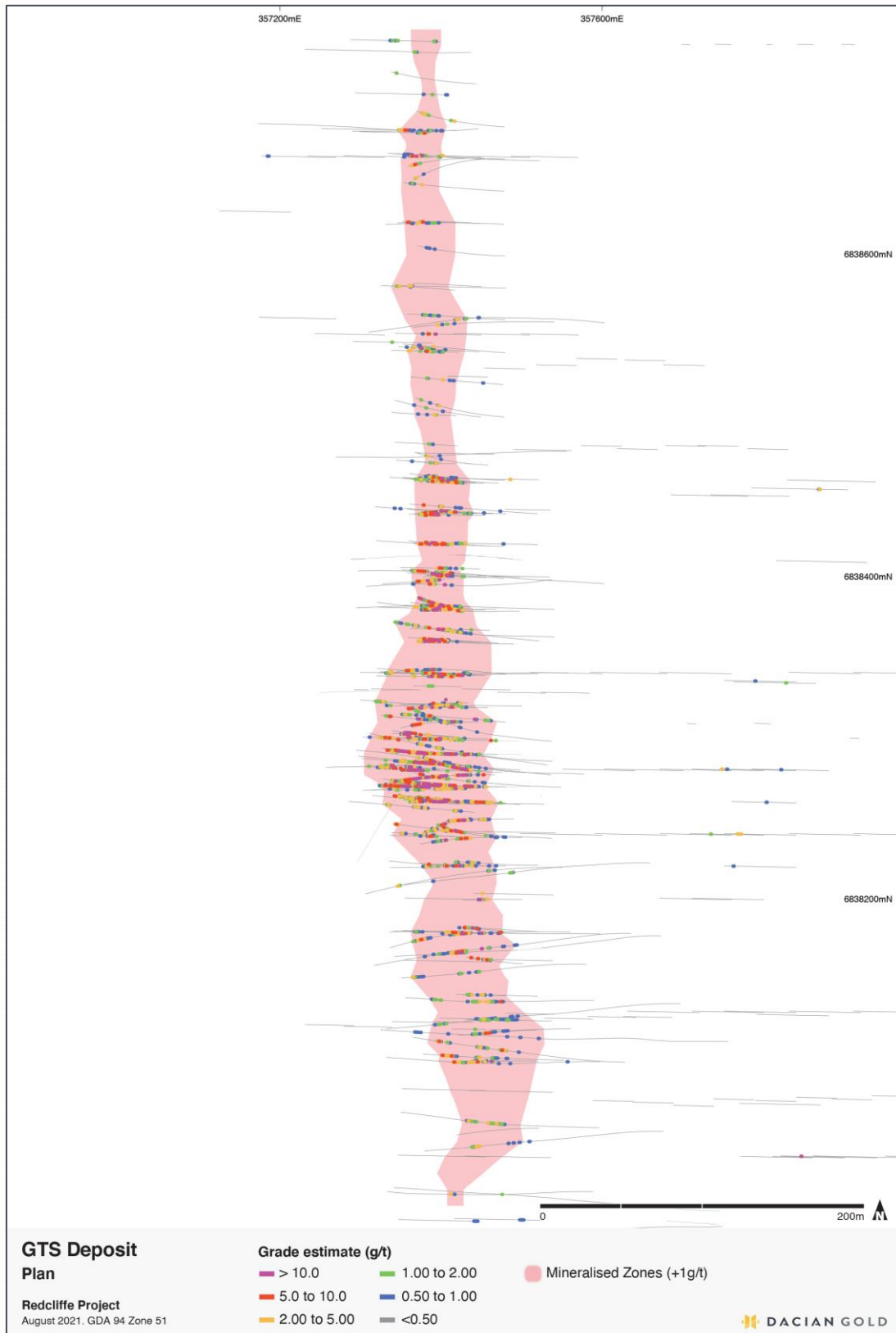
## MINING AND METALLURGICAL METHODS AND PARAMETERS

Previous operators mined both deposits using the methods currently in use by Dacian. It is assumed that the same mining methods will be applicable for extraction of in-situ material included in this MRE update.

The ore is intended to be processed at the Jupiter Processing Facility, part of the Mt Morgans Gold Operation (MMGO). Recoveries achieved to date are 92.3%.

## Redcliffe Project

(Includes the deposits of Hub, Kelly, Mesa\West Lode, Redcliffe, Bindy and Nambi).

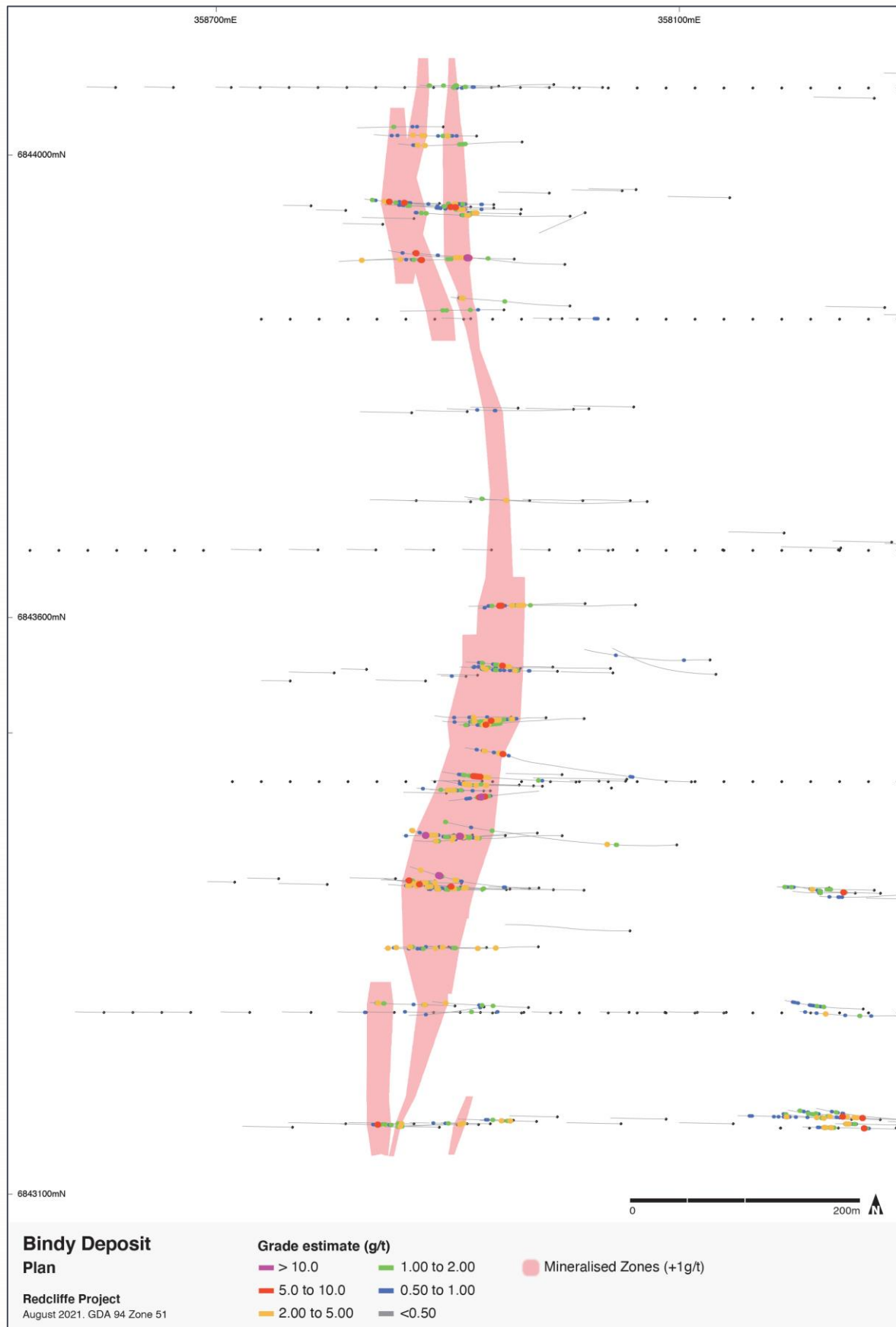


**Figure 9: GTS plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**

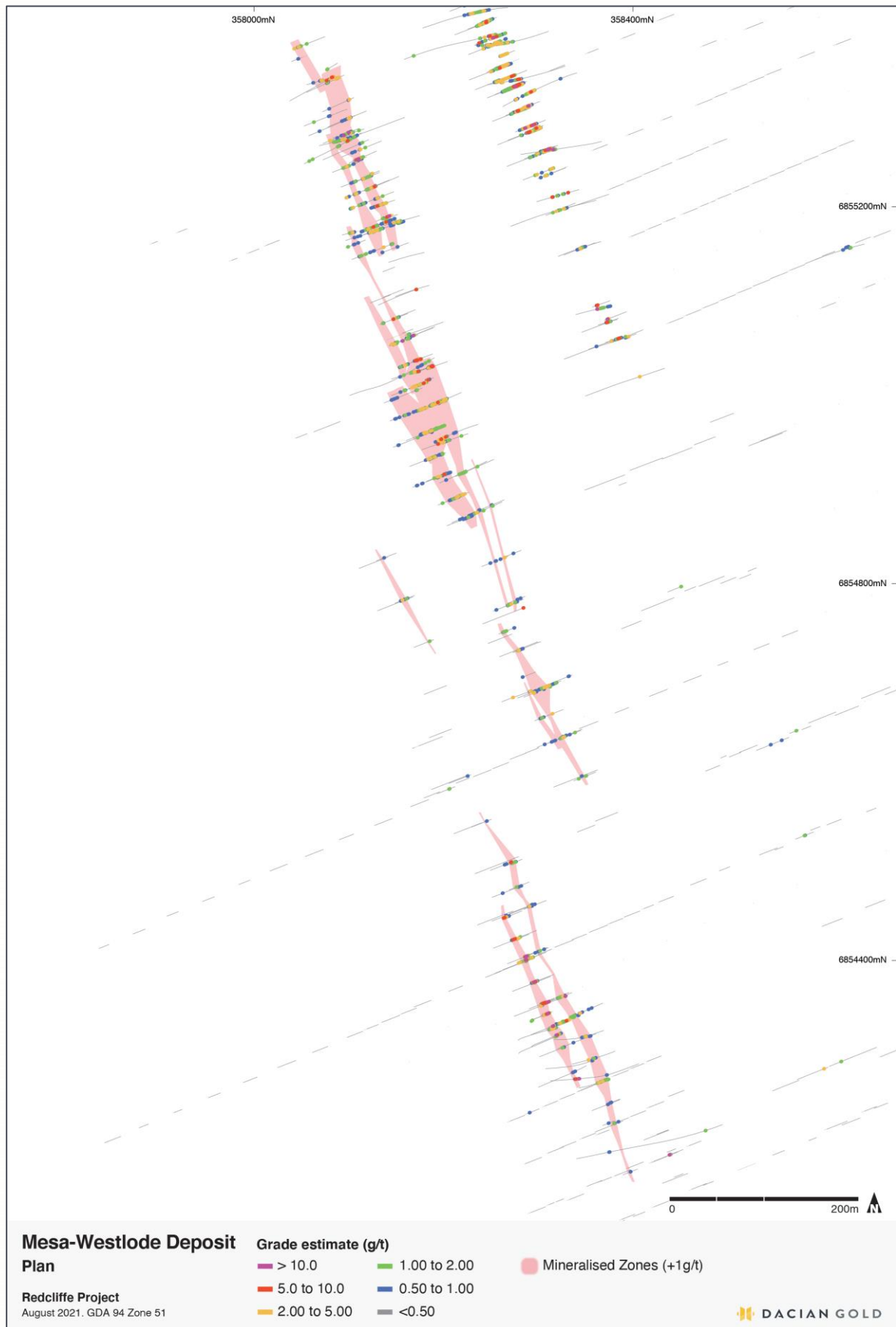


**Figure 10: Kelly plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**





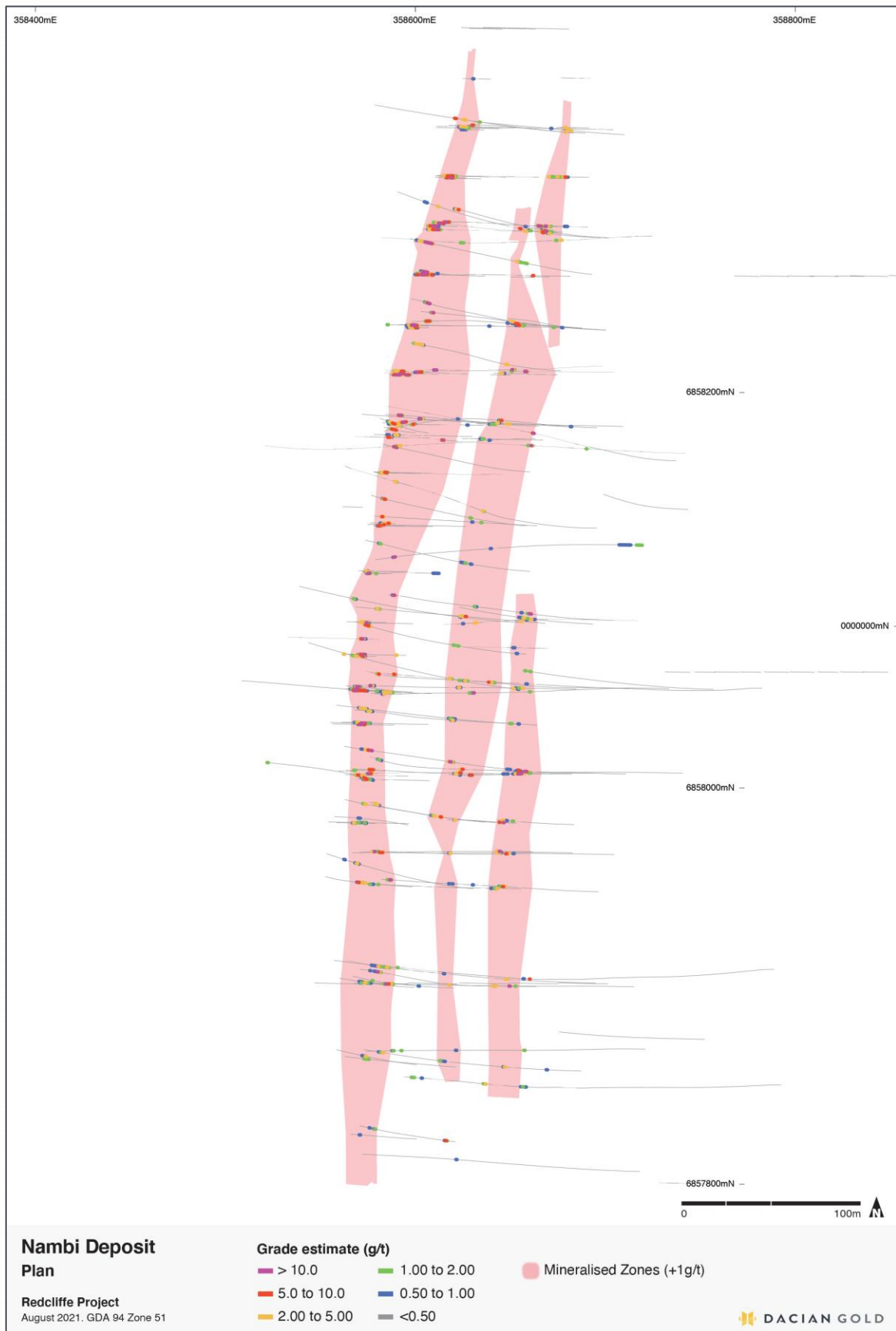
**Figure 11: Bindy plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**



**Figure 12: Mesa–Westlode plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**



**Figure 13: Redcliffe Deposit plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**



**Figure 14: Nambi plan showing the mineralisation wireframes used to constrain the Mineral Resources, resource drillholes by gold grades, and the June 2021 end of month pit surfaces.**

## GEOLOGY AND GEOLOGICAL INTERPRETATION

Mineralisation at the Redcliffe Gold Project is hosted largely within Archaean-aged mafic schist and volcano-sediment package (including chert, black shale, graphitic in part) and intermediate-mafic rocks. A mylonitic fabric is observable in the lithologies. Gold mineralisation generally occurs in northerly striking, sub-vertical to steep dipping zones associated with silica-sulphide-mica alteration and veining. The exception to this is Kelly, where the mineralisation dips approximately 45° to the east and West Lode, which dips at approximately 60° to the west.

At Hub, the majority of the mineralisation is hosted in a narrow (~ 4 m wide) vertical to steep west dipping lode. Several minor subsidiary hanging and footwall lodes are present. The main lode has been cut by late dolerite and lamprophyre dykes which offset and disrupt the mineralisation in places. The depth of complete oxidation varies from between 50 and 100 m below surface which is underlain by a transitional horizon typically 25 m thick to the top of fresh horizon. A thin laterite cap covers the deposit.

The mineralisation at Kelly is hosted in 4-5 shallow east dipping lodes which can be up to 20 m true thickness. There are through broad groups of domains along strike that are separated by zones of no mineralisation or areas of poor drill coverage and hence the mineralisation interpretation has not been extended through these zones. The depth to the base of complete oxidation varies from around 50 – 80 m which continues into 30 – 50 m transitional horizon. The majority of the mineralisation is hosted within the oxidised and transitional horizons.

The Mesa and West Lode mineralisation is hosted in separate narrow northwest trending lodes (Mesa is located to the southwest and West Lode to the northeast). The Mesa lodes consist of three separate lodes that are subvertical and are 3 – 5 m in width. The West lodes consist of multiple flat lying west dipping lodes dipping to the west. True widths vary from 2 m to up to 10 m. The base of complete oxidation lies around 50 m below the surface and is underlain by a 15 – 20 m thick transitional zone.

The Redcliffe deposit consists of a single northwest trending sub-vertical zone that is around 20 m in true width. The base of complete oxidation lies around 50 m below the surface, with the base of transitional lying approximately a further 10 m below.

The Bindi mineralisation is hosted in a series of narrow to wide (up to 20 m) steep east dipping north trending lodes, with one main lode and several subsidiary footwall and hanging wall lodes. A thin laterite cover (~5 m) overlies the deposit. The complete base of oxidation lies around 70 m below the surface, underlain by a 10 – 30 m transitional zone.

The Nambi deposit consists of five steeply west dipping north trending sub-parallel lodes, with the more extensive lode as the footwall lode. Lode widths are generally around 2 – 3 m. This deposit has a shallow oxidation profile compared to the other deposits, with the base of complete oxidation around the lodes being about 10 m below the surface. The base of transition is around 30 m below the surface.

GTS is approximately 700 m long north trending vertical dipping deposit. The width varies from 60 m in the south to 10 m in the northern sections. Within the wider parts of the deposit it appears that the mineralisation is flat dipping within the broader steep dipping mineralisation envelope. There is a laterite blanket (around 5 m thick) covering the deposit. The mineralisation does not extend into the laterite. The base of complete oxidation is around 50 m – 60 m below the surface and the top of fresh is around a further 20 m below.

The confidence in the geological interpretation is based on the drill spacing and the geometry of the mineralisation. The deposits of Hub, Redcliffe, Bindi, Nambi and GTS have a high confidence, while Kelly and Mesa\West Lode have a moderate confidence.

Wireframe interpretations have been created for weathering surfaces including, base of laterite, base of complete oxidation and top of fresh rock and mineralised domains. For Hub, wireframe interpretations have also been created to represent the known extent of both dolerite and lamprophyre dykes which brecciate and stope out the mineralised zones.

Wireframes were interpreted using cross sections that were spaced according to the drill spacing. Generally, the sections were east-west oriented or slightly oblique to east-west. Section spacing is generally 25 m to 50 m. DD and RC drilling have been used primarily for wireframe interpretation. AC and RAB drilling were

only used to provide guidance for the interpretation process but have been excluded from grade estimations.

#### **DRILLING TECHNIQUES**

NTM/DCN RC drilling was completed by Ausdrill, Challenge Drilling and PDX Pty Ltd. A 5.25 or 5.5 inch bit was used.

There is no definitive data available on the drilling contractor and hole size used for RC drilling by the historical operators.

NTM/DCN DD drilling was conducted by WDD with a DR800 truck mounted rig and Terra Drilling using Hanjhin 7000 track mounted rig. Core sizes included NQ, NQ2, NQ3, HQ and PQ3. All core was oriented using a downhole orientation tool. Some holes were pre-collared by RC.

There was no DD drilling carried out by the historical operators. The Hub MRE is based on sampling carried out using Reverse Circulation drilling (RC) and Diamond Drilling (DD). A total of 148 drillholes for a total of 22,769 m at depths ranging from 30 to 435 m. This includes 113 RC (14,341 m), 20 DD (3,911 m) and 15 DD with RC pre-collar (4,547 m). Holes included in the Hub MRE were drilled from 2018 to 2021, initially by NTM Gold Limited (NTM) and subsequently by Dacian.

The Kelly MRE is based on 108 RC holes for 13,061 m with hole depths ranging from 66 m to 283 m. The holes were drilled by Pacrim Energy Ltd (Pacrim) from 2010 – 2012, Redcliffe Resources Ltd (Redcliffe) from 2012 – 2015 and NTM in 2016.

The Mesa/West Lode MRE was based on 139 RC holes for a total of 9,800 m. The majority of the holes were drilled by Austwhim Resources (Austwhim) from 1987 to 1987. A small number of holes were drilled by Newmont Corporation (Newmont), but dates are unknown. One hole was drilled by NTM in 2020.

The Redcliffe MRE is based on 66 holes for a total of 4,596 m. Nine holes were drilled by Newmont (date unknown), Austwhim drilled 37 holes in 1987 and Pacrim 20 holes in 2007.

The Bindy MRE is based on 46 holes for a total of 8988.1 m. Within this there was one RC pre-collared DD hole with 1551.4 m of DD drilling. All holes were drilled by NTM, 41 were drilled in 2017, with the remainder drilled in 2018, 2019 and 2020.

The Nambi MRE is based on 138 holes; 123 RC, 7 RC pre-collar DD holes and 8 DD holes for a total of 22,979 m. Of these holes, 65 were drilled by CRA (date unknown), 7 by Aurora Gold (date unknown), 36 by Pacrim (2007) and 30 by NTM (2016 – 2020).

The GTS MRE is based on 182 holes; 169 RC, 4 RC pre-collar DD holes and 9 DD holes for a total of 22,663 m. Of these 141 holes were drilled by Pacrim (2007 to 2010), 40 by NTM (2016 – 2021) and 1 unknown.

#### **SAMPLING AND SUB-SAMPLING TECHNIQUES AND SAMPLE ANALYSIS METHOD**

DD core was sawn using a diamond blades and ½ core collected for assay on a 0.2 m to ~2 m basis, generally to geological contacts. Assay samples were collected from the same side of the core.

Samples from NTM/DCN drilling were prepared at BV in Perth or Kalgoorlie, or ALS Kalgoorlie or SGS Kalgoorlie – depending on the year. The sample preparation and analysis methodology was very similar across all laboratories. Samples were dried, and the entire sample pulverised to 90% passing 75 µm, and a reference sub-sample of approximately 200 g retained. The sub-sample was then pulverised to form a nominal charge of 40g (BV) or 50g (ALS) for the analysis (FA/AAS). The procedure is industry standard for this type of sample.

There is no information available on the historical operator's sample preparation and analytical techniques.

For NTM/DCN RC drilling 1 m drill samples are passed through a cone splitter installed directly below a rig mounted cyclone. A 2 – 3 kg sub-sample is collected in a calico bag (primary sample) and the balance in a plastic bag. The calico bag is placed within the corresponding plastic bag for later collection if required. A 5 m composite sample is made by spearing the reject sample in the plastic bag. If the 5 m composite returns > 0.1 g/t Au, the 1 m sample is then submitted for assay.



For the 2020/2021 RC drilling program at Hub and Bindy, as the mineralisation locations were well known, 1 m samples were collected and submitted instead of collecting a 5 m composite for zones 10 – 15 m above the mineralisation and generally through to the end of hole.

There is limited information available on the historical operators, but it appears that either 5 m or 1 m samples were taken.

Bulk Density (BD) data was derived from core collected at this project and neighboring deposits drilled by NTM Gold.

Fresh and transitional BD measurements have been collected from Hub, Mertondale, GTS and Nambi deposits.

Bulk density measurements were completed using Archimedes method of measurements on sticks of core.

A series of pit samples were collected from the Nambi pit (located to the north) to obtain oxide and transitional measurements.

## ESTIMATION METHODOLOGY

For the deposits including Hub, Kelly, Bindy, Mesa, Westlode and Nambi, the estimation method involved Ordinary Kriging (“OK”) of 1 m downhole composites to estimate gold into a 3D block model. Some of the domains only contained a few composite assays. The grades of these domains were assigned the mean grade of the composites, rather than an estimated grade.

Only RC and DD drilling are included in the compositing and estimation process. The initial sampling generally occurs at 1 m intervals for the RC drilling and variable sample lengths from 0.2 to 1.4 m in the DD drilling. Samples within each mineralisation domain were therefore composited to 1 m using Surpac software “best fit” option and a threshold inclusion of samples at sample length 50% of the targeted composite length.

Variogram modelling was undertaken within Snowden Supervisor (“Supervisor”) for the composited data for all domains with sufficient data to produce robust variograms. All variogram models were undertaken by transforming the composite data to Gaussian space, modelling a Gaussian variogram, and then back-transforming the Gaussian models to real space for use in interpolation. For the poorly informed domains, variograms models were adopted from the modelled variograms and the orientation modified accordingly.

The influence of extreme grade values was reduced by high grade capping where required. The high-grade capping limits were determined using a combination of top-cut analysis tools (grade histograms, log probability plots and coefficient of variation). These were reviewed and applied on a domain-by-domain basis.

The Kriging Neighbourhood Analysis (“KNA”) function within Supervisor software was used to determine the most appropriate estimation parameters such as minimum and maximum samples, discretisation and search distance to be used for the estimation.

For each deposit, a parent block size was selected based on the data spacing and domain morphology and the sub-block size to ensure sufficient volume resolution resulting in the following:

Deposit	Parent Block Size			Sub-Block Size		
	Y(m)	X(m)	Z(m)	Y(m)	X(m)	Z(m)
Hub	12.5	2	10	3.125	0.25	2.5
Kelly	12.5	5	5	3.125	2.5	2.5
Mesa	12.5	4	5	3.125	0.25	2.5
WL	12.5	4	5	3.125	0.25	2.5
Redcliffe	10	4	5	2.5	1	2.5
Bindy	25	5	10	3.125	0.625	2.5
Nambi	20	5	10	2.5	0.625	2.5
GTS	5	5	2.5	2.5	2.5	1.25



Gold was estimated using Geovia Surpac v7.4.2 (Surpac) with hard domain boundaries and parameters optimised for each domain. The minimum and maximum number of samples for each of the deposits is as follows:

Deposit	No. of samples	
	Minimum	Maximum
Hub	6	18
Kelly	6	16
Mesa	4	16
WL	6	18
Redcliffe	4	16
Bindy	6	18
Nambi	6	16

Search distances were based on the modelled variograms. A second search passes were used, however the proportion of material represented by the second pass is minor. The search distances and second pass search factors are as follows:

Deposit	Search Distance	Second pass search factor
Hub	50	2.5/3
Kelly	28/38/43/45/115	2
Mesa	80	2
WL	40	1.3/1.4
Redcliffe	125	2
Bindy	75	2.5
Nambi	70	2

The GTS deposit was estimated using the non-linear, Localised Uniform Conditioning (LUC) method. LUC is a post-processed approach based on an OK estimate, which is able to produce SMU-scale block grade estimates that are not over-smoothed.

Samples were composited to 1 m within the single estimation domain using best fit length option and a threshold inclusion of samples at sample length 50% of the targeted composite length.

The influence of extreme grade values was reduced by applying a top cap of 25 g/t Au. In addition, a distance based top cut was also applied for 5 g/t Au at a distance greater than 10 m.

The gold grade variogram model was undertaken by transforming the composite data to Gaussian space, modelling a Gaussian variogram, and then back-transforming the Gaussian models to real space for use in interpolation. The general orientation of the mineralisation domain is steep however variogram modelling resulted in a major direction along strike (000°) and semi-major direction dipping at -55° to the east.

LUC estimation was undertaken using a Panel block size of 20(N)m × 10(E)m × 10(RL)m. The final SMU estimation block size for the LUC was set at 5(N)m × 5(E)m × 2.5(RL)m. Selection of the Panel was used based primarily on data spacing.

LUC estimation is based on Panel block estimates undertaken using OK. This was followed by a Change of Support (CoS) which uses the composite gold grade distribution and variogram model to define a gold grade distribution at the SMU block scale. An Information Effect correction, which accounts for the imperfect predictions that dense GC data will produce, was modelled as part of the CoS, assuming a GC drill spacing of 8mY × 5mX × 1mRL. Uniform Conditioning (UC) was then undertaken to produce a model of the SMU block grade, tonnage and metal distribution within each Panel, which is conditioned to the Panel grade. The resulting array variables for a range of cut-off grades is stored in the Panel block model. Finally, LUC is undertaken whereby the UC SMU block grade distribution stored in the Panel model is devolved to the SMU block model via a discretization post-processing procedure, thus resulting in a single grade value per SMU block.

Search radius parameters were based on the anisotropy evident in the variogram, and by visual inspection of the pattern of informing composite selection. For the OK panel estimate, a single pass estimate was used with a minimum (6) and maximum (18) numbers of allowable samples were selected based on KNA. For the

SMU ranking estimate, a single pass was also used but with a minimum (6) and maximum (18) composites. During estimation, locally varying rotations were used for both the variogram model and search neighbourhood. These were based on interpreted surfaces that reflect the plane of maximum continuity of the gold mineralisation within the domain. The major and semi-major axes of the variograms and searches were thus oriented parallel to these planes.

Isatis v2018 was used to undertake the LUC estimation, with the results being imported into the final Surpac v6.9 block model.

The final insitu bulk densities applied are a mixture of actual bulk density measurements, experiences from other deposits from the Northern Goldfields of Western Australia and the depths of the weathering profiles. Generally the bulk densities are based on the weathering profiles. The bulk densities applied are as follows:

Project	Rocktype	Weathering domain		
		Oxide	Transitional	Fresh
Hub	Laterite	2.5	-	-
	All	1.8	2.5	2.7
Kelly	porphyry	1.8	2.2	2.7
	granodiorite	1.8	2.2	2.7
	granite	1.7	2.1	2.6
Mesa\WL	All	1.8	2.2	2.7
Redcliffe	All	1.8	2.2	2.7
Bindi	Laterite	2.5	-	-
	All	1.8	2.2	2.7
Nambi	All	1.8	2.2	2.7
GTS	All	1.8	2.5	2.7

## CLASSIFICATION

The Mineral Resources are classified as Indicated and Inferred.

Classification has been based on several criteria including the quality of drill data, estimation confidence, consideration of potential mining methodology, drillhole spacing and visual geological controls on continuity of mineralisation.

Indicated Mineral Resources are typically defined by 25 m × 25 m spaced drilling intersections. Estimation is undertaken in the first pass with an average distance to informing sample of less than 40 m.

Inferred Mineral Resources are defined by wider drilling intersections generally approaching 50 m x 50 m where the confidence that the continuity of mineralisation can be extended along strike and at depth. Estimation includes areas of a second pass and the average distance to informing sample of less than 80 m.

## CUT-OFF GRADE

The Mineral Resource has been quoted inside the interpreted mineralised domains, and either above a reporting cut-off grade of 0.5 g/t Au where above the 300 m RL, or above a reporting cut-off grade of 2.0 g/t Au where below the 300 m RL.

## MINING AND METALLURGICAL METHODS AND PARAMETERS

It is assumed that mining primarily would be by open pits methods except for those deposits that show sufficient tenor above the higher cut-off grade applied for the relevant RL to warrant inclusion of Mineral Resources as extractable by underground mining methods.

It is assumed that the ore would be transported and processed at the Mt Morgans Operation.

Minimum width dimensions of ore to be mined is assumed as 2 m which approximates to the minimum thickness of the mineralisation estimation domains.

The following table displays the metallurgical test work conducted at ALS Perth during September 2020 on mineralisation for various Redcliffe Project mineralisation, with a consistent gravity separation grind size of P80 passing 150 µm.

Deposit	Material type	Comp #	Material Source	Leach grid size (P80 µm)	Gravity Gold Recovery (%)	Total Gold Recovery (%)
Bindy	Fresh	1	GTDD012 225-227 (2)	150	11.37	87.11
				106	11.69	90.48
				75	11.56	94.02
GTS	Fresh	2	GTDD009 100-103 (2)	150	5.11	68.05
				106	5.13	72.14
				75	4.93	78.14
GTS	Oxide	3	GTDD007 38-40 (2)	150	15.26	87.17
				106	15.09	90
				75	14.87	93.45
GTS	Transitional	4	GTDD009 89-92 (2)	150	3.67	78.67
				106	3.44	80.86
				75	3.44	85.73
Nambi	Fresh (lens E2)	5	NBRC137D 60.5-61.5 (2)	150	24.9	88.7
				106	24.25	90.78
				75	25.64	91.72
Nambi	Fresh (lens E1)	6	NBRC137D 115.5-117 (2)	150	31.95	89.93
				106	31.96	92.89
				75	32.78	94.65
Nambi	Fresh (main lens)	7	NBRC137D 186.25-187.75 (2)	150	68.15	94.12
				106	68.47	95.75
				75	70.05	97.03
Redcliffe deposit	Fresh (lens E)	8	19RRC064 101-102 (2)	150	13.76	85.83
				106	13.9	89.15
				75	13.83	91.33
Redcliffe deposit	Transitional (lens E)	9	19RRC066 43-44 (2)	150	7.07	92.63
				106	7.15	95.88
				75	7.16	96.27
Hub	Fresh	10	19RRC028 136-137; 19RRC073D 180-181	150	21.07	85.85
				106	21.4	90.36
				75	22.99	93.69
Hub	Oxide	11	19RRC079 31-32 (2); 19RRC082 31-32 (2);	150	17.74	86.54
				106	18.56	95.81
				75	19	98.08
Hub	Transitional	12	19RRC042 104-105 (2); 19RRC092 90-91 (2)	150	24.69	93.77
				106	24.64	95.43
				75	26.33	96.88

## APPENDIX 2 – JORC TABLES

### Jupiter

#### Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
<b>Sampling techniques</b>	<i>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i>	<ul style="list-style-type: none"> <li>Surface RC holes were angled to intersect the targeted mineralised zones at optimal angles.</li> <li>In-pit RC holes were dominantly angled to the west to intersect the prevailing east dip and plunge of the mineralisation, but also vertical to target mineralised zones at optimal angles, and to fit around historic workings.</li> <li>For historical RC drilling, where available, the original logs and laboratory results that are in the central SQL Server database are retained by Dacian as either original hard copies or as scanned copies.</li> <li>Dominion Mining Limited drilled 93*, 94* and 95* prefixed holes (168 holes) Ausdrill, Robinsons and Drillex RC rigs. 1 m samples were collected using a riffle splitter. Only samples expected to be anomalous were sent to the onsite lab for analysis.</li> <li>For Dacian RC holes, face sampling hammer bits with size from 5¼" to 5¾" were used (99% of reverse circulation (RC) holes) except where a 4¾" and 3½" face sampling hammer was used for 98 and 2 holes respectively.</li> <li>The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.</li> </ul>
	<i>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</i>	<ul style="list-style-type: none"> <li>Dacian surface diamond core was sampled as half core at 1m intervals or to geological contacts. To ensure representative sampling, half core samples were always taken from the same side of the core.</li> <li>Dacian RC holes are sampled over the entire length of hole. Dacian RC drilling was sampled at 1m intervals via an on-board cone splitter</li> </ul>
	<i>Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling -problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</i>	<ul style="list-style-type: none"> <li>Dacian surface diamond core was sampled as half core at 1m intervals or to geological contacts. Sampling did not cross geological boundaries. Samples were cut in half, sampled into lengths in sample bags to achieve approximately 3kg, and submitted to a contract laboratory for crushing and pulverising to produce either a 40g or 50g charge for fire assay.</li> <li>Dacian surface RC holes are sampled over the entire length of hole. Dacian RC drilling was sampled at 1m intervals via an on-board cone splitter to achieve approximately 3kg samples. Samples were then submitted to a contract laboratory for crushing and pulverising to produce either a 40g or 50g charge for fire assay.</li> <li>Dacian in pit RC holes were sampled over the entire length of hole on 1m intervals via an on-board cone splitter to achieve approximately 3kg samples.</li> <li>Prior to December, 2020, all samples were submitted to a contract laboratory for crushing and pulverising to produce either a 40 g or 50 g charge for fire assay.</li> <li>After December, 2020, GC samples were submitted to the on-site laboratory for Pulverise and Leach (PAL) analyses using a 600 g subsample.</li> </ul>
<b>Drilling techniques</b>	<i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i>	<ul style="list-style-type: none"> <li>Drilling that informed the Mineral Resource estimate (MRE) was exclusively surface drilling, which included 9,532 RC holes for 347,462 m, 67 diamond drill (DD) holes for 14,422.81 m, and 49 RC holes with DD tails for 13,684.78 m.</li> <li>Drilling that intersected modelled mineralisation lodes or other mineralised and modelled geological objects, whose data were used to estimate grades for the Mineral Resource estimate (MRE), included 7,188 RC holes for 272,383 m, of which 6,479 holes for 190,013 m were drilled for grade control (GC) purposes (average of 29 m), 65 diamond drill (DD) holes for 13,473.81 m, and 46 RC holes with DD tails for 12,463.14 m.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>98% of holes that intersected modelled mineralisation were drilled by Dacian.</li> <li>Dominion Mining Limited drilled 93*, 94* and 95* prefixed holes (168 holes) Ausdrill, Robinsons and Drillex RC rigs. 1 m samples were collected using a riffle splitter. Only samples expected to be anomalous were sent to the onsite lab for analysis.</li> <li>and one Dominion hole were removed from the resource modelling database,</li> <li>The following number of holes with specified prefixes were ignored or removed from the MRE, as their data were considered unreliable. <ul style="list-style-type: none"> <li>14 of the 39 "95*" prefixed holes</li> <li>44 of the 190 "HR*" prefixed holes</li> <li>Five of the "HD*" prefixed holes</li> </ul> </li> <li>90 of Dacian's RC GC holes were removed, as their data had not been acquired in time, or were dummy entries in the database that had not been drilled.</li> <li>The Jupiter area includes many historic drilling types not used in the MRE.</li> <li>Dacian Diamond drilling was mostly carried out with NQ2 sized equipment, along with minor HQ3 and PQ2, using standard tube. Surface drill core was orientated using a Reflex orientation tool.</li> <li>Dominion holes (94MCRC and 95MCRC holes) were drilled with RC rigs utilising face-sampling hammers for maximum sample return.</li> <li>Other than the drill type being RC, nothing is known about the MM historic holes.</li> </ul>
<b>Drill sample recovery</b>	<i>Method of recording and assessing core and chip sample recoveries and results assessed.</i>	<ul style="list-style-type: none"> <li>Recoveries from Dominion drilling, while not recorded in the database, were noted as being generally greater than 60%.</li> <li>Recoveries from other historical holes are unknown.</li> <li>Recoveries from Dacian diamond drilling were measured and recorded into the database.</li> <li>Recoveries in fresh material generally achieved &gt; 90%.</li> </ul>
	<i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i>	<ul style="list-style-type: none"> <li>Dacian RC holes were drilled with a powerful rig with compressor and booster compressor to ensure enough air to maximise sample recovery. The splitter is cleaned at the end of each rod, to ensure that efficient sample splitting. The weight of each sample split is monitored. Drilling is stopped if the sample split size changes significantly.</li> <li>Dacian RC drilling sample volumes, quality and recoveries are monitored by the supervising geologist, with a geologist always supervising RC drilling activities to ensure good recoveries</li> </ul>
	<i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i>	<ul style="list-style-type: none"> <li>For Dacian drilling, no relationship has been observed between sample recovery and grade.</li> </ul>
<b>Logging</b>	<i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i>	<ul style="list-style-type: none"> <li>All diamond drill holes were logged for recovery, RQD, geology and structure. For Dacian drilling, diamond core was photographed both wet and dry.</li> <li>All RC holes were logged for geology, alteration, and visible structure.</li> <li>All RC chip trays were photographed.</li> <li>All drill holes were logged in full.</li> <li>RC drilling was logged by passing a portion of each sampled metre into a sieve to remove rock flour from coarse chips, the chips are then washed and placed into metre marked chip trays for logging. Where the material type does not allow for the recovery of coarse rock chips the rock flour is retained as a record. The un-sieved sample is also observed for logging purposes. The detail is considered common industry practice and is at the appropriate level of detail to support mineralization studies.</li> <li>Dacian's DD core was photographed wet and dry, and geotechnically logged to industry standards.</li> <li>All Dominion RC holes have lithological, weathering and mineralisation</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>information stored in the database.</p> <ul style="list-style-type: none"> <li>For historical RC drilling, where available the original logs and laboratory results are retained by Dacian as either original hard copies or as scanned copies.</li> <li>The Competent Person is satisfied that the logging detail supports the MRE.</li> </ul>
	<i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i>	<ul style="list-style-type: none"> <li>All holes are logged qualitatively by geologists familiar with the geology and control on the mineralisation for various geological attributes including weathering, primary lithology, primary &amp; secondary textures, colour and alteration.</li> <li>For Dacian drilling, diamond core was photographed both wet and dry. For RC drilling chip trays are photographed. Diamond core is retained on site.</li> </ul>
	<i>The total length and percentage of the relevant intersections logged.</i>	<ul style="list-style-type: none"> <li>All diamond drill holes were logged for recovery, RQD, geology, and structure. Structural measurements are taken using a kenometer to record alpha and beta angles relative to a bottom of hole line marked on the oriented core. The quality of the bottom of hole orientation line is also recorded.</li> <li>All Dacian drill holes were logged in full, from start of hole to bottom of hole.</li> </ul>
<b>Sub-sampling techniques and sample preparation</b>	<i>If core, whether cut or sawn and whether quarter, half or all core taken.</i>	<ul style="list-style-type: none"> <li>Core was cut in half using an automatic core saw at either 1m intervals or to geological contacts; core samples were collected from the same side of the core where orientations were completed.</li> </ul>
	<i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i>	<ul style="list-style-type: none"> <li>Dacian RC samples were collected via on-board cone splitters. Most samples were dry, any wet samples are recorded as wet, this data is then entered into the sample condition field in the drillhole database.</li> <li>The RC sample was split using the cone splitter to give an approximate 3kg sample. The remainder was collected into a plastic sack as a retention sample. At the grain size of the RC chips, this method of splitting is considered appropriate.</li> <li>Historical RC samples were collected at the rig using riffle splitters if dry while wet samples were bagged for later splitting. Samples condition was not recorded for most of the historic sampling. For historic RC drilling, information on the QAQC programs used is limited but acceptable with original batch reports having been reviewed and retained by Dacian.</li> <li>The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.</li> </ul>
	<i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i>	<ul style="list-style-type: none"> <li>For RC drilling, sample quality was maintained by monitoring sample volume and by cleaning splitters on a regular basis. If due to significant groundwater inflow or drilling limitations sample quality became degraded (consecutive intervals of wet sample or poor sample recovery), the RC hole was abandoned.</li> </ul>
	<i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i>	<ul style="list-style-type: none"> <li>For Dacian RC drilling, RC field duplicates were taken from the on-board cone splitter at 1 in 50 or 1 in 25 for exploration and infill drilling respectively.</li> <li>Externally prepared Certified Reference Materials were inserted within the sample stream for QAQC.</li> <li>For Dacian samples analysed by fire assay, sample preparation was conducted by a contract, National Association of Testing Authorities (NATA) Australia accredited laboratory. After drying, the sample is subject to a primary crush, then pulverised to 85% passing 75µm.</li> <li>For Dacian samples analysed by PAL, dried samples were subjected to a primary and secondary crush to 90% passing 3 mm, before being cone split into a 600g subsample. The 600 g sample was then pulverised to 90% passing 80µm and simultaneously leached for 60 minutes in a PAL machine using 2kg of grinding media, 1 Litre of water and 2 x 10g cyanide tablets (75% NaCN). The leached solution was separated by centrifuge and analysed by AAS.</li> <li>No information is available for the historic holes.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<i>Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.</i>	<ul style="list-style-type: none"> <li>For Dacian exploration DD drilling field duplicates were not taken.</li> <li>FOR Dacian RC drilling, field duplicates are generally taken a 1 in 25 samples.</li> </ul>
	<i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i>	<ul style="list-style-type: none"> <li>Sample sizes are considered appropriate to correctly represent the gold mineralisation based on the style of mineralisation, the thickness and consistency of the intersections, the sampling methodology and assay value ranges for gold.</li> </ul>
<b>Quality of assay data and laboratory tests</b>	<i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i>	<ul style="list-style-type: none"> <li>For Dacian drilling prior to December 2020, the analytical technique used was a 40g or 50g lead collection fire assay and analysed by Atomic Absorption Spectrometry (AAS). This is a full digestion technique. Samples were analysed at Bureau Veritas in Perth or Kalgoorlie, Western Australia. This is a commonly used method for gold analysis and is considered appropriate for this project.</li> <li>For in-pit RC GC drilling after December 2020, samples were analysed at the onsite SGS laboratory, using a Pulverise and Leach (PAL) technique which analyses a 600g subsample. The leached solution is analysed by AAS. PAL is a partial digestion method.</li> <li>Most of the Dominion holes were analysed at their onsite lab using fire assay (50g). The remaining 19 holes were assayed using fire assay at Analabs.</li> <li>No information regarding the analysis of the historic holes is known.</li> <li>For Dacian drilling analysed at Bureau Veritas, sieve analysis was carried out by the laboratory to ensure the grind size of 85% passing 75µm was being attained.</li> <li>For Dacian surface RC and diamond drilling, QAQC procedures involved the use of certified reference materials, standards (1 in 20) and blanks (1 in 50). For diamond drilling additional coarse blanks and standards are submitted around observed mineralisation.</li> <li>For Dacian in-pit RC drilling, QAQC procedures involved the use of certified reference materials (1 in 20) and blanks (1 in 20).</li> <li>Results were assessed as each laboratory batch was received and were acceptable in all cases.</li> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>No QAQC data has been reviewed for historic drilling, although mine production and twinned drill holes have validated drilling results. The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.</li> </ul>
	<i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i>	<ul style="list-style-type: none"> <li>Quantitative geophysical data on six holes, most notably wireline gamma-density data, were captured by Surtech using sonde serial number 9239B, with logging by unit SL33, and a caesium radioactive source.</li> <li>The updated density estimate was based on the analysis of gamma-density values filtered to be within 20% of the nominal hole diameter, determined by the density caliper arm. The data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging, which was available for only 32 m from surface for one hole, GAGC_400_0379. The average density porosity across the 32 m, assumed to be entirely oxide, was calculated as 10% of the mass. Reduced porosities of 7.5% and 5% were assumed for the transitional and fresh materials respectively.</li> <li>Geophysical sondes used in the wireline data capture were calibrated against known density standards and repeat logging of a calibration hole at Mt Morgans.</li> <li>Single and three arm callipers were used in-hole to identify areas where blowouts and significant aberrations in the hole rugosity were encountered; any deviations from within 20% of the nominal hole diameter were removed from the analysis.</li> <li>The wireline gamma-density data were compared to the core density</li> </ul>



Criteria	JORC Code explanation	Commentary
		for transitional material, which showed that acceptable correlations existed for inclusion of either dataset in the MRE.
	<i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i>	<ul style="list-style-type: none"> <li>• Certified reference materials demonstrate that sample assay values are accurate.</li> <li>• Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>• Commercial laboratories used by Dacian were audited in April 2021 by the Competent Person. The laboratory is monitored regularly by Dacian through QAQC practices, and strong communication channels are in place for data quality.</li> <li>• The on-site laboratory visited by the Competent Person twice in December 2020, is monitored regularly by Dacian through QAQC practices, and strong communication channels are in place for data quality.</li> <li>• Umpire laboratory test work was completed in 2019 over mineralised intersections with good correlation of results.</li> <li>• Umpire testwork of grade control pulp duplicate samples from December 2020 through June 2021 between PAL/LW_AAS and FA40AAS methods showed high correlation.</li> <li>• QAQC of gamma-density showed a strong positive correlation (<math>r^2 = 0.88</math>), although significant scatter was evident in the scatter plot below, indicating potential error for local gamma-density determinations. This justifies the averaging of values as opposed to estimating the density, which may result in locally inaccurate estimates due to the low number of holes (six) from which the density were determined.</li> <li>• Geophysical sondes used in the wireline data capture were calibrated against known density standards and repeat logging of a calibration hole at Mt Morgans.</li> </ul>
<b>Verification of sampling and assaying</b>	<i>The verification of significant intersections by either independent or alternative company personnel.</i>	<ul style="list-style-type: none"> <li>• Significant intersections were visually field verified by company geologists.</li> </ul>
	<i>The use of twinned holes.</i>	<ul style="list-style-type: none"> <li>• In areas of grade control, the drill spacing is at 10 m by 10 m and 10 m by 8 m (X by Y), and numerous examples exist of mineralisation showing repeated visual continuity for the estimated volumes.</li> <li>• Variogram models for the grade continuity incorporate a moderately high nugget and a short-range first structure that accounts for a high proportion of the variance. Therefore, for statistical confidence, twin drilling at spacings closer than 5 m are unlikely to be valuable for informing the repeatability of the grade mineralisation, and instead the high visual continuity and density of the drill spacing has informed the confidence in the estimate.</li> </ul>
	<i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i>	<ul style="list-style-type: none"> <li>• Prior to 2021, primary data was collected into a custom logging Excel spreadsheet and then imported into a DataShed drillhole database. The logging spreadsheet included validation processes to ensure the entry of correct data.</li> <li>• From January 2021, primary data was collected into LogChief logging software by MaxGeo and then imported into a Data Shed drillhole database. Logchief has internal data validation.</li> </ul>
	<i>Discuss any adjustment to assay data.</i>	<ul style="list-style-type: none"> <li>• Assay values that were below detection limit are stored in the database in this form, but are adjusted to equal half of the detection limit value for grade estimates. The following records were set to half detection limit: <ul style="list-style-type: none"> <li>○ Negative below detection limit assays</li> <li>○ Zeros</li> <li>○ Nulls</li> <li>○ Unsampled intervals</li> </ul> </li> <li>• Any negatives below -1 were set to null, as these represent lab error codes such as samples not received, samples destroyed in sample preparation, insufficient sample volume/weight etc.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Location of data points</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>All hole collars and down-hole surveys were captured in MGA94 Zone 51 grid using differential GPS to 3cm accuracy.</li> <li>Mine workings support the locations of historic drilling.</li> <li>Dacian RC holes were down hole surveyed with a north seeking gyro tool at 30m intervals down the hole.</li> <li>Dacian in-pit RC holes were down hole surveyed with a north seeking gyro tool, where the depth was greater than 30m.</li> <li>Dacian DD holes were down hole surveyed with a north seeking gyro tool at 12m intervals down the hole.</li> <li>Historic holes have no down hole survey information recorded.</li> </ul>
	<i>Specification of the grid system used.</i>	<ul style="list-style-type: none"> <li>The grid system used is MGA94 Zone 51 grid.</li> </ul>
	<i>Quality and adequacy of topographic control.</i>	<ul style="list-style-type: none"> <li>Topographic surfaces were prepared from detailed ground, mine and aerial surveys.</li> <li>Material above all surfaces was coded in the model as depleted to ensure no mineralisation above these surfaces was included in the MRE.</li> <li>The Competent Person is satisfied that the topographic control provides the quality required to report the Mineral Resources in accordance with the JORC Code.</li> </ul>
<b>Data spacing and distribution</b>	<i>Data spacing for reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>For the Dacian RC exploration drilling at Mt Marven South, the nominal hole spacing of surface drilling is approximately 40x40m in the core of the mineralisation. Surrounding this is 80x120m.</li> </ul>
	<i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i>	<ul style="list-style-type: none"> <li>Dacian in-pit RC holes are drilled to a 10 x 5m spacing for grade control purposes, and which has informed the MRE.</li> <li>The mineralised domains have sufficient continuity in both geology and grade to be considered appropriate for the Mineral Resource estimation procedures and classification applied under the JORC Code, and mining has further supported this.</li> </ul>
	<i>Whether sample compositing has been applied.</i>	<ul style="list-style-type: none"> <li>Samples have been composited to 1m lengths in mineralised lodes for statistics and estimation.</li> <li>Compositing was completed using a 'best-fit' method in Datamine software, which forces all samples to be included in one of the composites by adjusting composite lengths, while keeping it as close as possible to 1m.</li> </ul>
<b>Orientation of data in relation to geological structure</b>	<i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i>	<ul style="list-style-type: none"> <li>Dacian RC holes were drilled at a planned bearing of 270° (azimuth) relative to MGA94 grid north at a planned dip of -60° which is approximately perpendicular to orientation of mineralised lodes within the Mt Marven open pit.</li> <li>The majority of surface and in-pit RC holes have been drilled to approximately 270° relative to MGA94 grid north, although due to the location of the historic pit, it was necessary to drill some holes in variable directions due to access and operational restrictions, deeper targets, and some minor variable lode orientations.</li> </ul>
	<i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i>	<ul style="list-style-type: none"> <li>No orientation-based sampling bias has been identified in the data.</li> </ul>
<b>Sample security</b>	<i>The measures taken to ensure sample security.</i>	<ul style="list-style-type: none"> <li>Chain of custody is managed by Dacian. Samples are stored on site until collected for transport to the sample preparation laboratory in Kalgoorlie. Dacian personnel have no contact with the samples once they are picked up for transport. Tracking spreadsheet are used by Dacian personnel to track the progress of samples.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of sampling techniques and data.</i>	<ul style="list-style-type: none"> <li>Regular reviews of RC and DD sampling techniques are completed by the Dacian Senior Geologists and the Principal Resource Geologist, which concluded that sampling techniques are satisfactory.</li> <li>Commercial laboratories used by Dacian were audited in April 2021 by</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>the Competent Person.</p> <ul style="list-style-type: none"> <li>The Competent Person visited the on-site contract laboratory twice in December 2020 to review processes. All laboratories were performing at and producing results for a standard required to report a MRE in accordance with the JORC Code.</li> <li>Review of Dacian QAQC data has been carried out by company geologists.</li> </ul>

## Jupiter

### Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
<b>Mineral tenement and land tenure status</b>	<i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i>	<ul style="list-style-type: none"> <li>Jupiter is an active open pit mine which started in December 2017. The Jupiter deposit is located within Mining Lease 39/236, which is wholly owned by Mt Morgans WA Mining Pty Ltd, a wholly owned subsidiary of Dacian Gold Ltd and subject to a tonnage-based royalty. Dacian announced a successful equity raising (ASX July 13, 2018) to enable the extinguishment of this royalty.</li> </ul>
	<i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.</i>	<ul style="list-style-type: none"> <li>The above tenements are all in good standing.</li> </ul>
<b>Exploration done by other parties</b>	<i>Acknowledgment and appraisal of exploration by other parties.</i>	<ul style="list-style-type: none"> <li>Open pit mining occurred at Jupiter (Doublejay – Jenny, Joanne and Potato Patch open pits) in the 1990's.</li> <li>Other companies to have explored the deposit area include Whim Creek Consolidated NL, Dominion Mining, Plutonic Resources, Homestake Gold, Placer Pty Ltd, Barrick Gold Corporation, Croesus Mining NL, Metex Resources NL, Delta Gold, and Range River Gold.</li> <li>A high proportion of the historic data is confirmed by recent drilling and is of a quality that, in the Competent Person's view, supports the MRE at the classification applied.</li> </ul>
<b>Geology</b>	<i>Deposit type, geological setting and style of mineralisation.</i>	<ul style="list-style-type: none"> <li>The deposit is Archean lode gold style.</li> <li>The Jupiter deposit is interpreted to comprise structurally controlled mesothermal gold mineralisation related to syenite intrusions within altered basalt. A majority of mineralisation is associated with large shallow east dipping shears, with significant mineralisation developing where these shears crosscut syenite intrusions or the altered basalt proximal to the syenite intrusions.</li> <li>The largest, most continuous and generally highest tenor lodes are formed within the Cornwall Shear Zone (CSZ), a deposit-wide structure.</li> <li>Several small structures in the form of shears, faults and veins dip either steeply to the west, or moderately towards the north-west, north and/or north-east.</li> </ul>
<b>Drill hole information</b>	<i>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole</i>	<ul style="list-style-type: none"> <li>All information that is material to the understanding of exploration and infill drilling results completed by Dacian is documented in the appendices (results table) that accompany this announcement.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p>down hole length and interception depth hole length</p> <p>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</p>	<ul style="list-style-type: none"> <li>No drill hole information related to new exploration drilling has been excluded.</li> </ul>
<b>Data aggregation methods</b>	<p>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.</p> <p>Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</p> <p>The assumptions used for any reporting of metal equivalent values should be clearly stated.</p>	<ul style="list-style-type: none"> <li>Exploration results are reported as length weighted averages of the individual sample intervals.</li> <li>No aggregation of data has been undertaken.</li> <li>Exploration results are not being reported.</li> <li>No metal equivalent values have been used</li> </ul>
<b>Relationship between mineralisation widths and intercept lengths</b>	<p>These relationships are particularly important in the reporting of Exploration Results.</p> <p>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</p> <p>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').</p>	<ul style="list-style-type: none"> <li>Dacian RC holes were dominantly drilled at a bearing of 270° (azimuth) relative to MGA94 51 grid north at a dip of -60°.</li> <li>The holes are drilled approximately perpendicular to the orientation of the expected trend of mineralisation</li> <li>It is interpreted that true width is approximately 60%–100% of down hole intersections depending on the orientation of the target which varies along strike and down dip.</li> </ul>
<b>Diagrams</b>	<p>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</p>	<ul style="list-style-type: none"> <li>Relevant diagrams have been included within the main body this ASX release.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Balanced Reporting</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>All Dacian hole collars were surveyed in MGA94 Zone 51 grid using differential GPS to within 3cm. Dacian holes were down-hole surveyed either with a north seeking gyroscopic tool at 30m intervals to 20cm accuracy.</li> <li>Historic and Dacian mined volumes have all been surveyed by contract or Dacian surveyors to create valid topographic surfaces or 3D solids.</li> </ul>
	<i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
<b>Other substantive exploration data</b>	<i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i>	<ul style="list-style-type: none"> <li>In February 2020, downhole/wireline logging was undertaken by Surtech Systems to achieve gamma-density values at 10 cm spacing downhole for two grade control holes.</li> <li>The logging in counts-per-second (c/s) used a compensated density logging tool equipped with a Cs137 radioactive source.</li> <li>The CPS values were then converted to physical property values using calibrations determined specifically for each physical property parameter.</li> <li>The final data were supplied in a Logging ASCII Standard (CSV) file format.</li> <li>The type of instrument used was a 9239 Dual Density Instrument.</li> <li>Single and three arm callipers were used in-hole to identify areas where blowouts and significant aberrations in the hole rugosity were encountered; any deviations from within 20% of the nominal hole diameter (1,460 mm for RC) were removed from the analysis.</li> <li>The internal consistency of the downhole gamma-density data was demonstrated by repeat logging of against a calibration hole at Mt Morgans.</li> <li>Prior to mobilisation to site, the instrument was calibrated immediately against standard materials for density.</li> <li>Calliper-filtered gamma density readings related to transitional mineralisation, and were compared against dry water immersion/Archimedes method core density samples from the diamond drill core.</li> <li>A high correlation was shown between the gamma-density and core density determinations.</li> <li>The wireline geophysical logging for a nearby deposit, Ganymede, also included borehole magnetic resonance (BMR) data, which quantitatively assesses the porosity of the material logged. The BRM logs were used to adjust the gamma-density values to a dry density.</li> </ul>
<b>Further work</b>	<i>The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i>	<ul style="list-style-type: none"> <li>Infill MRE drilling; north, south, east and depth extensional drilling; RPEEE and LOM pit optimisation; UG review.</li> </ul>

## Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
<b>Database integrity</b>	<i>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</i>	<ul style="list-style-type: none"> <li>The data base has been systematically audited by a Dacian geologist. Original drilling records were compared to the equivalent records in the data base (where original records were available). Any discrepancies were noted and rectified by the data base manager.</li> </ul>
	<i>Data validation procedures used.</i>	<ul style="list-style-type: none"> <li>Historic logs were located and additional logging information, particularly relating to weathering, was input into the database.</li> <li>Ongoing database (DB) validation has been undertaken by a dedicated DB administrator communicating with geologists as the primary data sources and labs.</li> <li>Extensive validation was undertaken by the database administrator.</li> <li>Data were loaded into DataShed back-end SQL Server DB on a related data schema, providing a referentially integral database with primary key relations and look-up validation fields.</li> <li>Additional validation completed in Datamine by Dacian geologists, with any validation issues relayed to DB administrator. All Dacian drilling data has been verified as part of a continuous validation procedure. Once a drill hole is imported into the data base reports of the collar, down-hole survey, geology, and assay data are produced. These are then checked by a Dacian geologist in geological software and any corrections are sent to the data base administrator to complete.</li> <li>All data were checked for the following errors: <ul style="list-style-type: none"> <li>Duplicate drillhole IDs</li> <li>Missing collar coordinates</li> <li>Mis-matched or missing FROM or TO fields in the interval tables (assays, logging etc)</li> <li>FROM value greater than TO value in interval tables</li> <li>Non-contiguous sampling intervals</li> <li>Sampling interval overlap in the assay table</li> <li>The first sample in the interval file not starting at 0 m</li> <li>Interval tables with depths greater than the collar table EOH depth.</li> <li>Survey data were checked for large deviations in azimuth and dip between consecutive records, with none found.</li> </ul> </li> </ul>
<b>Site visits</b>	<i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i>	<ul style="list-style-type: none"> <li>The Competent Person has made several site visits during 2020 and 2021, and has worked with the site-based geologists and mining engineers on the MRE and reconciliation processes relevant to this estimate.</li> <li>Inspection of the equipment used by Dacian's drilling contractor at the time of the visits found all operators working to a standard required to report a MRE in accordance with the JORC Code.</li> <li>The Competent Person visited the on-site laboratory twice in December to review processes, and each of the two National Association of Testing Authorities (NATA) accredited offsite contract laboratories in 2021. All laboratories were performing at and producing results for a standard required to report a MRE in accordance with the JORC Code.</li> </ul>
	<i>If no site visits have been undertaken indicate why this is the case.</i>	N/A
<b>Geological interpretation</b>	<i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i>	<ul style="list-style-type: none"> <li>The confidence in the geological interpretation around the GC and resource development drilling areas is very high where the drilling density is at 10 m by 10 m out to 20 m by 20 m, and is based on mining exposure as well as a high drilling density. Visual confirmation of lode position and orientations has been observed and mapped in the Mount Marven operating open pit.</li> <li>Ongoing infill drilling has confirmed geological and grade continuity.</li> </ul>
	<i>Nature of the data used and of any assumptions made.</i>	<ul style="list-style-type: none"> <li>Geological and structural logging and pit mapping have been used to assist identification and delineation of lithology and mineralisation.</li> <li>All lodes were treated as hard-boundaries for statistics and estimation.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>• Alternate interpretations may consider a different gold grade cut-off for the modelling of mineralisation, which may increase the tonnages and lower the grade for a reduced grade cut-off and vice-versa for an increased grade. Either of these are likely to result in a similar balance of metal.</li> <li>• However, the volumes and grades in the mineralisation model have been demonstrated by open pit ore mark-outs at slightly higher-grade cut-offs, and which show that the boundaries of the mineralisation are suitable for the delineation of ore and waste</li> <li>• Doublejay geological objects modelled were: <ul style="list-style-type: none"> <li>○ Lodes: 67 (including two CSZ lodes)</li> <li>○ Syenite intrusive pipes: two (Joanne and Jenny)</li> <li>○ Syenite stocks: 2</li> <li>○ Syenite dykes: 5</li> <li>○ Porphyry dykes or combined intrusive bodies: 2</li> </ul> </li> <li>• Heffernans geological objects modelled were: <ul style="list-style-type: none"> <li>○ Lodes: 61 (including eight CSZ lodes)</li> <li>○ Syenite intrusive pipes: 1</li> <li>○ Syenite dykes: 4</li> <li>○ Porphyry dykes: 5</li> </ul> </li> <li>• Ganymede geological objects modelled were: <ul style="list-style-type: none"> <li>○ Lodes: 41</li> <li>○ Syenite intrusive pipes: 1</li> <li>○ Porphyry dykes: 3</li> </ul> </li> </ul>
	<i>The use of geology in guiding and controlling Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>• The mineralisation was modelled with a relatively strict gold cut-off of 0.3 g/t Au, which has been confirmed as appropriate for the mining methods and ore markouts. All modelled lodes were treated as hard boundaries for statistics and estimation, although where geological and statistical observations deemed suitable, the lodes were grouped into domains for increased sample counts.</li> <li>• The composited samples within the modelled lode objects were used to estimate the corresponding block object codes with the resource block model.</li> <li>• The lodes show high continuity through the oxidation/weathering profile without dispersion halos. Statistics were reviewed, including grade distributions, and contact analysis, between the oxidation domains, which showed that evidence for boundaries was weak, although almost all lodes do not transect any of the modelled oxidation surfaces. Therefore, no hard boundaries by oxidation domain were applied.</li> </ul>
	<i>The factors affecting continuity both of grade and geology.</i>	<ul style="list-style-type: none"> <li>• The larger syenite intrusive pipes are the core bodies from which the lodes protrude as flat-lying, stacked, mineralised structures. There is evidence that the syenite stocks and dykes are also associated with higher grade mineralisation.</li> <li>• Contact and continuity statistical analysis confirmed that no or soft boundaries existed for the lodes within and outside the syenites.</li> </ul>
<b>Dimensions</b>	<i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i>	<ul style="list-style-type: none"> <li>• The Jupiter Mineral Resource area extends over a strike length of 2,080m (from 6,811,400mN – 6,813,480mN) and includes the 800m vertical interval from 500mRL to -300mRL.</li> </ul>
<b>Estimation and modelling techniques</b>	<i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i>	<ul style="list-style-type: none"> <li>• Samples were composited to 1 m intervals (“composites”) based on assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.</li> <li>• To model the spatial continuity of gold grades, variography was conducted in Supervisor 8.12. Statistics were length-weighted.</li> <li>• Composite samples were declustered prior to variography for the statistical domains that contained lodes (i.e. not syenite and porphyry domains).</li> <li>• A normal-score transform was applied to continuity analysis data.</li> <li>• After variograms were modelled, a back-transform model was exported with Datamine rotations for use in Datamine parameter files.</li> <li>• Variograms were modelled for each statistical domain where possible, or borrowed from the most geologically related domain. Many statistical domains showed good variograms. Other variograms were coerced into the plane of the</li> </ul>



Criteria	JORC Code explanation	Commentary
		<p>lode orientations, and then variograms were constructed with reasonable structures evident for most, although some required variograms to be informed entirely by the lode orientations and geometries guided by modelling of other, better informed statistical domains.</p> <p>Doublejay:</p> <ul style="list-style-type: none"> <li>For most lode domains and the syenite and porphyry domains, a short-range (~6 m to ~15 m in the major and semi-major directions, less in the minor direction) and long range structure (20 m to 50 m in the major direction) were modelled.</li> <li>The CSZ showed longer ranges in all directions for all structures.</li> <li>Multi-block KNA was undertaken. KNA found that a 10 x 10 x 5 block size gave the best statistics, marginally better than 5 x 5 x 2.5 block size, which was considered more appropriate for the drillhole density across the unmined area of the deposit. The KNA confirmed that the best statistics were for minimum samples of 8 to 10 and maximum samples of between 15–20 inclusive, although for porphyry and syenites the minimum was dropped to 6. Max samples per drillhole were set to 4 for all lodes and domains other than CSZ, which was set to 3. A max of 4 for lodes was selected because. The short-range structure was often very short (11 m to 27 m), so forcing 3 samples per drillhole and with a minimum of 8 samples to achieve a minimum of 3 holes in any estimate was detrimental to the estimates of lode fringes.</li> <li>The largest short-range modelled was for Syenite domain 6 of 49 m. The full range of any variogram modelled was capped at 5 x the short range if the experimental variography suggested longer.</li> <li>The best statistics were achieved for a search ellipse size matching the short-range structure in all cases, followed by the full range.</li> <li>Statistics were invariable for changes in discretization.</li> <li>Insufficient samples were available to model FW3 (no variogram maps could be calculated), therefore, the variogram modelled for FW2 was borrowed.</li> <li>An unrotated block model was created in MGA Zone 51 grid to cover the extent of the deposit. The deposit is a subset of the larger Jupiter deposit; therefore, to avoid overlap with the Heffernans MRE, the model is relatively truncated to the mineralisation. However, the mining area has been established, and therefore mining studies do not require infrastructure design elements to be built using the model cells.</li> <li>A parent block size of 10 m x 10 m x 5 m (X x Y x Z) was chosen, which was supported by drill hole spacing in X and Y directions. Some areas of tighter drilling at grade control density exist, but most of the deposit has been drilled at a density of 20 m x 20 m out to 40 m x 40 m on the fringes. The dominant 1 m sample length and the Jupiter bench height of 5 m support the shorter block height. Nominally spaced 10 m to 20 m pierce points have been achieved, although this is highly variable resulting from the variable hole angles.</li> <li>Sub-celling to 1/8 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.</li> <li>Based on statistical analysis that no or soft boundaries existed, the CSZ and lodes were estimated with all corresponding composites for the lode number, inside and outside the syenites.</li> <li>The estimate employed OK within a 3-pass expanding search ellipse strategy, honouring the anisotropic ratios orthogonally, which was based on KNA results to improve the local grade estimate without unacceptable error, while ensuring a globally unbiased estimate.</li> <li>Lodes:</li> <li>Pass 1: 1st short-range structure of the statistical domain variogram with dynamic anisotropy applied.</li> <li>Pass 2: full range of the variogram, except for CSZ domain 30001, which has three structures, the third being too large for a second pass search ellipse.</li> <li>Pass 3: typically 5 times the first ellipse volume, but adjusted to 6 x and 7 x for lodes that required larger search volumes to estimate fringe blocks, and 10 x for the deep syenite where it is mostly uninformed by samples. The min and max samples were dropped to 4 and 8 respectively.</li> <li>To handle the wireframe flexures (and local variability in the lode orientations known from mining to exist), dynamic anisotropy was applied for the 1st pass</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>of mineralisation only.</p> <p>Hefferenans:</p> <ul style="list-style-type: none"> <li>• All of the oxide and transitional, and most of the fresh material within the current and RPEEE pit shells have been depleted. The following describes the modelling briefly in context of the grade control model.</li> <li>• The CSZ, hanging-wall showed the best variogram.</li> <li>• For most lode domains and the syenite and porphyry domains, a short-range and longer-range structure were modelled.</li> <li>• All variograms contained a high to very high nugget when back-transformed.</li> <li>• KNA was initially undertaken on a well-informed block within a well-informed area of the CSZ, but the statistics for this block were uninformative. Therefore, multi-block KNA was undertaken. KNA found that a 5 x 5 x 2.5 block size gave the best statistics, which was considered appropriate for the drillhole density for the unmined area of the deposit.</li> <li>• The KNA confirmed that the best statistics were for minimum samples of 8 to 10 and maximum samples of 24 to 28 were appropriate for lodes dependent on the domain, while 6 minimum and 12 maximum. The best statistics were achieved for a search ellipse size matching the short-range structure, followed by the full range. Statistics were invariable for changes in discretization.</li> <li>• Variogram data for CSZ reviewed by DR for orientation, nugget, and modelled structures Anisotropic ratios with application of successive search volumes and influence reviewed.</li> <li>• An unrotated block model was created in MGA Zone 51 grid to cover the extent of the deposit. The deposit is a subset of the larger Jupiter deposit; therefore, to avoid overlap with the Ganymede and Doublejay MREs, the model is relatively truncated to the mineralisation.</li> <li>• A parent block size of 5 m x 5 m x 2.5 m (X x Y x Z) was chosen, which was supported by drill hole spacing in X and Y directions. Some areas of tighter drilling at grade control density exist, most of the remainder of the deposit has been drilled at a density of 10 m by 10 m and 10 m by 8 m out. The dominant 1 m sample length and the Jupiter bench height of 5 m support the shorter block height.</li> <li>• Sub-celling to 1/40 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.</li> <li>• The estimate employed OK within a 3-pass expanding search ellipse strategy, honouring the anisotropic ratios orthogonally, which was based on KNA results to improve the local grade estimate without unacceptable error, while ensuring a globally unbiased estimate.</li> </ul> <p>Ganymede:</p> <ul style="list-style-type: none"> <li>• The CSZ, hanging-wall showed the best variogram, followed by the syenite and FW1 and FW2 statistical domains. Other variograms were coerced into the plane of the lode orientations, and then variograms were constructed with reasonable structures evident for most, although some required variograms to be informed entirely by the lode orientations and geometries guided by modelling of other, better informed statistical domains.</li> <li>• For most lode domains and the syenite and porphyry domains, a short-range (~6 m to ~15 m) and longer (but relatively short around 20 m) range structure were modelled. The CSZ also had two spherical structures modelled, but the longer range was much longer than other domains, reflecting the greater size and continuity of the lodes. Variography for two poorly informed supergene statistical domains yielded a single spherical structure.</li> <li>• All variograms contained a high to very high nugget when back-transformed.</li> <li>• KNA was initially undertaken on a well-informed block within a well-informed area of the CSZ, but the statistics for this block were uninformative. Therefore, multi-block KNA was undertaken. KNA found that a 5 x 5 x 2.5 block size gave the best statistics, marginally better than 10 x 10 x 5, which was considered more appropriate for the drillhole density across the partially mined area of the deposit. The KNA confirmed that the best statistics were for minimum samples of 7 to 9 and maximum samples of typically less than 20. The best statistics were achieved for a search ellipse size matching the short-range structure, followed by the full range. Statistics were invariable for changes in</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>discretization.</p> <ul style="list-style-type: none"> <li>Variogram data for CSZ reviewed by DR for orientation, nugget, and modelled structures Anisotropic ratios with application of successive search volumes and influence reviewed.</li> <li>An unrotated block model was created in MGA Zone 51 grid to cover the extent of the deposit. The deposit is a subset of the larger Jupiter deposit; therefore, to avoid overlap with the Heffernans MRE, the model is relatively truncated to the mineralisation. However, the mining area has been established, and therefore mining studies do not require infrastructure design elements to be built using the model cells.</li> <li>A parent block size of 10 m x 10 m x 5 m (X x Y x Z) was chosen, which was supported by drill hole spacing in X and Y directions. Some areas of tighter drilling at grade control density exist, but most of the deposit has been drilled at a density of 20 m x 20 m out to 40 m x 40 m on the fringes. The dominant 1 m sample length and the Jupiter bench height of 5 m support the shorter block height. Nominally spaced 10 m to 20 m pierce points have been achieved, although this is highly variable resulting from the variable hole angles.</li> <li>Sub-celling to 1/8 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.</li> <li>The estimate employed OK within a 3-pass expanding search ellipse strategy, honouring the anisotropic ratios orthogonally, which was based on KNA results to improve the local grade estimate without unacceptable error, while ensuring a globally unbiased estimate.</li> <li>Lodes:</li> <li>Pass 1: 1st range structure of the statistical domain variogram with dynamic anisotropy applied. min 7 to 9, max 17 to 23, max per hole 4</li> <li>Pass 2: full range of the variogram, min 7 to 9, max 17 to 23, max per hole 4</li> <li>Pass 3: 200 m search ellipse (major); min 3, max 10, max per hole 4</li> <li>To handle the wireframe flexures (and local variability in the lode orientations known from mining to exist), dynamic anisotropy was applied for the 1st pass of mineralisation only.</li> </ul>
	<i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i>	<ul style="list-style-type: none"> <li>Previous estimates provided higher overall tonnages with higher grades; however, these were completed prior to a large amount of additional drilling occurring and the introduction of density estimates based on quantitative data.</li> <li>Production figures are not able to be reconciled with confidence, as Jupiter material is blended prior to crushing at the Jupiter mill with Mount Marven and previously Westralia UG when it was operating until mid-2020.</li> <li>GC models are reconciled throughout the mining process. These show good agreement to the resource model in mined areas where the interpretation methodology agrees.</li> </ul>
	<i>The assumptions made regarding recovery of by-products.</i>	<ul style="list-style-type: none"> <li>No assumptions have been made regarding the recovery of by-products.</li> </ul>
	<i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i>	<ul style="list-style-type: none"> <li>No other variables have been estimated.</li> </ul>
	<i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i>	<ul style="list-style-type: none"> <li>For Doublejay, a parent block size of 10 m x 10 m x 5 m (X by Y by Z) was chosen, which was supported by KNA and by drill hole spacing in KNA Y and Z directions. In the mine area, most of the deposit has been sampled at a density of 10 m x 10 m out to 40 m x 40 m on the fringes. Sub-celling to 1/5 the parent cell in all directions has provided very high resolution for volume control at the GC and ore markout level. to account for the moderately thin lode wireframes.</li> <li>For Heffernans, a parent block size of 5 m x 4 m x 2.5 m (X by Y by Z) was chosen. The model is entirely supported by GC drilling at a spacing of 10 m by 10 m or 10 m by 8 m (X by Y) with 1 m sample lengths down-hole, and therefore the smaller block size is supported. Sub-celling to 1/40 the parent cell in all directions has provided very high resolution for volume control at the GC and ore markout level.</li> <li>For Ganymede, a parent block size of 10 m x 10 m x 5 m (X by Y by Z) was chosen, which was supported by KNA and by drill hole spacing in KNA Y and Z</li> </ul>

Criteria	JORC Code explanation	Commentary
		directions. In the mine area, most of the deposit has been sampled at a density of 20 m x 20 m out to 40 m x 40 m on the fringes. Sub-celling to 1/5 the parent cell in all directions has provided very high resolution for volume control at the GC and ore markout level. to account for the moderately thin lode wireframes.
	<i>Any assumptions behind modelling of selective mining units.</i>	<ul style="list-style-type: none"> <li>The SMU for Jupiter is 5 m by 5 m by 2.5 m and 2.5 m<sup>3</sup> depending on the flitch mining approach, and therefore the block models have been designed to fit the SMU.</li> </ul>
	<i>Any assumptions about correlation between variables.</i>	<ul style="list-style-type: none"> <li>No assumptions have been made about correlation between variables.</li> </ul>
	<i>Description of how the geological interpretation was used to control the resource estimates.</i>	<ul style="list-style-type: none"> <li>Geology and grade are used to define the mineralisation lodes. Within each lode, whose modelling is outlined above, the estimate was constrained to blocks within the lode wireframe using only top-cut composited samples from the corresponding lode.</li> </ul>
	<i>Discussion of basis for using or not using grade cutting or capping.</i>	<ul style="list-style-type: none"> <li>High-grade top-caps were applied to limit the influence of extreme outliers on the grade estimate. The top-caps were applied to the mineralisation domains following statistical analysis completed in Snowden Supervisor™ software.</li> <li>Top-cuts were applied by lithological model type, and by domain groupings, while individual lodes were also reviewed to ensure the domain top-cut was appropriate.</li> <li>The top-cuts were kept at around 1% – 2% of the grade distribution for each lode.</li> <li>For Doublejay, high-grade top-cuts ranged as follows: <ul style="list-style-type: none"> <li>CSZ lodes: 20 g/t Au</li> <li>Other lodes: 1.5 g/t – 19 g/t Au</li> <li>Syenite: 1.75 g/t – 5 g/t Au</li> <li>Porphyry: 0.75 g/t Au – 2.5 g/t Au</li> </ul> </li> <li>For Heffernans, high-grade top-cuts ranged as follows: <ul style="list-style-type: none"> <li>CSZ lodes: 7.3 g/t – 28 g/t Au</li> <li>Other lodes: 7 g/t – 35 g/t Au</li> <li>Syenite: 5 g/t – 10 g/t Au</li> <li>Porphyry: 2 g/t Au</li> </ul> </li> <li>For Ganymede, high-grade top-cuts ranged as follows: <ul style="list-style-type: none"> <li>Lodes: 4.4 g/t – 27 g/t Au</li> <li>Syenite: 3.7 g/t Au</li> <li>Porphyry: 0.5 g/t – 1.1 g/t Au</li> </ul> </li> </ul>
	<i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i>	<ul style="list-style-type: none"> <li>Validation of the estimate was completed for the resource block models using numerical methods (histograms, CDFs and swath plots) and validated visually against the input raw drillhole data, declustered data, composites and blocks.</li> </ul>
<b>Moisture</b>	<i>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</i>	<ul style="list-style-type: none"> <li>Tonnages and grades have been estimated on a dry in situ basis.</li> </ul>
<b>Cut-off parameters</b>	<i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i>	<ul style="list-style-type: none"> <li>The MRE has been reported above a lower cut-off of 0.5 g/t Au above a RPEEE pit optimisation shell, and above a lower cut-off of 2.0 g/t Au below the same RPEEE shell, which has included the following parameters and assumptions: <ul style="list-style-type: none"> <li>Mining by open pit excavation</li> <li>Ore loss of 6%</li> <li>Mining dilution of 12%</li> <li>Processing recovery 92.3% for all material types</li> <li>Australian gold price of \$2,400/oz</li> <li>Gold royalty of 2.5%</li> <li>Mining rates are based on the long-term performance of the currently operating Jupiter gold mine.</li> <li>Geotechnical inputs are derived from detailed geotechnical investigations completed by geotechnical consultants.</li> </ul> </li> <li>The reporting cut-off parameters were selected based on known open pit economic cut-off grades.</li> <li>The potential to extract mineralisation via underground mining methods has not been considered due to the depth of drilling and mineralisation.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Mining factors or assumptions</b>	<i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i>	<ul style="list-style-type: none"> <li>• The ore is being processed at the adjacent Jupiter Processing Facility, part of the MMGO. Recoveries achieved to date are 92.3%.</li> <li>• Dacian has been mining Jupiter via open pit methods since December 2017. It is assumed that the same mining methods will be applicable for extraction of in-situ material included in this MRE update.</li> </ul>
<b>Metallurgical factors or assumptions</b>	<i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i>	<ul style="list-style-type: none"> <li>• The ore is processed at the proximal Jupiter Processing Facility, part of the MMGO. Recoveries achieved to date are 92.3%.</li> </ul>
<b>Environmental factors or assumptions</b>	<i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i>	<ul style="list-style-type: none"> <li>• Jupiter is an active open pit mine at the Mount Morgans Gold Operation with all requisite environmental approvals in place.</li> <li>• Waste rock is stored in a conventional waste dump.</li> </ul>

Criteria	JORC Code explanation	Commentary																																																																																		
Bulk density	Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.	<ul style="list-style-type: none"><li>The core-immersion method determinations from Jupiter diamond core number 20,806 on a variety of whole, half and quarter core, approximately 10% of which are from the top 50 m of the hole, although some of these may have been drilled from pit floors or other in-pit platforms.<table><tr><th>Material type</th><th>Count of sample_type</th></tr><tr><td>HALF_BQ</td><td>573</td></tr><tr><td>HALF_HQ2</td><td>828</td></tr><tr><td>HALF_HQ3</td><td>5,332</td></tr><tr><td>HALF_NQ2</td><td>10,745</td></tr><tr><td>HALF_PQ2</td><td>32</td></tr><tr><td>QUARTER_HQ2</td><td>455</td></tr><tr><td>QUARTER_HQ3</td><td>99</td></tr><tr><td>QUARTER_NQ2</td><td>1,590</td></tr><tr><td>QUARTER_PQ2</td><td>1,150</td></tr><tr><td>WHOLE_HQ3</td><td>1</td></tr><tr><td>WHOLE_NQ2</td><td>1</td></tr><tr><td>Grand Total</td><td>20,806</td></tr></table></li><li>Quantitative gamma-density measurements were captured on six Ganymede GC holes and four Doublejay resource development holes in February 2021 by Surtech to mitigate the risk of the lack of density determinations in oxide and transitional material.<p>Doublejay:</p><ul style="list-style-type: none"><li>Density values assigned in the previous MRE, tabulated below, were used to compare against the gamma-density values and provide cross-validation:<table><tr><th>Oxidation</th><th>Waste (Mafic)</th><th>Mineralisation (shear-hosted in mafic)</th><th>Syenite</th></tr><tr><td>Oxide</td><td>1.80</td><td>1.80</td><td>2.24</td></tr><tr><td>Trans</td><td>2.83</td><td>1.80</td><td>2.55</td></tr><tr><td>Fresh</td><td>2.94</td><td>2.86</td><td>2.65</td></tr></table></li></ul></li><li>The gamma-density values were filtered to be within 20% of the nominal hole diameter, determined by the density caliper arm. The data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging, which was available for:<ul style="list-style-type: none"><li>DJRD_STG2_0099 from 100.1 m to 109.02 m</li><li>DJRD_STG2_0101 from 24.41 m to 79.27 m</li></ul></li><li>The average porosity (assumed to be all fresh) for the data was 3%, which was used to adjust all densities from the gamma.</li><li>The gamma-density data could not be extracted by lithological type, but the values were confirmed to be from the following:<table><tr><th>Zone</th><th>Type</th><th>Wireline Geophysics Records (10 cm points)</th><th>Metres Logged</th></tr><tr><td></td><td>Mafic waste</td><td>65,175</td><td>6,517.5</td></tr><tr><td>10</td><td>CSZ</td><td>1,300</td><td>130</td></tr><tr><td>1002</td><td>Syenite</td><td>50</td><td>5</td></tr><tr><td>1004</td><td>Syenite</td><td>25</td><td>2.5</td></tr><tr><td>1021</td><td>Syenite</td><td>1,975</td><td>197.5</td></tr><tr><td>14</td><td>CSZ</td><td>1,100</td><td>110</td></tr><tr><td>3046</td><td>Mineralisation lode</td><td>2,275</td><td>227.5</td></tr><tr><td>3047</td><td>Mineralisation lode</td><td>3,750</td><td>375</td></tr><tr><td>3102</td><td>Mineralisation lode</td><td>1,875</td><td>187.5</td></tr></table></li><li>The Doublejay Mineral Resources are almost entirely depleted for Oxide and transitional material. Therefore, the gamma-density data are derived from fresh material, and instead of using the data for assignment or estimation, the data were used to validate the core density determinations, with the following observations made:<ul style="list-style-type: none"><li>A small amount of weathering impact was noted in the immersion-method core densities not noted in the gamma-densities at the same RL.</li><li>The gamma-density data largely correlates with the values for the same depths in the core densities, once the scatter is removed and</li></ul></li></ul>	Material type	Count of sample_type	HALF_BQ	573	HALF_HQ2	828	HALF_HQ3	5,332	HALF_NQ2	10,745	HALF_PQ2	32	QUARTER_HQ2	455	QUARTER_HQ3	99	QUARTER_NQ2	1,590	QUARTER_PQ2	1,150	WHOLE_HQ3	1	WHOLE_NQ2	1	Grand Total	20,806	Oxidation	Waste (Mafic)	Mineralisation (shear-hosted in mafic)	Syenite	Oxide	1.80	1.80	2.24	Trans	2.83	1.80	2.55	Fresh	2.94	2.86	2.65	Zone	Type	Wireline Geophysics Records (10 cm points)	Metres Logged		Mafic waste	65,175	6,517.5	10	CSZ	1,300	130	1002	Syenite	50	5	1004	Syenite	25	2.5	1021	Syenite	1,975	197.5	14	CSZ	1,100	110	3046	Mineralisation lode	2,275	227.5	3047	Mineralisation lode	3,750	375	3102	Mineralisation lode	1,875	187.5
Material type	Count of sample_type																																																																																			
HALF_BQ	573																																																																																			
HALF_HQ2	828																																																																																			
HALF_HQ3	5,332																																																																																			
HALF_NQ2	10,745																																																																																			
HALF_PQ2	32																																																																																			
QUARTER_HQ2	455																																																																																			
QUARTER_HQ3	99																																																																																			
QUARTER_NQ2	1,590																																																																																			
QUARTER_PQ2	1,150																																																																																			
WHOLE_HQ3	1																																																																																			
WHOLE_NQ2	1																																																																																			
Grand Total	20,806																																																																																			
Oxidation	Waste (Mafic)	Mineralisation (shear-hosted in mafic)	Syenite																																																																																	
Oxide	1.80	1.80	2.24																																																																																	
Trans	2.83	1.80	2.55																																																																																	
Fresh	2.94	2.86	2.65																																																																																	
Zone	Type	Wireline Geophysics Records (10 cm points)	Metres Logged																																																																																	
	Mafic waste	65,175	6,517.5																																																																																	
10	CSZ	1,300	130																																																																																	
1002	Syenite	50	5																																																																																	
1004	Syenite	25	2.5																																																																																	
1021	Syenite	1,975	197.5																																																																																	
14	CSZ	1,100	110																																																																																	
3046	Mineralisation lode	2,275	227.5																																																																																	
3047	Mineralisation lode	3,750	375																																																																																	
3102	Mineralisation lode	1,875	187.5																																																																																	



Criteria	JORC Code explanation	Commentary																																																																																				
		<p>the banding disregarded for comparison.</p> <ul style="list-style-type: none"><li>○ A cluster between 2.8 t/m³ and 3.1 t/m³ existed, which provides little indication of a relationship between fresh lithologies and density.</li><li>○ However, there were distinct bands noted for the (mostly) fresh core densities, which could not be ignored, and therefore the data were coded by zone and oxidation to determine the geological relationships, which were averaged for comparison:</li><li>○</li></ul> <table><tr><th>Oxidation</th><th>Waste (Mafic)</th><th>Mineralisation (shear-hosted in mafic)</th><th>Syenite (waste and mineralisation)</th><th>Porphyries</th></tr><tr><td>Oxide</td><td>N/A</td><td>N/A</td><td>N/A</td><td>N/A</td></tr><tr><td>Trans</td><td>2.94</td><td>2.82</td><td>N/A</td><td>2.76</td></tr><tr><td>Fresh</td><td>2.94</td><td>2.86</td><td>2.91</td><td>2.84</td></tr></table> <ul style="list-style-type: none"><li>• Although very limited transitional material remained, it was carefully considered. The transitional mineralisation averaged 2.82, but the graphs suggest an assignment of 2.65 is more appropriate. The syenite density values were adjusted to those closer to the analysis defined for the Ganymede quantitative data.</li><li>• The values assigned for oxide and transitional material by bench are shown below:</li></ul> <table><tr><th>Oxidation</th><th>Waste (Mafic)</th><th>Mineralisation (shear-hosted in mafic)</th><th>Syenite (waste and mineralisation)</th><th>Porphyries</th></tr><tr><td>Oxide</td><td>N/A (1.80 used in macro)</td><td>N/A (1.80 used in macro)</td><td>N/A (2.24 used in macro)</td><td>N/A (2.24 used in macro)</td></tr><tr><td>Trans</td><td>2.82</td><td>2.65</td><td>2.65</td><td>2.76</td></tr><tr><td>Fresh</td><td>2.94</td><td>2.86</td><td>2.75</td><td>2.84</td></tr></table> <p>Heffernans:</p> <ul style="list-style-type: none"><li>• Gamma-density data were not available at the time of density assignment for these deposits. However, the Mineral Resources for these areas are entirely depleted for Oxide and transitional material. Therefore, core-immersion method determinations were used for the density assignment.</li></ul> <table><tr><th>Lithology</th><th>Oxidation</th><th>Value</th></tr><tr><td rowspan="3">Mafic mineralisation</td><td>Oxide</td><td>1.8</td></tr><tr><td>Transitional</td><td>1.8</td></tr><tr><td>Fresh</td><td>2.86</td></tr><tr><td rowspan="3">Mafic waste</td><td>Oxide</td><td>1.8</td></tr><tr><td>Transitional</td><td>2.83</td></tr><tr><td>Fresh</td><td>2.94</td></tr><tr><td rowspan="3">Syenite</td><td>Oxide</td><td>2.24</td></tr><tr><td>Transitional</td><td>2.55</td></tr><tr><td>Fresh</td><td>2.65</td></tr><tr><td rowspan="3">Porphyry</td><td>Oxide</td><td>2.15</td></tr><tr><td>Transitional</td><td>2.61</td></tr><tr><td>Fresh</td><td>2.73</td></tr><tr><td rowspan="3">Carbonatite</td><td>Oxide</td><td>N/A</td></tr><tr><td>Transitional</td><td>2.6</td></tr><tr><td>Fresh</td><td>2.72</td></tr><tr><td>Transported sand</td><td>All</td><td>2.2</td></tr><tr><td>Dump fill</td><td>All</td><td>2.0</td></tr></table> <p>Ganymede</p> <ul style="list-style-type: none"><li>• For Ganymede, density values assigned in the previous MRE, tabulated below, were used to compare and validate the gamma-density values:</li></ul>	Oxidation	Waste (Mafic)	Mineralisation (shear-hosted in mafic)	Syenite (waste and mineralisation)	Porphyries	Oxide	N/A	N/A	N/A	N/A	Trans	2.94	2.82	N/A	2.76	Fresh	2.94	2.86	2.91	2.84	Oxidation	Waste (Mafic)	Mineralisation (shear-hosted in mafic)	Syenite (waste and mineralisation)	Porphyries	Oxide	N/A (1.80 used in macro)	N/A (1.80 used in macro)	N/A (2.24 used in macro)	N/A (2.24 used in macro)	Trans	2.82	2.65	2.65	2.76	Fresh	2.94	2.86	2.75	2.84	Lithology	Oxidation	Value	Mafic mineralisation	Oxide	1.8	Transitional	1.8	Fresh	2.86	Mafic waste	Oxide	1.8	Transitional	2.83	Fresh	2.94	Syenite	Oxide	2.24	Transitional	2.55	Fresh	2.65	Porphyry	Oxide	2.15	Transitional	2.61	Fresh	2.73	Carbonatite	Oxide	N/A	Transitional	2.6	Fresh	2.72	Transported sand	All	2.2	Dump fill	All	2.0
Oxidation	Waste (Mafic)	Mineralisation (shear-hosted in mafic)	Syenite (waste and mineralisation)	Porphyries																																																																																		
Oxide	N/A	N/A	N/A	N/A																																																																																		
Trans	2.94	2.82	N/A	2.76																																																																																		
Fresh	2.94	2.86	2.91	2.84																																																																																		
Oxidation	Waste (Mafic)	Mineralisation (shear-hosted in mafic)	Syenite (waste and mineralisation)	Porphyries																																																																																		
Oxide	N/A (1.80 used in macro)	N/A (1.80 used in macro)	N/A (2.24 used in macro)	N/A (2.24 used in macro)																																																																																		
Trans	2.82	2.65	2.65	2.76																																																																																		
Fresh	2.94	2.86	2.75	2.84																																																																																		
Lithology	Oxidation	Value																																																																																				
Mafic mineralisation	Oxide	1.8																																																																																				
	Transitional	1.8																																																																																				
	Fresh	2.86																																																																																				
Mafic waste	Oxide	1.8																																																																																				
	Transitional	2.83																																																																																				
	Fresh	2.94																																																																																				
Syenite	Oxide	2.24																																																																																				
	Transitional	2.55																																																																																				
	Fresh	2.65																																																																																				
Porphyry	Oxide	2.15																																																																																				
	Transitional	2.61																																																																																				
	Fresh	2.73																																																																																				
Carbonatite	Oxide	N/A																																																																																				
	Transitional	2.6																																																																																				
	Fresh	2.72																																																																																				
Transported sand	All	2.2																																																																																				
Dump fill	All	2.0																																																																																				



Criteria	JORC Code explanation	Commentary																																																																			
		<table><tr><td>Oxidation</td><td>Waste</td><td>Mineralisation</td></tr><tr><td>Oxide</td><td>1.80</td><td>1.80</td></tr><tr><td>Trans</td><td>2.83</td><td>1.80</td></tr><tr><td>Fresh</td><td>2.94</td><td>2.86</td></tr></table>	Oxidation	Waste	Mineralisation	Oxide	1.80	1.80	Trans	2.83	1.80	Fresh	2.94	2.86																																																							
Oxidation	Waste	Mineralisation																																																																			
Oxide	1.80	1.80																																																																			
Trans	2.83	1.80																																																																			
Fresh	2.94	2.86																																																																			
		<ul style="list-style-type: none"><li>The updated density estimate was based on the analysis of gamma-density values filtered to be within 20% of the nominal hole diameter, determined by the density caliper arm. The data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging, which was available for only 32 m from surface for one hole, GAGC_400_0379. The average density porosity across the 32 m, assumed to be entirely oxide, was calculated as 10% of the mass. Reduced porosities of 7.5% and 5% were assumed for the transitional and fresh materials respectively.</li><li>Two clear trends were noted in the final adjusted gamma-density values:<ul style="list-style-type: none"><li>A vertical alignment of density for fresh mineralisation and waste, i.e. the density is invariable for changes in depth, and has a visual average of 2.9 t/m<sup>3</sup>, which was assigned to the fresh mineralisation and waste.</li><li>A gradational, inverse relationship between density and depth (as the depth decreases, the density increases) for oxide and transitional material. There was no relationship noted between density and lithology. The densities were averaged by depth for the oxide and transitional material to account for the positive relationship between density and depth.</li></ul></li><li>The density assignment was calculated as follows:<ul style="list-style-type: none"><li>An average for each 5 m bench depth was calculated for the caliper-filtered, porosity-adjusted data.</li><li>An order-relation adjustment that ensured that the average density for each successively shallower bench was equal to or less than the bench below it.</li><li>As no data existed for oxide and transitional syenite, and porphyry material, the proportion from visual fresh values were used to reduce the density against waste and mineralisation, as follows:<ul style="list-style-type: none"><li>Syenite: 2.65/2.9</li><li>Porphyry: 2.75/2.9</li></ul></li></ul></li><li>The values assigned for oxide and transitional material by bench</li><li>Caliper filtered, pore and order relation adjusted density averages assigned by bench for oxide and transitional material only are shown below:</li></ul>																																																																			
		<table><tr><td>bench_top_5m</td><td>Mineralisation density value assigned</td><td>Syenite density value assigned</td><td>Porphyry density value assigned</td></tr><tr><td>&gt;=400</td><td>1.62</td><td>1.48</td><td>1.54</td></tr><tr><td>395</td><td>1.70</td><td>1.55</td><td>1.61</td></tr><tr><td>390</td><td>1.86</td><td>1.70</td><td>1.76</td></tr><tr><td>385</td><td>1.92</td><td>1.75</td><td>1.82</td></tr><tr><td>380</td><td>1.93</td><td>1.76</td><td>1.83</td></tr><tr><td>375</td><td>1.95</td><td>1.78</td><td>1.85</td></tr><tr><td>370</td><td>1.95</td><td>1.78</td><td>1.85</td></tr><tr><td>365</td><td>2.08</td><td>1.90</td><td>1.97</td></tr><tr><td>360</td><td>2.10</td><td>1.92</td><td>1.99</td></tr><tr><td>355</td><td>2.25</td><td>2.06</td><td>2.13</td></tr><tr><td>350</td><td>2.25</td><td>2.06</td><td>2.13</td></tr><tr><td>345</td><td>2.47</td><td>2.26</td><td>2.34</td></tr><tr><td>340</td><td>2.47</td><td>2.26</td><td>2.34</td></tr><tr><td>335</td><td>2.47</td><td>2.26</td><td>2.34</td></tr><tr><td>&lt;=330</td><td>2.47</td><td>2.26</td><td>2.34</td></tr></table>	bench_top_5m	Mineralisation density value assigned	Syenite density value assigned	Porphyry density value assigned	>=400	1.62	1.48	1.54	395	1.70	1.55	1.61	390	1.86	1.70	1.76	385	1.92	1.75	1.82	380	1.93	1.76	1.83	375	1.95	1.78	1.85	370	1.95	1.78	1.85	365	2.08	1.90	1.97	360	2.10	1.92	1.99	355	2.25	2.06	2.13	350	2.25	2.06	2.13	345	2.47	2.26	2.34	340	2.47	2.26	2.34	335	2.47	2.26	2.34	<=330	2.47	2.26	2.34			
bench_top_5m	Mineralisation density value assigned	Syenite density value assigned	Porphyry density value assigned																																																																		
>=400	1.62	1.48	1.54																																																																		
395	1.70	1.55	1.61																																																																		
390	1.86	1.70	1.76																																																																		
385	1.92	1.75	1.82																																																																		
380	1.93	1.76	1.83																																																																		
375	1.95	1.78	1.85																																																																		
370	1.95	1.78	1.85																																																																		
365	2.08	1.90	1.97																																																																		
360	2.10	1.92	1.99																																																																		
355	2.25	2.06	2.13																																																																		
350	2.25	2.06	2.13																																																																		
345	2.47	2.26	2.34																																																																		
340	2.47	2.26	2.34																																																																		
335	2.47	2.26	2.34																																																																		
<=330	2.47	2.26	2.34																																																																		
	<i>The bulk density for bulk material must have been measured by methods that adequately account for void</i>	<ul style="list-style-type: none"><li>Void space has been accounted for in the industry-standard, immersion method core density determination process.</li><li>The data were adjusted for measured porosity in fresh Ganymede and Doublejay material utilising borehole magnetic resonance (BMR) data. The</li></ul>																																																																			

Criteria	JORC Code explanation	Commentary
	<i>spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i>	<p>BMR data quantitatively assesses the porosity of the material logged, from which the percentage of porosity was removed to provide an in-situ, dry bulk density.</p> <ul style="list-style-type: none"> <li>A porosity of 5% and 3% was applied to the density of fresh material respectively for Ganymede and Doublejay.</li> <li>Porosity values of 10% for oxide and 7.5% for transitional were assumed</li> </ul>
	<i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i>	<ul style="list-style-type: none"> <li>For gamma-density, the data are quantitative and independent of sample weight, and have been analysed by modelled material types.</li> <li>For core immersion-method density data, no relationship to sample weight has been determined, and is expected to be unrelated, as the core density data show little variation with lithological types.</li> </ul>
<b>Classification</b>	<i>The basis for the classification of the Mineral Resources into varying confidence categories.</i>	<ul style="list-style-type: none"> <li>The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on: <ul style="list-style-type: none"> <li>Drill density data</li> <li>Geological understanding</li> <li>Quality of gold assay grades</li> <li>Continuity of gold grades</li> <li>Economic potential for mining.</li> </ul> </li> <li>For Indicated Mineral Resources, statistical consideration has been employed to assess the grade estimate quality in considering large, contiguous, and coherent zones of blocks form zones where: <ul style="list-style-type: none"> <li>Large areas are formed that have been grade control drilled, but also extending out to where drill hole spacing reaches 20 m to 20 m max.</li> <li>Estimation was chiefly undertaken in search passes of 1 and 2.</li> <li>Number of samples was predominantly near the optimum.</li> <li>Slope of regression formed large volumes of &gt; 0.4 with cores of 0.6.</li> </ul> </li> <li>For Measured Mineral Resources, large contiguous volumes were required that that had reached a GC drill spacing of 10 m by 10 m, or not more than 20 m by 20 m near the GC drilling areas and where very high grade continuity was established.</li> <li>The remainder of the mineralisation was classified as Inferred.</li> </ul>
	<i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i>	<ul style="list-style-type: none"> <li>All factors the Competent Person has deemed relevant to the MRE have been incorporated into the classification of Mineral Resources.</li> </ul>
	<i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i>	<ul style="list-style-type: none"> <li>The result appropriately reflects the Competent Person's view of the deposit.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of Mineral Resource estimates.</i>	<ul style="list-style-type: none"> <li>Internal audits were completed by Dacian, which verified the technical inputs, methodology, parameters and results of the estimate.</li> </ul>
<b>Discussion of relative accuracy/confidence</b>	<i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative</i>	<ul style="list-style-type: none"> <li>The accuracy of the MRE is communicated through the classification assigned to the deposit. The MRE has been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this table.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>accuracy and confidence of the estimate.</i>	
	<i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i>	<ul style="list-style-type: none"> <li>The MRE statement relates to a global estimate of in-situ tonnes and grade.</li> </ul>
	<i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i>	<ul style="list-style-type: none"> <li>Production figures are not able to be reconciled with confidence, as Jupiter material is blended prior to crushing at the Jupiter mill with Mount Marven and previously Westralia UG when it was operating until mid-2020.</li> </ul>

## Mt Marven

### Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
<b>Sampling techniques</b>	<p><i>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i></p>	<ul style="list-style-type: none"> <li>Surface reverse circulation (RC) drilling chips and diamond drilling (DD) core informed the Mt Marven Mineral Resource estimate (MRE) update.</li> <li>All DD and 80% of RC holes that intersected mineralisation were drilled by Dacian from 2019.</li> <li>Surface RC holes were angled to intersect the targeted mineralised zones at optimal angles.</li> <li>In-pit RC holes were variably angled and vertical to target mineralised zones at optimal angles, and to fit around historic workings.</li> <li>For historical RC drilling, where available the original logs and laboratory results that are in the central SQL Server database are retained by Dacian as either original hard copies or as scanned copies.</li> <li>94MCRC (107 holes) and 95MCRC holes (29 holes) was undertaken by Dominion Mining Limited using RC rigs from Ausdrill, Robinsons and Drillex. 1m samples were collected using a riffle splitter. Only samples expected to be anomalous were sent to the onsite lab for analysis.</li> <li>MM holes (32 holes) were drilled during 1987-1988 by Taurus Resources. No information exists regarding drill contractor or sample methodologies; however, after review of the assay table in the database, all samples were taken at 1m intervals.</li> <li>The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.</li> </ul>
	<p><i>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</i></p>	<ul style="list-style-type: none"> <li>Dacian surface diamond core was sampled as half core at 1m intervals or to geological contacts. To ensure representative sampling, half core samples were always taken from the same side of the core.</li> <li>Dacian RC holes are sampled over the entire length of hole. Dacian RC drilling was sampled at 1m intervals via an on-board cone splitter</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling -problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</i>	<ul style="list-style-type: none"> <li>Dacian surface diamond core was sampled as half core at 1m intervals or to geological contacts. Sampling did not cross geological boundaries. Samples were cut in half, sampled into lengths in sample bags to achieve approximately 3kg, and submitted to a contract laboratory for crushing and pulverising to produce either a 40g or 50g charge for fire assay.</li> <li>Dacian surface RC holes are sampled over the entire length of hole. Dacian RC drilling was sampled at 1m intervals via an on-board cone splitter to achieve approximately 3kg samples. Samples were then submitted to a contract laboratory for crushing and pulverising to produce either a 40g or 50g charge for fire assay.</li> <li>Dacian in pit RC holes are sampled over the entire length of hole on 1m intervals via an on-board cone splitter to achieve approximately 3kg samples. Prior to December, 2020, samples were submitted to a contract laboratory for crushing and pulverising to produce either a 40g or 50g charge for fire assay. After December, 2020, samples were submitted to the on-site laboratory for Pulverise and Leach (PAL) analyses using a 600g subsample.</li> </ul>
<b>Drilling techniques</b>	<i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i>	<ul style="list-style-type: none"> <li>Drilling that informed the Mineral Resource estimate (MRE) included 1,688 reverse circulation (RC) holes for 75,966 m and 7 surface diamond drill (DD) holes for 1,945.45 m.</li> <li>Drilling that intersected modelled mineralisation included 1,119 reverse circulation (RC) holes for 44,501 m and 2 diamond drill (DD) holes for 466.35 m.</li> <li>Rotary Air Blast drilling (RAB) and was used to guide the geological and mineralisation interpretation, but the data were not used in for grade estimation.</li> <li>For Dacian RC holes, a 5¼" face sampling hammer bit was used except to drill Dacian Mt Marven South holes, where a 5" face sampling hammer was used.</li> <li>Dacian Diamond drilling was mostly carried out with NQ2 sized equipment, along with minor HQ3 and PQ2, using standard tube. Surface drill core was orientated using a Reflex orientation tool.</li> <li>Dominion holes (94MCRC and 95MCRC holes) were drilled with RC rigs utilising face-sampling hammers for maximum sample return.</li> <li>Other than the drill type being RC, nothing is known about the MM historic holes.</li> </ul>
<b>Drill sample recovery</b>	<i>Method of recording and assessing core and chip sample recoveries and results assessed.</i>	<ul style="list-style-type: none"> <li>Recoveries from Dominion drilling, while not recorded in the database, were noted as being generally greater than 60%.</li> <li>Recoveries from historical MM holes are unknown.</li> <li>Recoveries from Dacian diamond drilling were measured and recorded into the database.</li> <li></li> <li></li> </ul>
	<i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i>	<ul style="list-style-type: none"> <li>Dacian RC holes were drilled with a powerful rig with compressor and booster compressor to ensure enough air to maximise sample recovery. The splitter is cleaned at the end of each rod, to ensure that efficient sample splitting. The weight of each sample split is monitored. Drilling is stopped if the sample split size changes significantly.</li> <li>Dacian RC drilling sample volumes, quality and recoveries are monitored by the supervising geologist, with a geologist always supervising RC drilling activities to ensure good recoveries</li> </ul>
	<i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i>	<ul style="list-style-type: none"> <li>In Dacian, drilling no relationship has been observed between sample recovery and grade.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Logging</b>	<i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i>	<ul style="list-style-type: none"> <li>• All diamond drill holes were logged for recovery, RQD, geology and structure. For Dacian drilling, diamond core was photographed both wet and dry.</li> <li>• All RC holes were logged for geology, alteration, and visible structure.</li> <li>• All RC chip trays were photographed.</li> <li>• All drill holes were logged in full.</li> <li>• RC drilling was logged by passing a portion of each sampled metre into a sieve to remove rock flour from coarse chips, the chips are then washed and placed into metre marked chip trays for logging. Where the material type does not allow for the recovery of coarse rock chips the rock flour is retained as a record. The un-sieved sample is also observed for logging purposes. The detail is considered common industry practice and is at the appropriate level of detail to support mineralization studies.</li> <li>• Dacian's DD core was photographed wet and dry, and geotechnically logged to industry standards.</li> <li>• All Dominion RC holes have lithological, weathering and mineralisation information stored in the database.</li> <li>• For historical RC drilling, where available the original logs and laboratory results are retained by Dacian as either original hard copies or as scanned copies.</li> <li>• The Competent Person is satisfied that the logging detail supports the MRE.</li> </ul>
	<i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i>	<ul style="list-style-type: none"> <li>• All holes are logged qualitatively by geologists familiar with the geology and control on the mineralisation for various geological attributes including weathering, primary lithology, primary &amp; secondary textures, colour and alteration.</li> <li>• For Dacian drilling, diamond core was photographed both wet and dry. For RC drilling chip trays are photographed. Diamond core is retained on site.</li> </ul>
	<i>The total length and percentage of the relevant intersections logged.</i>	<ul style="list-style-type: none"> <li>• All diamond drill holes were logged for recovery, RQD, geology, and structure. Structural measurements are taken using a kenometer to record alpha and beta angles relative to a bottom of hole line marked on the oriented core. The quality of the bottom of hole orientation line is also recorded.</li> <li>• All Dacian drill holes were logged in full, from start of hole to bottom of hole.</li> </ul>
<b>Sub-sampling techniques and sample preparation</b>	<i>If core, whether cut or sawn and whether quarter, half or all core taken.</i>	<ul style="list-style-type: none"> <li>• Core was cut in half using an automatic core saw at either 1m intervals or to geological contacts; core samples were collected from the same side of the core where orientations were completed.</li> </ul>
	<i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i>	<ul style="list-style-type: none"> <li>• Dacian RC samples were collected via on-board cone splitters. Most samples were dry, any wet samples are recorded as wet, this data is then entered into the sample condition field in the drillhole database.</li> <li>• The RC sample was split using the cone splitter to give an approximate 3kg sample. The remainder was collected into a plastic sack as a retention sample. At the grain size of the RC chips, this method of splitting is considered appropriate.</li> <li>• Dominion historical RC samples were collected at the rig using riffle splitters if dry while wet samples were bagged for later splitting. Samples condition was not recorded for a majority of the historic sampling. For historic RC drilling, information on the QAQC programs used is limited but acceptable with original batch reports having been reviewed and retained by Dacian.</li> <li>• The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i>	<ul style="list-style-type: none"> <li>For RC drilling, sample quality was maintained by monitoring sample volume and by cleaning splitters on a regular basis. If due to significant groundwater inflow or drilling limitations sample quality became degraded (consecutive intervals of wet sample or poor sample recovery), the RC hole was abandoned.</li> </ul>
	<i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i>	<ul style="list-style-type: none"> <li>For Dacian RC drilling, RC field duplicates were taken from the on-board cone splitter at 1 in 50 or 1 in 25 for exploration and infill drilling respectively.</li> <li>Externally prepared Certified Reference Materials were inserted within the sample stream for QAQC.</li> <li>For Dacian samples analysed by fire assay, sample preparation was conducted by a contract, National Association of Testing Authorities (NATA) Australia accredited laboratory. After drying, the sample is subject to a primary crush, then pulverised to 85% passing 75µm.</li> <li>For Dacian samples analysed by PAL, dried samples were subjected to a primary and secondary crush to 90% passing 3 mm, before being cone split into a 600g subsample. The 600g sample was then pulverised to 90% passing 80µm and simultaneously leached for 60 minutes in a PAL machine using 2kg of grinding media, 1 Litre of water and 2 x 10g cyanide tablets (75% NaCN). The leached solution was separated by centrifuge and analysed by AAS.</li> <li>No information is available for the historic holes.</li> <li></li> </ul>
	<i>Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.</i>	<ul style="list-style-type: none"> <li>For Dacian exploration DD drilling field duplicates were not taken.</li> <li>For Dacian RC drilling, field duplicates are generally taken a 1 in 25 samples.</li> </ul>
	<i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i>	<ul style="list-style-type: none"> <li>Sample sizes are considered appropriate to correctly represent the gold mineralisation based on the style of mineralisation, the thickness and consistency of the intersections, the sampling methodology and assay value ranges for gold.</li> </ul>
<b>Quality of assay data and laboratory tests</b>	<i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i>	<ul style="list-style-type: none"> <li>For Dacian surface drilling, and in pit RC drilling prior to December 2020, the analytical technique used was a 40g or 50g lead collection fire assay and analysed by Atomic Absorption Spectrometry (AAS). This is a full digestion technique. Samples were analysed at Bureau Veritas in Perth or Kalgoorlie, Western Australia. This is a commonly used method for gold analysis and is considered appropriate for this project.</li> <li>For in pit RC drilling after December 2020, samples were analysed at the onsite SGS laboratory, using a Pulverise and Leach (PAL) technique which analyses a 600g subsample. The leached solution is analysed by AAS. PAL is a partial digestion method.</li> <li>The majority (117 of 136) of the Dominion holes were analysed at their onsite lab using fire assay (50g). The remaining 19 holes were assayed using fire assay at Analabs.</li> <li>No information regarding the analysis of the 32 MM series holes is known.</li> <li>For Dacian drilling analysed at Bureau Veritas, sieve analysis was carried out by the laboratory to ensure the grind size of 85% passing 75µm was being attained.</li> <li>For Dacian surface RC and diamond drilling, QAQC procedures involved the use of certified reference materials, standards (1 in 20) and blanks (1 in 50). For diamond drilling additional coarse blanks and standards are submitted around observed mineralisation.</li> <li>For Dacian in-pit RC drilling, QAQC procedures involved the use of certified reference materials (1 in 20) and blanks (1 in 20).</li> <li>Results were assessed as each laboratory batch was received and were</li> </ul>



Criteria	JORC Code explanation	Commentary
		<p>acceptable in all cases.</p> <ul style="list-style-type: none"> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>No QAQC data has been reviewed for historic drilling, although mine production and twinned drill holes have validated drilling results. The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.</li> </ul>
	<i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i>	<ul style="list-style-type: none"> <li>Quantitative geophysical data, most notably wireline gamma-density data, were captured by Surtech using sonde serial number 9239B, with logging by unit SL33, and a caesium radioactive source.</li> <li>Data were captured from MVGC_395_0035 and MVGC_395_0064 on 18/02/2021, entirely logging transitional material.</li> <li>To adjust the gamma-density values by porosity, the values of 10% for oxide, 7.5% for transitional and 5% for fresh were applied based on analysis from Ganymede wireline logging, which incorporated borehole magnetic resonance (BMR) data to quantitatively measure moisture or porosity.</li> <li>Geophysical sondes used in the wireline data capture were calibrated against known density standards and repeat logging of a calibration hole at Mt Morgans.</li> <li>Single and three arm callipers were used in-hole to identify areas where blowouts and significant aberrations in the hole rugosity were encountered; any deviations from within 20% of the nominal hole diameter were removed from the analysis.</li> <li>The wireline gamma-density data were compared to the core density for transitional material, which showed that acceptable correlations existed for inclusion of either dataset in the MRE.</li> </ul>
	<i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i>	<ul style="list-style-type: none"> <li>Certified reference materials demonstrate that sample assay values are accurate.</li> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>Commercial laboratories used by Dacian were audited in April 2021 by the Competent Person. The laboratory is monitored regularly by Dacian through QAQC practices, and strong communication channels are in place for data quality.</li> <li>The on-site laboratory was visited by the Competent Person twice in December 2020, is monitored regularly by Dacian through QAQC practices, and strong communication channels are in place for data quality.</li> <li>Umpire laboratory test work was completed in 2019 over mineralised intersections with good correlation of results.</li> <li>Umpire testwork of grade control pulp duplicate samples from December 2020 through June 2021 between PAL/LW_AAS and FA40AAS methods showed high correlation.</li> <li></li> </ul>
<b>Verification of sampling and assaying</b>	<i>The verification of significant intersections by either independent or alternative company personnel.</i>	<ul style="list-style-type: none"> <li>Significant intersections were visually field verified by company geologists.</li> </ul>
	<i>The use of twinned holes.</i>	<ul style="list-style-type: none"> <li>In areas of grade control, the drill spacing is at 10 m x 5 m, and numerous examples exist of mineralisation showing repeated visual continuity for the estimated volumes.</li> <li>The mineralisation at Mt Marven South is analogous to the grade control areas.</li> <li>Variogram models for the grade continuity at Mt Marven incorporate a moderately high nugget and a short-range first structure that accounts for a high proportion of the variance. Therefore, for statistical confidence, twin drilling at spacings closer than 5 m are unlikely to be valuable for informing the repeatability of the grade mineralisation, and instead the high visual continuity and density of the drill spacing has informed the confidence in the estimate.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i>	<ul style="list-style-type: none"> <li>• Prior to 2021, primary data was collected into a custom logging Excel spreadsheet and then imported into a DataShed drillhole database. The logging spreadsheet included validation processes to ensure the entry of correct data.</li> <li>• From January 2021, primary data was collected into LogChief logging software by MaxGeo and then imported into a Data Shed drillhole database. Logchief has internal data validation.</li> <li>•</li> </ul>
	<i>Discuss any adjustment to assay data.</i>	<ul style="list-style-type: none"> <li>• Assay values that were below detection limit are stored in the database in this form, but are adjusted to equal half of the detection limit value for grade estimates. The following records were set to half detection limit:</li> <li>• Negative below detection limit assays</li> <li>• Zeros</li> <li>• Nulls</li> <li>• Unsampled intervals</li> <li>• Any negatives below -1 were set to null, as these represent lab error codes such as samples not received, samples destroyed in sample preparation, insufficient sample volume/weight etc.</li> </ul>
<b>Location of data points</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>• All Dacian hole collars were surveyed in MGA94 Zone 51 grid using differential GPS to 3cm accuracy.</li> <li>• Historic drill hole collar coordinates were tied to a local grid with subsequent conversion to MGA94 Zone 51.</li> <li>• Mine workings support the locations of historic drilling.</li> <li>• Dacian RC holes were down hole surveyed with a north seeking gyro tool at 30m intervals down the hole.</li> <li>• Dacian in-pit RC holes were down hole surveyed with a north seeking gyro tool, where the depth was greater than 30m.</li> <li>• Dacian DD holes were down hole surveyed with a north seeking gyro tool at 12m intervals down the hole.</li> <li>• Historic holes have no down hole survey information recorded.</li> </ul>
	<i>Specification of the grid system used.</i>	<ul style="list-style-type: none"> <li>• The grid system used is MGA94 Zone 51 grid.</li> </ul>
	<i>Quality and adequacy of topographic control.</i>	<ul style="list-style-type: none"> <li>• Topographic surfaces were prepared from detailed ground, mine and aerial surveys.</li> <li>• Material above all surfaces was coded in the model as depleted to ensure no mineralisation above these surfaces was included in the MRE.</li> <li>• The Competent Person is satisfied that the topographic control provides the quality required to report the Mineral Resources in accordance with the JORC Code.</li> </ul>
<b>Data spacing and distribution</b>	<i>Data spacing for reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>• For the Dacian RC exploration drilling at Mt Marven South, the nominal hole spacing of surface drilling is approximately 40x40m in the core of the mineralisation. Surrounding this is 80x120m.</li> <li>•</li> </ul>
	<i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i>	<ul style="list-style-type: none"> <li>• Dacian in-pit RC holes are drilled to a 10 x 5m spacing for grade control purposes, and which has informed the MRE.</li> <li>• The mineralised domains have sufficient continuity in both geology and grade to be considered appropriate for the Mineral Resource estimation procedures and classification applied under the JORC Code, and mining has further supported this.</li> </ul>
	<i>Whether sample compositing has been applied.</i>	<ul style="list-style-type: none"> <li>• Samples have been composited to 1m lengths in mineralised lodes for statistics and estimation.</li> <li>• Compositing was completed using a 'best-fit' method in Datamine software, which forces all samples to be included in one of the composites by adjusting composite lengths, while keeping it as close as possible to 1m.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Orientation of data in relation to geological structure</b>	<i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i>	<ul style="list-style-type: none"> <li>At Mt Marven South, Dacian RC holes were drilled at a planned bearing of 240° (azimuth) relative to MGA94 grid north at a planned dip of -60° which is approximately perpendicular to orientation of mineralised lodes within the Mt Marven open pit.</li> <li>The majority of surface and in-pit RC holes have been drilled to approximately 240° relative to MGA94 grid north, although due to the location of the historic pit, it was necessary to drill some holes towards approximately 60° relative to MGA94 grid north.</li> <li></li> </ul>
	<i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i>	<ul style="list-style-type: none"> <li>No orientation-based sampling bias has been identified in the data.</li> </ul>
<b>Sample security</b>	<i>The measures taken to ensure sample security.</i>	<ul style="list-style-type: none"> <li>Chain of custody is managed by Dacian. Samples are stored on site until collected for transport to the sample preparation laboratory in Kalgoorlie. Dacian personnel have no contact with the samples once they are picked up for transport. Tracking spreadsheet are used by Dacian personnel to track the progress of samples.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of sampling techniques and data.</i>	<ul style="list-style-type: none"> <li>Regular reviews of RC and DD sampling techniques are completed by the Dacian Senior Geologists and the Principal Resource Geologist, which concluded that sampling techniques are satisfactory.</li> <li>Commercial laboratories used by Dacian were audited in April 2021 by the Competent Person.</li> <li>The Competent Person visited the on-site contract laboratory twice in December 2020 to review processes. All laboratories were performing at and producing results for a standard required to report a MRE in accordance with the JORC Code.</li> <li>Review of Dacian QAQC data has been carried out by company geologists.</li> </ul>

## Mt Marven

### Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
<b>Mineral tenement and land tenure status</b>	<i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i>	<ul style="list-style-type: none"> <li>The Mt Marven project includes an active open pit gold mine. The Mt Marven project is located within Mining Leases M39/36 and M39/1107, 100% owned by Mt Morgans WA Mining Pty Ltd, a wholly owned subsidiary of Dacian Gold Ltd.</li> </ul>
	<i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.</i>	<ul style="list-style-type: none"> <li>The above tenements are all in good standing.</li> </ul>
<b>Exploration done by other parties</b>	<i>Acknowledgment and appraisal of exploration by other parties.</i>	<ul style="list-style-type: none"> <li>At Mt Marven, open pit mining occurred between 1989 and 1996, mostly when under operation by Dominion Mining. Exploration activities have been undertaken by Croesus Mining NL, Metex Resources NL, Homestake Gold, Barrick Gold and Placer Pty Ltd.</li> <li>A high proportion of the historic data is confirmed by recent drilling and is of a quality that, in the Competent Person's view, supports the MRE at the classification applied.</li> </ul>
<b>Geology</b>	<i>Deposit type, geological setting</i>	<ul style="list-style-type: none"> <li>The deposit is Archean lode gold style.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>and style of mineralisation.</i>	<ul style="list-style-type: none"> <li>The Mt Marven deposit consists of a series of lode structures within basalt flows and felsic rock intrusions, generally striking north to north-west and dipping approximately 60-75°. Mineralisation is associated with basalt hosted shearing and sheared intrusive contacts. Mineralised intervals typically display a combination of chlorite-carbonate to sericite-albite alteration with increased fine disseminated sulphide (predominantly pyrite with lesser chalcopyrite).</li> <li>Mineralisation within felsic rock intrusions is associated with quartz-carbonate veining with pyrite-chalcopyrite, and disseminated pyrite-chalcopyrite adjacent to the veins as a selvage. Mineralisation and host rocks within the nearby open pit confirm the geometry of the mineralisation.</li> <li>There are both visual and non-visual mineralization types at Mount Marven. Some mineralized shear zones are clearly visible within pit exposures and in drill chips, distinguished by goethitic to hematitic red defined zones that correlate with grades greater than 0.3g/t Au. Beneath the oxidized profile, higher gold grades are sometimes associated with higher disseminated pyrite and sometimes associated with silica-sericite +/- albite alteration.</li> </ul>
<b>Drill hole information</b>	<i>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length</i>	<ul style="list-style-type: none"> <li>All information that is material to the understanding of exploration and infill drilling results completed by Dacian is documented in the appendices (results table) that accompany this announcement.</li> <li></li> </ul>
	<i>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</i>	<ul style="list-style-type: none"> <li>No drill hole information related to new exploration drilling has been excluded.</li> <li></li> </ul>
<b>Data aggregation methods</b>	<i>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.</i>	<ul style="list-style-type: none"> <li>Exploration results are reported as length weighted averages of the individual sample intervals.</li> </ul>
	<i>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</i>	<ul style="list-style-type: none"> <li>No aggregation of data has been undertaken.</li> <li>Exploration results are not being reported.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>The assumptions used for any reporting of metal equivalent values should be clearly stated.</i>	<ul style="list-style-type: none"> <li>No metal equivalent values have been used</li> </ul>
<b>Relationship between mineralisation widths and intercept lengths</b>	<i>These relationships are particularly important in the reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>At Mt Marven, Dacian RC holes were drilled at a bearing of 240° (azimuth) relative to MGA94 grid north at a dip of -60°.</li> </ul>
	<i>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</i>	<ul style="list-style-type: none"> <li>The holes are drilled approximately perpendicular to the orientation of the expected trend of mineralisation</li> </ul>
	<i>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').</i>	<ul style="list-style-type: none"> <li>It is interpreted that true width is approximately 60-100% of down hole intersections depending on the orientation of the target which varies along strike and down dip.</li> </ul>
<b>Diagrams</b>	<i>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</i>	<ul style="list-style-type: none"> <li>Relevant diagrams have been included within the main body this ASX release.</li> </ul>
<b>Balanced Reporting</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>All Dacian hole collars were surveyed in MGA94 Zone 51 grid using differential GPS to within 3cm. Dacian holes were down-hole surveyed either with a north seeking gyroscopic tool at 30m intervals to 20cm accuracy.</li> <li></li> </ul>
	<i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
<b>Other substantive exploration data</b>	<i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i>	<ul style="list-style-type: none"> <li>In February 2020, downhole/wireline logging was undertaken by Surtech Systems to achieve gamma-density values at 10 cm spacing downhole for two grade control holes.</li> <li>The logging in counts-per-second (c/s) used a compensated density logging tool equipped with a Cs137 radioactive source.</li> <li>The CPS values were then converted to physical property values using calibrations determined specifically for each physical property parameter.</li> <li>The final data were supplied in a Logging ASCII Standard (CSV) file format.</li> <li>The type of instrument used was a 9239 Dual Density Instrument.</li> <li>Single and three arm callipers were used in-hole to identify areas where blowouts and significant aberrations in the hole rugosity were encountered; any deviations from within 20% of the nominal hole diameter (1,460 mm for RC) were removed from the analysis.</li> <li>The internal consistency of the downhole gamma-density data was demonstrated by repeat logging of against a calibration hole at Mt Morgans.</li> <li>Prior to mobilisation to site, the instrument was calibrated immediately against standard materials for density.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>• Calliper-filtered gamma density readings related to transitional mineralisation, and were compared against dry water immersion/Archimedes method core density samples from the diamond drill core.</li> <li>• A high correlation was shown between the gamma-density and core density determinations.</li> <li>• The wireline geophysical logging for a nearby deposit, Ganymede, also included borehole magnetic resonance (BMR) data, which quantitatively assesses the porosity of the material logged. The BRM logs were used to adjust the gamma-density values to a dry density.</li> </ul>
<b>Further work</b>	<p><i>The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).</i></p> <p><i>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i></p>	<ul style="list-style-type: none"> <li>• Infill MRE drilling; north, south and depth extensional drilling; RPEEE and LOM pit optimisation; UG review.</li> <li>• Estimate the highly discrete volumes of copper, as found in the base of the Mt Marven main pit in a small structure. Copper is assayed on grade control holes only, so during grade control model estimates, copper will be estimated to inform the expected recovery of gold. This will be further mitigated by a cyanide monitor, expected in place in Q1 FY2022.</li> </ul>

## Mt Marven

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
<b>Database integrity</b>	<i>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</i>	<ul style="list-style-type: none"> <li>• The data base has been systematically audited by a Dacian geologist. Original drilling records were compared to the equivalent records in the data base (where original records were available). Any discrepancies were noted and rectified by the data base manager.</li> </ul>
	<i>Data validation procedures used.</i>	<ul style="list-style-type: none"> <li>• Historic logs were located and additional logging information, particularly relating to weathering, was input into the database.</li> <li>• Ongoing database (DB) validation has been undertaken by a dedicated DB administrator communicating with geologists as the primary data sources and labs.</li> <li>• Extensive validation was undertaken by the database administrator.</li> <li>• Data were loaded into DataShed back-end SQL Server DB on a related data schema, providing a referentially integral database with primary key relations and look-up validation fields.</li> <li>• Additional validation completed in Datamine by Dacian geologists, with any validation issues relayed to DB administrator. All Dacian drilling data has been verified as part of a continuous validation procedure. Once a drill hole is imported into the data base reports of the collar, down-hole survey, geology, and assay data are produced. These are then checked by a Dacian geologist in geological software and any corrections are sent to the data base administrator to complete.</li> <li>• All data were checked for the following errors: <ul style="list-style-type: none"> <li>○ Duplicate drillhole IDs</li> <li>○ Missing collar coordinates</li> <li>○ Mis-matched or missing FROM or TO fields in the interval tables (assays, logging etc)</li> <li>○ FROM value greater than TO value in interval tables</li> <li>○ Non-contiguous sampling intervals</li> <li>○ Sampling interval overlap in the assay table</li> <li>○ The first sample in the interval file not starting at 0 m</li> </ul> </li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Interval tables with depths greater than the collar table EOH depth.</li> <li>Survey data were checked for large deviations in azimuth and dip between consecutive records, with none found.</li> </ul>
<b>Site visits</b>	<i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i>	<ul style="list-style-type: none"> <li>The Competent Person has made several site visits during 2020 and 2021, and has worked with the site-based geologists and mining engineers on the MRE and reconciliation processes relevant to this estimate.</li> <li>Inspection of the equipment used by Dacian's drilling contractor at the time of the visits found all operators working to a standard required to report a MRE in accordance with the JORC Code.</li> <li>The Competent Person visited the on-site laboratory twice in December to review processes, and each of the two National Association of Testing Authorities (NATA) accredited offsite contract laboratories in 2021. All laboratories were performing at and producing results for a standard required to report a MRE in accordance with the JORC Code.</li> </ul>
	<i>If no site visits have been undertaken indicate why this is the case.</i>	N/A
<b>Geological interpretation</b>	<i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i>	<ul style="list-style-type: none"> <li>The confidence in the geological interpretation in the central part of Mount Marven is very high, as it is based on mining exposure as well as a high drilling density. Visual confirmation of lode position and orientations has been observed and mapped in the Mount Marven operating open pit.</li> <li>In the area of the model which sits to the north or the south of the Mount Marven open pit, the confidence in the geological model is moderate, with a lower confidence resulting from the lower drilling density, and no existing mining.</li> <li>Ongoing infill drilling has confirmed geological and grade continuity.</li> </ul>
	<i>Nature of the data used and of any assumptions made.</i>	<ul style="list-style-type: none"> <li>Geological and structural logging and pit mapping have been used to assist identification and delineation of lithology and mineralisation.</li> <li>All lodes were treated as hard-boundaries for statistics and estimation.</li> </ul>
	<i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>Alternate interpretations may consider a different gold grade cut-off for the modelling of mineralisation, which may increase the tonnages and lower the grade for a reduced grade cut-off and vice-versa for an increased grade. Either of these are likely to result in a similar balance of metal.</li> <li>However, the volumes and grades mineralisation model has been demonstrated by open pit ore mark-outs at slightly higher-grade cut-offs, and which show that the boundaries of the mineralisation are suitable for the delineation of ore and waste.</li> </ul>
	<i>The use of geology in guiding and controlling Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>Mount Marven is hosted by massive to pillowed basalts, which are variably altered, sheared, oxidised and mineralised. There are a series of lode structures striking north and dipping at 60° – 75° to the east, shallowing in the east. Mineralised shear zones can be hematite altered in the oxide material and sericite/carbonate altered in fresh rock.</li> <li>The mineralisation was modelled with a relatively strict gold cut-off of 0.3 g/t Au, which has been confirmed as appropriate for the mining methods and ore markouts.</li> <li>Porphyry units are also mineralised at times but not visually recognisable as mineralised.</li> <li>The following objects were modelled that the Competent Person considers adequate to control the MRE. <ul style="list-style-type: none"> <li>Lodes: 67</li> <li>Porphyry dykes: 34</li> <li>Oxidation/weathering: base of complete oxidation (BOCO), top of fresh (TOFR)</li> </ul> </li> </ul>
	<i>The factors affecting continuity both of grade and geology.</i>	<ul style="list-style-type: none"> <li>The mineralised lodes at Mount Marven occur within a greater shear corridor and are hosted by both mafic and porphyry units suggesting gold mineralization continued post-intrusion. A WNW structure splits the mineralization between the historic northern and southern pit.</li> </ul>
<b>Dimensions</b>	<i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i>	<ul style="list-style-type: none"> <li>The Mount Marven Mineral Resource area extends over a SE-NW strike length of 900m (from 6811800 m N – 6812700 m N). It extends from 419350 mE to 420200 mE and extends from surface (approximately 425mRL) to 150mRL.</li> </ul>



Criteria	JORC Code explanation	Commentary
<b>Estimation and modelling techniques</b>	<i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i>	<ul style="list-style-type: none"> <li>Samples were composited to 1 m intervals ("composites") based on assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.</li> <li>High-grade top-cuts ranging from 4.9 – 20g/t Au were applied to the mineralisation domains following statistical analysis completed in Snowden Supervisor™ software.</li> <li>The top-cuts were kept at around 1% – 2% of the grade distribution for each lode.</li> <li>To model the spatial continuity of gold grades, variography was conducted in Supervisor 8.12. Statistics were length-weighted.</li> <li>Composite samples were declustered prior to variography for the statistical domains that contained lodes. A normal-score transform was applied to all data.</li> <li>In total, there are 62 individual mineralized lodes at Mount Marven. Due to lack of data in some lodes, they were grouped together based on lode orientation, statistics and location. The groups consist of the following: <ul style="list-style-type: none"> <li>Supergene envelope</li> <li>NNW-SSE lodes in north-western pit area</li> <li>NNW-SSE lodes in southern area</li> <li>N-S lodes in southern area</li> <li>NW-SE lodes in southern area</li> <li>Lode 6 – WNW structure splitting north and south pit</li> <li>Lode 25 – large, flat EW lode at northern end</li> </ul> </li> <li>Variograms were modelled for each of the above lode groups – seven in total. The majority of the variograms yielded poor experimental variograms, however, the modelling of short-range and long-range spherical structures was possible.</li> <li>Two spherical structures were modelled for each lode group.</li> <li>After variograms were modelled, a back-transform model was exported with Datamine rotations for use in Datamine parameter files. All variograms contained a low nugget when back-transformed, and typically a very high proportion of the variance accounted for in the short-range structure.</li> <li>Multi-block kriging neighbourhood analysis (KNA) was undertaken using Supervisor™ software to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE), slope of regression (SOR) and negative weights were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids.</li> <li>KNA found that a 5 x 5 x 5m block size was among the best statistics, and was considered most appropriate considering the drill density. KNA suggested using between 6 and 8 minimum samples and between 16 and 20 maximum samples. The maximum samples allowed per drillhole was set to 3 for all lodes. These parameters were set for the first pass.</li> <li>The KNA suggested adopting a search ellipse size matching the short-range structure in all cases, followed by the full range. The short range structure was often very short (6m to 28m in the major directions.)</li> <li>The second pass was the full range of the variogram, from 16.8 m to 57.6 m, and the minimum samples was 10 and maximum was 20. The third pass was 8x to 12x the full range of the variogram, from 60 m to 224 m, and the minimum samples was 4 and maximum was 8.</li> <li>The major direction was modelled with a ratio of between 1.2x to 2.3x the semi-major direction, and 2.3x 6.8x the minor direction. The latter of 6.8x ratio to the minor is an exception, relating to domain South, which incorporates the elongated lodes drilled to a lower density, and that have almost entirely been classified as Inferred.</li> <li>Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains. The technique is considered appropriate to allow the geostatistical continuity determined from variography to weight samples during estimation.</li> <li>Dynamic anisotropy was used only on the first pass to prevent wildly fluctuating large ellipses from weighting samples in high angles to the prevailing orientations of the lodes.</li> <li>Geological modelling was undertaken in Leapfrog Geo 6.0 software.</li> <li>Compositing, block modelling and grade estimation were undertaken using</li> </ul>



Criteria	JORC Code explanation	Commentary
		<p>Datamine™ RM software.</p> <ul style="list-style-type: none"> <li>The estimation technique is appropriate to allow a locally adequate estimate for detailed mine planning and with a globally unbiased estimate per lode.</li> </ul>
	<i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i>	<ul style="list-style-type: none"> <li>Previous estimates provided lower overall tonnages with similar grades; however, these were completed prior to a large amount of additional drilling occurring and the introduction of density estimates based on quantitative data.</li> <li>Production figures are not able to be reconciled with confidence, as material from Mount Marven is blended together with Jupiter material prior to crushing at the Jupiter mill.</li> </ul>
	<i>The assumptions made regarding recovery of by-products.</i>	<ul style="list-style-type: none"> <li>No assumptions have been made regarding the recovery of by-products.</li> </ul>
	<i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i>	<ul style="list-style-type: none"> <li>To date, the elevated soluble copper grades at Mount Marven have not had an adverse impact on gold recovery through the mill.</li> <li>Analysis of the assays from the Pulp-and-Leach (Leachwell™) sample preparation method used by the site-based laboratory (provides an estimate of the cyanide-soluble portion of gold) against duplicate fire assays has shown a very high correlation, indicating that copper oxides are either not present or are in a form that does not impact gold recovery for the samples.</li> <li>Copper values have been averaged for each lode and included in the model to assist with planning.</li> </ul>
	<i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i>	<ul style="list-style-type: none"> <li>A parent block size of 5 m x 5 m x 5 m (X x Y x Z) was chosen, which was supported KNA and by drill hole spacing in KNA Y and Z directions. In the mine area, most of the deposit has been sampled at a density of 5 m x 10 m (on a rotated drilling grid to enable drilling perpendicular to the mineralisation direction) out to 80 m x 40 m on the fringes.</li> <li>Sub-celling to 1/5 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.</li> </ul>
	<i>Any assumptions behind modelling of selective mining units.</i>	<ul style="list-style-type: none"> <li>No assumptions have been made regarding SMUs.</li> </ul>
	<i>Any assumptions about correlation between variables.</i>	<ul style="list-style-type: none"> <li>While some copper assays have been taken, the dataset is not sufficient to enable correlation analysis.</li> </ul>
	<i>Description of how the geological interpretation was used to control the resource estimates.</i>	<ul style="list-style-type: none"> <li>Geology and grade are used to define the mineralisation lodes at Mount Marven. Within each lode, whose modelling is outlined above, the estimate was constrained to blocks within the lode wireframe using only top-cut composited samples from the corresponding lode.</li> </ul>
	<i>Discussion of basis for using or not using grade cutting or capping.</i>	<ul style="list-style-type: none"> <li>High-grade top-caps were applied to limit the influence of extreme outliers on the grade estimate. The top-caps were applied to the mineralisation domains following statistical analysis.</li> <li>The top-cuts were kept at around 1% – 2% of the grade distribution for each lode.</li> </ul>
	<i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i>	<ul style="list-style-type: none"> <li>Validation of the estimate was completed for the resource block models using numerical methods (histograms, CDFs and swath plots) and validated visually against the input raw drillhole data, declustered data, composites and blocks.</li> </ul>
<b>Moisture</b>	<i>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</i>	<ul style="list-style-type: none"> <li>Tonnages and grades have been estimated on a dry in situ basis.</li> </ul>
<b>Cut-off parameters</b>	<i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i>	<ul style="list-style-type: none"> <li>The reporting cut-off parameters were selected based on known open pit economic cut-off grades.</li> <li>The potential to extract mineralisation via underground mining methods has not been considered due to the depth of drilling and mineralisation.</li> <li>The MRE has been reported above a lower cut-off of 0.5 g/t Au and within a pit optimisation shell that allows the test of reasonable prospects of eventual economic extraction (RPEEE) for the undepleted MRE, and without the inclusion of dilution and ore loss, as the Competent Person considers these excessive economic modifying factors, whereas the other parameters are</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>based on in-situ material parameters or fixed costs:</p> <ul style="list-style-type: none"> <li>○ Gold price A\$2,400/oz</li> <li>○ Pit overall slope angles: oxide 44°, transitional, 49° fresh 63°</li> <li>○ Ore loss 0%</li> <li>○ Dilution 0%</li> <li>○ Mining costs (scaled by RL range as per actual rates): 425 m RL: A\$7.06/t – 360 m RL: A\$9.24/t</li> <li>○ Processing recovery 92% (oxide, transitional and fresh)</li> <li>○ Processing costs: oxide: A\$20.50/t; transitional A\$22.50/t; fresh A\$24.50/t</li> <li>○ Refining cost: A\$1.60/oz</li> <li>○ Gold royalty of 2.5%</li> <li>○ Discount rate: 5%</li> </ul>
<b>Mining factors or assumptions</b>	<i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i>	<ul style="list-style-type: none"> <li>• Dacian began open pit production at Mount Marven in July 2020. It is assumed that the same mining methods will be applicable for extraction of in-situ material included in this MRE update.</li> </ul>
<b>Metallurgical factors or assumptions</b>	<i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i>	<ul style="list-style-type: none"> <li>• The ore is processed at the proximal Jupiter Processing Facility, part of the MMGO. Recoveries achieved to date are 92.3%.</li> </ul>
<b>Environmental factors or assumptions</b>	<i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts,</i>	<ul style="list-style-type: none"> <li>• Mount Marven is an active open pit mine at the Mount Morgans Gold Operation with all requisite environmental approvals in place.</li> <li>• Waste rock is stored in a conventional waste dump.</li> </ul>

Criteria	JORC Code explanation	Commentary								
	<i>particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i>									
<b>Bulk density</b>	<i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i>	<ul style="list-style-type: none"><li>Density used to estimate tonnages for the MRE update has been determined from 891 core immersion method samples.</li><li>Surtech captured quantitative wireline gamma-density data from two holes at Mount Marven in early 2021, entirely within the transitional zone.</li><li>A high graphical correlation (compared visually) was shown between the gamma-density and core density determinations.</li><li>Density assignments by oxidation type for waste and mineralization, adjusted for porosity are shown below:</li><li><table><tr><th>Material</th><th>Density value (t/m<sup>3</sup>)</th></tr><tr><td>Oxide</td><td>1.9</td></tr><tr><td>Transitional</td><td>2.3</td></tr><tr><td>Fresh</td><td>2.8</td></tr></table></li></ul>	Material	Density value (t/m <sup>3</sup> )	Oxide	1.9	Transitional	2.3	Fresh	2.8
Material	Density value (t/m <sup>3</sup> )									
Oxide	1.9									
Transitional	2.3									
Fresh	2.8									
	<i>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i>	<ul style="list-style-type: none"><li>Void space has been accounted for in the industry-standard, immersion method core density determination process.</li><li>No borehole magnetic resonance data were captured, therefore the data were not porosity or moisture adjusted.</li><li>Instead, the data were adjusted for an assumed porosity by using the porosity adjustment by oxidation state for a nearby deposit with a similar weathering profile, Ganymede, which utilised borehole magnetic resonance (BMR) data. The BMR data quantitatively assesses the porosity of the material logged, from which the percentage of porosity was removed to provide an in-situ, dry bulk density.</li><li>Porosity values of 10% for oxide, 7.5% for transitional and 5% for fresh were applied to the density.</li></ul>								
	<i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i>	<ul style="list-style-type: none"><li>For gamma-density, the data are quantitative and independent of sample weight, and have been analysed by modelled material types.</li><li>For core immersion-method density data, no relationship to sample weight has been determined, and is expected to be unrelated, as the core density data show little variation with lithological types.</li></ul>								
<b>Classification</b>	<i>The basis for the classification of the Mineral Resources into varying confidence categories.</i>	<ul style="list-style-type: none"><li>The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:<ul style="list-style-type: none"><li>Drill density data</li><li>Geological understanding</li><li>Quality of gold assay grades</li><li>Continuity of gold grades</li><li>Economic potential for mining.</li></ul></li><li>Unclassified material:<ul style="list-style-type: none"><li>Part of lode 74, a flat lying oxide zone, located on the south-eastern extent of the model remained unclassified due to very limited drill density.</li></ul></li><li>Indicated Mineral Resources:<ul style="list-style-type: none"><li>Statistical consideration has been employed to assess the grade estimate quality in considering large, contiguous and coherent zones of blocks form zones where:</li><li>Large areas are formed that have been grade control drilled, but also extending out to where drill hole spacing reaches 20 m to 20 m max.</li><li>Estimation was chiefly undertaken in search passes of 1 and 2.</li></ul></li></ul>								

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>○ Number of samples was predominantly near the optimum.</li> <li>○ Slope of regression formed large volumes of &gt; 0.4 with cores of 0.6.</li> <li>• The remainder of the mineralisation was classified as Inferred.</li> </ul>
	<i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i>	<ul style="list-style-type: none"> <li>• All factors the Competent Person has deemed relevant to the MRE have been incorporated into the classification of Mineral Resources.</li> </ul>
	<i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i>	<ul style="list-style-type: none"> <li>• The result appropriately reflects the Competent Person's view of the deposit.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of Mineral Resource estimates.</i>	<ul style="list-style-type: none"> <li>• Internal audits were completed by Dacian, which verified the technical inputs, methodology, parameters and results of the estimate.</li> </ul>
<b>Discussion of relative accuracy/confidence</b>	<i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i>	<ul style="list-style-type: none"> <li>• The accuracy of the MRE is communicated through the classification assigned to the deposit. The MRE has been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this table.</li> </ul>
	<i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i>	<ul style="list-style-type: none"> <li>• The MRE statement relates to a global estimate of in-situ tonnes and grade.</li> </ul>
	<i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i>	<ul style="list-style-type: none"> <li>• Production figures are not able to be reconciled with confidence, as material from Mount Marven is blended with Jupiter material prior to crushing at the Jupiter mill.</li> </ul>

# Maxwell Bore

## Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
<b>Sampling techniques</b>	<i>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i>	<ul style="list-style-type: none"> <li>Surface Reverse Circulation (RC) chips informed both the Mineral Resource estimate (MRE).</li> </ul>
	<i>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</i>	<ul style="list-style-type: none"> <li>Dacian RC holes were sampled over the entire length of hole. Dacian RC drilling was sampled at 1m intervals via an on-board cone splitter.</li> </ul>
	<i>Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</i>	<ul style="list-style-type: none"> <li>Dacian RC holes within mineralisation were sampled on 1 m intervals in mineralisation via an on-board cone splitter (Dacian) mounted at the base of the cyclone to achieve a representative split of approximately 3 kg samples.</li> <li>Dacian surface RC holes were sampled over the entire length of hole.</li> <li>Dacian samples were submitted to a National Association of Testing Authorities (NATA) certified contract laboratory for crushing and pulverising to produce either a 40 g or 50 g charge for fire assay with an atomic absorption spectrometry (AAS) finish.</li> <li>Historic sampling practices are unknown.</li> </ul>
<b>Drilling techniques</b>	<i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i>	<ul style="list-style-type: none"> <li>Drilling that informed the modelling area of the MRE included 119 Reverse Circulation (RC) drill holes for 10,170 m, all of which intersected mineralisation and were used to estimate grades, while air core (AC) and rotary air blast (RAB) were used to guide, but not inform, the MRE.</li> <li>Dacian drilled 97% of the RC holes. The remainder were drilled in 1998 by an unknown company, but Homestake, the company whose drilling dates are closest to the involved in the area drilled RAB and AC in 1999.</li> <li>For Dacian RC holes, a face sampling hammer bit was used.</li> <li>Dominion holes were drilled with RC rigs utilising 5¼" to 5 ¾" face-sampling hammer bits for maximum sample return.</li> </ul>
<b>Drill sample recovery</b>	<i>Method of recording and assessing core and chip sample recoveries and results assessed.</i>	<ul style="list-style-type: none"> <li>Recoveries from historical holes are unknown.</li> <li>Recoveries from Dacian diamond drilling were measured and recorded into the database. Recovery was generally above 95% in fresh rock.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i>	<ul style="list-style-type: none"> <li>Dacian RC holes were drilled with a powerful rig with compressor and booster compressor to ensure enough air to maximise sample recovery. The splitter was cleaned at the end of each rod, to ensure that efficient sample splitting. The weight of each sample split was monitored. Drilling was stopped if the sample split size changed significantly.</li> <li>Dacian RC drilling activities, sample volumes, quality and recoveries were monitored by the supervising geologist to ensure good recoveries</li> <li>Sample splitters were cleaned on a regular basis.</li> </ul>
	<i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i>	<ul style="list-style-type: none"> <li>No relationship has been noted between sample recovery and grade.</li> </ul>
<b>Logging</b>	<i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i>	<ul style="list-style-type: none"> <li>All RC holes were logged for geology, alteration, and visible structure.</li> <li>All RC chip trays were photographed.</li> <li>All drill holes were logged in full.</li> <li>RC drilling was logged by passing a portion of each sampled metre into a sieve to remove rock flour from coarse chips, the chips are then washed and placed into metre marked chip trays for logging. The unsieved sample was also observed for logging purposes.</li> <li>For Dacian drilling, where the material type does not allow for the recovery of coarse rock chips the rock flour is retained as a record. The detail is considered common industry practice and is at the appropriate level of detail to support the MRE.</li> <li>For historical RC drilling, where available the original logs and laboratory results are retained by Dacian as either original hard copies or as scanned copies.</li> <li>The Competent Person is satisfied that the logging detail supports the MRE.</li> </ul>
	<i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i>	<ul style="list-style-type: none"> <li>All holes were logged qualitatively by geologists familiar with the geology and control on the mineralisation for various geological attributes including weathering, primary lithology, primary &amp; secondary textures, colour and alteration.</li> <li>The wireline geophysical data logged throughout Mt Morgans by Surtech systems in February 2021 is quantitative in nature. The data were used to assist the density determination of the MRE, although they were not taken from the Maxwell Bore deposit.</li> </ul>
	<i>The total length and percentage of the relevant intersections logged.</i>	<ul style="list-style-type: none"> <li>All drill holes were logged in full, from start of hole to bottom of hole.</li> </ul>
<b>Sub-sampling techniques and sample preparation</b>	<i>If core, whether cut or sawn and whether quarter, half or all core taken.</i>	<ul style="list-style-type: none"> <li>N/A</li> </ul>
	<i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i>	<ul style="list-style-type: none"> <li>The Dacian RC sample was split using the cone splitter to give an approximate 3kg sample. The remainder of the sample was collected into a plastic sack as a retention sample. At the grain size of the RC chips, this method of splitting is considered appropriate.</li> <li>Most samples were dry; any wet samples are recorded as wet; this data is then entered into the sample condition field in the drillhole database.</li> <li>At all times, an attempt was made to keep samples dry. If due to significant groundwater inflow or drilling limitations sample quality became degraded (consecutive intervals of wet sample or poor sample recovery), the RC hole was abandoned.</li> </ul>



Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>No information was available for historic RC samples.</li> </ul>
	<i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i>	<ul style="list-style-type: none"> <li>For RC drilling, the sub-sample preparation by splitting by cone splitters, which is an industry standard method of creating a representative split.</li> <li>Dacian RC sample preparation was conducted by a contract, NATA Australia accredited laboratory.</li> <li>After drying, samples were subject to a primary crush, then pulverised and homogenised to 85% passing 75µm before a 40 g or 50 g charge was scooped. This is an industry standard and appropriate method for preparing samples for fire assay.</li> </ul>
	<i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i>	<ul style="list-style-type: none"> <li>For Dacian RC drilling, RC field duplicates were taken from the on-board cone splitter at 1 in 50 or 1 in 25 for exploration and infill drilling respectively.</li> <li>Externally prepared Certified Reference Materials were inserted within the sample stream for QAQC.</li> <li>No information is available for the historic holes.</li> <li>The internal consistency of the wireline geophysical data was demonstrated by repeat logging of against a calibration hole at Mt Morgans. <ul style="list-style-type: none"> <li>The wireline geophysical data logged throughout Mt Morgans by Surtech systems in February 2021 was used to inform the MRE, although they were not taken from the Maxwell Bore deposit.</li> </ul> </li> <li>Prior to mobilisation to site, the instrument was calibrated immediately against standard materials for density.</li> <li>A high correlation was shown between the gamma-density and core density determinations where collected on the same holes.</li> </ul>
	<i>Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.</i>	<ul style="list-style-type: none"> <li>For Dacian RC drilling, field duplicates are generally taken a 1 in 25 samples.</li> </ul>
	<i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i>	<ul style="list-style-type: none"> <li>Sample sizes are considered appropriate to correctly represent the gold mineralisation based on the style of mineralisation, the thickness and consistency of the intersections, the sampling methodology and assay value ranges for gold.</li> </ul>
<b>Quality of assay data and laboratory tests</b>	<i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i>	<ul style="list-style-type: none"> <li>The analytical technique used was lead collection fire assay and analysed by Atomic Absorption Spectrometry (AAS) on a 40g or 50g for Dacian samples, and unknown weight for historic samples. This is a full digestion technique. This is a commonly used method for gold analysis and is considered appropriate for this project.</li> <li>For Dacian drilling analysed at Bureau Veritas, sieve analysis was carried out by the laboratory to ensure the grind size of 85% passing 75µm was being attained.</li> <li>Dacian QAQC procedures involved the use of certified reference materials, standards (1 in 20) and blanks (1 in 50). For diamond drilling additional coarse blanks and standards are submitted around observed mineralisation.</li> <li>Results were assessed as each laboratory batch was received and were acceptable in all cases.</li> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>Field duplicates for the four historical RC holes were inserted at a rate of ~1:35, which showed results of lower precision than Dacian samples but which were acceptable for inclusion in the MRE.</li> <li>The six standards inserted with the historical sample stream were unknown, while four of the five blanks were at detection limit, with one insignificantly above.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i>	<ul style="list-style-type: none"> <li>The wireline gamma-density data logged throughout Mt Morgans by Surtech systems in February 2021 were used to assist the density determination of the MRE, although they were not taken from the Maxwell Bore deposit.</li> <li>The logging in counts-per-second (c/s) used a compensated density logging tool equipped with a Cs137 radioactive source.</li> <li>The CPS values were then converted to physical property values using calibrations determined specifically for each physical property parameter.</li> <li>The final data were supplied in a Logging ASCII Standard (CSV) file format.</li> <li>Single and three arm callipers were used in-hole to identify areas where blowouts and significant aberrations in the hole rugosity were encountered; any deviations from within 20% of the nominal hole diameter were removed from the analysis.</li> </ul>
	<i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i>	<ul style="list-style-type: none"> <li>Certified reference materials demonstrate that sample assay values are accurate.</li> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>Commercial laboratories used by Dacian were audited in April 2021 by the Competent Person. The laboratory is monitored regularly by Dacian through QAQC practices, and strong communication channels are in place for data quality.</li> </ul>
<b>Verification of sampling and assaying</b>	<i>The verification of significant intersections by either independent or alternative company personnel.</i>	<ul style="list-style-type: none"> <li>Significant intersections were visually field verified by several company geologists.</li> </ul>
	<i>The use of twinned holes.</i>	<ul style="list-style-type: none"> <li>Recent have verified the intersections of historic mineralisation by either confirming the continuity of the mineralisation and geological interpretations or twinning the mineralisation.</li> </ul>
	<i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i>	<ul style="list-style-type: none"> <li>Prior to 2021, primary data was collected into a custom logging Excel spreadsheet and then imported into a DataShed drillhole database. The logging spreadsheet included validation processes to ensure the entry of correct data.</li> <li>From January 2021, primary data was collected into LogChief logging software by MaxGeo and then imported into a Data Shed drillhole database. Logchief has internal data validation.</li> <li></li> </ul>
	<i>Discuss any adjustment to assay data.</i>	<ul style="list-style-type: none"> <li>Assay values that were below detection limit are stored in the database in this form, but are adjusted to equal half of the detection limit value for grade estimates. The following records were set to half detection limit: <ul style="list-style-type: none"> <li>Negative below detection limit assays</li> <li>Zeros</li> <li>Nulls</li> <li>Unsampled intervals</li> </ul> </li> <li>Any negatives below -1 were set to null, as these represent lab error codes such as samples not received, samples destroyed in sample preparation, insufficient sample volume/weight etc.</li> </ul>
<b>Location of data points</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>All Dacian hole collars were surveyed in a local grid with transform parameters determined from surveyed pillars accurately surveyed in both the local "MTM2017" grid and MGA94 Zone 51 grid using differential GPS to 3cm accuracy.</li> <li>Historic drill hole collar coordinates were tied to a local Dominion Mining grid with subsequent conversion to MGA94 Zone 51.</li> <li>The down-hole survey method for 160 RC holes and 57 DD holes (including diamond tails) informing the resource is varied. Survey methods include Eastman SS, Reflex, Gyro, Camtek, Sunto, SingleShot, Devi Rapid, Azi Aligner and EMS.</li> <li>Open pit (OP) mine workings support the locations of historic drilling.</li> <li>UG DD and all Dacian RC holes were down hole surveyed with a north seeking gyro tool at &lt;=30m intervals down the hole.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>Specification of the grid system used.</i>	<ul style="list-style-type: none"> <li>The grid system used is the local “MTM2017” grid, with all collars and surveys transformed from either the MGA94 Zone 51 or historic Dominion grids.</li> </ul>
	<i>Quality and adequacy of topographic control.</i>	<ul style="list-style-type: none"> <li>Topographic surfaces were prepared from detailed ground, mine, and aerial surveys.</li> <li>Material above all surfaces was coded in the model as depleted to ensure no mineralisation above these surfaces was included in the MRE.</li> <li>The Competent Person is satisfied that the topographic control provides the quality required to report the Mineral Resources in accordance with the JORC Code.</li> </ul>
<b>Data spacing and distribution</b>	<i>Data spacing for reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported</li> <li>The drill hole spacing is highly variable as a result of the variable drilling and sampling techniques.</li> <li>Craic face samples have been taken on 4 m advances, which has created a highly clustered dataset when incorporated with the exploration and resource drilling. Therefore, samples were declustered prior to statistics, and the face samples were used in the first estimation pass only.</li> <li>The exploration RC holes are typically on 20 m sections, although they extend wider to 80 m sections outside of the modelled mineralisation.</li> </ul>
	<i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i>	<ul style="list-style-type: none"> <li>The mineralised domains have sufficient continuity in both geology and grade to be considered appropriate for the Mineral Resource estimation procedures and classification applied under the JORC Code.</li> </ul>
	<i>Whether sample compositing has been applied.</i>	<ul style="list-style-type: none"> <li>Samples have been composited to 1m lengths in mineralised lodes for statistics and estimation.</li> <li>Compositing was completed using a ‘best-fit’ method in Surpac software, which forces all samples to be included in one of the composites by adjusting composite lengths, while keeping it as close as possible to 1m.</li> </ul>
<b>Orientation of data in relation to geological structure</b>	<i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i>	<ul style="list-style-type: none"> <li>Surface holes were drilled entirely to the north and –60° dip, which is at an angle that approximates a perpendicular orientation of mineralised lodes.</li> </ul>
	<i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i>	<ul style="list-style-type: none"> <li>No orientation-based sampling bias has been identified in the data.</li> </ul>
<b>Sample security</b>	<i>The measures taken to ensure sample security.</i>	<ul style="list-style-type: none"> <li>Chain of custody was managed by the companies that owned the projects at the time, and no issues regarding historic sample security are known.</li> <li>Dacian samples were stored on site until collected for transport to the sample preparation laboratory in Kalgoorlie. Dacian personnel had no contact with the samples once they are picked up for transport. Tracking spreadsheets were used by Dacian personnel to track the progress of samples.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of sampling techniques and data.</i>	<ul style="list-style-type: none"> <li>Regular reviews of RC -sampling techniques were completed by the Dacian Senior Geologists and the Principal Resource Geologist, which concluded that sampling techniques are satisfactory.</li> <li>No audits or reviews have been documented for historic sampling</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>techniques, but the data have been reviewed by checking historic logging files with database records.</p> <ul style="list-style-type: none"> <li>Commercial laboratories used by Dacian were audited in April 2021 by the Competent Person.</li> <li>The Competent Person visited the on-site contract laboratory twice in December 2020 to review processes. All laboratories were performing at and producing results for a standard required to report a MRE in accordance with the JORC Code.</li> <li>Review of Dacian QAQC data has been carried out by company geologists.</li> </ul>

## Maxwell Bore

### Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
<b>Mineral tenement and land tenure status</b>	<i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i>	<ul style="list-style-type: none"> <li>The deposit is located within Mining Lease M39/1120, which is 100% owned by Mt Morgans WA Mining Pty Ltd, a wholly owned subsidiary of Dacian Gold Ltd.</li> </ul>
	<i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.</i>	<ul style="list-style-type: none"> <li>The above tenement is in good standing with no known security issues or impediments to obtaining a license to operate in the area.</li> </ul>
<b>Exploration done by other parties</b>	<i>Acknowledgment and appraisal of exploration by other parties.</i>	<ul style="list-style-type: none"> <li>Open pit and underground mining has occurred since the 1890s across Mt Morgans.</li> <li>Exploration activities at the deposit have been undertaken by Delta Gold, Indian Ocean Resources, Dominion Mining Ltd, Croesus, Forrest Gold, and Homestake.</li> </ul>
<b>Geology</b>	<i>Deposit type, geological setting and style of mineralisation.</i>	<ul style="list-style-type: none"> <li>The deposit is Achaean lode-gold-style, hosted in the Yilgarn Craton, Western Australia.</li> <li>The gold mineralisation has been deposited in lodes along a BIF-chert ridge, dominantly contained within the BIF-chert units, but also is emplaced along the contacts of the mafic material, forms larger halos around the units, and occasionally obliquely transects the BIF-chert units at low-angles resulting from unmeasured local structural controls.</li> <li>The BIF-chert units and lodes are dominantly buried beneath an extensive, shallow colluvial cover and laterite to the west, but also outcrop in parts of the central and north</li> <li>The variably deep weathering/oxidation profile extends 10 m – 50 m to the base of the completely oxidised surface, and ~25 m – 70 m to the top of fresh surface.</li> </ul>
<b>Drill hole information</b>	<i>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p>down hole length and interception depth</p> <p>hole length</p>	
	<p>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</p>	<ul style="list-style-type: none"> <li>• Exploration results are not being reported.</li> </ul>
<b>Data aggregation methods</b>	<p>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.</p>	<ul style="list-style-type: none"> <li>• Exploration results are not being reported.</li> <li>• No grade-weighting or other techniques have been applied to gold grades in figures.</li> </ul>
	<p>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</p>	<ul style="list-style-type: none"> <li>• Exploration results are not being reported.</li> </ul>
	<p>The assumptions used for any reporting of metal equivalent values should be clearly stated.</p>	<ul style="list-style-type: none"> <li>• No metal equivalent values have been used</li> </ul>
<b>Relationship between mineralisation widths and intercept lengths</b>	<p>These relationships are particularly important in the reporting of Exploration Results.</p>	<ul style="list-style-type: none"> <li>• The drilling angle of holes is entirely to the north, intersecting the moderate to steep southerly dip at a high angle.</li> <li>• Exploration results are not being reported.</li> </ul>
	<p>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</p>	<ul style="list-style-type: none"> <li>• The holes are drilled approximately perpendicular to the orientation of the plane of mineralisation.</li> </ul>
	<p>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').</p>	<ul style="list-style-type: none"> <li>• It is interpreted that true width is approximately 60-100% of down hole intersections depending on the orientation of the target which varies along strike and down dip.</li> </ul>
<b>Diagrams</b>	<p>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</p>	<ul style="list-style-type: none"> <li>• Relevant diagrams have been included within the main body this ASX release.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Balanced Reporting</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>All hole collars were surveyed in MGA94 Zone 51 grid.</li> <li>Dacian holes used a differential GPS to within 3cm accuracy. Dacian holes were down-hole surveyed either with a north seeking gyroscopic tool at 30m intervals to 20cm accuracy.</li> <li>The method of collar and down-hole survey for historic drill hole collar coordinates is unknown.</li> </ul>
	<i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
<b>Other substantive exploration data</b>	<i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i>	<ul style="list-style-type: none"> <li>The wireline geophysical data logged throughout Mt Morgans by Surtech systems in February 2021 was used to inform the MRE, although they were not taken from the Maxwell Bore deposit.</li> </ul>
<b>Further work</b>	<i>The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i>	<ul style="list-style-type: none"> <li>OP optimisation of the MRE is planned, which will provide guidance on the locations of infill drilling to permit a MRE update.</li> </ul>

## Maxwell Bore

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
<b>Database integrity</b>	<i>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</i>	<ul style="list-style-type: none"> <li>The data base has been systematically audited by Dacian geologists and database-specialist consultant geologists. Original drilling records were compared to the equivalent records in the data base (where original records were available). Any discrepancies were noted and rectified by the data base manager.</li> </ul>
	<i>Data validation procedures used.</i>	<ul style="list-style-type: none"> <li>Historic logs were located and additional logging information, particularly relating to weathering, was input into the database.</li> <li>Ongoing database (DB) validation has been undertaken by a dedicated DB</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>administrator communicating with geologists as the primary data sources and labs.</p> <ul style="list-style-type: none"> <li>• Extensive validation was undertaken by the database administrator.</li> <li>• Data were loaded into DataShed back-end SQL Server DB on a related data schema, providing a referentially integral database with primary key relations and look-up validation fields.</li> <li>• Additional validation completed in Datamine by Dacian geologists, with any validation issues relayed to DB administrator. All Dacian drilling data has been verified as part of a continuous validation procedure. Once a drill hole is imported into the data base reports of the collar, down-hole survey, geology, and assay data are produced. These are then checked by a Dacian geologist in geological software and any corrections are sent to the data base administrator to complete.</li> <li>• All data were checked for the following errors: <ul style="list-style-type: none"> <li>○ Duplicate drillhole IDs</li> <li>○ Missing collar coordinates</li> <li>○ Mis-matched or missing FROM or TO fields in the interval tables (assays, logging etc)</li> <li>○ FROM value greater than TO value in interval tables</li> <li>○ Non-contiguous sampling intervals</li> <li>○ Sampling interval overlap in the assay table</li> <li>○ The first sample in the interval file not starting at 0 m</li> <li>○ Interval tables with depths greater than the collar table EOH depth.</li> </ul> </li> <li>• Survey data were checked for large deviations in azimuth and dip between consecutive records, with none found.</li> </ul>
<b>Site visits</b>	<i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i>	<ul style="list-style-type: none"> <li>• The Competent Person has made a site visit during 2020, and has worked with the site-based geologists on the MRE.</li> <li>• Inspection of the equipment used by Dacian's drilling contractor at the time of the visit found all operators working to a standard required to report the MREs in accordance with the JORC Code.</li> <li>• The Competent Person visited the on-site laboratory twice in December to review processes, and each of the two National Association of Testing Authorities (NATA) accredited offsite contract laboratories in 2021. All laboratories were performing at and producing results for a standard required to report the MREs in accordance with the JORC Code.</li> </ul>
	<i>If no site visits have been undertaken indicate why this is the case.</i>	<ul style="list-style-type: none"> <li>• N/A</li> </ul>
<b>Geological interpretation</b>	<i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i>	<ul style="list-style-type: none"> <li>• The confidence in the geological interpretations for the MRE is moderate to high, as the drilling density is 20 m by 20 m in most of the deposit, and the angle of intersection of the mineralisation is perpendicular.</li> </ul>
	<i>Nature of the data used and of any assumptions made.</i>	<ul style="list-style-type: none"> <li>• Geological logging has been used to assist identification and delineation of lithology, weathering and mineralisation.</li> <li>• The following mineralisation modelling techniques were incorporated into the modelling, which has formed assumptions regarding the continuity: <ul style="list-style-type: none"> <li>○ Logging of weathering was used to model base-of-complete-oxidation (BOCO) and top-of-fresh (TOFR) surfaces. Isolated peaks and troughs created by variable logging were ignored for a smoother surface that is assumed to be less likely to be influenced by subjective differences or error in the logging.</li> <li>○ Any internal waste units not assayed across several metres were excluded from mineralisation wireframes to provide coherent geometries.</li> <li>○ All lodes were modelled above a moderately strict cut-off of 0.5g/t, except for the retention of continuity, where lower grades were allowed.</li> <li>○ Boundary strings were utilised to control the strike and down dip extents beyond the last known drill hole data.</li> <li>○ Amorphous blob-shapes were prevented to avoid estimates 'seeing' composites across holes and around fluid boundaries.</li> <li>○ All lodes were treated as hard-boundaries for statistics and estimation.</li> </ul> </li> <li>• The deposit has been divided into four domains based on the orientation of the</li> </ul>



Criteria	JORC Code explanation	Commentary
		<p>lodes:</p> <ul style="list-style-type: none"> <li>○ Max_West</li> <li>○ Max_NW</li> <li>○ Max_Central</li> <li>○ Max_East</li> </ul> <ul style="list-style-type: none"> <li>• Porphyries and meta-sandstone/siltstone and other sedimentary lithologies exist in the stratigraphy, but they are minor or not associated with or proximal to the modelled mineralisation, and so they have not been modelled.</li> </ul>
	<i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>• Alternate interpretations may consider a different gold grade cut-off for the modelling of mineralisation, which will change the tonnages and have a complementary higher or lower grade. Either of these are likely to result in a similar balance of metal.</li> <li>• Differences may result from alternate mining software used or approaches to solid volumes modelled, as the Leapfrog modelling method tends to create more fluid and drillhole constrained objects than a sectionally produced wireframe approach.</li> </ul>
	<i>The use of geology in guiding and controlling Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>• The mineralisation was modelled with a relatively strict gold cut-off of 0.3 g/t Au, which was confirmed by statistical evidence and other deposits in Mt Morgans Gold Operation (MMGO) that are being or have been mined using the same modelling cut-off for ore–waste delineation.</li> <li>• All modelled lodes were treated as hard boundaries for statistics and estimation, although where geological and statistical observations deemed suitable, the lodes were grouped into domains for increased sample counts.</li> <li>• The composited samples within the modelled lode objects were used to estimate the corresponding block object codes with the resource block model.</li> <li>• The lodes show high continuity through the oxidation/weathering profile without dispersion halos. Statistics were reviewed, including grade distributions, and contact analysis, between the oxidation domains, which showed that no boundaries were present, and therefore no hard boundaries by oxidation domain were applied.</li> <li>• Displacement by brittle faulting is evident in the stratigraphy and mineralisation. The fault plane orientations are unclear, but the significant offset across the planes was incorporated into the models of the lodes and stratigraphy by truncation on the fault planes into new objects.</li> <li>• The mineralisation was modelled with a relatively strict gold cut-off of 0.3 g/t Au, which has been confirmed as appropriate for the mining methods and ore markouts.</li> <li>• The following objects were modelled that the Competent Person considers adequate to control the MRE. <ul style="list-style-type: none"> <li>○ Lodes: 15</li> <li>○ BIF–chert units::8</li> </ul> </li> <li>• Oxidation/weathering: base of complete oxidation (BOCO), top of fresh (TOFR)</li> </ul>
	<i>The factors affecting continuity both of grade and geology.</i>	<ul style="list-style-type: none"> <li>• While the mineralisation is not entirely hosted within the BIF–chert horizons, the extensive continuity of the BIF–chert ridge has led to a reasonable confidence in the mineralisation and grade continuity, notwithstanding the brittle offsets.</li> <li>• The modelling of the fault planes has caused the continuity to be reduced, but without the offsets applied, the mineralisation continuity displays unrealistic warping of the mineralisation and stratigraphic wireframes.</li> <li>• The lodes show high continuity through the oxidation/weathering profile without dispersion halos.</li> </ul>
<b>Dimensions</b>	<i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i>	<ul style="list-style-type: none"> <li>• The Maxwells Mineral Resource area extends over an east-west strike length of 640m (from 419,960mE – 420,600mE), has a maximum width of 40m and includes the 200m vertical interval from 450mRL to 250mRL.</li> <li>• The thickness of the lodes ranges from 2 m – 10 m, averaging 3 m.</li> </ul>
<b>Estimation and modelling techniques</b>	<i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values,</i>	<ul style="list-style-type: none"> <li>• Geological modelling, sample compositing, block modelling and grade estimation were undertaken using Surpac™ software.</li> <li>• Statistical analysis including variography was undertaken in Supervisor™ software.</li> <li>• Samples were composited to 1 m intervals (“composites”) based on assessment of the raw drillhole sample intervals. Statistics were weighted by</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p><i>domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i></p>	<p>composite length in Supervisor.</p> <ul style="list-style-type: none"> <li>• Statistical analysis was completed in Snowden Supervisor™ 8.14 software, including modelling of the spatial continuity of gold grades by variography.</li> <li>• Statistics were length-weighted.</li> <li>• Cell de-clustering analysis using cell size combinations of 10 m to 50 m in X, Y and Z directions were undertaken for the Max_Central domain, as the data were more clustered. A 20 m cube was selected based on the analysis that the declustered mean grade was significantly lower than the naïve mean, while being within the range of other declustered cell sizes and not extremely lower. De-clustering was also analysed for the other domains, but was not applied, as it had immaterial impact on statistics reviewed.</li> <li>• Domains were based on spatial characteristics (location, orientation, and geometry) of lodes.</li> <li>• Visual validation of composite grades was reviewed in Surpac to determine if there were any trends with depth or accumulation on weathering/oxidation boundaries.</li> <li>• Multi-block kriging neighbourhood analysis (KNA) was undertaken to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE), slope of regression (SOR) and negative weights were determined for a range of block sizes, minimum and maximum samples, search dimensions, and discretisation grids. Statistics were invariable for changes in discretisation.</li> <li>• Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains. The technique is considered appropriate to allow the geostatistical continuity determined from variography to weight samples during estimation and allow a locally adequate estimate for detailed mine planning, while ensuring a globally unbiased estimate per lode.</li> <li>• A three-pass expanding search ellipse strategy was used, honouring the anisotropic ratios from the relevant domain variogram orthogonally, except for the first pass, which employed dynamic anisotropy (DA), and the dynamic orientation of the search ellipse in Surpac causes the major and semimajor directions to be incorrect. DA was employed as local flexures not related to modelled structural offsets (which divided the deposit's modelled objects) were evident.</li> <li>• Search parameters for each pass were as follows:</li> <li>• Pass 1: <ul style="list-style-type: none"> <li>○ Search ellipse size 44 m, isotropic in the major-semimajor plane, DA</li> <li>○ Minimum samples: 9</li> <li>○ Maximum samples: 22</li> <li>○ Maximum samples per hole: 6</li> <li>○ Discretisation: 3 by 3 by 3</li> </ul> </li> <li>• Pass 2: <ul style="list-style-type: none"> <li>○ Search ellipse size 100% of the full range of the domain variogram (44 m to 118 m)</li> <li>○ Minimum samples: 9</li> <li>○ Maximum samples: 22</li> <li>○ Maximum samples per hole: 6</li> <li>○ Discretisation: 3 by 3 by 3</li> </ul> </li> <li>• Pass 3: <ul style="list-style-type: none"> <li>○ Search ellipse size 300 m</li> <li>○ Minimum samples: 4</li> <li>○ Maximum samples: 10</li> <li>○ Maximum samples per hole: 6</li> <li>○ Discretisation: 3 by 3 by 3</li> </ul> </li> <li>• Grades have not been interpolated into the waste, as there is little evidence for a grade halo or mineralisation in other objects.</li> </ul>
	<p><i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i></p>	<ul style="list-style-type: none"> <li>• A previous MRE by Ashmore Consulting with Sean Serle as Competent Person was announced by Dacian Gold in 2018:</li> </ul>

Criteria	JORC Code explanation	Commentary																																																						
		<table><tr><th colspan="3">Indicated</th><th colspan="3">Inferred</th><th colspan="3">Total</th></tr><tr><th>kt</th><th>Au (g/t)</th><th>koz</th><th>kt</th><th>Au (g/t)</th><th>koz</th><th>kt</th><th>Au (g/t)</th><th>koz</th></tr><tr><td>413</td><td>1.2</td><td>16</td><td>309</td><td>0.9</td><td>9</td><td>722</td><td>1.1</td><td>25</td></tr></table> <ul style="list-style-type: none"><li>In 2019, Dacian Gold updated the MRE following the receipt of data from 37 RC holes for a total length of 2,900m drilled during 2019:</li></ul> <table><tr><th colspan="3">Indicated</th><th colspan="3">Inferred</th><th colspan="3">Total</th></tr><tr><th>kt</th><th>Au (g/t)</th><th>koz</th><th>kt</th><th>Au (g/t)</th><th>koz</th><th>kt</th><th>Au (g/t)</th><th>koz</th></tr><tr><td>250</td><td>1.4</td><td>11</td><td>40</td><td>1.6</td><td>2</td><td>290</td><td>1.3</td><td>12</td></tr></table> <p>The decreased MRE related to reporting within a reasonable prospects for eventual economic extraction (RPEEE) pit optimisation shell.</p> <ul style="list-style-type: none"><li>The deposit has not been mined; therefore, no production data is available.</li></ul>	Indicated			Inferred			Total			kt	Au (g/t)	koz	kt	Au (g/t)	koz	kt	Au (g/t)	koz	413	1.2	16	309	0.9	9	722	1.1	25	Indicated			Inferred			Total			kt	Au (g/t)	koz	kt	Au (g/t)	koz	kt	Au (g/t)	koz	250	1.4	11	40	1.6	2	290	1.3	12
Indicated			Inferred			Total																																																		
kt	Au (g/t)	koz	kt	Au (g/t)	koz	kt	Au (g/t)	koz																																																
413	1.2	16	309	0.9	9	722	1.1	25																																																
Indicated			Inferred			Total																																																		
kt	Au (g/t)	koz	kt	Au (g/t)	koz	kt	Au (g/t)	koz																																																
250	1.4	11	40	1.6	2	290	1.3	12																																																
	<i>The assumptions made regarding recovery of by-products.</i>	<ul style="list-style-type: none"><li>No assumptions have been made regarding the recovery of by-products.</li></ul>																																																						
	<i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i>	<ul style="list-style-type: none"><li>No deleterious elements have been estimated.</li></ul>																																																						
	<i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i>	<ul style="list-style-type: none"><li>A parent block size of 15 m x 15 m x 10 m (X x Y x Z) was chosen, which was supported KNA and by drill hole spacing all directions.</li><li>Sub-celling to 1/8 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.</li><li>Most of the deposit has been drilled at a density of 20m by 20m and out to 40m by 40m on the fringes.</li></ul>																																																						
	<i>Any assumptions behind modelling of selective mining units.</i>	<ul style="list-style-type: none"><li>No assumptions have been made regarding SMUs.</li></ul>																																																						
	<i>Any assumptions about correlation between variables.</i>	<ul style="list-style-type: none"><li>Gold has been estimated univariately and in isolation of other variables.</li></ul>																																																						
	<i>Description of how the geological interpretation was used to control the resource estimates.</i>	<ul style="list-style-type: none"><li>Geology and grade were used to define the mineralisation lodes. Within each lode, the estimate was constrained to blocks within the lode wireframe using only top-cut composited samples from the corresponding lode.</li></ul>																																																						
	<i>Discussion of basis for using or not using grade cutting or capping.</i>	<ul style="list-style-type: none"><li>High-grade top-caps were applied to limit the influence of extreme outliers on the grade estimate. The top-caps were applied to the mineralisation domains following statistical analysis.</li><li>Top-cuts were determined for the lodes within the three statistical domains, as follows:<ul style="list-style-type: none"><li>Max_West: uncut (no outliers)</li><li>Max_NW: uncut (no outliers)</li><li>Max_Central: 9g/t Au</li><li>Max_East: 6 g/t</li></ul></li><li>The top-cuts were kept at around 1% – 2% of the distribution.</li></ul>																																																						
	<i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i>	<ul style="list-style-type: none"><li>Validation of the estimate was completed for the resource block models using numerical methods (histograms, CDFs and swath plots) and validated visually against the input raw drillhole data, declustered data, composites and blocks.</li></ul>																																																						
<b>Moisture</b>	<i>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</i>	<ul style="list-style-type: none"><li>Tonnages and grades have been estimated on a dry in situ basis.</li></ul>																																																						

Criteria	JORC Code explanation	Commentary
<b>Cut-off parameters</b>	<i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i>	<ul style="list-style-type: none"> <li>The MRE has been reported above a lower cut-off of 0.5 g/t Au.</li> <li>A RL was considered for reporting above the MRE at this cut-off; however, as the mineralisation is no more than 140 m depth from surface RPEEE is established for the shallow depths, no RL cut-off was applied.</li> <li>The reporting cut-off parameters were selected based on known UG economic cut-off grades from Dacian's Westralia UG operation.</li> </ul>
<b>Mining factors or assumptions</b>	<i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i>	It is assumed that the deposit will be amenable to open pit methods, as has been undertaken for similar deposits in the MMGO project.
<b>Metallurgical factors or assumptions</b>	<i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i>	<ul style="list-style-type: none"> <li>The ore is intended to be processed at the Jupiter Processing Facility, part of the Mt Morgans Gold Operation (MMGO). Recoveries achieved to date are 92.3%.</li> </ul>
<b>Environmental factors or assumptions</b>	<i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported.</i>	<ul style="list-style-type: none"> <li>Maxwell Bore lies within a MMGO mining leases, where many historic pits and several mines are active, in a very mature mining district. Therefore, Dacian believes that there will be no impediments to the approval of mining the deposits again.</li> <li>Waste rock will be stored in a conventional waste dump.</li> </ul>

Criteria	JORC Code explanation	Commentary																											
	<i>Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i>																												
<b>Bulk density</b>	<i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i>	<ul style="list-style-type: none"> <li>The wireline gamma-density data logged throughout Mt Morgans by Surtech systems in February 2021 were used to assist the density determination of the MRE, although they were not taken from the Maxwell Bore deposit.</li> <li>The density for mafic material of differing oxidation states was taken from the density assigned to the Craic deposit, whose style of mineralisation is mafic-hosted. The waste laterite and colluvium was assigned based on the Competent Person's knowledge of similar material throughout Mt Morgans and similar geological settings in the Yilgarn. As the BIF material was frequently logged as chert-rich BIF or chert, the densities applied were lower than those determined by wireline gamma-density and diamond core immersion methods.</li> <li>The final densities assigned were: <table border="1"> <thead> <tr> <th>Lithology</th><th>Oxidation state</th><th>Density value (t/m<sup>3</sup>)</th></tr> </thead> <tbody> <tr> <td>colluvium</td><td>Transported</td><td>1.4</td></tr> <tr> <td>laterite</td><td>Transported</td><td>2.0</td></tr> <tr> <td>BIF-chert</td><td>Completely oxidised</td><td>1.6</td></tr> <tr> <td>BIF-chert</td><td>Transitional</td><td>2.2</td></tr> <tr> <td>BIF-chert</td><td>Fresh</td><td>2.65</td></tr> <tr> <td>mafic</td><td>Completely oxidized</td><td>1.8</td></tr> <tr> <td>mafic</td><td>Transitional</td><td>2.3</td></tr> <tr> <td>mafic</td><td>Fresh</td><td>2.75</td></tr> </tbody> </table> </li> </ul>	Lithology	Oxidation state	Density value (t/m <sup>3</sup> )	colluvium	Transported	1.4	laterite	Transported	2.0	BIF-chert	Completely oxidised	1.6	BIF-chert	Transitional	2.2	BIF-chert	Fresh	2.65	mafic	Completely oxidized	1.8	mafic	Transitional	2.3	mafic	Fresh	2.75
Lithology	Oxidation state	Density value (t/m <sup>3</sup> )																											
colluvium	Transported	1.4																											
laterite	Transported	2.0																											
BIF-chert	Completely oxidised	1.6																											
BIF-chert	Transitional	2.2																											
BIF-chert	Fresh	2.65																											
mafic	Completely oxidized	1.8																											
mafic	Transitional	2.3																											
mafic	Fresh	2.75																											
	<i>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i>	<ul style="list-style-type: none"> <li>The gamma-density data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging.</li> </ul>																											
	<i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i>	<ul style="list-style-type: none"> <li>For gamma-density, the data are quantitative and independent of sample weight, and have been analysed by modelled material types.</li> <li>For core immersion-method density data, no relationship to sample weight has been determined, and is expected to be unrelated, as the core density data show little variation with lithological types.</li> </ul>																											
<b>Classification</b>	<i>The basis for the classification of the Mineral Resources into varying confidence categories.</i>	<p>The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:</p> <ul style="list-style-type: none"> <li>Drill density data</li> <li>Geological understanding</li> <li>Quality of gold assay grades</li> <li>Continuity of gold grades</li> <li>Economic potential for mining.</li> </ul> <ul style="list-style-type: none"> <li>For Indicated Mineral Resources, statistical consideration has been employed to assess the grade estimate quality in considering large, contiguous and coherent zones of blocks form zones where: <ul style="list-style-type: none"> <li>From the 15 total lodes modelled in the deposit, only two lodes each from the Max_Central and Max_East domains total that displayed the highest geological confidence were considered.</li> <li>Drill hole spacing reached a nominal maximum of 20 m.</li> <li>Estimation dominantly was undertaken in search pass 1.</li> <li>Number of samples was near the optimum.</li> <li>Slope of regression formed large volumes of &gt; 0.4 with cores of 0.6.</li> </ul> </li> <li>Inferred Mineral Resources: <ul style="list-style-type: none"> <li>All other mafic-hosted mineralisation, as the drill hole spacing and pierce was never greater than 80 m within the geological model that is considered robust.</li> </ul> </li> <li>Unclassified material:</li> </ul>																											

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>All material outside of the mineralisation.</li> </ul>
	<i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i>	<ul style="list-style-type: none"> <li>All factors the Competent Person has deemed relevant to the MRE have been incorporated into the classification of Mineral Resources.</li> </ul>
	<i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i>	<ul style="list-style-type: none"> <li>The result appropriately reflects the Competent Person's view of the deposit.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of Mineral Resource estimates.</i>	<ul style="list-style-type: none"> <li>Internal audits were completed by Dacian, which verified the technical inputs, methodology, parameters and results of the estimate.</li> </ul>
<b>Discussion of relative accuracy/confidence</b>	<i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i>	<ul style="list-style-type: none"> <li>The accuracy of the MRE is communicated through the classification assigned to the deposit. The MRE has been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this table.</li> </ul>
	<i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i>	<ul style="list-style-type: none"> <li>The MRE statement relates to a global estimate of in-situ tonnes and grade.</li> </ul>
	<i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i>	<ul style="list-style-type: none"> <li>The deposit has not been mined; therefore, no production data is available.</li> </ul>



## Beresford, Allanson, and Morgans North and Phoenix Ridge

### Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.	<p>RC drilling for Plutonic was conducted by Drillex and Green Drilling using 140 mm drill bits with samples collected at the rig for every metre. Samples were returned through the rods and sampling hose to a cyclone and were then put through a riffle splitter to collect approximately 2 kg – 5 kg samples.</p> <p>Besides the Plutonic drilling, no information exists for sample methodologies prior to 2013; however, after review of the assay table in the database, all RC samples were taken at 1 m intervals and it appears as though diamond samples were taken at 1 m intervals or to geological contacts.</p> <p>From 2013 onwards, RC drilling was performed by Challenge Drilling, Raglan Drilling and Strike Drilling using 140 mm drill bits with samples collected at the rig for every metre. Samples were returned through the rods and sampling hose to a cyclone, and were then put through a cone splitter to collect approximately 2 kg – 3 kg samples in pre-numbered calico bags. The bulk reject was retained on site in green mining bags near the drill hole collar. RC drilling was sampled at 1 m intervals for the entire hole length.</p> <p>For RC holes, a 5¼" face sampling bit was used to collect drill chips.</p> <p>Face samples were collected by Plutonic using a line chip method. The geologist set out sample runs based on geological units, collected using a geological hammer to break off fragments. The sample was collected to be representative of the unit whereby small representative chips were taken from across the complete individual sampling interval. The sample was collected in a pre-numbered calico bag utilising a sampling ring to secure the bag firmly. Due to the poddy fine-grained nature of the gold at Westralia, the sample size was large (up to 3 kg), with the actual amount collected dependent on how fractured the rock was.</p> <p>RC holes are sampled over the entire length of hole. Dacian RC drilling was sampled at 1 m intervals via an on-board cone splitter. Historical RC samples were collected at 1m using riffle splitters.</p> <p>Dacian samples were submitted to a contract laboratory for crushing and pulverising to produce either a 40g or 50g charge for fire assay.</p> <p>Most Dacian drill holes had diamond tails drilled by Westralian Diamond Drillers using NQ2 size core.</p>
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	<p>Surface diamond core was sampled as half core at 1 m intervals or to geological contacts. To ensure representative sampling, half core samples were always taken from the same side of the core.</p> <p>Face channel samples were taken from left to right in underground ore development drives on every advance of 3.5 m – 4 m at a height of 1.5 m.</p> <p>Channel samples were across the width of the thickness of mineralised bodies in the face over 1 m intervals or to geological contacts.</p>

Criteria	JORC Code explanation	Commentary
		<p>Channel samples were taken as close to perpendicular to the angle of the mineralisation as possible to achieve an apparent true thickness.</p> <p>Most underground diamond core was full core sampled to produce as large a sample as possible. One hole in each program (maximum 10 holes per program) were half cored. All holes were sampled at max 1 m intervals or to geological contacts.</p> <p>RC holes were sampled over entire hole lengths on 1 m intervals in mineralisation via an on-board cone splitter mounted at the base of the cyclone.</p>
	<p>Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</p>	<p>Dacian RC holes were sampled over the entire length of hole on 1 m intervals via an on-board cone splitter to achieve approximately 3 kg samples. Samples were then submitted to a contract laboratory for crushing and pulverising to produce either a 40g or 50g charge for fire assay.</p> <p>Dacian surface diamond core was sampled as half core on 1 m intervals or to geological contacts. Sampling did not cross geological boundaries. cut in half, sampled into lengths in sample bags to achieve approximately 3 kg, and submitted to a contract laboratory for crushing and pulverising to produce either a 40 g or 50 g charge for fire assay.</p> <p>Most underground diamond core was full core sampled to produce as large a sample as possible. One hole in each program (maximum 10 holes per program) were half cored. All holes were sampled at max 1 m intervals or to geological contacts.</p> <p>Face samples were submitted to an onsite laboratory outsourced to an external provider for Pulverise and Leach (PAL). A 600 g subsample was pulverised and leached then analysed by AAS.</p>
Drilling techniques	<ul style="list-style-type: none"> <li>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</li> </ul>	<p>Reverse circulation (RC) percussion drilling, surface and underground diamond drilling, and underground face sampling were used to inform the Mineral Resource estimate (MRE).</p> <p>Aircore (AC) was used to guide the geological and mineralisation interpretation, but the data were not used in the grade estimate.</p> <p>Surface Diamond drilling was mostly carried out with NQ2 sized equipment, along with minor HQ3 and PQ2, using standard tube. Surface drill core was orientated using a Reflex orientation tool.</p> <p>For deeper surface holes, RC pre-collars were followed with diamond tails.</p> <p>Underground diamond drilling was carried out with NQ2 sized equipment. Underground drill core was not oriented consistently, but where it was oriented was undertaken using a Reflex orientation tool.</p>
Drill sample recovery	<ul style="list-style-type: none"> <li>Method of recording and assessing core and chip sample recoveries and results assessed.</li> </ul>	<p>Recoveries from historical drilling are unknown.</p> <p>Recoveries from Dacian surface core drilling were measured and recorded in the database. Recoveries from Dacian underground core drilling were measured and recorded in the database only for the mineralised sedimentary sequence, and not for the Hangingwall mafic/intrusive stratigraphy.</p> <p>Recoveries average 99.08% within the sedimentary package with minor core loss in fresh core that is very</p>

Criteria	JORC Code explanation	Commentary
		broken due to the interaction of multiple structures or pervasively talc altered ultramafic.
	<ul style="list-style-type: none"> <li>Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> </ul>	<p>For Dacian RC holes, a powerful rig with compressor and booster compressor was used to ensure enough air to maximise sample recovery. The splitter is cleaned at the end of each rod, to ensure that efficient sample splitting. The weight of each sample split was monitored, and drilling was stopped if the sample split size changes significantly.</p> <p>For Dacian diamond holes, the core is returned via inner tubes and extracted onto core trays marked up by depth to ensure core loss is recorded.</p>
	<ul style="list-style-type: none"> <li>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</li> </ul>	For Dacian drilling, no relationship exists between sample recovery and grade.
Logging	<ul style="list-style-type: none"> <li>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> </ul>	<p>All diamond drill holes were logged for recovery, RQD, geology and structure. For Dacian drilling, diamond core was photographed both wet and dry.</p> <p>All development faces were mapped for geology and structure.</p> <p>The Competent Person is satisfied that the logging detail supports the MRE.</p>
	<ul style="list-style-type: none"> <li>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</li> </ul>	<p>Logging is qualitative, as determined by geologists familiar with the geology and controls on the mineralisation.</p> <p>Validation of logging against geochemistry was routinely undertaken.</p>
	<ul style="list-style-type: none"> <li>The total length and percentage of the relevant intersections logged.</li> </ul>	<p>All RC and AC drill holes were logged for geology, alteration and structure. All RC chip trays were photographed.</p> <p>All drill holes were logged in full.</p>
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> <li>If core, whether cut or sawn and whether quarter, half or all core taken.</li> </ul>	<p>Plutonic samples were sent to Amdel Laboratories in Kalgoorlie. When received, samples were sorted and then dried. The sample was then subject to a primary crush, then pulverised so that 80% passes a 75µm sieve.</p> <p>Apart from Plutonic drilling, no information exists for sample preparation prior to 2013.</p> <p>Between 2013 and 2015; and mid-2016 to mid-2018, Dacian samples were sent to Bureau Veritas Laboratories in Perth and Kalgoorlie. When received, RC samples were sorted and then dried. The sample was then subject to a primary crush, then pulverised so that 85% passes a 75µm sieve.</p> <p>Dacian surface core was cut in half using an automatic core saw at either 1m intervals or to geological contacts; core samples were collected from the same side of the core where orientations were completed.</p> <p>Dacian underground core was full core sampled at either 1m intervals or to geological contacts.</p> <p>Approximately 1 hole in 10 was cut in half using an automatic core saw at either 1m intervals or to geological contacts.</p>
	<ul style="list-style-type: none"> <li>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</li> </ul>	Plutonic samples were sent to Amdel Laboratories in Kalgoorlie. When received, samples were sorted and then dried. The sample was then subject to a primary crush, then pulverised so that 80% passes a 75 µm sieve.

Criteria	JORC Code explanation	Commentary
		<p>Apart from Plutonic drilling, no information exists for sample preparation prior to 2013.</p> <p>Between 2013 and 2015; and mid-2016 to mid-2018, Dacian samples were sent to Bureau Veritas Laboratories in Perth and Kalgoorlie. When received, RC samples were sorted and then dried. The sample was then subject to a primary crush, then pulverised so that 85% passes a 75µm sieve.</p> <p>Historical RC samples were collected at the rig using riffle splitters. Samples were generally dry. For historic RC drilling, information on the QAQC programs used is acceptable. Dacian RC samples were collected via on-board cone splitters. Most samples were dry. For RC drilling, sample quality was maintained by monitoring sample volume and by cleaning splitters on a regular basis.</p> <p>RC and diamond sample preparation was conducted by a contract laboratory. After drying, the sample was subjected to a primary crush, then pulverised to 85% passing 75µm.</p> <p>Underground face samples were collected as 3 kg – 5 kg channel samples generally as a horizontal line 1.5m from the development floor. Where the geology was not vertically consistent, the sample line was orientated to be as close to perpendicular to the mineralisation as possible, or a second sample line was taken.</p>
	<ul style="list-style-type: none"> <li>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> </ul>	<p>Underground face sample preparation was conducted onsite by a contract laboratory. After drying, the sample was subjected to a primary and secondary crush to 90% passing 3 mm, before being cone split into a 600 g subsample. The 600 g sample was then pulverised to 90% passing 80µm and simultaneously leached for 60 minutes in a Pulverise and Leach (PAL) machine using 2 kg of grinding media, 1 Litre of water and 2 x 10 g cyanide tablets (75% NaCN). The leached solution was separated by centrifuge and analysed by AAS.</p>
	<ul style="list-style-type: none"> <li>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</li> </ul>	<p>RC field duplicates were mostly taken at 1 in 25.</p> <p>Duplicate samples were taken at 1 in 8 underground faces.</p> <p>Externally prepared Certified Reference Materials within the sample stream, and all laboratories utilised internal QAQC protocols.</p>
	<ul style="list-style-type: none"> <li>Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.</li> </ul>	<p>Field duplicates were mostly taken at 1 in 25.</p>
	<ul style="list-style-type: none"> <li>Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul>	<p>Sample sizes are considered appropriate to correctly represent the gold mineralisation based on the style of mineralisation, the thickness and consistency of the intersections, the sampling methodology and assay value ranges for gold.</p>
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> <li>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</li> </ul>	<p>For the Dacian drilling, the analytical technique used was a 40 g or 50 g lead collection fire assay and analysed by Atomic Absorption Spectrometry. This is a full digestion technique. Samples were analysed at Bureau Veritas and Intertek Laboratories in Perth or Kalgoorlie, Western Australia.</p>

Criteria	JORC Code explanation	Commentary
		<p>For Dacian drilling, sieve analysis was carried out by the laboratory to ensure the grind size of 85% passing 75µm was being attained.</p> <p>For Dacian RC and diamond drilling, QAQC procedures involved the use of certified reference materials (1 in 20) and blanks (1 in 50). Results were assessed as each laboratory batch was received and were acceptable in all cases.</p> <p>For Dacian RC grade control drilling, QAQC procedures involved the use of certified reference materials (1 in 20) and blanks (1 in 20). Results were assessed as each laboratory batch was received and were acceptable in all cases.</p> <p>For Dacian AC drilling, QAQC procedures involved the use of certified reference materials (1 in 50) and blanks (1 in 50). Results were assessed as each laboratory batch was received and were acceptable in all cases.</p> <p>For Dacian underground face samples, the analytical technique used was a 600 g Pulverise and Leach (PAL) method followed by Atomic Absorption Spectrometry. Samples were analysed by SGS laboratories at an onsite laboratory. PAL is a partial digestion method. However, analysis has shown a very strong correlation between FA and PAL on duplicate samples. Therefore, the Competent Person is confident that the PAL method typically approximates the fire assay technique.</p>
	<ul style="list-style-type: none"> <li>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</li> </ul>	N/A
	<ul style="list-style-type: none"> <li>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</li> </ul>	<p>For Dacian underground face samples, QAQC procedures involved the use of certified reference materials (1 every 25% of faces sampled) and blanks (1 every 25% of faces sampled). Results were assessed as each laboratory batch was received.</p> <p>QAQC data has been reviewed by the Competent Person for historic RC drilling and the results are considered acceptable for including the samples in the MRE.</p> <p>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</p> <p>Certified reference materials demonstrate that sample assay values are accurate.</p> <p>Umpire laboratory testwork was completed in 2019 over mineralised intersections with good correlation of results.</p> <p>Commercial laboratories used by Dacian were audited quarterly in 2019.</p>
Verification of sampling and assaying	<ul style="list-style-type: none"> <li>The verification of significant intersections by either independent or alternative company personnel.</li> </ul>	<p>Significant intersections were visually field verified by company geologists during underground production.</p> <p>The Competent Person has confirmed mineralised intersections at several underground headings for Beresford and Allanson.</p>
	<ul style="list-style-type: none"> <li>The use of twinned holes.</li> </ul>	<p>Twin holes were completed at Westralia underground. Results compared reasonably well for the mineralisation style.</p>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</li> </ul>	<p>Primary logging and sampling data were collected into Excel spreadsheets with data validation control and password protection.</p> <p>Assay data were provided by laboratories in a standardised format.</p> <p>Data were then imported by DataShed front-end software into a back-end Maxwell Database Schema 4.5.2 SQL Server DB, which provided a referentially integral database with primary key relations and look-up validation fields.</p>
	<ul style="list-style-type: none"> <li>Discuss any adjustment to assay data.</li> </ul>	<p>Data preparation of the resource modelling database included setting all of the following gold assay records to the half of the detection limit (HDL) of 0.01 (i.e. 0.005) set in the Bureau Veritas (BV) Kalgoorlie laboratory contract for the method:</p> <ul style="list-style-type: none"> <li>Negative below detection limit (BDL) assays</li> <li>Zeros</li> <li>Nulls</li> </ul> <p>Unsampled intervals within the zone table. Some lodes contain significant proportions of unsampled intervals, which if left untreated would create high-grade biases, as the sampled intervals would be allowed to represent and estimate more volume than appropriate. These were assumed to be unsampled because of lack of identifiable mineralisation, and as such the database was coded with 1 m intervals at the detection limit of 0.005 g/t Au.</p> <p>Although another approach may be selected, such as setting to ¼ detection limit, this approach is consistent across all Dacian MREs, and the Competent Person believes it has no material impact on the MRE. Further, to eliminate negative records may create high-grade biases.</p> <p>Any negatives below –1 were set to null in the compositing process by Surpac, as these are lab error codes (numerous values in the single, tens and thousands figures), which include the following in exhaustive types:</p> <ul style="list-style-type: none"> <li>Samples not received but listed in sample submissions</li> <li>Samples received but not listed in sample submissions</li> <li>Samples destroyed in sample preparation</li> <li>Insufficient sample volume/weight</li> </ul>
Location of data points	<ul style="list-style-type: none"> <li>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</li> </ul>	<p>Across Westralia, down-hole surveying included the following types:</p> <ul style="list-style-type: none"> <li>North-seeking, non-magnetic DeviFlex Rapid and DeviGyro Overshot Xpress with an azimuth aligner = 88% of the total holes and 73% of the total metres surveyed.</li> <li>Magnetic camera shots: 3% of the total holes and 4% of the total metres surveyed.</li> <li>Compass, dummy, planned and unknown methods: 9% of the total holes and 23% of the total metres surveyed.</li> </ul> <p>Historic drill hole collar coordinates were tied to a historic MTM local grid with subsequent conversion to MGA94 Zone 51, and then conversion to MTM2017 grid.</p>



Criteria	JORC Code explanation	Commentary
		<p>Most historic, near surface mine workings support the locations of historic drilling. However, review of data found 41 holes with significant discrepancies between the historic as-built void surveys and historic hole collar locations, so that collars appeared drilled from impossible locations. For these, the holes were repositioned to the most logical location, as recent drilling did not intersect the mineralisation in the same location. The average difference from original to amended location was 2.73 m, with a maximum of 13.6 m.</p> <p>All Dacian surface hole collars were surveyed in MGA94 Zone 51 grid using differential GPS.</p> <p>Dacian surface holes were down hole surveyed either with multi-shot EMS, Reflex multi-shot tool or north seeking gyro tool.</p> <p>Underground diamond drill holes were surveyed using a Leica TS16 total station using the MTM mine grid co-ordinates, which can then be converted to MGA94 Zone 51 grid co-ordinates values.</p> <p>Underground diamond drill holes were downhole surveyed using a Devi flex Rapid downhole survey tool.</p> <p>Underground face samples were digitised to the surveyed underground development pickup, using a distance from a surveyed laser station calculated using a Leica digital distometer.</p>
	<ul style="list-style-type: none"> <li>Specification of the grid system used.</li> </ul>	<p>The grid system was a local mine grid, "MTM2017", meaning Mt Morgans 2017 mine grid, established for the Westralia mine corridor to align the stratigraphy orthogonally in a north-south orientation. The grid system employs the following two-point transformation from MGA Zone 51 and RL adjustment from Australian Height Datum (AHD):</p> <ul style="list-style-type: none"> <li>MGA Zone 51 Point 1 X: 408785.389</li> <li>MGA Zone 51 Point 1 Y: 6817690.085</li> <li>MTM2017 Point 1 X: 10143.521</li> <li>MTM2017 Point 1 Y: 11494.699</li> <li>MGA Zone 51 Point 2 X: 409424.940</li> <li>MGA Zone 51 Point 2 Y: 6816715.961</li> <li>MTM2017 Point 2 X: 10305.661</li> <li>MTM2017 Point 2 Y: 10340.223</li> <li>MTM2017 RL: AHD RL + 2000m</li> </ul>
	<ul style="list-style-type: none"> <li>Quality and adequacy of topographic control.</li> </ul>	<p>The topographic surfaces used to code the resource block models included an 'as-built' survey file prepared from detailed ground and mine surveys.</p> <p>As-built historic Westralia pits used to code the resource block model included those intersecting mineralisation: Westralia, Morgans North and Millionaires, and those intersecting waste portions of the model areas: King St, Recreation, Ramornie and Sarah.</p> <p>Material above all surfaces was coded in the models as depleted to ensure no mineralisation was included in the MRE.</p> <p>The Competent Person is satisfied that the topographic control provides the quality required to report the Mineral Resources in accordance with the JORC Code.</p>
	<ul style="list-style-type: none"> <li>Data spacing for reporting of Exploration Results.</li> </ul>	<p>Exploration results are not being report.</p>

Criteria	JORC Code explanation	Commentary
Data spacing and distribution	<ul style="list-style-type: none"> <li>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</li> </ul>	<p>The nominal exploration hole spacing of drilling is approximately 80 m by 80 m, infilled to 20 m by 20 m for grade control purposes. Face samples are taken every ore development cut, which is approximately every 3.5 m, over levels approximately 17 m apart vertically.</p> <p>However, the data spacing varies from the access to underground drilling locations provides some areas with mineralisation pierce points of 10 m by 10 m (Y by Z) out to 100 m by 100 m, which is the widest drillhole spacing for Inferred Mineral Resources on the peripheries of lodes, although the grades are typically below the reporting cut-off.</p>
	<ul style="list-style-type: none"> <li>Whether sample compositing has been applied.</li> </ul>	<p>Sample compositing has not been applied for raw samples.</p> <p>for statistics and estimation, samples were composited to</p> <p>Based on the variable sample lengths below 1 m, to reduce sample bias and seek an equal-weighting, the statistical compositing used the 'best-fit' method in Surpac, which forces all samples to be included in one of the composites by adjusting the composite length, while keeping it as close as possible to 1 m. Composite lengths shorter than 51% of the composite length (1 m) were rejected. The resulting composite lengths used for estimation were dominated by 1 m.</p>
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> <li>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</li> </ul>	<p>Surface drill holes have been angled to between 50-65 degrees, which is approximately perpendicular to the orientation of the expected trend of mineralisation.</p> <p>Underground diamond holes vary considerably due to the location of drilling platforms. However, the drilling platforms are located within the development such that the drilling orientation often achieves a high angle to the plane of the stratigraphy.</p> <p>Face channel samples were taken from left to right in underground ore development drives on every advance of 3.5 m – 4 m at a height of 1.5 m.</p> <p>Channel samples were across the width of the thickness of mineralised bodies in the face over 1 m intervals or to geological contacts.</p>
	<ul style="list-style-type: none"> <li>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material</li> </ul>	<p>The Competent Person is not aware of any sampling bias resulting from drilling orientation.</p>
Sample security	<ul style="list-style-type: none"> <li>The measures taken to ensure sample security.</li> </ul>	<p>Chain of custody is managed by Dacian. Samples are stored on site until collected for transport to the sample preparation laboratory in Kalgoorlie.</p> <p>For samples submitted to the on-site contract laboratory samples are delivered to the laboratory facility by Dacian personnel. Dacian personnel have no contact with the samples once they are picked up for transport. Tracking sheets have been set up to track the progress of samples.</p>
Audits or reviews	<ul style="list-style-type: none"> <li>The results of any audits or reviews of sampling techniques and data.</li> </ul>	<p>Ashmore Advisory reviewed RC and diamond core sampling techniques in April 2018 and concluded that sampling techniques are satisfactory.</p> <p>The Competent Person regularly visits site and periodically inspects core logging and sampling facilities, and active drill sites.</p>

Criteria	JORC Code explanation	Commentary
		<p>All Dacian sampling, logging and QAQC procedures are documented and reviewed when updated.</p> <p>Commercial laboratories used by Dacian have been audited quarterly in 2019 to early 2020 before Westralia mining was ceased, and in April 2021 by the Competent person. Sample preparation and assaying processes were satisfactory.</p>

## Beresford, Allanson, and Morgans North and Phoenix Ridge

### Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> <li>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</li> </ul>	Westralia is an active underground gold mine which started in May 2017. The Westralia and Ramornie deposits are located within Mining Lease 39/18 and is held 100% by Mt Morgans WA Mining Pty Ltd, a wholly owned subsidiary of Dacian Gold Ltd.
	<ul style="list-style-type: none"> <li>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</li> </ul>	<p>No caveats, liens or other non-government royalties are held against the tenement.</p> <p>The tenement is in good standing.</p>
Exploration done by other parties	<ul style="list-style-type: none"> <li>Acknowledgment and appraisal of exploration by other parties</li> </ul>	Open pit and underground mining has occurred since the 1890s. Other companies to have explored the deposit area include Whim Creek Consolidated NL, Dominion Mining, Plutonic Resources, Homestake Gold, Barrick Gold Corporation, Delta Gold and Range River Gold.
Geology	<ul style="list-style-type: none"> <li>Deposit type, geological setting and style of mineralisation.</li> </ul>	<p>The Westralia deposit lies within the Yilgarn Craton of Western Australia.</p> <p>The deposits are BIF hosted sulphide replacement, mesothermal Archaean gold deposits comprising sedimentary packages predominantly of BIF units, but which also include chert, mudstone, shales, conglomerate and minor felsic volcanoclastic rocks. All are intercalated within or separated by ultramafic volcanic rocks and variably intruded by felsic porphyry dykes and lamprophyres.</p> <p>Gold mineralisation is associated with microscopic quartz carbonate veinlets within BIF. BIF acts as the primary host for mineralisation though other rock types including basalt, porphyry intrusive and ultramafic may also be mineralised in smaller volumes and with less continuity.</p> <p>At Beresford, high grade moderate to steep south plunging shoots within the hangingwall sediment package of Beresford are controlled by D3a NNE steeply east dipping shears intersection with the BIF horizons. Refraction of the structure within the BIF may produce a component of strike slip deformation. These structures are known to be mineralised away from the BIF hosted deposits with multiple small mafic hosted deposits previously mined to the east including Ramornie, Ramornie North, and Sarah open pit deposits. This early D3a structure has long been attributed with controlling mineralisation.</p> <p>The second shoot orientation at Beresford plunges shallowly to the north. Pit mapping and detailed structural logging suggests this shoot orientation is</p>

Criteria	JORC Code explanation	Commentary
		associated with late D3b moderately east dipping BIF parallel shears, the largest of which results in a major thrust offset of the BIF stratigraphy with minor sinistral strike slip component. Within the hangingwall basalt sequence these structures are composed of anastomosing shears that show local variations in width and orientation. The shear zones are locally iron carbonate and sericite altered with minor disseminated sulphides. These structures have been modelled and broad projection of these structures reveals a strong correlation with shallow north plunging shoots away from detailed structural analysis.
Drill hole Information	<ul style="list-style-type: none"> <li>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>easting and northing of the drill hole collar</li> <li>elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>dip and azimuth of the hole</li> <li>down hole length and interception depth</li> <li>hole length.</li> </ul> </li> </ul>	Exploration results are not being reported.
	<ul style="list-style-type: none"> <li>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</li> </ul>	N/A
Data aggregation methods	<ul style="list-style-type: none"> <li>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.</li> </ul>	Exploration results are not being reported.
	<ul style="list-style-type: none"> <li>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</li> </ul>	N/A
	<ul style="list-style-type: none"> <li>The assumptions used for any reporting of metal equivalent values should be clearly stated.</li> </ul>	N/A
Relationship between mineralisation widths and intercept lengths	<ul style="list-style-type: none"> <li>These relationships are particularly important in the reporting of Exploration Results.</li> </ul>	Exploration results are not being reported.
	<ul style="list-style-type: none"> <li>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> </ul>	<p>Surface drill holes have been angled to between 50-65 degrees, which is approximately perpendicular to the orientation of the expected trend of mineralisation.</p> <p>Underground diamond holes vary considerably due to the location of drilling platforms. However, the drilling platforms are located within the development such that the drilling orientation often achieves a high angle to the plane of the stratigraphy.</p> <p>Face channel samples were taken from left to right in underground ore development drives on every advance of 3.5 m – 4 m at a height of 1.5 m.</p> <p>Channel samples were across the width of the thickness of mineralised bodies in the face over 1 m intervals or to geological contacts.</p>
	<ul style="list-style-type: none"> <li>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not</li> </ul>	N/A

Criteria	JORC Code explanation	Commentary
	known').	
Diagrams	<ul style="list-style-type: none"> <li>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</li> </ul>	Relevant diagrams have been included within the main body of text.
Balanced reporting	<ul style="list-style-type: none"> <li>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</li> </ul>	Exploration results are not being reported.
Other substantive exploration data	<ul style="list-style-type: none"> <li>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</li> </ul>	N/A
Further work	<ul style="list-style-type: none"> <li>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</li> </ul>	<p>For Beresford and Allanson, planning of underground drilling will target high-grade areas close to existing development to maximise material available for mill feed.</p> <p>For Phoenix Ridge, the high-grade area at depth requires improved geological knowledge to classify mineralisation with higher confidence Mineral Resources.</p>
	<ul style="list-style-type: none"> <li>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</li> </ul>	N/A

## Beresford, Allanson, and Morgans North and Phoenix Ridge

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	<ul style="list-style-type: none"> <li>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</li> </ul>	The data base has been systematically audited by a Dacian geologist. Original drilling records were compared to the equivalent records in the data base (where original records were available). Any discrepancies were noted and rectified by the data base manager.
	<ul style="list-style-type: none"> <li>Data validation procedures used.</li> </ul>	<p>Ongoing database (DB) validation has been undertaken by a dedicated DB administrator communicating with geologists as the primary data sources and labs.</p> <p>Extensive validation was undertaken by the database administrator.</p> <p>Data were loaded into DataShed back-end SQL Server DB on a related data schema, providing a referentially integral database with primary key relations and look-up validation fields.</p> <p>Additional validation completed Surpac by Dacian geologists, with any validation issues relayed to DB administrator. All Dacian drilling data has been verified as part of a continuous validation procedure. Once a drill hole is imported into the data base reports of the collar, down-</p>

Criteria	JORC Code explanation	Commentary
		<p>hole survey, geology, and assay data are produced. These are then checked by a Dacian geologist in geological software and any corrections are sent to the data base administrator to complete.</p> <p>All data were checked for the following errors:</p> <p>Duplicate drillhole IDs</p> <p>Missing collar coordinates</p> <p>Mis-matched or missing FROM or TO fields in the interval tables (assays, logging etc)</p> <p>FROM value greater than TO value in interval tables</p> <p>Non-contiguous sampling intervals</p> <p>Sampling interval overlap in the assay table</p> <p>The first sample in the interval file not starting at 0 m</p> <p>Interval tables with depths greater than the collar table EOH depth.</p> <p>Survey data were checked for large deviations in azimuth and dip between consecutive records, with none found.</p>
Site visits	<ul style="list-style-type: none"> <li>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</li> </ul>	<p>The Competent Person has made several site visits from 2020 through 2021, and has worked with the site-based geologists and mining engineers on the MRE and reconciliation processes relevant to this estimate.</p> <p>Inspection of the equipment used by Dacian's drilling contractor at the time of the visits found all operators working to a standard required to report a MRE in accordance with the JORC Code.</p> <p>The Competent Person visited the on-site contract laboratory twice in December to review processes, and each of the two National Association of Testing Authorities (NATA) accredited offsite laboratories in 2021. All laboratories were performing at and producing results for a standard required to report a MRE in accordance with the JORC Code.</p>
	<ul style="list-style-type: none"> <li>If no site visits have been undertaken indicate why this is the case.</li> </ul>	N/A
Geological interpretation	<ul style="list-style-type: none"> <li>Confidence in (or conversely, the uncertainty of ) the geological interpretation of the mineral deposit.</li> </ul>	<p>For Beresford and Allanson, the confidence in the geological interpretation is chiefly very high, which is based on mining exposure as well as a broadly high drilling density. Visual confirmation of lode orientations has been observed and mapped in underground development headings and the Westralia open pit.</p> <p>For Morgans North – Phoenix Ridge, the confidence in the geological model is moderate, with a lower confidence resulting from the lower drilling density, and heavy clustering where drilling density is high. The nature of structural controls on mineralisation and the differentiation into sharply offset fault blocks have not been established. No underground mining exposures are available to review the geological model, which extends to depths similar to Beresford.</p>
	<ul style="list-style-type: none"> <li>Nature of the data used and of any assumptions made.</li> </ul>	<p>Geological and structural logging and underground mapping have been used to assist identification and delineation of lithology and mineralisation.</p> <p>For modelling of all lodes, where high-grade mineralisation was present outside the logged BIF unit but adjacent to the contact, and continuity was present, the lode wireframe was extended laterally to include the sample.</p> <p>All lodes were treated as hard-boundaries for statistics and estimation.</p>
	<ul style="list-style-type: none"> <li>The effect, if any, of alternative interpretations on Mineral Resource</li> </ul>	<p>Previous attempts to interpret mineralisation for Beresford and Morgans North – Phoenix Ridge focused on grade-</p>



Criteria	JORC Code explanation	Commentary
	estimation.	<p>based, hard-boundary wireframes. This resulted in lower tonnages and higher grades than achievable in mining practice, as shown by reconciliation. These interpretations incorrectly assumed that higher grade populations may be joined up within the same stratigraphic unit, often across the bedding plane for the unit, so that mineralisation at the footwall and hanging wall contacts was included in the same mineralisation wireframe without evidence from cross-cutting structural controls. Intersections of higher-grade mineralisation show much lower continuity. Therefore, this approach has been discarded in favour of modelling of the geological controls on the mineralisation, which was undertaken for the previous estimate at Allanson.</p> <p>At Allanson and Beresford, previous estimates used high-grade limiting boundaries on the stratigraphic lodes, which prevented the influence of low-grade samples from the estimate within the high-grade zones. No visual continuity was established to support such high-grade boundaries, and contact analysis statistics for Fault Block 5 and 7 Red and Blue 1 BIFs of Beresford showed no evidence for domain boundaries.</p>
	<ul style="list-style-type: none"> <li>The use of geology in guiding and controlling Mineral Resource estimation.</li> </ul>	<p>Geology was the primary driver in the MRE, as each lode was formed from the BIF units as the hosts for mineralisation. Within each lode, whose modelling is outlined below, the estimate was constrained to blocks within the lode wireframe using only top-cut composited samples from the corresponding lode.</p> <p>For Beresford, moving from east to west from the hanging-wall to the footwall of the deposit, the stratigraphy is represented by Alpha BIF units named Red, Blue 1, Blue 2, Contact, Orange, Orange Repeat 1 and Orange Repeat 2, and Bravo package. Each fault block (FB) 5 through 12 formed a separate lode, with FB5 the largest as currently modelled, lying under Millionaires pit, and FB6 under FB 5 across an unnamed fault. FB12 is the deepest fault blocks and lies down-plunge from FB6 across the moderately south-plunging Sprint – Splay fault. FB7 lies under the historic Westralia pit, and along strike to the north of FB5. Under FB7 lies FB8, FB9 and FB10. Northwards and up-plunge of the Sprint – Splay Fault lies FB11.</p> <p>The distinct geological differences between each BIF unit, and the change in orientation between each Fault Block, prevented lode samples from being grouped for domain geostatistics. Further checks of statistics also confirmed that each lode formed distinct grade distributions. Not all units were present within each BIF, resulting in 67 lodes estimated.</p> <p>For Allanson, moving from east to west from the hanging-wall to the footwall of the deposit, the BIF stratigraphy is not divided into fault blocks, as it represents a smaller strike length than Beresford, within which the BIF units pinch out through lack of development to confirm mine scale faults. Moving from the The Alpha package is represented by only Red, Blue 1 and Contact. The Bravo package of BIF units has been separated into the Edga and Sarina units, and Allanson also includes the Charlie package consisting of the Monica and Rosie units, and the MRG (Morgans) and Package E units. The stratigraphic modelling resulted in 32 lodes.</p> <p>For Morgans North – Phoenix Ridge, moving from east to west from the hanging-wall to the footwall of the deposit,</p>

Criteria	JORC Code explanation	Commentary
		the stratigraphic model consists of Alpha package units of Red, Blue and Contact BIFs, and the Bravo package of Contact and “Bravo Package”, resulting in 29 lodes modelled.
	<ul style="list-style-type: none"> <li>The factors affecting continuity both of grade and geology.</li> </ul>	<p>The presence of structures within the BIF units, together with proximity to thickening across the BIF units, has led to higher-grade mineralisation. However, the structures are often not able to be discerned for structural measurements, and provide little continuity for 3D modelling, and as such they are not used to constrain the grade estimates.</p> <p>Geostatistical analysis showed that several lodes of Beresford formed variograms with short-range structures being longer in the semi-major direction for the full variogram range than the major direction. This is notable for the hanging-wall sequence in FB5 and FB7 of Red, Blue 1 and Blue 2, which confirms the structural observations of the alternate influences on mineralisation of the shallow, north plunging and moderately steep, south plunging structural controls.</p>
Dimensions	<ul style="list-style-type: none"> <li>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</li> </ul>	The Westralia Mineral Resource area extends over a SE-NW strike length of 2.2 km (from 9,900 m N – 12,250 m N), has a maximum width of 130 m (9900 m E – 10,940 m E) and extends from 2,500 m RL – 1,220 m RL.
Estimation and modelling techniques	<ul style="list-style-type: none"> <li>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</li> </ul>	<p>Samples were composited to 1 m intervals (“composites”) based on assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.</p> <p>The following high-grade top-cuts were applied to the mineralisation domains following statistical analysis (review of completed in Snowden Supervisor™ software:</p> <ul style="list-style-type: none"> <li>Beresford: 4 g/t – 68 g/t; 40 of 67 lodes</li> <li>Allanson: 3 g/t – 41 g/t; 24 of 32 lodes</li> <li>Morgans North – Phoenix Ridge: 4 g/t – 92 g/t; 15 of 29 lodes</li> </ul> <p>The top-cuts were generally kept at around 1% – 2% of the grade distribution for each lode, unless a the consistent, log-normal distribution justified a lower proportion cut, or an erratic upper tail of the distribution justified a higher proportion cut.</p> <p>To model the spatial continuity of gold grades, variography was conducted in Supervisor 8.13. Statistics were length-weighted.</p> <p>Composite samples were declustered prior to variography. A normal-score transform was applied to all data.</p> <p>Variograms were modelled for 27 of the 67 Beresford lodes, 11 of the 32 Allanson lodes and 9 of the 29 Morgans North – Phoenix Ridge lodes. A high proportion of the experimental variograms allowed robust modelling of variograms, which incorporated short-range and long-range spherical or exponential structures. The other lodes with less samples showed poorer experimental semivariograms, and as such variograms were borrowed from the better-informed lodes of the same BIF unit for all models, and further only within the same fault block for Beresford.</p> <p>For Beresford FB5 Red and Blue 1, three spherical structures were modelled, whereas two spherical or exponential structures were modelled for every other major lode.</p> <p>After variograms were modelled, a back-transform model was exported with Surpac rotations for use in Surpac parameter files. All variograms contained a very low to low</p>

Criteria	JORC Code explanation	Commentary
		<p>nugget when back-transformed, and typically a very high proportion of the variance accounted for in the short-range structure.</p> <p>Kriging neighbourhood analysis (KNA) was undertaken using Supervisor™ software to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE), slope of regression (SOR) and negative weights were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids.</p> <p>As face samples have not been used in every pass and they are highly clustered with significant sample bias, their influence was not considered in the KNA.</p> <p>Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains and low-grade halo domains around the mineralisation, inside which the composites for the high-grade domain were removed. The technique is considered appropriate to allow the grades to be weighted to the geostatistics calculated from variography.</p> <p>The small block size appropriately reflects the inputs of the underground scenario, and the sample spacing.</p> <p>For Beresford and Allanson, the estimate employed a five-pass search strategy to improve the local grade estimate for well-informed blocks and to ensure all blocks received a grade estimate.</p> <p>Each estimation pass used anisotropic ratios defined by the variogram for the lode, and which used samples from the corresponding lode only.</p> <p>The first pass for Beresford and Allanson estimated from composites within an anisotropic search ellipse segmented into octants that had a major direction of 30 m, as this was visually estimated as the average first spherical structure across the two deposits, and KNA established that the best statistics were achieved in smaller search neighbourhoods, although below the size of 30 m in the major direction very few blocks were estimated. This first pass search neighbourhood allowed the clustered face samples to inform the estimate in a very small search area to improve the local estimate and prevent them causing wider estimation bias. The estimate for the first pass was restricted to search ellipses with at least three adjacent octants containing composites.</p> <p>The second pass for Beresford and Allanson, and the first pass for Morgans North – Phoenix Ridge utilised an anisotropic search ellipse with a major direction distance of 40 m.</p> <p>The third pass for the three models did not use dynamic anisotropy to prevent wildly fluctuating large ellipses from weighting samples in high angles to the prevailing orientations of the lodes. The anisotropic search ellipse major distance was the full range of the variogram for all lodes other than Beresford Red and Blue 1 in Fault Block 5, which was set at the second spherical structure, as the third structure was much greater than models for other lodes.</p> <p>Geological modelling and database zone-coding were undertaken in Leapfrog Geo 6.0 software.</p> <p>Compositing, block modelling and grade estimation were undertaken using Surpac™ 2020 software.</p>

Criteria	JORC Code explanation	Commentary
		The estimation technique is appropriate to allow a locally adequate estimate for detailed mine planning and with a globally unbiased estimate per lode.
	<ul style="list-style-type: none"> <li>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</li> </ul>	Previous estimates provided lower overall tonnages with higher grades, which have not been achieved in production. However, production figures are not able to be reconciled with confidence, as material from Beresford and Allanson were blended together with Jupiter material prior to crushing at the Jupiter mill.
	<ul style="list-style-type: none"> <li>The assumptions made regarding recovery of by-products.</li> </ul>	No assumptions have been made regarding the recovery of by-products.
	<ul style="list-style-type: none"> <li>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</li> </ul>	No deleterious or other non-grade variables have been estimated.
	<ul style="list-style-type: none"> <li>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</li> </ul>	<p>A parent block size of 5 m x 10 m x 10 m (X x Y x Z) was chosen, which was supported KNA and by drill hole spacing in KNA Y and Z directions. The sample direction chiefly parallels the X direction, which is also across the strike of the BIF lenses, and therefore the block size was shorter to account for this. Some areas of tighter drilling at grade control density exist, but most of the deposit has been sampled at a density of 10 m x 10 m (Y by Z) out to 100 m x 100 m on the fringes. The dominant 1 m sample length support the shorter block height. Nominally spaced 10 m to 20 m pierce points have been achieved in the Y-Z plane, although this is highly variable resulting from the variable hole angles.</p> <p>Sub-celling to 1/8 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.</p>
	<ul style="list-style-type: none"> <li>Any assumptions behind modelling of selective mining units.</li> </ul>	No assumptions have been made regarding SMUs.
	<ul style="list-style-type: none"> <li>Any assumptions about correlation between variables.</li> </ul>	Only gold assays were available, and as such no analysis could be undertaken.
	<ul style="list-style-type: none"> <li>Description of how the geological interpretation was used to control the resource estimates.</li> </ul>	Geology was the primary driver in the MRE, as each lode was formed from the BIF units as the hosts for mineralisation. Within each lode, whose modelling is outlined below, the estimate was constrained to blocks within the lode wireframe using only top-cut composited samples from the corresponding lode.
	<ul style="list-style-type: none"> <li>Discussion of basis for using or not using grade cutting or capping.</li> </ul>	<p>High-grade top-caps were applied to limit the influence of extreme outliers on the grade estimate. The top-caps were applied to the mineralisation domains following statistical analysis.</p> <p>The top-cuts were generally kept at around 1% – 2% of the grade distribution for each lode, unless a the consistent, log-normal distribution justified a lower proportion cut, or an erratic upper tail of the distribution justified a higher proportion cut.</p>
	<ul style="list-style-type: none"> <li>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</li> </ul>	Validation of the estimate was completed for the resource block models using numerical methods (histograms, CDFs and swath plots) and validated visually against the input raw drillhole data, declustered data, composites and blocks.
Moisture	<ul style="list-style-type: none"> <li>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</li> </ul>	Tonnages and grades have been estimated on a dry in situ basis.
Cut-off parameters	<ul style="list-style-type: none"> <li>The basis of the adopted cut-off grade(s) or quality parameters applied.</li> </ul>	The Mineral Resource has been reported at a 2.0 g/t Au cut-off.

Criteria	JORC Code explanation	Commentary
		<p>The reporting cut-off parameters were selected based on known underground economic cut-off grades.</p> <p>The potential to extract mineralisation via open pit mining methods is expected to be reviewed as part of a scoping study for Westralia. Until then, Mineral Resources have only been considered for extraction via underground mining methods, and as such a lower reporting cut-off has not been selected for the near-surface mineralisation at Millionaires and Morgans North.</p>
Mining factors or assumptions	<ul style="list-style-type: none"> <li>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</li> </ul>	<p>Beresford and Allanson deposits were mined until April 2020 using underground long hole stoping methods. It is assumed the Mineral Resource will be mined using the same methods for underground.</p> <p>The potential to extract mineralisation via open pit mining methods is expected to be reviewed as part of a scoping study for Westralia. Until then, Mineral Resources have only been considered for extraction via underground mining methods.</p>
Metallurgical factors or assumptions	<ul style="list-style-type: none"> <li>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</li> </ul>	<p>The ore has been processed at the adjacent Jupiter Processing Facility, part of the MMGO. Recoveries achieved to date are 92.3%.</p>
Environmental factors or assumptions	<ul style="list-style-type: none"> <li>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</li> </ul>	<p>Westralia is an active underground mine at the Mount Morgans Gold Operation with all requisite environmental approvals in place.</p> <p>Waste rock is stored in a conventional waste dump.</p>
Bulk density	<ul style="list-style-type: none"> <li>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</li> </ul>	<p>Bulk density has been assigned to mineralisation and waste lodes separately following statistical analysis of 43,956 diamond core immersion method bulk density determinations.</p> <p>The results were consistent across Beresford, Allanson and Morgans North – Phoenix Ridge by RL for waste, and showed marginal variability with BIF units.</p> <p>Analysis showed that no relationship exists by BIF unit or, for Beresford, by FB with depth, other than the upper 100 m, where a gradational increase with depth for all BIF units across the deposits was observed in the immersion method data. The density increases to around 2.95 t/m<sup>3</sup> before</p>

Criteria	JORC Code explanation	Commentary																																																																																														
		<p>dropping to 2.91 t/m<sup>3</sup> for Beresford and Allanson, which was assigned to the base of the model from m RL.</p> <p>Waste showed a similar relationship with depth, although lower overall values, and stabilised once reaching a maximum of 2.84 t/m<sup>3</sup>.</p> <p>Density assignments by RL for waste and BIF material are shown in the tables below.</p> <p>Density assignment by base RL for all waste (non-BIF):</p> <table><thead><tr><th>RL</th><th>Density value</th></tr></thead><tbody><tr><td>0</td><td>2.84</td></tr><tr><td>2370</td><td>2.84</td></tr><tr><td>2380</td><td>2.83</td></tr><tr><td>2390</td><td>2.72</td></tr><tr><td>2400</td><td>2.71</td></tr><tr><td>2410</td><td>2.69</td></tr><tr><td>2420</td><td>2.67</td></tr><tr><td>2430</td><td>2.52</td></tr><tr><td>2440</td><td>2.39</td></tr></tbody></table> <p>Density assignment by base RL for Beresford BIF</p> <table><thead><tr><th>RL</th><th>Density value</th></tr></thead><tbody><tr><td>0</td><td>2.88</td></tr><tr><td>1680</td><td>2.92</td></tr><tr><td>1970</td><td>2.95</td></tr><tr><td>2300</td><td>2.99</td></tr><tr><td>2310</td><td>2.95</td></tr><tr><td>2320</td><td>2.95</td></tr><tr><td>2330</td><td>2.95</td></tr><tr><td>2340</td><td>2.91</td></tr><tr><td>2350</td><td>2.91</td></tr><tr><td>2360</td><td>2.91</td></tr><tr><td>2370</td><td>2.91</td></tr><tr><td>2380</td><td>2.72</td></tr><tr><td>2390</td><td>2.71</td></tr><tr><td>2410</td><td>2.69</td></tr><tr><td>2420</td><td>2.67</td></tr><tr><td>2430</td><td>2.52</td></tr><tr><td>2440</td><td>2.39</td></tr></tbody></table> <p>Density assignment by base RL for Allanson BIF</p> <table><thead><tr><th>RL</th><th>Density value</th></tr></thead><tbody><tr><td>0</td><td>2.91</td></tr><tr><td>2300</td><td>2.91</td></tr><tr><td>2310</td><td>2.99</td></tr><tr><td>2320</td><td>2.95</td></tr><tr><td>2330</td><td>2.95</td></tr><tr><td>2340</td><td>2.95</td></tr><tr><td>2350</td><td>2.91</td></tr><tr><td>2360</td><td>2.91</td></tr><tr><td>2370</td><td>2.91</td></tr><tr><td>2380</td><td>2.84</td></tr><tr><td>2390</td><td>2.82</td></tr><tr><td>2400</td><td>2.80</td></tr><tr><td>2410</td><td>2.65</td></tr><tr><td>2420</td><td>2.52</td></tr><tr><td>2430</td><td>2.42</td></tr><tr><td>2440</td><td>2.39</td></tr></tbody></table> <p>Density assignment by base RL for Morgans North – Phoenix Ridge BIF</p> <table><thead><tr><th>RL</th><th>Density value</th></tr></thead><tbody><tr><td>0</td><td>2.99</td></tr></tbody></table>	RL	Density value	0	2.84	2370	2.84	2380	2.83	2390	2.72	2400	2.71	2410	2.69	2420	2.67	2430	2.52	2440	2.39	RL	Density value	0	2.88	1680	2.92	1970	2.95	2300	2.99	2310	2.95	2320	2.95	2330	2.95	2340	2.91	2350	2.91	2360	2.91	2370	2.91	2380	2.72	2390	2.71	2410	2.69	2420	2.67	2430	2.52	2440	2.39	RL	Density value	0	2.91	2300	2.91	2310	2.99	2320	2.95	2330	2.95	2340	2.95	2350	2.91	2360	2.91	2370	2.91	2380	2.84	2390	2.82	2400	2.80	2410	2.65	2420	2.52	2430	2.42	2440	2.39	RL	Density value	0	2.99
RL	Density value																																																																																															
0	2.84																																																																																															
2370	2.84																																																																																															
2380	2.83																																																																																															
2390	2.72																																																																																															
2400	2.71																																																																																															
2410	2.69																																																																																															
2420	2.67																																																																																															
2430	2.52																																																																																															
2440	2.39																																																																																															
RL	Density value																																																																																															
0	2.88																																																																																															
1680	2.92																																																																																															
1970	2.95																																																																																															
2300	2.99																																																																																															
2310	2.95																																																																																															
2320	2.95																																																																																															
2330	2.95																																																																																															
2340	2.91																																																																																															
2350	2.91																																																																																															
2360	2.91																																																																																															
2370	2.91																																																																																															
2380	2.72																																																																																															
2390	2.71																																																																																															
2410	2.69																																																																																															
2420	2.67																																																																																															
2430	2.52																																																																																															
2440	2.39																																																																																															
RL	Density value																																																																																															
0	2.91																																																																																															
2300	2.91																																																																																															
2310	2.99																																																																																															
2320	2.95																																																																																															
2330	2.95																																																																																															
2340	2.95																																																																																															
2350	2.91																																																																																															
2360	2.91																																																																																															
2370	2.91																																																																																															
2380	2.84																																																																																															
2390	2.82																																																																																															
2400	2.80																																																																																															
2410	2.65																																																																																															
2420	2.52																																																																																															
2430	2.42																																																																																															
2440	2.39																																																																																															
RL	Density value																																																																																															
0	2.99																																																																																															



Criteria	JORC Code explanation	Commentary																												
		<table><tr><td>2310</td><td>2.99</td></tr><tr><td>2320</td><td>2.95</td></tr><tr><td>2330</td><td>2.95</td></tr><tr><td>2340</td><td>2.95</td></tr><tr><td>2350</td><td>2.91</td></tr><tr><td>2360</td><td>2.91</td></tr><tr><td>2370</td><td>2.91</td></tr><tr><td>2380</td><td>2.91</td></tr><tr><td>2390</td><td>2.65</td></tr><tr><td>2400</td><td>2.65</td></tr><tr><td>2410</td><td>2.65</td></tr><tr><td>2420</td><td>2.52</td></tr><tr><td>2430</td><td>2.42</td></tr><tr><td>2440</td><td>2.4</td></tr></table>	2310	2.99	2320	2.95	2330	2.95	2340	2.95	2350	2.91	2360	2.91	2370	2.91	2380	2.91	2390	2.65	2400	2.65	2410	2.65	2420	2.52	2430	2.42	2440	2.4
2310	2.99																													
2320	2.95																													
2330	2.95																													
2340	2.95																													
2350	2.91																													
2360	2.91																													
2370	2.91																													
2380	2.91																													
2390	2.65																													
2400	2.65																													
2410	2.65																													
2420	2.52																													
2430	2.42																													
2440	2.4																													
	<ul style="list-style-type: none"><li>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</li></ul>	<p>Void space has been accounted for in the industry-standard, immersion method core density determination process. Measurements were separated for rock type and alteration zones.</p> <p>It is assumed there are minimal void spaces in the rocks at Westralia. The MRE contains minor amounts of oxide and transitional material above the fresh bedrock.is no obvious correlation between bulk density and gold grade across the mineralised lodes.</p>																												
	<ul style="list-style-type: none"><li>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</li></ul>	<p>Analysis showed that no relationship exists by BIF unit or, for Beresford, by FB with depth, other than the upper 100 m, where a gradational increase with depth for all BIF units across the deposits was observed in the immersion method data. The density increases to around 2.95 t/m³ before dropping to 2.91 t/m³ for Beresford and Allanson, which was assigned to the base of the model from m RL.</p> <p>Waste showed a similar relationship with depth, although lower overall values, and stabilised once reaching a maximum</p>																												
Classification	<ul style="list-style-type: none"><li>The basis for the classification of the Mineral Resources into varying confidence categories.</li></ul>	<p>The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:</p> <ul style="list-style-type: none"><li>Drill density data</li><li>Geological understanding</li><li>Quality of gold assay grades</li><li>Continuity of gold grades</li><li>Economic potential for mining.</li></ul> <p>Unclassified material:</p> <ul style="list-style-type: none"><li>Mined areas and any unstoped material along drives and between mined stopes where substantial and prohibitive backfilling would be required, making the volumes fail the JORC Code Clause 20 reasonable prospects test.</li><li>The zone between Beresford South and North cannot be joined, and therefore a volume has been set as unclassified.</li></ul> <p>For Indicated Mineral Resources, statistical consideration has been employed to assess the grade estimate quality in considering large, contiguous and coherent zones of blocks form zones where:</p> <ul style="list-style-type: none"><li>Large areas are formed that encircle measured and all GC areas, but also extending out to where drill hole spacing reaches 25 m to 30 m max.</li><li>Estimation was undertaken in search passes of 1 and 2.</li><li>Number of samples was near the optimum.</li></ul>																												

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Slope of regression formed large volumes of &gt; 0.4 with cores of 0.6..</li> <li>The drilling density sharply reduces in the north and south extents of any lode. In these cases, the boundary was tightly constrained, unless the statistics showed that the estimate was poorer at these limits, in which cases the Indicated boundary was reduced.</li> </ul> <p>For Beresford and Allanson, Measured Mineral Resources required the following additional considerations:</p> <ul style="list-style-type: none"> <li>In and around GC areas or DH density of 10 m spacing only where face samples and resource drilling provide high numbers of holes and samples</li> <li>Slope of regression formed large volumes of &gt; 0.7.</li> <li>Average distance to samples was low.</li> </ul> <p>For Beresford and Allanson, Mineralisation volumes that had been depleted by mined material (i.e. blocks within underground voids, as built for both stopes and development) was left unclassified. Mineralisation that was unmined was further reviewed with the mine planning engineering team to incorporate their significant experience and knowledge of mining of Westralia. Where material is considered infeasible for extraction due to either complete destruction of access to other parts of the underground, or could only be extracted with prohibitive costs, it was set to unclassified. This meets the criteria for Clause 20 of the JORC Code (material may only be classified as Mineral Resources if it has reasonable prospects of eventual economic extraction).</p>
	<ul style="list-style-type: none"> <li>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</li> </ul>	All factors the Competent Person has deemed relevant to the MRE have been incorporated into the classification of Mineral Resources.
	<ul style="list-style-type: none"> <li>Whether the result appropriately reflects the Competent Person's view of the deposit.</li> </ul>	The result appropriately reflects the Competent Person's view of the deposit.
Audits or reviews	<ul style="list-style-type: none"> <li>The results of any audits or reviews of Mineral Resource estimates.</li> </ul>	Internal audits were completed by Dacian, which verified the technical inputs, methodology, parameters and results of the estimate.
Discussion of relative accuracy/ confidence	<ul style="list-style-type: none"> <li>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</li> </ul>	The accuracy of the MREs is communicated through the classification assigned to the various parts of the deposits. The MREs have been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this table.
	<ul style="list-style-type: none"> <li>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</li> </ul>	The MRE statement relates to a global estimate of in-situ tonnes and grade.
	<ul style="list-style-type: none"> <li>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</li> </ul>	N/A

## Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
<b>Sampling techniques</b>	<i>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i>	<ul style="list-style-type: none"> <li>Surface and underground (UG) Diamond (DD) core, surface Reverse Circulation (RC) chips and surface RC chips with DD tail (RCD) core informed both the Transvaal and Craic Mineral Resource estimates (MRE).</li> <li>Underground drive face samples taken by chipping channels cut into drive faces were also used to inform the Craic MRE within the first pass of the grade estimate.</li> <li>Quantitative wireline gamma-density data was captured by geophysical sondes in Dacian RC and DD holes for informing the density estimates.</li> </ul>
	<i>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</i>	<ul style="list-style-type: none"> <li>Dacian surface diamond core was sampled as half core at 1m intervals or to geological contacts. To ensure representative sampling, half core samples were always taken from the same side of the core.</li> <li>Dacian RC holes were sampled over the entire length of hole. Dacian RC drilling was sampled at 1m intervals via an on-board cone splitter.</li> <li>Face samples were sampled across the full length of the drive face, perpendicular to the lode orientations, and to geological contacts.</li> <li>Geophysical sondes used in the wireline data capture were calibrated against known density standards and repeat logging of a calibration hole at Mt Morgans.</li> <li>The wireline gamma-density data were compared to the core density for transitional material, which showed that acceptable correlations existed for inclusion of either dataset in the MRE.</li> </ul>
	<i>Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</i>	<ul style="list-style-type: none"> <li>RC holes within mineralisation were dominantly sampled on 1 m intervals in mineralisation via either a riffle splitter or on-board cone splitter mounted at the base of the cyclone to achieve a representative split of approximately 3 kg samples.</li> <li>Diamond core was sampled as half core if drilled from surface or full core if UG on 1 m intervals or to geological contacts, sampled into lengths in sample bags to achieve approximately 3 kg.</li> <li>Dacian surface RC holes were sampled over the entire length of hole.</li> <li>Surface samples were submitted to NATA certified contract laboratory for crushing and pulverising to produce either a 40 g or 50 g charge for fire assay with an atomic absorption spectrometry (AAS) finish.</li> <li>Face samples were collected by Range River on underground drives on 4.5 m – 5.5 m advances across the full width of the face and perpendicular to lode orientations on approximately 1 m lengths or to geological contacts. The samples were collected by cutting channels into the drive face and chipping pieces of the channel into sample bags.</li> <li>Face samples and UG DD core was submitted to an on-site laboratory for crushing and pulverizing. The sample charge size for fire assay is unknown, but is believed to have been either from 30 g to 50 g, with an atomic absorption spectrometry (AAS) finish.</li> </ul>
<b>Drilling techniques</b>	<i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i>	<ul style="list-style-type: none"> <li>Drilling that informed the Craic MRE included 91 Reverse Circulation (RC) drill holes for 31,344.2 m, 91 diamond (DD) holes for 9,045.17 m, seven RC holes with diamond tails (RCD) for 1,279.2 m and 113 face samples for 427.08 m.</li> <li>Drilling that informed the Transvaal MRE update included 623 Reverse Circulation (RC) drill holes for 56640 m, 274 diamond (DD) holes for 18,736.55 m, and 52 RCD holes for 16,851.79 m. Face samples were not included for the Transvaal MRE, as no information was available for them.</li> <li>Drilling that intersected modelled Transvaal mineralisation and was used to estimate grades for the MRE update, included 1,307 RC drill holes for 17,277.52 m, 654 diamond (DD) holes for 4,983.11 m, and 353 RCD holes for 4,647.29 m.</li> <li>Drilling that intersected modelled Craic mineralisation and was used to estimate grades for the MRE update, included 498 RC drill holes for 1,707.22 m, 79 diamond (DD) holes for 195.64 m, 6 RCD holes for 23.16 m, and 74 face samples for 147.75 m</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Nearly 100% of holes that intersected Craic mineralisation were drilled since from 1990, 95% since 2000, and 4% by Dacian.</li> <li>87% of holes that intersected Transvaal mineralisation were drilled since from 1990, 13% since 2000, and 10% by Dacian.</li> <li>Reverse circulation (RC) drilling and surface diamond drilling informed the Minerals Resource estimate (MRE) for Transvaal and Craic, while face sampling of drives informed the first pass only for Craic.</li> <li>For Dacian RC holes, a 5¼" to 5 ¾" face sampling hammer bit was used.</li> <li>UG DD drilling was mostly sampled whole core with NQ2 sized equipment.</li> <li>Dacian DD was sampled as half core, mostly HQ3 and PQ3 with minor PQ2.</li> </ul>
<b>Drill sample recovery</b>	<i>Method of recording and assessing core and chip sample recoveries and results assessed.</i>	<ul style="list-style-type: none"> <li>Recoveries from historical holes are unknown.</li> <li>Recoveries from Dacian diamond drilling were measured and recorded into the database.</li> </ul>
	<i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i>	<ul style="list-style-type: none"> <li>Dacian RC holes were drilled with a powerful rig with compressor and booster compressor to ensure enough air to maximise sample recovery. The splitter was cleaned at the end of each rod, to ensure that efficient sample splitting. The weight of each sample split was monitored. Drilling was stopped if the sample split size changed significantly.</li> <li>Dacian RC drilling activities, sample volumes, quality and recoveries were monitored by the supervising geologist to ensure good recoveries</li> <li>Sample splitters were cleaned on a regular basis.</li> <li>As the UG DD core has a smaller diameter, the core was sampled whole.</li> </ul>
	<i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i>	<ul style="list-style-type: none"> <li>No relationship has been noted between sample recovery and grade.</li> </ul>
<b>Logging</b>	<i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i>	<ul style="list-style-type: none"> <li>All RC holes were logged for geology, alteration, and visible structure.</li> <li>All RC chip trays were photographed.</li> <li>All drill holes were logged in full.</li> <li>RC drilling was logged by passing a portion of each sampled metre into a sieve to remove rock flour from coarse chips, the chips are then washed and placed into metre marked chip trays for logging. The un-sieved sample was also observed for logging purposes. For Dacian drilling, where the material type does not allow for the recovery of coarse rock chips the rock flour is retained as a record. The detail is considered common industry practice and is at the appropriate level of detail to support the MRE.</li> <li>Dacian's DD core was photographed wet and dry, and geotechnically logged to industry standards.</li> <li>For historical RC drilling, where available the original logs and laboratory results are retained by Dacian as either original hard copies or as scanned copies.</li> <li>The Competent Person is satisfied that the logging detail supports the MRE.</li> </ul>
	<i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i>	<ul style="list-style-type: none"> <li>All holes were logged qualitatively by geologists familiar with the geology and control on the mineralisation for various geological attributes including weathering, primary lithology, primary &amp; secondary textures, colour and alteration.</li> <li>For Dacian drilling, diamond core was photographed both wet and dry. For RC drilling chip trays are photographed. Diamond core is retained on site.</li> <li>The wireline gamma-density data is quantitative in nature.</li> </ul>
	<i>The total length and percentage of the relevant intersections logged.</i>	<ul style="list-style-type: none"> <li>All surface diamond drill holes were logged for recovery, RQD, geology, and structure. Structural measurements were taken using a kenometer to record alpha and beta angles relative to a bottom of hole line marked on the oriented core. The quality of the bottom of hole orientation line is also recorded.</li> <li>All drill holes were logged in full, from start of hole to bottom of hole.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Sub-sampling techniques and sample preparation</b>	<i>If core, whether cut or sawn and whether quarter, half or all core taken.</i>	<ul style="list-style-type: none"> <li>Core was cut in half using a core saw at either 1 m intervals or to geological contacts; core samples were collected from the same side of the core where orientations were completed.</li> </ul>
	<i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i>	<ul style="list-style-type: none"> <li>Dacian RC samples were collected via on-board cone splitters. Most samples were dry, any wet samples are recorded as wet, this data is then entered into the sample condition field in the drillhole database.</li> <li>At all times, an attempt was made to keep samples dry. If due to significant groundwater inflow or drilling limitations sample quality became degraded (consecutive intervals of wet sample or poor sample recovery), the RC hole was abandoned.</li> <li>The RC sample was split using the cone splitter to give an approximate 3kg sample. The remainder was collected into a plastic sack as a retention sample. At the grain size of the RC chips, this method of splitting is considered appropriate.</li> <li>Dominion historical RC samples were collected at the rig using riffle splitters if dry while wet samples were bagged for later splitting. Samples condition was not recorded for a majority of the historic sampling. For historic RC drilling, information on the QAQC programs used is limited but acceptable with original batch reports having been reviewed and retained by Dacian.</li> </ul>
	<i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i>	<ul style="list-style-type: none"> <li>For RC drilling, the sub-sample preparation by splitting by cone or riffle splitters is an industry standard method of creating a representative split.</li> <li>For non-grade control (GC) RC surface drilling, sample preparation was conducted by contract, National Association of Testing Authorities (NATA) Australia accredited laboratories.</li> <li>After drying, Dacian samples were subject to a primary crush, then pulverised and homogenised to 85% passing 75µm before a 40 g or 50 g charge was scooped. This is an industry standard and appropriate method for preparing samples for fire assay.</li> </ul>
	<i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i>	<ul style="list-style-type: none"> <li>For Dacian RC drilling, RC field duplicates were taken from the on-board cone splitter at 1 in 50 or 1 in 25 for exploration and infill drilling respectively.</li> <li>Externally prepared Certified Reference Materials were inserted within the sample stream for QAQC.</li> <li>Dacian completed a drilling program of RC and diamond drilling in 2013 to confirm and infill Transvaal historic sampling. A total of seven RC drill holes were completed for 1,462m and nine diamond drill holes with RC precollars were completed for 4,345.65m.</li> <li>In addition sampling of one historical diamond drill hole, 94TVRD004 was completed in 2014. Much of the historical assay information for the Transvaal drilling comprises large generic assay batches (not original batches) that only have gold values and do not include weight or lab QC information. These batches may not have assay method information included (currently UN_UN).</li> <li>For the Range River data, a total of seven original batches were able to be sourced. These have been loaded with QC information, however sample weights were not originally reported with these batches.</li> <li>The Competent Person has reviewed the analysis of available historic QC samples, and the Dacian confirmatory/infill drilling, and found that the available results showed a low risk to reporting a MRE.</li> <li>The internal consistency of the downhole gamma-density data was demonstrated by repeat logging of against a calibration hole at Mt Morgans.</li> <li>Prior to mobilisation to site, the instrument was calibrated immediately against standard materials for density.</li> <li>A high correlation was shown between the gamma-density and core density determinations.</li> </ul>
	<i>Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.</i>	<ul style="list-style-type: none"> <li>For Dacian exploration DD drilling field duplicates were not taken.</li> <li>For Dacian RC drilling, field duplicates are generally taken a 1 in 25 samples.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i>	<ul style="list-style-type: none"> <li>Sample sizes are considered appropriate to correctly represent the gold mineralisation based on the style of mineralisation, the thickness and consistency of the intersections, the sampling methodology and assay value ranges for gold.</li> </ul>
<b>Quality of assay data and laboratory tests</b>	<i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i>	<ul style="list-style-type: none"> <li>For surface drilling, the analytical technique used was a 40g or 50g lead collection fire assay and analysed by Atomic Absorption Spectrometry (AAS). This is a full digestion technique. This is a commonly used method for gold analysis and is considered appropriate for this project.</li> <li>Non-GC Samples were analysed at NATA accredited laboratories.</li> <li>GC holes were analysed at an onsite lab using fire assay (50g).</li> <li>For Dacian drilling analysed at Bureau Veritas, sieve analysis was carried out by the laboratory to ensure the grind size of 85% passing 75µm was being attained.</li> <li>For Dacian surface RC and diamond drilling, QAQC procedures involved the use of certified reference materials, standards (1 in 20) and blanks (1 in 50). For diamond drilling additional coarse blanks and standards are submitted around observed mineralisation.</li> <li>Results were assessed as each laboratory batch was received and were acceptable in all cases.</li> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>No QAQC data has been reviewed for historic drilling, although mine production and twinned drill holes have validated drilling results. The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.</li> </ul>
	<i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i>	<ul style="list-style-type: none"> <li>Quantitative geophysical data, most notably wireline gamma-density data, were captured by Surtech using a dual-density instrument, sonde serial number 9239B, with logging by unit SL33, and a caesium radioactive source.</li> <li>The logging in counts-per-second (c/s) used a compensated density logging tool equipped with a Cs137 radioactive source.</li> <li>The CPS values were then converted to physical property values using calibrations determined specifically for each physical property parameter.</li> <li>The final data were supplied in a Logging ASCII Standard (CSV) file format.</li> <li>Single and three arm callipers were used in-hole to identify areas where blowouts and significant aberrations in the hole rugosity were encountered; any deviations from within 20% of the nominal hole diameter (1,460 mm for RC) were removed from the analysis.</li> </ul>
	<i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i>	<ul style="list-style-type: none"> <li>Certified reference materials demonstrate that sample assay values are accurate.</li> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>Commercial laboratories used by Dacian were audited in April 2021 by the Competent Person. The laboratory is monitored regularly by Dacian through QAQC practices, and strong communication channels are in place for data quality.</li> <li>Where QC data are available, acceptable levels of precision and accuracy have been established.</li> </ul>
<b>Verification of sampling and assaying</b>	<i>The verification of significant intersections by either independent or alternative company personnel.</i>	<ul style="list-style-type: none"> <li>Significant intersections were visually field verified by several company geologists.</li> </ul>
	<i>The use of twinned holes.</i>	<ul style="list-style-type: none"> <li>Recent confirmatory RC holes drilled with pierce points &lt;5 m from historic mineralisation pierce points have verified the intersections of historic mineralisation by either confirming the continuity of the mineralisation and geological interpretations or twinning the mineralisation.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<p><i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i></p>	<ul style="list-style-type: none"> <li>• Prior to 2021, primary data was collected into a custom logging Excel spreadsheet and then imported into a DataShed drillhole database. The logging spreadsheet included validation processes to ensure the entry of correct data.</li> <li>• From January 2021, primary data was collected into LogChief logging software by MaxGeo and then imported into a Data Shed drillhole database. Logchief has internal data validation.</li> </ul>
	<p><i>Discuss any adjustment to assay data.</i></p>	<ul style="list-style-type: none"> <li>• Assay values that were below detection limit are stored in the database in this form, but are adjusted to equal half of the detection limit value for grade estimates. The following records were set to half detection limit: <ul style="list-style-type: none"> <li>○ Negative below detection limit assays</li> <li>○ Zeros</li> <li>○ Nulls</li> <li>○ Unsampled intervals</li> </ul> </li> <li>• Any negatives below -1 were set to null, as these represent lab error codes such as samples not received, samples destroyed in sample preparation, insufficient sample volume/weight etc.</li> </ul>
<b>Location of data points</b>	<p><i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i></p>	<ul style="list-style-type: none"> <li>• All Dacian hole collars were surveyed in MGA94 Zone 51 grid using differential GPS to 3cm accuracy.</li> <li>• Craic UG DD and all Dacian RC holes were down hole surveyed with a north seeking gyro tool at &lt;=30m intervals down the hole.</li> <li>• For historic RC holes, surveys were either by magnetic camera shot or unknown. Most Transvaal surveys have an unknown method, but have been taken on 5 m to 10 m intervals at high precision, so it is assumed they are magnetic camera shot surveys.</li> <li>• Dacian DD holes were down hole surveyed with a north seeking gyro tool at 12m intervals down the hole.</li> <li>• Historic holes have no down hole survey information recorded.</li> <li>• Historic drill hole collar coordinates were tied to a local grid with subsequent conversion to MGA94 Zone 51. The transformation parameters were taken from the Dominion Mining reference manual, which were used to recalculate the collar positions in GDA94 MGA51 by the Competent Person as a check on the accuracy, finding little to no difference in the positions for Transvaal.</li> <li>• Craic: <ul style="list-style-type: none"> <li>○ For Craic, of the 1,342 DD, RCD, RC and face samples, 41 RC holes (3 drilled in 1986, 8 drilled in 1988, one drilled in 1990, 17 drilled in 1992 and 12 drilled in 1997) had an "Orig_Grid_ID" collar survey ID of "TVL" (Transvaal), all of which did not match the transform parameters. The greatest difference of the errors was 5.9 m.</li> <li>○ Of these holes with errors, three were beyond the limits of the mineralisation interpretation, 22 were drilled from surface above the current pit and whose intervals agreed with the waste or mineralisation in the surrounding holes, and the remainder were drilled under the pit and also agreed with the waste or mineralisation in the surrounding holes.</li> <li>○ The Competent Person reviewed the potential shift in the mineralisation interpretation and grade estimate, and concluded that there was no material impact on the MRE.</li> <li>○ Approximately 20% of the Craic face samples were found to be in impossible locations in relation to the UG development, which occurred from rounding or copying of Z/RL coordinate values from a previous record. The Competent Person noted that the mineralisation interpretation and grade estimate displayed high-visual correlation with the drives, and the resulting face sample locations were clearly located within the drives from logical vertical shift. Therefore, the Z coordinate/RL value in the database was adjusted to force the collar position to be ~1 m above the floor of the drive from which they were sampled.</li> <li>○ The Competent Person is satisfied that the recent Dacian 2021 drill holes have confirmed the locations of the mineralisation with acceptable accuracy for supporting the MRE.</li> </ul> </li> <li>• All Dacian hole collars were surveyed in MGA94 Zone 51 grid using differential GPS to within 3cm. Dacian holes were down-hole surveyed either with a north seeking gyroscopic tool at 30m intervals to 20cm accuracy.</li> <li>• Open pit (OP) and UG mine workings support the locations of historic drilling.</li> </ul>
	<p><i>Specification of the grid system used.</i></p>	<ul style="list-style-type: none"> <li>• The grid system used is MGA94 Zone 51 grid.</li> <li>• Historic drill hole collar coordinates were tied to a local grid with subsequent</li> </ul>

Criteria	JORC Code explanation	Commentary
		conversion to MGA94 Zone 51.
	<i>Quality and adequacy of topographic control.</i>	<ul style="list-style-type: none"> <li>Topographic surfaces were prepared from detailed ground, mine and aerial surveys.</li> <li>Material above all surfaces was coded in the model as depleted to ensure no mineralisation above these surfaces was included in the MRE.</li> <li>The Competent Person is satisfied that the topographic control provides the quality required to report the Mineral Resources in accordance with the JORC Code.</li> </ul>
<b>Data spacing and distribution</b>	<i>Data spacing for reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported</li> <li>The drill hole spacing is highly variable as a results of the variable drilling and sampling techniques.</li> <li>Craic and Transvaal RC GC holes have achieved a high density of mineralisation pierce points in and ~20 m below the pits of up to 4 m by 4 m.</li> <li>Craic face samples have been taken on 4 m advances, which has created a highly clustered dataset when incorporated with the exploration and resource drilling. Therefore, samples were declustered prior to statistics, and the face samples were used in the first estimation pass only.</li> <li>The exploration RC and DD holes are typically on 20 m sections, although they extend wider to 40 m sections outside of the modelled mineralisation.</li> <li>Transvaal holes and face samples have achieved a high density of mineralisation pierce points in well drilled areas of 5 m by 5 m to 20 m by 20 m, extending out to 80 m by 80 m on the fringes of the deposit.</li> </ul>
	<i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i>	<ul style="list-style-type: none"> <li>The mineralised domains have sufficient continuity in both geology and grade to be considered appropriate for the Mineral Resource estimation procedures and classification applied under the JORC Code, and the high correlation of historically mined lodes and mineralised structures with the mineralisation interpretation has further supported this.</li> </ul>
	<i>Whether sample compositing has been applied.</i>	<ul style="list-style-type: none"> <li>Samples have been composited to 1m lengths in mineralised lodes for statistics and estimation.</li> <li>Compositing was completed using a 'best-fit' method in Surpac software, which forces all samples to be included in one of the composites by adjusting composite lengths, while keeping it as close as possible to 1m.</li> </ul>
<b>Orientation of data in relation to geological structure</b>	<i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i>	<ul style="list-style-type: none"> <li>Surface holes were drilled at a planned bearing (azimuth) that approximates a perpendicular orientation of mineralised lodes.</li> <li>The nature of the UG DD holes means the drilling orientations are highly variable, but most holes achieve a high angle to the planes of mineralisation.</li> </ul>
	<i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i>	<ul style="list-style-type: none"> <li>No orientation-based sampling bias has been identified in the data.</li> </ul>
<b>Sample security</b>	<i>The measures taken to ensure sample security.</i>	<ul style="list-style-type: none"> <li>Chain of custody was managed by the companies that owned the projects at the time, and no issues regarding historic sample security are known.</li> <li>Dacian samples were stored on site until collected for transport to the sample preparation laboratory in Kalgoorlie. Dacian personnel had no contact with the samples once they are picked up for transport. Tracking spreadsheets were used by Dacian personnel to track the progress of samples.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of sampling techniques and data.</i>	<ul style="list-style-type: none"> <li>Regular reviews of RC and DD sampling techniques were completed by the Dacian Senior Geologists and the Principal Resource Geologist, which concluded that sampling techniques are satisfactory.</li> <li>No audits or reviews have been documented for historic sampling techniques, but the data have been reviewed by checking historic logging files with database records.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Commercial laboratories used by Dacian were audited in April 2021 by the Competent Person.</li> <li>The Competent Person visited the on-site contract laboratory twice in December 2020 to review processes. All laboratories were performing at and producing results for a standard required to report a MRE in accordance with the JORC Code.</li> <li>Review of Dacian QAQC data has been carried out by company geologists.</li> </ul>

## Transvaal and Craic

### Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
<b>Mineral tenement and land tenure status</b>	<i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i>	<ul style="list-style-type: none"> <li>The Craic and Transvaal deposits are located within Mining Lease M39/228, 100% owned by Mt Morgans WA Mining Pty Ltd, a wholly owned subsidiary of Dacian Gold Ltd.</li> </ul>
	<i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.</i>	<ul style="list-style-type: none"> <li>The above tenements are all in good standing.</li> </ul>
<b>Exploration done by other parties</b>	<i>Acknowledgment and appraisal of exploration by other parties.</i>	<ul style="list-style-type: none"> <li>Exploration activities have been undertaken by Anaconda, Auswhim, Dominion, Homestake Gold, Plutonic, Placer and Range River.</li> <li>A high proportion of the historic data is confirmed by recent drilling and is of a quality that, in the Competent Person's view, supports the MRE at the classification applied.</li> <li>The initial ore reserve for Transvaal was 1 Mt @ 3 g/t, then increased to 2 Mt @ 3.45 g/t (this being unreliable due to poor record keeping).</li> <li>The Transvaal open pit (OP) was mined by Plutonic from late 1991 through mid-1994. In a project summary document, Plutonic estimated that 900 koz was mined from Transvaal OP, but did not know this with accuracy.</li> <li>For UG mining, Plutonic reported knowledge of 500 t @ 5 g/t for 80 koz being UG resources from an unreferenced source. A feasibility study from Nov 1995 through Jan 1996 used a resource of 596 kt @ 5.96 g/t between the 340 m RL and 195 m RL.</li> <li>Plutonic regained the operation in Jan 1996, which received a final feasibility study that showed a life of mine (LOM) of 509 kt @ 5.32 g/t @ 74 koz, targeting yearly stope production of 170 kt/a.</li> <li>The first cut in the Transvaal portal took place on 22/03/1996. The final UG blast block took place in April 1998. During the UG mining, 7,571.4 m was developed, and 599,704 t @ 3.87 g/t for 68,102 oz was trucked to the mill.</li> </ul>
<b>Geology</b>	<i>Deposit type, geological setting and style of mineralisation.</i>	<ul style="list-style-type: none"> <li>The deposit is Archean lode gold style.</li> <li>Both deposits consist of a series of mineralised structures within greenschist facies altered basalt flows and quartz feldspar porphyry dyke intrusions.</li> <li>The lodes strike north to NNE, dip steeply east and generally plunge moderately to the north. The porphyry dykes strike NNE to NE, and display a moderate dip to the E or NE, cross-cutting or delineating the mineralised structures into the lodes.</li> <li>Gold mineralisation is hosted within north-northeast trending shear-hosted lodes. For Transvaal, the anastomosing lode-porphyry bodies are hosted along an extension of the Ramornie Transvaal Shear Zone, whereas the mineralisation of Craic is hosted on a parallel local shear structure east of the Ramornie Transvaal Shear Zone on two dominant mineralised structures.</li> <li>High-grade accumulations are evident at the contacts within the pre-mineralising porphyry dykes.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Mineralised intervals typically display altered and fractured or strained zones in the basalt and an alteration mineral assemblage associated with elevated pyrite-pyrrhotite that is a combination of chlorite-carbonate to sericite-albite alteration. For Transvaal, these alteration zones are distinct, but at Craic they are more subtle and thinner.</li> <li>Mineralisation is hosted within porphyries across the contacts of the basalt within the planes of the mineralised structures, but the grades rapidly decrease moving into the porphyries, and therefore have not been classified nor reported.</li> <li>Mineralisation and host rocks within the OP exposures confirm the geometry of the mineralisation.</li> <li>The oxidation profile for Transvaal is very shallow, with no or sub-metre scale completely oxidized material. The transitional zone extends only 10s of metres.</li> <li>For Craic, a deeper oxidation profile of 1 m – 5 m completely oxidised and 25 m – 40 m of transitional material.</li> </ul>
<b>Drill hole information</b>	<i>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
	<i>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
<b>Data aggregation methods</b>	<i>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> <li>No grade-weighting or other techniques have been applied to gold grades in figures.</li> </ul>
	<i>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
	<i>The assumptions used for any reporting of metal equivalent values should be clearly stated.</i>	<ul style="list-style-type: none"> <li>No metal equivalent values have been used</li> </ul>
<b>Relationship between mineralisation widths and</b>	<i>These relationships are particularly important in the reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>Most drill holes are angled to the west so that intersections are orthogonal to the expected orientation of mineralisation. It is interpreted that true width is approximately 60%–100% of down hole intersections.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>intercept lengths</b>	<i>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</i>	<ul style="list-style-type: none"> <li>The holes are drilled approximately perpendicular to the orientation of the plane of mineralisation.</li> </ul>
	<i>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').</i>	<ul style="list-style-type: none"> <li>It is interpreted that true width is approximately 60-100% of down hole intersections depending on the orientation of the target which varies along strike and down dip.</li> </ul>
<b>Diagrams</b>	<i>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</i>	<ul style="list-style-type: none"> <li>Relevant diagrams have been included within the main body this ASX release.</li> </ul>
<b>Balanced Reporting</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>Historic drill hole collar coordinates were tied to a local grid with subsequent conversion to MGA94 Zone 51. The transformation parameters were taken from the Dominion Mining reference manual, which were used to recalculate the collar positions in GDA94 MGA51 by the Competent Person as a check on the accuracy, finding little to no difference in the positions for Transvaal.</li> </ul> <p><b>Craic</b></p> <ul style="list-style-type: none"> <li>For Craic, of the 1,342 DD, RCD, RC and face samples, 41 RC holes (3 drilled in 1986, 8 drilled in 1988, one drilled in 1990, 17 drilled in 1992 and 12 drilled in 1997) had an "Orig_Grid_ID" collar survey ID of "TVL" (Transvaal), all of which did not match the transform parameters. The greatest difference of the errors was 5.9 m.</li> <li>Of these holes with errors, three were beyond the limits of the mineralisation interpretation, 22 were drilled from surface above the current pit and whose intervals agreed with the waste or mineralisation in the surrounding holes, and the remainder were drilled under the pit and also agreed with the waste or mineralisation in the surrounding holes.</li> <li>The Competent Person reviewed the potential shift in the mineralisation interpretation and grade estimate, and concluded that there was no material impact on the MRE.</li> <li>Approximately 20% of the Craic face samples were found to be in impossible locations in relation to the UG development, which occurred from rounding or copying of Z/RL coordinate values from a previous record. The Competent Person noted that the mineralisation interpretation and grade estimate displayed high-visual correlation with the drives, and the resulting face sample locations were clearly located within the drives from logical vertical shift. Therefore, the Z coordinate/RL value in the database was adjusted to force the collar position to be ~1 m above the floor of the drive from which they were sampled.</li> <li>The Competent Person is satisfied that the recent Dacian 2021 drill holes have confirmed the locations of the mineralisation with acceptable accuracy for supporting the MRE.</li> <li>All Dacian hole collars were surveyed in MGA94 Zone 51 grid using differential GPS to within 3cm. Dacian holes were down-hole surveyed either with a north seeking gyroscopic tool at 30m intervals to 20cm accuracy.</li> </ul>
	<i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>Results.</i>	
<b>Other substantive exploration data</b>	<i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i>	<ul style="list-style-type: none"> <li>In February 2021, downhole/wireline logging was undertaken by Surtech Systems to achieve gamma-density values at 10 cm spacing downhole as described within this Table 1 on six RC holes at Craic, and six DD and three RC holes at Transvaal.</li> </ul>
<b>Further work</b>	<i>The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i>	<ul style="list-style-type: none"> <li>UG optimisation of the MRE for inclusion in the Dacian LOM is planned, which will provide guidance on the locations of infill drilling to permit a MRE update.</li> </ul>

## Transvaal and Craic

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
<b>Database integrity</b>	<i>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</i>	<ul style="list-style-type: none"> <li>The data base has been systematically audited by Dacian geologists and database-specialist consultant geologists. Original drilling records were compared to the equivalent records in the data base (where original records were available). Any discrepancies were noted and rectified by the data base manager.</li> </ul>
	<i>Data validation procedures used.</i>	<ul style="list-style-type: none"> <li>Historic logs were located and additional logging information, particularly relating to weathering, was input into the database.</li> <li>Ongoing database (DB) validation has been undertaken by a dedicated DB administrator communicating with geologists as the primary data sources and labs.</li> <li>Extensive validation was undertaken by the database administrator.</li> <li>Data were loaded into DataShed back-end SQL Server DB on a related data schema, providing a referentially integral database with primary key relations and look-up validation fields.</li> <li>Additional validation completed in Datamine by Dacian geologists, with any validation issues relayed to DB administrator. All Dacian drilling data has been verified as part of a continuous validation procedure. Once a drill hole is imported into the data base reports of the collar, down-hole survey, geology, and assay data are produced. These are then checked by a Dacian geologist in geological software and any corrections are sent to the data base administrator</li> </ul>



Criteria	JORC Code explanation	Commentary
		<p>to complete.</p> <ul style="list-style-type: none"> <li>All data were checked for the following errors: <ul style="list-style-type: none"> <li>Duplicate drillhole IDs</li> <li>Missing collar coordinates</li> <li>Mis-matched or missing FROM or TO fields in the interval tables (assays, logging etc)</li> <li>FROM value greater than TO value in interval tables</li> <li>Non-contiguous sampling intervals</li> <li>Sampling interval overlap in the assay table</li> <li>The first sample in the interval file not starting at 0 m</li> <li>Interval tables with depths greater than the collar table EOH depth.</li> </ul> </li> <li>Survey data were checked for large deviations in azimuth and dip between consecutive records, with none found.</li> </ul>
<b>Site visits</b>	<i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i>	<ul style="list-style-type: none"> <li>The Competent Person has made several site visits during 2020 and 2021, and has worked with the site-based geologists and mining engineers on the MRE and reconciliation processes relevant to this estimate.</li> <li>Inspection of the equipment used by Dacian's drilling contractor at the time of the visits found all operators working to a standard required to report the MREs in accordance with the JORC Code.</li> <li>The visits confirmed that the topography resembled the DTM surface used in the MRE, no historic depletion existed that had not been accounted for, and that no physical impediments were noted for the reasonable prospects of eventual economic extraction.</li> <li>The drill site inspections included checks of the database records and diamond core against collar locations, drilling angles and dips, hole depths by peg notes and RC sample bags where available, and geological logging against sample bags and diamond core.</li> <li>The diamond core sampling and storage facilities are in good condition.</li> <li>Regular discussions between the Competent Person during the preparation of the MRE with site-based geologists confirmed that they held a good understanding of the geology, the mineralisation controls on the MRE, and that their adherence to the Dacian procedures ensured good sample quality.</li> <li>The site visit indicated that there were no matters presented that would prevent reporting the MRE in accordance with the JORC Code.</li> <li>The Competent Person visited the on-site laboratory twice in December to review processes, and each of the two National Association of Testing Authorities (NATA) accredited offsite contract laboratories in 2021. All laboratories were performing at and producing results for a standard required to report the MREs in accordance with the JORC Code.</li> </ul>
	<i>If no site visits have been undertaken indicate why this is the case.</i>	<ul style="list-style-type: none"> <li>N/A</li> </ul>
<b>Geological interpretation</b>	<i>Confidence in (or conversely, the uncertainty of ) the geological interpretation of the mineral deposit.</i>	<ul style="list-style-type: none"> <li>The confidence in the geological interpretations for both MREs is very high, as it is based on mining exposure as well as a high drilling density. Visual confirmation of lode position and orientations has been observed and mapped in the OP and UG exposures.</li> <li>Ongoing infill drilling has confirmed geological and grade continuity.</li> </ul>
	<i>Nature of the data used and of any assumptions made.</i>	<ul style="list-style-type: none"> <li>Geological logging has been used to assist identification and delineation of lithology and mineralisation.</li> <li>All lodes were treated as hard-boundaries for statistics and estimation.</li> </ul>
	<i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>Alternate interpretations may consider a different gold grade cut-off for the modelling of mineralisation, which may increase the tonnages and lower the grade for a reduced grade cut-off and vice-versa for an increased grade. Either of these are likely to result in a similar balance of metal.</li> <li>However, the volumes and grades mineralisation model has been demonstrated by UG stope production shapes, and which show that the boundaries of the mineralisation are suitable for the delineation of ore and waste.</li> </ul>
	<i>The use of geology in guiding and controlling Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>All lodes were treated as hard-boundaries for statistics and estimation.</li> <li>High-grade accumulations are noted within the porphyries across the contacts of the basalt, and within the planes of the mineralised structures. The samples and volumes within the mineralised structures and in the porphyry volumes have been estimated independently with a hard boundary to the basalt-hosted</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>mineralisation within the same lode. However, the grades rapidly decrease moving into the porphyries where sample density is lower, causing higher-grade clustering within the porphyries near their contacts, so that the grades are likely to have smeared through the thickness of the porphyry volumes without an ability (such as an alteration halo or other geologically confirmed hard boundary) to control the grades from smearing away from the contact into the porphyry volume. Therefore, have not been classified nor reported.</p> <ul style="list-style-type: none"> <li>Statistics were reviewed, including grade distributions, contact analysis and variogram continuity, between the oxidation domains, which showed that no boundaries were present, and therefore no hard boundaries by oxidation domain were applied.</li> <li>Porphyry units are also mineralised at times but not visually recognisable as mineralised. Lodes generally are truncated by the porphyries into discrete lode objects, but where the mineralising structures cross-cut the porphyries, the mineralisation appears to extend sub-metre scale into the porphyries, and therefore the MREs exclude porphyry-hosted mineralisation.</li> <li>The following objects were modelled that the Competent Person considers adequate to control the MRE. <ul style="list-style-type: none"> <li>Transvaal lodes: 50</li> <li>Transvaal porphyry dykes: 22</li> <li>Craic lodes: 18</li> <li>Craic porphyry dykes: 27</li> <li>Transvaal oxidation/weathering: top of fresh (TOFR)</li> <li>Craic oxidation/weathering: base of complete oxidation (BOCO), TOFR</li> </ul> </li> </ul>
	<i>The factors affecting continuity both of grade and geology.</i>	<ul style="list-style-type: none"> <li>The mineralised lodes occur within a greater shear corridor and are hosted by both mafic and porphyry units suggesting gold mineralization was post-intrusion, but mineralisation preferenced the mafic material.</li> <li>Grades above 0.5 g/t Au display a high continuity, and therefore this was selected as the mineralisation modelling cut-off.</li> <li>The mineralised structures are laterally continuous beyond the modelled mineralisation, yet the mineralisation shows sharp cut-offs laterally either where the mafic units are intruded by the pophyries or for other unknown reasons. Therefore, the modelling cut-off has a high influence on the continuity of the grade.</li> <li>Mineralised intervals typically display altered and fractured or strained zones in the basalt and an alteration mineral assemblage associated with elevated pyrite-pyrrhotite that is a combination of chlorite-carbonate to sericite-albite alteration. For Transvaal, these alteration zones are distinct, but at Craic they are more subtle and thinner. The alteration zones are generally difficult to model.</li> </ul>
<b>Dimensions</b>	<i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i>	<ul style="list-style-type: none"> <li>The Transvaal Mineral Resource area extends over a N-S strike length of 900m (from 6811800 m N – 6812700 m N). It extends from 419350 mE to 420200 mE and extends from surface (approximately 425mRL) to 150mRL.</li> <li>The Craic Mineral Resource extends laterally over a NNE-SSW strike length of 350 m, and 185 m ENE-WSW, and 215 m vertical depth (425 m RL to 210 m RL). The lodes are from 2 m – 7 m thick.</li> <li>For Transvaal, three domains were created based on lode spatial groupings and orientations, which were used to calculate statistics, top-cuts and model variograms. <ul style="list-style-type: none"> <li>The NNE-striking domain encompasses 42 lodes, six of which are considered major based on size and sample counts. The lodes in this domain are lying in the dominant orientation for the deposit from south to central north. OP and UG mining has depleted much of the upper parts of these lodes.</li> <li>The NNW-striking domain encompasses seven total and two major lodes lying in the central north to the north, with a north-northwest strike and shallow to moderate plunge.</li> <li>A single lode forms the NW-striking domain, which strikes north-west and lies near the central-southern area of the deposit, which has been mostly depleted by open pit mining.</li> </ul> </li> <li>For Craic, all lodes displayed similar geometries and orientations within a tight extent, therefore, all lodes were grouped into a single domain.</li> </ul>
	<i>The nature and</i>	<ul style="list-style-type: none"> <li>Samples were composited to 1 m intervals ("composites") based on</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Estimation and modelling techniques</b>	<i>appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i>	<p>assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.</p> <ul style="list-style-type: none"> <li>Statistical analysis was completed in Snowden Supervisor™ 8.14 software, including modelling of the spatial continuity of gold grades by variography. Statistics were length-weighted.</li> <li>Multi-block kriging neighbourhood analysis (KNA) was undertaken using Supervisor™ software to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE), slope of regression (SOR) and negative weights were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids.</li> <li>Geological modelling, sample compositing, block modelling and grade estimation were undertaken using Surpac™ software.</li> <li>Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains. The technique is considered appropriate to allow the geostatistical continuity determined from variography to weight samples during estimation.</li> <li>The estimation technique is appropriate to allow a locally adequate estimate for detailed mine planning and with a globally unbiased estimate per lode.</li> </ul> <p>Transvaal</p> <ul style="list-style-type: none"> <li>As only 157 Transvaal composites out of 2,510 sat above the top of fresh rock, analysis for the oxidation profile was meaningless. The lodes show strong continuity regardless of the weathering, with no supergene dispersion halo evident. Therefore, the lodes were not split by the oxidation profile.</li> <li>Multi-block KNA statistics were reviewed for the mineralised mafic domains, using a maximum of 3 samples per drillhole:</li> <li>Combinations of 5 m, 10 m and 20 m block sizes in X, Y and Z directions were reviewed.</li> <li>5x by 10y by 5z block size gave among the best statistics and was considered more appropriate for the drillhole density.</li> <li>A search ellipse size matching the full range structure.</li> <li>Transvaal experimental semivariograms did not provide coherent anisotropic directions, so the models were coerced into the plane of mineralisation. This ensured that the anisotropic directions made geological sense by forcing the major direction down-plunge with the mineralisation, the semi-major was orthogonal within the plane of mineralisation, and the minor was across strike.</li> <li>Two spherical structures were modelled for each lode group.</li> <li>After variograms were modelled, a back-transform model was exported with Datamine rotations for use in Datamine parameter files. All variograms contained a low nugget when back-transformed, and typically a very high proportion of the variance accounted for in the short-range structure.</li> <li>A hard-boundary for composites and estimation across the oxidation type boundaries was not applied for the following reasons:</li> <li>Sufficient samples for contact analysis were only available for lode object 4, which included 56 and 128 transitional and fresh samples respectively.</li> <li>Visual review of the locations of the oxide and transitional samples showed that all oxide most transitional samples within mineralisation have been depleted by the pit surface.</li> <li>Minor lodes are almost entirely within the transitional or fresh oxidation type.</li> <li>Minor lodes contain insufficient samples for further splitting by a hard-boundary.</li> <li>The OK estimate was undertaken in three passes based on KNA: <ul style="list-style-type: none"> <li>A search ellipse size 75% of the full range structure, expanding out to 150% and 250% on passes two and 3.</li> <li>Minimum samples of 8 or 9 gave statistics that were at the lower end of acceptable prior to a significant decrease in the quality of statistics, relaxed to two samples in the third pass to allow all blocks to be estimated.</li> <li>Between 22 and 24 maximum samples inclusive gave the best statistics before diminishing returns were noted, providing little benefit to the estimate and increasing smoothing and conditional bias; the maximum samples was reduced to 10 on the third pass to ensure previously unestimated fringe blocks would not be informed by samples at extreme distances from the estimated blocks.</li> </ul> </li> </ul>

Criteria	JORC Code explanation	Commentary																								
		<ul style="list-style-type: none"><li>○ Statistics were invariable for changes in discretisation.</li></ul> <p><b>Craic</b></p> <ul style="list-style-type: none"><li>• Face samples, which exist in lodes 1, 12 and 13, were excluded from statistical analysis to prevent their high-grade, selective and clustered sampling from biasing the statistics.</li><li>• Craic composite samples were declustered prior to variography for the major lodes of the statistical domains that contained lodes. A normal-score transform was applied to all data.</li><li>• Statistics were invariable for changes in discretisation.</li><li>• The second pass was the full range of the variogram, from 16.8 m to 57.6 m and the minimum samples was 10 and maximum was 20. The third pass was 8x to 12x the full range of the variogram, from 60 m to 224 m, and the minimum samples was 4 and maximum was 8.</li><li>• The major direction was modelled with a ratio of between 1.2x to 2.3x the semi-major direction, and 2.3x 6.8x the minor direction. The latter of 6.8x ratio to the minor is an exception, relating to domain South, which incorporates the elongated lodes drilled to a lower density, and that have almost entirely been classified as Inferred.</li><li>• Dynamic anisotropy was used only on the first pass to prevent wildly fluctuating large ellipses from weighting samples in high angles to the prevailing orientations of the lodes.</li><li>• The OK estimate was undertaken in four passes based on KNA:<ul style="list-style-type: none"><li>○ The first pass was conducted for lodes 1, 12 and 13 using face samples, using a search ellipse of 14 m, which was approximately 2 x the short range spherical structure of the variogram, as below this estimated too few blocks and above this the face samples had too large an influence.</li><li>○ A search ellipse size of 20 m was used for the second pass of all lodes, expanding out to 150% for the third pass, after which the fourth pass at 100 m was not required, as all blocks had been estimated in prior passes.</li><li>○ A minimum of 6 gave statistics that were at the lower end of acceptable prior to a significant decrease in the quality of statistics, relaxed to four samples in the third pass to allow all blocks to be estimated.</li><li>○ A maximum of 14 samples inclusive gave the best statistics before e diminishing returns were noted, providing little benefit to the estimate and increasing smoothing and conditional bias; the maximum samples was reduced to 10 on the third pass to ensure previously unestimated fringe blocks would not be informed by samples at extreme distances from the estimated blocks.</li></ul></li></ul>																								
	<i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i>	<p>Both Transvaal and Craic have historic production records available. However, the mineralisation has not been modelled to accurately take into account the full volumes of the mineralisation that has been depleted by the OP extraction, and therefore the reconciliation is likely to be unreliable. However, the mineralisation modelled in the MRE updates shows strong agreement with the mining voids.</p> <p><b>Transvaal</b></p> <ul style="list-style-type: none"><li>• The most recent Transvaal estimate was undertaken by RungePincocKMinarco in 2015, which was publicly announced by Dacian in 2015, shown below.</li></ul> <table><tr><th>Classification</th><th>Tonnes (kt)</th><th>Au g/t</th><th>Au Oz</th></tr><tr><td>Measured</td><td>367</td><td>5.76</td><td>68,000</td></tr><tr><td>Indicated</td><td>404</td><td>5.31</td><td>69,000</td></tr><tr><td>Inferred</td><td>482</td><td>4.71</td><td>73,000</td></tr><tr><td>TOTAL</td><td>1,253</td><td>5.21</td><td>210,000</td></tr></table> <ul style="list-style-type: none"><li>• The previous MRE classified Measured Mineral Resources, which the Competent Person does not believe has been established, and therefore has not been retained for the MRE update.</li></ul> <p><b>Craic</b></p> <ul style="list-style-type: none"><li>• The most recent Craic estimate was undertaken by BMGS in December 2020, which was publicly announced by Dacian in May 2021, shown below.</li></ul> <table><tr><th>Classification</th><th>Tonnes (kt)</th><th>Au g/t</th><th>Au Oz</th></tr></table>	Classification	Tonnes (kt)	Au g/t	Au Oz	Measured	367	5.76	68,000	Indicated	404	5.31	69,000	Inferred	482	4.71	73,000	TOTAL	1,253	5.21	210,000	Classification	Tonnes (kt)	Au g/t	Au Oz
Classification	Tonnes (kt)	Au g/t	Au Oz																							
Measured	367	5.76	68,000																							
Indicated	404	5.31	69,000																							
Inferred	482	4.71	73,000																							
TOTAL	1,253	5.21	210,000																							
Classification	Tonnes (kt)	Au g/t	Au Oz																							

Criteria	JORC Code explanation	Commentary								
		<table><tr><td>Inferred</td><td>96</td><td>9.41</td><td>29,000</td></tr><tr><td>TOTAL</td><td>96</td><td>9.41</td><td>29,000</td></tr></table> <ul style="list-style-type: none"><li>The previous MRE did not classify Indicated Mineral Resources, as the drill hole data density, QAQC, bulk density data, and confidence in the geological interpretation was lower. The increased data has lead to both an Indicated component of the MRE update and a lower overall MRE</li></ul>	Inferred	96	9.41	29,000	TOTAL	96	9.41	29,000
Inferred	96	9.41	29,000							
TOTAL	96	9.41	29,000							
	<i>The assumptions made regarding recovery of by-products.</i>	<ul style="list-style-type: none"><li>No assumptions have been made regarding the recovery of by-products.</li></ul>								
	<i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i>	<ul style="list-style-type: none"><li>No deleterious elements have been estimated.</li></ul>								
	<i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i>	<ul style="list-style-type: none"><li>A parent block size of 5 m x 10 m x 5 m (X x Y x Z) was chosen for both deposits, which was supported KNA and by drill hole spacing in KNA Y and Z directions. Most of both deposits have been sampled at a density that has created pierce mineralisation points space at least 20 m x 20 m for Craic and 25 m x 25 m for Transvaal, out to 80 m x 80 m on the fringes.</li><li>Sub-celling to 1/8 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode wireframes.</li></ul>								
	<i>Any assumptions behind modelling of selective mining units.</i>	<ul style="list-style-type: none"><li>No assumptions have been made regarding SMUs.</li></ul>								
	<i>Any assumptions about correlation between variables.</i>	<ul style="list-style-type: none"><li>Gold has been estimated univariately and in isolation of other variables.</li></ul>								
	<i>Description of how the geological interpretation was used to control the resource estimates.</i>	<ul style="list-style-type: none"><li>Geology and grade were used to define the mineralisation lodes. Within each lode, the estimate was constrained to blocks within the lode wireframe using only top-cut composited samples from the corresponding lode.</li></ul>								
	<i>Discussion of basis for using or not using grade cutting or capping.</i>	<ul style="list-style-type: none"><li>High-grade top-caps were applied to limit the influence of extreme outliers on the grade estimate. The top-caps were applied to the mineralisation domains following statistical analysis.</li><li>Additionally, distance limiting top-cuts were applied to the grade estimate to prevent Au &gt;=</li><li>Top-cuts were determined for Transvaal lodes within three statistical domains, while a single top-cut was determined for porphyry material, as follows:<ul style="list-style-type: none"><li>TV_NNE_Strike domain: 38 g/t</li><li>TV_NNW_Strike domain: 15 g/t</li><li>TV_NW_Strike domain (lode 14): 14 g/t</li><li>Porphyry: 4 g/t</li></ul></li><li>For Craic, a continuous distribution was noted for Craic mineralisation, which indicated no extreme outliers. Therefore, relatively high top-cuts Were applied:<ul style="list-style-type: none"><li>Mineralisation: 85 g/t Au</li><li>Porphyry: 28 g/t Au.</li><li>However, a high-grade population was noted in the Craic grade distributions above 20 g/t, which did not display continuity to allow a high-grade sub-domain to be modelled. Therefore, a distance limit of 15 m was applied for grades above 20 g/t to be excluded from the grade estimate.</li></ul></li><li>The top-cuts were kept at around 1% – 2% of the grade distribution for each lode or statistical domain.</li></ul>								
	<i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i>	<ul style="list-style-type: none"><li>Validation of the estimate was completed for the resource block models using numerical methods (histograms, CDFs and swath plots) and validated visually against the input raw drillhole data, declustered data, composites and blocks.</li></ul>								
<b>Moisture</b>	<i>Whether the tonnages are estimated on a dry basis or</i>	<ul style="list-style-type: none"><li>Tonnages and grades have been estimated on a dry in situ basis.</li></ul>								



Criteria	JORC Code explanation	Commentary
	<i>with natural moisture, and the method of determination of the moisture content.</i>	
<b>Cut-off parameters</b>	<i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i>	<ul style="list-style-type: none"> <li>The MRE has been reported above a lower cut-off of 2.0 g/t Au.</li> <li>The reporting cut-off parameters were selected based on known UG economic cut-off grades from Dacian's Westralia UG operation.</li> <li>Pit optimisations using parameters that the Competent Person deemed appropriate tests for reasonable prospects for eventual economic extraction (RPEEE) were reviewed, which showed that insufficient material was included above the pit to warrant reporting at lower cut-off grades for Mineral Resources in OP mining scenarios.</li> </ul>
<b>Mining factors or assumptions</b>	<i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i>	<ul style="list-style-type: none"> <li>Previous operators mined both deposits using the methods currently in use by Dacian. It is assumed that the same mining methods will be applicable for extraction of in-situ material included in this MRE update.</li> </ul>
<b>Metallurgical factors or assumptions</b>	<i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i>	<ul style="list-style-type: none"> <li>The ore is intended to be processed at the Jupiter Processing Facility, part of the Mt Morgans Gold Operation (MMGO). Recoveries achieved to date are 92.3%.</li> </ul>
<b>Environmental factors or assumptions</b>	<i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields</i>	<ul style="list-style-type: none"> <li>Transvaal and Craic are within the MMGO mining leases, having been working mines in the past, achieving all requisite environmental approvals. Dacian believes that there will be no impediments to the approval of mining the deposits again.</li> <li>Waste rock will be stored in a conventional waste dump.</li> </ul>



Criteria	JORC Code explanation	Commentary																								
	<i>project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i>																									
<b>Bulk density</b>	<i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i>	<p>Immersion-method density was determined on diamond core. Quantitative gamma-density measurements were captured in February 2021 by Surtech. Transvaal:</p> <ul style="list-style-type: none"> <li>Core immersion/Archimedes method data: <ul style="list-style-type: none"> <li>1,601 half NQ2 core samples were available.</li> <li>Samples only taken in fresh rock with no other weathering profile represented.</li> <li>Composited to 1 meter across mafics and porphyries then averaged to give density for comparison with the wireline data.</li> </ul> </li> <li>Density values assigned in the previous MRE, tabulated below, were used to compare and validate the gamma-density values: <table border="1"> <tr> <th>Oxidation</th><th>Porphyry</th><th>Mineralisation &amp; Mafic waste</th></tr> <tr> <td>Oxide</td><td>N/A</td><td>N/A</td></tr> <tr> <td>Trans</td><td>N/A</td><td>N/A</td></tr> <tr> <td>Fresh</td><td>2.72</td><td>2.87</td></tr> </table> </li> <li>The updated density estimate was based on the analysis of gamma-density values filtered to be within 20% of the nominal hole diameter, determined by the density caliper arm. The data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging.</li> <li>The following observations were made: <ul style="list-style-type: none"> <li>For fresh material, the density was invariable for changes in depth, visually averaged to be 2.9 t/m<sup>3</sup>, which was assigned to the fresh mineralisation and waste.</li> <li>A vertical alignment of density for fresh porphyry material, with a visual average of 2.7 t/m<sup>3</sup>.</li> <li>There was no influence of RC or DD hole type on the densities.</li> <li>There is no relationship between density and lithology. As the weathering profile is so shallow, which is confirmed by the densities, an estimated visual average was assigned for oxide and transitional densities.</li> <li>The gamma-densities for fresh agree with the previous assignment calculated from DD core.</li> </ul> </li> <li>The final densities were applied based on the above. <table border="1"> <tr> <th>Oxidation</th><th>Porphyry</th><th>Mineralisation &amp; Mafic waste</th></tr> <tr> <td>Oxide</td><td>N/A</td><td>N/A</td></tr> <tr> <td>Trans</td><td>2.3</td><td>2.6</td></tr> <tr> <td>Fresh</td><td>2.7</td><td>2.9</td></tr> </table> </li> </ul> <p><b>Craic:</b></p> <ul style="list-style-type: none"> <li>Wireline gamma-density data were captured by Surtech on six holes for 886.2 m</li> <li>The density values were adjusted by borehole magnetic resonance (BMR) imaging, giving a quantitative, porosity-adjusted value (dry-bulk density).</li> <li>Compared to the oxidation logging and the oxidation model, the gamma-density data show a gradational increase with depth within the shallow oxidation profile to the TOFR, after which the data are stable in a reasonably tight range.</li> <li>Core immersion/Archimedes method data were captured by Range River on 21 holes surface and underground diamond for 644.02 m</li> <li>There is no information on the core immersion-method density samples, and therefore the data were not used.</li> <li>The final density values assigned to the Craic MRE are shown below.</li> </ul>	Oxidation	Porphyry	Mineralisation & Mafic waste	Oxide	N/A	N/A	Trans	N/A	N/A	Fresh	2.72	2.87	Oxidation	Porphyry	Mineralisation & Mafic waste	Oxide	N/A	N/A	Trans	2.3	2.6	Fresh	2.7	2.9
Oxidation	Porphyry	Mineralisation & Mafic waste																								
Oxide	N/A	N/A																								
Trans	N/A	N/A																								
Fresh	2.72	2.87																								
Oxidation	Porphyry	Mineralisation & Mafic waste																								
Oxide	N/A	N/A																								
Trans	2.3	2.6																								
Fresh	2.7	2.9																								

Criteria	JORC Code explanation	Commentary		
		Oxidation type	Porphyry	Mineralisation & Mafic waste
		Oxide	1.7	1.7
		Transitional	2.3	2.6
		Fresh	2.7	2.9
	<i>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i>	<ul style="list-style-type: none"> <li>Void space has been accounted for in the industry-standard, immersion method core density determination process.</li> <li>The data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging.</li> </ul>		
	<i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i>	<ul style="list-style-type: none"> <li>For gamma-density, the data are quantitative and independent of sample weight, and have been analysed by modelled material types.</li> <li>For core immersion-method density data, no relationship to sample weight has been determined, and is expected to be unrelated, as the core density data show little variation with lithological types.</li> </ul>		
<b>Classification</b>	<i>The basis for the classification of the Mineral Resources into varying confidence categories.</i>	<p>The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:</p> <ul style="list-style-type: none"> <li>Drill density data</li> <li>Geological understanding</li> <li>Quality of gold assay grades</li> <li>Continuity of gold grades</li> <li>Economic potential for mining.</li> </ul> <p>Indicated Mineral Resources:</p> <ul style="list-style-type: none"> <li>Statistical consideration has been employed to assess the grade estimate quality in considering large, contiguous and coherent zones of blocks form zones where: <ul style="list-style-type: none"> <li>Drill hole spacing reaches a nominal maximum of 25 m.</li> <li>Estimation was undertaken in search passes of 1 and 2.</li> <li>Number of samples was near the optimum.</li> <li>Slope of regression formed large volumes of &gt; 0.4 with cores of 0.6.</li> </ul> </li> <li>Unclassified material: <ul style="list-style-type: none"> <li>Porphyries.</li> <li>Single intercept and other poorly informed lodes.</li> <li>Remnant material that AW determined failed the RPEEE test from UG depletion.</li> </ul> </li> <li>Inferred Mineral Resources: <ul style="list-style-type: none"> <li>All other mafic-hosted mineralisation.</li> </ul> </li> </ul>		
	<i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i>	<ul style="list-style-type: none"> <li>All factors the Competent Person has deemed relevant to the MRE have been incorporated into the classification of Mineral Resources.</li> </ul>		
	<i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i>	<ul style="list-style-type: none"> <li>The result appropriately reflects the Competent Person's view of the deposit.</li> </ul>		
<b>Audits or reviews</b>	<i>The results of any audits or reviews of Mineral Resource estimates.</i>	<ul style="list-style-type: none"> <li>Internal audits were completed by Dacian, which verified the technical inputs, methodology, parameters and results of the estimate.</li> </ul>		
<b>Discussion of relative accuracy/confidence</b>	<i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed</i>	<ul style="list-style-type: none"> <li>The accuracy of the MRE is communicated through the classification assigned to the deposit. The MRE has been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this table.</li> </ul>		

Criteria	JORC Code explanation	Commentary
	<i>appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i>	
	<i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i>	<ul style="list-style-type: none"> <li>The MRE statement relates to a global estimate of in-situ tonnes and grade.</li> </ul>
	<i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i>	<ul style="list-style-type: none"> <li>Both Transvaal and Craic have production records available. However, the mineralisation has not been modelled to accurately take into account the full volumes of the mineralisation that has been depleted by the OP extraction, and therefore the reconciliation is likely to be unreliable. However, the mineralisation modelled in the MRE updates shows strong agreement with the mining voids.</li> </ul>

## Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
<b>Sampling techniques</b>	<i>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i>	<ul style="list-style-type: none"> <li>Surface and underground (UG) Diamond (DD) core, surface Reverse Circulation (RC) chips and surface RC chips with DD tail (RCD) core informed both the Mineral Resource estimate (MRE).</li> </ul>
	<i>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</i>	<ul style="list-style-type: none"> <li>Dacian surface diamond core was sampled as half core at 1m intervals or to geological contacts. To ensure representative sampling, half core samples were always taken from the same side of the core.</li> <li>Dacian RC holes were sampled over the entire length of hole. Dacian RC drilling was sampled at 1m intervals via an on-board cone splitter.</li> </ul>
	<i>Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</i>	<ul style="list-style-type: none"> <li>RC holes within mineralisation were dominantly sampled on 1 m intervals in mineralisation via either a riffle splitter (historic samples) or on-board cone splitter (Dacian) mounted at the base of the cyclone to achieve a representative split of approximately 3 kg samples.</li> <li>Diamond core was sampled as half core if drilled from surface or full core if UG on 1 m intervals or to geological contacts, sampled into lengths in sample bags to achieve approximately 3 kg.</li> <li>Dacian surface RC holes were sampled over the entire length of hole.</li> <li>Surface samples were submitted to NATA certified contract laboratory for crushing and pulverising to produce either a 40 g or 50 g charge for fire assay with an atomic absorption spectrometry (AAS) finish.</li> </ul>
<b>Drilling techniques</b>	<i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i>	<ul style="list-style-type: none"> <li>Drilling that informed the modelling area of the MRE included 1,258 Reverse Circulation (RC) drill holes for 41,467 m, 380 diamond (DD) holes for 94,366.04 m, and 18 RC holes with diamond tails (RCD) for 11,374.97 m. However, many of these holes were targeted at the Westralia stratigraphy from which the Ramornie structure (host of the modelled mineralisation) intersects in the south.</li> <li>Drilling that intersected modelled mineralisation and was used to estimate grades for the MRE update included 194 RC drill holes for 704 m, 81 diamond (DD) holes for 303.202 m, and 5 RCD holes for 18 m.</li> <li>Of the 63% of holes that intersected mineralisation drilled since from 2000, 33% were drilled by Dacian. The remainder were drilled from 1988.</li> <li>For Dacian RC holes, a 5¼" to 5 ¾" face sampling hammer bit was used.</li> <li>UG DD drilling was mostly sampled whole core with NQ2 sized equipment.</li> <li>Dacian DD was sampled as half core, mostly HQ3 and PQ3 with minor PQ2.</li> <li>Dominion holes were drilled with RC rigs utilising face-sampling hammers for maximum sample return.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Drill sample recovery</b>	<i>Method of recording and assessing core and chip sample recoveries and results assessed.</i>	<ul style="list-style-type: none"> <li>Recoveries from historical holes are unknown.</li> <li>Recoveries from Dacian diamond drilling were measured and recorded into the database. Recovery was generally above 95% in fresh rock.</li> </ul>
	<i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i>	<ul style="list-style-type: none"> <li>Dacian RC holes were drilled with a powerful rig with compressor and booster compressor to ensure enough air to maximise sample recovery. The splitter was cleaned at the end of each rod, to ensure that efficient sample splitting. The weight of each sample split was monitored. Drilling was stopped if the sample split size changed significantly.</li> <li>Dacian RC drilling activities, sample volumes, quality and recoveries were monitored by the supervising geologist to ensure good recoveries</li> <li>Sample splitters were cleaned on a regular basis.</li> <li>As the UG DD core has a smaller diameter, the core was sampled whole.</li> </ul>
	<i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i>	<ul style="list-style-type: none"> <li>No relationship has been noted between sample recovery and grade.</li> </ul>
<b>Logging</b>	<i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i>	<ul style="list-style-type: none"> <li>All RC holes were logged for geology, alteration, and visible structure.</li> <li>All RC chip trays were photographed.</li> <li>All drill holes were logged in full.</li> <li>RC drilling was logged by passing a portion of each sampled metre into a sieve to remove rock flour from coarse chips, the chips are then washed and placed into metre marked chip trays for logging. The unsieved sample was also observed for logging purposes. For Dacian drilling, where the material type does not allow for the recovery of coarse rock chips the rock flour is retained as a record. The detail is considered common industry practice and is at the appropriate level of detail to support the MRE.</li> <li>All Dominion RC holes have lithological, weathering and mineralisation information stored in the database.</li> <li>For historical RC drilling, where available the original logs and laboratory results are retained by Dacian as either original hard copies or as scanned copies.</li> <li>Dacian's DD core was photographed wet and dry, and geotechnically logged to industry standards.</li> <li>The Competent Person is satisfied that the logging detail supports the MRE.</li> </ul>
	<i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i>	<ul style="list-style-type: none"> <li>All holes were logged qualitatively by geologists familiar with the geology and control on the mineralisation for various geological attributes including weathering, primary lithology, primary &amp; secondary textures, colour and alteration.</li> <li>For Dacian drilling, diamond core was photographed both wet and dry. For RC drilling chip trays are photographed. Diamond core is retained on site.</li> <li>The wireline gamma-density data is quantitative in nature.</li> </ul>
	<i>The total length and percentage of the relevant intersections logged.</i>	<ul style="list-style-type: none"> <li>All surface diamond drill holes were logged for recovery, RQD, geology, and structure. Structural measurements were taken using a kenometer to record alpha and beta angles relative to a bottom of hole line marked on the oriented core. The quality of the bottom of hole orientation line is also recorded.</li> <li>All drill holes were logged in full, from start of hole to bottom of hole.</li> </ul>
<b>Sub-sampling techniques and sample preparation</b>	<i>If core, whether cut or sawn and whether quarter, half or all core taken.</i>	<ul style="list-style-type: none"> <li>Core was cut in half using a core saw at either 1 m intervals or to geological contacts; core samples were collected from the same side of the core where orientations were completed.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i>	<ul style="list-style-type: none"> <li>• Dacian RC samples were collected via on-board cone splitters. Most samples were dry, any wet samples are recorded as wet, this data is then entered into the sample condition field in the drillhole database.</li> <li>• At all times, an attempt was made to keep samples dry. If due to significant groundwater inflow or drilling limitations sample quality became degraded (consecutive intervals of wet sample or poor sample recovery), the RC hole was abandoned.</li> <li>• The RC sample was split using the cone splitter to give an approximate 3kg sample. The remainder was collected into a plastic sack as a retention sample. At the grain size of the RC chips, this method of splitting is considered appropriate.</li> <li>• Dominion historical RC samples were collected at the rig using riffle splitters if dry while wet samples were bagged for later splitting. Samples condition was not recorded for a majority of the historic sampling. For historic RC drilling, information on the QAQC programs used is limited but acceptable with original batch reports having been reviewed and retained by Dacian.</li> </ul>
	<i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i>	<ul style="list-style-type: none"> <li>• For RC drilling, the sub-sample preparation by splitting by cone or riffle splitters is an industry standard method of creating a representative split.</li> <li>• For non-grade control (GC) RC surface drilling, sample preparation was conducted by a contract, National Association of Testing Authorities (NATA) Australia accredited laboratory.</li> <li>• Most Dominion samples were prepared at an onsite lab, while the remainder of their samples were assayed by fire assay at Analabs.</li> <li>• After drying, Dacian samples were subject to a primary crush, then pulverised and homogenised to 85% passing 75µm before a 40 g or 50 g charge was scooped. This is an industry standard and appropriate method for preparing samples for fire assay.</li> </ul>
	<i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i>	<ul style="list-style-type: none"> <li>• For Dacian RC drilling, RC field duplicates were taken from the on-board cone splitter at 1 in 50 or 1 in 25 for exploration and infill drilling respectively.</li> <li>• Externally prepared Certified Reference Materials were inserted within the sample stream for QAQC.</li> <li>• No information is available for the historic holes.</li> <li>• The internal consistency of the wireline geophysical data was demonstrated by repeat logging of against a calibration hole at Mt Morgans. <ul style="list-style-type: none"> <li>◦ The wireline geophysical data logged throughout Mt Morgans by Surtech systems in February 2021, although they were not taken from the Ramornie deposit.</li> </ul> </li> <li>• Prior to mobilisation to site, the instrument was calibrated immediately against standard materials for density.</li> <li>• A high correlation was shown between the gamma-density and core density determinations where collected on the same holes.</li> </ul>
	<i>Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.</i>	<ul style="list-style-type: none"> <li>• For Dacian exploration DD drilling field duplicates were not taken.</li> <li>• For Dacian RC drilling, field duplicates are generally taken a 1 in 25 samples.</li> </ul>
	<i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i>	<ul style="list-style-type: none"> <li>• Sample sizes are considered appropriate to correctly represent the gold mineralisation based on the style of mineralisation, the thickness and consistency of the intersections, the sampling methodology and assay value ranges for gold.</li> </ul>



Criteria	JORC Code explanation	Commentary
<b>Quality of assay data and laboratory tests</b>	<i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i>	<ul style="list-style-type: none"> <li>For surface drilling, the analytical technique used was a 40g or 50g lead collection fire assay and analysed by Atomic Absorption Spectrometry (AAS). This is a full digestion technique. This is a commonly used method for gold analysis and is considered appropriate for this project.</li> <li>Non-GC Samples were analysed at NATA accredited laboratories.</li> <li>Most Dominion holes were analysed at an onsite lab using fire assay (50g), while the remainder were assayed by fire assay at Analabs.</li> <li>No information regarding the analysis of the 32 MM series holes is known.</li> <li>For Dacian drilling analysed at Bureau Veritas, sieve analysis was carried out by the laboratory to ensure the grind size of 85% passing 75µm was being attained.</li> <li>For Dacian surface RC and diamond drilling, QAQC procedures involved the use of certified reference materials, standards (1 in 20) and blanks (1 in 50). For diamond drilling additional coarse blanks and standards are submitted around observed mineralisation.</li> <li>Results were assessed as each laboratory batch was received and were acceptable in all cases.</li> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>No QAQC data has been reviewed for historic drilling, although mine production and twinned drill holes have validated drilling results. The historic drilling that informs the MRE has been almost entirely mined or represents an insignificant proportion of the informing data.</li> </ul>
	<i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i>	<ul style="list-style-type: none"> <li>The wireline gamma-density data logged throughout Mt Morgans by Surtech systems in February 2021 were used to assist the density determination of the MRE, although they were not taken from the Ramornie deposit.</li> <li>As the Ramornie mineralisation is proximal to Transvaal and Criac, the lodes lie on extensions from Westralia through to Transvaal, and the geology and mineralisation types are equivalent to Transvaal, the densities applied were selected from Craic and Transvaal data and analysis.</li> <li>The Transvaal and Craic density estimates utilised quantitative geophysical data, most notably wireline gamma-density data, that was captured by Surtech using a dual-density instrument, sonde serial number 9239B, with logging by unit SL33, and a caesium radioactive source.</li> <li>The logging in counts-per-second (c/s) used a compensated density logging tool equipped with a Cs137 radioactive source.</li> <li>The CPS values were then converted to physical property values using calibrations determined specifically for each physical property parameter.</li> <li>The final data were supplied in a Logging ASCII Standard (CSV) file format.</li> <li>Single and three arm callipers were used in-hole to identify areas where blowouts and significant aberrations in the hole rugosity were encountered; any deviations from within 20% of the nominal hole diameter were removed from the analysis.</li> </ul>
	<i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i>	<ul style="list-style-type: none"> <li>Certified reference materials demonstrate that sample assay values are accurate.</li> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>Commercial laboratories used by Dacian were audited in April 2021 by the Competent Person. The laboratory is monitored regularly by Dacian through QAQC practices, and strong communication channels are in place for data quality.</li> <li>The on-site laboratory was visited by the Competent Person twice in December 2020, is monitored regularly by Dacian through QAQC practices, and strong communication channels are in place for data quality.</li> <li>Umpire laboratory test work was completed in 2019 over mineralised</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>intersections with good correlation of results.</p> <ul style="list-style-type: none"> <li>• Umpire testwork of grade control pulp duplicate samples from December 2020 through June 2021 between PAL/LW_AAS and FA40AAS methods showed high correlation.</li> <li>• Where QC data are available, acceptable levels of precision and accuracy have been established.</li> </ul>
<b>Verification of sampling and assaying</b>	<i>The verification of significant intersections by either independent or alternative company personnel.</i>	<ul style="list-style-type: none"> <li>• Significant intersections were visually field verified by several company geologists.</li> </ul>
	<i>The use of twinned holes.</i>	<ul style="list-style-type: none"> <li>• Recent have verified the intersections of historic mineralisation by either confirming the continuity of the mineralisation and geological interpretations or twinning the mineralisation.</li> </ul>
	<i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i>	<ul style="list-style-type: none"> <li>• Prior to 2021, primary data was collected into a custom logging Excel spreadsheet and then imported into a DataShed drillhole database. The logging spreadsheet included validation processes to ensure the entry of correct data.</li> <li>• From January 2021, primary data was collected into LogChief logging software by MaxGeo and then imported into a Data Shed drillhole database. Logchief has internal data validation.</li> </ul>
	<i>Discuss any adjustment to assay data.</i>	<ul style="list-style-type: none"> <li>• Assay values that were below detection limit are stored in the database in this form, but are adjusted to equal half of the detection limit value for grade estimates. The following records were set to half detection limit: <ul style="list-style-type: none"> <li>○ Negative below detection limit assays</li> <li>○ Zeros</li> <li>○ Nulls</li> <li>○ Unsampled intervals</li> </ul> </li> <li>• Any negatives below -1 were set to null, as these represent lab error codes such as samples not received, samples destroyed in sample preparation, insufficient sample volume/weight etc.</li> </ul>
<b>Location of data points</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>• All Dacian hole collars were surveyed in a local grid with transform parameters determined from surveyed pillars accurately surveyed in both the local "MTM2017" grid and MGA94 Zone 51 grid using differential GPS to 3cm accuracy.</li> <li>• Historic drill hole collar coordinates were tied to a local Dominion Mining grid with subsequent conversion to MGA94 Zone 51.</li> <li>• The down-hole survey method for 160 RC holes and 57 DD holes (including diamond tails) informing the resource is varied. Survey methods include Eastman SS, Reflex, Gyro, Camtek, Sunto, SingleShot, Devi Rapid, Azi Aligner and EMS.</li> <li>• Open pit (OP) mine workings support the locations of historic drilling.</li> <li>• UG DD and all Dacian RC holes were down hole surveyed with a north seeking gyro tool at &lt;=30m intervals down the hole.</li> </ul>
	<i>Specification of the grid system used.</i>	<ul style="list-style-type: none"> <li>• The grid system used is the local "MTM2017" grid, with all collars and surveys transformed from either the MGA94 Zone 51 or historic Dominion grids.</li> </ul>
	<i>Quality and adequacy of topographic control.</i>	<ul style="list-style-type: none"> <li>• Topographic surfaces were prepared from detailed ground, mine, and aerial surveys.</li> <li>• Material above all surfaces was coded in the model as depleted to ensure no mineralisation above these surfaces was included in the MRE.</li> <li>• The Competent Person is satisfied that the topographic control provides the quality required to report the Mineral Resources in accordance with the JORC Code.</li> </ul>
<b>Data spacing and distribution</b>	<i>Data spacing for reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>• Exploration results are not being reported</li> <li>• The drill hole spacing is highly variable as a result of the variable drilling and sampling techniques.</li> <li>• RC GC holes have achieved a high density of mineralisation pierce points in and ~20 m below the pits of up to 4 m by 4 m.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>The exploration RC and DD holes are typically on 20 m sections, although they extend wider to 80 m sections and greater, at which spacing the material has not been classified.</li> </ul>
	<i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i>	<ul style="list-style-type: none"> <li>The mineralised domains have sufficient continuity in both geology and grade to be considered appropriate for the Mineral Resource estimation procedures and classification applied under the JORC Code, and mining has shown a high correlation with the historically mined lodes with the mineralisation interpretation.</li> <li>There is less confidence in the interpretation of the deeper, flatter-dipping Ramornie South lodes, as this is these are the only lodes with the orientation, and the lodes have been drilled exclusively from underground on a shallower angle than optimum.</li> <li>This has been mitigated by the data density of nominal 20 m spaced pierce points and classification as Inferred.</li> </ul>
	<i>Whether sample compositing has been applied.</i>	<ul style="list-style-type: none"> <li>Samples have been composited to 1m lengths in mineralised lodes for statistics and estimation.</li> <li>Compositing was completed using a 'best-fit' method in Surpac software, which forces all samples to be included in one of the composites by adjusting composite lengths, while keeping it as close as possible to 1m.</li> </ul>
<b>Orientation of data in relation to geological structure</b>	<i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i>	<ul style="list-style-type: none"> <li>Surface holes were drilled at a planned bearing (azimuth) that approximates a perpendicular orientation of mineralised lodes.</li> <li>The nature of the UG DD holes means the drilling orientations are highly variable.</li> <li>Additionally, the deeper, flatter lodes of Ramornie South have been predominantly drilled from UG on a flat angle, which has caused a lower than optimum angle of intercept for most drilling into the lodes. This has caused a lower confidence in the mineralisation model.</li> <li>This has been mitigated by the data density of nominal 20 m spaced pierce points and classification as Inferred.</li> <li>Where possible, the surface drill holes have mostly intersected the mineralisation at a high angle.</li> </ul>
	<i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i>	<ul style="list-style-type: none"> <li>No orientation-based sampling bias has been identified in the data.</li> </ul>
<b>Sample security</b>	<i>The measures taken to ensure sample security.</i>	<ul style="list-style-type: none"> <li>Chain of custody was managed by the companies that owned the projects at the time, and no issues regarding historic sample security are known.</li> <li>Dacian samples were stored on site until collected for transport to the sample preparation laboratory in Kalgoorlie. Dacian personnel had no contact with the samples once they are picked up for transport. Tracking spreadsheets were used by Dacian personnel to track the progress of samples.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of sampling techniques and data.</i>	<ul style="list-style-type: none"> <li>Regular reviews of RC and DD sampling techniques were completed by the Dacian Senior Geologists and the Principal Resource Geologist, which concluded that sampling techniques are satisfactory.</li> <li>No audits or reviews have been documented for historic sampling techniques, but the data have been reviewed by checking historic logging files with database records.</li> <li>Commercial laboratories used by Dacian were audited in April 2021 by the Competent Person.</li> <li>The Competent Person visited the on-site contract laboratory twice in December 2020 to review processes. All laboratories were performing at and producing results for a standard required to report a MRE in accordance with the JORC Code.</li> <li>Review of Dacian QAQC data has been carried out by company geologists.</li> </ul>

# Ramornie

## Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
<b>Mineral tenement and land tenure status</b>	<i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i>	<ul style="list-style-type: none"> <li>The Ramornie deposit is located within two Mining Leases, M39/018 (~95% by area) and M39/228 (~5%), 100% owned by Mt Morgans WA Mining Pty Ltd, a wholly owned subsidiary of Dacian Gold Ltd.</li> </ul>
	<i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.</i>	<ul style="list-style-type: none"> <li>The above tenements are all in good standing.</li> </ul>
<b>Exploration done by other parties</b>	<i>Acknowledgment and appraisal of exploration by other parties.</i>	<ul style="list-style-type: none"> <li>Open pit and underground mining has occurred since the 1890s across Mt Morgans.</li> <li>Exploration activities at the deposit have been undertaken by Anaconda, Auswhim, Dominion, Homestake Gold, Plutonic, Placer, Barrick, and Range River.</li> <li>A high proportion of the historic data is confirmed by recent drilling and is of a quality that, in the Competent Person's view, supports the MRE at the classification applied.</li> </ul>
<b>Geology</b>	<i>Deposit type, geological setting and style of mineralisation.</i>	<ul style="list-style-type: none"> <li>The mineralisation has been formed along three parallel structures to or within the local Ramornie – Transvaal Shear that cross-cuts the Westralia stratigraphy in greenschist facies altered basalt flows.</li> <li>Gold mineralisation is hosted within north-northeast trending shear-hosted lodes.</li> <li>The style of mineralisation is less well understood than other deposits, such as the proximal Transvaal and Craic deposits, but as the former lies on the same local Ramornie – Transvaal Shear, the mineralisation style is expected to be equivalent.</li> <li>Mineralisation and host rocks within the OP exposures confirm the geometry of the mineralisation.</li> <li>A relatively shallow oxidation profile exists of 5 m – 10 m completely oxidised and ~25 m of transitional material.</li> <li>The deposit has been divided into three zones based on the three structural corridors hosting the modelled lodes, all of which strike north relative to Grid North (NE in MTM2017); this division forms the “Ramornie Complex” of: <ul style="list-style-type: none"> <li>Ramornie South – a structure that hosts sub-vertical lodes that dip steeply to the NW and SE (MTM2017 grid) which were mined from the Ramornie and Ramornie North pits, and, at the SW end, a discrete mineralised area that has developed four lodes that dip and plunge moderately to the NE across the structure.</li> <li>Ramornie Central – a structure that hosts sub-vertical lodes that dip steeply to the SE (MTM2017 grid)</li> <li>Ramornie – a structure that hosts sub-vertical lodes that dip steeply to the SE (MTM2017 grid), and which were mined in the Sarah pit.</li> </ul> </li> <li>The porphyry dykes strike NNE to NE, and display a moderate dip to the E or NE, cross-cutting or delineating the mineralised structures into the lodes.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Drill hole information</b>	<i>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
	<i>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
<b>Data aggregation methods</b>	<i>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> <li>No grade-weighting or other techniques have been applied to gold grades in figures.</li> </ul>
	<i>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
	<i>The assumptions used for any reporting of metal equivalent values should be clearly stated.</i>	<ul style="list-style-type: none"> <li>No metal equivalent values have been used</li> </ul>
<b>Relationship between mineralisation widths and intercept lengths</b>	<i>These relationships are particularly important in the reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>The drilling angle of holes is highly variable owing to the surface RC and DD, in-pit GC, and UG DD drilling types and locations.</li> <li>Additionally, the deeper, flatter lodes of Ramornie South have been exclusively drilled from UG on a flat angle, which has caused a lower than optimum angle of intercept for most drilling into the lodes. This has caused a lower confidence in the mineralisation model.</li> </ul>
	<i>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</i>	<ul style="list-style-type: none"> <li>The surface drill holes have mostly intersected the mineralisation at a high angle.</li> </ul>
	<i>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
<b>Diagrams</b>	<i>Appropriate maps and sections</i>	<ul style="list-style-type: none"> <li>Relevant diagrams have been included within the main body this ASX</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>(with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</i>	release.
<b>Balanced Reporting</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>All Dacian hole collars were surveyed in MGA94 Zone 51 grid using differential GPS to within 3cm. Dacian holes were down-hole surveyed either with a north seeking gyroscopic tool at 30m intervals to 20cm accuracy.</li> <li>Historic drill hole collar coordinates were tied to a local grid with subsequent conversion to MGA94 Zone 51. The transformation parameters were taken from the Dominion Mining reference manual, which were used to recalculate the collar positions in GDA94 MGA51 by the Competent Person as a check on the accuracy, finding little to no difference in the positions for Transvaal.</li> <li>The Competent Person is satisfied that the recent Dacian 2021 drill holes have confirmed the locations of the mineralisation with acceptable accuracy for supporting the MRE.</li> </ul>
	<i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
<b>Other substantive exploration data</b>	<i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i>	<ul style="list-style-type: none"> <li>The wireline geophysical data logged throughout Mt Morgans by Surtech systems in February 2021 was used to inform the MRE, although they were not taken from the Maxwell Bore deposit.</li> <li>Gamma-density values at 10 cm spacing were measured downhole as described within this Table 1 on six RC holes at Craic, and six DD and three RC holes at Transvaal. Analysis and results were used to inform the density estimate for Ramornie.</li> </ul>
<b>Further work</b>	<i>The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large- scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i>	<ul style="list-style-type: none"> <li>UG optimisation of the MRE for inclusion in the Dacian LOM is planned, which will provide guidance on the locations of infill drilling to permit a MRE update.</li> </ul>

## Ramornie

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)



Criteria	JORC Code explanation	Commentary
<b>Database integrity</b>	<i>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</i>	<ul style="list-style-type: none"> <li>The data base has been systematically audited by Dacian geologists and database-specialist consultant geologists. Original drilling records were compared to the equivalent records in the data base (where original records were available). Any discrepancies were noted and rectified by the data base manager.</li> </ul>
	<i>Data validation procedures used.</i>	<ul style="list-style-type: none"> <li>Historic logs were located and additional logging information, particularly relating to weathering, was input into the database.</li> <li>Ongoing database (DB) validation has been undertaken by a dedicated DB administrator communicating with geologists as the primary data sources and labs.</li> <li>Extensive validation was undertaken by the database administrator.</li> <li>Data were loaded into DataShed back-end SQL Server DB on a related data schema, providing a referentially integral database with primary key relations and look-up validation fields.</li> <li>Additional validation completed in Datamine by Dacian geologists, with any validation issues relayed to DB administrator. All Dacian drilling data has been verified as part of a continuous validation procedure. Once a drill hole is imported into the data base reports of the collar, down-hole survey, geology, and assay data are produced. These are then checked by a Dacian geologist in geological software and any corrections are sent to the data base administrator to complete.</li> <li>All data were checked for the following errors: <ul style="list-style-type: none"> <li>Duplicate drillhole IDs</li> <li>Missing collar coordinates</li> <li>Mis-matched or missing FROM or TO fields in the interval tables (assays, logging etc)</li> <li>FROM value greater than TO value in interval tables</li> <li>Non-contiguous sampling intervals</li> <li>Sampling interval overlap in the assay table</li> <li>The first sample in the interval file not starting at 0 m</li> <li>Interval tables with depths greater than the collar table EOH depth.</li> </ul> </li> <li>Survey data were checked for large deviations in azimuth and dip between consecutive records, with none found.</li> </ul>
<b>Site visits</b>	<i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i>	<ul style="list-style-type: none"> <li>The Competent Person has made several site visits during 2020 and 2021, and has worked with the site-based geologists and mining engineers on the MRE and reconciliation processes relevant to this estimate.</li> <li>Inspection of the equipment used by Dacian's drilling contractor at the time of the visits found all operators working to a standard required to report the MREs in accordance with the JORC Code.</li> <li>The Competent Person visited the on-site laboratory twice in December to review processes, and each of the two National Association of Testing Authorities (NATA) accredited offsite contract laboratories in 2021. All laboratories were performing at and producing results for a standard required to report the MREs in accordance with the JORC Code.</li> </ul>
	<i>If no site visits have been undertaken indicate why this is the case.</i>	<ul style="list-style-type: none"> <li>N/A</li> </ul>
<b>Geological interpretation</b>	<i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i>	<ul style="list-style-type: none"> <li>The confidence in the geological interpretations for the MRE is low to moderate, as the drilling density is low in most of the deposit, and the angle of intersection of the mineralisation is low.</li> <li>Where OP extraction has occurred and the lodes extend below the pit or along the same mineralising structure, the confidence is moderate.</li> </ul>
	<i>Nature of the data used and of any assumptions made.</i>	<ul style="list-style-type: none"> <li>Geological logging has been used to assist identification and delineation of lithology, weathering and mineralisation.</li> <li>The following mineralisation modelling techniques were incorporated into the modelling, which has formed assumptions regarding the continuity: <ul style="list-style-type: none"> <li>Logging of weathering was used to model base-of-complete-oxidation (BOCO) and top-of-fresh (TOFR) surfaces. Isolated peaks and troughs created by variable logging were ignored for a smoother surface that is assumed to be less likely to be influenced by subjective differences or error in the logging.</li> </ul> </li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Any internal waste units not assayed across several metres were excluded from mineralisation wireframes to provide coherent geometries.</li> <li>All lodes were modelled above a moderately strict cut-off of 0.5g/t, except for the retention of continuity, where lower grades were allowed.</li> <li>Boundary strings were utilised to control the strike and down dip extents beyond the last known drill hole data.</li> <li>Amorphous blob-shapes were prevented to avoid estimates 'seeing' composites across holes and around fluid boundaries.</li> <li>All lodes were treated as hard-boundaries for statistics and estimation.</li> <li>Porphyry intrusions were modelled predominately in the Ramornie Central area on the same trend of the those modelled at Beresford (Westralia mine corridor).</li> </ul>
	<i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>Alternate interpretations may consider a different gold grade cut-off for the modelling of mineralisation, which will change the tonnages and have a complementary higher or lower grade for. Either of these are likely to result in a similar balance of metal.</li> <li>Differences may result from alternate mining software used or approaches to solid volumes modelled, as the Leapfrog modelling method tends to create more fluid and drillhole constrained objects than a sectionally produced wireframe approach.</li> <li>Further drilling is likely to improve the geological understanding of Ramornie.</li> </ul>
	<i>The use of geology in guiding and controlling Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>All lodes were treated as hard-boundaries for statistics and estimation.</li> <li>High-grade accumulations are noted within the porphyries across the contacts of the basalt, and within the planes of the mineralised structures. The samples and volumes within the mineralised structures and in the porphyry volumes have been estimated independently with a hard boundary to the basalt-hosted mineralisation within the same lode. However, the grades rapidly decrease moving into the porphyries where sample density is lower, causing higher-grade clustering within the porphyries near their contacts, so that the grades are likely to have smeared through the thickness of the porphyry volumes without an ability (such as an alteration halo or other geologically confirmed hard boundary) to control the grades from smearing away from the contact into the porphyry volume. Therefore, have not been classified nor reported,</li> <li>Statistics were reviewed, including grade distributions, contact analysis and variogram continuity, between the oxidation domains, which showed that no boundaries were present, and therefore no hard boundaries by oxidation domain were applied.</li> <li>Porphyry units are also mineralised at times but not visually recognisable as mineralised. Lodes generally are truncated by the porphyries into discrete lode objects, but where the mineralising structures cross-cut the porphyries, the mineralisation appears to extend sub-metre scale into the porphyries, and therefore the MREs exclude porphyry-hosted mineralisation.</li> <li>The following objects were modelled that the Competent Person considers adequate to control the MRE. <ul style="list-style-type: none"> <li>Lodes: 21</li> <li>Porphyry dykes: 32</li> <li>Oxidation/weathering: base of complete oxidation (BOCO), top of fresh (TOFR)</li> </ul> </li> </ul>
	<i>The factors affecting continuity both of grade and geology.</i>	<ul style="list-style-type: none"> <li>The mineralised lodes at Mount Marven occur within a greater shear corridor and are hosted by both mafic and porphyry units suggesting gold mineralization continued post-intrusion. A WNW structure splits the mineralization between the historic northern and southern pit.</li> </ul>
<b>Dimensions</b>	<i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i>	<ul style="list-style-type: none"> <li>Ramornie South: <ul style="list-style-type: none"> <li>Strike length: 800 m</li> <li>Width: 237 m</li> <li>Depth: 210 m</li> </ul> </li> <li>Ramornie Central: <ul style="list-style-type: none"> <li>Strike length: 360 m</li> <li>Width: 76 m</li> <li>Depth: 180 m</li> </ul> </li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Ramornie North: <ul style="list-style-type: none"> <li>Strike length: 1,115 m</li> <li>Width: 120 m</li> <li>Depth: 195 m</li> </ul> </li> </ul> <p>The thickness of the lodes ranges from 2 m – 10 m, averaging 3 m.</p>
<b>Estimation and modelling techniques</b>	<i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i>	<ul style="list-style-type: none"> <li>Samples were composited to 1 m intervals ("composites") based on assessment of the raw drillhole sample intervals. Statistics were weighted by composite length in Supervisor.</li> <li>Statistical analysis was completed in Snowden Supervisor™ 8.14 software, including modelling of the spatial continuity of gold grades by variography.</li> <li>Statistics were length-weighted.</li> <li>Cell de-clustering analysis using cell size combinations of 5m to 20 m in X, Y and Z directions was undertaken for 10 largest lodes by volume.</li> <li>Domains were based on spatial characteristics (location, orientation, and geometry) of lodes.</li> <li>Visual validation of composite grades was reviewed in Surpac to determine if there were any trends with depth or accumulation on weathering/oxidation boundaries.</li> <li>A final cell de-cluster size of 15m X, 15m Y and 10m Z was used for the estimate.</li> <li>Composites were split by weathering domains and hole type to review populations requiring separate treatment in the estimate.</li> <li>A total of 10 composites (out of 1,036) were flagged as mineralisation within porphyry solid volumes used for the estimation. Given the low number and the spatial variation of these composites, the impact on the estimation is considered immaterial.</li> <li>Insufficient statistics existed above the oxide and transitional surfaces within the lodes. The lodes show continuity regardless of the weathering, with no supergene dispersion halo evident. Therefore, the lodes were not split by the oxidation profile.</li> <li>Multi-block kriging neighbourhood analysis (KNA) was undertaken using Supervisor™ software to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE), slope of regression (SOR) and negative weights were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids. Statistics were invariable for changes in discretisation.</li> <li>Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains. The technique is considered appropriate to allow the geostatistical continuity determined from variography to weight samples during estimation.</li> <li>Geological modelling, sample compositing, block modelling and grade estimation were undertaken using Leapfrog™ software.</li> <li>The estimation technique is appropriate to allow a locally adequate estimate for detailed mine planning and with a globally unbiased estimate per lode.</li> <li>A three-pass expanding search ellipse strategy was used, honouring the anisotropic ratios orthogonally. Search parameters for each pass were as follows: <ul style="list-style-type: none"> <li>Pass 1 = 25m</li> <li>Pass 2 = 50m</li> <li>Pass 3 = 100m</li> </ul> </li> <li>Grades have not been interpolated into the waste, as there is short range continuity of the lodes at Ramornie and little evidence for a grade halo. There were examples of lodes crossing into porphyries however, the mineralisation has been estimated and depleted within these areas.</li> <li>In each pass, the search ellipse anisotropic ratios and orientations honoured the variogram model.</li> <li>All Lodes:</li> <li>1<sup>st</sup> Pass: <ul style="list-style-type: none"> <li>Max samples 16</li> <li>Min samples 6</li> <li>Max samples per drillhole 6</li> <li>Face samples – N/A</li> <li>No octants</li> <li>Grade Limiting of from 8g/t to 25m</li> </ul> </li> </ul>

Criteria	JORC Code explanation	Commentary																																																						
		<ul style="list-style-type: none"><li>2<sup>nd</sup> pass:<ul style="list-style-type: none"><li>Max samples 10</li><li>Min samples 2</li><li>Max samples per drillhole 6</li><li>Face samples – N/A</li><li>No octants.</li><li>Grade Limiting from 8g/t to 25m</li></ul></li><li>3<sup>rd</sup> pass:<ul style="list-style-type: none"><li>Max samples 10</li><li>Min samples 2</li><li>Max samples per drillhole 6</li><li>Face samples – N/A</li><li>No octants.</li><li>Grade Limiting above 8g/t to 25m</li></ul></li></ul>																																																						
	<i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i>	<ul style="list-style-type: none"><li>A previous MRE by Ashmore Consulting with Sean Serle as Competent Person was announced by Dacian Gold in 2018:<table><tr><th colspan="3">Indicated</th><th colspan="3">Inferred</th><th colspan="3">Total</th></tr><tr><th>kt</th><th>Au (g/t)</th><th>koz</th><th>kt</th><th>Au (g/t)</th><th>koz</th><th>kt</th><th>Au (g/t)</th><th>koz</th></tr><tr><td>160</td><td>4.1</td><td>21</td><td>422</td><td>4.0</td><td>55</td><td>582</td><td>4.1</td><td>76</td></tr></table></li><li>The “Ramornie OP” MRE previously reported by Dacian was removed due to changes in the Company’s geological understanding of this deposit. The “Ramornie UG” MRE was updated and then publicly updated to 27 koz by Dacian Gold for a reduced area, which was considered to show more reasonable prospects for eventual economic extraction (RPEEE):<table><tr><th colspan="3">Indicated</th><th colspan="3">Inferred</th><th colspan="3">Total</th></tr><tr><th>kt</th><th>Au (g/t)</th><th>koz</th><th>kt</th><th>Au (g/t)</th><th>koz</th><th>kt</th><th>Au (g/t)</th><th>koz</th></tr><tr><td>212</td><td>3.2</td><td>22</td><td>61</td><td>3.1</td><td>6</td><td>274</td><td>3.1</td><td>27</td></tr></table></li><li>The Ramornie UG MRE was then removed from Dacian Gold’s global tabulations on 11/05/2021 as part of a Greater Westralia Area (GWMA) update announcement, which allowed Dacian Gold time to update the MRE for this announcement in full context of the “Ramornie Complex”, rather than isolated zones of the larger mineralised structures.</li><li>The Competent Person is not satisfied that the previous MREs took appropriate account of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data). Therefore, no comparison has been made to the previous MREs.</li><li>Historic mine production figures from the Ramornie pits were not been available to the Competent Person for reconciling the MRE. However, the mineralisation mined by OP methods shows high correlation to the holes drilled and mineralisation modelled on the entire Ramornie resource database since OP extraction.</li></ul>	Indicated			Inferred			Total			kt	Au (g/t)	koz	kt	Au (g/t)	koz	kt	Au (g/t)	koz	160	4.1	21	422	4.0	55	582	4.1	76	Indicated			Inferred			Total			kt	Au (g/t)	koz	kt	Au (g/t)	koz	kt	Au (g/t)	koz	212	3.2	22	61	3.1	6	274	3.1	27
Indicated			Inferred			Total																																																		
kt	Au (g/t)	koz	kt	Au (g/t)	koz	kt	Au (g/t)	koz																																																
160	4.1	21	422	4.0	55	582	4.1	76																																																
Indicated			Inferred			Total																																																		
kt	Au (g/t)	koz	kt	Au (g/t)	koz	kt	Au (g/t)	koz																																																
212	3.2	22	61	3.1	6	274	3.1	27																																																
	<i>The assumptions made regarding recovery of by-products.</i>	<ul style="list-style-type: none"><li>No assumptions have been made regarding the recovery of by-products.</li></ul>																																																						
	<i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i>	<ul style="list-style-type: none"><li>No deleterious elements have been estimated.</li></ul>																																																						
	<i>In the case of block model interpolation, the block size in relation to the average sample spacing and the</i>	<ul style="list-style-type: none"><li>A parent block size of 15 m x 15 m x 10 m (X x Y x Z) was chosen, which was supported KNA and by drill hole spacing all directions.</li><li>Sub-celling to 1/8 of parent cell in all directions has provided appropriate resolution for volume control to account for the moderately thin lode</li></ul>																																																						

Criteria	JORC Code explanation	Commentary
	<i>search employed.</i>	<p>wireframes.</p> <ul style="list-style-type: none"> <li>Most of the deposit has been drilled at a density of 20m by 20m and out to 40m by 40m on the fringes.</li> </ul>
	<i>Any assumptions behind modelling of selective mining units.</i>	<ul style="list-style-type: none"> <li>No assumptions have been made regarding SMUs.</li> </ul>
	<i>Any assumptions about correlation between variables.</i>	<ul style="list-style-type: none"> <li>Gold has been estimated univariately and in isolation of other variables.</li> </ul>
	<i>Description of how the geological interpretation was used to control the resource estimates.</i>	<ul style="list-style-type: none"> <li>Geology and grade were used to define the mineralisation lodes. Within each lode, the estimate was constrained to blocks within the lode wireframe using only top-cut composited samples from the corresponding lode.</li> </ul>
	<i>Discussion of basis for using or not using grade cutting or capping.</i>	<ul style="list-style-type: none"> <li>High-grade top-caps were applied to limit the influence of extreme outliers on the grade estimate. The top-caps were applied to the mineralisation domains following statistical analysis.</li> <li>A global Top-cuts were determined for Transvaal lodes within three statistical domains, while a single top-cut was determined for porphyry material, as follows: <ul style="list-style-type: none"> <li>Ramornie South flat-dip domain: 12 g/t</li> <li>Ramornie South steep-dip domain: no top-cut (no outliers)</li> <li>Ramornie Central domain 1: 25 g/t</li> <li>Ramornie Central domain 2: 30 g/t</li> <li>Ramornie North domain: no top-cut (no outliers)</li> </ul> </li> <li>The top-cuts were kept at around 1% – 3% of the grade distribution for each lode or statistical domain, for ~5% of the metal.</li> </ul>
	<i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i>	<ul style="list-style-type: none"> <li>Validation of the estimate was completed for the resource block models using numerical methods (histograms, CDFs and swath plots) and validated visually against the input raw drillhole data, declustered data, composites and blocks.</li> </ul>
<b>Moisture</b>	<i>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</i>	<ul style="list-style-type: none"> <li>Tonnages and grades have been estimated on a dry in situ basis.</li> </ul>
<b>Cut-off parameters</b>	<i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i>	<ul style="list-style-type: none"> <li>The MRE has been reported above a lower cut-off of 0.5 g/t Au where above the 290 m RL or above a lower cut-off of 2.0 g/t Au where below the 290 m RL.</li> <li>The RL split for the changes to the cut-off grade were selected by the Competent Person, who considered that the higher-grades were required approximately 150 m from the topographic surface, while above this, the tenor of the mineralisation did not appear to support a deeper RL split.</li> <li>The reporting cut-off parameters were selected based on known UG economic cut-off grades from Dacian's OP and UG operations.</li> </ul>
<b>Mining factors or assumptions</b>	<i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i>	<ul style="list-style-type: none"> <li>Previous operators mined both deposits using the methods currently in use by Dacian. It is assumed that the same mining methods will be applicable for extraction of in-situ material included in this MRE update.</li> </ul>

Criteria	JORC Code explanation	Commentary												
<b>Metallurgical factors or assumptions</b>	<i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i>	<ul style="list-style-type: none"> <li>The ore is intended to be processed at the Jupiter Processing Facility, part of the Mt Morgans Gold Operation (MMGO). Recoveries achieved to date are 92.3%.</li> </ul>												
<b>Environmental factors or assumptions</b>	<i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i>	<ul style="list-style-type: none"> <li>Ramornie, Ramornie North, Sarah and Westralia are within the MMGO mining leases, having been working mines in the past or (latter) an active mine, achieving all requisite environmental approvals. Dacian believes that there will be no impediments to the approval of mining the deposits again.</li> <li>Waste rock will be stored in a conventional waste dump.</li> </ul>												
<b>Bulk density</b>	<i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i>	<ul style="list-style-type: none"> <li>Specific gravity (immersion method) determinations number 1391 from surface drilling and 402 from UG drilling. These are plotted by depth to determine if any relationship exists, notwithstanding the issue that UG depths are not related to the depth from surface. However, the analysis shows that a high proportion of the data fall within a range of ~2.65 t/m<sup>3</sup> – 2.9 t/m<sup>3</sup>.</li> <li>This data was used to confirm that the gamma density data from the closest and geologically related deposit, Craic, was suitable from which to apply densities. The densities applied to the Craic MRE update (in this announcement) are listed below by lithological and oxidation types.</li> </ul> <table border="1"> <thead> <tr> <th>Oxidation</th><th>Porphyry</th><th>Mineralisation &amp; Mafic waste</th></tr> </thead> <tbody> <tr> <td>Oxide</td><td>1.6 (none)</td><td>1.7</td></tr> <tr> <td>Trans</td><td>2.3</td><td>2.6</td></tr> <tr> <td>Fresh</td><td>2.7</td><td>2.9</td></tr> </tbody> </table>	Oxidation	Porphyry	Mineralisation & Mafic waste	Oxide	1.6 (none)	1.7	Trans	2.3	2.6	Fresh	2.7	2.9
Oxidation	Porphyry	Mineralisation & Mafic waste												
Oxide	1.6 (none)	1.7												
Trans	2.3	2.6												
Fresh	2.7	2.9												
	<i>The bulk density for bulk material must have been measured by methods that adequately account for void</i>	<ul style="list-style-type: none"> <li>Void space has been accounted for in the industry-standard, immersion method core density determination process.</li> <li>The gamma-density data were further adjusted by total porosity determined by borehole magnetic resonance (BMR) logging.</li> </ul>												



Criteria	JORC Code explanation	Commentary
	<i>spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i>	
	<i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i>	<ul style="list-style-type: none"> <li>For gamma-density, the data are quantitative and independent of sample weight, and have been analysed by modelled material types.</li> <li>For core immersion-method density data, no relationship to sample weight has been determined, and is expected to be unrelated, as the core density data show little variation with lithological types.</li> </ul>
<b>Classification</b>	<i>The basis for the classification of the Mineral Resources into varying confidence categories.</i>	<p>The Mineral Resources have been classified based on the guidelines specified in The JORC Code. Classification level is based on:</p> <ul style="list-style-type: none"> <li>Drill density data</li> <li>Geological understanding</li> <li>Quality of gold assay grades</li> <li>Continuity of gold grades</li> <li>Economic potential for mining.</li> </ul> <ul style="list-style-type: none"> <li>Unclassified material: <ul style="list-style-type: none"> <li>Mined volumes including mineralisation were set to 0 and insitu set to 1.</li> <li>No exploration potential mineralisation was classified, as the drilling density for modelled mineralisation was insufficient to support an Inferred classification.</li> <li>Mined areas, chiefly the historical pits and UG workings, were set to AIR min code for depletion purposes.</li> </ul> </li> <li>For Inferred Mineral Resources, the following statistical considerations for the quality of the grade estimate were used to classify large, contiguous, and coherent zones of blocks: <ul style="list-style-type: none"> <li>Drill hole spacing reaches 20 m to 20 m.</li> <li>Estimation was undertaken in search passes of 1 and 2.</li> <li>Number of samples was used was near the optimum.</li> </ul> </li> </ul>
	<i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i>	<ul style="list-style-type: none"> <li>All factors the Competent Person has deemed relevant to the MRE have been incorporated into the classification of Mineral Resources.</li> </ul>
	<i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i>	<ul style="list-style-type: none"> <li>The result appropriately reflects the Competent Person's view of the deposit.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of Mineral Resource estimates.</i>	<ul style="list-style-type: none"> <li>Internal audits were completed by Dacian, which verified the technical inputs, methodology, parameters and results of the estimate.</li> </ul>
<b>Discussion of relative accuracy/confidence</b>	<i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that</i>	<ul style="list-style-type: none"> <li>The accuracy of the MRE is communicated through the classification assigned to the deposit. The MRE has been classified in accordance with the JORC Code (2012 Edition) using a qualitative approach. All factors that have been considered have been adequately communicated in Section 1 and Section 3 of this table.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>could affect the relative accuracy and confidence of the estimate.</i>	
	<i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i>	<ul style="list-style-type: none"> <li>The MRE statement relates to a global estimate of in-situ tonnes and grade.</li> </ul>
	<i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i>	<ul style="list-style-type: none"> <li>Historic mine production figures from the Ramornie pits were not been available to the Competent Person for reconciling the MRE. However, the mineralisation mined by OP methods shows high correlation to the holes drilled and mineralisation modelled on the entire Ramornie resource database since OP extraction.</li> </ul>

## McKenzie Well

### Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> <li>Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.</li> <li>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</li> <li>Aspects of the determination of mineralisation that are Material to the Public Report.</li> <li>In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.</li> </ul>	<ul style="list-style-type: none"> <li>Surface Reverse Circulation (RC) drilling was carried out over the McKenzie Well prospect.</li> <li>Surface (RC) holes were angled to intersect the targeted mineralised zones at optimal angles to pierce as close to perpendicular as possible.</li> <li>The 90 DCN RC holes all intercepted mineralisation and were sampled over the entire length of hole on 1 m intervals via the inner tube to a cyclone and over an on-board cone splitter to produce a primary sample split of approximately 3 kg.</li> <li>DCN samples were submitted to a contract laboratory for crushing and pulverising to produce either a 40 g or 50 g charge for fire assay.</li> <li>For all historical RC drilling, Dacian has retained the original logs and laboratory results as either original hard copies or as scanned copies.</li> <li>The 25 historical RC drillholes—17 of which intercepted mineralisation—were drilled by Carpentaria Exploration Company Pty Ltd between 1987 and 1990 using a RC rig contracted from Robinson Drilling in Kalgoorlie.</li> <li>The original logs for the historical drilling and laboratory results are retained by Dacian as either original hard copies or as scanned copies. The samples were collected on 1 m intervals into plastic bags using a riffle splitter, and composited to 2 m for analysis by Australian Assay Laboratories Group in Leonora for crushing and pulverising to produce a 50 g charge for fire assay with a 0.01 ppm detection limit.</li> </ul>
Drilling techniques	<ul style="list-style-type: none"> <li>Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).</li> </ul>	<ul style="list-style-type: none"> <li>For Dacian RC holes, a 5¼" face sampling bit was used.</li> <li>For Historic RC drilling across the McKenzie Well project RC holes were completed using a Schram rig contracted from Robinson Drilling (Kalgoorlie), hole diameters are not recorded, but field</li> </ul>

Criteria	JORC Code explanation	Commentary
		observations of historic RC collars suggest the bit size was approximately 5 inch.
Drill sample recovery	<ul style="list-style-type: none"> <li>Method of recording and assessing core and chip sample recoveries and results assessed.</li> <li>Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> <li>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</li> </ul>	<ul style="list-style-type: none"> <li>RC drilling sample volumes, quality and recoveries were monitored by the supervising geologist, with a geologist always supervising RC drilling activities.</li> <li>RC holes were drilled with a powerful rig with compressor and booster compressor to ensure enough air to maximise sample recovery. The splitter is cleaned at the end of each rod, to ensure that efficient sample splitting. The weight of each sample split was monitored. Drilling is stopped if the sample split size changes significantly</li> <li>Recoveries from historical drilling are unknown.</li> <li>In DCN drilling no relationship exists between sample recovery and grade.</li> </ul>
Logging	<ul style="list-style-type: none"> <li>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> <li>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.</li> <li>The total length and percentage of the relevant intersections logged.</li> </ul>	<ul style="list-style-type: none"> <li>RC drilling was logged by passing a portion of each sampled metre into a sieve to remove rock flour from coarse chips, the chips are then washed and placed into metre marked chip trays for logging. Where the material type does not allow for the recovery of coarse rock chips the rock flour is retained as a record. The un-sieved sample is also observed for logging purposes. The detail is considered common industry practice and is at the appropriate level of detail to support mineralization studies.</li> <li>RC drilling is logged qualitatively by company geologists for various geological attributes including weathering, primary lithology, primary &amp; secondary textures, colour and alteration. All drill chips are photographed in the chip trays and RC chip trays are retained on site.</li> <li>At McKenzie Well, historic RC holes were logged for geology, alteration and structure, The Company retains copies of either the original or scanned copies of the geological logs.</li> <li>All DCN and historic drill holes were logged in full from start of hole to bottom of hole.</li> </ul>
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> <li>If core, whether cut or sawn and whether quarter, half or all core taken.</li> <li>If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.</li> <li>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> <li>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</li> <li>Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.</li> <li>Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul>	<ul style="list-style-type: none"> <li>DCN RC samples were collected via on-board cone splitters. A majority of samples were dry. Any wet samples were recorded as wet under sample condition, this data is then entered into a database.</li> <li>The RC sample was split using the cone splitter to give an approximate 3 kg sample. The remainder was collected into a plastic sack as a retention sample. At the grain size of the RC chips, this method of splitting is considered appropriate.</li> <li>For RC drilling, sample quality was maintained by monitoring sample volume and by cleaning splitters on a regular basis. If due to significant groundwater inflow or drilling limitations sample quality is degraded (consecutive intervals of wet sample or poor sample recovery) the RC hole is abandoned.</li> <li>Sample sizes are considered appropriate to correctly represent the gold mineralisation based on the style of mineralisation, the thickness and consistency of the intersections, the sampling methodology and assay value ranges for gold.</li> <li>Externally prepared Certified Reference Materials are inserted as QAQC.</li> <li>RC field duplicates were taken at 1 in 50.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>For DCN samples, sample preparation was conducted by a contract laboratory. After drying, the sample is subject to a primary crush, then pulverised to 85% passing 75µm.</li> <li>All historical RC samples were collected at the rig using riffle splitters. Samples condition was not recorded for a majority of the historic sampling. For historic RC drilling, information on the QAQC programs used is limited but acceptable with original batch reports having been reviewed and retained by DCN.</li> </ul>
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> <li>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</li> <li>For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</li> <li>Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.</li> </ul>	<ul style="list-style-type: none"> <li>For DCN drilling, the analytical technique used was a 40 g or 50 g lead collection fire assay and analysed by Atomic Absorption Spectrometry. This is a full digestion technique. Samples were analysed at Bureau Veritas in Perth or Kalgoorlie, Western Australia. This is a commonly used method for gold analysis and is considered appropriate for this project.</li> <li>For DCN drilling, sieve analysis was carried out by the laboratory to ensure the grind size of 85% passing 75 µm was being attained.</li> <li>For DCN RC drilling, QAQC procedures involved the use of certified reference materials (1 in 20) and blanks (1 in 50).</li> <li>Results were assessed as each laboratory batch was received and were acceptable in all cases.</li> <li>QAQC data has been reviewed for historic RC drilling and is acceptable.</li> <li>Laboratory QAQC includes the use of internal standards using certified reference material, blanks, splits and replicates.</li> <li>Certified reference materials demonstrate that sample assay values are accurate.</li> <li>Umpire laboratory test work was completed in 2019 over mineralised intersections with good correlation of results.</li> <li>Commercial laboratories used by DCN were audited in November 2019.</li> <li>For historic RC drilling, a fire assay technique was used and are viewed as appropriate with a detection limit of 0.01 ppm for all results. Information on the QAQC programs used is limited, although original batch reports have been reviewed and retained by DCN. Historic RC assay results will not be used for resource estimation or economic evaluation until a number of the historic assays have been validated through the completion of twinned RC holes by DCN.</li> </ul>
Verification of sampling and assaying	<ul style="list-style-type: none"> <li>The verification of significant intersections by either independent or alternative company personnel.</li> <li>The use of twinned holes.</li> <li>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</li> <li>Discuss any adjustment to assay data.</li> </ul>	<ul style="list-style-type: none"> <li>Significant intersections were verified visually in the field by company geologists and Senior Geologists.</li> <li>At McKenzie Well, historic RC drilling has been twinned by the 2020 drilling. A twin of a Dacian RC hole was also undertaken. The results confirm high repeatability of the mineralised intervals, although statistical analysis has not yet been undertaken.</li> <li>Primary data was collected into an Excel spread sheets and then imported into a Data Shed drillhole database. The logging spreadsheet includes validation processes to ensure the entry of correct data.</li> <li>Assay values that were below detection limit are stored in the database in this form, but were</li> </ul>

Criteria	JORC Code explanation	Commentary
		removed during the statistical compositing process to ensure many half-detection limit samples did not overly influence statistics and the grade estimate.
Location of data points	<ul style="list-style-type: none"> <li>• Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</li> <li>• Specification of the grid system used.</li> <li>• Quality and adequacy of topographic control.</li> </ul>	<ul style="list-style-type: none"> <li>• All DCN hole collars were surveyed in MGA94 Zone 51 grid using differential GPS.</li> <li>• DCN holes were down hole surveyed with a north-seeking gyro tool at 30 m intervals down the hole.</li> <li>• Historic drill hole collar coordinates were tied to a local grid or were surveyed in AMG with subsequent conversion to MGA94 Zone 51. For McKenzie Well, the historic RC hole collars were located in the field and surveyed in MGA94 Zone 51 grid using differential GPS to confirm the original and subsequently translated coordinates.</li> <li>• The topographic surface was prepared from triangulation of the DGPS collars, which resulted in a relatively flat-lying surface with minimal risk to the Mineral Resources.</li> </ul>
Data spacing and distribution	<ul style="list-style-type: none"> <li>• Data spacing for reporting of Exploration Results.</li> <li>• Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</li> <li>• Whether sample compositing has been applied.</li> </ul>	<ul style="list-style-type: none"> <li>• For the DCN RC drilling at McKenzie Well, the nominal hole spacing of surface drilling is approximately 40 m x 40 m, and 20 m x 40 m in the central area of the prospect.</li> <li>• Samples were not composited prior to or during chemical analysis. Samples were statistically composited within the estimation software, Surpac, to 1 m.</li> </ul>
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> <li>• Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</li> <li>• If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</li> </ul>	<ul style="list-style-type: none"> <li>• At McKenzie Well, RC holes were drilled at a bearing (Azimuth) of 210° relative to MGA94 grid north, at a dip of -60°, which is approximately perpendicular to orientation of the host stratigraphy.</li> <li>• As the drilling provides evenly spaced pierce points intersecting the mineralisation at a high-angle, the Competent Person deems that the orientation of the drillholes poses minimal risk to use of samples in preparing the Mineral Resource estimate.</li> </ul>
Sample security	<ul style="list-style-type: none"> <li>• The measures taken to ensure sample security.</li> </ul>	<ul style="list-style-type: none"> <li>• Chain of custody is managed by DCN. Samples are stored on site until collected for transport to the sample preparation laboratory in Kalgoorlie. DCN personnel have no contact with the samples once they are picked up for transport. Tracking sheets have been set up to track the progress of samples. Bureau Veritas, an ISO and NATA certified analysis company, have a robust sample management system based on bar coding, LIMS and other controls.</li> </ul>
Audits or reviews	<ul style="list-style-type: none"> <li>• The results of any audits or reviews of sampling techniques and data.</li> </ul>	<ul style="list-style-type: none"> <li>• Regular reviews of RC sampling techniques are completed by DCN geologists, and concluded that sampling techniques are satisfactory. The Competent Person reviewed the sampling practices of the drilling contractor, and found that the practices presented minimal risk to reporting Mineral Resources.</li> <li>• Commercial laboratories used by DCN have been audited in November, 2019.</li> <li>• Review of QAQC data has been carried out by the Competent Person, who deemed the sampling and results to be of minimal risk to reporting the Mineral Resource estimate.</li> </ul>

# McKenzie Well

## Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> <li>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</li> <li>The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.</li> </ul>	<ul style="list-style-type: none"> <li>McKenzie Well exploration project is located within Mining Lease M39/1137. M39/1137 is 100% owned by Dacian Gold Ltd.</li> <li>The above tenement is in good standing.</li> </ul>
Exploration done by other parties	<ul style="list-style-type: none"> <li>Acknowledgment and appraisal of exploration by other parties.</li> </ul>	<ul style="list-style-type: none"> <li>At McKenzie Well, previous exploration activities were completed by Carpentaria Exploration Company Pty Ltd between 1987 and 1990, as described in Section 1.</li> </ul>
Geology	<ul style="list-style-type: none"> <li>Deposit type, geological setting and style of mineralisation.</li> </ul>	<ul style="list-style-type: none"> <li>All Dacian Gold deposits are located within the Yilgarn Craton of Western Australia.</li> <li>The McKenzie Well exploration project occurs within the same stratigraphy as the Westralia project and it is assumed that the mineralisation type, setting and style is comparable to Westralia.</li> <li>The Westralia (including the Phoenix Ridge deposit) group of deposits are BIF hosted, sulphide replacement, mesothermal Archaean gold deposits comprising sedimentary packages composed predominantly of BIF but also including chert, mudstone, shales, conglomerate and minor felsic volcanoclastic rocks. All are intercalated within or separated by ultramafic volcanic rocks and variably intruded by felsic porphyry dykes and lamprophyres. Gold mineralisation is associated with quartz carbonate fractures and fine veinlets within BIF. BIF acts as the primary host for mineralisation though other rock types including basalt, porphyry intrusive and ultramafic may also be mineralised in smaller volumes and with less continuity. The grade and geometry of mineralisation is controlled by cross cutting structures that are interpreted to introduce reduced fluids into the oxidised BIF host.</li> <li>The Mineral Resources are hosted within two banded iron formation limbs of an overturned, south plunging syncline with vergence to the ESE at the fold hinge, where several axial planar lodes have developed.</li> </ul>
Drill hole Information	<ul style="list-style-type: none"> <li>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>easting and northing of the drill hole collar</li> <li>elevation or RL (Reduced Level – elevation above sea level in meters) of the drill hole collar</li> <li>dip and azimuth of the hole</li> <li>down hole length and interception depth</li> <li>hole length.</li> </ul> </li> <li>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</li> </ul>	Exploration results are not being reported.



Criteria	JORC Code explanation	Commentary
Data aggregation methods	<ul style="list-style-type: none"> <li>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.</li> <li>Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</li> <li>The assumptions used for any reporting of metal equivalent values should be clearly stated.</li> </ul>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
Relationship between mineralisation widths and intercept lengths	<ul style="list-style-type: none"> <li>These relationships are particularly important in the reporting of Exploration Results.</li> <li>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> <li>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').</li> </ul>	<ul style="list-style-type: none"> <li>At McKenzie Well, surface drill holes are angled to –60 degrees which is approximately perpendicular to the orientation of the expected trend of mineralisation. It is interpreted that true width is approximately 60-100% of down hole intersections depending on the orientation of the target which varies along strike and down dip.</li> </ul>
Diagrams	<ul style="list-style-type: none"> <li>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</li> </ul>	<ul style="list-style-type: none"> <li>Relevant diagrams have been included within the main body of this ASX release for the Mineral Resources. Exploration results are not being reported.</li> </ul>
Balanced reporting	<ul style="list-style-type: none"> <li>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</li> </ul>	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
Other substantive exploration data	<ul style="list-style-type: none"> <li>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</li> </ul>	<ul style="list-style-type: none"> <li>All interpretations for McKenzie Well mineralisation are consistent with observations made and information gained during mining at the analogous Westralia UG mining projects including Beresford and Allanson.</li> <li>Exploration results are not being reported.</li> </ul>
Further work	<ul style="list-style-type: none"> <li>The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).</li> <li>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</li> </ul>	<ul style="list-style-type: none"> <li>Infill drilling to increase Mineral Resource confidence, mine studies and metallurgical testwork are all planned.</li> </ul>

## McKenzie Well

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	<ul style="list-style-type: none"> <li>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</li> </ul>	<ul style="list-style-type: none"> <li>Ongoing database (DB) validation is undertaken by a dedicated DB administration geologist on an ongoing basis, who communicates with geologists to ensure the primary data sources and labs maintain high quality and remain within validation limits.</li> <li>Extensive validation has been and is undertaken by the database administrator. Data was loaded into DataShed with a back-end SQL Server DB via a relational data schema, providing a referentially integral database with primary key relations and look-up validation fields.</li> <li>Additional validation was completed in Surpac by Dacian geologists, with any validation issues relayed to DB administrator.</li> </ul>
	<ul style="list-style-type: none"> <li>Data validation procedures used.</li> </ul>	<ul style="list-style-type: none"> <li>All data were checked for the following errors: <ul style="list-style-type: none"> <li>Duplicate drillhole IDs</li> <li>Missing collar coordinates</li> <li>Mis-matched or missing FROM or TO fields in the interval tables (assays, logging etc.)</li> <li>FROM value greater than TO value in interval tables</li> <li>Non-contiguous sampling intervals</li> <li>Sampling interval overlap in the assay table</li> <li>The first sample in the interval file not starting at 0 m</li> <li>Interval tables with depths greater than the collar table EOH depth.</li> <li>Survey data were checked for large deviations in azimuth and dip between consecutive records, with none found.</li> </ul> </li> </ul>
Site visits	<ul style="list-style-type: none"> <li>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</li> <li>If no site visits have been undertaken indicate why this is the case.</li> </ul>	<ul style="list-style-type: none"> <li>The Competent Person has not visited the site of McKenzie Well, but has made several visits to the Mt Morgans area, including the same BIF stratigraphy that hosts the Westralia Area deposits. The Competent Person relied on colleagues for their knowledge and guidance in the preparation of the MRE, and has reviewed the drilling and sampling practices for the same drilling contractor as the RC drilling campaign that sampled the deposit for Dacian Gold.</li> <li>The Competent Person has not visited Bureau Veritas, the laboratory in Kalgoorlie, that undertook the assaying for Dacian samples.</li> </ul>
Geological interpretation	<ul style="list-style-type: none"> <li>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</li> </ul>	<ul style="list-style-type: none"> <li>The confidence in the geological model is moderately high. The BIF stratigraphy conforms well to the nominal mineralisation modelling cut-off of 0.3 g/t Au. Geological mapping of the BIF outcrops was used to guide the surface extension of the mineralisation wireframe interpretations. The mapping and wireframes broadly showed high correlation. Geological logging was informed by strong knowledge of the Westralia stratigraphy, in which the resources are located.</li> </ul>
	<ul style="list-style-type: none"> <li>Nature of the data used and of any assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>Detailed geological, alteration and structural logging in conjunction with chemical assays have</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>been used during the interpretation process to minimise assumptions and risk.</p> <ul style="list-style-type: none"> <li>The DGPS collar pick-ups in 2019 of the pegs of the 17 historic drillholes completed in 1988 ("MWRC1" through "MWRC19"), and which informed the Mineral Resource estimate, are assumed to be in the original positions of the collars without significant movement. Although it is possible that the pegs may have moved to a significant degree, these historic holes have been infilled to a high degree by the density of recent 2020 drilling by Dacian Gold (90 holes), meaning that the Mineral Resource estimate does not rely on any clusters of historic holes. Although no holes have been twinned, the mineralisation intercepts between the historic and recent drilling shows good visual correlation.</li> </ul>
	<ul style="list-style-type: none"> <li>The effect, if any, of alternative interpretations on Mineral Resource estimation.</li> </ul>	<ul style="list-style-type: none"> <li>A change in the mineralisation modelling cut-off used may yield different tonnages and grades. However, the Competent Person expects the variance in volumes to be low, while the estimate of global metal is likely to balance when compared to alternate estimates of tonnages and grade.</li> </ul>
	<ul style="list-style-type: none"> <li>The use of geology in guiding and controlling Mineral Resource estimation.</li> </ul>	<ul style="list-style-type: none"> <li>Geology, alteration, structure and chemistry have been used to guide the model. Wireframes have been constructed for the host BIF mineralisation as determined by the geological logging and chemical assays. The Mineral Resources are hosted within two banded iron formation limbs of an overturned, south plunging syncline with vergence to the SSE at the fold hinge, where several axial planar lodes have developed. The geological model of the banded iron formation (BIF) forms the basis of the mineralisation model, as the two showed high visual correlation. The wireframes of BIF encompass 10 lodes of mineralisation, lodes 1 through 5 lying on the western-most Viper Tooth limb, and lodes 6 through 10 lying on the eastern-most Welshgreen limb. The lodes were used to select and composite samples as hard-boundaries, determine statistics, and estimate grades by each individual lode by the corresponding composites within the lode.</li> <li>Following statistical analysis, two statistical domains representing the lodes of the two limbs were created to group mineralisation lenses together. Composites were selected within the mineralisation discretely. The block model was coded with the wireframes and the MRE was conducted by constraining composites and blocks to each relevant domain</li> <li>Investigation of the geological logging was undertaken for the presence porphyry dykes that commonly deplete the mineralisation in the Westralia deposits, but only insignificant intercepts were identified, and no geological continuity was established.</li> </ul>
	<ul style="list-style-type: none"> <li>The factors affecting continuity both of grade and geology.</li> </ul>	<ul style="list-style-type: none"> <li>The geology has a substantial impact on the grade and continuity. Spatial statistics were undertaken on the Viper Tooth and Welshgreen domains, resulting in variogram models with moderate nuggets and a single, short range structure in the major, along strike direction for 32 m and 40 m</li> </ul>

Criteria	JORC Code explanation	Commentary
		respectively. These ranges were approximately 1.5-times higher than the semi-major, down-dip direction, and up to 15-times higher than across the strike, which is across the bedding of the banded iron formation units.
Dimensions	<ul style="list-style-type: none"> <li>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</li> </ul>	<ul style="list-style-type: none"> <li>The lodes all outcrop at surface in part. The true thickness ranges from 2 m to 14 m, averaging approximately 4 m.</li> <li>The lodes of the Viper Tooth limb exhibit a strike length of approximately 550 m in a WSW direction, and extend 170 m NNE across strike, where lode 1 synformally folds under the Welshgreen limb. The depth from surface to the base of lode 1 is 150 m, although the nominal average depth of all Viper Tooth lodes is 45 m. Lodes formed in the axial plane as fold nose cleavage style mineralisation are shorter in length – these are coplanar with the Viper Tooth lodes, and therefore have been grouped with this domain.</li> <li>The Welshgreen domain lodes strike 335 m NW, exhibit a plan extent across strike of 65 m, and extend 65 m from surface, averaging approximately 40 m.</li> </ul>
Estimation and modelling techniques	<ul style="list-style-type: none"> <li>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</li> </ul>	<ul style="list-style-type: none"> <li>Samples were composited to 1 m intervals based on assessment of the raw drillhole sample intervals.</li> <li>The following high-grade top-cuts were applied to the mineralisation domains following statistical analysis completed in Snowden Supervisor™ software: <ul style="list-style-type: none"> <li>Viper Tooth domain: no top-cut.</li> <li>Welshgreen domain lodes: 7 g/t Au top-cap.</li> </ul> </li> <li>Quantitative kriging neighbourhood analysis (QKNA) was undertaken using Supervisor™ software to assess the effect of changing key kriging neighbourhood parameters on block grade estimates. Kriging efficiency (KE) and slope of regression (SOR) were determined for a range of block sizes, minimum and maximum samples, search dimensions and discretisation grids.</li> <li>Ordinary kriging was adopted to interpolate grades into cells for the mineralised domains.</li> <li>The block size appropriately reflects the inputs of the open-pit scenario, and the drillhole spacing, which varies from 20 m to 40 m sections along strike. Mineralisation pierce points are evenly spaced, varying from 20 m to 40 m in the Viper Tooth domain and 40 m to 80 m in the Welshgreen domain.</li> <li>The estimate employed a three-pass search strategy to improve the local grade estimate for well-informed blocks and to ensure all blocks received a grade estimate. The first pass was equal to the full range of the variogram model—32 m for the Viper Tooth domain lodes and 40 m for the Welshgreen domain lodes—honouring the anisotropic ratios orthogonally (approximately 1.5:1 major:semi-major and 14:1 major:minor for lodes of both domains). The second pass equated to 200% of the full range, and the third was set to 200 m. All blocks received an estimated grade, and therefore no assignment was necessary.</li> <li>Dynamic anisotropy was used for lode 1 of the Viper Tooth domain, as the wireframe folded</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>around in a synformal shape. A very minor number of samples were included in the folded wireframe, and as such did not influence the statistics. Therefore, dynamic anisotropy was used instead of splitting into separate domains.</p> <ul style="list-style-type: none"> <li>All geological modelling and grade estimation was undertaken using Surpac™ 2020 software.</li> </ul>
	<ul style="list-style-type: none"> <li>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</li> </ul>	<ul style="list-style-type: none"> <li>Unpublished, internal estimates undertaken by a previous DCN geologist in alternate software yielded comparable results.</li> </ul>
	<ul style="list-style-type: none"> <li>The assumptions made regarding recovery of by-products.</li> </ul>	<ul style="list-style-type: none"> <li>No assumptions have been made regarding recovery of by-products.</li> </ul>
	<ul style="list-style-type: none"> <li>Estimation of deleterious elements or other non-grade variables of economic significance (e.g. Sulphur for acid mine drainage characterisation).</li> </ul>	<ul style="list-style-type: none"> <li>No deleterious or other non-grade variables have been estimated.</li> </ul>
	<ul style="list-style-type: none"> <li>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</li> </ul>	<ul style="list-style-type: none"> <li>Drilling chiefly lies on 40 m by 40 m grid angled obliquely to the SSW to intersect the strike of the stratigraphy and mineralisation at a high-angle. The grid was infilled to 20 m by 20 m on 5 sections. Kriging neighbourhood analysis statistics showed with is nominally 40 m by 20m in the Y direction</li> </ul>
	<ul style="list-style-type: none"> <li>Any assumptions behind modelling of selective mining units.</li> </ul>	<ul style="list-style-type: none"> <li>No assumptions have been made regarding SMUs.</li> </ul>
	<ul style="list-style-type: none"> <li>Any assumptions about correlation between variables.</li> </ul>	<ul style="list-style-type: none"> <li>No assumptions have been made about correlation between variables.</li> </ul>
	<ul style="list-style-type: none"> <li>Description of how the geological interpretation was used to control the resource estimates.</li> </ul>	<ul style="list-style-type: none"> <li>The mineralisation lodes, representing the banded iron formation</li> </ul>
	<ul style="list-style-type: none"> <li>Discussion of basis for using or not using grade cutting or capping.</li> </ul>	<ul style="list-style-type: none"> <li>Top-cuts (or caps) were reviewed by statistical domain. The Viper Tooth lodes were not cut, as their maxima (approximately 7 g/t) did not display outliers beyond the classically log-normal distributions, and the CV was below 1.0. The Welshgreen lodes were top-capped at 7 g/t.</li> </ul>
	<ul style="list-style-type: none"> <li>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</li> </ul>	<ul style="list-style-type: none"> <li>Standard model validation has been completed using numerical methods (histogram and swath plots) and validated visually against the input raw drillhole data, composites and blocks.</li> </ul>
Moisture	<ul style="list-style-type: none"> <li>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</li> </ul>	<ul style="list-style-type: none"> <li>The tonnages are estimated on a dry basis. The densities taken from other deposits of the Westralia area were adjusted to remove moisture content, and were taken from mining reconciliation.</li> </ul>
Cut-off parameters	<ul style="list-style-type: none"> <li>The basis of the adopted cut-off grade(s) or quality parameters applied.</li> </ul>	<ul style="list-style-type: none"> <li>The Mineral Resources have been reported above a lower cut-off of 0.5 g/t Au, which is the cut-off used by Dacian Gold for low-grade stockpiles in active mining, and also an industry standard in the Competent Person's experience.</li> </ul>
Mining factors or assumptions	<ul style="list-style-type: none"> <li>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>The Mineral Resources are assumed to be amenable to open pit mining methods based on numerous other similar deposits in the Mt Morgans successfully mined by Dacian Gold and previous operators. The Mineral Resources lie approximately 9.6 km from the historic Westralia pit and approximately 23.7 km and 29 km respectively as the crow flies and via potential haul route to the Jupiter mill. It is assumed that these distances will not cause any issues with haulage that would prevent the Mineral Resources from achieving reasonable prospects for eventual economic extraction.</li> </ul>

Criteria	JORC Code explanation	Commentary
Metallurgical factors or assumptions	<ul style="list-style-type: none"> <li>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>The Mt Morgans mine site is an active mining operation that has established high recoveries for BIF-hosted mineralisation recently mined by Dacian Gold within the same Westralia stratigraphy as that modelled for the McKenzie Well Mineral Resources. Therefore, any material mined and processed from the deposit is assumed to conform to results of processing of Westralia mineralisation.</li> </ul>
Environmental factors or assumptions	<ul style="list-style-type: none"> <li>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>The Mt Morgans mine site is an active mining operation with waste and residue disposal in place. The Mineral Resource model includes the same Westralia stratigraphy as that recently mined by Dacian Gold, and therefore any material mined and processed from the deposit is assumed to conform to the same material and methods that gained environmental approval in recent mining.</li> </ul>
Bulk density	<ul style="list-style-type: none"> <li>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</li> </ul>	<ul style="list-style-type: none"> <li>The bulk density has been assumed, as no density data were available for the McKenzie Well drilling. The densities chosen were selected from information on other Westralia deposits. The densities for these deposits have been determined by immersion method.</li> </ul>
	<ul style="list-style-type: none"> <li>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.</li> </ul>	<ul style="list-style-type: none"> <li>The immersion method used for the density values taken from other Westralia deposits has adequately accounted for void spaces. Moisture has not been considered in the original density, and therefore a conservative density assignment has been used. The densities of various rock types have not been considered in the assignment. The Competent Person has reflected the risk of density to the MRE in the classification.</li> </ul>
	<ul style="list-style-type: none"> <li>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</li> </ul>	<ul style="list-style-type: none"> <li>The bulk density is assumed to be influenced by the host rock and not the gold content. No other chemical analyses are available to determine the relationship to density, e.g. sulphide content.</li> </ul>
Classification	<ul style="list-style-type: none"> <li>The basis for the classification of the Mineral Resources into varying confidence categories.</li> <li>Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</li> <li>Whether the result appropriately reflects the Competent Person's view of the deposit.</li> </ul>	<ul style="list-style-type: none"> <li>The Mineral Resources have been classified as entirely Inferred within the mineralisation volumes. Although the Competent Person deems that a reasonable confidence has been established in the geological model, the quality of the samples is deemed to be high, and a moderate confidence lies in the grade estimate, the confidence in the quality control and density data is low.</li> </ul>
Audits or reviews	<ul style="list-style-type: none"> <li>The results of any audits or reviews of Mineral Resource estimates.</li> </ul>	<ul style="list-style-type: none"> <li>The Mineral Resource estimate has been the subject of Dacian Gold's internal peer review process prior to public release.</li> </ul>
Discussion of relative accuracy/ confidence	<ul style="list-style-type: none"> <li>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application</li> </ul>	<ul style="list-style-type: none"> <li>The Mineral Resource accuracy is communicated through the classification of Inferred assigned to the deposit. The MRE has been classified in accordance with the JORC Code using a qualitative approach. All factors that have been</li> </ul>



Criteria	JORC Code explanation	Commentary
	<p>of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</p> <ul style="list-style-type: none"> <li>• The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</li> <li>• These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</li> </ul>	<p>considered have been adequately communicated in Section 1 and Section 3 of this Table.</p>

## Redcliffe Gold Project – Table 1 (JORC Code, 2012)

Includes the deposits of Hub, Kelly, Mesa\West Lode, Redcliffe, Bindy and Nambi

### SECTION 1 SAMPLING TECHNIQUES AND DATA

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
<b>Sampling techniques</b>	<i>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i>	<ul style="list-style-type: none"> <li>The Hub MRE is based on sampling carried out using Reverse Circulation drilling (RC) and Diamond Drilling (DD). A total of 148 drillholes for a total of 22,769 m at depths ranging from 30 to 435 m. This includes 113 RC (14,341 m), 20 DD (3,911 m) and 15 DD with RC pre-collar (4,547 m). Holes included in the Hub MRE were drilled from 2018 to 2021, initially by NTM Gold Limited (NTM) and subsequently by Dacian Gold Limited (DCN).</li> <li>The Kelly MRE is based on 108 RC holes for 13,061 m with hole depths ranging from 66 m to 283 m. The holes were drilled by Pacrim Energy Ltd (Pacrim) from 2010 – 2012, Redcliffe Resources Ltd (Redcliffe) from 2012 – 2015 and NTM in 2016.</li> <li>The Mesa\West Lode MRE was based on 139 RC holes for a total of 9,800 m. The majority of the holes were drilled by Austwhim Resources (Austwhim) from 1987 to 1987. A small number of holes were drilled by Newmont Corporation (Newmont), but dates are unknown. One hole was drilled by NTM in 2020.</li> <li>The Redcliffe MRE is based on 66 holes for a total of 4,596 m. Nine holes were drilled by Newmont (date unknown), Austwhim drilled 37 holes in 1987 and Pacrim 20 holes in 2007.</li> <li>The Bindy MRE is based on 46 holes for a total of 8988.1 m. Within this there was one RC pre-collared DD hole with 1551.4 m of DD drilling. All holes were drilled by NTM, 41 were drilled in 2017, with the remainder drilled in 2018, 2019 and 2020.</li> <li>The Nambi MRE is based on 138 holes; 123 RC, 7 RC pre-collar DD holes and 8 DD holes for a total of 22,979 m. Of these holes, 65 were drilled by CRA (date unknown), 7 by Aurora Gold (date unknown), 36 by Pacrim (2007) and 30 by NTM (2016 – 2020).</li> <li>The GTS MRE is based on 182 holes; 169 RC, 4 RC pre-collar DD holes and 9 DD holes for a total of 22,663 m. Of these 141 holes were drilled by Pacrim (2007 to 2010), 40 by NTM (2016 – 2021) and 1 unknown.</li> </ul>
	<i>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</i>	<ul style="list-style-type: none"> <li>For the later operators (NTM/DCN) procedures were carried out under Company protocols which are aligned with current industry practice.</li> <li>Sampling protocols for the historical operators (Newmont, Pacrim, CRA, Aurora Gold and Austwhim) are unknown.</li> </ul>
	<i>Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</i>	<ul style="list-style-type: none"> <li>For the historical operators, no information is available</li> <li>RC holes drilled by NTM/DCN were drilled with a 5.25 inch face-sampling bit, 1 m samples collected through a cyclone and cone splitter, to form a 2 – 3 kg single metre sample and a bulk 25 – 40 kg reject sample.</li> <li>DD samples were collected from NQ, NQ2, NQ3, HQ and PQ3 diamond core. Core was measured, oriented (where possible), photographed and then cut in half. Samples of ½ core were selected based on geological observations and were between 0.2 m and 2 m in length.</li> <li>The NTM\DCN samples (post-2016) were dispatched to were dispatched to Bureau Veritas (BV) in Perth or Kalgoorlie, SGS Kalgoorlie or ALS in Kalgoorlie. These samples were sorted and dried by the assay laboratory, pulverised to form a 40g (BV) or 50g (ALS) charge for Fire Assay/AAS.</li> </ul>
<b>Drilling techniques</b>	<i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard</i>	<ul style="list-style-type: none"> <li>NTM/DCN RC drilling was completed by Ausdrill, Challenge Drilling and PXD Pty Ltd. A 5.25 or 5.5 inch bit was used.</li> <li>There is no definitive data available on the drilling contractor and</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i>	<p>hole size used for RC drilling by the historical operators.</p> <ul style="list-style-type: none"> <li>NTM/DCN DD drilling was conducted by WDD with a DR800 truck mounted rig and Terra Drilling using Hanjhin 7000 track mounted rig. Core sizes included NQ, NQ2, NQ3, HQ and PQ3. All core was oriented using a downhole orientation tool. Some holes were pre-collared by RC.</li> <li>There was no DD drilling carried out by the historical operators.</li> </ul>
<b>Drill sample recovery</b>	<i>Method of recording and assessing core and chip sample recoveries and results assessed.</i>	<ul style="list-style-type: none"> <li>For the historical operators there is no data indicating if recoveries were assessed.</li> <li>For NTM/DCN RC drilling the majority of samples were dry, some wet samples were experienced at depth. This was recorded in the database.</li> <li>RC recoveries and quality were visually estimated, and any low recoveries recorded in the database.</li> <li>All core was measured, with recovery calculated against the drill run, which is recorded in the database. Core recovery within the total transition and fresh material was high, with most runs recovering 100%. Only two DD holes intersect the mineralisation in the oxide profile and the recovery is variable, with average of 67%. All other mineralisation intersections with the oxide are by RC.</li> </ul>
	<i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i>	<ul style="list-style-type: none"> <li>No data is available on the historical operators.</li> <li>RC face-sample bits, PVC casing in the top 6 m and dust suppression were used to minimise sample loss. RC samples are collected through a cyclone and cone splitter, with the bulk of the sample deposited in a plastic bag and a sub sample up to 3 kg collected in a calico bag and placed within the green bag. Cyclone and cone splitter are cleaned between rods and at EOH to minimise contamination.</li> <li>Ground water egress into the holes resulted in some damp to wet samples at depth, which have been noted in the database. Sample quality was noted on drill logs, and drilling of the hole was terminated when sample quality was compromised at depth.</li> <li>DD core was sampled on a 0.2 m to 2 m basis, generally to geological contacts, and collected as ½ core, with the sampling side kept consistent.</li> </ul>
	<i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i>	<ul style="list-style-type: none"> <li>For NTM/DCN drilling no relationship between recovery and grade was noted, no biases were observed, and sample recovery is overall consistently good.</li> </ul>
<b>Logging</b>	<i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i>	<ul style="list-style-type: none"> <li>Over 98% of the RC chips were geologically logged using the various companies standard logging codes.</li> <li>All DD core was geologically and structurally logged.</li> </ul>
	<i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i>	<ul style="list-style-type: none"> <li>Logging of NTM/DCN RC chips recorded lithology, mineralogy, mineralisation, weathering, colour and other features of the samples.</li> <li>All samples from NTM/DCN drilling were wet-sieved and stored in chip trays. These trays were stored off site for future reference. The procedure for historical operators is not known.</li> <li>Logging of DD core recorded lithology, mineralogy, mineralisation, weathering, colour, recovery, structures and RQD. Structural measurements were taken using a kenometer to record alpha and beta angles relative to a bottom of hole line marked on the oriented core. The quality of the bottom of hole orientation line is also recorded.</li> <li>These trays were photographed and then stored off site for future reference.</li> </ul>
	<i>The total length and percentage of the relevant intersections logged.</i>	<ul style="list-style-type: none"> <li>All holes were logged in full.</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Sub-sampling techniques and sample preparation</b>	<i>If core, whether cut or sawn and whether quarter, half or all core taken.</i>	<ul style="list-style-type: none"> <li>DD core was sawn using a diamond blades and ½ core collected for assay on a 0.2 m to ~2 m basis, generally to geological contacts. Assay samples were collected from the same side of the core.</li> </ul>
	<i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i>	<ul style="list-style-type: none"> <li>For NTM/DCN RC drilling 1 m drill samples are passed through a cone splitter installed directly below a rig mounted cyclone. A 2 – 3 kg sub-sample is collected in a calico bag (primary sample) and the balance in a plastic bag. The calico bag is placed within the corresponding plastic bag for later collection if required. A 5 m composite sample is made by spearing the reject sample in the plastic bag. If the 5 m composite returns &gt; 0.1 g/t Au, the 1 m sample is then submitted for assay.</li> <li>For the 2020/2021 RC drilling program at Hub and Bindy, as the mineralisation locations were well known, 1 m samples were collected and submitted instead of collecting a 5 m composite for zones 10 – 15 m above the mineralisation and generally through to the end of hole.</li> <li>There is limited information available on the historical operators, but it appears that either 5 m or 1 m samples were taken.</li> </ul>
	<i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i>	<ul style="list-style-type: none"> <li>Samples from NTM/DCN drilling were prepared at BV in Perth or Kalgoorlie, or ALS Kalgoorlie or SGS Kalgoorlie – depending on the year. The sample preparation and analysis methodology was very similar across all laboratories. Samples were dried, and the entire sample pulverised to 90% passing 75 µm, and a reference sub-sample of approximately 200 g retained. A nominal 40 g or 50 g was used for the analysis (FA/AAS). The procedure is industry standard for this type of sample.</li> <li>There is no information available on the historical operator's sample preparation and analytical techniques.</li> </ul>
	<i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i>	<ul style="list-style-type: none"> <li>NTM/DCN inserted Certified Reference Materials (CRM's), blanks and duplicates within each batch of samples. Selected samples are also re-analysed to confirm anomalous results.</li> <li>Some QAQC was conducted by the historical operators but the confidence is lower.</li> </ul>
	<i>Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.</i>	<ul style="list-style-type: none"> <li>For NTM/DCN RC drilling 1 m samples are split on the rig using a cone splitter, mounted directly under the cyclone. Three samples per hundred were collected off the secondary port as field duplicates. An analysis of these results indicate mixed results, depending upon the laboratory. The Kalgoorlie based laboratories performed better than the Perth based laboratories. It is unknown if this is laboratory related or inherent nature of the gold mineralisation.</li> <li>For NTM/DCN DD drilling, sampling of the remaining half core was not undertaken.</li> </ul>
	<i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i>	<ul style="list-style-type: none"> <li>NTM/DCN sample sizes are considered appropriate to give an indication of mineralisation given the particle sizes and the practical requirement to maintain manageable sample weights.</li> </ul>
<b>Quality of assay data and laboratory tests</b>	<i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i>	<ul style="list-style-type: none"> <li>NTM/DCN samples were analysed for Au via a 40 g or 50 g fire assay / AAS finish which gives total digestion and is appropriate for high-grade samples.</li> <li>The analytical technique used by the historical operators is unknown.</li> </ul>
	<i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i>	<ul style="list-style-type: none"> <li>No geophysical tools have been used.</li> </ul>
	<i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i>	<ul style="list-style-type: none"> <li>NTM/DCN company QA/QC protocols for 1 m RC sampling is as follows:</li> <li>Three field duplicates per 100 samples</li> <li>Four Certified Reference Material (CRMs) samples inserted per 100 samples.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Three coarse blanks submitted per 100 samples.</li> <li>NTM/DCN company QA/QC protocols for 5 m RC sampling is as follows:</li> <li>Four Certified Reference Material (CRMs) and blank samples inserted per 100 samples.</li> <li>No field duplicates were used.</li> <li>NTM/DCN company QA/QC protocols for DD sampling is as follows:</li> <li>No half core duplicates were submitted.</li> <li>Six CRMs inserted per 100 samples.</li> <li>Four blanks per 100 samples.</li> <li>If an analysis of the returned QA/QC samples noted discrepancies, the batch was re-assayed or resampled.</li> <li>Some QA/QC data pre-2016 (pre-NTM/DCN) does exist, but there is a limited number and it is of limited value as the background information is not available.</li> <li>An analysis of QA/QC data for the main laboratories used (ALS-Perth, Bureau Veritas-Perth and Bureau Veritas-Kalgoorlie) indicates that:</li> <li>The insertion rate of CRMs was around 5%, which is within acceptable limits.</li> <li>The performance of the CRMs is considerate moderate.</li> <li>The performance of the blanks submitted to all the laboratories was within acceptable limits.</li> <li>Pacrim conducted pulp repeats, which when analysed returned an acceptable result. No pulp repeats were submitted by NTM/DCN.</li> <li>NTM/DCN submitted around 100 umpire pulp duplicates, using two different pairs of laboratories. The performance of one pair was not deemed acceptable.</li> <li>The 2007 – 2021 data did not contain any coarse reject duplicates.</li> <li>The overall performance of the QA/QC data is below what is considered an acceptable level, however the resource category assigned (Inferred and Indicated) to the deposits takes into account the performance of the laboratories.</li> </ul>
<b>Verification of sampling and assaying</b>	<i>The verification of significant intersections by either independent or alternative company personnel.</i>	<ul style="list-style-type: none"> <li>Significant intersections from the NTM/DCN drilling were visually field verified by either the Senior Exploration Geologists, or NTM's Exploration Manager and Managing Director. The Competent Person also has visually reviewed significant intersections in several holes and verified their database records.</li> </ul>
	<i>The use of twinned holes.</i>	<ul style="list-style-type: none"> <li>No twinning of holes has been identified in the drillhole data.</li> </ul>
	<i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i>	<ul style="list-style-type: none"> <li>For NTM/DCN drilling, all field logging was carried out via the LogChief software on a SurfacePro tablet. Logchief has internal data validation. Assay files are received electronically from the laboratory. All the data is imported into DataShed drillhole database which is managed by MaxGeo. All data is stored in a Company database system and maintained by the Database Manager (MaxGeo).</li> <li>Historical data in the database was inherited from previous operators of the various tenements and there are no records of how validation was carried out.</li> </ul>
	<i>Discuss any adjustment to assay data.</i>	<ul style="list-style-type: none"> <li>Assay values that were below detection limit are stored in the database in this form, but are adjusted to equal half of the detection limit value when exported for reporting.</li> </ul>
<b>Location of data points</b>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>For NTM/DCN drilling, all drillhole collar locations (except 20RDD002) are determined by DGPS and hence within 5 cm accuracy.</li> <li>A full breakdown of the method used to determine collar locations from all drilling is as follows:</li> </ul>

Criteria	JORC Code explanation	Commentary																																												
		<table><tr><th rowspan="2">Deposit</th><th colspan="4">Collar pickup method</th></tr><tr><th>Unknown</th><th>GPS</th><th>DGPS</th><th>CT*</th></tr><tr><td>Hub</td><td>-</td><td>1</td><td>147</td><td>-</td></tr><tr><td>Kelly</td><td>5</td><td>17</td><td>86</td><td>-</td></tr><tr><td>Mesa/West Lode</td><td>110</td><td>-</td><td>29</td><td>-</td></tr><tr><td>Redcliffe</td><td>46</td><td>-</td><td>20</td><td>-</td></tr><tr><td>Bindy</td><td>-</td><td>1</td><td>45</td><td>-</td></tr><tr><td>Nambi</td><td>72</td><td>1</td><td>64</td><td>1</td></tr><tr><td>GTS</td><td>10</td><td>7</td><td>159</td><td>6</td></tr></table> <ul style="list-style-type: none"><li>*assumed to be ‘closed traverse’</li><li>For NTM/DCN drilling the drill rig mast was set up using a clinometer and rig is orientated using handheld compass. Downhole surveys were conducted by a downhole gyro and measurements taken at varying intervals of approximately every 5 m to 50 m.</li><li>For the historical operators there is a mixture of downhole surveys (method unknown) and azimuth readings at the collar only.</li><li>Some historic collar RL positions were adjusted to reflect more recent and more accurate pickups by DGPS.</li></ul>	Deposit	Collar pickup method				Unknown	GPS	DGPS	CT*	Hub	-	1	147	-	Kelly	5	17	86	-	Mesa/West Lode	110	-	29	-	Redcliffe	46	-	20	-	Bindy	-	1	45	-	Nambi	72	1	64	1	GTS	10	7	159	6
Deposit	Collar pickup method																																													
	Unknown	GPS	DGPS	CT*																																										
Hub	-	1	147	-																																										
Kelly	5	17	86	-																																										
Mesa/West Lode	110	-	29	-																																										
Redcliffe	46	-	20	-																																										
Bindy	-	1	45	-																																										
Nambi	72	1	64	1																																										
GTS	10	7	159	6																																										
	Specification of the grid system used.	<ul style="list-style-type: none"><li>Grid projection is GDA94, Zone 51.</li></ul>																																												
	Quality and adequacy of topographic control.	<ul style="list-style-type: none"><li>A DTM has been created for the Redcliffe Gold Project based on all available DGPS data, with an accuracy of 5 cm. Relative Levels have been assigned based on this DTM.</li></ul>																																												
Data spacing and distribution	Data spacing for reporting of Exploration Results.	<ul style="list-style-type: none"><li>For Hub the drill spacing is on an approximate 25 m grid which extends to 50 m in some areas.</li><li>For Kelly the drill sections are aligned at approximately 100 m along strike and 20 m across strike.</li><li>Mesa/West Lode drilling is mainly spaced 25 m along strike, with some areas up to 50 m. Drill spacing across strike is generally at 20 m.</li><li>Redcliffe drilling sections along strike are spaced at 20 – 40 m, while across strike is 10 – 20 m.</li><li>Bindy drilling is spaced mostly at 20 m along strike with some 40 m spaced sections. Drilling across strike is generally at a 20 m spacing.</li><li>Nambi drilling is spaced at 25 m along strike and 10 – 20 across strike.</li><li>For GTS, holes are generally spaced on 20 m northerly sections, with some sections spaced on 10 m sections. Across section holes are spaced at 10 m, 20 m and 40 m.</li></ul>																																												
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	<ul style="list-style-type: none"><li>The resource classification applied to each of the individual deposits reflects the level of confidence reached when taking into account drillhole spacing, confidence in geological interpretation, QA/QC and the amount of historical drilling.</li></ul>																																												
	Whether sample compositing has been applied.	<ul style="list-style-type: none"><li>The Mineral Resource estimation was conducted using 1 m composites. As the RC drilling was all 1 m no compositing effectively took place. For DD drilling some composites were used if sample intervals were less than 1 m.</li></ul>																																												
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	<ul style="list-style-type: none"><li>The vast majority the drilling is orientated perpendicular to the strike of the individual deposits. Also, the majority of the drilling intersects the mineralisation at high angles resulting in close to true widths being generated.</li></ul>																																												
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	<ul style="list-style-type: none"><li>The drill hole azimuths and dips are generally perpendicular to the mineralisation and hence should not introduce any sampling bias.</li></ul>																																												
Sample security	The measures taken to ensure sample security.	<ul style="list-style-type: none"><li>The chain of custody for NTM/DCN was managed by NTM/DCN. Samples are stored on-site until collected for transport to the respective laboratories. NTM/DCN personnel have no contact with the samples once they leave site. Tracking sheets are used to record the progress of the samples.</li></ul>																																												



Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>The chain of custody for the historical drilling is unknown.</li> </ul>
<b>Audits or reviews</b>	<i>The results of any audits or reviews of sampling techniques and data.</i>	<ul style="list-style-type: none"> <li>Sampling and assaying techniques are considered industry standard. Batch assay data is routinely reviewed to ascertain laboratory performance. The laboratory is advised of any discrepancies and samples are re-assayed.</li> <li>Bureau Veritas was audited in April 2021 by the company Principal Resource Geologist.</li> </ul>

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
<b>Mineral tenement and land tenure status</b>	<i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i>	<ul style="list-style-type: none"> <li>The RC &amp; DD drilling occurred within tenement E37/1205 which is held 100% by NTM GOLD Ltd. The Project is located 55km NE of Leonora in the Eastern Goldfields of Western Australia.</li> </ul>
	<i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</i>	<ul style="list-style-type: none"> <li>The tenement subject to this report is in good standing with the Western Australian DMIRS.</li> </ul>
<b>Exploration done by other parties</b>	<i>Acknowledgment and appraisal of exploration by other parties.</i>	<ul style="list-style-type: none"> <li>Previous exploration at the Project has been completed by Ashton, Dominion Mining, Sons of Gwalia and CRAE in the 1990's. Mining of the Nambi and Nambi South pits was undertaken by Ashton. Pacrim Energy Ltd/Redcliffe Resources Ltd completed exploration in the area from in 2007-2016. Where relevant, assay data from this earlier exploration has been incorporated into NTM database.</li> </ul>
<b>Geology</b>	<i>Deposit type, geological setting and style of mineralisation.</i>	<ul style="list-style-type: none"> <li>Mineralisation at the Redcliffe Gold Project is hosted largely within Archaean-aged mafic schist and volcano- sediment package (including chert, black shale, graphitic in part) and intermediate-mafic rocks. A mylonitic fabric is observable in the lithologies. Gold mineralisation generally occurs in northerly striking, sub-vertical to steep dipping zones associated with silica-sulphide-mica alteration and veining. The exception to this is Kelly, where the mineralisation dips approximately 45° to the east and West Lode, which dips at approximately 60° to the west.</li> <li>At Hub, the majority of the mineralisation is hosted in a narrow (~ 4 m wide) vertical to steep west dipping lode. Several minor subsidiary hanging and footwall lodes are present. The main lode has been cut by late dolerite and lamprophyre dykes which offset and disrupt the mineralisation in places. The depth of complete oxidation varies from between 50 and 100 m below surface which is underlain by a transitional horizon typically 25 m thick to the top of fresh horizon. A thin laterite cap covers the deposit.</li> <li>The mineralisation at Kelly is hosted in 4-5 shallow east dipping lodes which can be up to 20 m true thickness. There are through broad groups of domains along strike that are separated by zones of no mineralisation or areas of poor drill coverage and hence the mineralisation interpretation has not been extended through these zones. The depth to the base of complete oxidation varies from around 50 – 80 m which continues into 30 – 50 m transitional horizon. The majority of the mineralisation is hosted within the oxidised and transitional horizons.</li> <li>The Mesa and West Lode mineralisation is hosted in separate narrow northwest trending lodes (Mesa is located to the southwest and West Lode to the northeast). The Mesa lodes consist of three separate lodes that are subvertical and are 3 – 5 m in width. The West lodes consist of multiple flat lying west dipping lodes dipping to the west. True widths vary from 2 m to up to 10 m. The base of complete oxidation lies around 50 m below the surface and is underlain by a 15 – 20 m thick transitional zone.</li> <li>The Redcliffe deposit consists of a single northwest trending sub-vertical zone that is around 20 m in true width. The base of complete oxidation lies around 50 m below the surface, with the base of transitional lying approximately a further 10 m below.</li> <li>The Bindy mineralisation is hosted in a series of narrow to wide (up to 20 m) steep east dipping north trending lodes, with one main lode and several subsidiary footwall and hanging wall lodes. A thin laterite cover (~5 m) overlies the deposit. The complete base of oxidation lies around 70 m below the surface, underlain by a 10 – 30 m transitional zone.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>The Nambi deposit consists of five steeply west dipping north trending sub-parallel lodes, with the more extensive lode as the footwall lode. Lode widths are generally around 2 – 3 m. This deposit has a shallow oxidation profile compared to the other deposits, with the base of complete oxidation around the lodes being about 10 m below the surface. The base of transition is around 30 m below the surface.</li> <li>GTS is approximately 700 m long north trending vertical dipping deposit. The width varies from 60 m in the south to 10 m in the northern sections. Within the wider parts of the deposit it appears that the mineralisation is flat dipping within the broader steep dipping mineralisation envelope. There is a laterite blanket ( around 5 m thick) covering the deposit. The mineralisation does not extend into the laterite. The base of complete oxidation is around 50 m – 60 m below the surface and the top of fresh is around a further 20 m below.</li> </ul>
<b>Drill hole Information</b>	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length.	<ul style="list-style-type: none"> <li>Exploration results are not being reported. All drillhole details are included in previous announcements.</li> </ul>
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	<ul style="list-style-type: none"> <li>Exploration results are not being reported.</li> </ul>
<b>Data aggregation methods</b>	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.	<ul style="list-style-type: none"> <li>Grades are reported as down-hole length-weighted averages of grades. No top cuts have been applied to the reporting of the assay results.</li> </ul>
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	<ul style="list-style-type: none"> <li>All higher-grade intervals are included in the reported grade intervals.</li> </ul>
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	<ul style="list-style-type: none"> <li>No metal equivalent values are used.</li> </ul>
<b>Relationship between mineralisation widths and intercept lengths</b>	These relationships are particularly important in the reporting of Exploration Results.	<ul style="list-style-type: none"> <li>The geometry of the mineralisation at depth is interpreted to vary from steeply west dipping to sub-vertical. (80° to 90°). All assay results are based on down-hole lengths, and true width of mineralisation is not known.</li> </ul>
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	
<b>Diagrams</b>	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	<ul style="list-style-type: none"> <li>Refer to Figure in the body of text.</li> </ul>
<b>Balanced reporting</b>	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	<ul style="list-style-type: none"> <li>Exploration results are not being reported</li> </ul>

Criteria	JORC Code explanation	Commentary
<b>Other substantive exploration data</b>	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	<ul style="list-style-type: none"> <li>No other exploration data has been identified.</li> </ul>
<b>Further work</b>	The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).	<ul style="list-style-type: none"> <li>Infill drilling, mining studies testwork is planned to increase the understanding of the Hub deposit.</li> </ul>
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	<ul style="list-style-type: none"> <li>Refer to diagrams in the body of the text.</li> </ul>

## Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
<b>Database integrity</b>	<i>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. Data validation procedures used.</i>	<ul style="list-style-type: none"> <li>The database is hosted by and has been systematically audited by Maxgeo data consultants, who communicated with geologists to ensure the primary data sources and labs maintain high quality and remain within validation limits.</li> <li>Extensive validation has been and is undertaken by the database administrator. Data was loaded into DataShed with a back-end SQL Server DB via a relational data schema, providing a referentially integral database with primary key relations and look-up validation fields. Additional validation was completed in Surpac by Dacian geologists, with any validation issues relayed to DB administrator.</li> <li>The Redcliffe Gold Project drillhole database was provided as an export of the highest priority data available to an Access database prior to the Mineral Resource estimate (MRE). The Redcliffe Gold Project drillhole database is managed by Maxgeo who provided an export of the complete data set as an Access database prior to mineral resource estimation.</li> </ul>
	<i>Data validation procedures used.</i>	<ul style="list-style-type: none"> <li>The database was checked for collar discrepancies (Elevations, grid co-ordinates), survey discrepancies (azimuth/dip variations), assay discrepancies (duplicate values, from and to depth errors, missing samples, unsampled intervals).</li> <li>A 3D review of collars and hole surveys was completed in Surpac to ensure that there were no errors in collar placement or dip and azimuths of drill holes. Some collar elevation errors were noted and these were corrected.</li> </ul>
<b>Site visits</b>	<i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is the case.</i>	<ul style="list-style-type: none"> <li>The Competent Person visited the deposit site in June 2021.</li> <li>The visit confirmed that the topography resembled the DTM surface used in the MRE, no known historic depletion existed that had not been accounted for, and that no physical impediments were noted for the reasonable prospects of eventual economic extraction.</li> <li>The drill site inspections included checks of the database records and diamond core against collar locations, drilling angles and dips, hole depths by peg notes and RC sample bags where available, and geological logging against sample bags and diamond core.</li> <li>The diamond core sampling and storage facilities were in good condition, and core inspected correlated with the geological logging and mineralised intervals in the database and which were used to inform the MRE. Discussions during the site visit and during the preparation of the MRE with the site geologists confirmed that they held a good understanding of the geology, the mineralisation controls on the MRE, and that their adherence to the procedures reviewed ensured good sample quality.</li> <li>The site visit indicated that there were no matters presented that would prevent reporting the MRE in accordance with the JORC Code.</li> </ul>
<b>Geological interpretation</b>	<i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i>	<ul style="list-style-type: none"> <li>The confidence in the geological interpretation is based on the drill spacing and the geometry of the mineralisation. The deposits of Hub, Redcliffe, Bindy, Nambi and GTS have a high confidence, while Kelly and Mesa\West Lode have a moderate confidence.</li> <li>Wireframe interpretations have been created for weathering surfaces including, base of laterite, base of complete oxidation and top of fresh rock and mineralised domains. For Hub, wireframe interpretations have also been created to represent the known extent of both dolerite and lamprophyre dykes which brecciate and stoep out the mineralised zones.</li> <li>Wireframes were interpreted using cross sections that were spaced according to the drill spacing. Generally, the sections were east-west oriented or slightly oblique to east-west. Section spacing is generally 25 m to 50 m. DD and RC drilling have been used primarily for wireframe interpretation. AC and RAB drilling were only used to provide guidance for the interpretation process but have been excluded from grade estimations.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<i>Nature of the data used and of any assumptions made.</i>	<ul style="list-style-type: none"> <li>Data is sourced from the drill logging and recent RC chip logging/ DD core logging.</li> <li>The logging has been used to interpret lithology units, major structural features, and mineralisation trends.</li> <li>Weathering surfaces were interpreted for laterite (if present), oxide, transitional and primary weathering boundaries from available logging data. This data allowed the density values for the mineral resource estimate to be sub-divided by weathering domains.</li> </ul>
	<i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>For Hub, mineralisation domains were created using a lower cut-off of around 0.45 g/t Au.</li> <li>For deposits including GTS, Kelly, Mesa\Westlode, Nambi and Redcliffe, mineralisation domains were created using a lower cut-off of around 0.30 g/t Au.</li> <li>In some cases, lower grades were included to produce geological continuity. Minimum downhole intersections were limited to 2 m. Recent drilling has confirmed the historical mineralisation interpretation with generally only minor modifications required for the updated interpretation.</li> </ul>
	<i>The use of geology in guiding and controlling Mineral Resource estimation.</i>	<ul style="list-style-type: none"> <li>The weathering profile for all deposits has been modelled to include laterite, oxide, transitional and fresh material. Laterite is not present at all deposits but where it has been included, the mineralisation interpretation does not extend into the laterite profile.</li> <li>A statistical review of mineralised sample data by oxidation state (oxide, transitional and fresh) determined that there was no notable difference in grade distribution and the combination of sample composites across weathering boundaries for statistics and grade estimation was justified.</li> <li>At the Hub deposit, the mineralisation interpretation does not extend into the interpreted dolerite and lamprophyre dykes which are observed to brecciate and stope out the mineralised zones.</li> </ul>
	<i>The factors affecting continuity both of grade and geology.</i>	<ul style="list-style-type: none"> <li>The domain interpretations have been modelled to a nominal grade cut-off of approximately 0.45 g/t Au cut-off at Hub and 0.30 g/t Au cut-off at GTS, Bindy, Kelly, Mesa\Westlode, Nambi and Redcliffe. These cut-off's are supported by weak inflection points in the sample data for each area and allowed the mineralisation model to have optimum continuity.</li> <li>For deposits where the mineralization is typically narrow such as Mesa\Westlode, and Nambi, it does appear to pinch and swell, giving variable thickness of mineralisation and localised very high grades over short ranges.</li> <li>Dolerite and lamprophyre dyke intrusives have been modelled from the logging data in the Hub area. These dykes directly influence the mineralisation and have been accounted for in the Hub Mineral Resource.</li> </ul>
<b>Dimensions</b>	<i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i>	<ul style="list-style-type: none"> <li>The Hub deposit is 915 m long and extends 335 m below surface, striking 350°, with a vertical dip. The interpreted mineralisation ranges in thickness from 1 to 10 m wide with an average width of approximately 2.5 m. There are minor footwall and hanging lodes that are parallel to the main interpreted mineralisation. The mineralisation is truncated into three distinct zones by cross cutting lamprophyre dykes at the south and dolerite dykes to the north that have been identified in RC and DD drilling.</li> <li>The Kelly deposit is 1,090 m long and extends 110 m below surface, striking 000°, with a -35° dip to the east. The interpreted mineralisation includes 15 domains of variable thickness ranging from 2 to 30 m but on average are 10 m wide.</li> <li>The Mesa deposit is 725 m long and extends 125 m below surface, striking 335°, with a vertical dip. The interpreted mineralisation includes 3 domains ranging in thickness from 1.5 to 6 m with an average width of approximately 1.8 m.</li> <li>The Westlode deposit is 850 m long and extends 125 m below surface, striking 335°, with a vertical dip. The interpreted mineralisation includes 10 domains ranging in thickness from 1.5 to 20 m with an</li> </ul>



Criteria	JORC Code explanation	Commentary																																																																					
		<p>average width of approximately 4.5 m.</p> <ul style="list-style-type: none"><li>• The Redcliffe deposit is 535 m long and extends 120 m below surface, striking 335°, with a vertical dip. The interpreted mineralisation ranges in thickness from 2 to 30 m with an average width of approximately 11 m.</li><li>• The Bindy deposit is 950 m long and extends 285 m below surface, overall striking 000°, with a vertical dip. The interpreted mineralisation includes 8 domains ranging in thickness from 1.5 to 25 m with an average width of approximately 8 m.</li><li>• The Nambi deposit is 575 m long and extends 425 m below surface, striking 010°, with a vertical dip. The interpreted mineralisation includes 5 domains ranging in thickness from 1.5 to 7 m with an average width of approximately 2.5 m.</li><li>• The GTS deposit is 730 m long and extends 230 m below surface, striking 000°, with a vertical dip. The interpreted mineralisation ranges in thickness from 10 to 50 m.</li></ul>																																																																					
<b>Estimation and modelling techniques</b>	<i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i>	<ul style="list-style-type: none"><li>• For the deposits including Hub, Kelly, Bindy, Mesa, Westlode and Nambi, the estimation method involved Ordinary Kriging (“OK”) of 1 m downhole composites to estimate gold into a 3D block model. Some of the domains only contained a few composite assays. The grades of these domains were assigned the mean grade of the composites, rather than an estimated grade.</li><li>• Only RC and DD drilling are included in the compositing and estimation process. The initial sampling generally occurs at 1 m intervals for the RC drilling and variable sample lengths from 0.2 to 1.4 m in the DD drilling. Samples within each mineralisation domain were therefore composited to 1 m using Surpac software “best fit” option and a threshold inclusion of samples at sample length 50% of the targeted composite length.</li><li>• Variogram modelling was undertaken within Snowden Supervisor (“Supervisor”) for the composited data for all domains with sufficient data to produce robust variograms. All variogram models were undertaken by transforming the composite data to Gaussian space, modelling a Gaussian variogram, and then back-transforming the Gaussian models to real space for use in interpolation. For the poorly informed domains, variograms models were adopted from the modelled variograms and the orientation modified accordingly.</li><li>• The influence of extreme grade values was reduced by high grade capping where required. The high-grade capping limits were determined using a combination of top-cut analysis tools (grade histograms, log probability plots and coefficient of variation). These were reviewed and applied on a domain-by-domain basis.</li><li>• The Kriging Neighbourhood Analysis (“KNA”) function within Supervisor software was used to determine the most appropriate estimation parameters such as minimum and maximum samples, discretisation and search distance to be used for the estimation.</li><li>• For each deposit, a parent block size was selected based on the data spacing and domain morphology and the sub-block size to ensure sufficient volume resolution resulting in the following:</li></ul> <table><tr><th rowspan="2">Deposit</th><th colspan="3">Parent Block Size</th><th colspan="3">Sub-Block Size</th></tr><tr><th>Y(m)</th><th>X(m)</th><th>Z(m)</th><th>Y(m)</th><th>X(m)</th><th>Z(m)</th></tr><tr><td>Hub</td><td>12.5</td><td>2</td><td>10</td><td>3.125</td><td>0.25</td><td>2.5</td></tr><tr><td>Kelly</td><td>12.5</td><td>5</td><td>5</td><td>3.125</td><td>2.5</td><td>2.5</td></tr><tr><td>Mesa</td><td>12.5</td><td>4</td><td>5</td><td>3.125</td><td>0.25</td><td>2.5</td></tr><tr><td>WL</td><td>12.5</td><td>4</td><td>5</td><td>3.125</td><td>0.25</td><td>2.5</td></tr><tr><td>Redcliffe</td><td>10</td><td>4</td><td>5</td><td>2.5</td><td>1</td><td>2.5</td></tr><tr><td>Bindy</td><td>25</td><td>5</td><td>10</td><td>3.125</td><td>0.625</td><td>2.5</td></tr><tr><td>Nambi</td><td>20</td><td>5</td><td>10</td><td>2.5</td><td>0.625</td><td>2.5</td></tr><tr><td>GTS</td><td>5</td><td>5</td><td>2.5</td><td>2.5</td><td>2.5</td><td>1.25</td></tr></table>	Deposit	Parent Block Size			Sub-Block Size			Y(m)	X(m)	Z(m)	Y(m)	X(m)	Z(m)	Hub	12.5	2	10	3.125	0.25	2.5	Kelly	12.5	5	5	3.125	2.5	2.5	Mesa	12.5	4	5	3.125	0.25	2.5	WL	12.5	4	5	3.125	0.25	2.5	Redcliffe	10	4	5	2.5	1	2.5	Bindy	25	5	10	3.125	0.625	2.5	Nambi	20	5	10	2.5	0.625	2.5	GTS	5	5	2.5	2.5	2.5	1.25
Deposit	Parent Block Size			Sub-Block Size																																																																			
	Y(m)	X(m)	Z(m)	Y(m)	X(m)	Z(m)																																																																	
Hub	12.5	2	10	3.125	0.25	2.5																																																																	
Kelly	12.5	5	5	3.125	2.5	2.5																																																																	
Mesa	12.5	4	5	3.125	0.25	2.5																																																																	
WL	12.5	4	5	3.125	0.25	2.5																																																																	
Redcliffe	10	4	5	2.5	1	2.5																																																																	
Bindy	25	5	10	3.125	0.625	2.5																																																																	
Nambi	20	5	10	2.5	0.625	2.5																																																																	
GTS	5	5	2.5	2.5	2.5	1.25																																																																	

Criteria	JORC Code explanation	Commentary																																																		
		<ul style="list-style-type: none"> <li>Gold was estimated using Geovia Surpac v7.4.2 (Surpac) with hard domain boundaries and parameters optimised for each domain. The minimum and maximum number of samples for each of the deposits is as follows: <table border="1"> <thead> <tr> <th rowspan="2">Deposit</th><th colspan="2">No. of samples</th></tr> <tr> <th>Minimum</th><th>Maximum</th></tr> </thead> <tbody> <tr> <td>Hub</td><td>6</td><td>18</td></tr> <tr> <td>Kelly</td><td>6</td><td>16</td></tr> <tr> <td>Mesa</td><td>4</td><td>16</td></tr> <tr> <td>WL</td><td>6</td><td>18</td></tr> <tr> <td>Redcliffe</td><td>4</td><td>16</td></tr> <tr> <td>Bindy</td><td>6</td><td>18</td></tr> <tr> <td>Nambi</td><td>6</td><td>16</td></tr> </tbody> </table> </li> <li>Search distances were based on the modelled variograms. A second search passes were used, however the proportion of material represented by the second pass is minor. The search distances and second pass search factors are as follows: <table border="1"> <thead> <tr> <th>Deposit</th><th>Search Distance</th><th>Second pass search factor</th></tr> </thead> <tbody> <tr> <td>Hub</td><td>50</td><td>2.5/3</td></tr> <tr> <td>Kelly</td><td>28/38/43/45/115</td><td>2</td></tr> <tr> <td>Mesa</td><td>80</td><td>2</td></tr> <tr> <td>WL</td><td>40</td><td>1.3/1.4</td></tr> <tr> <td>Redcliffe</td><td>125</td><td>2</td></tr> <tr> <td>Bindy</td><td>75</td><td>2.5</td></tr> <tr> <td>Nambi</td><td>70</td><td>2</td></tr> </tbody> </table> </li> <li>The GTS deposit was estimated using the non-linear, Localised Uniform Conditioning (LUC) method. LUC is a post-processed approach based on an OK estimate, which is able to produce SMU-scale block grade estimates that are not over-smoothed.</li> <li>Samples were composited to 1 m within the single estimation domain using best fit length option and a threshold inclusion of samples at sample length 50% of the targeted composite length.</li> <li>The influence of extreme grade values was reduced by applying a top cap of 25 g/t Au. In addition, a distance based top cut was also applied for 5 g/t Au at a distance greater than 10 m.</li> <li>The gold grade variogram model was undertaken by transforming the composite data to Gaussian space, modelling a Gaussian variogram, and then back-transforming the Gaussian models to real space for use in interpolation. The general orientation of the mineralisation domain is steep however variogram modelling resulted in a major direction along strike (000°) and semi-major direction dipping at -55° to the east.</li> <li>LUC estimation was undertaken using a Panel block size of 20(N)m × 10(E)m × 10(RL)m. The final SMU estimation block size for the LUC was set at 5(N)m × 5(E)m × 2.5(RL)m. Selection of the Panel was used based primarily on data spacing.</li> <li>LUC estimation is based on Panel block estimates undertaken using OK. This was followed by a Change of Support (CoS) which uses the composite gold grade distribution and variogram model to define a gold grade distribution at the SMU block scale. An Information Effect correction, which accounts for the imperfect predictions that dense GC data will produce, was modelled as part of the CoS, assuming a GC drill spacing of 8mY × 5mX × 1mRL. Uniform Conditioning (UC) was then undertaken to produce a model of the SMU block grade, tonnage and metal distribution within each Panel, which is conditioned to the Panel grade. The resulting array variables for a range of cut-off grades is stored in the Panel block model. Finally, LUC is undertaken whereby the UC SMU block grade distribution stored in the Panel model is devolved to the SMU block model via a discretization post-processing procedure,</li> </ul>	Deposit	No. of samples		Minimum	Maximum	Hub	6	18	Kelly	6	16	Mesa	4	16	WL	6	18	Redcliffe	4	16	Bindy	6	18	Nambi	6	16	Deposit	Search Distance	Second pass search factor	Hub	50	2.5/3	Kelly	28/38/43/45/115	2	Mesa	80	2	WL	40	1.3/1.4	Redcliffe	125	2	Bindy	75	2.5	Nambi	70	2
Deposit	No. of samples																																																			
	Minimum	Maximum																																																		
Hub	6	18																																																		
Kelly	6	16																																																		
Mesa	4	16																																																		
WL	6	18																																																		
Redcliffe	4	16																																																		
Bindy	6	18																																																		
Nambi	6	16																																																		
Deposit	Search Distance	Second pass search factor																																																		
Hub	50	2.5/3																																																		
Kelly	28/38/43/45/115	2																																																		
Mesa	80	2																																																		
WL	40	1.3/1.4																																																		
Redcliffe	125	2																																																		
Bindy	75	2.5																																																		
Nambi	70	2																																																		

Criteria	JORC Code explanation	Commentary																																																					
		<p>thus resulting in a single grade value per SMU block.</p> <ul style="list-style-type: none"><li>Search radius parameters were based on the anisotropy evident in the variogram, and by visual inspection of the pattern of informing composite selection. For the OK panel estimate, a single pass estimate was used with a minimum (6) and maximum (18) numbers of allowable samples were selected based on KNA. For the SMU ranking estimate, a single pass was also used but with a minimum (6) and maximum (18) composites. During estimation, locally varying rotations were used for both the variogram model and search neighbourhood. These were based on interpreted surfaces that reflect the plane of maximum continuity of the gold mineralisation within the domain. The major and semi-major axes of the variograms and searches were thus oriented parallel to these planes.</li><li>Isatis v2018 was used to undertake the LUC estimation, with the results being imported into the final Surpac v6.9 block model.</li></ul>																																																					
	<i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i>	<ul style="list-style-type: none"><li>Historical mining (post-1990) has taken place at Mesa, West Lode, Redcliffe and Nambi. Production records exist for some of the deposits, but they are not detailed enough to be used for verification of the estimates.</li><li>For Hub, an alternate 2D accumulation check estimate for the two largest domains compared well to the final estimate and also compares well to the previous MRE completed in 2020.</li></ul>																																																					
	<i>The assumptions made regarding recovery of by-products.</i>	<ul style="list-style-type: none"><li>No by-product recoveries were considered.</li></ul>																																																					
	<i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i>	<ul style="list-style-type: none"><li>No estimation has been completed for other elements or deleterious elements.</li></ul>																																																					
	<i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i>	<ul style="list-style-type: none"><li>Parent block sizes were generally based on approximately half the intersecting drill spacing. The parent and sub-cell sizes for all the deposits are as follows:</li></ul> <table><tr><th rowspan="2">Deposit</th><th colspan="3">Parent cells</th><th colspan="2">Sub-cells</th></tr><tr><th>X (m)</th><th>Y (m)</th><th>Z (m)</th><th>X (m)</th><th>Y (m)</th></tr><tr><td>Hub</td><td>2</td><td>12.5</td><td>10</td><td>0.25</td><td>3.125</td></tr><tr><td>Kelly</td><td>5</td><td>12.5</td><td>5</td><td>2.5</td><td>3.125</td></tr><tr><td>Mesa\WL</td><td>4</td><td>12.5</td><td>5</td><td>0.25</td><td>3.125</td></tr><tr><td>Redcliffe</td><td>4</td><td>10</td><td>5</td><td>1</td><td>2.5</td></tr><tr><td>Bindy</td><td>5</td><td>25</td><td>10</td><td>0.625</td><td>3.125</td></tr><tr><td>Nambi</td><td>5</td><td>20</td><td>10</td><td>0.625</td><td>2.5</td></tr><tr><td>GTS</td><td>5</td><td>5</td><td>2.5</td><td>5</td><td>5</td></tr></table>	Deposit	Parent cells			Sub-cells		X (m)	Y (m)	Z (m)	X (m)	Y (m)	Hub	2	12.5	10	0.25	3.125	Kelly	5	12.5	5	2.5	3.125	Mesa\WL	4	12.5	5	0.25	3.125	Redcliffe	4	10	5	1	2.5	Bindy	5	25	10	0.625	3.125	Nambi	5	20	10	0.625	2.5	GTS	5	5	2.5	5	5
Deposit	Parent cells			Sub-cells																																																			
	X (m)	Y (m)	Z (m)	X (m)	Y (m)																																																		
Hub	2	12.5	10	0.25	3.125																																																		
Kelly	5	12.5	5	2.5	3.125																																																		
Mesa\WL	4	12.5	5	0.25	3.125																																																		
Redcliffe	4	10	5	1	2.5																																																		
Bindy	5	25	10	0.625	3.125																																																		
Nambi	5	20	10	0.625	2.5																																																		
GTS	5	5	2.5	5	5																																																		
	<i>Any assumptions behind modelling of selective mining units.</i>	<ul style="list-style-type: none"><li>The block model definition parameters included a primary block size and sub-blocking deemed appropriate for the mineralisation and to provide adequate volume definition. These dimensions are suitable for block estimation and modelling the selectivity for either an open pit or underground mining operation.</li></ul>																																																					
	<i>Any assumptions about correlation between variables.</i>	<ul style="list-style-type: none"><li>No correlation analysis between other elements and gold was conducted.</li></ul>																																																					
	<i>Description of how the geological interpretation was used to control the resource estimates.</i>	<ul style="list-style-type: none"><li>The mineralised domains acted as a hard boundary to control the gold estimation.</li><li>The mineralised domains did not extend into the interpreted laterite weathering profile or into the post mineralisation dykes.</li></ul>																																																					
	<i>Discussion of basis for using or not using grade cutting or capping.</i>	<ul style="list-style-type: none"><li>Composite gold grade distributions within each of the mineralisation domains were assessed to determine if a high-grade cutting or capping should be applied.</li><li>High grade capping was determined using a combination of statistical analysis tools (grade histograms, log probability (“LN”) plots and effects on the coefficient of variation (“CV”) and metal at risk analysis on each individual domain. In some cases, no capping was applied. The grade capping used for the deposits is as follows (domain dependant):</li></ul>																																																					

Criteria	JORC Code explanation	Commentary																																																											
		<table><tr><td>Deposit</td><td>Grade capping (Au g/t)</td></tr><tr><td>Hub</td><td>3, 4, 6, 30, 50, 999</td></tr><tr><td>Kelly</td><td>4, 5, 6, 7, 8, 15, 999</td></tr><tr><td>Mesa\WL</td><td>6, 11, 23, 999</td></tr><tr><td>Redcliffe</td><td>11</td></tr><tr><td>Bindy</td><td>20</td></tr><tr><td>Nambi</td><td>5, 10, 18</td></tr><tr><td>GTS</td><td>25</td></tr></table> <ul style="list-style-type: none"><li>Additional distance based top cutting ( 5 g/t Au at 10 m) was used for GTS.</li></ul>	Deposit	Grade capping (Au g/t)	Hub	3, 4, 6, 30, 50, 999	Kelly	4, 5, 6, 7, 8, 15, 999	Mesa\WL	6, 11, 23, 999	Redcliffe	11	Bindy	20	Nambi	5, 10, 18	GTS	25																																											
Deposit	Grade capping (Au g/t)																																																												
Hub	3, 4, 6, 30, 50, 999																																																												
Kelly	4, 5, 6, 7, 8, 15, 999																																																												
Mesa\WL	6, 11, 23, 999																																																												
Redcliffe	11																																																												
Bindy	20																																																												
Nambi	5, 10, 18																																																												
GTS	25																																																												
	<i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i>	<ul style="list-style-type: none"><li>Prior to grade estimation, volumetric comparison of the wireframe solid volume to that of the block model volume for each domain was completed.</li><li>The model grade estimate has been checked by comparing composite data with block model grades in swath plots (north/east/elevation) for each estimated domain. A visual comparison in long section has also been completed between block grades and total drill intersection grades. Also, a global comparison with the cut grade drill hole composites with the block model grades for each lode domain was completed.</li><li>The block model visually and statistically reflects the input data.</li></ul>																																																											
<b>Moisture</b>	<i>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</i>	<ul style="list-style-type: none"><li>Tonnages are reported on a dry basis with sampling and analysis having been conducted to avoid water content density issues. No work has been completed on the moisture content.</li></ul>																																																											
<b>Cut-off parameters</b>	<i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i>	<ul style="list-style-type: none"><li>The Mineral Resource has been quoted inside the interpreted mineralised domains, and either above a reporting cut-off grade of 0.5 g/t Au where above the 300 m RL, or above a reporting cut-off grade of 2.0 g/t Au where below the 300 m RL.</li></ul>																																																											
<b>Mining factors or assumptions</b>	<i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i>	<ul style="list-style-type: none"><li>For all deposits, except Hub, it is assumed that mining would be by open pits methods. For Hub, it is assumed that there would be a combination of open cut and underground. It is also assumed that the ore would be transported and processed at the Mt Morgans Operation.</li><li>Minimum width dimensions of ore to be mined is assumed as 2 m which approximates to the minimum thickness of the mineralisation estimation domains.</li></ul>																																																											
<b>Metallurgical factors or assumptions</b>	<i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i>	<ul style="list-style-type: none"><li>The following table displays the metallurgical test work conducted at ALS Perth during September 2020 on mineralisation for various Redcliffe Project mineralisation, with a consistent gravity separation grind size of P80 passing 150 µm.</li></ul> <table><tr><th>Deposit</th><th>Material type</th><th>Comp #</th><th>Material Source</th><th>Leach grid size (P80 µm)</th><th>Gravity Gold Recovery (%)</th><th>Total Gold Recovery (%)</th></tr><tr><td rowspan="3">Bindy</td><td rowspan="3">Fresh</td><td rowspan="3">1</td><td rowspan="3">GTDD012 225-227 (2)</td><td>150</td><td>11.37</td><td>87.11</td></tr><tr><td>106</td><td>11.69</td><td>90.48</td></tr><tr><td>75</td><td>11.56</td><td>94.02</td></tr><tr><td rowspan="3">GTS</td><td rowspan="3">Fresh</td><td rowspan="3">2</td><td rowspan="3">GTDD009 100-103 (2)</td><td>150</td><td>5.11</td><td>68.05</td></tr><tr><td>106</td><td>5.13</td><td>72.14</td></tr><tr><td>75</td><td>4.93</td><td>78.14</td></tr><tr><td rowspan="3">GTS</td><td rowspan="3">Oxide</td><td rowspan="3">3</td><td rowspan="3">GTDD007 38-40 (2)</td><td>150</td><td>15.26</td><td>87.17</td></tr><tr><td>106</td><td>15.09</td><td>90</td></tr><tr><td>75</td><td>14.87</td><td>93.45</td></tr><tr><td rowspan="3">GTS</td><td rowspan="3">Transitional</td><td rowspan="3">4</td><td rowspan="3">GTDD009 89-92 (2)</td><td>150</td><td>3.67</td><td>78.67</td></tr><tr><td>106</td><td>3.44</td><td>80.86</td></tr><tr><td>75</td><td>3.44</td><td>85.73</td></tr></table>	Deposit	Material type	Comp #	Material Source	Leach grid size (P80 µm)	Gravity Gold Recovery (%)	Total Gold Recovery (%)	Bindy	Fresh	1	GTDD012 225-227 (2)	150	11.37	87.11	106	11.69	90.48	75	11.56	94.02	GTS	Fresh	2	GTDD009 100-103 (2)	150	5.11	68.05	106	5.13	72.14	75	4.93	78.14	GTS	Oxide	3	GTDD007 38-40 (2)	150	15.26	87.17	106	15.09	90	75	14.87	93.45	GTS	Transitional	4	GTDD009 89-92 (2)	150	3.67	78.67	106	3.44	80.86	75	3.44	85.73
Deposit	Material type	Comp #	Material Source	Leach grid size (P80 µm)	Gravity Gold Recovery (%)	Total Gold Recovery (%)																																																							
Bindy	Fresh	1	GTDD012 225-227 (2)	150	11.37	87.11																																																							
				106	11.69	90.48																																																							
				75	11.56	94.02																																																							
GTS	Fresh	2	GTDD009 100-103 (2)	150	5.11	68.05																																																							
				106	5.13	72.14																																																							
				75	4.93	78.14																																																							
GTS	Oxide	3	GTDD007 38-40 (2)	150	15.26	87.17																																																							
				106	15.09	90																																																							
				75	14.87	93.45																																																							
GTS	Transitional	4	GTDD009 89-92 (2)	150	3.67	78.67																																																							
				106	3.44	80.86																																																							
				75	3.44	85.73																																																							

Criteria	JORC Code explanation	Commentary						
		Nambi	Fresh (lens E2)	5	NBRC137 D 60.5-61.5 (2)	150 106 75	24.9 24.25 25.64	88.7 90.78 91.72
		Nambi	Fresh (lens E1)	6	NBRC137 D 115.5-117 (2)	150 106 75	31.95 31.96 32.78	89.93 92.89 94.65
		Nambi	Fresh (main lens)	7	NBRC137 D 186.25-187.75 (2)	150 106 75	68.15 68.47 70.05	94.12 95.75 97.03
		Redcliffe deposit	Fresh (lens E)	8	19RRC06 4 101-102 (2)	150 106 75	13.76 13.9 13.83	85.83 89.15 91.33
		Redcliffe deposit	Transitional (lens E)	9	19RRC06 6 43-44 (2)	150 106 75	7.07 7.15 7.16	92.63 95.88 96.27
		Hub	Fresh	10	19RRC02 8 136-137; 19RRC07 3D 180-181	150 106 75	21.07 21.4 22.99	85.85 90.36 93.69
		Hub	Oxide	11	19RRC07 9 31-32 (2); 19RRC08 2 31-32 (2);	150 106 75	17.74 18.56 19	86.54 95.81 98.08
		Hub	Transitional	12	19RRC04 2 104-105 (2); 19RRC09 2 90-91 (2)	150 106 75	24.69 24.64 26.33	93.77 95.43 96.88
<b>Environmental factors or assumptions</b>	<i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i>	<ul style="list-style-type: none"> <li>It is considered that there are no significant environmental factors, which would prevent the eventual extraction of material from these deposits, especially since some of the deposits have been historically mined. Environmental surveys and assessments will form a part of future pre-feasibility.</li> </ul>						
<b>Bulk density</b>	<i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i>	<ul style="list-style-type: none"> <li>Bulk Density (BD) data was derived from core collected at this project and neighboring deposits drilled by NTM Gold.</li> <li>Fresh and transitional BD measurements have been collected from Hub, Mertondale, GTS and Nambi deposits.</li> </ul>						
	<i>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i>	<ul style="list-style-type: none"> <li>Bulk density measurements were completed using Archimedes method of measurements on sticks of core.</li> <li>A series of pit samples were collected from the Nambi pit (located to the north) to obtain oxide and transitional measurements.</li> </ul>						
	<i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i>	The final insitu bulk densities applied are a mixture of actual bulk density measurements, experiences from other deposits from the Northern Goldfields of Western Australia and the depths of the weathering profiles. Generally the bulk densities are based on the weathering profiles. The bulk densities applied are as follows:						

Criteria	JORC Code explanation	Commentary				
		Project	Rocktype	Weathering domain		
				Oxide	Transitional	Fresh
		Hub	Laterite	2.5	-	-
			All	1.8	2.5	2.7
		Kelly	porphyry	1.8	2.2	2.7
			granodiorite	1.8	2.2	2.7
			granite	1.7	2.1	2.6
		Mesa\WL	All	1.8	2.2	2.7
		Redcliffe	All	1.8	2.2	2.7
		Bindy	Laterite	2.5	-	-
			All	1.8	2.2	2.7
		Nambi	All	1.8	2.2	2.7
		GTS	All	1.8	2.5	2.7
<b>Classification</b>	<i>The basis for the classification of the Mineral Resources into varying confidence categories.</i>	<ul style="list-style-type: none"> <li>The Mineral Resources are classified as Indicated and Inferred.</li> <li>Classification has been based on several criteria including the quality of drill data, estimation confidence, consideration of potential mining methodology, drillhole spacing and visual geological controls on continuity of mineralisation.</li> <li>Indicated Mineral Resources are typically defined by 25 m × 25 m spaced drilling intersections. Estimation is undertaken in the first pass with an average distance to informing sample of less than 40 m.</li> <li>Inferred Mineral Resources are defined by wider drilling intersections generally approaching 50 m x 50 m where the confidence that the continuity of mineralisation can be extended along strike and at depth. Estimation includes areas of a second pass and the average distance to informing sample of less than 80 m.</li> </ul>				
	<i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i>	<ul style="list-style-type: none"> <li>This classification is considered appropriate given the confidence that can be gained from the existing data density and results from drilling.</li> <li>The resource classifications are based on the quality of information for the geological domaining, as well as the drill spacing and geostatistical measures to provide confidence in the tonnage and grade estimates.</li> </ul>				
	<i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i>	<ul style="list-style-type: none"> <li>The Mineral Resource classification and results appropriately reflect the Competent Person's view of the deposits and the current level of risk associated with the project to date</li> </ul>				
<b>Audits or reviews</b>	<i>The results of any audits or reviews of Mineral Resource estimates.</i>	<ul style="list-style-type: none"> <li>The mineralisation domaining, estimation parameters, classification and reporting have all been internally peer reviewed.</li> </ul>				
<b>Discussion of relative accuracy/confidence</b>	<i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i>	<ul style="list-style-type: none"> <li>The confidence in the data quality, drilling methods and analytical results is reflected in the resource classification.</li> <li>Local variations can be expected such as pinch and swell and the influence of the late-stage cross-cutting dykes. Where appropriate, closer spaced drilling will improve confidence in the estimate.</li> <li>Bulk density test work needs to continue to increase confidence in the reported resource, especially within the oxide and transitional profiles.</li> </ul>				
	<i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i>	<ul style="list-style-type: none"> <li>The Mineral Resources constitute global resource estimates for each deposit.</li> </ul>				
	<i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i>	<ul style="list-style-type: none"> <li>Some of the deposits have been previously mined, but no high confidence production data is available.</li> </ul>				



## Section 4 Estimation and Reporting of Ore Reserves

### Jupiter Open Pit

Criteria	JORC Code (2012) explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	<p><i>Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.</i></p> <p><i>Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.</i></p>	<p>Mineral Resource estimates for the Heffernans and Doublejay Deposits as at 30 June 2021 as per Table 1 of this ASX release have been used for Ore Reserve estimation for the Jupiter open pit.</p> <p>The Mineral Resource estimates reported for the Heffernans and Doublejay Deposits are inclusive of the Ore Reserves.</p>
Site visits	<p><i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i></p> <p><i>If no site visits have been undertaken indicate why this is the case.</i></p>	<p>The 2021 Jupiter Ore Reserve Estimate was based on mine designs undertaken by Dacian site personnel. The designs and associated Ore Reserves were independently reviewed by Mr Ross Cheyne, Principal Consultant and Director of Oreology Consulting Pty Ltd, an independent mine engineering consulting group.</p> <p>Mr. Cheyne is a Fellow of the Australian Institute of Mining and Metallurgy (109345) and is the Competent Person with respect to the Ore Reserve estimate for the Jupiter open pits.</p> <p>Mr Cheyne undertook a site visit in 2016 while acting as CP for the Jupiter Ore Reserves at the DFS phase.</p> <p>A more recent site visit was undertaken in August 2021 by Mr Andrew Cooper, a Principal Consultant of Oreology Consulting Pty Ltd. Mr Cooper undertook the following activities:</p> <ul style="list-style-type: none"> <li>- General site familiarization</li> <li>- Inspection of the open pit working areas and associated stockpiling areas</li> </ul>
Study status	<p><i>The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.</i></p> <p><i>The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.</i></p>	<p>Development of the Jupiter open pit mine commenced in December 2017. Study work completed to update the Ore Reserve Estimate comprises detailed mine design and scheduling that considers open pit mining conditions and performance experienced since December 2017. This includes:</p> <ul style="list-style-type: none"> <li>- Contracted pricing for open pit mining works</li> <li>- Application of current mine owner costs</li> <li>- Incorporation of geotechnical review and recommendations during pit design</li> <li>- Recent mining performance regarding equipment productivity and availability</li> <li>- Recent ore processing performance and costs</li> </ul> <p>The mine plan is considered technically achievable and involves the application of conventional technology and open pit mining methods widely utilised in the Western Australian goldfields.</p> <p>The Ore Reserve Estimate and associated mine plan and financial modelling is supported by actual project to date mining performance, and current operating mining costs, processing costs and recovery information.</p>
Cut-off parameters	<p><i>The basis of the cut-off grade(s) or quality parameters applied</i></p>	<p>Break-even cut-off grades were determined by considering:</p> <ul style="list-style-type: none"> <li>- Gold price;</li> <li>- Achieved gold recovery from ore processing;</li> <li>- Mining costs, comprised of current mining contractor mine owner costs;</li> <li>- Current ore processing costs; and</li> <li>- Royalties</li> </ul>

Criteria	JORC Code (2012) explanation	Commentary
		The calculated breakeven cut-off grade at a gold prices of 2,100 AUD/oz equates to 0.33 g/t. However, to mitigate the risk of reduced processing recoveries at the lower grade ranges, Dacian have elected to report the open pit Ore Reserve at a cut-off grade of 0.5 g/t.
Mining factors or assumptions	<p><i>The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).</i></p> <p><i>The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.</i></p> <p><i>The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.</i></p> <p><i>The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).</i></p> <p><i>The mining dilution factors used.</i></p> <p><i>The mining recovery factors used.</i></p> <p><i>Any minimum mining widths used.</i></p> <p><i>The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.</i></p> <p><i>The infrastructure requirements of the selected mining methods.</i></p>	<p>No material changes have been made to the pit designs for Heffernans and Doublejay since the last reported Ore Reserve in 2020. The 2021 Ore Reserve comprises re-reporting within the same designs utilising the updated 2021 Mineral Resource Estimates</p> <p>All pits are currently being mined via mechanised open pit methods utilising conventional mining equipment. Mining commenced in December 2017 and the mining methodology and equipment selected remains unchanged and continues to be appropriate.</p> <p>Regular geotechnical inspections by an independent geotechnical engineer have been carried out on the Jupiter open pit. Recommendations have been included during detailed pit design.</p> <p>Pit designs were validated against optimised pit shells as part of the initial design process for the 2020 Ore Reserve Estimate. This has not been updated for the 2021 Ore reserve Estimate.</p> <p>Ore dilution was modelled through conversion of the subcelled Mineral Resource Model to a regularised 5m X by 5m Y by 2.5m Z block size. This is considered an appropriate Selective Mining Unit (SMU) size for the equipment size and bench height being mined in the Jupiter open pits.</p> <p>Mining loss has been included as part of the regularisation process. No additional operation ore loss has been included.</p> <p>Minimum mining bench widths of 30m have been assumed based on selected mining equipment.</p> <p>No Inferred Mineral Resources have been included in the Ore Reserve Estimate. Inferred Mineral Resources were treated as waste and assigned no economic value.</p> <p>The proposed mine design and associated mine plan does not require any further expansion of the current mining and processing infrastructure.</p>

Criteria	JORC Code (2012) explanation	Commentary
Metallurgical factors or assumptions	<p><i>The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.</i></p> <p><i>Whether the metallurgical process is well-tested technology or novel in nature.</i></p> <p><i>The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.</i></p> <p><i>Any assumptions or allowances made for deleterious elements.</i></p> <p><i>The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.</i></p> <p><i>For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?</i></p>	<p>The Mt Morgans process plant was commissioned in late March 2018 and includes a Semi Autogenous Grinding, Ball Milling and Pebble Crushing (SABC) comminution circuit followed by conventional gravity and carbon-in-leach (CIL) process.</p> <p>The metallurgical process is commonly used in Western Australian and international gold mining. The same process configuration was previously utilised at Mt Morgans during the 1990s.</p> <p>A metallurgical test work program was completed during the 2016 DFS using samples from diamond drill core and RC drill chips to determine:</p> <ul style="list-style-type: none"> <li>- physical properties for comminution circuit design;</li> <li>- optimal grind size; and</li> <li>- gold recovery.</li> </ul> <p>Since the process plant was commissioned in late March 2018, a total of 9.2Mt (dry) was milled until the end of June 2021. The average gold recovery over this period was 92.6% for a blended feed from the Jupiter open pits, Westralia underground as well as the Mt Marven open pit. A recovery of 92% was used for the economic evaluation of the Jupiter open pits.</p> <p>No deleterious elements were identified from the mineralogical/metallurgical assessments carried out during the 2016 DFS and evidence of such has not been observed during ore processing operations from plant commissioning in March 2018 to June 2021.</p> <p>In addition to processing ore from the Heffernans and Doublejay deposits as a component of the mill feed blend from March 2018, under previous owners approximately 10Mt of ore was treated through the historic Mt Morgans treatment plant during the 1990s. This included ore mined from the historic Joanne and Jenny pits (now subject to a cutback as the Doublejay pit). The average recovery during the 10 year period was 91.4%.for 740,000 ounces produced.</p> <p>Not applicable. No minerals are defined by a specification.</p>
Environmental	<p><i>The status of studies of potential environmental impacts of the mining and processing operation.</i></p> <p><i>Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.</i></p>	<p>All regulatory approvals and permits have been granted for ongoing mining and processing at Mt Morgans, including current mining of the Jupiter Deposit.</p> <p>Waste rock characterisation was completed on drill samples as a component of the 2016 DFS. All Jupiter waste rocks were characterised as non-acid forming (NAF) with the exception of highly localised portions of basalt and to a lesser extent, intermediate quartz porphyry. This material accounts for less than 6% of all waste rock mined from the Jupiter pits as a whole.</p>
Infrastructure	<p><i>The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.</i></p>	<p>Mt Morgans is located in the immediate vicinity of the Laverton and Leonora townships and is within driving distance of Kalgoorlie, a major regional hub. Access to the site is via sealed public highways and public and private unsealed roads.</p>

Criteria	JORC Code (2012) explanation	Commentary
		<p>The site workforce is primarily fly-in, fly-out (FIFO) from Perth via the public Laverton airstrip.</p> <p>The Mt Morgans site is well established with a modern processing plant, associated 16.5MW gas fired power station, bore field and tailings storage facility; a 400 person capacity accommodation village; administration offices; workshops; reverse osmosis and waste water treatment plants.</p>
Costs	<p><i>The derivation of, or assumptions made, regarding projected capital costs in the study.</i></p> <p><i>The methodology used to estimate operating costs.</i></p> <p><i>Allowances made for the content of deleterious elements.</i></p> <p><i>The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.</i></p> <p><i>The source of exchange rates used in the study.</i></p> <p><i>Derivation of transportation charges. The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.</i></p> <p><i>The allowances made for royalties payable, both Government and private.</i></p>	<p>For the 2021 Jupiter Open Pit Ore Reserve Estimate, no additional capital is required as part of the associated mine plan.</p> <p>Operating costs have been estimated using current contract pricing for contractors currently engaged at Mt Morgans, current ore processing costs and mine owner costs.</p> <p>No deleterious elements have been identified and therefore no allowances were required.</p> <p>The financial analysis of the open pits utilised a gold price of AUD 2100 per ounce before royalties.</p> <p>All revenue and cost calculations have been done using Australian Dollars, hence application of an exchange rate has not been required.</p> <p>Transportation and refining charges of \$1.38/oz are based on current contract pricing applicable to Mt Morgans.</p> <p>In addition, a 2.5% Western Australian State Government royalty has been allowed for.</p> <p>This results in a net gold price of \$2046.12/oz.</p>
Revenue factors	<p><i>The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.</i></p> <p><i>The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.</i></p>	<p>Ore production and gold recovery estimates for revenue calculations were based on detailed mine designs, mine schedules, mining factors and cost estimates for mining and processing.</p> <p>A base gold price of AUD\$2100 has been used for economic analysis.</p>
Market assessment	<p><i>The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.</i></p> <p><i>A customer and competitor analysis along with the identification of likely market windows for the product.</i></p> <p><i>Price and volume forecasts and the basis for these forecasts.</i></p> <p><i>For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.</i></p>	<p>There is a transparent quoted market for the sale of gold.</p> <p>No industrial minerals have been considered.</p>
Economic	<i>The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs</i>	The Jupiter Ore Reserve is based on current mining contractor costs, ore processing costs and mine owner costs.

Criteria	JORC Code (2012) explanation	Commentary
	<p><i>including estimated inflation, discount rate, etc.</i></p> <p><i>NPV ranges and sensitivity to variations in the significant assumptions and inputs.</i></p>	<p>Economic analysis carried out as part of the Ore Reserve estimate process confirms the Mt Morgans operation yields a positive cashflow. Discounting has not been assessed due to the short mine life of the pits.</p> <p>As with all gold projects, the primary sensitivity is price. All Jupiter pits remain cash positive with a 10% reduction in gold price. At -20% the Doublejay pits remain cash positive (i.e. 95% of the Ore Reserve)</p>
Social	<p><i>The status of agreements with key stakeholders and matters leading to social licence to operate.</i></p>	<p>Mt Morgans is an operating mine site and has good working relationships with neighboring stakeholders.</p> <p>Granted tenements of types appropriate to the activities performed cover all areas of Mining Operations.</p> <p>The Nyalpa Pirniku Native Title Claim was accepted for registration on 15 May 2019. The Claim covers the majority of the Mt Morgans tenements, including Mining Lease M39/236 within which the Heffernans and Doublejay deposits are located. Native Title is yet to be determined, and in the case that it is granted, it is not expected to impact mining of the Heffernans and Doublejay deposits, as M39/236 pre-dates the Claim.</p>
Other	<p><i>To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:</i></p> <p><i>Any identified material naturally occurring risks.</i></p> <p><i>The status of material legal agreements and marketing arrangements.</i></p> <p><i>The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.</i></p>	<p>There are no likely identified naturally occurring risks that may affect the Jupiter Ore Reserve Estimate area.</p> <p>Contractual agreements are in place for all material services and supply of goods required for the Mt Morgans operation.</p> <p>All regulatory approvals and permits have been granted for ongoing mining and processing at Mt Morgans, including current mining of the Jupiter deposit.</p>
Classification	<p><i>The basis for the classification of the Ore Reserves into varying confidence categories.</i></p> <p><i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i></p> <p><i>The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).</i></p>	<p>The classification of the 2021 Jupiter Ore Reserve Estimate has been carried out and reported in accordance with the 2012 Edition of the JORC Code.</p> <p>The 2021 Jupiter Ore Reserve Estimate reflects the Competent Person's view of the deposit.</p> <p>The Probable Ore Reserve is based on that portion of Indicated Mineral Resource within the mine designs that may be economically extracted and includes allowance for dilution and ore loss. No Probable Ore Reserves have been derived from Measured Mineral Resource.</p>
Audits or reviews	<p><i>The results of any audits or reviews of Ore Reserve estimates.</i></p>	<p>Peer review on the 2021 Jupiter Ore Reserve Estimate has been completed internally by Dacian and externally by Orelog Consulting Pty Ltd.</p>

Criteria	JORC Code (2012) explanation	Commentary
Discussion of relative accuracy confidence	<p><i>Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.</i></p> <p><i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i></p> <p><i>Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.</i></p> <p><i>It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available</i></p>	<p>It is noted that Ore Reserve Estimates are an estimation only and subject to numerous variables common to mining projects and/or operations. It is however, in the opinion of the Competent Person that at the time of reporting, economic extraction of the 2021 Jupiter Ore Reserve estimate can be reasonably justified.</p> <p>Detailed mine designs and schedules; application of Modifying Factors for ore loss, dilution and ore processing gold recovery; and subsequent financial analysis used to estimate Ore Reserves are all supported by historical and current production data.</p>



## Westralia Underground

Criteria	JORC Code (2012) explanation	Commentary
<i>Mineral Resource estimate for conversion to Ore Reserves</i>	<p><i>Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.</i></p> <p><i>Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.</i></p>	<p>The Mineral Resource estimate for the Beresford and Allanson Deposits as at 31 March 2021 and as detailed in ASX release dated 11 May 2021 have been used for Ore Reserve estimation for the Westralia underground mine.</p> <p>The Mineral Resources estimates reported for the Beresford and Allanson Deposits are inclusive of the Ore Reserves.</p>
<i>Site visits</i>	<p><i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i></p> <p><i>If no site visits have been undertaken indicate why this is the case.</i></p>	<p>The Beresford and Allanson Ore Reserve estimations were completed by Mr Andrew Cooper, Principal Underground Mining Engineer of Orelogy Consulting Pty Ltd, an independent mine engineering consulting group.</p> <p>Mr Cooper is a Member of the Australian Institute of Mining and Metallurgy and is the Competent Person with respect to the Ore Reserve estimate for the Westralia underground mine.</p> <p>Mr Cooper conducted a site visit in August 2021 as part of the min planning study and reserves process. The following activities were completed:</p> <ul style="list-style-type: none"> <li>- General site familiarization.</li> <li>- Inspection of the existing underground development, stoping and infrastructure areas, in particular the starting faces of initial planned development.</li> <li>- Inspections of the portals, ROM, and surface infrastructure.</li> </ul>
<i>Study status</i>	<p><i>The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.</i></p> <p><i>The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.</i></p> <p><i>The basis of the cut-off grade(s) or quality parameters applied</i></p>	<p>Under the ownership of Dacian Gold Ltd, development of the Westralia underground mine commenced in May 2017 and subsequently ore was mined via open stoping methods from both the Beresford and Allanson deposits from January 2018 through to August 2020, following which, the mine was placed into care and maintenance.</p> <p>The current mine planning study work completed for the Westralia Ore Reserve estimate comprised detailed mine designs and mining schedules that consider underground mining conditions experienced since May 2017; application of industry current contract mining rates for underground mining works; application of historic pricing for surface ore haulage; mine owner costs estimates considering historical cost data; current ore processing costs and processing performance since the plant was commissioned in late March 2018.</p> <p>The current mine planning study work completed for the Westralia Beresford and Allanson deposits utilized modifying factors based on historical operational performance and first principle analysis.</p> <p>The study demonstrates that the mine plans are technically achievable and economically viable at the time of reporting. The mine plan involves the application of conventional mining methods and technologies widely utilised in the Western Australian goldfields.</p> <p>Break-even cut-off grades were determined by considering:</p> <ul style="list-style-type: none"> <li>- Gold price;</li> <li>- Achievable gold recovery from ore processing;</li> <li>- Mining costs, comprised of industry current mining contractor rates and mine owner historical/current costs;</li> <li>- Historic surface ore haulage contractor pricing;</li> <li>- Current ore processing costs; and Royalties</li> </ul>

Criteria	JORC Code (2012) explanation	Commentary
Mining factors or assumptions	<p><i>The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).</i></p> <p><i>The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.</i></p> <p><i>The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.</i></p> <p><i>The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).</i></p> <p><i>The mining dilution factors used.</i></p> <p><i>The mining recovery factors used.</i></p> <p><i>Any minimum mining widths used.</i></p>	<p>Estimation of the Ore Reserve was completed by detailed design of underground mining areas. Updated detailed mine designs were completed to honour the 31 March 2021 Mineral Resource estimates for the Beresford and Allanson deposits.</p> <p>The Beresford and Allanson deposits has been successfully mined via top-down long hole open stoping with pillars utilising conventional mining equipment in the Westralia underground mine area since January 2018.</p> <p>The mining method selected is top-down open stoping with pillars. Mining geometries and geotechnical conditions expected in the current Ore Reserve estimate are suitable for ongoing use of this method. This is a continuation of the existing mining method and is aligned with the selected method from previous studies.</p> <p>The mining method generally accesses the orebody via a 1:7 gradient decline centrally located along strike in the footwall of the orebody for Beresford deposit and in the hangingwall for Allanson. Ore drives are mined along strike from a central level access and uphole stoping retreats to this central access. Rib and sill pillars are placed based on maximum hydraulic radius.</p> <p>The study geotechnical parameters are based on the Dacian's Ground Control Management Plan (GCMP) which is informed by stoping and geotechnical performance observed from May 2017 through to August 2020 and supported by independent geotechnical analysis completed during the 2016 DFS Mining Study.</p> <p>Sublevel spacing is 20m (floor-to-floor). Mining recovery taking into account stope size and rib/sill pillars for Beresford is 82% and Allanson 79%.</p> <p>The Westralia Ore Reserve is based on the Beresford and Allanson Mineral Resource models as at 31 March 2021, the results of which were announced to the ASX on 11 May 2021.</p> <p>Underground stopes have been designed to an assumed minimum mining width of 1.1m based on practical blast hole diameters and spacing, explosive types and operating performance observed within the mining area to date. A dilution "skin" of 0.2m on both the hangingwall (HW) and footwall (FW) has been applied to the designed stope shapes to account for blast-induced over-break in line with previous studies based on geotechnical analysis.</p> <p>Historic stope performance of all stopes mined to date have informed the dilution modifying factors applied to the Westralia Ore Reserve estimation. Additional dilution factors in excess of the 0.2m "skin" have been applied. These factors range from 5%-16% for individual lodes within the mines.</p> <p>A 5% dilution factor has been applied to the lateral development component of the Ore Reserve estimate at zero grade.</p> <p>Mining recovery for stopes has been estimated at 95% and is in addition to allowances made for in-situ rib and sill pillars required to maintain stope void stability.</p>

Criteria	JORC Code (2012) explanation	Commentary
		<p>Mining recovery of 95% has been applied to the lateral development.</p> <p>All stopes are designed using Deswik Stope Optimiser at 1.1m Minimum Mining Width (MMW). The designed stope was expanded by 0.2m on the HW &amp; FW to include the dilution skin.</p>
<i>Mining factors or assumptions</i>	<p><i>The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.</i></p> <p><i>The infrastructure requirements of the selected mining methods.</i></p>	<p>Inferred Mineral Resource material contained within stope designs has been treated as waste within the Ore Reserve.</p> <p>Ore drives have been designed in 3.0m segments to represent advance length per cut. Development cuts containing &gt;50% Measured or Indicated Mineral Resource material have been included in the Ore Reserve, otherwise they are treated as waste rock.</p> <p>The proposed mine design includes expansion of existing underground infrastructure as required for ventilation, power, dewatering, and mining services. There are no additional surface or significant underground infrastructure requirements other than extensions of services to support mine development</p>
<i>Metallurgical factors or assumptions</i>	<p><i>The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.</i></p> <p><i>Whether the metallurgical process is well-tested technology or novel in nature.</i></p> <p><i>The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.</i></p> <p><i>Any assumptions or allowances made for deleterious elements.</i></p> <p><i>The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.</i></p>	<p>The Mt Morgans process plant was commissioned in late March 2018 and includes a Semi Autogenous Grinding, Ball Milling and Pebble Crushing (SABC) comminution circuit followed by conventional gravity and carbon-in-leach (CIL) process.</p> <p>The metallurgical process is commonly used in Western Australian and international gold mining. The same process configuration was previously utilised at Mt Morgans during the 1990s.</p> <p>A metallurgical test work program was completed during the 2016 DFS using samples from diamond drill core and RC drill chips to determine:</p> <ul style="list-style-type: none"> <li>- physical properties for comminution circuit design;</li> <li>- optimal grind size; and</li> <li>- gold recovery.</li> </ul> <p>Since the process plant was commissioned in late March 2018, a total of 6.7Mt (dry) was milled until the end of August 2020 when production from the Westralia underground mine ceased. The average gold recovery over this period for a blended feed was 92.9%.</p> <p>A gold recovery of 92.7% has been used for calculated break-even cut-off grades for Ore Reserve estimation for all underground deposits.</p> <p>No deleterious elements were identified from the mineralogical/metallurgical assessments carried out during the 2016 DFS and evidence of such was not observed during the period March 2018 to August 2020 when ore from the Beresford and Allanson deposits was processed.</p> <p>In addition to processing ore from the Beresford and Allanson deposits as a component of the mill feed blend from March 2018 through to August 2020, under previous owners approximately 10Mt of ore was treated through the historic Mt Morgans treatment plant during the 1990s. This included BIF-hosted ore mined from the Westralia</p>

Criteria	JORC Code (2012) explanation	Commentary
	<i>For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?</i>	<p>underground mine. The average recovery during the 10 year period was 91.4%.for 740,000 ounces produced.</p> <p>A total of 6.7 Mt of ore has been treated through the new Mt Morgans process plant from commissioning in March 2018 to the end of August 2020. Gold recovery has averaged 92.9%.</p> <p>Not Applicable</p>
Environmental	<p><i>The status of studies of potential environmental impacts of the mining and processing operation.</i></p> <p><i>Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.</i></p>	<p>All regulatory approvals and permits have been granted for ongoing mining and processing at Mt Morgans, including mining of the Westralia underground.</p> <p>Westralia waste rocks are characterised as non-acid forming (NAF). The current location of waste rock landform was selected based on proximity to operations and so that there is minimal disturbance to previously rehabilitated landforms.</p> <p>Process plant tailings are characterised as NAF with the exception of ore from the Allanson deposit which is considered potentially acid forming, however, it accounts for less than ~5% of project tails volume.</p>
Infrastructure	<i>The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.</i>	<p>Mt Morgans is located in the immediate vicinity of the Laverton and Leonora townships and is within driving distance of Kalgoorlie, a major regional hub. Access to the site is via sealed public highways and public and private unsealed roads.</p> <p>The site workforce is primarily fly-in, fly-out (FIFO) from Perth via the public Laverton airport.</p> <p>The Mt Morgans site is well established with a modern processing plant, associated 16.5MW gas fired power station, bore field and tailings storage facility; a 400 person capacity accommodation village; administration offices; workshops; reverse osmosis and waste water treatment plants.</p>
Costs	<p><i>The derivation of, or assumptions made, regarding projected capital costs in the study.</i></p> <p><i>The methodology used to estimate operating costs.</i></p> <p><i>Allowances made for the content of deleterious elements.</i></p> <p><i>The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.</i></p> <p><i>The source of exchange rates used in the study.</i></p>	<p>Projected sustaining capital costs for the Westralia Ore Reserve are based on industry current mining contractor rates with respect to mine development. There are no significant infrastructure capital costs outside of standard mine development costs.</p> <p>Operating costs for the Westralia Ore Reserve have been estimated using industry current mining contractor rates, current processing costs and estimated mine owner costs.</p> <p>No deleterious elements were identified from the mineralogical/metallurgical assessments carried out during the 2016 DFS and evidence of such was not observed during the period March 2018 to August 2020 when ore from the Beresford and Allanson deposits was processed.</p> <p>Break-even financial analysis has been performed at a gold price of AUD\$2100.</p> <p>All revenue and cost calculations have been completed using Australian Dollars, hence application of an exchange rate has not been required.</p>

Criteria	JORC Code (2012) explanation	Commentary
	<p><i>Derivation of transportation charges. The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.</i></p> <p><i>The allowances made for royalties payable, both Government and private.</i></p>	<p>Transportation and refining charges are based on current contract pricing applicable to Mt Morgans.</p> <p>The 2.5% Western Australian State Government royalty has been allowed for.</p>
Revenue factors	<p><i>The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.</i></p> <p><i>The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.</i></p>	<p>Ore production and gold recovery estimates for revenue calculations were based on detailed mine designs, mine schedules, mining factors and cost estimates for mining and processing.</p> <p>A gold price of AUD\$2100 has been used for economic analysis.</p>
Market assessment	<p><i>The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.</i></p> <p><i>A customer and competitor analysis along with the identification of likely market windows for the product.</i></p> <p><i>Price and volume forecasts and the basis for these forecasts.</i></p> <p><i>For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.</i></p>	<p>There is a transparent quoted market for the sale of gold.</p> <p>No industrial minerals have been considered.</p>
Economic	<p><i>The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.</i></p> <p><i>NPV ranges and sensitivity to variations in the significant assumptions and inputs.</i></p>	<p>The Westralia Ore Reserve update is based on industry current mining contractor costs, current processing costs and estimated mine owner costs. A cash flow analysis was completed for each mine area with all applicable operating and capital costs applied to determine break-even gold grades.</p> <p>Cost modeling of the Ore Reserves Update yielded a positive NPV.</p> <p>Sensitivity analysis has been carried out and the Ore Reserve Estimate is most sensitive to mined grade, gold price, and stope dilution/recovery.</p>
Social	<p><i>The status of agreements with key stakeholders and matters leading to social licence to operate.</i></p>	<p>Mt Morgans is an operating mine site and has good working relationships with neighboring stakeholders.</p> <p>Granted tenements of types appropriate to the activities performed cover all areas of Mining Operations.</p> <p>The Nyalpa Pirniku Native Title Claim was accepted for registration on 15 May 2019. The Claim covers the majority of the Mt Morgans tenements, including Mining Lease M39/18 within which the Beresford and Allanson deposits are located. Native Title is yet to be determined, and in the case that it is granted, it is not expected to impact mining of the Beresford and Allanson deposits, as M39/18 pre-dates the Claim.</p>
Other	<p><i>To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:</i></p> <p><i>Any identified material naturally occurring risks.</i></p>	<p>There are no likely identified naturally occurring risks that may impact the Project.</p>



Criteria	JORC Code (2012) explanation	Commentary
	<p><i>The status of material legal agreements and marketing arrangements.</i></p> <p><i>The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.</i></p>	<p>A Letter of Intent has been issued to an underground mining contractor and contractual negotiations are currently being finalised for recommencement of mining the Westralia underground in September 2021. All other material services and supply of goods required for the Mt Morgans operation are in place.</p> <p>All regulatory approvals and permits have been granted for ongoing mining and processing at Mt Morgans, including recommencement of the Westralia underground mine.</p>
Classification	<p><i>The basis for the classification of the Ore Reserves into varying confidence categories.</i></p> <p><i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i></p> <p><i>The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).</i></p>	<p>The classification of the initial Ore Reserve has been carried out in accordance with the JORC Code 2012.</p> <p>The Ore Reserve results reflect the Competent Persons view of the deposits.</p> <p>The Probable Ore Reserve is based on that portion of Indicated Mineral Resource within the mine designs that may be economically extracted and includes allowance for dilution and ore loss.</p> <p>The Proved Ore Reserve is based on that portion of Measured Mineral Resource within the mine designs that may be economically extracted and includes allowance for dilution and ore loss.</p>
Audits or reviews	<p><i>The results of any audits or reviews of Ore Reserve estimates.</i></p>	<p>The Westralia Ore Reserve estimate update was completed by mining consultants Orelogy Pty Ltd and was subject to internal peer review by both Orelogy and employees of Dacian Gold Ltd.</p>
Discussion of relative accuracy confidence	<p><i>Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.</i></p> <p><i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i></p> <p><i>Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.</i></p>	<p>The Ore Reserve estimate for the Westralia underground mine has been prepared within the guidelines of the 2012 JORC Code.</p> <p>Detailed mine designs and schedules; application of Modifying Factors for ore loss, dilution and ore processing gold recovery; and subsequent financial analysis has been used to estimate Ore Reserves, which in the opinion of the Competent Persons provide for a good level of confidence.</p>



Criteria	JORC Code (2012) explanation	Commentary
	<i>It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available</i>	