

Springdale graphite performs exceptionally in battery anode material benchmark tests

Highlights:

- Springdale Graphite Project material has performed exceptionally in test programs at a specialist facility in Germany
- Results from micronisation, spheronisation and purification met industry specification for battery anode material with purification up to 99.99% graphite content achieved
- The graphite also performed exceptionally in jet milling tests – Jet milled graphite products can also achieve premium prices in graphite markets
- Comet is engaged in discussions with multiple parties regarding commercial options for the Springdale Graphite Project

Comet Resources Ltd (Comet or the Company) (ASX:CRL) is pleased to provide the results of specialist test work on natural flake graphite from its Springdale Graphite Project (Springdale) located in Western Australia. The test work results demonstrated the suitability of Springdale's graphite to undergo micronisation (in hammer mills), spheronisation and purification processes to the high specification levels necessary to produce precursor material for use in the manufacture of lithium-ion battery anodes. Additional test work will be conducted to optimise the results of the already impressive initial test results.

In addition, the Springdale graphite sample was also tested for performance in jet milling. Due to the fine flake size, the material was easy to micronise in a jet mill with good throughput and low energy consumption. The product was assessed as achieving industry standards for jet mill specification. Jet milled product, like lithium-ion battery anode precursor material, can also achieve premium pricing in graphite markets.

The results of the test work confirm Springdale's graphite material is high-value and suitable for value added processing, a key factor for future project economics. No graphite project will produce 100% lithium-ion battery anode precursor material, so it is therefore necessary to have other high-value saleable graphite products for the balance of the graphite produced to achieve the highest average revenue mix. The Company considers it exceptional that Springdale's graphite product has also performed well in jet milled tests, in addition to testing for generation of lithium-ion battery anode precursor materials.

Comet Managing Director, Matthew O'Kane, commented, ***"The results from the specialist test programs in Germany are fantastic! They confirm graphite material from Springdale has met key battery anode grade benchmarks as well successfully producing high-value jet milled product. These results greatly increase the prospects for future development of the project. We will now assess future work programs, which include work to further optimise the processing of spherical graphite. With the continued push towards electrification, demand for these battery anode grade products should grow exponentially."***

Summary of test programs:

Analysis of the dried concentrate material prior to testing:

The concentrate material is a very fine graphite product. As a commercial grade, the concentrate would meet the specification of grade -200 mesh, the finest standard grade for flake graphite.

The loss on ignition (LOI) value of the concentrate material is relatively high at 95% (Carbon content), while fraction analysis showed that the LOI content is relatively similar for all size fractions, indicating successful results from flotation in the production of the concentrate.

The mean particle size, measured by laser analysis, was approximately 30 microns. The specific surface area is higher, however the density was lower when compared to a Chinese standard -200 mesh product.

The oxidation resistance of the product was measured by thermogravimetric analysis. A relatively low oxidation resistance was measured, which is likely due to the relatively high surface area.

Jet Milling and Impact Milling value added graphite products:

In the jet mill, the graphite concentrate processed very well. The throughput was high, and the energy consumption was low. The products from jet milling, as confirmed by laser analysis, appear very typical for this product category. The normal range of jet mill products can therefore be produced with Springdale concentrate as feed material. All properties are in line with common standards for jet milled, with only the density after milling being lower than for normal jet milled product. This lower density may make Springdale jet milled product well suited to applications related to conductivity, where lower density products perform better.

Impact milling was carried out with a hammer mill. Again, the concentrate was used as feed material. After several samples runs stable values were achieved, and it is assumed that stable processing will also be possible in commercial production. All the properties of the product from the impact mill are quite normal, except for the density, which is also lower here, although not as low as in the case of the jet milled product.

Purified Spherical Graphite - Battery Anode Material (BAM):

Micronisation:

As a first step, micronised graphite was produced without issue. Grinding tests were undertaken with the impact (hammer) mill, with two samples of an average particle size of 20 and 14 microns being produced in larger quantities. These two size fractions were then used as feed material for the spheronisation test work.

Spheronisation:

The material performed well during spheronisation. It was possible to get spherical graphite with acceptable properties for battery anode material with relative ease. The particle size distribution of the spheronized material is typical for spherical graphite. The ratio between d90 and d10 particle diameters is acceptable. With a further optimization, all standard target sizes (d50 values) for spherical graphite can likely be achieved exactly. This will be part of the future optimisation test work. Various pictures were taken of the spherical graphite using a scanning electron microscope (SEM). The SEM pictures of the spherical graphite 20 micron (SPG 20) and spherical graphite 14 micron (SPG 14) show that the material consists mainly of very well-rounded graphite spheres, which is very positive. The distribution of different particle sizes is rather narrow, producing a relatively homogenous product, which is also desirable.

The tap density is lower than best specification. A high tap density is preferred as it results in batteries with higher capacities. More optimisation test work will be undertaken to see if the tap density can be increased further. This optimisation test work will be undertaken both during production of the graphite concentrate, and also during processing into spherical graphite product.

The yield is relatively low at present compared to other graphite. Normally it is possible to achieve yields approximately 50%. The yield for the Springdale material was in the 30 to 40%

range. It is probably the high proportion of fines in the feed product that is separated off by the classifier which generates the lower yield. This will also undergo optimisation in future testing to improve yields.



Picture 1: SEM image of 20 micron spherical graphite

Purification:

After the spheronisation was completed a sample of the material was first purified with an intensive alkaline method, based on a caustic roasting process. The purification went well. An LOI value of 99.96% (carbon content) was measured in the purified product, which is above the general minimum specification for spherical graphite of 99.95%.

Assay of the purified material was then undertaken using the Inductively Coupled Plasma (ICP) technique. Essentially all elements present in the gangue are at a low level after the purification, especially the critical detrimental elements for use in batteries, such as Iron, Silicon, Chromium and Copper, which were measured at levels below the typical specification limits for BAM. Three element assays were slightly elevated, Sodium, Nickel and Calcium. Sodium is very likely a residue from the alkaline digestion (Sodium Hydroxide) and can presumably be reduced significantly by further optimization of the purification process. The same applies for Nickel, which is most probably coming from the Nickel crucible used during purification. The only element which was found in higher concentration than usual was

Calcium. Presumably, a modified acid treatment can lower the Calcium value. Often a limit of 25 ppm is given for Ca. This should be achievable without great effort.

A second sample of material was then purified using Hydrofluoric Acid (HF). LOI value was measured at 99.99% (carbon content) in the HF purified product, better than the alkaline method, and nearly 100% pure carbon content. ICP assay of the HF purified material is presently underway and results will be reported once received.

Testing Background:

Test work completed initially in 2019 and 2020 identified that graphite concentrate from Springdale, in particular in the high grade area of the resource, was quite a unique product due to its very fine size fraction, and also due the platy nature of the fine flake. Recognising that these properties may potentially have applications for BAM, a decision was made earlier in 2021 to generate a bulk sample of graphite concentrate to send to Germany for evaluation by a specialist graphite test facility. This press release details the results of that testing regime.

Consultants Engaged:

The design of the process flowsheet to produce the concentrate, and the preparation of the graphite concentrate itself, was performed by Independent Metallurgical Operations (IMO) in Perth, Australia. The concentrate was then shipped to ProGraphite GmbH in Untergriesbach, Germany, where the testing programs detailed in this press release were completed.

Commercial Engagement:

The Company is presently engaged in discussions with multiple downstream users of graphite products regarding the Springdale Graphite Project. Detailed results from the testing programs described in this press release have been shared under confidentiality agreements and management is engaged in ongoing discussions.

This announcement has been authorised by the Board of Comet Resources Limited

For further information please contact:

MATTHEW O'KANE

Managing Director

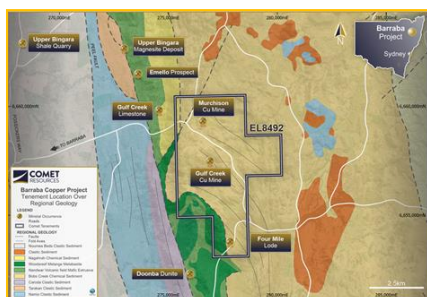
-  (08) 6489 1600
-  comet@cometres.com.au
-  cometres.com.au
-  Suite 9, 330 Churchill Avenue Subiaco WA 6008
-  PO Box 866 Subiaco WA 6904

About Comet Resources



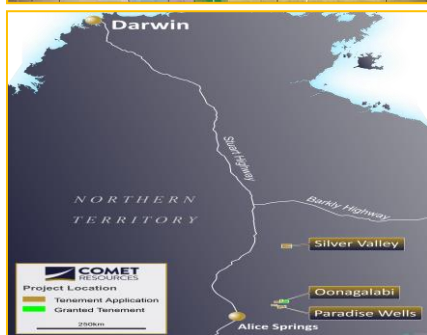
Santa Teresa Gold Project (Mexico)

The Santa Teresa Gold Project is comprised of two mineral claims totalling 202 hectares located in the gold rich El Alamo district, approximately 100 km southeast of Ensenada, Baja California, Mexico; and 250 km southeast of San Diego, California, USA. The Project is prospective for high grade gold. In addition to the two claims of the Project, two additional claims totalling a further 378 hectares in the surrounding El Alamo district are being acquired from EARL.



Barraba Copper Project (NSW)

The 2,375ha exploration license that covers the project area, EL8492, is located near the town of Barraba, approximately 550km north of Sydney. It sits along the Peel Fault line and encompasses the historic Gulf Creek and Murchison copper mines. The region is known to host volcanogenic massive sulphide (VMS) style mineralisation containing copper, zinc, lead and precious metals. Historical workings at Gulf Creek produced high-grade copper and zinc for a short period around the turn of the 19th century, and this area will form a key part of the initial exploration focus.



Northern Territory Projects (NT)

The portfolio of Northern Territory exploration licenses and exploration license applications covers an area of approximately 840km². Although historical exploration results were indicative of near surface gold and copper mineralisation, very limited modern exploration has occurred. Comet plans to utilise modern exploration techniques to rapidly advance the scale of known mineralisation, especially where known geophysical and geochemical anomalies exist that have not been comprehensively drill tested.



Springdale Graphite Project (WA)

The 100% owned Springdale graphite project is located approximately 30 kilometres east of Hopetoun in South Western Australia. The project is situated on free hold land with good access to infrastructure, being within 150 kilometres of the port at Esperance via sealed roads. The tenements lie within the deformed southern margin of the Yilgarn Craton and constitute part of the Albany-Fraser Orogen. Comet owns 100% of the three tenement's (E74/562 and E74/612) that make up the Springdale project, with a total land holding of approximately 198 square kilometres.

Competent Persons Statement

The information in this report that relates to Mineral Resources and metallurgical test work conducted on sample material from the Mineral Resource is based on information compiled by Matthew Jones, who is a Competent Persons and Member of The Australasian Institute of Mining and Metallurgy. Matthew Jones is a consultant and was previously Exploration Manager of the Company. He has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Matthew Jones consents to the inclusion in this report of the matters based on their information in the form and context in which it appears.

Forward-Looking Statement

This announcement includes forward-looking statements. Forward-looking statements include, but are not limited to, statements concerning Comet Resources Limited's planned exploration programs, corporate activities and any, and all, statements that are not historical facts. When used in this document, words such as "could," "plan," "estimate," "expect," "intend," "may", "potential," "should" and similar expressions are forward-looking statements. Comet Resources Limited believes that its forward-looking statements are reasonable; however, forward looking statements involve risks and uncertainties and no assurance can be given that actual future results will be consistent with these forward-looking statements. All figures presented in this document are unaudited and this document does not contain any forecasts of profitability or loss.

JORC Code, 2012 Edition – Table 1

Section 1. Sampling Techniques and Data

(Criteria listed in the preceding section also apply to all succeeding sections)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information. 	<ul style="list-style-type: none"> Diamond drilling was done to collect adequate samples for metallurgical and ore characterisation testwork. Individual sample intervals including graphitic zones were sampled based on logged geology intervals and can vary from 0.3m to 1.5m with the majority of samples at 1m intervals. Samples were ¼ PQ3 or ¼ HQ3 core and were cut and sampled at Nagrom Labs from Comet specified cut sheets using either an automatic diamond core saw where competent, or manually by hand using a paint scraper, where soft and friable (oxidised clays). Core was first cut in half lengthwise and then one half was cut in half again for the ¼ core sample. This produced an approximate 2kg sample which is considered representative of the full drill metre interval sampled. Drill samples selected for analysis were limited to those containing visible graphite, together with a one to two metre buffer of barren country rock. Graphite quality and rock classifications were visually determined by field geologist. Metallurgical test samples of ¾ PQ diameter core were visually selected from mineralised intervals of HD024 and HD031. The samples represent typical mineralised zones drilled within the project area.
Drilling techniques	<p>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</p>	<ul style="list-style-type: none"> Diamond Drilling (DD) was conducted with Rotary Mud (MR) pre-collars. DD and RM was completed by DDH1 Drilling using a track mounted Sandvik DE710 diamond rig (Rig 42). Core size was PQ3 (85mm diameter) and HQ3 (61.1mm diameter) triple tube system. All inclined core holes were oriented using a True Core PQ or HQ orientation tool, TC0999/TC0156. Due to the deeply oxidized nature of the core not all orientations were successful, so the majority of the core remains un-orientated. Where orientated successfully dip and dip direction structural measurements were collected using a rocket launcher style CORE Orientation device or cradle.
Drill sample recovery	<ul style="list-style-type: none"> Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material. 	<ul style="list-style-type: none"> DD Sample recovery was measured and recorded for each core run. Downhole depths were validated against core blocks and drillers sheets. DD core recoveries were good in fresh and moderately weathered material. Core recovery was reduced in some instances in highly weathered clay zones and this was recorded in sampling details. Twin hole comparison of RC vs Diamond Indicated that there is no sample bias for graphite assays There does not appear to be any relationship between sample recovery and grade.
Logging	<ul style="list-style-type: none"> Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. 	<ul style="list-style-type: none"> All drillholes were geologically logged in full by an independent geologist. MR pre-collars were bagged from the collar water and logged but not sampled. All data is initially captured on paper logging sheets



	<ul style="list-style-type: none"> • Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. • The total length and percentage of the relevant intersections logged. 	<ul style="list-style-type: none"> • and transferred to pre-formatted excel tables and loaded into the project specific drillhole database. • The logging and reporting of visual graphite percentages on field logs is semi-quantitative. A reference to previous logs and assays is used as a reference. • All logs are checked and validated by an external geologist before loading into the database. Logging is of sufficient quality for current studies.
<p>Sub-sampling techniques and sample preparation</p>	<ul style="list-style-type: none"> • If core, whether cut or sawn and whether quarter, half or all core taken. • If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. • For all sample types, the nature, quality and appropriateness of the sample preparation technique. • Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. • Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. • Whether sample sizes are appropriate to the grain size of the material being sampled. 	<ul style="list-style-type: none"> • All sampling was carefully marked up on core and core trays (where oxidised and difficult to write on) with paint markers and photographed before core trays were sent to the Nagrom for cutting and sampling. • Diamond core samples were cut lengthwise using a manual core saw. The core was cut in half, and then one half was quartered to provide samples for metallurgical testwork and assaying respectively. One quarter core is kept for reference in the trays. • Individual ¼ core samples were collected in labelled foil trays and prepped as below. • Duplicate samples were inserted at the NAGROM Lab in Perth using a coarse crushed split of the specified sample interval. Coarse duplicates were inserted approximately 1:25 samples. • Samples sizes are considered appropriate and representative of graphite material being sampled.
<p>Quality of assay data and laboratory tests</p>	<ul style="list-style-type: none"> • The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. • For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. • Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established. 	<ul style="list-style-type: none"> • Analysis was completed at Nagrom and IMO • Quarter core analytical samples were separately coarse crushed to a nominal topsize of 6.3mm (CRU01), dried at 105°C (DRY01), and where over 2.5kg riffle split (SPL01). • The sample is then pulverised to 80% passing 75µm (PUL01). • A LabfitCS2000 combustion /IR analyser was used for Graphitic Carbon analysis (0.1 % to 100% detection limits). • Graphitic Carbon (TGC; CS003, 0.1% lower detection), Total Carbon (TC; CS001, 0.1% detection limit) and Total Sulphur (TS; CS001, 0.1% detection limit) is analysed by Total Combustion Analysis. • For TC and TGC, the prepared sample is dissolved in HCl over heat until all carbonate material is removed. The residue is then heated to drive off organic content. The final residue is combusted in oxygen with a Carbon-Sulphur Analyser and analysed for Total Graphitic Carbon (TGC) and Total Carbon (TC). • Sample size is appropriate for the material being tested. • QC measures include duplicate samples, blanks and certified standards (1:20) • CRL is confident that the assay results are accurate and precise and that no bias has been introduced.
		<ul style="list-style-type: none"> • All data is initially captured on paper logging sheets and transferred to pre-formatted excel tables and loaded into the project specific drillhole database. Paper logs are scanned and stored on the companies server. Original logs are stored in the Perth office. • Assay data is provided as .pdf and .csv files from the laboratory and entered into the project specific drillhole database. Spot checks are made against the laboratory certificates. • No adjustments have been made to assay data.

Location of data points	<ul style="list-style-type: none"> Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. Specification of the grid system used. Quality and adequacy of topographic control. 	<ul style="list-style-type: none"> Collar positions were set out using a handheld Garmin GPS with reported accuracy of 5m and reported using MGA94 Zone 51. Two pegs were lined up using a Suunto sighting compass and a tape laid out on the ground between the pegs to align the rig. Drillers also checked rig alignment with the non-magnetic AXIS CHAMP GYRO. A final collar position was recorded using a handheld Garmin GPS. For inclined holes downhole surveys (dip and azimuth) were taken using a non-magnetic AXIS CHAMP GYRO Serial number 13232
Data spacing and distribution	<ul style="list-style-type: none"> Data spacing for reporting of Exploration Results. Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. Whether sample compositing has been applied. 	<ul style="list-style-type: none"> In the Northern Zone previous drilling has been completed on 100 – 200m spaced drill lines roughly perpendicular to strike with holes nominally 30m apart. The 2019 DD holes were designed as cross twin metallurgical holes and are thus not on a pre-determined grid spacing. New drilling range from 5m to 40m from existing drilling and are considered infill. In the Western Zone previous drilling has been completed on 80 – 200m spaced drill lines roughly perpendicular to strike with holes nominally 30m apart. A single hole was drilled as a 40m step out from a previous intersection. No sample compositing has been done.
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material. 	<ul style="list-style-type: none"> Drilling indicates that the graphite-rich stratigraphy is part of a kilometre-scale syncline with the western limb striking at around 034° and dipping between 50° to 75° to the SE and the eastern limb dipping shallow to moderately (around 30°) to the SW. The dip and strike of stratigraphy in the fold closure is variable but shallows significantly from 15° to 40° to the south. Drillholes were planned to intersect the lithology/mineralisation at right angles or as close as possible to right angles. The folded nature of the stratigraphy and lack of previous structural information in the North zone resulted in two of the twin holes appearing to have been drilled sub-parallel of structures. These holes are clearly identified in reporting of results.
Sample security	<ul style="list-style-type: none"> The measures taken to ensure sample security. 	<ul style="list-style-type: none"> Whole core in PQ and HQ trays was sent to Nagrom Labs in Perth on pallets for cutting and sampling with no core sampling conducted in the field. All trays and pallets were photographed and documented before leaving site. Core trays were stacked and securely strapped on pallets and then delivered by CRL field personnel from Springdale to Freight Lines Group (FLG) Depot in Ravensthorpe. Consignment notes were completed and signed on handing over the pallets to FLG. FLG then transported the core pallets directly to Nagrom Labs in Perth. Comet Exploration Manager visited Nagrom in Perth and verified all core was present and undisturbed. At Nagrom, cut samples were logged and barcode scanned throughout the analytical process.
Audits or reviews	<ul style="list-style-type: none"> The results of any audits or reviews of sampling techniques and data. 	<ul style="list-style-type: none"> External geological consultants conducted site visits in September 2019 during the drilling program to observe all drilling. All procedures were considered industry standard, well supervised and well carried out.

Section 2. Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area. 	<ul style="list-style-type: none"> Exploration tenements E74/562 and E74/612 are current and 100% owned by Comet Resources Ltd. The licences are over freehold land with sealed road access 20km away. The company is not aware of any impediments relating to the licence or area.
Exploration done by other parties	<ul style="list-style-type: none"> Acknowledgment and appraisal of exploration by other parties. 	<ul style="list-style-type: none"> Unpublished and verbal reports of graphite mineralisation encountered in shallow calcrete/limestone drilling and extractive industry operations at the Springdale Project.
Geology	<ul style="list-style-type: none"> Deposit type, geological setting and style of mineralisation. 	<ul style="list-style-type: none"> The Springdale Project overlies an underexplored remnant Archaean greenstone belt within the Archaean Munglinup Gneiss. The greenstone belt (Jerdacuttup Greenstone Belt) is located within the deformed southern margin of the Yilgarn Craton and constitutes part of the Northern Foreland lithotectonic unit of the Albany-Frazer Orogen. Graphite mineralisation is hosted within metamorphosed Archaean mafic, granitic and sedimentary rocks. A high-resolution aeromagnetic survey flown in September 2017 showed that stratigraphy is tightly folded with NE-trending fold axes and that graphite-rich stratigraphy is strongly associated with units of low magnetic response in the project area. Drilling has revealed that the graphite-rich stratigraphy is part of a kilometre-scale syncline with the western limb striking at around 034° and dipping moderately (around 50°) to the SW and the eastern limb striking at around 176° and dipping shallow to moderately (around 30°) to the SE. The dip of stratigraphy in the fold hinge shallows significantly to 15°-20° to the south.
Drill hole information	<ul style="list-style-type: none"> A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length. If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case. 	<ul style="list-style-type: none"> The collar information for holes commented on in this release have been reported previously in ASX releases on the 24/10/2019 (Outstanding Graphite Results from Latest Diamond Drilling) and 25/11/2020 (West Zone Hole Confirms High Grade Graphite Continuity).
Data aggregation methods	<ul style="list-style-type: none"> In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. 	<ul style="list-style-type: none"> Intersections are calculated as weighted averages, using a 1% TGC cutoff and maximum 1m consecutive internal waste. No upper cut as used.

	<ul style="list-style-type: none"> The assumptions used for any reporting of metal equivalent values should be clearly stated. 	
Relationship between mineralisation widths and intercept lengths	<ul style="list-style-type: none"> These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known'). 	<ul style="list-style-type: none"> The bedrock geology comprises highly deformed gneiss and associated metamorphic lithologies. Exploration to date is still insufficient to quantify the amount of deformation and therefore to determine the true dip and strike of lithology with any precision at any given point in space. All attempts to orient drilling perpendicular to the dip direction are made but cannot be guaranteed. As such, true thickness are difficult to estimate. All intersections are therefore reported as downhole only.
Diagrams	<p>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</p>	<ul style="list-style-type: none"> Relevant maps reported previously in ASX releases on the 24/10/2019 (Outstanding Graphite Results from Latest Diamond Drilling) and 25/11/202 (West Zone Hole Confirms High Grade Graphite Continuity).
Balanced reporting	<ul style="list-style-type: none"> Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results. 	<ul style="list-style-type: none"> Plans and sections that show spatially relevant information in an unbiased and balanced manner have been presented previously in ASX releases on the 24/10/2019 (Outstanding Graphite Results from Latest Diamond Drilling) and 25/11/202 (West Zone Hole Confirms High Grade Graphite Continuity). Graphitic carbon assays for all intervals sampled were also provided in the releases.
Other substantive exploration data	<ul style="list-style-type: none"> Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances. 	<ul style="list-style-type: none"> Previous announcements by the company include a maiden JORC 2012 graphite resource (ASX 6/12/2018) Graphite characterisation results (ASX: 29/06/2016), and initial graphene metallurgy (ASX: 4/04/201, 10/01/2018, and 17/09/2018). Drill assay results (6/04/2016, 27/09/2016, 2/11/2016, 15/11/2016, 9/02/2017, 15/09/2017, 6/11/2017, 10/11/2017, 12/12/2017, 6/03/2018, 13/03/2018, 17/04/2018, 8/5/2018, 2/10/2018, 7/05/2019, 18/6/2019, 24/10/2019, 25/11/2019). The dominant activity undertaken in the period covered by this announcement was metallurgical testwork aimed at testing how graphite concentrate from the high grade zone of the Springdale Graphite Project performed in tests designed to assess its ability to process into battery anode precursor material, and other value added products using fine graphite as the feed material. The work was undertaken on a composite sample prepared from two intervals, one being 6m from 26 – 32m from hole HD031 and 43.7m from 42 – 85.7m from hole HD024. These intervals represent shallow, high-grade graphite mineralisation that Comet believes has the potential for economic extraction via open pit mining methods. The sample material was delivered to Metallurgy Pty Ltd (Metallurgy) metallurgical laboratory with the testwork managed by metallurgical experts, Independent Metallurgical operations (IMO). Metallurgy received the prepared composite from Comet Resources as 2kg charges stage crushed to 100% passing 3.35mm. Twenty Five of the 2kg charges were combined and blended, with 40 kg representatively sub-sampled prior to stage grinding and undergoing several flotation and regrinding stages, respectively utilising a standard Denver flotation cell and vertical stirred regrind mill. Specialist reagent Ekofol-452G was utilized to conduct the flotation testing. Resulting flotation concentrates were sized at industry standard sizes, dried and submitted for total carbon and loss on ignition assay to determine the



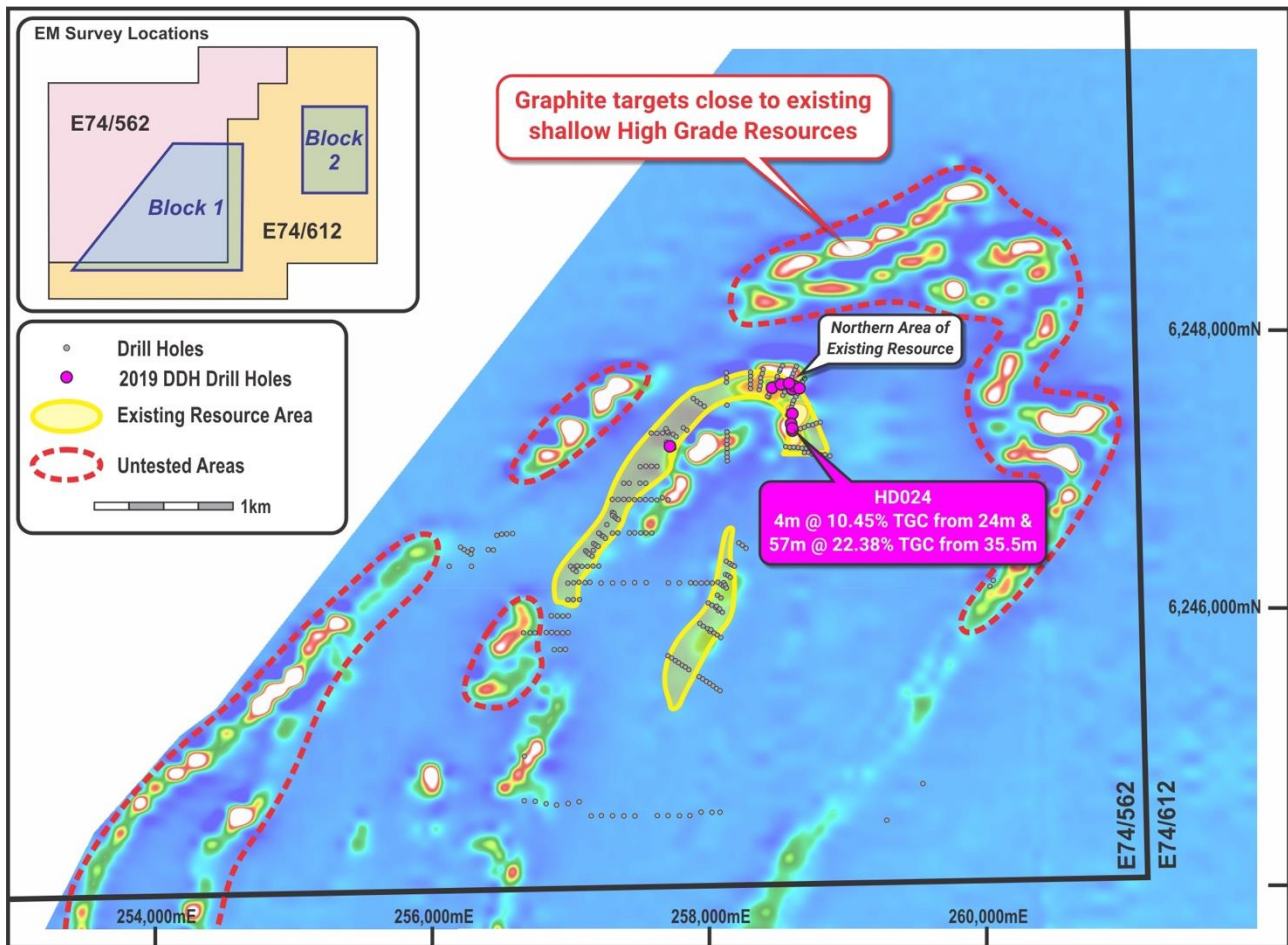
		<p>graphite content of each size fraction.</p> <ul style="list-style-type: none"> • A Bulk sample of approximately 13kg of concentrate was then sent to ProGraphite GmbH in Untergriesbach, Germany for testing. • Upon arrival at ProGraphite the concentrate material was dried. This material was then subsequently used for all test work. • A sample of the dried material was first classified and sized. The material is a very fine size fraction and would be categorised as -200 mesh product on the Chinese classification system. The material has a d50 of 29.3 microns. LOI of the material was 95.10%. • Jet milling was carried out with an AFG jet mill from Hosokawa Alpine. The dried concentrate was used as feed material. The material processed very well. The throughput was high and the relative energy consumption low. The products from jet milling look very typical for this product category. This was also confirmed by the laser analyses. Density of the product is lower than for other jet milled products. • Impact milling was carried out with a hammer mill. Again, the dried concentrate was used as feed material. After a number of trials, stable values were achieved, and ProGraphite assume that stable processing will also be possible in commercial use. <p>Spheronisation and purification:</p> <ul style="list-style-type: none"> • Micronizing was completed by using an impact mill with an internal classifier. The mill operates in a continuous mode, i.e. the amount of graphite in the grinding chamber is kept on a constant level. The amount of graphite which has reached the final size and therefore leaves the mill through the air classifier is replaced by fresh feed material. The target size of the spherical graphite was d50 of approx. 15 micron and d50 of approx. 20 micron. The feed material was easy to use. The flowability was good and the micronizing throughput was on average level. Two feed grades for spheronization were produced, both with mean particles sizes (d50 values) already close to the final products of 15 micron and 20 micron. • The spheronisation was conducted with a specific mill, optimized to change the shape of the particles while at the same time impeding further significant particle grinding. The mill has an internal classifier, which separates the fine material, which doesn't report in the final product. During the spheronisation step, some fine material splits from the graphite particles. Such split material is also separated by the classifier. The fine split material is called the "by-product". Due to the considerable proportion of fine particle sizes in the starting material (concentrate from the flotation), the amount of by-product in the tests with this material is increased. ProGraphite uses a batch mill for the spheronisation procedure. The internal air classifier permanently removes the fines during the spheronisation process: at the beginning the fines, which are already in the feed product, during the spheronisation the resulting split material. The speed (rotation) of the air classifier in combination with the air flow through the mill/air classifier define the size of the fines being removed. The aim of the spheronisation step is to produce round graphite particles with high tap density, high yield of coarse products and a low ratio of d90:d10. • The material is suitable for spheronisation; it was possible to get spherical graphite with acceptable properties. The particle size distribution is typical for spherical graphite. The ratio between d90 and d10 is acceptable. The tap density is comparatively low. A high tap density is preferred as it results in batteries with
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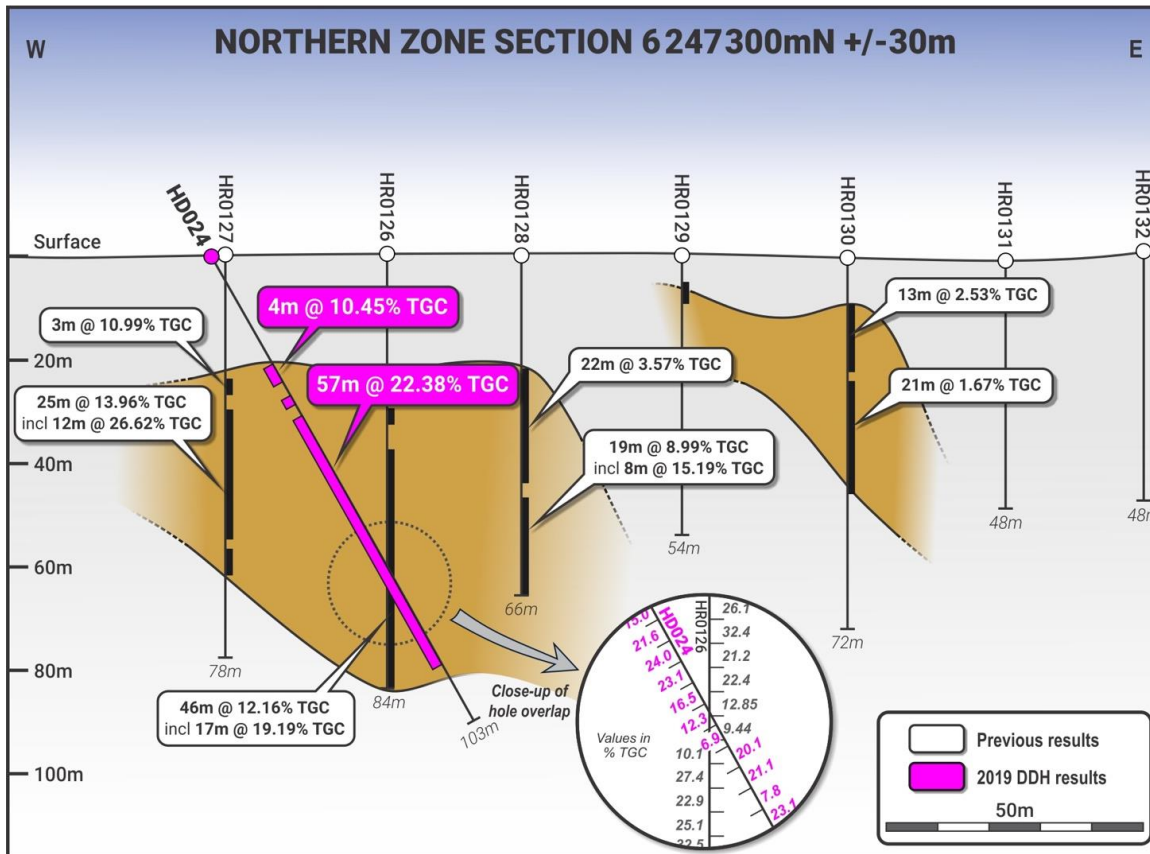
		<p>higher capacities. It would take more test work to see if the tap density can be increased further. Further work to increase the tap density should be undertaken.</p> <ul style="list-style-type: none"> • The material seems to be more suitable for the production of finer SPG types, as used by EV manufacturers. • 80 g of the spherical graphite produced was the used for an intensive purification. The main chemical used was NaOH and a hot alkaline digestion followed by an acid wash was carried out. The purification went well. An LOI value of 99.96% was measured, which is more than is normally considered a minimum for spherical graphite (99.95%). • The product after purification was then examined by an external ICP analysis. The critical values for use in batteries, such as Fe, Si, Cr, Cu are below the typical specification limits. • HF Purification was also performed on an 80g sample of spheronised product. An LOI value of 99.99% was measured, which is more than is normally considered a minimum for spherical graphite (99.95%). ICP analysis is ongoing and will be reported at a future date.
<p>Further work</p>	<ul style="list-style-type: none"> • The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). • Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive. 	<ul style="list-style-type: none"> • Exploration drilling will be ongoing in the area of the JORC resource. • Further holes are planned to test targets generated through the HeliTEM survey and metallurgical characterisation of graphite will be ongoing..

APPENDICIES – Plans and Cross Sections

HD024

Hole	Depth (m)	MGA East	MGA North	RL (m)	Precollar (m)	Dip	Azimuth (magnetic)	Significant Intercept
HD024	103.4	258595	6247280	26	20	-60	75	4m @ 10.45% TGC from 24m
								2m @ 3.25% TGC from 31m
								57m @ 22.38% TGC from 35.5m¹





HD031

Hole	Depth (m)	MGA East	MGA North	RL (m)	Precollar (m)	Dip	Azimuth (magnetic)	Significant Intercept
HD031	51.7	257163	6246415	30.7	20	-60	305.5	2.3m @ 4.73% TGC from 20.7m 10.9m @ 10.61% TGC from 25m Incl. 6.0m @ 17.57% TGC from 26m 1.0m @ 2.1% TGC from 43m

