ASX RELEASE
23 NOVEMBER 2022

KILIMANI DEEP FEEDER SYSTEMS AND NYANZAGA REGIONAL DRILLING BUILDS RESOURCE GROWTH POTENTIAL

Highlights

- OreCorp drilling at Kilimani and Nyanzaga has returned significant results including **24m @ 2.15g/t Au** from 100m down hole at Kilimani
- Kilimani MRE area remains open at depth and to the north and south
- Aircore (**AC**) drilling has returned encouraging results for follow-up northwest and southwest of the Nyanzaga Deposit
- OreCorp is pursuing opportunities to extend Nyanzaga's 10.7-year mine life as defined in its Definitive Feasibility Study (**DFS**) completed in August 2022
- OreCorp is continuing financing discussions for development of the Nyanzaga Gold Project (**Nyanzaga** or **Project**) and targeting first gold in 2025

OreCorp Limited (**OreCorp** or the **Company**) (ASX:ORR) is pleased to announce assay results from recent drilling at its 2.60Moz Project in Tanzania.

A DFS for Nyanzaga completed in August 2022 estimated the Project has a combined open pit and underground production target of 2.83Moz[1]. OreCorp is advancing financing discussions for the Project's construction and development in parallel with pursuing opportunities to increase its 10.7-year mine life estimated in the DFS and has generated an Exploration Target of approximately 4.0Mt to 6.0Mt at approximately 3.4g/t to 4.0g/t gold[2] below, and in addition to the production target.

OreCorp's recent drilling program aimed to test:

- Interpreted structures representing deep feeder structures and lodes proximal to the Kilimani Mineral Resource Estimate (**Kilimani MRE**);
- Geotechnical conditions around and along the proposed portal and decline. One geotechnical hole was extended to test the western limb of the Nyanzaga Anticline at depth; and
- Geochemically blind regional geological targets in the west of the Special Mining Licence (**SML**).

Drilling to test for potential deep feeder structures to the Kilimani MRE reported significant intersections in all holes with better intercepts including:

- 6m @ 2.77g/t gold from 124m (NYZRC1313)
- 7m @ 4.69g/t gold from 135m (NYZRC1315)
- 13m @ 1.09g/t gold from 88m (NYZRC1319)
- 24m @ 2.15g/t gold from 100m (NYZRC1326)

[1] Cautionary Statement - The production target for the Project comprises 92% Probable Ore Reserves and 8% Inferred Mineral Resources. There is a low level of geological confidence associated with Inferred Mineral Resources, and there is no certainty that further exploration work will result in the determination of Indicated Mineral Resources or that the production target itself will be realised.

[2] Cautionary Statement - The potential quantity and grade of the Exploration Target is conceptual in nature and is therefore an approximation. There has been insufficient exploration to estimate a Mineral Resource and it is uncertain if further exploration will result in the estimation of a Mineral Resource.

Intersections on the South Fault, at the western end of the Kilimani MRE, indicate that this structure is consistently mineralised along strike, and is open at depth and to the north. The results suggest that the South Fault acts as a feeder structure to the lodes between the South and North Faults.

The extended geotechnical hole ended in gold mineralisation in the lower part of the Nyanzaga mine sequence with 3.05m @ 1.10g/t gold from 599m to end of hole (**EOH**). The hole ended due to technical limitations with the drill rig and will be re-entered and extended in the near future.

This hole is approximately 110m down dip of the historical intersection of 10m @ 5.41g/t gold (NYZRCDD0053) and suggests that further high grade mineralisation may be developed in the western limb of the Nyanzaga Anticline. There has been limited drilling in this area and it represents an excellent opportunity to expand the recently announced Exploration Target.

OreCorp's wide-spaced regional AC drilling in the western portion of the SML reported significant results including:

- 4m @ 1.04g/t gold from 0m (surface) and 12m @ 1.81g/t gold from 8m *including 4m @ 4.07g/t gold from 12m* (NYGAC1697)
- 4m @ 1.59g/t gold from 40m (NYGAC1720)

These results highlight the opportunity for near surface, high grade mineralisation within the SML boundary. All of the intercepts are located under transported cover, where historical exploration has been deemed ineffective. The mineralisation in NYGAC1697 is open along strike for 400m north and south.

OreCorp's Executive Chairman Matthew Yates said:

"*The results from the programs are highly encouraging. We have identified the feeder zones at Kilimani and we can now expand on this. The deep hole on the western limb of Nyanzaga will be very significant for the depth potential at Nyanzaga and the regional aircore drilling illustrates the potential for further near surface mineralisation proximal to what will be the Nyanzaga mill*".

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1. Nyanzaga Gold Project

1.1. Overview

The Nyanzaga Project is in the Archean Sukumaland Greenstone Belt, forming part of the Lake Victoria Goldfields of the Tanzanian craton (**Figure 1**). The Project comprises SML 653/2021, granted to Sotta Mining Corporation Limited (**SMCL**) on 13 December 2021 for a period of 15 years, 11 granted prospecting licences and one prospecting licence application. The SML encompasses the Nyanzaga and Kilimani deposits and other exploration prospects.

The Project is held by SMCL, in which OreCorp holds an 84% interest through its wholly owned subsidiary Nyanzaga Mining Company Limited, and the Government of Tanzania holds a 16% free carried interest.

OreCorp announced the results of its DFS in August 2022 (ASX Announcement dated 22 August 2022 "*Nyanzaga DFS Delivers Robust Results*"). The Project is expected to deliver an average gold production of 234 koz pa over a 10.7 year LOM, with >242 koz pa (average) for the first 10 years peaking at 295 koz pa in Year 6 delivering a total of approximately 2.5 Moz of gold produced over the LOM.

Figure 1: Lake Victoria Goldfields, Tanzania

1.2. Kilimani Feeder Structures Reverse Circulation/Diamond Drilling

A total of 15 RC drill holes (one with DD tail) for 2,831.3m of drilling were completed at the Kilimani Deposit to test:

- Interpreted structures representing deep feeder structures to the Kilimani MRE; and
- Stratabound lodes proximal to the Kilimani MRE.

The geology of the Kilimani MRE is interpreted to comprise stratabound gold lodes in the anticlinal closure of a northwest trending anticline. Two subvertical, west-northwest striking fault systems on either side of the Kilimani MRE (the North and South Faults) are interpreted to be feeder structures to the layer parallel stratabound lodes in the anticlinal closure.

Drill hole locations are shown in **Figure 2**, and on section in **Figure 3**.

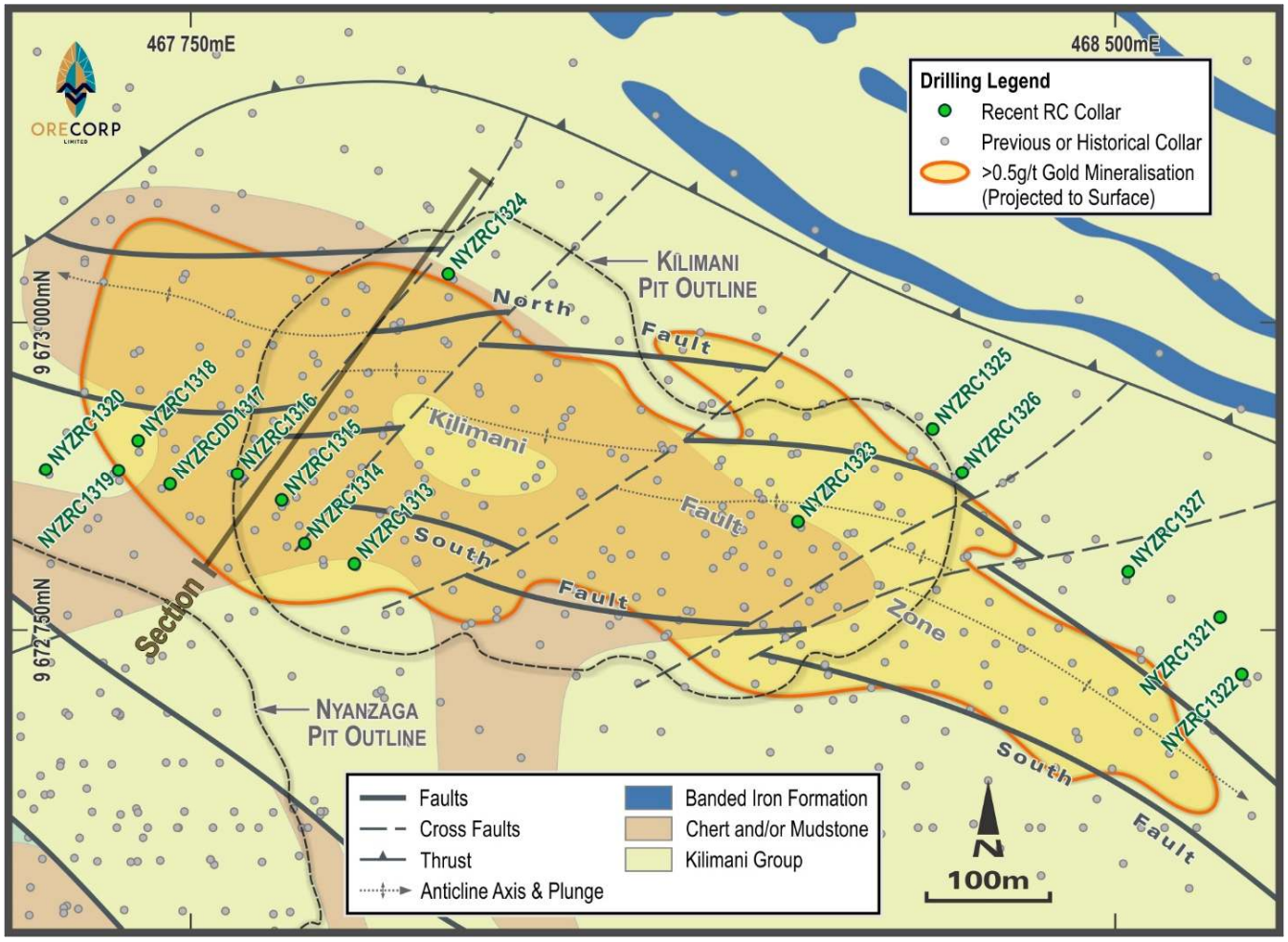

Figure 2: Kilimani Deposit with Recent RC Drilling

Significant intercepts (>1.0 g/t gold, minimum 2m interval) returned from the recent drilling include:

- 6m @ 2.77g/t gold from 124m (NYZRC1313, South Fault)
- 7m @ 4.69g/t gold from 135m (NYZRC1315, South Fault)
- 13m @ 1.09g/t gold from 88m (NYZRC1319, South Fault)
- 24m @ 2.15g/t gold from 100m (NYZRC1326, Stratabound Lode)

Refer to **Appendix 1** for JORC Table 1 and **Appendix 2** for a full list of significant intercepts.

The drilling is generally located on the margins of the MRE, with deep intersections in the South Fault outside the MRE. Shallow intercepts in the drilling either confirm or close out marginal portions of the Kilimani MRE.

Eight holes (NYZRC1313 to NYZRC1320 and NYZRCDD1317) tested the South Fault of the Kilimani MRE, (**Figure 2**). Six holes are interpreted to intersect the feeder structure at depth, with NYZRC1315 reporting an intersection of 7m @4.69g/t gold from 135m, located outside the current Kilimani MRE (**Figure 3**). Two holes failed to reach target.

Seven holes (NYZRC1321 to NYZRC1327) tested the North Fault of the Kilimani MRE. Hole NYZRC1325 reported a significant intercept of 2m @ 2.01g/t gold from 95m associated with the North Fault. Due to technical limitations three holes failed to reach target depth. Two holes intersected the interpreted position of the North Fault but did not intersect significant mineralisation.

Several intercepts interpreted as "stratabound" mineralisation were intersected including 24m @ 2.15g/t gold from 100m in NYZRC1326. This intersection is located outside the existing Kilimani MRE.

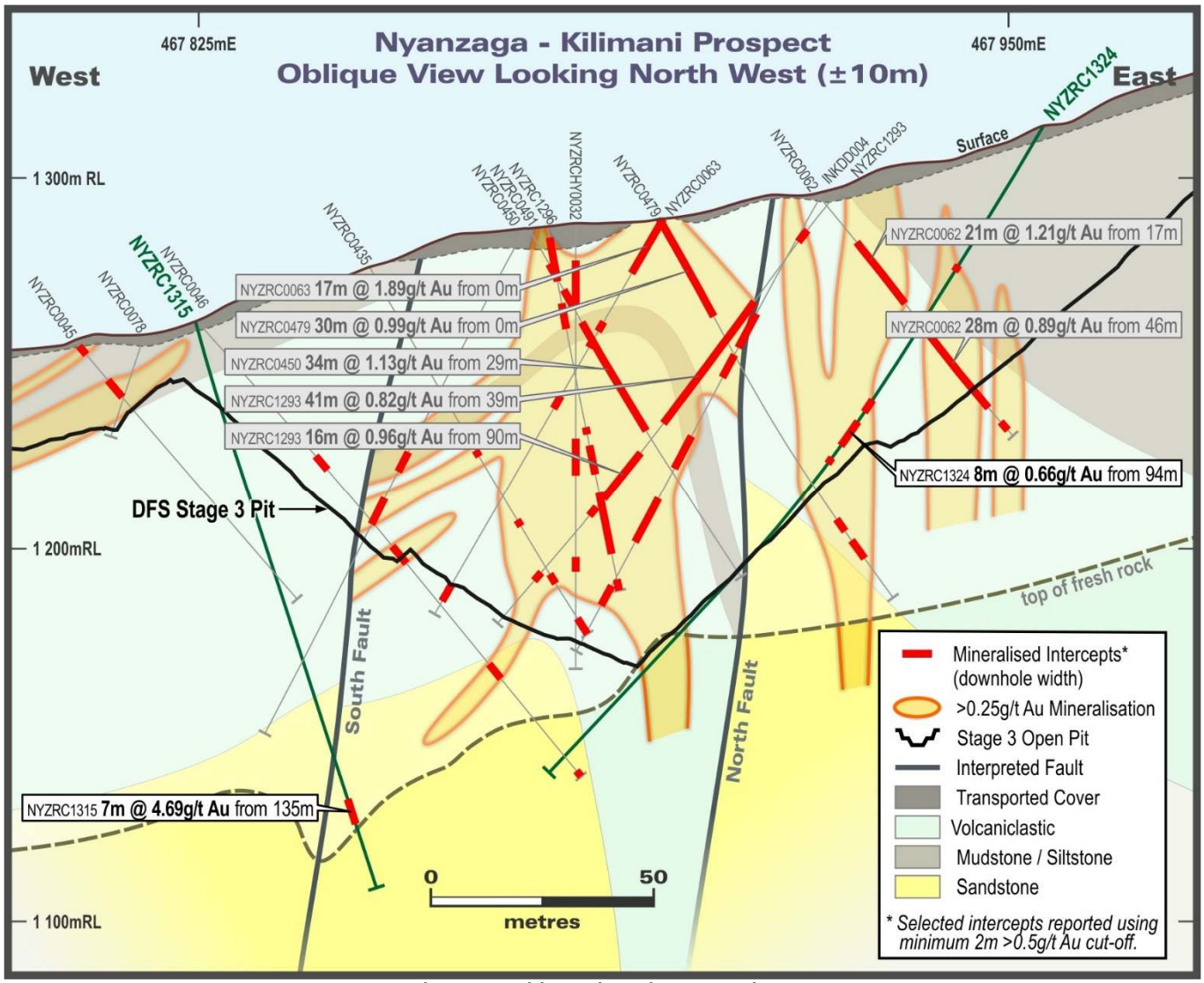

Figure 3: Kilimani Oblique Section

1.3. Nyanzaga Geotechnical Drilling

Geotechnical drilling was completed west of the Nyanzaga Deposit and drilled towards the east with the objective of testing the depth of weathering around and along the proposed portal and decline. One geotechnical hole (NYZRCDD1312) was extended to test the western limb of the Nyanzaga Anticline.

The hole was drilled to 602.5m with drilling abandoned due to technical limitations with the drill rig. NYZRCDD1312 ended in gold mineralisation in the lower part of the Nyanzaga mine sequence (C1 Chert) reporting 3.05m @ 1.10g/t gold from 599m (>0.50g/t gold, minimum 2m interval), (**Figure 4**). This intersection is highly significant in that it is located 110m down dip of the intersection in NYZRCDD0053 of 15m @ 3.94g/t gold from 438m (including 10m @ 5.41 g/t gold) hosted in C1 chert,

which suggests that higher grade gold mineralisation may be located in the undrilled C1 chert host rock located below the end of hole.

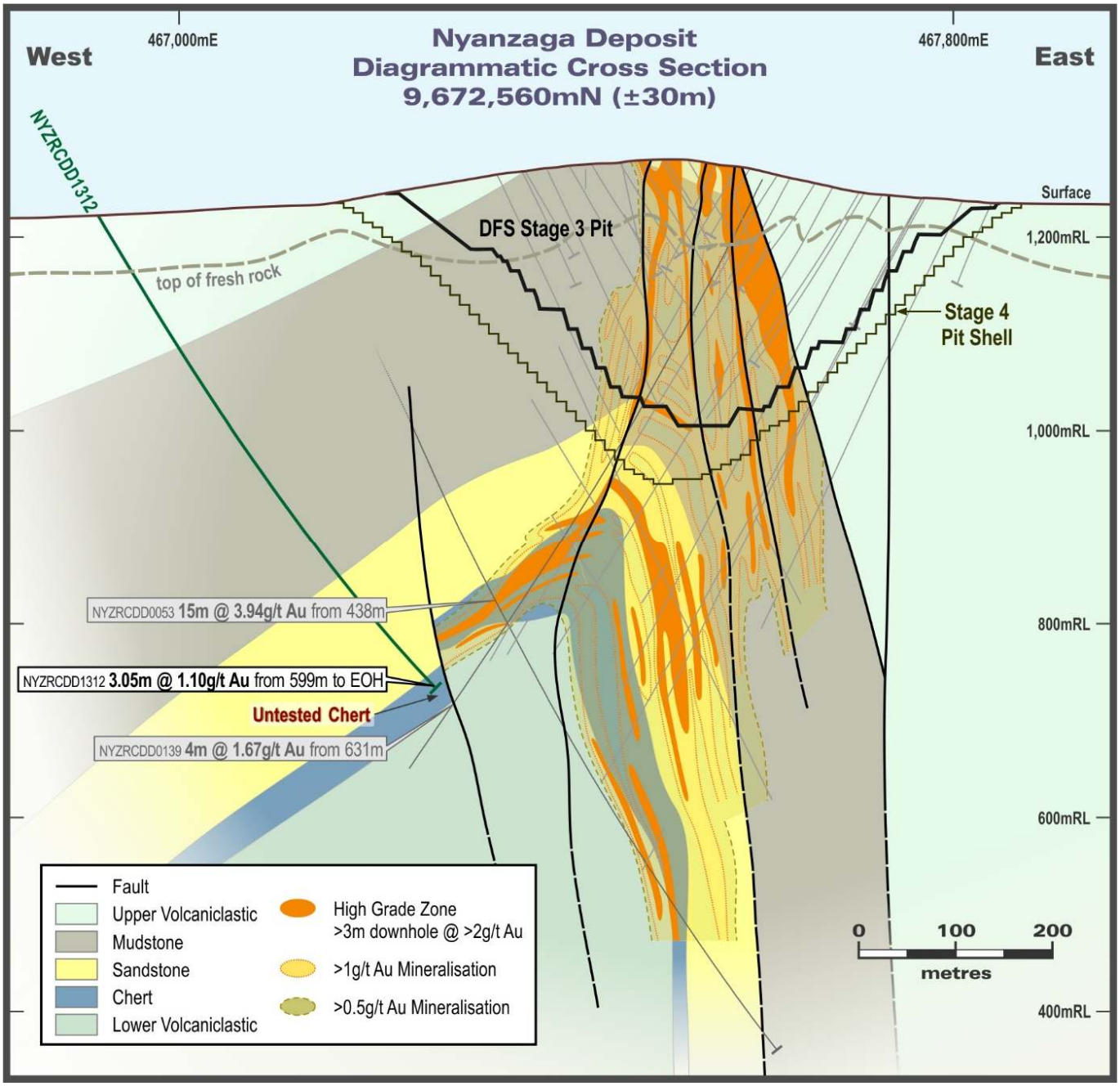

Figure 4: Drill Section 9,672,560mN Showing NYZRCDD1312

The Company plans to re-enter hole NYZRCDD1312 and drill through the C1 chert into the lower volcaniclastic rocks, looking for extensions of the higher grade material located in NYZRCDD0053.

Results from the geotechnical drilling have improved confidence in the underground design with the boxcut and portal located in an area of relatively shallow weathering (top of fresh rock at 30-35m) and favourable ground conditions identified for the proposed decline.

A new drill hole, approximately 300m west of NYCRZDD1312, is proposed in the future to test for an interpreted repeat anticline west of the Nyanzaga Anticline.

1.4. Western Corridor and the "Wingi Igneous Complex" Aircore Drilling

A total of 213 AC drill holes for 12,919m of drilling were completed to test the gold potential of the "Western Corridor" located within the SML to the west of the Nyanzaga Deposit (**Figure 5**). These areas are interpreted to contain generally geochemically "blind" gold targets associated with structural trends and demagnetisation of the basement rocks beneath areas of laterite and colluvial cover, where soil sampling is ineffective.

The regional AC drilling reported significant results (>0.1 g/t gold, minimum 2 m interval) including:

- 2m @ 0.75g/t gold from 12m and 4m @ 0.34g/t gold from 24m (NYGAC1537)
- 4m @ 0.46g/t gold from 48m (NYGAC1566)
- 4m @ 0.31g/t gold from 56m (NYGAC1591)
- 4m @ 1.59g/t gold from 40m (NYGAC1720)
- 4m @ 0.31g/t gold from 52m (NYGAC1621)
- 4m @ 1.04g/t gold from 0m (surface) and 12m @ 1.81g/t gold from 8m *including 4m @ 4.07g/t gold from 12m* (NYGAC1697)
- 4m @ 1.59g/t gold from 40m (NYGAC1720)
- 7m @ 0.40g/t gold from 48m (NYGAC1724)

Hole locations are shown on **Figure 5**. Refer to **Appendix 1** for JORC Table 1 and **Appendices 3** and **4** for a full list of significant intercepts and holes.

The drilling was completed on east west lines 400m apart, with vertical holes drilled to fresh rock at 50 to 100 spacing. The drilling west and southwest of the Nyanzaga Deposit was designed to test for extensions of structure in sediments and felsic intrusive rocks previously identified in the Nyanzaga South 1 Prospect area where historical drilling identified extensive arsenic anomalism and gold mineralisation, interpreted to be associated with flat lying quartz veins.

The current drilling has confirmed the presence of felsic and intermediate intrusive rocks emplaced in volcaniclastic sediments, forming a northwest striking igneous complex over 1,000m long and up to 500m wide, now referred to as the "Wingi Igneous Complex" (**WIC**), shown in **Figure 5** and **Figure 6**. The intrusives identified in the WIC are potential heat and metal sources to the gold mineralisation identified in the Nyanzaga area, and represent high priority exploration targets.

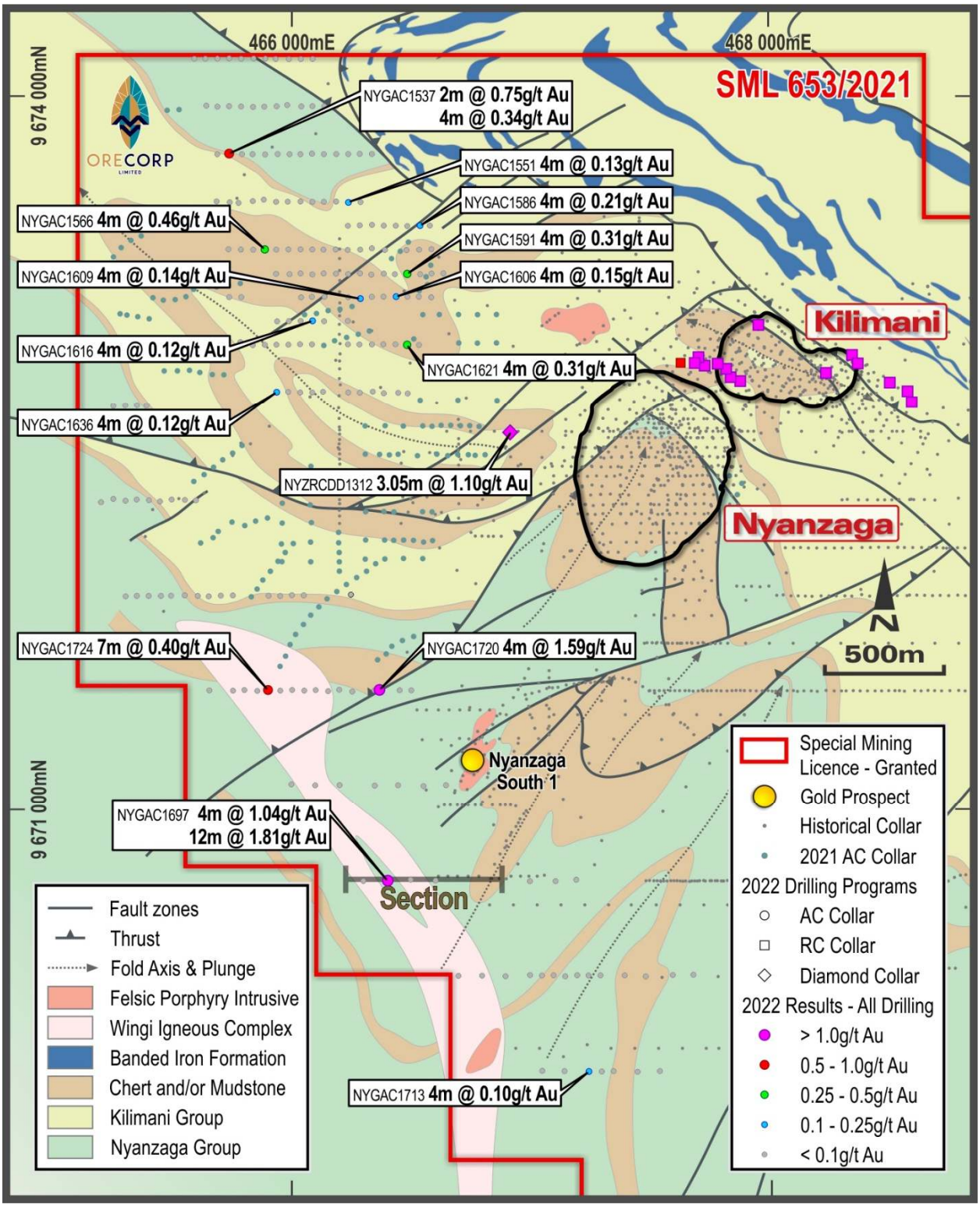

Figure 5: SML 653/2021 with Locations of Recent Drill Holes

The significant drill results in NYGAC1697 are hosted in a quartz vein within volcaniclastic sediments in the centre of WIC. Other anomalous results are located to the northwest and southeast within, or along strike of, the WIC. The significant gold mineralisation extends from surface, with logging suggesting the mineralisation occurs within subcropping basement in the vicinity of NYGAC1697, but with transported cover developed over drilling to the north, south and west (**Figure 6**).

Follow up AC drilling along the strike extent of the WIC is warranted, including both infill drill lines and infill holes between existing drilling.

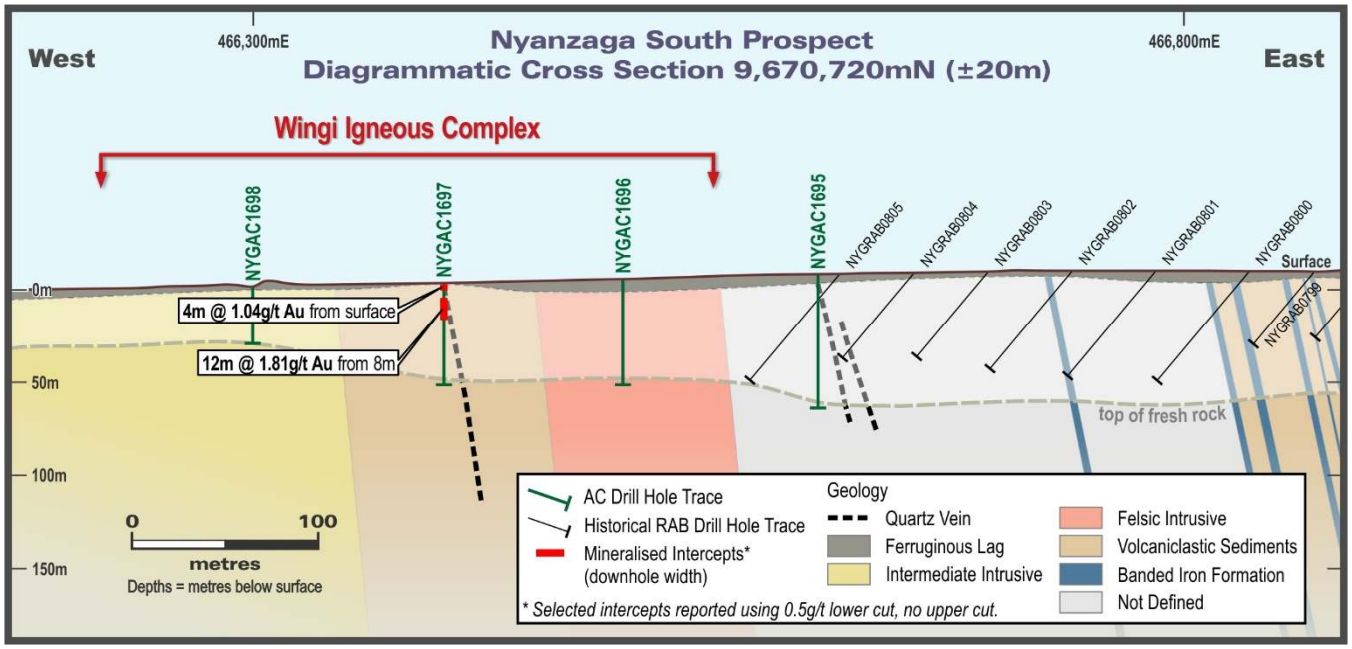

Figure 6: Drill Section 9,670,720mN

The drill lines northwest of the Nyanzaga Deposit were designed to test for structure in sediments located in the hangingwall, and broadly along strike to the northwest, of the Nyanzaga Deposit. Ten isolated holes reported significant anomalism.

Follow-up work will include multi-element sampling of the end of hole samples, along with pXRF sampling of the existing 4m composite samples, looking to identify pathfinder element trends in the data, and particularly Arsenic, which may lead to further drill targets.

A total of 171 AC holes for 7,775m were completed in the north-western area of the SML in 2021 (**Figure 5**). The assay results did not pass QA/QC criteria to the satisfaction of the Competent Person and are reported here as containing no significant mineralisation. QA/QC work on these samples is ongoing.

ABOUT ORECORP LIMITED

OreCorp Limited is a Western Australian based mining exploration company listed on the Australian Securities Exchange (ASX) under the code 'ORR'. The Company is well funded with no debt. OreCorp's key project is the Nyanzaga Gold Project in northwest Tanzania.

DISCLAIMER / FORWARD-LOOKING STATEMENTS

This announcement may contain certain forward-looking statements, guidance, forecasts, estimates, prospects and projections in relation to future matters that may involve risks or uncertainties and may involve significant items of subjective judgement and assumptions of future events, which as at the date of this announcement are considered reasonable, that may or may not eventuate (**Forward-Looking Statements**). Forward-Looking Statements can generally be identified by the use of forward-looking words such as, 'anticipates', 'estimates' 'will', 'should', 'could', 'may', 'expects', 'plans', 'forecast', 'target' or similar expressions and may include, without limitation, statements regarding plans, strategies and objectives of management, anticipated production and expected costs. Indications of, and guidance on future earnings, cash flows, costs, financial position and performance are also Forward-Looking Statements.

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JORC 2012 COMPETENT PERSONS STATEMENTS

The information in this release that relates to new Exploration Results in relation to the Nyanzaga Project is based on and fairly represents information and supporting documentation prepared by Mr John McIntyre, a competent person who is a Member of the Australian Institute of Geoscientists. Mr McIntyre is a consultant to OreCorp Limited. Mr McIntyre has sufficient experience that is relevant to the style of mineralisation and type of deposits under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr McIntyre consents to the inclusion in this release of the Exploration Results for the Nyanzaga Project in the form and context in which they appear.

The information in this announcement relating to previous Exploration Results, Exploration Targets, estimates of Mineral Resources, Ore Reserves Statements and the production target in relation to the Project is extracted from the ASX announcements dated 1 November 2022 ("*OreCorp Identifies Opportunities to Extend Life of Mine at Nyanzaga Gold Project*"), 22 August 2022 ("*Nyanzaga DFS Delivers Robust Results*"), 5 May 2022 ("*DFS Completion and Kilimani MRE Update within Nyanzaga SML*"), 11 March 2022 ("*Final Kilimani Drilling Results*") and 12 September 2017 ("*MRE Update for the Nyanzaga Project Increasing Category and Grade*") which are available to view on the Company's website www.orecorp.com.au.

The Company confirms that it is not aware of any new information or data that materially affects the information included in the original announcements and, in the case of Mineral Resources and Ore Reserves Statements, that all material assumptions and technical parameters underpinning the Mineral Resources and Ore Reserves Statements, and the production target and any forecast financial information derived from the production target in the original announcements continue to apply and have not materially changed. The Company confirms that the form and context in which the Competent Persons' (being Messrs Allan Earl, Malcolm Titley, Anton Geldenhuys, Jim Brigden and John Haywood) findings are presented have not been materially modified from the original announcements.

APPENDIX 1 - NYANZAGA PROJECT JORC CODE (2012 EDITION) TABLE 1

Section 1: Sampling Techniques and Data, Nyanzaga (SML653/2021)		
Criteria	**JORC Code explanation**	**Commentary**
Sampling techniques	*Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as downhole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.*	RC Drilling: For the RC and DD pre-collar drill samples were collected through a cyclone at 1m intervals for the entire length of the hole, with a sample collected after splitting through a 3 tier riffle splitter. Diamond Drilling: Core samples were assayed at nominal 1m intervals. Core was split using a diamond saw and half core sampled consistently from the same side of the core relative to the orientation line. 2021 and 2022 AC samples were collected through a cyclone in 1m samples, the 1m sample is spear sampled, and a composite or the spear samples were collected using a riffle splitter to make a 2kg composite sample over 4 metres. Details of the sampling techniques for historical (pre OreCorp) RC and DDH sampling are discussed in previous announcements; historical Rotary Air Blast (RAB) and Aircore (AC) drilling are largely not detailed. Historical RAB and AC samples were collected through a cyclone and composite samples were collected using a riffle splitter to make a 1.5-3kg composite sample over 3 metres. RAB drilling is open hole while AC drilling uses a face sampling blade. Selective samples were taken from generally 3m composite intervals and re-sampled over 1 metre. OreCorp Tanzania Limited (OTL) has followed the same sampling and QAQC practices as previously used by Barrick Exploration Africa Limited (BEAL).
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	**RC Drilling:** samples were collected after splitting through a 3 tier riffle splitter. A standard, blank or duplicate were inserted in every 10th sample interval for each hole. A duplicate was taken as the third QA/QC sample. The cyclone was cleaned before the start of each hole. **Diamond Drilling** - Core was correctly fitted in the core boxes prior to sampling to ensure that only one side of the core is sampled consistently. A standard, blank or duplicate were inserted in every 10th sample interval for each hole. A duplicate was taken as the third QA/QC sample. **AC Drilling** -the 1m sample is spear sampled, and a composite of the spear samples was prepared using a riffle splitter to make a 2kg composite sample over 4 metres. A standard, blank or duplicate were inserted in every 10th sample interval for each hole. A field duplicate was taken as the third QA/QC sample. The cyclone was cleaned before the start of each hole.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to	Aspects of the determination of mineralisation that are Material to the Public Report are discussed under the sampling sections above and drilling methods below**.**

Section 1: Sampling Techniques and Data, Nyanzaga (SML653/2021)		
Criteria	**JORC Code explanation**	**Commentary**
	produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information	
Drilling techniques	*Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	**RC Drilling:** A large diameter hammer of 5.5" was used throughout the all the RC drilling programs. The cyclone was cleaned before the start of each hole. Samples were collected at 1 metre intervals in plastic bags and their weight (25-35kg) was recorded in a log-book. If required wet samples were collected in polythene bags and allowed to air dry before splitting, although drilling was generally stopped when sample became wet. Magnetic susceptibility readings were taken every metre. The dry 1m samples collected above were disgorged into a three tier riffle splitter. The materials collected in the residue buckets on either side of the splitter were poured back into the splitter to ensure the homogeneity of the sample. The splitter and sample collection boxes were cleaned after every metre drilled. After the 2nd split a 4 to 5kg sample was collected from one of the buckets in a small pre-labelled and tagged plastic bag. The bag was folded over several times and stapled to prevent sample leakage. The contents of the second bucket were poured into a pre-labelled plastic sample bag, containing the sample interval marked on an aluminium or plastic tag, for storage at the Nyanzaga camp. **Diamond Drilling:** Core sizes range from PQ to NQ. PQ or HQ was employed to penetrate the soil, laterite and saprolite horizons for metallurgical and geotechnical holes and NQ was used consistently whenever fresh rock was encountered, excluding NYZRCDD1312, which was drilled entirely in HQ. Core recovery is generally high (above 90%) in the mineralised areas, and particularly if these mineralised zones were intersected in fresh rock. If the ore zones are intersected in the regolith like in metallurgical holes, core recovery can be as low as 40%, but every attempt was made to recover above 80%. Core orientation was completed using the Reflex Gyro tool, nominally on every run, and the bottom of hole marked with a line drawn on the core. Technicians transported the core to camp site, then checked the validity of orientation marks, fit the cores using a 6m long angle-liner fitted in a horizontal plane and join the orientation marks by drawing a line with an arrow pointing down hole. The core was then photographed; a Geo-Technician completed a geotechnical data log that includes (Interval, core recovery, RQD and fracture frequency etc). Magnetic susceptibility readings are taken every metre. Only half of the cut core is sent to the lab, the other half is marked with a sample number and stored in racks at Nyanzaga site. Prior to storing the core, Apparent Relative Density (ARD) measurements are taken (every metre) and the data incorporated into the database. The Au assay values received are posted in red or white permanent ink on the corresponding core intervals. The deposit style lends itself to this kind of sampling and no issues are anticipated based on what is known about procedures in place at the time of drilling. OTL 2021-22 Drilling

Section 1: Sampling Techniques and Data, Nyanzaga (SML653/2021)		
Criteria	**JORC Code explanation**	**Commentary**
		AC Drilling: Undertaken using a face sampling 5.5" hammer for the entire hole in the 2021 and the 2022 program. Sample was collected in bags from the cyclone.
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.*	**RC Drilling:** The samples were weighed on a spring scale and the sample weight was written down immediately after being weighed. Recovery was assessed by comparing the recovered weight against the expected weight of the lithology. Recovery was recorded into electronic data entry forms and then uploaded into the Geobase database. Recovery was typically good, with low recovery in wet or collar samples. **Diamond Drilling**: Core recovery was measured by ORR geologists by measuring the actual lengths of core in the orientated, reconstructed and measured core compared to that estimated between drillers blocks. Recovery was recorded into electronic data entry forms and then uploaded into the Geobase database. Recovery was 95%. **AC Drilling:** Samples were bagged at the cyclone and a visual estimate of recovery was made and entered into electronic data entry forms and then uploaded into the Geobase database. Recovery was typically good.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	For AC and RC Recovery was maximised by ensuring the drilling was dry, pausing the drill feed at the end of metres, and generally ensuring all sample was captured in the bulk sample bag. Cyclone, splitters and sample buckets were cleaned regularly. Protocols for sample collection, sample preparation and assaying generally meet industry standard practice for this type of gold deposit. Diamond core was extracted using standard wire line methods, with the exception of the geotechnical drilling which incorporated the triple tube system to maximise recovery.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	No correlations have been recognised between sample recovery and grade.
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	Drill holes have been logged to the nearest cm for DD and every metre for RC. Geological logging has included lithology, lithological contact type, texture, minerals present, and percentage of minerals. Geotechnical logging records the casing sizes, bit sizes, depths, intervals, core recovery, weathering index, RQD, fracture index, jointing and joint wall alteration, and a simple geological description. Where DD cores were oriented Alpha and Beta angles of fabrics, bedding, veining and contacts were recorded at point depths. Core orientations were measured at the drill site by the driller and checked by the geologists who then drew orientation lines on the core. The cores were transported from drilling site to camp core shed every day. Upon receipt in the Camp core shed, cores

Section 1: Sampling Techniques and Data, Nyanzaga (SML653/2021)		
Criteria	**JORC Code explanation**	**Commentary**
		were cleaned or washed (if required) and core blocks were re-checked by ABGE staff. Orientation lines were also cross-checked at the core yard by the logging crew. The core was reportedly photographed, wet and dry, using a camera mounted on a framed structure to ensure a constant angle and distance from the camera but not all photographs is in the provided database. Magnetic susceptibility readings were taken after every metre. For unconsolidated cores this is measured in situ and results recorded in SI units (Kappa) in the assay log sheets. Geotechnical logging records the casing sizes, bit sizes, depths, intervals, core recovery, weathering index, RQD, fracture index, jointing and join wall alteration, and a simple geological description. All cores were oriented with Alpha and Beta angles of fabrics recorded at point depths. The line is drawn 90º clockwise from the orientation line along the length of the core to indicate where the core must be cut. This is to ensure that each half of the core will be a mirror image of the other. Where there is no orientation, a line is chosen to at 90º to the predominant structure so that each cut half of the core will be a mirror image. Core cutting by diamond saw is conducted in a dedicated core saw shed, while unconsolidated material is split using spoons or trowels. Core is cut in half, or in the case of unconsolidated material. A 1m half core is removed from the core box for assaying. Each sample interval is placed in a plastic bag with a sample ticket. The bag is labelled with the hole and sample numbers using a marker pen. Bulk density readings, where available, were taken at every 1 m interval within the same lithology whereby a piece of core with a length of not less than 10cm is used. Density is measured using the buoyancy method prior to 2021. In 2021, density was measured using the calliper method as the core was too soft and porous for the buoyancy method. For earlier drillholes, measurements were carried out on half core, later whole core was used. The RC and DDH data is of a quality to support a future potential mineral resource estimation, should sufficient drilling be completed. The RAB and AC data is not intended to be used in any future potential mineral resource estimation.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Logging includes both qualitative and quantitative properties of the sample material.
	The total length and percentage of the relevant intersections logged.	All newly reported drilling has been logged.
Subsampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.*	For the diamond core a line is drawn 90 degrees clockwise from the orientation line along the length of the core to indicate where the core must be cut. This is to ensure that each half of the core will be a mirror image of the other, as much as possible. Where there is no orientation, a line is chosen at 90 degrees to the predominant structure so that each cut half of the core will be a mirror image.

Section 1: Sampling Techniques and Data, Nyanzaga (SML653/2021)		
Criteria	**JORC Code explanation**	**Commentary**
		Core cutting by diamond saw was conducted in a dedicated core saw shed. Core is cut in half and a 1m half core is removed from the core box for assaying. Each sample interval is placed in a plastic bag with a sample ticket. The bag is labelled with the hole and sample numbers using a marker pen.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	RC samples were split 50:50 through a riffle splitter. Reports were seen that some samples were moist / wet. From experience at Nyanzaga, such wet samples usually occurred at the base of the oxide / transitional zones. AC samples were spear sampled, with the resulting 4m composite split to 2kg through a riffle splitter. Moisture/water content for both RC and AC is recorded qualitatively.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The sample preparation technique comprises crushing, milling and then splitting off of a 50gm charge, and is appropriate for the style and type of mineralisation expected in the project area.
	Quality control procedures adopted for all subsampling stages to maximise representivity of samples.	Umpire quality control samples have been systematically submitted. QA/QC protocols and a review of blank, standard and duplicate quality control data conducted on a batch by batch basis. Laboratory introduced QAQC samples are assessed.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.	A standard, blank or duplicate were inserted in every 10th sample interval for each hole. A field duplicate was taken as the third QA/QC sample.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Field duplicate precision analysis results are within acceptable limits for a nuggety gold body, indicating that results are repeatable and therefore the sample sizes are likely appropriate. For- AC, RC and DD drilling, sample sizes of around 3 to 5kg are appropriate to the grain size of the material being sampled.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	RC samples from the 2022 program were assayed by 50 g fire assay with an AAS finish at Nesch Mintec, Mwanza. The AC samples were assayed by 50 g fire assay with an ICP/MPAES finish at Nesch Mintec, Mwanza. Both methods are considered appropriate for the material being assayed and is considered a near total digest for gold in this environment. All the samples from the 2021 program were assayed by 50 g fire assay with an AAS finish at Nesch Mintec, Mwanza. This is considered appropriate for the material being assayed and is considered a near total digest for gold in this environment.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	Magnetic susceptibility readings were taken using a KT9 Kappameter and results were recorded in SI units (Kappa). No handheld XRF instrumentation was used.
	Nature of quality control procedures adopted (e.g.	Field QC measures included inserting standards, blanks and field duplicate samples.

Section 1: Sampling Techniques and Data, Nyanzaga (SML653/2021)		
Criteria	**JORC Code explanation**	**Commentary**
	standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	For RC and AC drilling representative sieved/washed samples were also taken from each metre drilled and kept in chip trays for loggings and reference. After completion of every hole, a check was done between the geologist and the technician in charge of the sampling, to confirm; the final depth of the hole, number of samples collected, sample number intervals and QAQC sample insertion/duplicates including number and sample numbers, at the rig. In the fourth 10m sample interval the duplicate samples were taken. The duplicate was taken at the same time and from the same bucket as the original sample. The pre-prepared sample sheet clearly indicated the type and interval where the QAQC sample was to be inserted. A standard, blank or duplicate were inserted in each 10 sample interval for each hole. Sample numbers were sequential. QAQC samples were inserted randomly within the 10 sample interval. A duplicate was taken as the third QAQC sample. A blank was inserted in the interval after visual mineralisation is observed. It was at the discretion of the geologist whether or not additional standards should be added in broad zones of mineralisation. Laboratory Introduced Quality Control Measures were routinely reported by the laboratory and include: the laboratory's internal certified standards, repeat samples taken from the first stage sample prep, assay repeatability tests, reproducibility tests and grind checks. These test the various stages of the analytical process. The data indicates that overall (apart from the batches discussed below*) the analytical results obtained during the reporting period have shown to be both precise and accurate. A few inconsistencies have been identified within a limited number of batches however when interrogated further there has not been any consistent problems on a batch level to warrant further checking. *Sample submission batches OTL0052a, OTL0053, OTL0060 and OTL0062 related to the 2021 AC drilling did not pass QA/QC criteria to the satisfaction of the Competent Person and are reporter here as containing no significant mineralisation. QA/QC work is ongoing and these results might be restated upon completion of further QA/QC work.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.*	Verification of drilling processes and some significant intersections has been undertaken by senior geologists on site, and by the Competent Person (for the AC and DDH programs) during site visits during and after the drilling program. Sampling techniques were observed to conform with those presented in the Sampling Techniques section of Section 1 of this Table. Several reported significant intersections were reviewed in the core or sample trays.
	The use of twinned holes.	No twinning of these holes has been completed.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	OreCorp field data were first logged onto field sheets then typed up into spread sheets with strict built-in validation controls and look-up codes. These spread sheets were sent to the database manager who uploaded them to the main, secure database in Perth. All field data and assay data were verified and validated upon receipt. The database is managed off-site by an independent and professional database manager. Data collection and entry procedures were documented and training given to all staff. Scans of original field sheets are stored digitally without alteration.
	Discuss any adjustment to assay data.	No adjustments have been made to the assay data.
Location of data points	*Accuracy and quality of surveys used to locate drillholes (collar and downhole surveys), trenches, mine*	All drill hole collars have been surveyed using DGPS by GlEAM Tanzania Limited. No downhole survey was done during the AC drilling. All RC and DD holes from the recently completed program were surveyed every 30 metres using a Reflex GYRO tool.

Section 1: Sampling Techniques and Data, Nyanzaga (SML653/2021)		
Criteria	**JORC Code explanation**	**Commentary**
	workings and other locations used in Mineral Resource estimation.	
	Specification of the grid system used.	The grid system is UTM Arc 1960, Zone 36S.
	Quality and adequacy of topographic control.	A drone survey, to resurvey the Nyanzaga trig base station was undertaken in 2019. Data from this was used to create a surface DEM of the area. This data was used to assign RL's to the drilling as the DTM from the drone survey was deemed more accurate than the existing DTM.
Data spacing and distribution	*Data spacing for reporting of Exploration Results.*	Reconnaissance AC drilling was undertaken in 400m spaced traverses, with holes located at 50m or 100m spacing along lines, generally designed to cross and test soil and interpreted stratigraphic and structural targets. RC drilling was designed to test for feeder structures along the edges of the Kilimani system, with generally single holes spaced 40m apart on the NW and SDE ends or the system, with holes oriented perpendicular to strike. The diamond drill hole was designed to test a target along a set cross section, with the drilling located slightly oblique to the strike of the west limb of the Nyanzaga Anticline.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	RC drill spacing is potentially adequate to assume a degree of geological and grade continuity to support any future re-estimation of the Kilimani MRE. The single DD hole is not sufficient on its own to be used for any future MRE estimation. The aircore drilling is not considered suitable for any future MRE estimation.
	Whether sample compositing has been applied.	Composite sampling was applied to the AC drilling.
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	The majority of RC drilling is oriented towards the NE at -60^{o}, with the interpreted mineralisation trends striking WNW dipping towards the SW. Any structures in the AC drilling are of unknown orientation.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No sampling bias has been identified on the basis of drill orientation.

Section 1: Sampling Techniques and Data, Nyanzaga (SML653/2021)		
Criteria	**JORC Code explanation**	**Commentary**
Sample security	*The measures taken to ensure sample security.*	All samples were removed from the field at the end of each day's work program. Drill samples were stored in a guarded sample farm before being dispatched to the Laboratories in sealed containers.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	Audit review of the various drill sampling techniques and assaying have been undertaken by BEAL and Geobase, documented in previous announcements. The sampling methodology applied to data follow standard industry practice. A procedure of QAQC involving appropriate standards, duplicates, blanks and internal laboratory checks is and has been employed in all sample types.

Section 2: Reporting of Exploration Results, Nyanzaga Project		
Criteria	**JORC Code explanation**	**Commentary**
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	The Project is in north-western Tanzania, approximately 60 kilometres south-south west of Mwanza in the Sengerema District. The Nyanzaga and Kilimani deposits lie within the granted SML 653/2021 covering 23.4km^2. The Company also has a number of Prospecting Licences surrounding the SML. Under the new Tanzanian legislative changes which have been approved by the Tanzanian Parliament statutory royalties of 6%, (reduced to 4% in the case of gold sold at refinery centres in Tanzania) are payable to the Tanzanian Government, based on the gross value method. This is in addition to the 0.3% community levy and 1% clearing fee on the value of all minerals exported from Tanzania from 1 July 2017. In accordance with the new legislative changes, the Tanzanian Government now holds a 16% free carried interest in the joint venture company which holds the SML. There is a Framework Agreement and Shareholders Agreement in place governing the operations of the joint venture company.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	SML 653/2021 was granted on 13 December 2021 for a period of 15 years.
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	The work at the Nyanzaga Project is set out below.

Section 2: Reporting of Exploration Results, Nyanzaga Project		
Criteria	**JORC Code explanation**	**Commentary**
		1996 – Maiden Gold JV with Sub Sahara Resources – Acquired aerial photography, Landsat imagery and airborne magnetic and radiometric survey data. Completed soil and rock chip sampling, geological mapping, a helicopter-borne magnetic and radiometric geophysical survey and a small RC drill program. 1997 to 1998 – AVGold (in JV with Sub Sahara) – Completed residual soil sampling, rock chip and trench sampling and a ground magnetic survey. 1999 to 2001 – Anglovaal Mining Ltd (in JV with Sub Sahara) – Conducted further soil sampling, rock chip sampling, trenching, ground magnetic survey, IP and resistivity survey and limited RC and Diamond drilling. 2002 – Placer Dome JV with Sub Sahara Resources – Completed trenching, structural mapping, petrographic studies, RAB/AC, RC and diamond drilling. 2003 – Sub Sahara Resources – Compilation of previous work including literature surveys, geological mapping, air photo and Landsat TM analysis, geophysical surveys, geological mapping, geochemical soil and rock chip surveys and various RAB, RC and DDH drilling programs. 2004 to 2009 – Barrick Exploration Africa Ltd (BEAL) JV with Sub Sahara Resources - Embarked on a detailed surface mapping, re-logging, analysis and interpretation to consolidate a geological model and acceptable interpretative map. They also carried out additional soil and rock chip sampling, petrographic analysis, geological field mapping as well as RAB, CBI, RC and diamond drilling. A high resolution airborne geophysical survey (included magnetic, IP and resistivity) was flown over the Nyanzaga Project area totalling 400 square kilometres. To improve the resolution of the target delineation process, BEAL contracted Geotech Airborne Limited and completed a helicopter Versatile Time Domain Electromagnetic (VTEM) survey in August 2006. Metallurgical test work and an independent resource estimation was also completed (independent consultant). 2009 to 2010 – Western Metals/Indago Resources – Work focused on targeting and mitigating the identified risks in the resource estimation. The main objectives were to develop confidence in continuity of mineralisation in the Nyanzaga deposit to a level required for a feasibility study. The independent consultant was retained by Indago to undertake the more recent in-pit estimate of gold resources per JORC code for the Nyanzaga Project which was completed in May 2009. Drilling was completed on extensions and higher grade zones internal to the optimized pit shell. 2010 to 2014 – Acacia undertook an extensive step out and infill drilling program and updated the geological and resource models. 2015 to present – OTL has undertaken extensive work, primarily at Nyanzaga and also on regional targets. This work has included detailed mapping including structural and alteration mapping, drilling and soil sampling. This includes the Kilimani area.

Section 2: Reporting of Exploration Results, Nyanzaga Project		
Criteria	**JORC Code explanation**	**Commentary**
		Mineral Resource Estimates have been completed on the Nyanzaga and Kilimani Prospects. A Definitive Feasibility Study (see ASX announcement dated 22 August 2022) has defined a Mineral Resource at Nyanzaga, and includes a portion of the MRE at Kilimani in the Production Schedule.
Geology	*Deposit type, geological setting and style of mineralisation.*	The Nyanzaga Project is located on the northeastern flank of the Sukumaland Archaean Greenstone Belt. It is hosted within Nyanzian greenstone volcanic rocks and sediments typical of greenstone belts of the East African craton. The Nyanzaga deposit occurs within a sequence of folded Nyanzian sedimentary and volcanic rocks. Current interpretation of the Nyanzaga deposit has recognised a sequence of mudstone, sandstone and chert that are interpreted to form a northerly plunging anticline. Current interpretation of the Kilimani deposit has recognised again, a sequence of chert, mudstone, sandstone and agglomerate that are interpreted to form a possible double plunging, west-north westerly to east south-east plunging antiform. The Nyanzaga and Kilimani deposits are orogenic gold deposit types. The mineralisation is hosted by a cyclical sequence of chemical and clastic sediments (chert/sandstone/siltstone) interbedded volcaniclastic rocks bound by footwall and hanging wall volcanoclastic units. At Nyanzaga, three key alteration assemblages have been identified; Stage 1, Crustiform carbonate stockwork; Stage 2, Silica – sericite - dolomite breccia replacement overprint; and Stage 3, Silica-sulphide-gold veins. At Kilimani, most of the recognised mineralisation occurs in the oxidised profile. Where intersected in fresh material, the mineralisation is associated with strongly carbonated stock work and disseminated replacement. Mineralisation at Kilimani is reported as stratigraphically controlled in chert, mudstone, sandstones and interbedded volcaniclastic rocks. At Kilimani, the distribution of the gold mineralisation is related to dilation associated with; 1) competency contrast near the sedimentary cycle boundaries resulting in stratabound mineralisation; and 2) sub-vertical faulting, fracturing and brecciation related to the folding and subsequent shearing along the NE limb of the fold.
Drillhole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drillholes:* • *Easting and northing of the drillhole collar*	All historical drill hole collar locations (easting and northing given in UTM 1960, Zone 36N), collar elevations (m), dip (°) and azimuth (° Grid UTM) of the drill holes, down hole length (m) and total hole length. This information has been the subject of ASX releases on 22 September 2015, 11 May 2017, 30 June 2017, 12 September 2017, 2 June 2020, 4 February 2022, 11 March 2022, 5 May 2022 and 1 November 2022. Data relating to new drilling discussed in this report is included in appendices 2 and 3.

Section 2: Reporting of Exploration Results, Nyanzaga Project		
Criteria	**JORC Code explanation**	**Commentary**
	• *Elevation or RL (Reduced Level – elevation above sea level in metres) of the drillhole collar* • *Dip and azimuth of the hole* • *Downhole length and interception depth* • *Hole length.*	
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	All information is included. Not applicable.
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.*	Significant intercepts in RC and DD are reported based on a minimum width of 2m, and a maximum consecutive internal dilution of no more than 2m for 0.5 and 1.0 g/t Au cut-offs and minimum width of 3m and a maximum consecutive internal dilution of no more than 2m for 2.0 g/t Au cut-off. Significant intercepts in AC are reported on a minimum width of 2m for 0.1g/t Au and 1.0g/t Au cut-off. All previous drill results both for Nyanzaga and for Kilimani were reported in the Company's 22 September 2015, 11 May 2017, 30 June 2017, 12 September 2017, 2 June 2020, 4 February 2022, 11 March 2022, 5 May 2022 and 1 November 2022 ASX releases.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Not applicable.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	Not applicable. Gold only is being reported.
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.*	Geological interpretation, field mapping and drill testing of the resource area suggests that the gold mineralisation within the Nyanzaga Deposit is located in a combination of either north striking structures; or stratabound structures parallel to bedding contacts in the east limb and nose of the Nyanzaga Anticline respectively. Kilimani mineralisation zone is related to folded stratabound mineralisation and steeper fault hosted mineralisation.

Section 2: Reporting of Exploration Results, Nyanzaga Project		
Criteria	**JORC Code explanation**	**Commentary**
	If the geometry of the mineralisation with respect to the drillhole angle is known, its nature should be reported.	Drilling results are quoted as downhole intersections. For Nyanzaga true mineralisation width is interpreted as approximately 50% to 70% of intersection length for holes drilled dipping at 60° to 90° at 220° to 280° magnetic and intersecting the eastern limb of the folded mineralised sequences. True mineralisation width is interpreted as lower, at approximately 40% to 60% of intersection length for those holes drilled on easterly azimuths intersecting the western limb of the fold closure. For Kilimani, true mineralisation is interpreted as >80% of intersection width for stratabound mineralisation and 40-60% for the steeper fault controlled mineralisation. For intersections outside of the deposits the orientation of any mineralised structures, and the true widths of intersections, are unknown.
	If it is not known and only the downhole lengths are reported, there should be a clear statement to this effect (e.g. 'downhole length, true width not known').	Not applicable. Stated above.
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drillhole collar locations and appropriate sectional views.*	Appropriate diagrams and tabulations of intercepts have been reported.
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	All significant and non-significant intercepts have been tabled in either this release (for the new holes reported here) or in the appendices of the previous ASX releases on 22 September 2015, 11 May 2017 and 30 June 2017 for both Kilimani, Nyanzaga and regional project drilling. Also in the Kilimani Resource Report, 2022.

Section 2: Reporting of Exploration Results, Nyanzaga Project		
Criteria	**JORC Code explanation**	**Commentary**
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Airborne and ground magnetics, radiometric, VTEM, gravity and IP geophysical survey work was carried out that defines the stratigraphy, structures possibly influencing mineralisation and chargeability signatures reflecting the extent of disseminated sulphide replacement at depth. Additionally, satellite imagery (GeoImagery) and meta data images were procured. Bulk Density was carried out on 56,040 core samples for the SML area, collected every 1m interval down hole in selected DD drill holes. 17,020 records of geotechnical data have been documented within the SML dataset by recording alpha, beta, dip direction and structure type. 34,115 records of rock characteristics have been documented within the SML dataset by recording lithology type, texture, weathering, alteration and veining. The 2006 Nyanzaga metallurgical work indicated elevated arsenic (As 230-340ppm As) and mercury (Hg 3-98ppm Hg); but low silver, antimony and molybdenum potential deleterious or contaminating substances present. The 2022 Kilimani metallurgical test work carried out on 6 oxide samples indicated overall gold extraction (gravity and leach) of 93-98%, averaging 96%. Fast leach kinetics with >90% extraction within the first four hours and ultimate extraction achieved within 12-24 hours. The comminution test work, reported at closing screen size of 106µm, indicated that the Kilimani oxide material has a soft to medium hardness (BWi 9.0-15.3kw/h) and low competency (SMC A x b 2987.2 – 66.9). No evidence of preg-robbing was found. In all the 2022 test work samples, the organic carbon, arsenic, antimony and tellurium levels are comparable to that in Nyanzaga oxide material, indicating that these elements are highly unlikely to cause any gold extraction complications.
Further work	*The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).*	Planning for follow up exploration is underway for potential further testing of: • The Wingi Igneous Complex; • The west limb of the Nyanzaga Anticline; • Extensions to the Kilimani feeder structures, and in particular, the north end of the South Fault.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	N/A

APPENDIX 2 – RC/DD DRILLING SIGNIFICANT INTERCEPTS

		Arc1960 UTM 36S						Min 2m @ 0.25 g/t Au				Min 2m @ 0.5 g/t Au				Min 2m @ 1.0 g/t Au			
SiteID	Drill Type	East	North	Elev	Tdepth	Dip	Azi	From	To	Interval	Au (g/t)	From	To	Interval	Au (g/t)	From	To	Interval	Au (g/t)
NYZRC1313	RC	467,883	9,672,804	1,255	216	-68	37	107	130	23	1.01	110	112	2	0.63	124	130	6	2.77
								137	139	2	0.37	118	120	2	1.00				
								142	145	3	0.27	124	130	6	2.77				
								148	153	5	0.40	167	171	4	0.72				
								167	172	5	0.67								
NYZRC1314	RC	467,842	9,672,820	1,255	148	-73	33	6	10	4	0.77	6	8	2	1.39	6	8	2	1.39
								33	35	2	0.36	111	116	5	0.89				
								80	83	3	0.30	137	139	2	0.67				
								87	89	2	0.32								
								106	118	12	0.59								
								122	124	2	0.29								
								137	139	2	0.67								
NYZRC1315	RC	467,824	9,672,855	1,259	160	-75	35	2	8	6	0.33	135	142	7	4.69	135	142	7	4.69
								44	47	3	0.42								
								76	78	2	0.44								
								135	142	7	4.69								
NYZRC1316	RC	467,788	9,672,877	1,261	82	-68	37		13	13	0.86		12	12	0.91				
								25	30	5	0.87	25	30	5	0.87				
								44	46	2	0.29								
								55	58	3	0.31								
								64	68	4	0.28								
								71	76	5	0.44								
NYZRC1318	RC	467,707	9,672,904	1,261	170	-62	35	120	141	21	0.51	120	122	2	0.74	125	127	2	1.35
								151	158	7	0.53	125	129	4	0.99				
NYZRC1319	RC	467,691	9,672,880	1,259	171	-72	35	80	109	29	0.86	80	108	28	0.88	88	101	13	1.09
								137	169	32	0.79	137	140	3	1.58	149	154	5	1.24
												144	165	21	0.86	159	163	4	1.00
NYZRC1320	RC	467,632	9,672,880	1,258	151	-77	35	100	107	7	0.27								

		Arc1960 UTM 36S						Min 2m @ 0.25 g/t Au				Min 2m @ 0.5 g/t Au				Min 2m @ 1.0 g/t Au			
SiteID	Drill Type	East	North	Elev	Tdepth	Dip	Azi	From	To	Interval	Au (g/t)	From	To	Interval	Au (g/t)	From	To	Interval	Au (g/t)
								136	138	2	0.33								
NYZRC1321	RC	468,585	9,672,760	1,339	200	-57	235	146	149	3	0.56	146	149	3	0.56				
								167	169	2	0.32								
NYZRC1322	RC	468,603	9,672,714	1,327	228	-67	215	70	72	2	0.76								
								118	122	4	0.31								
								218	225	7	0.35								
NYZRC1323	RC	468,243	9,672,838	1,302	156	-65	35	13	24	11	0.93	13	17	4	1.42	13	15	2	2.08
								34	36	2	0.35	20	24	4	0.92	20	22	2	1.13
								39	58	19	0.71	40	45	5	1.18	41	44	3	1.44
								69	72	3	0.65	49	52	3	1.33	49	52	3	1.33
								75	82	7	0.46	69	72	3	0.65	89	91	2	1.26
								89	93	4	0.79	78	81	3	0.68				
												89	91	2	1.26				
NYZRC1324	RC	467,959	9,673,039	1,311	220	-60	215	12	15	3	0.41	44	46	2	0.64	87	91	4	1.65
								25	27	2	0.43	87	91	4	1.65				
								44	50	6	0.44	94	102	8	0.66				
								55	57	2	0.49	106	111	5	0.75				
								63	67	4	0.29								
								74	78	4	0.39								
								86	102	16	0.80								
								105	113	8	0.62								
								166	175	9	0.39								
								179	182	3	0.70								
								189	192	3	0.26								
NYZRC1325	RC	468,352	9,672,914	1,345	280	-63	215	94	125	31	0.80	95	105	10	1.00	95	97	2	2.01
								153	155	2	0.29	110	114	4	1.53	110	114	4	1.53
												121	125	4	0.88				
NYZRC1326	RC	468,376	9,672,878	1,337	214	-77	215	52	57	5	0.66	52	56	4	0.73	100	124	24	2.15
								87	97	10	1.39	87	91	4	1.25				
								100	142	42	1.43	94	97	3	2.70				
								155	157	2	0.26	100	126	26	2.05				
								179	184	5	1.09	131	136	5	0.61				

		Arc1960 UTM 36S						Min 2m @ 0.25 g/t Au				Min 2m @ 0.5 g/t Au				Min 2m @ 1.0 g/t Au			
SiteID	Drill Type	East	North	Elev	Tdepth	Dip	Azi	From	To	Interval	Au (g/t)	From	To	Interval	Au (g/t)	From	To	Interval	Au (g/t)
												179	182	3	1.56				
NYZRC1327	RC	468,511	9,672,797	1,337	210	-63	215	136	143	7	0.80	136	143	7	0.80	139	141	2	1.18
NYZRCDD1312	DD	466,916	9,672,585	1,223	602	-60	92	587	589	2	0.49	599	602	3.05	1.10				
								594	602.1	8.05	0.76								
NYZRCDD1317	DD	467,733	9,672,869	1,258	225	-75	35	41	58	17	0.41	41	45	4	0.55	93	95	2	1.74
								80	83	3	0.45	54	56	2	0.90	98	100	2	1.09
								89	113	24	0.70	93	102	9	1.04	174	177	3	2.83
								127	136	9	0.42	105	112	7	0.70				
								172	177	5	1.79	174	177	3	2.83				

Notes: (i) East, North, Elev (Elevation), TDepth (Total Depth), To, From and Interval are recorded in metres

APPENDIX 3 – AC DRILLING SIGNFICANT INTERCEPTS

		Arc1960 UTM 36S						Min 2m @ 0.1 g/t Au				Min 2m @ 1 g/t Au			
SiteID	Drill Type	East	North	Elev	Tdepth	Dip	Azi	From	To	Interval	Au	From	To	Interval	Au
NYGAC1537	AC	465,736	9,673,759	1,191	73	-90	0	12	14	2	0.75				
								24	28	4	0.34				
NYGAC1551	AC	466,237	9,673,554	1,225	79	-90	0	60	64	4	0.13				
NYGAC1566	AC	465,886	9,673,356	1,194	55	-90	0	48	52	4	0.46				
NYGAC1586	AC	466,538	9,673,456	1,253	83	-90	0	52	56	4	0.21				
NYGAC1591	AC	466,484	9,673,254	1,234	67	-90	0	56	60	4	0.31				
NYGAC1606	AC	466,438	9,673,158	1,228	103	-90	0	84	88	4	0.15				
NYGAC1616	AC	466,086	9,673,057	1,201	63	-90	0	0	4	4	0.12				
NYGAC1621	AC	466,484	9,672,956	1,223	61	-90	0	52	56	4	0.31				
NYGAC1636	AC	465,936	9,672,757	1,193	67	-90	0	36	40	4	0.12				
NYGAC1697	AC	466,403	9,670,701	1,170	55	-90	0	0	4	4	1.04	0	4	4	1.04
								8	20	12	1.81	12	16	4	4.07
								24	32	8	0.15				
NYGAC1713	AC	467,247	9,669,903	1,152	34	-90	0	24	28	4	0.11				
NYGAC1720	AC	466,367	9,671,504	1,185	76	-90	0	40	44	4	1.59	40	44	4	1.59
NYGAC1724	AC	465,899	9,671,504	1,171	57	-90	0	48	55	7	0.40				

APPENDIX 4 – DRILL HOLES WITH NO SIGNIFICANT INTERCEPTS (2021 AND 2022)

		Arc1960 UTM 36S					
SiteID	Drill Type	East	North	Elev (m)	Tdepth (m)	Dip (°)	Azi (°)
NYGAC1342	AC	466,307	9,672,612	1,203	55	-90	0
NYGAC1343	AC	466,308	9,672,494	1,203	36	-90	0
NYGAC1344	AC	466,368	9,672,493	1,205	47	-90	0
NYGAC1345	AC	466,409	9,672,491	1,206	35	-90	0
NYGAC1346	AC	466,446	9,672,493	1,207	35	-90	0
NYGAC1347	AC	466,527	9,672,487	1,210	36	-90	0
NYGAC1348	AC	466,608	9,672,494	1,212	35	-90	0
NYGAC1349	AC	466,654	9,672,488	1,214	29	-90	0
NYGAC1350	AC	466,696	9,672,493	1,215	36	-90	0
NYGAC1351	AC	466,741	9,672,491	1,216	36	-90	0
NYGAC1352	AC	466,769	9,672,489	1,217	30	-90	0
NYGAC1353	AC	466,811	9,672,491	1,219	33	-90	0
NYGAC1354	AC	466,786	9,672,610	1,219	33	-90	0
NYGAC1355	AC	466,747	9,672,614	1,217	42	-90	0
NYGAC1356	AC	466,708	9,672,613	1,216	29	-90	0
NYGAC1357	AC	466,667	9,672,615	1,215	32	-90	0
NYGAC1358	AC	466,550	9,673,083	1,232	48	-90	0
NYGAC1359	AC	466,619	9,673,083	1,237	65	-90	0
NYGAC1360	AC	466,700	9,673,083	1,242	65	-90	0
NYGAC1361	AC	466,779	9,673,083	1,246	65	-90	0
NYGAC1362	AC	466,859	9,673,083	1,249	48	-90	0
NYGAC1363	AC	466,859	9,672,964	1,240	47	-90	0
NYGAC1364	AC	466,779	9,672,963	1,238	54	-90	0
NYGAC1365	AC	466,701	9,672,964	1,235	65	-90	0
NYGAC1366	AC	466,779	9,672,842	1,229	35	-90	0
NYGAC1367	AC	466,619	9,672,843	1,225	46	-90	0
NYGAC1368	AC	466,539	9,672,722	1,213	46	-90	0
NYGAC1369	AC	466,697	9,672,722	1,219	45	-90	0
NYGAC1370	AC	466,861	9,672,721	1,224	59	-90	0
NYGAC1371	AC	466,512	9,672,980	1,225	43	-90	0
NYGAC1372	AC	465,958	9,672,042	1,182	50	-90	0
NYGAC1373	AC	465,956	9,672,117	1,184	53	-90	0
NYGAC1374	AC	465,959	9,672,204	1,188	12	-90	0
NYGAC1375	AC	465,956	9,672,363	1,192	18	-90	0
NYGAC1376	AC	465,959	9,672,288	1,193	18	-90	0
NYGAC1377	AC	466,080	9,672,443	1,196	22	-90	0
NYGAC1378	AC	466,079	9,672,361	1,197	53	-90	0
NYGAC1379	AC	466,076	9,672,281	1,203	47	-90	0
NYGAC1380	AC	466,078	9,672,125	1,189	65	-90	0
NYGAC1381	AC	466,079	9,672,042	1,186	48	-90	0
NYGAC1382	AC	466,199	9,672,003	1,189	60	-90	0
NYGAC1383	AC	466,199	9,672,042	1,190	52	-90	0

		Arc1960 UTM 36S					
SiteID	Drill Type	East	North	Elev (m)	Tdepth (m)	Dip (°)	Azi (°)
NYGAC1384	AC	466,198	9,672,081	1,191	54	-90	0
NYGAC1385	AC	466,196	9,672,122	1,193	60	-90	0
NYGAC1386	AC	466,196	9,672,165	1,200	58	-90	0
NYGAC1387	AC	466,082	9,672,206	1,207	60	-90	0
NYGAC1388	AC	467,837	9,672,403	1,237	49	-90	0
NYGAC1389	AC	467,870	9,672,324	1,233	50	-90	0
NYGAC1390	AC	467,889	9,672,371	1,230	31	-90	0
NYGAC1391	AC	466,793	9,672,373	1,222	40	-90	0
NYGAC1392	AC	466,753	9,672,374	1,220	40	-90	0
NYGAC1393	AC	466,710	9,672,371	1,218	40	-90	0
NYGAC1394	AC	466,670	9,672,373	1,216	40	-90	0
NYGAC1395	AC	466,632	9,672,371	1,214	40	-90	0
NYGAC1396	AC	466,582	9,672,369	1,212	40	-90	0
NYGAC1397	AC	466,548	9,672,371	1,210	40	-90	0
NYGAC1398	AC	466,508	9,672,373	1,209	40	-90	0
NYGAC1399	AC	466,428	9,672,373	1,205	40	-90	0
NYGAC1400	AC	466,389	9,672,374	1,204	40	-90	0
NYGAC1401	AC	466,309	9,672,371	1,201	40	-90	0
NYGAC1402	AC	466,309	9,672,252	1,200	40	-90	0
NYGAC1403	AC	466,309	9,672,133	1,198	40	-90	0
NYGAC1404	AC	466,308	9,672,053	1,194	40	-90	0
NYGAC1405	AC	466,390	9,672,054	1,198	40	-90	0
NYGAC1406	AC	466,468	9,672,056	1,202	40	-90	0
NYGAC1407	AC	466,549	9,672,055	1,207	40	-90	0
NYGAC1408	AC	466,591	9,672,131	1,212	40	-90	0
NYGAC1409	AC	466,553	9,672,125	1,209	40	-90	0
NYGAC1410	AC	466,510	9,672,132	1,206	40	-90	0
NYGAC1411	AC	466,469	9,672,133	1,204	40	-90	0
NYGAC1412	AC	466,427	9,672,132	1,201	40	-90	0
NYGAC1413	AC	466,389	9,672,133	1,200	40	-90	0
NYGAC1414	AC	466,386	9,672,253	1,203	40	-90	0
NYGAC1415	AC	466,428	9,672,251	1,204	40	-90	0
NYGAC1416	AC	466,549	9,672,252	1,210	40	-90	0
NYGAC1417	AC	466,588	9,672,251	1,212	40	-90	0
NYGAC1418	AC	466,626	9,672,615	1,214	40	-90	0
NYGAC1419	AC	466,588	9,672,611	1,212	40	-90	0
NYGAC1420	AC	466,549	9,672,612	1,211	40	-90	0
NYGAC1421	AC	466,468	9,672,612	1,208	40	-90	0
NYGAC1422	AC	466,391	9,672,613	1,206	40	-90	0
NYGAC1423	AC	465,175	9,673,263	1,169	50	-90	0
NYGAC1424	AC	465,215	9,673,292	1,170	50	-90	0
NYGAC1425	AC	465,250	9,673,325	1,171	50	-90	0
NYGAC1426	AC	465,283	9,673,364	1,172	50	-90	0

		Arc1960 UTM 36S					
SiteID	Drill Type	East	North	Elev (m)	Tdepth (m)	Dip (°)	Azi (°)
NYGAC1427	AC	465,324	9,673,394	1,173	50	-90	0
NYGAC1428	AC	465,367	9,673,413	1,173	50	-90	0
NYGAC1429	AC	465,408	9,673,450	1,174	50	-90	0
NYGAC1430	AC	465,446	9,673,478	1,174	50	-90	0
NYGAC1431	AC	465,498	9,673,507	1,176	50	-90	0
NYGAC1432	AC	465,544	9,673,515	1,177	50	-90	0
NYGAC1433	AC	465,589	9,673,522	1,179	50	-90	0
NYGAC1434	AC	465,278	9,673,086	1,172	50	-90	0
NYGAC1435	AC	465,352	9,673,074	1,175	50	-90	0
NYGAC1436	AC	465,307	9,673,081	1,174	50	-90	0
NYGAC1437	AC	465,400	9,673,065	1,177	50	-90	0
NYGAC1438	AC	465,509	9,673,146	1,179	50	-90	0
NYGAC1439	AC	465,416	9,673,154	1,176	50	-90	0
NYGAC1440	AC	465,460	9,673,143	1,178	50	-90	0
NYGAC1441	AC	465,555	9,673,158	1,180	50	-90	0
NYGAC1442	AC	465,587	9,673,189	1,182	50	-90	0
NYGAC1443	AC	465,635	9,673,209	1,182	50	-90	0
NYGAC1444	AC	465,684	9,673,199	1,184	50	-90	0
NYGAC1445	AC	465,734	9,673,205	1,186	50	-90	0
NYGAC1446	AC	465,783	9,673,214	1,188	37	-90	0
NYGAC1447	AC	465,476	9,673,940	1,176	45	-90	0
NYGAC1448	AC	465,526	9,673,943	1,177	45	-90	0
NYGAC1449	AC	465,175	9,673,263	1,169	49	-90	0
NYGAC1450	AC	465,463	9,672,846	1,180	49	-90	0
NYGAC1451	AC	465,519	9,672,847	1,182	50	-90	0
NYGAC1452	AC	465,570	9,672,849	1,183	50	-90	0
NYGAC1453	AC	465,613	9,672,840	1,185	50	-90	0
NYGAC1454	AC	465,666	9,672,831	1,186	50	-90	0
NYGAC1455	AC	465,714	9,672,830	1,188	50	-90	0
NYGAC1456	AC	465,588	9,672,379	1,182	46	-90	0
NYGAC1457	AC	465,631	9,672,408	1,184	23	-90	0
NYGAC1458	AC	465,671	9,672,439	1,185	31	-90	0
NYGAC1459	AC	465,709	9,672,470	1,186	43	-90	0
NYGAC1460	AC	465,751	9,672,498	1,187	49	-90	0
NYGAC1461	AC	465,791	9,672,530	1,188	50	-90	0
NYGAC1462	AC	465,617	9,672,121	1,179	41	-90	0
NYGAC1463	AC	465,669	9,672,143	1,181	40	-90	0
NYGAC1464	AC	465,690	9,672,170	1,182	37	-90	0
NYGAC1465	AC	465,748	9,672,209	1,184	50	-90	0
NYGAC1466	AC	465,802	9,672,194	1,184	50	-90	0
NYGAC1467	AC	465,847	9,672,213	1,185	50	-90	0
NYGAC1468	AC	465,897	9,672,226	1,186	49	-90	0
NYGAC1469	AC	466,006	9,672,119	1,186	50	-90	0

		Arc1960 UTM 36S					
SiteID	Drill Type	East	North	Elev (m)	Tdepth (m)	Dip (°)	Azi (°)
NYGAC1470	AC	465,972	9,672,081	1,184	50	-90	0
NYGAC1471	AC	465,941	9,672,044	1,181	50	-90	0
NYGAC1472	AC	465,909	9,672,002	1,180	50	-90	0
NYGAC1473	AC	465,878	9,671,965	1,178	40	-90	0
NYGAC1474	AC	465,854	9,671,927	1,177	34	-90	0
NYGAC1475	AC	465,829	9,671,895	1,176	31	-90	0
NYGAC1476	AC	466,229	9,671,947	1,188	50	-90	0
NYGAC1477	AC	466,272	9,671,976	1,191	50	-90	0
NYGAC1478	AC	466,313	9,672,002	1,193	50	-90	0
NYGAC1479	AC	466,351	9,672,034	1,196	50	-90	0
NYGAC1480	AC	466,188	9,671,917	1,186	50	-90	0
NYGAC1481	AC	466,147	9,671,886	1,184	50	-90	0
NYGAC1482	AC	466,113	9,671,853	1,181	50	-90	0
NYGAC1483	AC	466,079	9,671,818	1,179	50	-90	0
NYGAC1484	AC	466,048	9,671,779	1,177	50	-90	0
NYGAC1485	AC	466,015	9,671,737	1,175	50	-90	0
NYGAC1486	AC	465,992	9,671,695	1,174	50	-90	0
NYGAC1487	AC	465,973	9,671,646	1,173	42	-90	0
NYGAC1488	AC	465,950	9,671,603	1,172	50	-90	0
NYGAC1489	AC	466,360	9,671,630	1,185	50	-90	0
NYGAC1490	AC	466,396	9,671,655	1,187	50	-90	0
NYGAC1491	AC	466,420	9,671,687	1,189	50	-90	0
NYGAC1492	AC	466,464	9,671,712	1,192	50	-90	0
NYGAC1493	AC	466,511	9,671,728	1,195	50	-90	0
NYGAC1494	AC	466,918	9,671,705	1,217	85	-90	0
NYGAC1495	AC	467,128	9,671,704	1,225	67	-90	0
NYGAC1496	AC	466,535	9,673,184	1,236	50	-90	0
NYGAC1497	AC	466,569	9,673,208	1,240	50	-90	0
NYGAC1498	AC	466,563	9,673,242	1,240	50	-90	0
NYGAC1499	AC	466,583	9,673,290	1,244	50	-90	0
NYGAC1500	AC	466,325	9,673,014	1,214	27	-90	0
NYGAC1501	AC	466,279	9,673,000	1,210	34	-90	0
NYGAC1502	AC	466,230	9,672,987	1,208	50	-90	0
NYGAC1503	AC	466,179	9,672,973	1,204	50	-90	0
NYGAC1504	AC	466,134	9,672,953	1,202	50	-90	0
NYGAC1505	AC	466,252	9,673,117	1,210	50	-90	0
NYGAC1506	AC	466,202	9,673,105	1,207	50	-90	0
NYGAC1507	AC	466,152	9,673,100	1,204	50	-90	0
NYGAC1508	AC	466,053	9,673,083	1,199	31	-90	0
NYGAC1509	AC	466,103	9,673,087	1,202	50	-90	0
NYGAC1510	AC	466,489	9,673,387	1,239	50	-90	0
NYGAC1511	AC	466,455	9,673,349	1,234	50	-90	0
NYGAC1512	AC	466,418	9,673,318	1,230	50	-90	0

		Arc1960 UTM 36S					
SiteID	Drill Type	East	North	Elev (m)	Tdepth (m)	Dip (°)	Azi (°)
NYGAC1513	AC	465,590	9,674,157	1,181	50	-90	0
NYGAC1514	AC	465,636	9,674,157	1,183	50	-90	0
NYGAC1515	AC	465,687	9,674,157	1,185	50	-90	0
NYGAC1516	AC	465,736	9,674,158	1,187	50	-90	0
NYGAC1517	AC	465,787	9,674,156	1,189	50	-90	0
NYGAC1518	AC	465,839	9,674,157	1,192	50	-90	0
NYGAC1519	AC	465,888	9,674,157	1,196	50	-90	0
NYGAC1520	AC	465,931	9,674,156	1,199	79	-90	0
NYGAC1521	AC	465,987	9,674,155	1,205	83	-90	0
NYGAC1522	AC	466,037	9,674,155	1,212	85	-90	0
NYGAC1523	AC	466,087	9,674,156	1,219	73	-90	0
NYGAC1524	AC	466,185	9,673,957	1,237	73	-90	0
NYGAC1525	AC	466,136	9,673,958	1,229	85	-90	0
NYGAC1526	AC	466,086	9,673,958	1,222	91	-90	0
NYGAC1527	AC	466,039	9,673,957	1,218	97	-90	0
NYGAC1528	AC	465,980	9,673,962	1,212	67	-90	0
NYGAC1529	AC	465,936	9,673,957	1,207	96	-90	0
NYGAC1530	AC	465,884	9,673,955	1,202	89	-90	0
NYGAC1531	AC	465,837	9,673,955	1,196	72	-90	0
NYGAC1532	AC	465,786	9,673,956	1,190	79	-90	0
NYGAC1533	AC	465,736	9,673,958	1,187	55	-90	0
NYGAC1534	AC	465,687	9,673,956	1,185	60	-90	0
NYGAC1535	AC	465,640	9,673,960	1,182	67	-90	0
NYGAC1536	AC	465,687	9,673,756	1,188	61	-90	0
NYGAC1538	AC	465,790	9,673,757	1,194	67	-90	0
NYGAC1539	AC	465,834	9,673,756	1,199	65	-90	0
NYGAC1540	AC	465,887	9,673,755	1,204	82	-90	0
NYGAC1541	AC	465,940	9,673,757	1,210	83	-90	0
NYGAC1542	AC	465,990	9,673,756	1,215	92	-90	0
NYGAC1543	AC	466,035	9,673,756	1,219	79	-90	0
NYGAC1544	AC	466,084	9,673,758	1,224	91	-90	0
NYGAC1545	AC	466,134	9,673,756	1,228	97	-90	0
NYGAC1546	AC	466,186	9,673,757	1,234	103	-90	0
NYGAC1547	AC	466,237	9,673,757	1,239	55	-90	0
NYGAC1548	AC	466,284	9,673,758	1,244	85	-90	0
NYGAC1549	AC	466,336	9,673,757	1,248	73	-90	0
NYGAC1550	AC	466,288	9,673,555	1,226	91	-90	0
NYGAC1552	AC	466,186	9,673,557	1,222	77	-90	0
NYGAC1553	AC	466,134	9,673,557	1,218	67	-90	0
NYGAC1554	AC	466,086	9,673,556	1,215	65	-90	0
NYGAC1555	AC	466,036	9,673,558	1,211	56	-90	0
NYGAC1556	AC	465,982	9,673,557	1,207	70	-90	0
NYGAC1557	AC	465,934	9,673,556	1,202	43	-90	0

		Arc1960 UTM 36S					
SiteID	Drill Type	East	North	Elev (m)	Tdepth (m)	Dip (°)	Azi (°)
NYGAC1558	AC	465,882	9,673,565	1,199	40	-90	0
NYGAC1559	AC	465,836	9,673,559	1,196	43	-90	0
NYGAC1560	AC	465,776	9,673,552	1,192	43	-90	0
NYGAC1561	AC	465,739	9,673,554	1,189	60	-90	0
NYGAC1562	AC	465,684	9,673,558	1,184	47	-90	0
NYGAC1563	AC	465,733	9,673,357	1,187	42	-90	0
NYGAC1564	AC	465,786	9,673,356	1,189	51	-90	0
NYGAC1565	AC	465,837	9,673,356	1,192	50	-90	0
NYGAC1567	AC	465,934	9,673,355	1,197	43	-90	0
NYGAC1568	AC	465,985	9,673,356	1,200	55	-90	0
NYGAC1569	AC	466,036	9,673,357	1,203	49	-90	0
NYGAC1570	AC	466,085	9,673,356	1,205	48	-90	0
NYGAC1571	AC	466,132	9,673,355	1,207	76	-90	0
NYGAC1572	AC	466,184	9,673,356	1,210	75	-90	0
NYGAC1573	AC	466,234	9,673,354	1,213	72	-90	0
NYGAC1574	AC	466,287	9,673,356	1,217	76	-90	0
NYGAC1575	AC	466,336	9,673,361	1,222	79	-90	0
NYGAC1576	AC	466,390	9,673,354	1,227	85	-90	0
NYGAC1577	AC	466,481	9,673,354	1,236	61	-90	0
NYGAC1578	AC	466,534	9,673,356	1,243	67	-90	0
NYGAC1579	AC	466,586	9,673,358	1,247	61	-90	0
NYGAC1580	AC	466,235	9,673,456	1,217	79	-90	0
NYGAC1581	AC	466,285	9,673,457	1,220	79	-90	0
NYGAC1582	AC	466,336	9,673,460	1,224	85	-90	0
NYGAC1583	AC	466,386	9,673,456	1,230	76	-90	0
NYGAC1584	AC	466,436	9,673,456	1,236	54	-90	0
NYGAC1585	AC	466,484	9,673,455	1,243	55	-90	0
NYGAC1587	AC	466,579	9,673,457	1,257	77	-90	0
NYGAC1588	AC	466,636	9,673,256	1,247	91	-90	0
NYGAC1589	AC	466,586	9,673,255	1,243	49	-90	0
NYGAC1590	AC	466,538	9,673,252	1,239	55	-90	0
NYGAC1592	AC	466,432	9,673,252	1,230	91	-90	0
NYGAC1593	AC	466,386	9,673,255	1,226	39	-90	0
NYGAC1594	AC	466,333	9,673,250	1,221	43	-90	0
NYGAC1595	AC	466,286	9,673,256	1,216	70	-90	0
NYGAC1596	AC	466,236	9,673,253	1,210	100	-90	0
NYGAC1597	AC	466,185	9,673,255	1,207	74	-90	0
NYGAC1598	AC	466,133	9,673,256	1,204	100	-90	0
NYGAC1599	AC	466,086	9,673,252	1,202	67	-90	0
NYGAC1600	AC	466,036	9,673,256	1,200	49	-90	0
NYGAC1601	AC	465,990	9,673,252	1,198	55	-90	0
NYGAC1602	AC	465,933	9,673,254	1,195	54	-90	0
NYGAC1603	AC	466,585	9,673,155	1,238	85	-90	0

		Arc1960 UTM 36S					
SiteID	Drill Type	East	North	Elev (m)	Tdepth (m)	Dip (°)	Azi (°)
NYGAC1604	AC	466,533	9,673,158	1,235	91	-90	0
NYGAC1605	AC	466,485	9,673,158	1,231	97	-90	0
NYGAC1607	AC	466,384	9,673,158	1,221	91	-90	0
NYGAC1608	AC	466,335	9,673,157	1,217	103	-90	0
NYGAC1609	AC	466,287	9,673,150	1,213	73	-90	0
NYGAC1610	AC	466,236	9,673,156	1,209	96	-90	0
NYGAC1611	AC	466,137	9,673,158	1,204	49	-90	0
NYGAC1612	AC	466,083	9,673,157	1,201	43	-90	0
NYGAC1613	AC	466,038	9,673,155	1,199	49	-90	0
NYGAC1614	AC	466,235	9,673,056	1,209	65	-90	0
NYGAC1615	AC	466,135	9,673,055	1,203	54	-90	0
NYGAC1617	AC	466,037	9,673,056	1,198	52	-90	0
NYGAC1618	AC	465,987	9,673,055	1,196	48	-90	0
NYGAC1619	AC	465,938	9,673,054	1,194	48	-90	0
NYGAC1620	AC	466,533	9,672,955	1,225	73	-90	0
NYGAC1622	AC	466,435	9,672,958	1,219	67	-90	0
NYGAC1623	AC	466,384	9,672,958	1,216	71	-90	0
NYGAC1624	AC	466,336	9,672,958	1,213	51	-90	0
NYGAC1625	AC	466,283	9,672,957	1,209	44	-90	0
NYGAC1626	AC	466,235	9,672,958	1,207	54	-90	0
NYGAC1627	AC	466,084	9,672,958	1,200	42	-90	0
NYGAC1628	AC	466,034	9,672,958	1,198	66	-90	0
NYGAC1629	AC	465,985	9,672,956	1,196	48	-90	0
NYGAC1630	AC	465,935	9,672,957	1,194	48	-90	0
NYGAC1631	AC	465,886	9,672,956	1,193	48	-90	0
NYGAC1632	AC	465,836	9,672,955	1,191	52	-90	0
NYGAC1633	AC	465,783	9,672,967	1,189	54	-90	0
NYGAC1634	AC	465,736	9,673,156	1,187	36	-90	0
NYGAC1635	AC	465,787	9,673,156	1,188	56	-90	0
NYGAC1637	AC	465,984	9,672,758	1,195	55	-90	0
NYGAC1638	AC	466,035	9,672,756	1,196	61	-90	0
NYGAC1639	AC	466,085	9,672,755	1,198	67	-90	0
NYGAC1640	AC	466,131	9,672,758	1,200	73	-90	0
NYGAC1641	AC	466,236	9,672,755	1,202	79	-90	0
NYGAC1642	AC	466,285	9,672,755	1,204	43	-90	0
NYGAC1643	AC	466,339	9,672,759	1,208	49	-90	0
NYGAC1644	AC	466,386	9,672,752	1,211	55	-90	0
NYGAC1645	AC	466,446	9,672,754	1,214	55	-90	0
NYGAC1646	AC	466,486	9,672,751	1,214	55	-90	0
NYGAC1647	AC	465,389	9,672,699	1,177	49	-90	0
NYGAC1648	AC	465,349	9,672,700	1,176	67	-90	0
NYGAC1649	AC	465,300	9,672,699	1,174	67	-90	0
NYGAC1650	AC	465,250	9,672,697	1,169	49	-90	0

		Arc1960 UTM 36S					
SiteID	Drill Type	East	North	Elev (m)	Tdepth (m)	Dip (°)	Azi (°)
NYGAC1651	AC	465,198	9,672,292	1,171	31	-90	0
NYGAC1652	AC	465,250	9,672,306	1,173	55	-90	0
NYGAC1653	AC	465,301	9,672,298	1,174	59	-90	0
NYGAC1654	AC	465,348	9,672,303	1,175	45	-90	0
NYGAC1655	AC	465,400	9,672,301	1,177	65	-90	0
NYGAC1656	AC	465,446	9,672,295	1,178	68	-90	0
NYGAC1657	AC	465,495	9,672,303	1,179	61	-90	0
NYGAC1658	AC	465,551	9,672,302	1,181	70	-90	0
NYGAC1659	AC	465,597	9,672,300	1,182	61	-90	0
NYGAC1660	AC	465,302	9,671,897	1,167	55	-90	0
NYGAC1661	AC	465,349	9,671,899	1,168	60	-90	0
NYGAC1662	AC	465,398	9,671,899	1,169	61	-90	0
NYGAC1663	AC	465,450	9,671,899	1,170	64	-90	0
NYGAC1664	AC	465,492	9,671,899	1,170	43	-90	0
NYGAC1665	AC	465,550	9,671,901	1,171	41	-90	0
NYGAC1666	AC	465,604	9,671,899	1,173	35	-90	0
NYGAC1667	AC	465,651	9,671,897	1,173	36	-90	0
NYGAC1668	AC	465,701	9,671,900	1,174	31	-90	0
NYGAC1669	AC	465,752	9,671,901	1,173	31	-90	0
NYGAC1670	AC	465,902	9,671,899	1,175	41	-90	0
NYGAC1671	AC	465,951	9,671,898	1,176	51	-90	0
NYGAC1672	AC	466,000	9,671,902	1,177	55	-90	0
NYGAC1673	AC	466,050	9,671,901	1,179	61	-90	0
NYGAC1674	AC	466,248	9,671,904	1,187	47	-90	0
NYGAC1675	AC	466,501	9,671,502	1,189	58	-90	0
NYGAC1676	AC	466,452	9,671,503	1,187	74	-90	0
NYGAC1677	AC	466,347	9,671,502	1,183	82	-90	0
NYGAC1678	AC	466,253	9,671,497	1,180	67	-90	0
NYGAC1679	AC	466,152	9,671,499	1,177	33	-90	0
NYGAC1680	AC	466,052	9,671,501	1,175	55	-90	0
NYGAC1681	AC	465,951	9,671,501	1,172	58	-90	0
NYGAC1682	AC	465,854	9,671,500	1,169	65	-90	0
NYGAC1683	AC	465,752	9,671,501	1,167	52	-90	0
NYGAC1684	AC	465,653	9,671,502	1,166	52	-90	0
NYGAC1685	AC	465,998	9,671,107	1,169	67	-90	0
NYGAC1686	AC	466,098	9,671,104	1,172	51	-90	0
NYGAC1687	AC	466,200	9,671,105	1,174	46	-90	0
NYGAC1688	AC	466,348	9,671,102	1,177	47	-90	0
NYGAC1689	AC	466,445	9,671,104	1,180	35	-90	0
NYGAC1690	AC	466,552	9,671,100	1,183	52	-90	0
NYGAC1691	AC	466,647	9,671,104	1,186	43	-90	0
NYGAC1692	AC	467,194	9,670,705	1,176	35	-90	0
NYGAC1693	AC	467,107	9,670,699	1,174	48	-90	0

		Arc1960 UTM 36S					
SiteID	Drill Type	East	North	Elev (m)	Tdepth (m)	Dip (°)	Azi (°)
NYGAC1694	AC	467,000	9,670,699	1,174	58	-90	0
NYGAC1695	AC	466,603	9,670,702	1,174	72	-90	0
NYGAC1696	AC	466,499	9,670,706	1,172	57	-90	0
NYGAC1698	AC	466,300	9,670,700	1,167	31	-90	0
NYGAC1699	AC	466,699	9,670,303	1,161	63	-90	0
NYGAC1700	AC	466,798	9,670,304	1,161	55	-90	0
NYGAC1701	AC	466,897	9,670,301	1,159	55	-90	0
NYGAC1702	AC	467,000	9,670,306	1,157	42	-90	0
NYGAC1703	AC	467,099	9,670,306	1,156	30	-90	0
NYGAC1704	AC	467,198	9,670,306	1,156	41	-90	0
NYGAC1705	AC	467,296	9,670,305	1,157	56	-90	0
NYGAC1706	AC	467,397	9,670,305	1,158	55	-90	0
NYGAC1707	AC	467,486	9,670,301	1,159	46	-90	0
NYGAC1708	AC	467,600	9,670,307	1,161	49	-90	0
NYGAC1709	AC	467,686	9,670,307	1,167	56	-90	0
NYGAC1710	AC	467,545	9,669,904	1,165	31	-90	0
NYGAC1711	AC	467,452	9,669,902	1,160	19	-90	0
NYGAC1712	AC	467,351	9,669,905	1,155	31	-90	0
NYGAC1714	AC	467,145	9,669,905	1,151	46	-90	0
NYGAC1715	AC	467,051	9,669,906	1,150	43	-90	0
NYGAC1716	AC	467,301	9,669,903	1,153	37	-90	0
NYGAC1717	AC	467,246	9,670,305	1,156	43	-90	0
NYGAC1718	AC	467,148	9,670,301	1,156	31	-90	0
NYGAC1719	AC	467,050	9,670,305	1,156	39	-90	0
NYGAC1721	AC	466,199	9,671,505	1,178	61	-90	0
NYGAC1722	AC	466,100	9,671,503	1,176	70	-90	0
NYGAC1723	AC	466,001	9,671,504	1,173	75	-90	0
NYGAC1725	AC	465,800	9,671,504	1,168	61	-90	0
NYZGT0062	RC-DD	467,089	9,672,454	1,238	250.13	-55	128
NYZGT0063	RC-DD	466,899	9,672,525	1,223	200.30	-60	90
NYZGT0064	RC-DD	466,918	9,672,482	1,225	200.00	-60	92
NYZGT0065	DD	466,902	9,672,524	1,222	150.30	-80	90
NYZGT0066	RC	466,890	9,672,525	1,222	250.00	-90	0