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ASX ANNOUNCEMENT / MEDIA RELEASE

ASX: PRX

10 March 2023

Buccaneer Gold Project - Metallurgical Update

KEY POINTS

- **Metallurgical testwork completed on representative samples from the Buccaneer gold deposit by Independent Metallurgical Operations (IMO).**
- **Comminution testwork revealed all three composites (oxide, transitional and fresh) are amenable to conventional crushing and grinding processes.**
- **Gravity gold and cyanide leach testwork returned recoveries of 95.1%, 96.7% and 84.6% for the oxide, transition and fresh composites, respectively with gravity gold recoveries averaging 18.6%.**
    - ***fastest kinetics achieved for the oxide and transition composites.***
    - ***low cyanide and lime consumption for each of the oxide, transition and fresh composites.***
- **Low overall gold recoveries in the column leach testwork has shown that heap leaching is not a viable option for the Company.**
- **Study to evaluate processing and mining scenarios for the Buccaneer Mineral Resource continues, including the assessment of IMO's recommendations outlined in the technical report.**

Prodigy Gold NL (ASX: PRX) ("Prodigy Gold" or the "Company") is pleased to announce an update on activities underway on its 100% owned Buccaneer Project in the Tanami region of the Northern Territory. Independent Metallurgical Operations Pty Ltd ("IMO") were engaged by Prodigy Gold in 2022 to undertake metallurgical testwork on a series of gold bearing diamond core samples from the Buccaneer Project to a scoping study level. The testwork was initiated to determine the amenability of oxide, transition and fresh (sulphide) lithographs to gravity gold, carbon-in-leach ("CIL") and heap leach gold recovery. The results released in this announcement relate to metallurgical analyses for previously reported holes BCDD2102[1,2,], BCDD2103[3], BCDD2104[4,2] and BCDD2105[5,2] and BCDD2109[6] .

[1] ASX: 17 December 2021
[2] ASX: 11 February 2022
[3] ASX: 29 November 2021
[4] ASX: 29 November 2021
[5] ASX: 17 December 2021
[6] ASX: 29 November 2021

Management Commentary

Prodigy Gold Managing Director, Mark Edwards said: *"The Company is continuing with mining studies on the Buccaneer Mineral Resource to determine the best approach for advancing this project from an exploration target to a development project. The metallurgical testwork program completed over 2022 was designed to simulate the gold extraction performance of the run-of-mine material that could be processed on a heap leach pad or through a standard CIL plant, such as the facilities already located in the Tanami region.*

The 2.3km long monzogranite host rock at Buccaneer is the key control of the gold mineralisation. The majority of drilling is focussed in the southern 500 to 700 metres of this body, with good potential for additions to the existing resource to the north where drill spacing increases or the monzogranite remains significantly under-drilled. The requirement for future drilling work will form part of the strategic plan that is being developed as part of this ongoing study.

The testwork included in this release is now complete, highlighting that a combination of gravity and CIL processing is the most efficient way to extract the gold. Heap leaching is no longer the preferred option due to lower than expected gold recoveries. Going forward, the Company will focus on the gravity and CIL option."

Metallurgical Diamond Drilling and Testwork Introduction

An 8-hole program of geotechnical and metallurgical diamond core drilling, completed at the end of 2021, aimed at providing samples for metallurgical recovery testwork and to optimise the crush size for multiple extraction scenarios. Drill locations can be found in Figure 13, and Appendix 1, with results previously announced by Prodigy Gold on 29 November 2021, 17 December 2021 and 11 February 2022.

Preliminary metallurgical recovery testwork, including the testing of gold recoveries, leach times and consumption rates of key reagents, such as lime and cyanide, has now been completed. Crushing testwork indices for the three categories of rock, oxide, transition and fresh, as well as intermittent bottle roll ("IBR") tests at different crush sizes, and column leach tests were also completed during this process. The results of this testwork have now been reported and presented to the Company by IMO, along with recommendations for further testwork.

The gravity gold and cyanide leach option resulted in the fastest kinetics with the oxide and transition composites achieving the highest overall recoveries compared with the column leach gold recoveries (Figure 1).

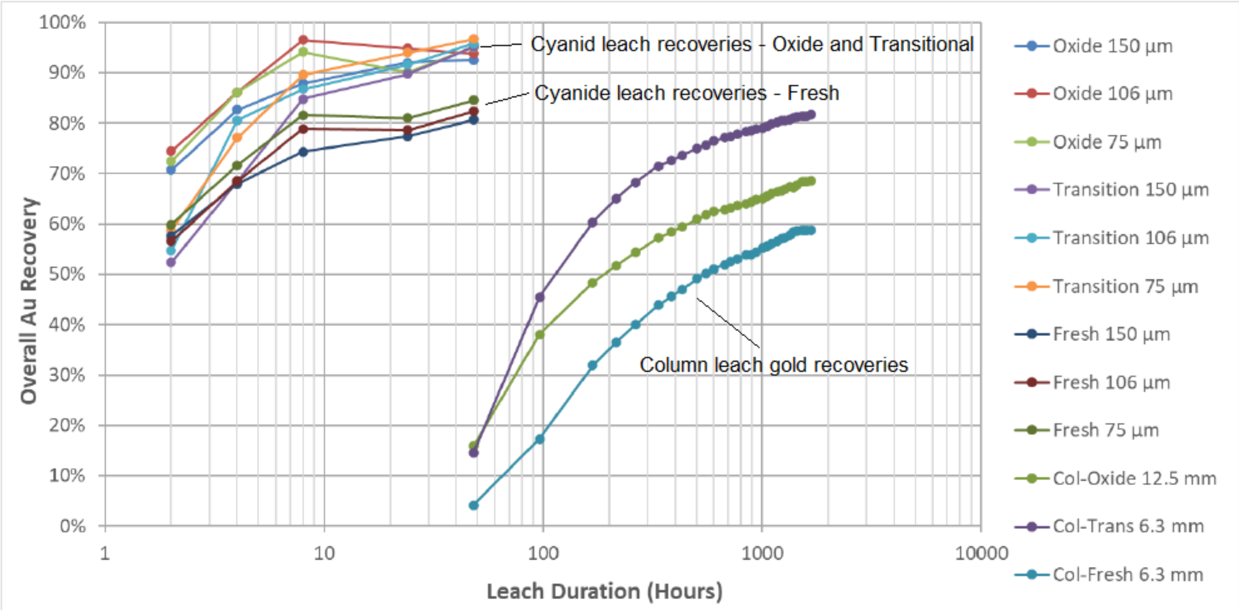

Figure 1 Comparison of Cyanide Leach Curves. Note "Col" - Column Leach.

Sample Provenance

Prodigy Gold provided IMO with representative core samples from the diamond drilling campaign conducted at the Buccaneer Project in 2021. These samples were utilised throughout the testwork program to generate four (4) composites representing the different mineralisation sources for metallurgical testwork.

The three main composites were generated as follows:

1. Oxide;
2. Transition; and
3. Fresh.

Due to mass constraints within the oxide composite intervals, a fourth barren oxide composite was generated in order to conduct the oxide comminution testwork and reserve enough mass for leaching testwork. It is referred to as the 'oxide comminution' composite.

Samples provided included ¾ HQ drill core, with intervals selected based on head grade data and preparation of the three composites, representing the oxide, transition and fresh (sulphide) zones. Comprehensive head grade analysis of defined composites was also required.

Scope of Testwork

The testwork was designed to provide Prodigy Gold with information at a Scoping Study level to analyse the best approach for processing the gold bearing material at Buccaneer. A summary of the metallurgical testwork that was requested for the project is outlined below:

- Comminution testwork, comprising
  - Bond abrasion index ("BAi")
  - Crushing work index ("CWi")
  - SMC test® (SAG Mill comminution testwork)
- Cyanide leaching testwork ("CIL"), comprising
  - Gravity gold ("GG") testwork using a 3 inch laboratory scale Knelson concentrator
  - Intensive cyanide leach on Knelson concentrate under Acacia Reactor conditions
  - Recombining the intensive leach residue and Knelson tail in preparation for bottle roll tests
  - Bottle roll cyanide leach testwork
  - Gold Diagnostic Leach test ("GDL") on one of the fresh composites (sample from LT-09) Leach Residue sample was added to the scope during the testwork program
- Base-line Intermittent Bottle Roll ("IBR") testwork, comprising
  - Kinetic leach testing
  - Feed and residue size by assay analysis
- Agglomeration and percolation testing – required to analyse heap leach potential
- Column Leach testing; comprising
  - Kinetic leach testing, and
  - Column feed and residue size by assay analysis.

Summary of Testwork Completed

Seven separate analytical tests were completed on the composites provided to IMO. These are noted below:

1. Head Grade Analysis

Required to understand the grades of the composites and were determined using standard 50gm fire assay for gold and four acid digest techniques with ICP/OES+MS for multi-elements.

- Average gold grades returned were 2.53g/t Au (oxide), 2.13g/t Au (transition) and 0.67g/t Au (fresh) (Table 1). Assaying indicated presence of coarse gold.
- Organic carbon and high antimony results don't appear to limit gold recovery.

- High copper grades in the fresh composite caused incomplete dissolution of gold but was studied further in the diagnostic leach.

2. Comminution Analysis

Designed to determine how the mineralised material performs under conventional crushing and grinding processes, typically used in gold processing plants.

- CWi testwork showed oxide, transition and fresh material to be soft.
- BAi results showed the oxide to be non-abrasive, transition to be mildly abrasive and fresh to be highly abrasive.
- t_a (abrasion parameter) values showed the oxide and transition material to be amenable to abrasive grinding and the fresh to be moderately amenable to abrasive grinding.
- SMC test® results showed the oxide material to be soft, transition material to be moderately soft and the fresh material to be moderately hard.
- Comminution testwork showed the mineralised material to be suitable for processing with conventional crushing and grinding circuits.

3. Gravity Gold and Cyanide Leach Testwork

Gravity gold and cyanide leaching are common processing pathways for gold bearing material, this testwork is aimed at understanding how the composites perform through these processes.

- Average gravity gold results were around 18.6% (Table 5) with the transitional material showing the highest result of 22.2% (Table 7).
- At P_{80} 75µm (80% mass passing 75µm sieve), the transition sample returned the highest CIL recovery at 96.7% (Table 7) with fresh returning the lowest gold recovery at 84.6% (Table 8).
- Grind size is seen to have an impact on the recovery of gold with finer grinds producing higher recoveries in general.
- Cyanide consumption is considered moderate and lime consumption was low for all three composites.
- Results showed that the Buccaneer mineralisation could be processed through a conventional CIL plant with a recommendation for a suitable gravity circuit.

4. Diagnostic Leach Analysis

This work was completed in order to establish the mineralogical causes for the low recoveries seen in the fresh composite.

- Testwork completed on fresh composite LT09 leach residue (P_{80} 75µm sample) showed (Table 9)
    - 13.4% of residual gold was leachable;
    - 15.2% of residual gold is locked in weak acid soluble minerals; and
    - 62.4% is locked in solid solution.
- Results showed that with additional cyanide, a finer grind and longer residence times, gold recovery would improve, but this would need to be optimised as it will result in higher processing operating cost.

5. Intermittent Bottle Roll Testwork

IBR is the initial testwork undertaken to determine the amenability of the three composites to heap leaching (Table 10).

- Transition sample showed moderate recoveries through IBR testwork, with a maximum of 80.1% recovery.
- The fresh composite showed low recoveries of between 15.6% and 44.5%.
    - Oxide composite crushed to P_{100} 12.5mm showed recoveries of 64.9% and P_{100} 25mm 63.0% recoveries.
- Overall low gold recoveries were noted in the IBR analysis, supporting the results of the Column Leach testwork.

6. Agglomeration and Percolation Analysis

Testwork to determine the optimum cement addition rate to allow percolation of the leach liquor through the composites.

- Oxide, transition and fresh composites showed both favourable rates of percolation and slumping.

7. Column Leach Testwork

This testwork is designed to understand the potential recoveries of the three composites once the agglomeration and percolation analysis is completed (Table 15).

- Results for each composite are noted as
  - Oxide – 68.6% gold recovery on P_{100} 12.5 mm sample;
  - Transition – 81.8% gold recovery on P_{100} 6.3 mm sample;
  - Fresh – 58.8% gold recovery on P_{100} 6.3 mm sample.
- The recoveries noted highlight the material is not suitable for heap leach processing as the recoveries are not high and the crushing required is more than typical for this style of deposit.

Overall results showed the Buccaneer gold mineralisation is not amenable to heap leach processing but more suitable for conventional CIL processing with a gravity gold separation process. As is typical to most other gold deposits, the grind size is an important consideration in the overall recovery of gold, with a finer grind providing higher recoveries at Buccaneer. It should be noted that a finer grind leads to higher crushing/grinding costs as well as higher reagent usages, requiring optimisation through further testwork. Head grade analyses testwork used a considerably smaller mass, which was derived from coarser material when compared with column leach samples; further indicating the presence of coarse gold at Buccaneer.

Further details are available on each analytical process below, including more details on the results as well as recommendation for further work.

<u>Detail of Testwork Completed</u>

1. Head Grade Analysis

Representative sub-samples of the three main testwork composites were pulverised and submitted to Intertek Group PLC (“Intertek”) for the following analysis:

- Duplicate 50g fire assay
  - Duplicate gold assays were consistent for the oxide and fresh composites; however, the transition composite duplicate gold assays indicate the presence of coarse gold;
- Four acid digest ICP/OES+MS assaying;
- HCl digest ICP/OES for Sulphate; and
- Total Carbon, Organic Carbon and Total Sulphur by Leco.

Head grade results are presented in Table 1.

Table 1 Head Grade Analysis

Element	Unit	Detection Limit	Oxide	Transition	Fresh
Target Au Grade			**2.41**	**2.84**	**1.73**
Au (Avg.)	g/t		2.53	2.13	0.67
Au	g/t	0.005	2.59	1.84	0.63
Au	g/t	0.005	2.46	2.42	0.70
As	ppm	20	448	390	1,236
Total Carbon	%	0.01	0.01	0.02	0.54
Organic Carbon	%	0.01	<0.01	0.02	0.01
Carbonate	%	0.01	0.01	<0.01	0.53
Cu	ppm	20	131	377	552
Total Sulphur	%	0.01	0.04	0.05	1.10
Sulphate	%	0.01	0.05	0.04	0.07
Sulphide	%	0.01	0.04	0.05	0.98
Sb	ppm	0.5	23.8	12.3	14.2
Te	ppm	2	<2	<2	4

2. Comminution Analysis

Prior to the stage crushing of each composite to P_{100} 50mm, twenty pieces were selected from each composite for Crushing Work Index ("CWi") testwork. The spoils from the CWi testwork were then utilised for Bond Abrasion Index ("BAi") testwork. A batch of 25kg of composite material was also stage crushed to P_{100} 32mm and utilised for the SMC test®. Results of all three comminution tests are presented below.

Crushing Work Index (CWi)

Results of the CWi testwork conducted are presented in Table 2, indicating:

- The oxide comminution composite testwork indicates the material is very soft;
- The transition composite indicates the transition material is also soft; and
- The fresh composite indicates the fresh material is soft.

Table 2 Crushing Work Index (CWi) Results Summary

Result	Units	Oxide Comminution Composite	Transition Composite	Fresh Composite
Average Work Index	**kWh/t**	**2.84**	**5.19**	**5.14**
Maximum Work Index	kWh/t	7.50	10.36	12.71
Minimum Work Index	kWh/t	1.64	2.73	2.43
Median Work Index	kWh/t	2.10	4.49	4.84
75th Percentile	kWh/t	3.06	6.21	5.47
85th Percentile	kWh/t	3.08	5.89	7.55
95th Percentile	kWh/t	5.94	10.14	8.49
Average Impact Energy	J	5.92	11.20	12.65
Maximum Impact Energy	J	15.61	23.83	38.52
Minimum Impact Energy	J	4.02	6.25	6.25
Average SG of Specimens	t/m^3	2.43	2.43	2.55

t = metric tonne

Bond Abrasion Index (BAi)

BAi testwork was conducted on the spoils from the CWi analysis for each of the 3 composites (Table 3).

BAi results are summarised as:

- Oxide comminution composite categorised the sample as non-abrasive.
- Transition composite categorised the sample as mildly abrasive.
- Fresh composite categorised the sample as highly abrasive.

Table 3 Bond Abrasion Index (BAi) Results Summary

Result	Units	Oxide Comminution Composite	Transition Composite	Fresh Composite
Bond Abrasion Index (BAi)	**g**	**0.0128**	**0.1913**	**0.3714**
Paddle In	g	86.4481	86.4745	86.2832
Paddle Out	g	86.4353	86.2832	85.9118

SMC Test®

All three composites underwent the SMC test® with results submitted to JK Tech Pty Ltd for data interpretation. The SMC test® results are presented in Table 4 and indicate the following:

- Axb (rock breakage parameters) results categorising the composites as:
  - Oxide: extremely soft (above 127 is considered very soft);
  - Transition: soft;
  - Fresh: medium hardness, (below 40 is considered hard).
- t_a (abrasion parameter) values indicated:
  - Oxide: is highly amenable to abrasive grinding;
  - Transition: is amenable to abrasive grinding;
  - Fresh: moderate amenability to abrasive grinding (<0.35 is relatively resistant to abrasive grinding).
- SAG Circuit Specific Energy (SCSE) values categorised the composites as:
  - Oxide: confirming material as very soft (<6.5 is considered very soft);
  - Transition: confirming as moderately soft to soft;
  - Fresh: indicating the mineralisation is moderately hard (>9.7 kWh/t is considered hard).

Table 4 SMC Test® Results Summary

Result	Units	Oxide Comminution Composite	Transition Composite	Fresh Composite
DWi	kWh/m³	0.3	3.7	5.9
	%	<1	16	40
Mia	kWh/t	2.8	12.6	17.3
Mih	kWh/t	1.1	8.2	12.5
Mic	kWh/t	0.6	4.3	6.5
SG	t/m³	1.64	2.61	2.75
A	#	81	61	65.5
b	#	6.3	1.15	0.71
ta	#	8.06	0.7	0.44
	%	0	24.2	49.9
Axb	#	510.3	70.2	46.5
	%	0.3	21.7	48.2
SCSE	kWh/t	6.82*	7.72	9.31
	%	10	19.3	47.7

**Sample parameters are outside the range of parameters used when developing the SCSE model. As such SCSE values for flagged samples should be treated with caution.*

3. *Gravity Gold Testwork*

Gravity recoverable gold was assessed for the three composites prior to CIL testing, following the flow sheet presented in Figure 2. A 15kg sub split each composite was ground to 80% passing 300µm and passed through a three-inch standard Knelson concentrator. The Knelson concentrates were subsequently intensively leached for 48 hours to ensure maximum gold recovery and accurate results.

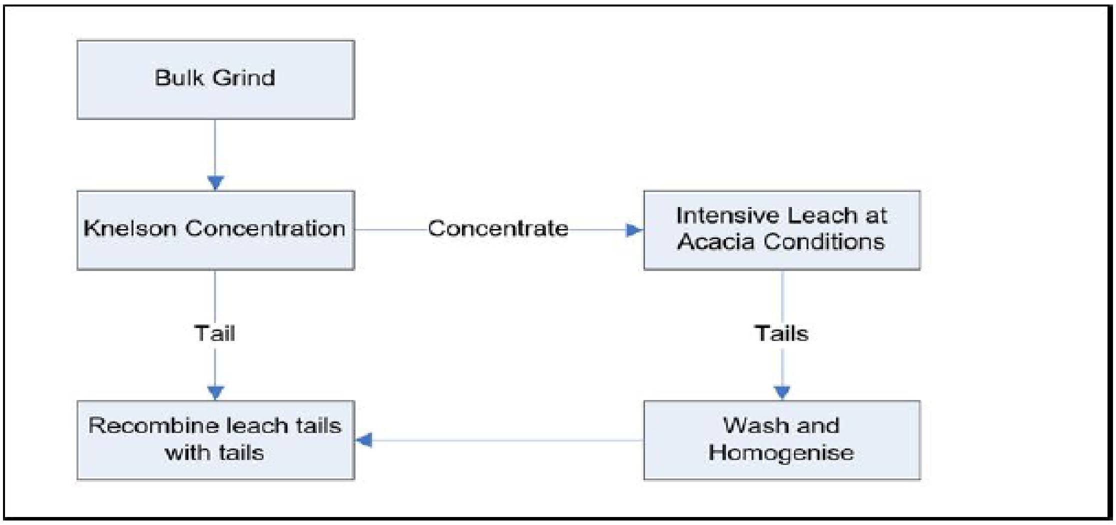

Figure 2 Gravity Testwork Block Flow Diagram

The Knelson concentrator mass recovery and intensive leach summary is presented in Table 5 for all three composites.

Table 5 Gravity Gold Concentrate Mass and Intensive Leach Summary

	Units	Oxide	Transition	Fresh
Feed Mass	g	14,664	14,802	14,789
Concentrate Mass	g	63.63	71.78	78.76
Tails Mass	g	14,600	14,730	14,710
Concentrate Mass Recovery	%	0.43	0.48	0.53
Au Leached in Intensive Leach	µg	3,026	5,082	2,046
Gravity Au per kg of sample	µg	206	343	138
Gravity Au Grade	g/t	0.206	0.343	0.138
Gravity Recovery (Averages)	%	16.6%	21.9%	17.4%
Overall Average Gravity Recovery	%		18.6%	

4. *Diagnostic Leach Analysis*

Knelson Tail + ILR Leach Testwork

To determine the amenability to traditional cyanide in leach gold processing the Knelson Tail and Intensive Leach Residue (ILR) were combined to undergo CIL testing under typical conditions and consistent with industry practice. The Knelson Tail + ILR leach testwork results were combined with the gravity gold leach results to obtain the overall gold recovery under CIL conditions. As a result, the gravity gold recovery for each composite was back calculated, which accounts for the reason it was not reported. Table 6 to 8 show the gravity gold and cyanide leach summaries for the oxide, transition and fresh composite respectively, with the performance summarised as:

- Gravity gold recovery was highest for the transition composite, averaging 21.9% gold recovery.
- Gravity gold recovery was lowest for the oxide and fresh composites, ranging from 16.6% to 17.4% gold recovery.
- The transition composite at P_{80} 75µm resulted in the highest gold recovery after 48 hours.

- On average the transition composite returned higher gold recoveries across the P_{80} 150, 106 and 75µm grind sizes compared with the oxide composite.
- The fresh composite showed the lowest gold recoveries for all grind sizes.
- Cyanide consumption is considered moderate for all three composites.
- Lime consumption is considered low for all three composites.

Table 6 Oxide Composite *Gravity gold and Cyanide Leach Summary*

Oxide Composite	P_{80} (µm)	Oxide LT-01 150	LT-02 106	LT-03 75
Gravity Recovery	%	15.8%	17.2%	16.7%
2 Hour Recovery	%	70.7%	74.5%	72.4%
4 Hour Recovery	%	82.7%	86.1%	86.2%
8 Hour Recovery	%	87.9%	96.5%	94.1%
24 Hour Recovery	%	92.1%	94.9%	90.1%
48 Hour Recovery	%	92.5%	93.8%	95.1%
Calculated Head Grade	g/t	1.32	1.22	1.25
Assayed Head Grade	g/t	2.53	2.53	2.53
Residue Grade	g/t	0.10	0.08	0.06
Gravity Recovery	g/t	0.21	0.21	0.21
Leach Recovery	g/t	1.01	0.94	0.98
Total Recovery	g/t	1.22	1.15	1.18
24 Hour Cyanide Consumption	kg/t	0.46	0.50	0.53
48 Hour Cyanide Consumption	kg/t	0.57	0.58	0.52
24 Hour Lime Consumption	kg/t	0.59	0.50	0.56
48 Hour Lime Consumption	kg/t	0.62	0.50	0.56

Table 7 Transition Composite *Gravity and Cyanide Leach Summary*

Transition Composite	P_{80} (µm)	Transition LT-04 150	LT-05 106	LT-06 75
Gravity Recovery	%	22.2%	21.6%	21.7%
2 Hour Recovery	%	52.4%	54.7%	58.8%
4 Hour Recovery	%	68.5%	80.6%	77.1%
8 Hour Recovery	%	84.8%	86.7%	89.6%
24 Hour Recovery	%	89.8%	91.7%	94.0%
48 Hour Recovery	%	95.2%	95.8%	96.7%
Calculated Head Grade	g/t	1.55	1.59	1.59
Assayed Head Grade	g/t	2.13	2.13	2.13
Residue Grade	g/t	0.08	0.07	0.05
Gravity Recovery	g/t	0.34	0.34	0.34
Leach Recovery	g/t	1.13	1.18	1.19
Total Recovery	g/t	1.47	1.52	1.53
24 Hour Cyanide Consumption	kg/t	0.36	0.28	0.30
48 Hour Cyanide Consumption	kg/t	0.44	0.41	0.37
24 Hour Lime Consumption	kg/t	0.35	0.26	0.24
48 Hour Lime Consumption	kg/t	0.35	0.26	0.24

Table 8 Fresh Composite Gravity and Cyanide Leach Summary

Fresh Composite		Fresh		
		LT-07	LT-08	LT-09
	P_{80} (µm)	150	106	75
Gravity Recovery	%	17.7%	17.3%	17.2%
2 Hour Recovery	%	57.7%	56.5%	59.8%
4 Hour Recovery	%	68.0%	68.5%	71.6%
8 Hour Recovery	%	74.3%	78.9%	81.6%
24 Hour Recovery	%	77.4%	78.7%	81.0%
48 Hour Recovery	%	80.6%	82.4%	84.6%
Calculated Head Grade	g/t	0.79	0.80	0.81
Assayed Head Grade	g/t	0.67	0.67	0.67
Residue Grade	g/t	0.15	0.14	0.12
Gravity Recovery	g/t	0.14	0.14	0.14
Leach Recovery	g/t	0.50	0.52	0.54
Total Recovery	g/t	0.63	0.66	0.68
24 Hour Cyanide Consumption	kg/t	0.48	0.39	0.43
48 Hour Cyanide Consumption	kg/t	0.55	0.57	0.64
24 Hour Lime Consumption	kg/t	0.22	0.15	0.19
48 Hour Lime Consumption	kg/t	0.22	0.15	0.19

Figure 3 shows the overall gold recovery kinetic curves for the three composites. The curves show that the transition and oxide material performed better than the fresh material.

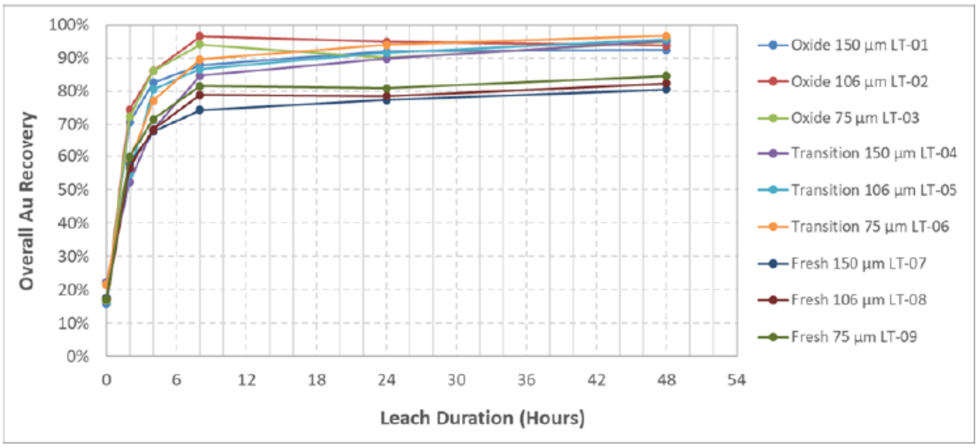

Figure 3 Gravity Gold + Cyanide Leach Curves

Overall Gold Recovery vs Particle Size P_{80} (µm)

Completion of the IBR and CIL testwork facilitated the investigation of overall gold recovery vs particle size P80 (µm). Figure 4 shows that gold liberation via size reduction is a determining factor in gold recovery for all three composites. This is a common phenomenon with gold leach testwork.

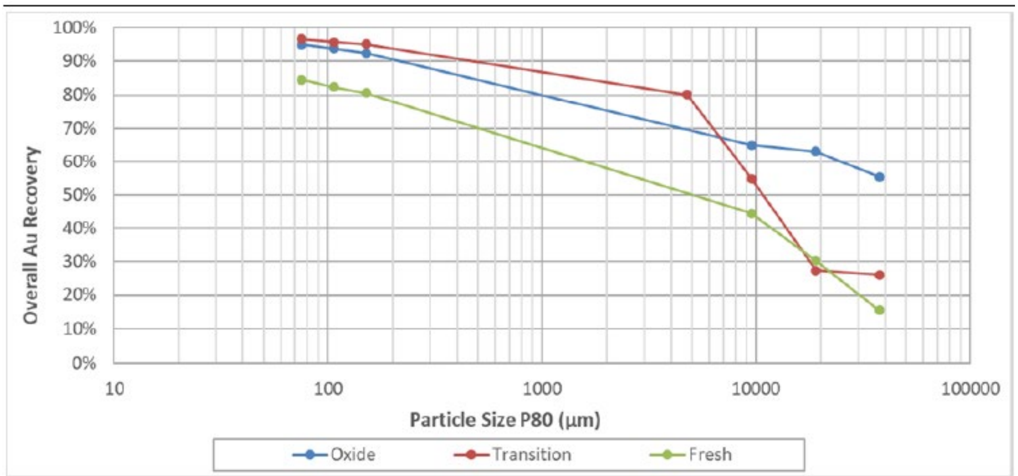

Figure 4 Gold Recovery vs Particle Size

LT-09 Leach Residue – Gold Diagnostic Leach Testwork

In order to establish the mineralogical causes for the fresh composite only achieving a maximum of 84.6% gold recovery, a gold diagnostic leach was carried out on the LT-09 (75µm) leach residue. A summary table of the diagnostic leach results is presented in Table 9 and shows both the solution analysis and the residue analysis, summarised as:

- After the use of standard test conditions, 13.4% of the residual gold or 0.019g/t Au still exists as cyanide leachable gold and could be recovered at 75µm with a longer leach residence time or increased cyanide addition. This would form the basis of future optimisation work.
- 15.2% of the residual gold or 0.022g/t Au is locked in weak acid soluble minerals (like quartz).
- Most of the residual gold, 62.4% or 0.089g/t Au, is locked in solid solution/sulphide occluded minerals. A finer grind may liberate the sulphide occluded gold, however this may not be economically viable, as the grind size of P_{80} 75µm is already low for gold mineralisation.
- Calculated gold head grades for both the solution and residue-based data are within assay analysis error and correspond with the LT-09 (75µm) residue assay grade of 0.12g/t.

Table 9 LT-09 (75µm) Leach Residue Diagnostic Leach Summary

	Au Distribution (%)		Au	Au Dist. w.r.t. LT-09 Calc. Head Grade
Diagnostic Leach Stage	Solution Basis	Residue Basis	(g/t)	(%)
Free Cyanidable Gold	22.5%	13.4%	0.019	2.4%
Intensive Cyanidable Gold	0.0%			
Weak Acid Soluble Gold	15.9%	15.2%	0.022	2.7%
Other Minerals Occluded Gold	11.6%			
Majority Sulphide Solid Solution Gold	26.3%	62.4%	0.089	11.0%
Majority Sulphide Occluded Gold	11.2%			
Other Refractory Gold	8.0%	5.1%	0.007	0.9%
Silicate Locked Gold	4.5%	3.8%	0.005	0.7%
LT-09 Leach Residue Calc. Head Grade			**0.142**	
LT-09 Calc. Head Grade			**0.807**	

5. Intermittent Bottle Roll Testwork

Intermittent Bottle Roll ("IBR") testing was the initial testwork undertaken to determine the amenability of the oxide, transition and fresh composites to heap leaching. Due to a limitation in the mass of oxide composite available, a sample of crush size P_{100} 6.3mm was not prepared/tested. The 6.3mm size was excluded due to the expectation that it would produce high gold recoveries but not be considered an economic crush size for a full-size operation compared with the 12.5mm crush size, which was expected to produce high gold recoveries.

IBR Leach Results

IBR leach results are summarised in Table 10 while the kinetic curves for the oxide, transition and fresh composites are presented in Figure 5 to 7, respectively. The IBR leach results indicate the following:

- The transition 6.3mm crush size exhibited the highest gold recovery at 80.1%.
- The oxide leach kinetic curves for the 12.5mm and 25mm crush sizes exhibited similar leach kinetics from the 72-hour point onwards, with 168-hour gold recoveries of 64.9% and 63.0%, respectively.
- The fresh composite exhibited the lowest overall gold recovery.
- Overall, low gold recovery was observed in IBR results indicating column leach testwork may not result in successful gold recovery.

Table 10 Intermittent Bottle Roll (IBR) Leach Results

		Oxide			Transition				Fresh			
	Test	IBR01	IBR02	IBR03	IBR04	IBR05	IBR06	IBR07	IBR08	IBR09	IBR10	IBR11
	P_{100} (mm)	50	25	12.5	50	25	12.5	6.3	50	25	12.5	6.3
0 hr Recovery	%	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2 hr Recovery	%	29.2	34.8	36.5	2.0	3.4	9.0	8.1	4.2	6.1	8.2	3.5
4 hr Recovery	%	40.7	41.8	51.7	6.0	6.0	17.5	25.7	5.6	9.1	18.1	7.8
24 hr Recovery	%	46.0	50.3	59.4	10.0	9.5	26.5	39.3	7.2	12.2	23.1	11.5
48 hr Recovery	%	51.0	57.2	64.7	15.9	15.3	40.8	59.6	9.6	19.5	32.8	15.6
72 hr Recovery	%	53.3	61.1	62.1	21.9	19.6	49.0	66.5	12.0	25.7	39.3	19.0
96 hr Recovery	%	54.4	62.3	63.0	24.0	22.2	51.5	75.8	14.6	25.7	41.0	20.7
168 hr Recovery	%	55.5	63.0	64.9	26.1	27.3	55.0	80.1	15.6	30.3	44.5	22.4
Composite Head Grade	g/t	2.53	2.53	2.53	2.13	2.13	2.13	2.13	0.67	0.67	0.67	0.67
Feed (SxA) Grade	g/t	1.88	1.61	1.56	0.58	0.56	3.74	1.06	0.44	1.10	1.47	0.83
Calculated Head Grade	g/t	1.30	1.20	1.53	0.75	1.74	3.26	1.12	1.05	0.99	0.92	1.70
Residue (SxA) Grade	g/t	0.58	0.45	0.53	0.56	1.22	1.26	0.16	0.82	0.63	0.40	1.27
Total Recovery	g/t	0.72	0.75	0.99	0.20	0.52	2.00	0.96	0.23	0.36	0.51	0.43
48 hr Cyanide Cons	kg/t	0.39	0.36	0.40	0.05	0.12	0.14	0.14	0.15	0.09	0.15	0.16
168 hr Cyanide Cons	kg/t	0.48	0.45	0.56	0.13	0.21	0.19	0.28	0.27	0.23	0.22	0.26
48 hr Lime Cons	kg/t	1.29	1.46	1.24	0.49	0.62	0.64	0.80	0.32	0.19	0.39	0.41
168 hr Lime Cons	kg/t	1.93	2.20	2.25	0.49	1.02	0.95	1.10	0.32	0.35	0.39	0.41
Average DO	ppm	6.21	6.26	6.27	6.15	6.19	6.35	6.24	5.98	6.15	5.84	6.13

SxA refers to Size by Assay

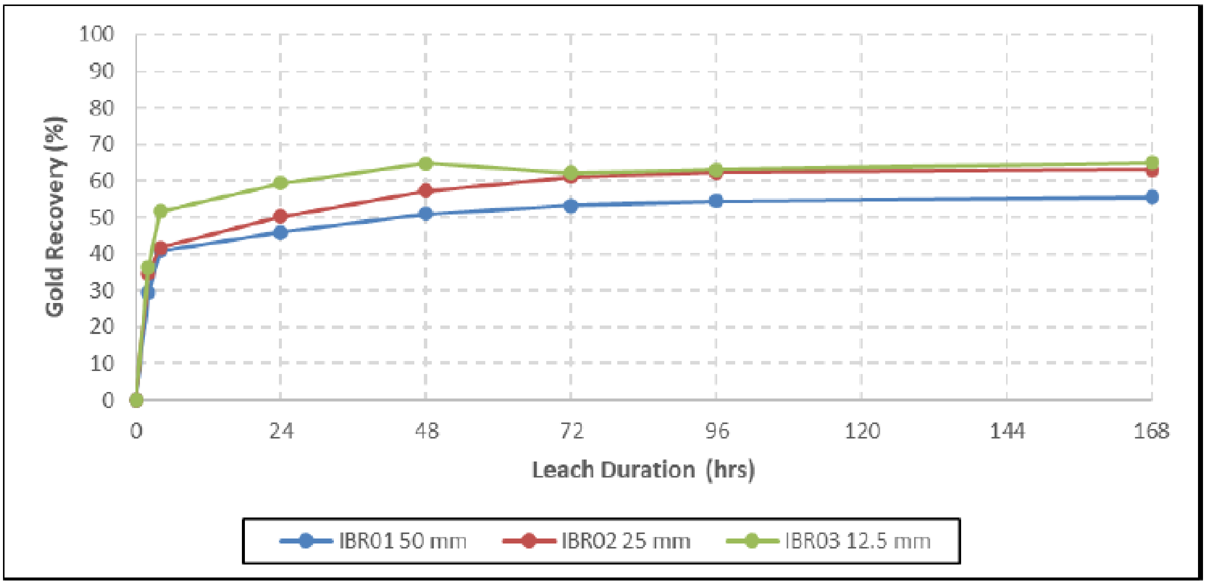

Figure 5 Oxide composite IBR Leach Kinetic Curves

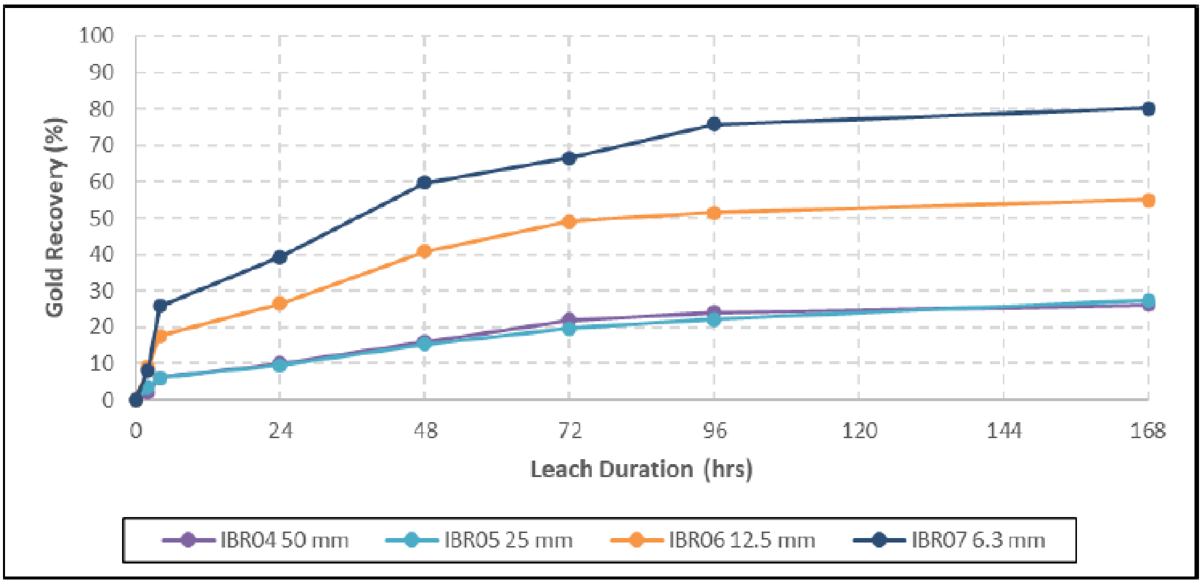

Figure 6 Transition composite IBR Leach Kinetic Curves

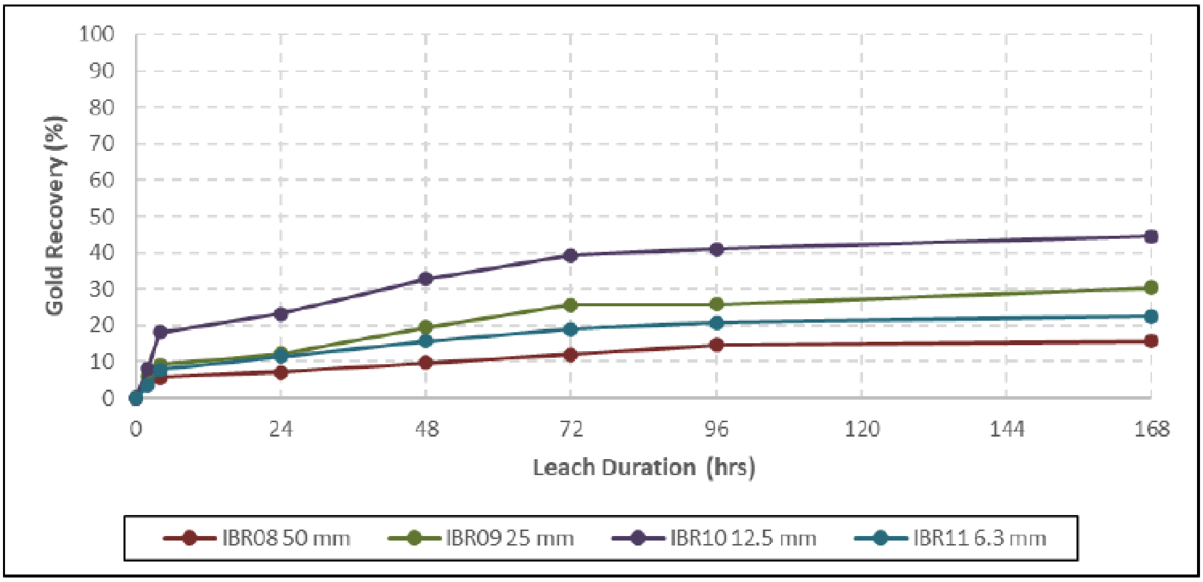

Figure 7 Fresh composite IBR Leach Kinetic Curves

A comparison of the calculated and assay head grade reveals biasing for the oxide and fresh composites. The variation observed in the transition composite is significant and shows that the samples most likely contain coarse gold.

6. Agglomeration and Percolation Testwork

Agglomeration and Percolation tests were undertaken on the composite samples to determine the optimum cement addition rate to allow percolation of leach liquor through the agglomerated composites. There are two main contributing factors which affect the agglomeration and subsequent percolation of the material:

1. Quantity of binding agent (cement); and
2. Moisture available to agglomerate with the mineralisation and the binder.

Percolation tests were conducted to determine the maximum percolation and the degree of slump for the agglomerated mineralisation. The mineralisation was loaded into a column of known diameter of 100mm and water percolated through the mineralisation from the bottom. The height of the mineralisation was measured and left to stand for two hours, after the two hours the mineralisation height was measured, the column was then vibrated in order to compact the mineralisation with the height being subsequently measured once more. Water was then drained from the bottom of the column and the volume of water drained over a specified time period was measured. The height of the mineralisation was then measured for a final time to obtain the worst-case slump value. IMO's experience indicates that slump results below 10% and percolation rates greater than 10,000l/m^2/h are required for heap leaching.

The agglomeration and percolation test results for varying cement ratios are presented in Table 11 to 13 for the oxide, transition and fresh composites, respectively and are summarised as follows:

- Oxide composite indicated satisfactory percolation rates for the 15kg/t and 20kg/t cement additions, reported as 11,940l/m^2/h and 28,644l/m^2/h.
- Oxide composite final slump values ranged from 7.7% to 6.3% at cement additions of 15kg/t and 20kg/t, respectively.
- Transition composite produced favourable results for both %slump (<10%) and percolation rates (>10,000l/m^2/h) for all cement additions.
- Fresh composite produced favourable results for both %slump (<10%) and percolation rates (>10,000l/m^2/h) for all cement additions.

Table 11 Oxide composite *Agglomeration and Percolation Results*

Cement (kg/t)	Feed % Moist.	Slump %			Loose Bulk Density (t/m^3)	Max. Perc. Rate (l/m^2/h)	Discharge Solution Clarity
		2 hr	2 hr + thump	Final Drained			
5	15.8	18.9	22.0	26.0	1.00	2,292	46
10	14.8	3.1	7.8	8.6	0.99	2,037	42
15	16.1	1.5	6.2	7.7	0.98	11,940	46
20	15.9	0.0	4.7	6.3	0.99	28,644	46

Table 12 Transition composite *Agglomeration and Percolation Results*

Cement (kg/t)	Feed % Moist.	Slump %			Loose Bulk Density (t/m^3)	Max. Perc. Rate (l/m^2/h)	Discharge Solution Clarity
		2 hr	2 hr + thump	Final Drained			
2	9.9	10.4	14.3	17.0	1.12	12,833	32
4	8.2	0.8	6.7	9.2	1.33	13,138	0
6	10.4	0.0	6.5	7.3	1.19	15,386	46
8	8.3	0.0	8.0	9.4	1.15	45,831	32

Table 13 Fresh composite *Agglomeration and Percolation Results*

Cement (kg/t)	Feed % Moist.	Slump %			Loose Bulk Density (t/m^3)	Max. Perc. Rate (l/m^2/h)	Discharge Solution Clarity
		2 hr	2 hr + thump	Final Drained			
2	10.1	1.9	5.1	9.4	1.36	15,399	0
4	5.9	0.8	7.8	8.8	1.21	22,661	17
6	8.1	0.8	8.0	8.8	1.21	43,997	12
8	6.5	0.6	4.9	6.1	1.21	25,862	23

7. Column Leach Testwork

Following the completion of the agglomeration and percolation testing, all three composites underwent column leach tests. Column leach is summarized in Table 14 showing a summary of the main testwork conditions.

Table 14 Column Leach Main Testwork Conditions

Composite	Crush Size (P_{100} mm)	Cement (kg/t)	Feed %Moist.	Water Type	Irrigation Rate (L/m²/h)	Target NaCN Conc. (ppm)	Target pH
Oxide	12.5	15	16.6	Perth Tap	10.0	250	10.0 - 10.5
Transition	6.30	6	8.7				
Fresh		4	7.3				

The three (3) columns were irrigated with 250ppm cyanide solution at a rate of 10l/m²/h for a duration of 60 days. The discharge from the column was contacted with carbon for twenty-four (24) hours and subsequently recycled back as feed solution every Monday, Wednesday and Friday. Once leaching was complete the columns were left to stand for two days, followed by flushing the column with Perth tap water until cyanide concentrations in the column discharge were below 60ppm.

Once complete, a 5kg sub split of the column residue was prepped and submitted for assay. Carbon assays are the preferred method for calculating recoveries due to extracted gold being calculated from one assay rather than two assays per sample point. This reduces the cumulative error associated with the final value from assaying of samples.

Column leach kinetic curves are presented in Figure 8 to 10 with summarised results provided in Table 15. These results indicate overall gold recoveries of;

- 68.6% Au recovery or 1.45g/t Au for the oxide composite crushed to P_{100} 12.5mm
- 81.8% Au recovery or 1.47g/t Au for the transition composite crushed to P_{100} 6.3mm, and
- 58.8% Au recovery or 0.85g/t Au for the fresh composite crushed to P_{100} 6.3mm.

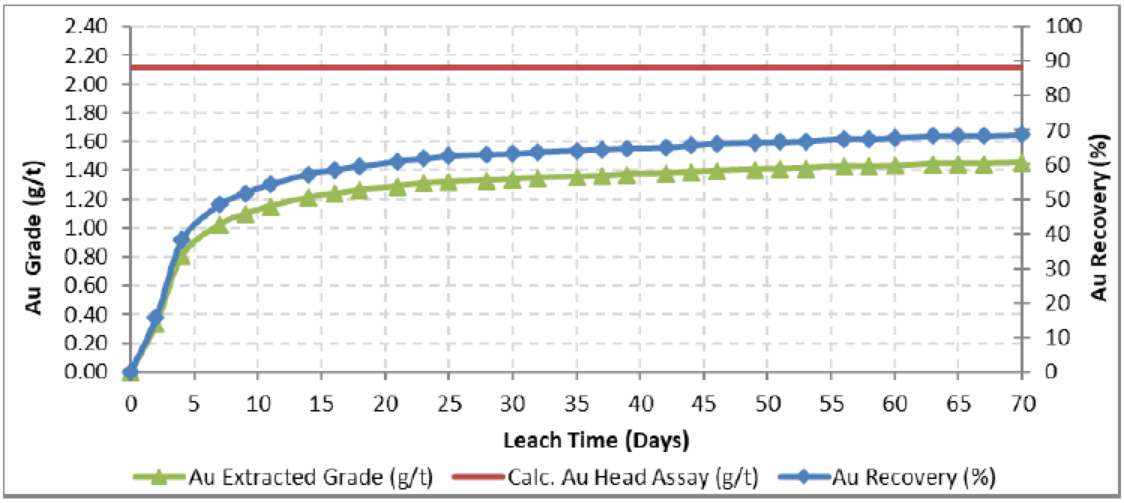

Figure 8 Oxide composite Column Leach Curves

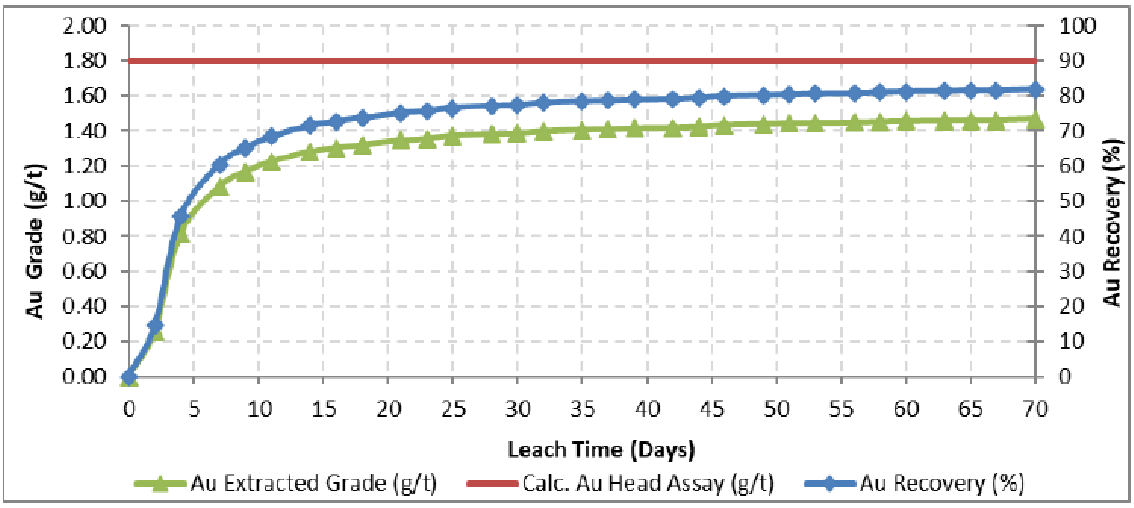

Figure 9 Transition composite Column Leach Curves

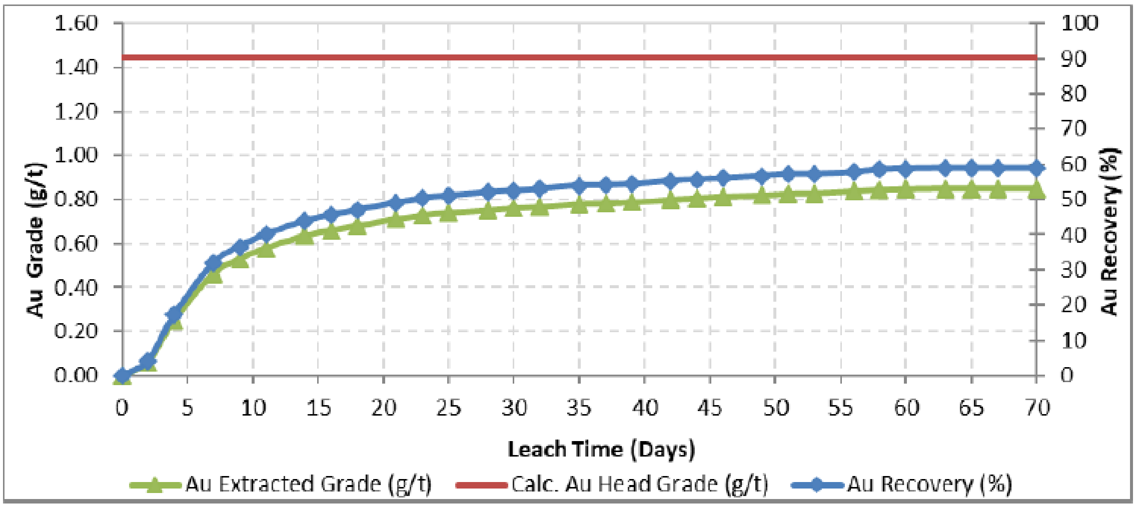

Figure 10 Fresh composite Column Leach Curves

Table 15 Oxide, Transition and Fresh Composite Summarised Column Results

	Units	Oxide	Transition	Fresh
Extracted Grade (Liquor)	g/t	1.37	1.47	0.85
Extracted Grade (Carbon)	g/t	1.45	1.47	0.85
Recovery (Liquor)*	%	67.3	81.9	58.7
Recovery (Carbon)*	%	68.6	81.8	58.8
Residue Assay*	g/t	0.665	0.326	0.596
Calc. Head (Liquor)	g/t	2.03	1.80	1.44
Calc. Head (Carbon)	g/t	2.13	1.79	1.45
Composite Assay Head Grade	g/t	2.53	2.13	0.67
Irrigation Ratio	m^3/t	7.88	5.94	5.93
Leach Duration	Days	60	60	60

**Residue head grade based on residue size by assay results*

Recommendations

Based on the results of the metallurgical testwork completed to date, the following recommendations for further process and project development were provided by IMO, including:

- Adopt the gravity gold and CIL processing flowsheet as the preferred option for future testwork;
- Undertake a program of testwork that is targeted at improving on the gold recovery of the fresh material by utilising the outcomes of the LT-09 Leach Residue – GDL testwork, namely:
    - Testing longer leach residence time or increased cyanide addition than the standard conditions used in this study, and
    - Testing a sulphide flotation stage followed by a pre-oxidation step prior to cyanide leaching.
    - Undertake both optical and scanning electron microscopy (SEM) analysis to determine the extent of gold associations with sulphide minerals, namely arsenopyrite.
    - Use finer crush size/increased sample mass for continued/more precise CIL testwork following from preliminary 2022 CIL testwork reported herein.

The Company will look to adopting each of these recommendations during the next phase of metallurgical evaluation.

Buccaneer Project – Background

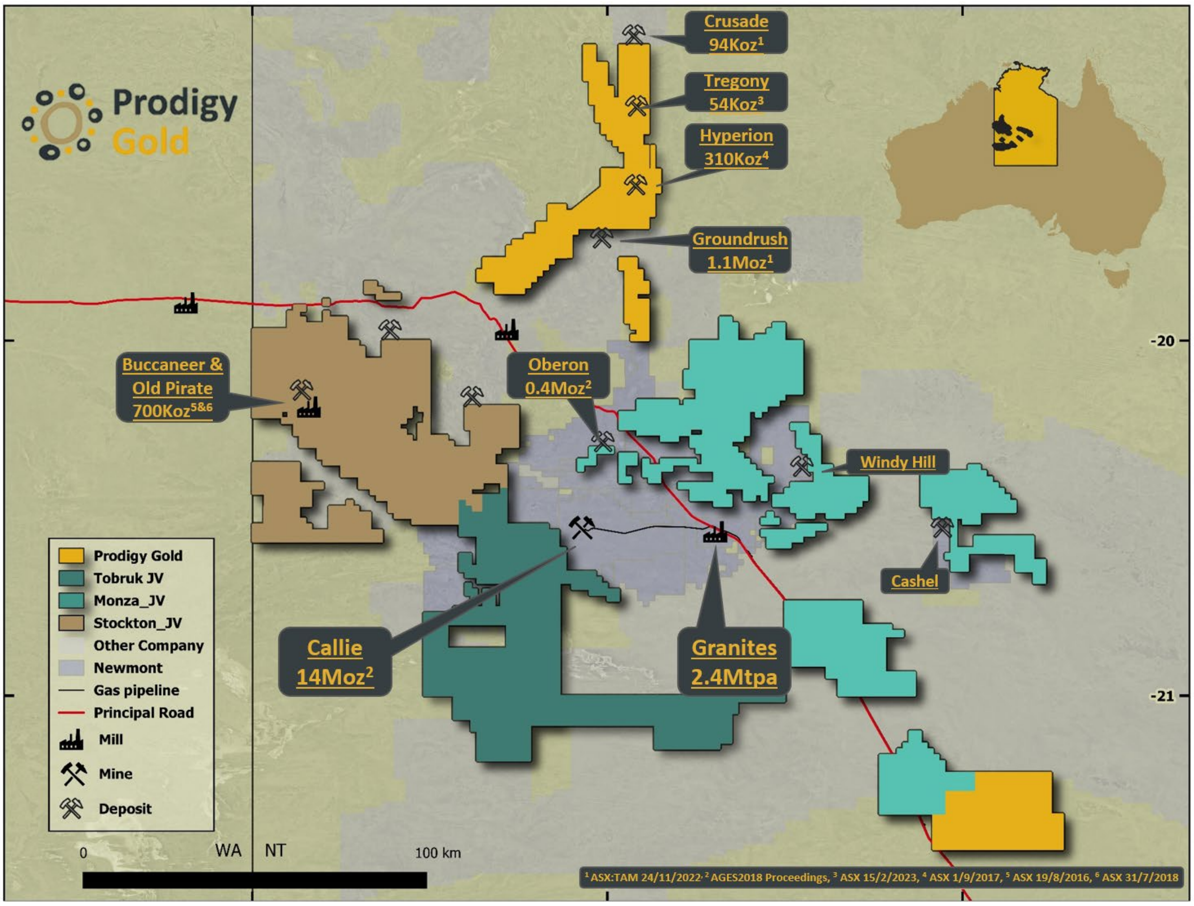

Figure 11 Buccaneer resource location with respect to other nearby mills and significant resources in the region and major Tanami project areas of Prodigy Gold

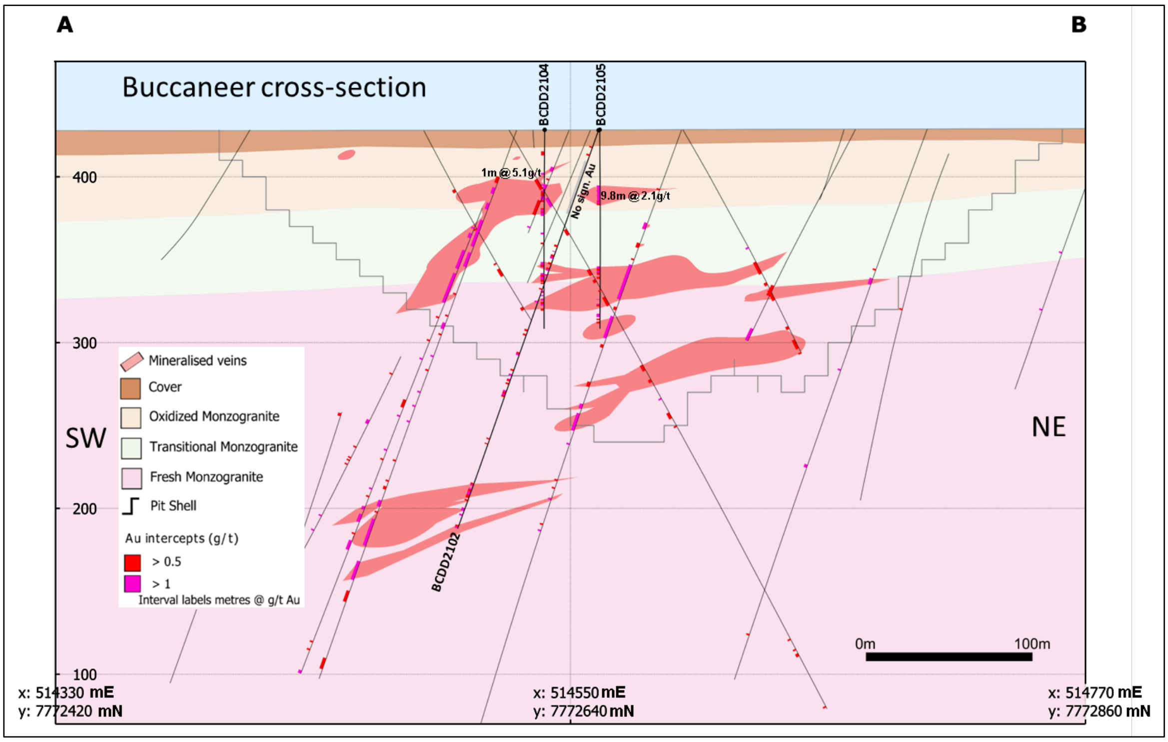

Figure 12 Southwest-northeast cross section through recent metallurgical holes showing selected gold results reported in on February 11 2022[7]

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[7] ASX: 11 February 2022

The Buccaneer Mineral Resource is currently estimated to be 10Mt @ 1.8g/t Au for 585koz above a 1g/t cut-off grade[8] (Appendix 2). The Mineral Resource cut-off grade is based on processing at a mill the scale of Northern Star/Tanami Gold's Central Tanami Joint Venture Project Processing Plant or a similar mill built on the Twin Bonanza Mineral Lease.

Gold mineralisation is disseminated within a monzogranite intrusion, and typically associated with quartz veins with visible gold often observed in the quartz stockwork veining. Mineralisation extends from near surface to a depth of over 500m and has been defined in several zones over an area of 2,300m by 800m (Figure 13). Mineralisation is often up to 150m thick with intervals of 20-40m wide at 1 to 5g/t Au[9]. The deposit remains open at depth, and aircore and RAB drilling suggest the potential for further strike extensions.

The project is well advanced featuring:

- Granted mineral lease
- Over 300 RC and diamond drillholes
- Exploration and mining agreement with the Traditional Owners administered by the Central Land Council
- Heritage, flora and fauna baseline surveys
- Accommodation camp and workshops
- Water bores with marginal to fresh water
- Airstrip
- Haul road access nearby to the Tanami Road
- 220kl of fuel storage

Studies undertaken over the last two years have evaluated processing scenarios for the Buccaneer Deposit. Deep weathering in the Tanami results in softer weathered rocks, and sulphide is often completely oxidised up to 100m below surface.

[8] ASX 1 September 2017
[9] ASX 1 September 2017

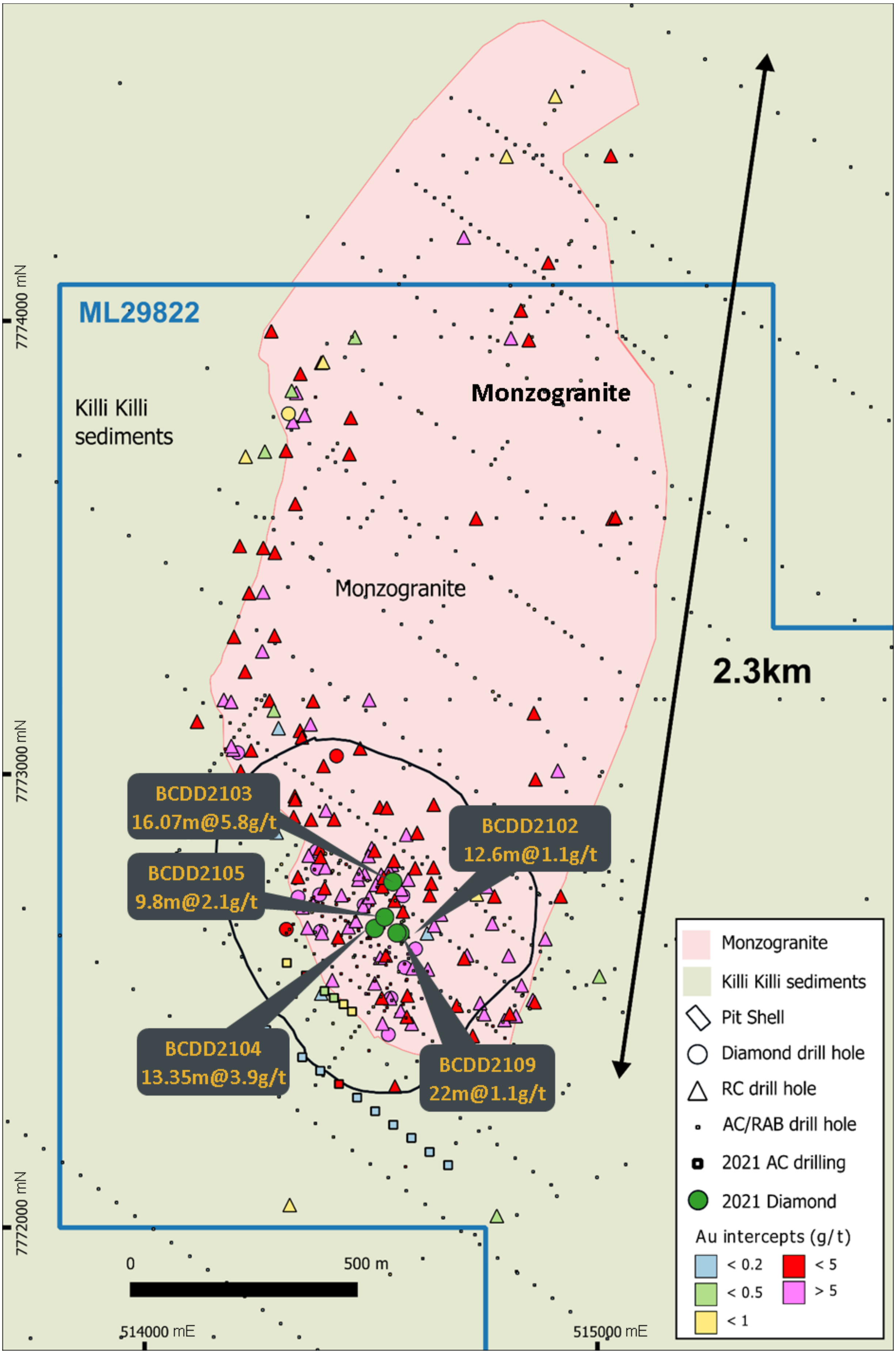

Figure 13 Highlighted recent and previous drill intercepts (max Au) along the Buccaneer Monzogranite[10]

[10] ASX: 29 November 2021 / 17 December 2021 / 11 February 2022

Authorised for release by Prodigy Gold's Board of Directors.

For further information contact:
Mark Edwards
Managing Director
+61 8 9423 9777

About Prodigy Gold NL

Prodigy Gold has a unique greenfields and brownfields exploration portfolio in the proven multi-million-ounce Tanami Gold Province. Prodigy Gold remains highly active in its systematic exploration approach and intends to continue exploration prioritising on:

- drilling targets on its Tanami North and Lake Mackay Projects
- growing confidence and size of Tanami North Project's Hyperion and Tregony Mineral Resources
- a scoping study on the Buccaneer Mineral Resource
- systematic evaluation of high potential early stage targets
- joint ventures to expedite discovery on other targets

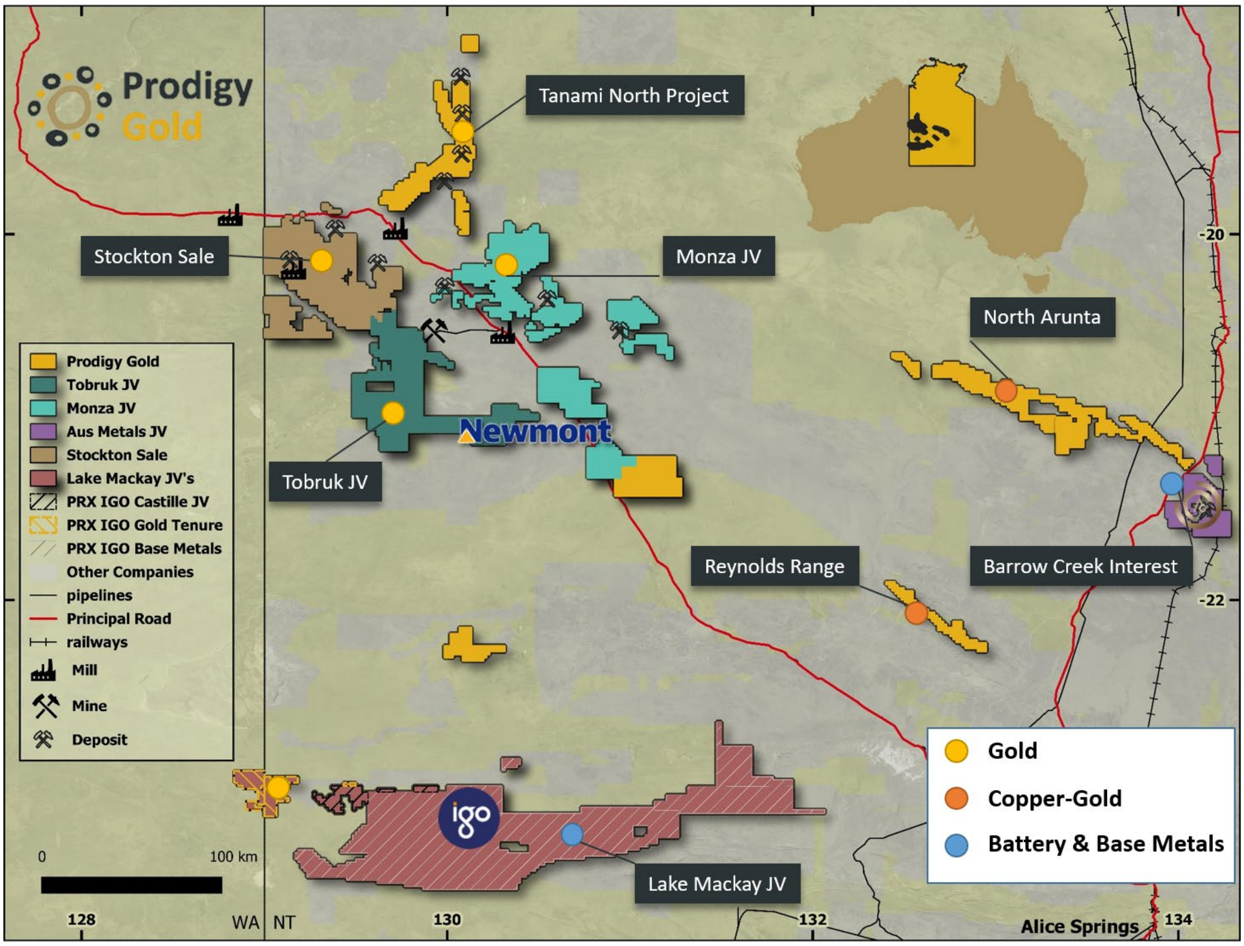

Figure 14 Prodigy Gold Major Project Areas

Competent Person's Statement

The information in this announcement that relates to metallurgy and metallurgical test work has been reviewed by Dr Andrew Dowling. Dr Dowling is not an employee of the Company but is employed by Independent Metallurgical Operations (IMO) who are providing services as a consultant. Dr Dowling is a fellow of the AusIMM (FAusIMM) and has sufficient experience with the style of processing response and type of deposit under consideration, and to the activities undertaken, to qualify as a competent person as defined in the 2012 edition of the "Australian Code for the Reporting of Exploration

Results, Mineral Resources and Ore Reserves" (The JORC Code). Dr Dowling consents to the inclusion in this report of the contained technical information in the form and context as it appears.

The Buccaneer Mineral Resource Estimate JORC report was released on the ASX 1 September 2017 – Buccaneer August 2017 Mineral Resource Estimate. The Company confirms that it is not aware of any new information or data that materially affects the Mineral Resources as reported on the 1 September 2017, and the assumptions and technical parameters underpinning the estimates in the 1 September 2017 release continue to apply and have not materially changed.

The information in this statement that relates to Mineral Resource for Old Pirate was previously released to the ASX on the 19 August 2016 – Old Pirate Updated Mineral Resource Estimate. This document can be found at www.asx.com.au (Stock Code: PRX) and at www.prodigygold.com.au. The 19 August 2016 release fairly represents information reviewed by Mr. David Williams, a Competent Person who is a member of the Australasian Institute of Mining and Metallurgy. At the time of the 19 August 2016 release Mr. Williams was a full-time employee of CSA Global Pty Ltd. Mr. Williams had previously provided written consent for the 19 August 2016 release.

The information in this report that relates to Mineral Resource for Hyperion (previously called Suplejack) was previously released to the ASX on the 31 July 2018 – Suplejack Resource Update. This document can be found at www.asx.com.au (Stock Code: PRX) and at www.prodigygold.com.au. The 31 July 2018 release fairly represents data and geological modelling reviewed by Mr. Matt Briggs who is a member of the Australasian Institute of Mining and Metallurgy and grade estimation and Mineral Resource estimates reviewed by Mr. Ian Glacken who is a Fellow of the Australia Institute of Geoscientists. At the time of the 31 July 2018 release Mr. Briggs was a fulltime employee of Prodigy Gold NL and Mr. Glacken was a fulltime employee of Optiro Pty Ltd. Mr. Briggs and Mr. Glacken had previously provided written consent for the 31 July 2018 release.

The information in this report that relates to Mineral Resource for Tregony was previously released to the ASX on the 15 February 2023 – Maiden Mineral Resource for Tregony Deposit and can be found at www.asx.com.au (Stock Code: PRX) and at www.prodigygold.com.au. The 15 February 2023 release fairly represents data review, geological modelling, grade estimation and Mineral Resource estimates completed by Mr. Mark Edwards who is a fellow of the Australasian Institute of Mining and Metallurgy. Mr. Edwards is a fulltime employee of Prodigy Gold NL. Mr. Edwards had previously provided written consent for the 15 February 2023 release.

This release contains updated information of results relating to drilling at the Buccaneer Project in three previous ASX announcements (17 December 2021 – Exceptional Results in Buccaneer Diamond Drilling, 29 November 2021 – Progress Results for Buccaneer Diamond Drilling and 11 February 2022 – Buccaneer Gold Project Update). The release also contains information from another release (ASX:TAM 24 November 2022 – Mineral Resource Updates Completed for Five Gold Deposits on the Central Tanami Project Joint Venture Yields 1.5M Ounces. The Company confirms that it is not aware of any new information or data that materially affects the Exploration Results as released on the 29 November 2021, 17 December 2021, 11 February 2022 and 24 November 2022 and the assumptions and technical parameters underpinning the Exploration Results in the listed releases continue to apply and have not materially changed.

The information in this announcement relating to the Buccaneer Resource, are based on information reviewed and checked by Mr Mark Edwards, FAusIMM, MAIG. Mr Edwards is a Fellow of the Australasian Institute of Mining and Metallurgy (AusIMM) and a Member of The Australasian Institute of Geoscientists (AIG) and has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (The "JORC Code"). Mr Edwards is a fulltime employee of the Company in the position of Managing Director and consents to the inclusion of the Exploration Results Mineral Resources and Metallurgical testwork Results in the form and context in which they appear.

Past Exploration results reported in this announcement have been previously prepared and disclosed by Prodigy Gold NL in accordance with JORC 2012, these releases can be found and reviewed on the company website, (www.prodigygold.com.au). The Company confirms that it is not aware of any new information or data that materially affects the information included in these market announcements. The Company confirms that the form and content in which the Competent Person's findings are presented here have not been materially modified from the original market announcements. Refer to www.prodigygold.com.au for details on past exploration results.

References

AGES 2018 Proceedings – Shaun Schmeider, Stuart Perazzo, Leon Griesel and Chris Robinson – Newmont Tanami Operations: Multiple new discoveries supporting transformational growth in a mature mining camp. Available at https://geoscience.nt.gov.au/gemis/ntgsjspui/handle/1/87092).

Appendix 1: Buccaneer Diamond drill collars used in metallurgical analyses

Hole ID	Grid	East	North	RL	Hole Type	Depth	Azimuth	Dip	Target
BCDD2102	MGA94-52	514564	7772650	432	DD	255	219	-70	Buccaneer
BCDD2103	MGA94-52	514548	7772763	432	DD	200.2	213	-65	Buccaneer
BCDD2104	MGA94-52	514508	7772660	428	DD	120	244	-90	Buccaneer
BCDD2105	MGA94-52	514530	7772685	432	DD	120.1	60	-90	Buccaneer
BCDD2109	MGA94-52	514557	7772650	432	DD	160.4	270	-60	Buccaneer

Appendix 2: Buccaneer August 2017 Mineral Resource Estimate (ASX: 1 September 2017)

Buccaneer Gold Deposit – Mineral Resource Estimate August 2017									
Oxide	Indicated			Inferred			Total		
	Tonnes (Mt)	Grade Au (g/t)	Metal (koz)	Tonnes (Mt)	Grade Au (g/t)	Metal (koz)	Tonnes (Mt)	Grade Au (g/t)	Metal (koz)
Oxidised	0.2	1.69	12	0.1	1.82	4	0.3	1.73	16
Transitional	0.7	1.69	40	0.5	1.52	22	1.2	1.63	62
Fresh	0.3	1.59	13	8.3	1.86	494	8.5	1.85	507
Total	1.2	1.67	65	8.8	1.84	521	10.0	1.82	585

Appendix 3: JORC Table 1 Buccaneer Diamond Drilling

SECTION 1: SAMPLING TECHNIQUES AND DATA

Criteria	JORC Code explanation	Commentary
Sampling techniques	*Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.*	Prodigy Gold contracted a diamond drill rig from United Drilling Services (UDS). For the Buccaneer diamond drill holes, HQ diameter core was collected from surface to end of hole. Upon completion of orientating and geological logging diamond core was selectively cut (twice) lengthways, producing a nominal 1kg quarter core sample (minimum 0.3 metres, maximum 1.3 metres, generally 1 metre).
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used	The diamond drilled holes were selectively sampled based on observations of structural fabric, alteration minerals or veining. Sampling was carried out under Prodigy Gold's protocols and QAQC procedures as per industry standard practice. Laboratory QAQC was also conducted. See further details below. Bag sequence is checked regularly by field staff and supervising geologist against a dedicated sample register. Based on previous analysis the collection of HQ core should provide confidence appropriate sample representivity.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information	The nature of gold and base metal mineralisation could be variable and include high grade, high nugget quartz veins, massive sulphide and disseminated sulphide typical of other deposits in the area. The orientation of mineralisation is not yet confirmed. The holes were selectively sampled via methods typically used on sulphide-related deposits at this stage of drilling as detailed above and below. Mineralisation shows a correlation to sulphide and veining, in particular pyrite, and quartz sulphide veining. Minor galena, molybdenite, and chalcopyrite are also infrequently observed. Prodigy Gold samples were submitted to Bureau Veritas Adelaide for crushing and pulverising to produce a 40g charge for Fire Assay with AAS finish. No screen fire assays were carried out in this update.

Criteria	JORC Code explanation	Commentary
Drilling techniques	*Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	Diamond drilling was undertaken by UDS generating core from surface to end of hole. Coring started and ended with HQ diameter. Core is oriented using the Reflex EZ Trac orientation tool.
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed*	Recoveries from drilling were generally 100%, though occasional near surface samples have recoveries of 50%. Intervals of lost core that impact mineralised intervals are noted in the results table. Intervals of lost core and core recovery are recorded as a part of the geological logging process. Core lengths recovered are verified against drilling depths marked on core blocks and inserted by the drilling contractor.
	Measures taken to maximise sample recovery and ensure representative nature of the samples	Drilling from surface to end of hole was triple tube to maximise recovery of unconsolidated material. Samples collected are quarter core cut by an experienced technician.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	There is no relationship between grade and recovery due to the consistently high core recovery. All samples are core. Intervals of lost core are not length weighted.
Logging	*Whether core and chip samples have been geologically and geo-technically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	Prodigy Gold drilling samples were geologically logged at the core yard by a geologist using a laptop. Data on lithology, weathering, alteration, mineral content and style of mineralisation, and quartz content and style of quartz were collected. Diamond core is also logged for structure. The remaining ¾ core was shipped to Perth for further mineral resource work.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Logging is both qualitative and quantitative. Lithological factors, such as the degree of weathering and strength of alteration are logged in a qualitative fashion. The presence of quartz veining, and minerals of economic importance are logged in a quantitative manner.
	The total length and percentage of the relevant intersections logged	The entire hole was logged in full by the Prodigy Gold geologists.
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.*	Diamond core was cut with a brick core saw. Quarter core was taken for analysis, and the remaining 3/4 placed in the original core tray and shipped to Perth for further mineral resource and metallurgical analyses. Blank material was sourced from Bureau Veritas. Two certified standards acquired from GeoStats Pty. Ltd., with different gold grade and lithology, were also used. Upon receipt by the laboratory fire assay samples were logged, weighed, and dried if wet. Samples were then crushed to 2mm (70% pass), then split using a riffle splitter, with 200g crushed to 75 µm (85% pass). 40g charges were then fire assayed. Upon receipt by the laboratory SFA samples were dried and crushed until more than 70% is finer than <2mm, then a 1000g split obtained by riffle splitting is pulverized until 85% is finer than 75 microns. • Samples are sieved through nominated mesh size using Nylon sieve cloth. The whole of the coarse fraction (including the cloth) is fire assayed to determine the portion of Gold contained in the coarse fraction. The fines are analysed by fire assay in duplicate. The weight fractions, and weighted average Au in the sample are determined. • The entire + fraction, including the mesh is weighed and then submitted for Fire Assay, with the minus fraction, after weighing having two 50g charges taken for analysis by Fire Assay. • All weights and assays are reported by the laboratory
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	Samples are core.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	All samples have been analysed for gold by Bureau Veritas in Adelaide. Samples were dried and the whole sample pulverised to 85% passing 75 µm, and a sub sample of approximately 200g is retained for Fire Assay which is considered appropriate for the material and mineralisation and is industry standard for this type of sample.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	At the laboratory, regular repeat and lab check samples are assayed. Lab duplicates are captured according to standard procedures. Sample weights are documented at several stages of the sample prep process.
	Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.	Core is recovered through triple tube drilling to minimise loss and to ensure the material recovered reflects the closest approximation of the insitu samples. Samples are quarter core and are considered representative for the style of mineralisation at Buccaneer. Maintaining ¾ core is required to provide enough rock-mass for metallurgical analyses.

Criteria	JORC Code explanation	Commentary
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Grain size of the monzogranite is relatively consistent and is not expected to impact sample representivity. The sample size is many multiple larger that the grain size of the gold and is appropriate for this style of mineralisation.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	Prodigy Gold use a lead collection fire assay using a 40g sample charge. For low detection, this is read by ICP-AES, which is an inductively coupled plasma atomic emission spectroscopy technique, with a lower detection limit of 0.001ppm Au and an upper limit of 1,000ppm Au which is considered appropriate for the material and mineralisation and is industry standard for this type of sample. These techniques are a total digestion of the sample. For multi-element sample analysis, the sample is assayed for a suite of 59 different accessory elements (multi-element using the Bureau Veritas MA100/1/2 routine which uses a mixed acid digestion and finish by a combination of ICP-OES and ICP-MS depending on which method provides the best detection limit). In addition to standards and blanks previously discussed, Bureau Veritas conducts internal lab checks using standards and blanks.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	Only laboratory analysis as described above was completed on the core.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	A blank or standard was inserted approximately every 20 samples. For drill samples, blank material was supplied by the assaying laboratory. Two certified standards, acquired from GeoStats Pty. Ltd., with different gold and lithology were also used. QAQC results are reviewed on a batch by batch basis and at the completion of the program. Some minor contamination of blanks occurred, however this is near the detection limit of the analytical technique.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.*	Significant intersections are calculated independently by both the project geologist and database administrator on receiving of the results. An independent geologist inspected the core interval.
	The use of twinned holes.	The drilling is for the collection of metallurgical samples and was typically approximately 40m from existing holes. The holes showed good correlation to the indicator model and adjacent holes.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Primary data is collected into an Excel spreadsheet and the drilling data was imported in the Maxwell Data Schema (MDS) version 4.5 The interface to the MDS used is DataShed version 4.62 and SQL 2017. DataShed is a system that captures data and metadata from various sources, storing the information to preserve the value of the data and increasing the value through integration with GIS systems. Security is set through both SQL and the DataShed configuration software. Prodigy Gold has an external consultant Database Administrator with expertise in programming and SQL database administration. Access to the database by the geoscience staff is controlled through security groups where they can export and import data with the interface providing full audit trails.
	Discuss any adjustment to assay data.	Assays are not adjusted. No transformations or alterations are made to assay data stored in the database. The lab's primary Au field is the one used for plotting purposes. No averaging of results for individual samples is employed.
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	Hole collars were laid out with handheld GPS, providing accuracy of ± 3m. Drilled hole location might vary from 'design' by as much as 5m (locally) due to constraints on access clearing. This degree of variation is deemed acceptable for exploration drilling.
	Specification of the grid system used.	The grid system used is MGA GDA94, Zone 52.
	Quality and adequacy of topographic control.	For holes surveyed by handheld GPS the RL has been updated based off the 15m SRTM data and recorded in the database.
Data spacing and distribution	*Data spacing for reporting of Exploration Results.*	BCDD2102, BCDD2104 and BCDD2105 were designed to intersect modelled mineralisation at Buccaneer, while additionally providing new knowledge in historical gaps in drilling. The placement of this program's drill holes was designed to provide additional mineralisation knowledge in the upper and lower portions of the hole, where historical drilling is locally absent. See previous reporting of the Buccaneer resource for commentary on drillhole numbers and spacing. In this area the drilling is approximately 40x40m to 80x40m.

Criteria	JORC Code explanation	Commentary
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Drilling prior to this announcement has been used to prepare Mineral Resource Estimates. It is anticipated that the results from this program will be used in any future update to resource estimates at Buccaneer. The current holes upgrade the confidence in the areas of drilling but are not expected to significantly change the resource estimate considering confidence limits of the current estimate as a predominantly inferred resource category.
	Whether sample compositing has been applied.	No compositing sampling has been applied.
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	Oxide mineralisation is near horizontal. Fresh rock mineralisation is typically 10-20 dip. Drilling is vertical to 65 degrees in dip. Intersection between the drillholes and mineralisation are perpendicular to near perpendicular. Within the mineralisation veining is at a high angle to the core axis and holes do not appear to have drilled down individual high-grade veins.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No orientation-based sampling bias has been identified in this data.
Sample security	*The measures taken to ensure sample security.*	Samples were transported from the rig to a secured camp operated by Prodigy Gold personnel, where they were sawn/sampled before being transported to Alice Springs (by Prodigy Gold) and loaded onto a contracted delivery service to Bureau Veritas Laboratories secure preparation facility in Adelaide. Prodigy Gold personnel have no contact with the samples once they have been dropped off for transport. Tracking sheets have been set up to track the progress of the samples. The preparation facilities use the laboratory's standard chain of custody procedure.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	Prodigy Gold conducted a Lab Visit to Bureau Veritas laboratory facilities in Adelaide in May 2021 and found no faults. QA/QC review of laboratory results shows that Prodigy Gold sampling protocols and procedures were generally effective.

SECTION 2: REPORTING OF EXPLORATION RESULTS

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	The Buccaneer Deposit is contained within ML29822 located in the Northern Territory. The mining lease is wholly owned by Prodigy Gold, and subject to a confidential mining agreement between Prodigy Gold and the Traditional Owners via Central Land Council (CLC). This agreement is completed with a view to meet obligations of Part IV of the Aboriginal Land Rights (NT) Act 1976. A heritage clearance has been completed prior to drilling to ensure the protection of cultural sites of significance. A NT mine management plan is in place for the operation of the mineral lease.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.	The mining lease is in good standing with the NT DPIR and no known impediments exist.
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	The Buccaneer Resource was originally discovered by North Flinders Mines in the late 1990s. Newmont Asia Pacific Ltd. (Newmont) acquired the property and continued active exploration through 2006. Newmont/North Flinders drilled a total of 830 holes into the prospect – 103 aircore, 669 RAB, 48 RC, and 10 RC with diamond extensions – totalling 51,082m and provided the foundation of understanding of the Buccaneer Deposit. The Buccaneer Project has had a considerable amount of drilling completed by previous explorers, which has defined the existing resource. The sampling has been carried out using a combination of aircore (AC), reverse circulation (RC) and diamond drilling. Significant historic RAB drilling covers the area and was used in developing the lithological and mineralisation interpretation. However, this data was not used in the estimate and is not detailed here. 124 AC, 51 RC and 9 RCD (RC with diamond tails) holes were drilled between 1993 and 2004 and was undertaken by several different companies: • 1993 – 1996 – RAB and DDH drilling by Newmont/North Flinders Mines • 1997 – 1999 – RC and RAB drilling by Newmont/North Flinders Mines • 2004 – AC, RAB and RC drilling by Newmont/North Flinders Mines

Criteria	JORC Code explanation	Commentary
Geology	*Deposit type, geological setting and style of mineralisation.*	Gold mineralisation is disseminated within a monzogranite intrusion, and typically associated with quartz veins. Visible gold is seen in the quartz stockwork veining. Mineralisation extends from near-surface to a depth of over 500m and has been defined in several zones over an area of 2,200m by 800m. Mineralisation within the main body of the monzogranite has been recognised to have a moderate north-easterly dip. Horizontal oxide mineralisation is observed overlying the monzogranite intrusion.
Drill hole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* • *easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* • *dip and azimuth of the hole* • *down hole length and interception depth hole length.*	All relevant historical drill hole information has been previously reported through open file reporting by previous explorers. Summaries of all material drill holes from previous Prodigy Gold drilling are available within the Company's ASX releases.
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case	No exploration information material to the announcement has been excluded. Subsequent to the completion of the 2017 resource estimate, approximately 35,000 geological logging records from drilling completed in 2012-2016 were identified as missing from the Company's database. These have been loaded into the database and are being reviewed to assess the potential for a resource estimate with enhanced geological input.
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.*	Prodigy Gold reports length weighted intervals with a nominal 0.5g/t gold lower cut-off. As geological context is understood in exploration data highlights may be reported in the context of the full program. No upper cut-offs have been applied to reported intersections.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Intersections are reported on a geological basis noting veining, alteration and grade. Samples are typically 0.2-2g/t Au on broad zones with shorter intervals of higher grade. These narrower higher-grade intervals are consistent, but unpredictable in location from hole to hole.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents are being reported.
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.* *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	Oxide mineralisation is near horizontal. Fresh rock mineralisation is typically 10-20 dip. Drilling is vertical to 65 degrees in dip. Intersection between the drillholes and mineralisation are perpendicular to near perpendicular. Within the mineralisation veining is at a high angle to the core axis and holes do not appear to have drilled down individual high grade veins. Mineralisation boundaries are gradational and diffuse and higher sensitive to the minimum selected grade being used. Reported intervals approximate true width.
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Refer to Figures and Tables in the body of the text.
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	Reported intervals include samples of more than 1m at >0.5g/t Au or where geologically significant. Intervals are geologically significant where sulphide and/or veining is logged.
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Appropriate data is provided in the announcement previous announcements and the 2017 resource statement.

Criteria	JORC Code explanation	Commentary
Further work	*The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).* *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive*	Further work would include improved geological understanding to confirm continuity of mineralisation and could be used as a basis to target extensions of the Resource as it is currently open at depth and in several strike directions. A scoping study level report is currently underway using this understanding of the metallurgical recovery. Further work includes using these results in future optimisation of the Mineral Resource. The deposit remains open to the north and RC/diamond drilling has been proposed to extend the resource.

SECTION 3: MODIFIED TABLE 1 WITH ADDITIONAL METALURGICAL-ANALYSES-SPECIFIC DISCUSSION

No Ore Reserve has been declared for Buccaneer. This ASX release has been prepared in compliance with the current JORC Code (2012) and the ASX Listing Rules. All material assumptions on which the metallurgical testwork results are based have been included in this release and disclosed in the table below.

Criteria	*JORC Code explanation*	*Commentary*
Metallurgical Modifying Factors	*The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.* *Whether the metallurgical process is well-tested technology or novel in nature.* *The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.* *Any assumptions or allowances made for deleterious elements.* *The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.* *For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?*	Appropriate metallurgical testwork has been undertaken to support the Scoping Study level report that is underway and recovery curves were generated based on the samples collected for testing. The samples tested are considered representative of the different material types throughout the mining area, that is Oxide, Transition and Fresh material. Testwork was completed looking at some deleterious elements such as Copper, Antimony, Tellurium, Nickel and Arsenic. These are known to affect this style of processing options. Pilot plant testing was not considered necessary at this early stage as the approach of leaching gold using cyanide, gravity/CIL and heap leaching are usual and proven technologies throughout the industry. No major presence of deleterious material has been identified.
Sub-sampling techniques and sampling preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.* *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* *For all sample types, the nature, quality, and appropriateness of the sample preparation technique.* *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* *Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.* *Whether sample sizes are appropriate to the grain size of the material being sampled.*	Core comprising the Oxide, Transition and Fresh composite samples were cut using a core saw in half, then in quarters. This quarter core was used in the metallurgical testing. At the metallurgical testing lab, the whole sample of each composite was crushed and homogenised, prior to test work. The three composites were selected based on their lithographic weathering state and tested for various metallurgical properties. Sample sizes are considered to be appropriate to correctly represent the geological model and the style of mineralisation.
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Metallurgical Flotation Testwork Procedure Summary Receipt of 4,597kg, consisting of 246 cut diamond drill core 1. Selection of intervals to achieve representative grades of Oxide, Transition and Fresh material. 2. Combine and homogenise Master Composites of the following: a. Oxide b. Barren Oxide c. Transition and d. Fresh Barren Oxide Composite generated for Oxide comminution testwork due to shortfall in Oxide Composite mass provided to the lab.

Criteria	JORC Code explanation	Commentary
		3. Stage crushing of the individual Master Composites and the Barren Oxide Composite of cut diamond drill core. 4. Individual homogenising of each Master Composite and the Barren Oxide Composite crushed samples. 5. Splitting of each Master Composite, as required, for the following testwork: a. Head sample assay for elemental characterisation b. Comminution testwork on the Barren Oxide and Transition and Fresh Master Composites c. Grind establishment, to generate a reference grind time for achieving target P80µm d. Gravity gold / CIL leach testwork e. 2m column leach testwork, including intermittent bottle rolls (IBR), feed and residue size-by-assay, and agglomeration/percolation testwork f. Depending on weight, samples were either pulverised, or homogenised, split and pulverised g. Samples dispatched for assay analysis to Intertek.

Appendix 4: Table A: Barren Oxide Comminution Composite Details

Hole ID	From	To	Length
	m	m	m
BCDD2103	39.6	40.1	0.5
BCDD2103	29.0	30.0	1.0
BCDD2103	36.6	37.6	1.0
BCDD2103	38.6	39.6	1.0
BCDD2103	31.0	32.0	1.0
BCDD2103	42.6	43.8	1.2
BCDD2103	28.0	29.0	1.0
BCDD2103	9.0	10.0	1.0
BCDD2103	24.0	25.0	1.0
BCDD2103	48.6	49.6	1.0
BCDD2103	40.1	40.6	0.5
BCDD2103	53.2	54.0	0.8
BCDD2103	45.6	46.6	1.0
BCDD2104	22.0	23.0	1.0
BCDD2104	21.0	22.0	1.0
BCDD2105	22.0	23.0	1.0
BCDD2105	53.0	54.0	1.0
BCDD2105	48.0	49.0	1.0
BCDD2105	54.0	55.0	1.0
BCDD2109	35.0	36.0	1.0
BCDD2109	16.0	17.0	1.0
BCDD2109	12.7	13.9	1.2
BCDD2109	23.3	24.0	0.7
Barren Oxide Composite			**21.9**

Appendix 4: Table B: Oxide Testwork Composite Details Summary

Hole ID	From	To	Length	Au
	m	m	m	g/t
BCDD2102	10.7	11.5	0.9	0.56
BCDD2102	15.6	16.6	1.0	0.59
BCDD2104	13.0	14.2	1.2	0.47
BCDD2104	20.1	21.0	0.9	0.42
BCDD2104	26.0	27.0	1.0	4.86
BCDD2104	33.0	33.6	0.6	6.20
BCDD2104	33.6	34.5	0.9	0.38
BCDD2104	36.5	37.2	0.7	1.13
BCDD2104	37.2	38.0	0.8	0.87
BCDD2104	38.0	39.0	1.0	0.56
BCDD2104	39.0	40.0	1.0	0.66
BCDD2104	40.0	41.1	1.1	2.66
BCDD2104	41.1	41.9	0.8	2.41
BCDD2104	41.9	42.6	0.7	1.51
BCDD2104	42.6	43.5	0.9	0.58
BCDD2104	47.3	48.0	0.7	0.52
BCDD2104	48.0	48.5	0.5	1.55
BCDD2104	48.5	49.5	1.0	1.08
BCDD2104	49.5	50.0	0.5	0.59
BCDD2104	50.0	51.0	1.0	3.72
BCDD2104	51.0	52.0	1.0	6.14
BCDD2105	10.0	11.0	1.0	0.43
BCDD2105	33.6	34.3	0.7	22.10
BCDD2105	35.0	36.0	1.0	0.47
BCDD2105	36.5	37.4	0.9	3.46
BCDD2105	39.5	40.0	0.5	1.33
BCDD2105	42.0	43.0	1.0	0.36
BCDD2105	43.0	43.5	0.5	0.64
BCDD2105	43.5	44.5	1.0	1.14
BCDD2105	44.5	45.5	1.0	0.54
BCDD2109	18.0	18.7	0.7	0.53
BCDD2109	18.7	19.5	0.8	0.71
BCDD2109	29.0	30.0	1.0	4.40
BCDD2109	30.0	30.7	0.7	3.86
BCDD2109	42.7	45.7	3.0	1.93
BCDD2109	45.7	48.7	3.0	4.76
BCDD2109	51.3	54.4	3.1	0.45
BCDD2109	54.4	54.8	0.4	11.80
Oxide Composite			**36.5**	**2.41**

Appendix 4: Table C: Transition Testwork Composite Details Summary

Hole ID	From	To	Length	Au
	m	m	m	g/t
BCDD2102	73.8	75.0	1.3	0.68
BCDD2102	77.0	77.8	0.8	0.40
BCDD2102	77.8	78.2	0.4	4.32
BCDD2102	80.0	81.3	1.3	0.45
BCDD2102	81.3	82.5	1.3	2.05
BCDD2102	85.0	86.3	1.3	0.51
BCDD2102	88.5	89.2	0.7	0.45
BCDD2102	89.2	90.2	1.0	3.03
BCDD2103	50.4	51.2	0.8	0.68
BCDD2103	51.2	51.4	0.2	0.71
BCDD2103	51.4	52.7	1.3	5.09
BCDD2103	53.0	53.2	0.2	0.33
BCDD2103	60.6	60.9	0.3	1.03
BCDD2103	75.8	76.7	1.0	0.71
BCDD2103	76.7	77.6	0.9	2.18
BCDD2103	85.0	86.0	1.0	0.35
BCDD2103	86.0	87.0	1.0	0.33
BCDD2103	89.0	89.9	0.9	1.79
BCDD2104	62.0	63.0	1.0	2.84
BCDD2104	68.0	69.0	1.0	0.68
BCDD2104	79.7	80.0	0.3	38.7
BCDD2104	80.0	80.5	0.5	64.2
BCDD2104	80.5	81.5	1.0	1.09
BCDD2104	81.5	82.5	1.0	0.46
BCDD2104	82.5	83.0	0.5	6.39
BCDD2104	83.7	84.2	0.5	0.43
BCDD2104	85.2	86.4	1.2	0.43
BCDD2104	86.4	87.5	1.2	1.54
BCDD2104	87.5	88.5	1.0	0.56
BCDD2104	88.5	89.0	0.5	1.52
BCDD2104	89.0	90.0	1.0	1.48
BCDD2105	82.5	83.8	1.3	0.96
BCDD2105	83.8	85.0	1.3	0.80
BCDD2105	85.0	86.3	1.3	1.21
BCDD2105	86.3	87.5	1.3	0.73
BCDD2105	87.5	88.8	1.3	0.43
BCDD2105	88.8	90.0	1.3	0.70
BCDD2109	69.3	70.6	1.3	0.61
BCDD2109	74.5	75.0	0.5	0.98
BCDD2109	75.0	76.0	1.0	26.4
BCDD2109	81.0	82.0	1.0	1.41
BCDD2109	82.9	84.0	1.1	0.49
BCDD2109	85.0	86.2	1.2	1.35
BCDD2109	86.2	87.3	1.1	0.72
BCDD2109	89.0	90.2	1.2	0.89
Transition Composite			**41.9**	**2.84**

Appendix 4: Table D: Fresh Testwork Composite Details Summary

Hole ID	From	To	Length	Au
	m	m	m	g/t
BCDD2102	92.7	93.5	0.8	3.23
BCDD2102	97.5	98.0	0.5	0.37
BCDD2102	101.6	102.4	0.8	0.82
BCDD2102	108.8	109.7	0.9	0.36
BCDD2102	109.7	110.6	0.9	6.92
BCDD2102	116.8	117.8	1.0	0.33
BCDD2102	127.8	129.0	1.3	0.47
BCDD2102	130.7	131.7	1.0	0.73
BCDD2102	142.4	143.4	1.0	0.90
BCDD2102	143.4	144.4	1.0	2.02
BCDD2102	149.7	150.2	0.5	0.39
BCDD2102	153.3	154.3	1.0	0.48
BCDD2102	156.4	157.5	1.2	1.82
BCDD2102	159.5	160.0	0.5	0.96
BCDD2102	160.0	161.0	1.0	0.56
BCDD2102	161.0	162.0	1.0	0.34
BCDD2102	162.0	163.0	1.0	0.47
BCDD2102	166.8	167.8	1.0	1.47
BCDD2102	167.8	168.8	1.0	0.82
BCDD2102	168.8	170.0	1.2	0.97
BCDD2102	170.0	171.0	1.0	0.49
BCDD2102	174.0	175.0	1.0	0.44
BCDD2102	177.0	178.0	1.0	0.32
BCDD2102	178.0	179.0	1.0	0.37
BCDD2102	196.5	197.3	0.8	0.43
BCDD2102	197.3	198.1	0.8	0.50
BCDD2102	199.8	200.6	0.8	0.38
BCDD2102	200.6	201.2	0.6	0.52
BCDD2102	202.0	203.1	1.1	0.31
BCDD2102	206.0	206.8	0.8	0.45
BCDD2102	206.8	207.7	0.9	0.34
BCDD2102	223.0	224.0	1.0	0.39
BCDD2102	226.0	227.0	1.0	0.55
BCDD2102	227.0	227.8	0.8	5.64
BCDD2102	229.5	230.3	0.8	1.84
BCDD2102	230.3	231.5	1.2	0.69

Hole ID	From	To	Length	Au
	m	m	m	g/t
BCDD2103	141.0	142.0	1.0	0.47
BCDD2103	144.0	145.0	1.0	0.36
BCDD2103	145.0	146.0	1.0	0.47
BCDD2103	146.0	147.0	1.0	0.63
BCDD2103	149.0	149.4	0.4	0.31
BCDD2103	151.0	152.0	1.0	0.43
BCDD2103	152.0	153.0	1.0	1.48
BCDD2103	153.0	153.6	0.6	0.37
BCDD2103	154.1	154.7	0.6	1.06
BCDD2103	154.7	155.1	0.4	144
BCDD2103	155.1	155.7	0.6	4.42
BCDD2103	155.7	156.0	0.3	1.55
BCDD2103	156.0	156.5	0.5	4.25
BCDD2103	162.0	163.0	1.0	0.60
BCDD2103	177.1	177.5	0.4	0.48
BCDD2103	177.5	178.0	0.5	1.05
BCDD2103	179.0	180.0	1.0	1.70
BCDD2103	180.0	181.0	1.0	0.80
BCDD2103	181.6	181.9	0.3	0.73
BCDD2103	182.2	182.4	0.2	0.36
BCDD2103	188.7	189.3	0.7	0.75
BCDD2104	90.0	90.5	0.5	1.20
BCDD2104	90.5	91.1	0.6	0.80
BCDD2104	91.1	91.8	0.7	0.74
BCDD2104	92.2	92.6	0.4	0.53
BCDD2104	92.6	93.1	0.5	0.85
BCDD2104	94.0	95.0	1.0	0.44
BCDD2104	97.1	97.5	0.5	5.30
BCDD2104	97.5	98.1	0.6	0.54
BCDD2104	98.1	98.4	0.3	1.04
BCDD2104	99.7	100.3	0.6	1.08
BCDD2104	102.0	103.0	1.0	2.26
BCDD2104	103.8	105.0	1.3	0.69
BCDD2104	105.0	106.0	1.0	1.51
BCDD2104	106.0	106.6	0.6	0.31
BCDD2104	106.6	107.9	1.3	0.43
BCDD2104	107.9	109.1	1.2	0.69
BCDD2104	109.1	110.1	1.1	0.36
BCDD2104	113.9	115.2	1.3	0.39
BCDD2105	92.0	93.0	1.0	0.37
BCDD2105	102.3	102.6	0.3	1.19
BCDD2105	105.0	105.6	0.6	0.97
BCDD2105	105.6	106.6	1.0	0.49
BCDD2105	107.4	108.0	0.7	0.38
BCDD2105	111.0	112.0	1.0	1.52

Hole ID	From	To	Length	Au
	m	m	m	g/t
BCDD2105	112.0	113.0	1.0	1.77
BCDD2105	114.0	114.8	0.8	0.45
BCDD2105	115.8	116.9	1.1	0.46
BCDD2105	117.5	118.8	1.3	0.38
BCDD2109	90.6	91.2	0.6	0.40
BCDD2109	91.2	92.2	1.0	0.31
BCDD2109	92.2	93.1	0.9	0.82
BCDD2109	93.1	94.3	1.2	7.96
BCDD2109	94.3	95.0	0.7	1.00
BCDD2109	96.0	97.0	1.0	1.93
BCDD2109	97.0	98.0	1.0	1.07
BCDD2109	98.0	98.6	0.6	1.69
BCDD2109	98.6	99.0	0.4	0.94
BCDD2109	99.0	100.0	1.0	1.30
BCDD2109	100.7	101.2	0.5	1.42
BCDD2109	102.0	103.0	1.0	0.34
BCDD2109	105.7	106.2	0.5	0.40
BCDD2109	109.0	109.9	0.9	2.19
BCDD2109	112.3	113.2	1.0	0.40
BCDD2109	113.2	114.2	1.0	1.36
BCDD2109	114.2	115.0	0.8	0.75
BCDD2109	115.0	116.3	1.3	2.13
BCDD2109	116.3	117.0	0.7	1.04
BCDD2109	121.0	121.9	0.9	0.37
BCDD2109	125.0	126.0	1.0	0.34
BCDD2109	127.0	128.0	1.0	0.35
BCDD2109	129.0	130.0	1.0	1.27
BCDD2109	130.0	131.0	1.0	1.06
BCDD2109	140.0	141.0	1.0	0.45
Fresh Composite			**131.1**	**1.73**