VICTORY METALS

WORLD CLASS RATIOS OF DYSPROSIUM & TERBIUM 8.8KM FROM MRE

Up to 9986ppm Heavy Rare Earth Enriched TREO

Highlights:

- **High value Rare Earth Mineralisation intersected 8.8km north from the exisiting Mineral Resource Rstimate ("MRE"). Significant highlights include:**
  - **up to 68% Heavy Rare Earth Oxide ("HREO") to Total Rare Earth Oxide ("TREO")**
  - **up to 7.75% Dysprosium ("Dy") and Terbium ("Tb") ratios of TREO**
- **These new assays extends Victory's exploration zone by approx 51km²** giving North Stanmore potential to become **one of the largest Heavy Rare Earth regolith ionic-clay hosted projects in the world**
- **Heavy Rare Earth Elements[1] Dy and Tb have a combined value approx 900% higher** than Light Rare Earth Elements Praseodymium ("Pr") and Neodymium ("Nd") [2]
- **These new assays extend Victory's exploration zone by approx 51km²** giving North Stanmore potential to become **one of the largest Heavy Rare Earth regolith ionic-clay hosted projects in the world**
- Over 60% of assay results now received from 81 AC drill holes from Victory's latest infill drilling program which continues to **confirm wide, shallow intersections and TREO grades of up to 9986ppm** at a >400ppm cut off. Significant highlights include:
  - **21m @ 1015ppm TREO from 17m (IF184)**
  - **12m @ 1697ppm TREO from 40m (IF208)**
  - **11m @ 1332ppm TREO from 29m (IF167)**
  - **10m @ 1226ppm TREO from 27m (IF198)**
  - **7m @ 1568ppm TREO from 25m (IF117)**
  - **2m @ 8693ppm TREO from 41m (IF036), including**
    - **1m @ 9986ppm TREO**
- **TREO average grade from 81 holes received to date is 1072ppm**
- **Incredibly low levels of radioactive elements Uranium ("U") 2.5ppm & Thorium ("Th") 8.5ppm**

[1] The terminology used in this report for the rare earth element follows this convention whereby the LREE are defined as La, Ce, Pr, Nd and Sm, and the HREE as Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb, Lu plus Y.

[2] Refer to https://www.metal.com/Rare-Earth-Oxides

Victory Metals Limited (ASX:VTM) ("Victory" or "the Company") is pleased to provide further assay results from the 13,718m aircore ("AC") infill resource definition drilling program at the Company's 100% owned North Stanmore Rare Earth Element ("REE") Project ("North Stanmore" or the "Project").

The North Stanmore REE Project currently incorporates an Inferred Mineral Resource of 250Mt with 130,000T of TREO, containing a high average HREO/TREO ratio of 33%, and significant percentages of combined DyTB and NdPr.

The assays from an initial 81 holes confirm long intersections and TREO grades up to 9,986ppm, an average grade of 1072ppm TREO and a Heavy Rare Earth Oxide ("HREO")/(TREO) ratio of 36% and significant intersections.

In addition to the infill drilling program, the Company identified further rare earth element mineralisation sourced from the underlying North Stanmore Alkaline intrusion extending the exploration area by approximately 8.8km to the north of the existing MRE.

The area has been drill tested with assays from a 20m interval confirming significant concentrations of heavy rare earth elements with an average HREO/TREO ratio of 58%, giving North Stanmore potential to increase its resource size. Further assays are pending from drilling in this area.

This drilling was outside the Company's existing exploration target which has a range from 700Mt to 1,100Mt at a grade range of 300-500ppm TREO[3] and therefore increasing the exploration zone for the Company and giving North Stanmore potential to become one of the largest Heavy Rare Earth regolith ionic-clay hosted Projects in the world.

Victory's CEO and Executive Director Brendan Clark, commented:

"We are thrilled to announce the latest assay results, confirming the exceptional Dysprosium and Terbium ratios of 7.75% of Total Rare Earth Oxide at our North Stanmore Heavy Rare Earth Element Project. This significant confirmation located 8.8km from our existing MRE, underscores the immense potential of our project."

"The rapid expansion of our exploration target solidifies North Stanmore's position as a premier Heavy Rare Earth project on a global scale. We are confident that with continued exploration and development efforts, North Stanmore will emerge as one of the largest and most valuable projects of its kind."

"The value proposition of Dysprosium and Terbium cannot be overstated, with a combined value 900% higher than the most valuable Light Rare Earth Elements Praseodymium and Neodymium. Our latest infill resource definition drilling program has confirmed 348ppm of Dysprosium and Terbium within the MRE area, further validating the significance of our project."

"In addition to our rare earth discovery, we are pleased to report significant Scandium ("Sc") anomalism 8.8km north of the MRE area. With Scandium's high value, this discovery adds another layer of value to our project."

"Our existing MRE confirms North Stanmore as Australia's largest Heavy Rare Earth Ionic-regolith clay hosted project, with a substantial resource base of 250Mt. Our focus remains on low-cost extraction methods to maximise the value of our Heavy Rare Earth Elements."

[3] Refer to Company ASX announcement 2 August 2023

"We are encouraged by the progress of our latest drilling program, with over 60% of assay results now received showing wide intersections and high TREO grades. Notable highlights include intersections of up to 9986ppm TREO, emphasising a quality project situated in Western Australia a very safe mining jurisdiction."

"These results further validate our confidence in the potential of North Stanmore and reaffirm our commitment to unlocking its full value for our shareholders."

NdPr+DyTb Peer Comparison Table

Project	**North Stanmore**	**North Stanmore**	**Penco**	**North Stanmore**	**Makuutu**	**Pela Ema**	**Carina**	**Caldiera**
Country	Australia	Australia	Chile	**Australia**	Uganda	Brazil	Brazil	Brazil
Company	ASX: VTM	ASX: VTM	TSX: ARA	**ASX: VTM**	ASX: IXR	Serra Verde	Alcara	ASX: MEI
Status	8.8km km N of MRE	INFILL MRE	MRE	**MRE**	MRE	MRE	MRE	MRE
Nd	11.87	15.89	12.5	**13.98**	23.3	14.54	15.29	17.94
Pr	2.44	4.07	2.9	**3.6**	5.5	4.45	4.34	6.53
Dy	**5.49**	3.38	**5.5**	**3.14**	3.7	2.46	2.79	0.81
Tb	**0.82**	0.54	**0.7**	**0.49**	0.7	0.42	0.46	0.18
DyTb	**6.31**	**3.92**	**6.2**	**3.64**	**4.4**	**2.88**	**3.25**	**0.99**
Other REE	79.38	76.12	78.4	**78.79**	66.8	78.13	77.12	74.54

Project	**Jiangxi**	**Jiangxi**	**Guangxi**	**Fujian**	**Guangdong**
Country	S. China	S. China	S. China	S. China	S. China
Company	Xunwu	Xinfen	Chongzuo	Changting	Jiangxi
Nd	20.6	20.1	22.4	20.5	22
Pr	7.1	6	5.9	5.6	7
Dy	1.7	4.1	4.3	5	3.6
Tb	0.5	0.8	0.8	0.8	0.6
DyTb	2.2	4.9	5.1	5.8	4.2
Other REE	70.1	69	66.6	68.1	66.80

Table 1 & 2: Comparison of NdPr+DyTb ratios amongst clay hosted REE projects [4]

[4] IXR- Makuutu
Data sourced from ASX:IXR 5 Nov. 2020; 22 Jan. 2021; 21 July; 2021; 16 Sept. 2021; 2 Oct, 2023; 1 Feb 2024
MEI-Caldiera Data Source
Meteoric Resources Investor Presentation July 2023
TSX:ARA Penco Data Source
Amended NI 43-101 Technical Report Preliminary Economic Assessment for the Penco Module Project Sept. 15 2021
& Hochschild Presentation Alcara "A unique, scalable and sustainable heavy rare earth project" Sept. 21 2021.
TSX:ARA Carina Nova Roma Deposit Data Source
Preliminary Economic Assessment Carina Rare Earth Element Project, Nova Roma, Goias, Brazil, Nov 3 2023 Prepared by Consultoria Mineral Ltda. 309 pp.
Serra Verde Ema Pela Deposit Data Sources
Hochschild Mining Presentation Alcara "A unique, scalable and sustainable heavy rare earth project" Sept. 21 2021.
Pinto Ward, C., (2017) Controls on the Enrichment of the Serra Verde Rare Earth Deposit, Brazil. PhD Thesis Imperial College London 442 pp.

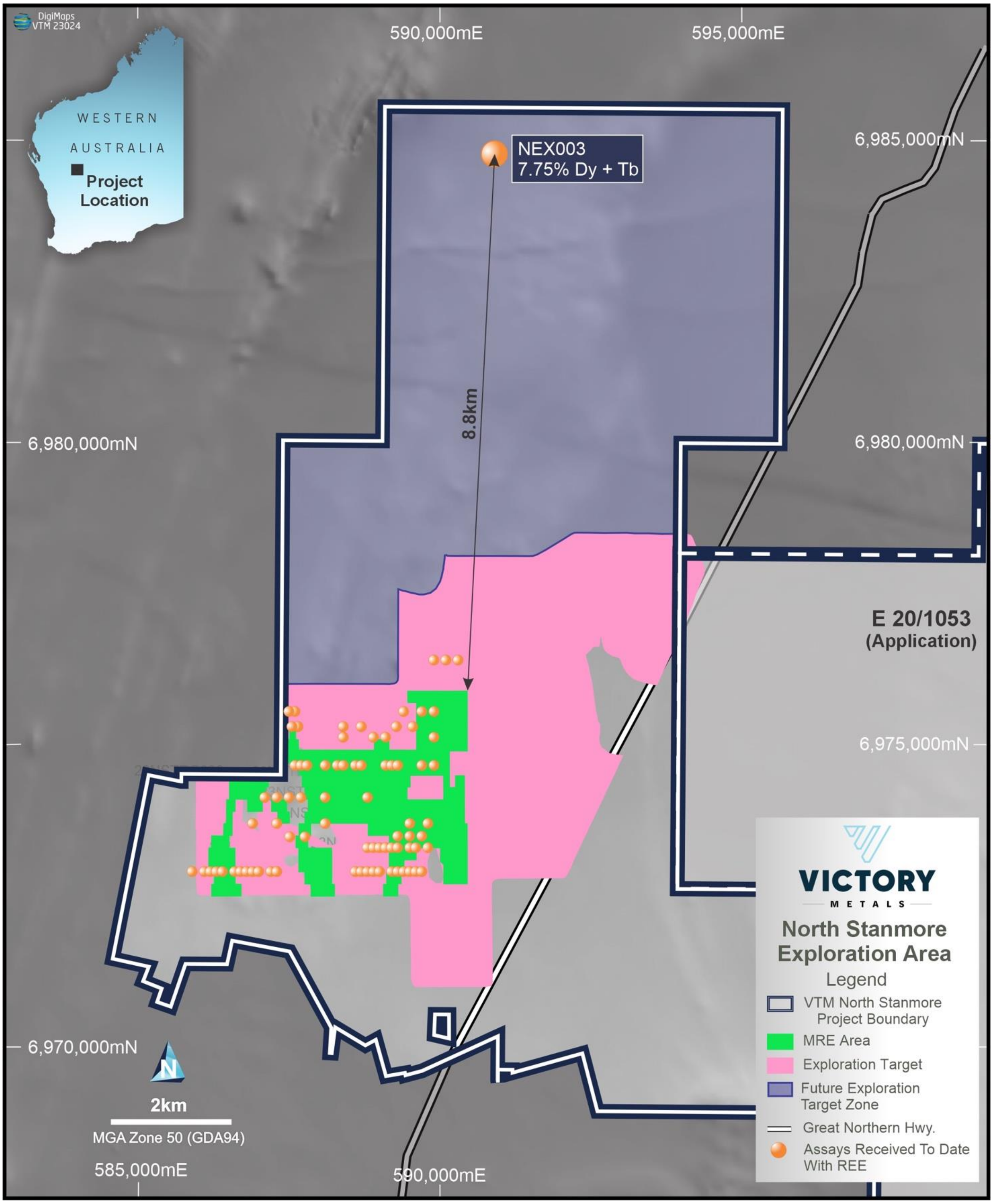

Figure 1: Map showing North Stanmore and the drill hole locations for the assays received to date (400ppm cut-off) and the Heavy Rare Earth minerilsation confirmed 8.8km from the MRE area

Technical Comments:

Many investors only consider total REO concentrations when comparing results reported for regolith-ionic clay-hosted REE systems. However, the value of regolith-ionic clay-hosted REE systems is potentially influenced by many factors. For example, the percentage of DyTb and NdPr is of considerable importance, because, DyTb is currently significantly more valuable than NdPr. There is higher commercial viability if metallurgy demonstrates ease of beneficiation using ammonium sulphate ((NH4)2SO4) or magnesium sulphate (MgSO4) with pH adjusted using sulphuric acid H2SO4 rather than HCl. It is also important for ores to have low ratios Thorium (Th) and Uranium (U) contents. Leachable & soluble ionic clay regolith projects, although of lower TREO grade to hard rock projects are potentially more attractive as hard tock projects require aggressive cracking/leaching conditions resulting in high CAPEX.

Figure 2 below shows excellent correlation between the initial MRE data and the in-fill assays received to date. Figure 2 continues to confirm North Stanmore regolith is strongly heavy REE enriched containing a significant proportion of high value DyTb. Using TREY-CeO2 >400 ppm, the in-fill data yield a TREY concentration of 1072 ppm with HREY/TREY of 36% which is similar to that of the MRE data.

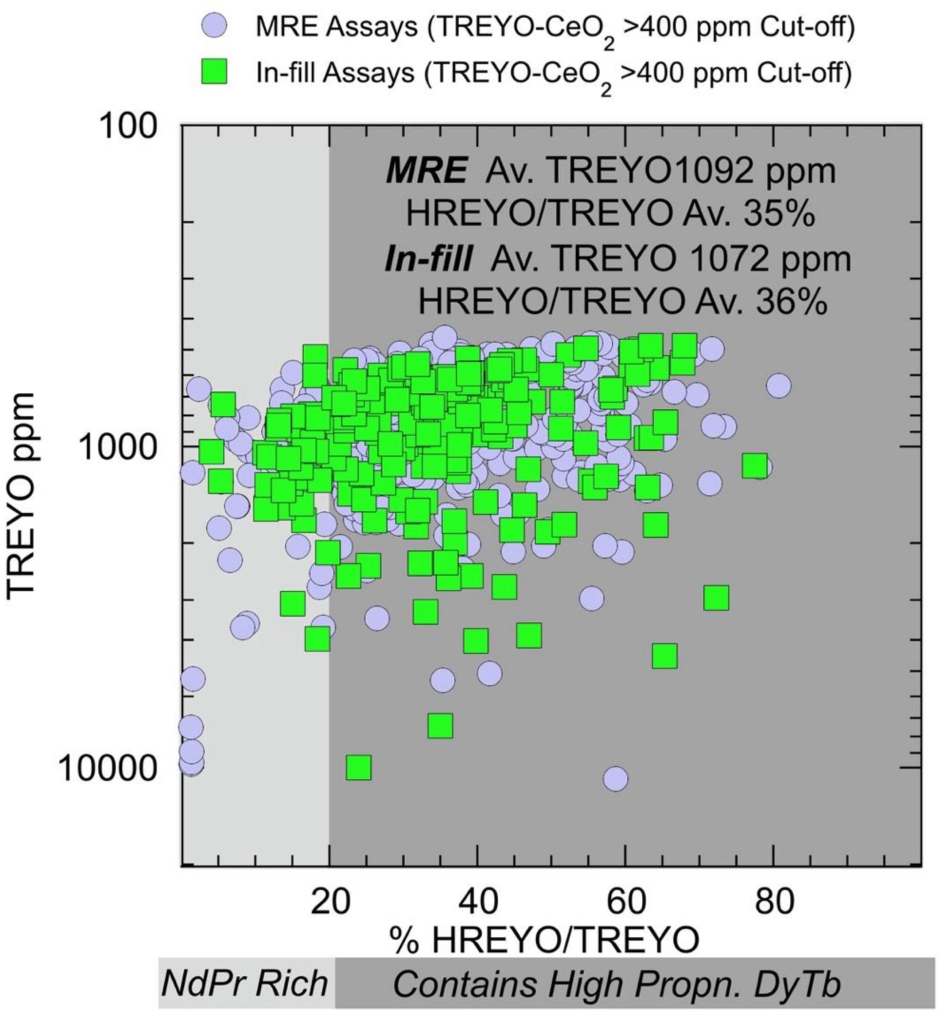

Figure 2: *Plot showing excellent agreement between the assays used for calculating the MRE and in-fill assays designed to improve the status and size of the initial resource estimate.*

The reason for subtracting CeO_2 fron the TREO concentration is to minimize the influence of C^{4+} gain. This occurs because Ce is affected by oxidation and can occur either as Ce^3+ or Ce^4+, by contrast all of the other REEs (except for Eu) only occur in the REE3+ state. Ce^4+ is mobile during weathering, separates from Ce^3+ and migrates upwards in the weathering profile, causing an increase in LREEs concentrations which can significantly skew TREY to higher values by the including intervals rich in Ce^4+. The expression, TREY-CeO_2 therefore allows the identification of assays containing significant

Ce^4+. Like other REE explorers, Victory uses this approach with a cut-off concentration of >400 ppm. The full data set received to-date from VTM's in-fill drilling program is given in the Appendix 1.

Figure 3 below shows that the majority of the North Stanmore assays exhibit negative Ce/Ce* anomalies (Ce/Ce* ratios of <1) and plot in the field characteristic of leachable ionic adsorption clay REE deposits from China, Brazil, Madagascar and Thailand.

For comparison, this figure also shows (ASX: IXR) data from Makuutu[5]. Although the North Stanmore and Makuutu data define virtually identical fields, in-fill data from the North Stanmore regolith ranges to significantly lower Ce/Ce* values which indicates substantial loss of Ce^4+. This could reflect the fact that the regolith above the North Stanmore intrusion has experienced a complex and longer weathering history than the younger crust in the African rift valley where Makuutu in Uganda is located.

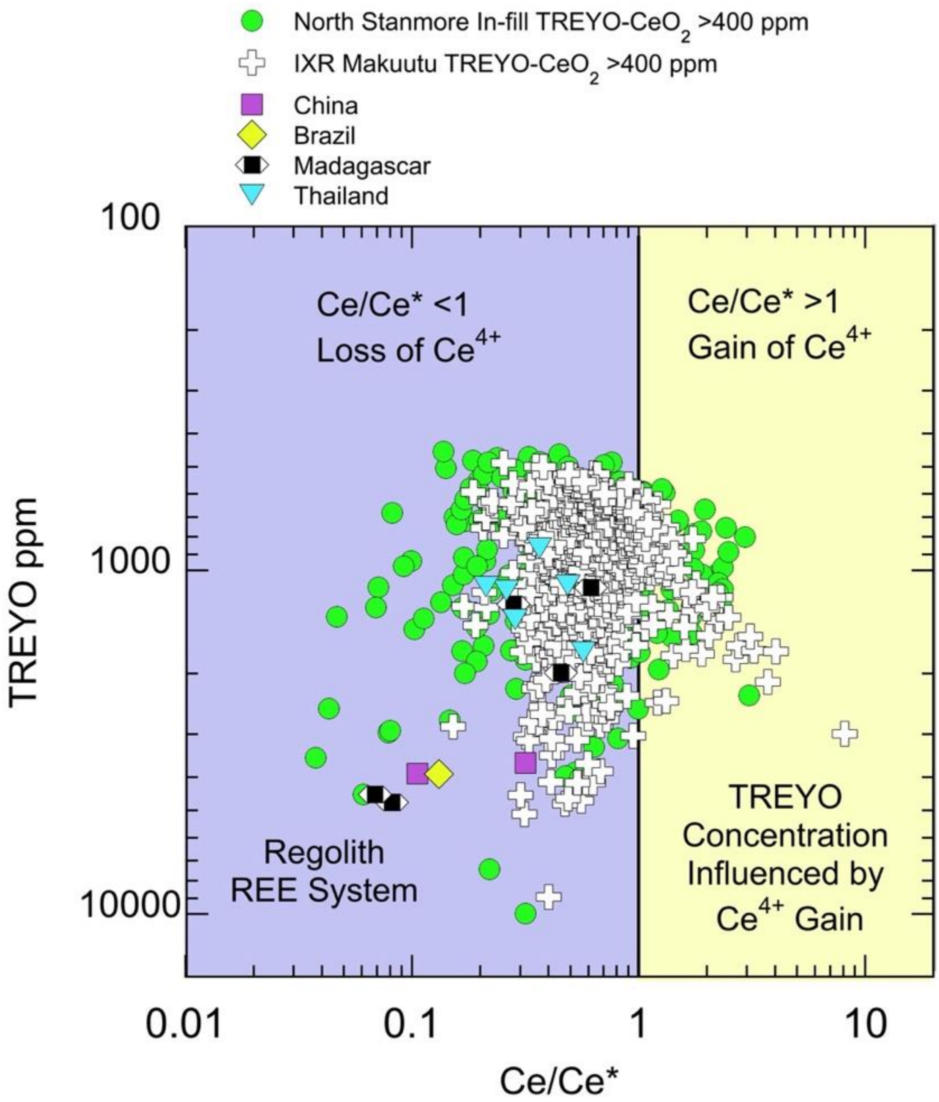

Figure 3: *Plot comparing variation in total REE- Yttrium Oxide (TREYO) concentration and Ce/Ce* ratio in North Stanmore in-fill samples with >400 ppm TREYO data for Makuutu[6] and with REE leachable ionic clay deposits from China, Brazil[7] , Madagascar[8] and Thailand[9].*

[5] IXR- Makuutu Data sourced from ASX:IXR 5 Nov. 2020; 22 Jan. 2021; 21 July; 2021; 16 Sept. 2021; 2 Oct, 2023; 1 Feb 2024

[6]ASX:IXR 5 Nov. 2020; 22 Jan. 2021; 21 July; 2021; 16 Sept. 2021; 2 Oct, 2023; 1 Feb 2024

[7] Moldoveanu G., & Papangelakis V. (2016) An overview of rare-earth recovery by ion-exchange leaching from ion-adsorption clays of various origins, Mineralogical Magazine. DOI: 10.1180/minmag.2016.080.051

[8] Ram et al., (2019) Characterisation of a rare earth element and zirconium bearing ion-adsorption clay deposit in Madagascar. Chemical Geology 522:93-107).

[9]Sanematsuet al., (2013) Geochemical and mineralogical characteristics of ion-adsorption type REE mineralization in Phuket, Thailand. Minerl Deposita 48: 437-451

An important discovery during step out drilling from the MRE area is that approximately 8.8 km north of the MRE AC drill hole NEX003 recorded a significant interval (from 24 to 44 m) that contained elevated scandium (average Sc2O3 48 ppm) containing a high proportion of Dy and Tb (HREO/TREO of 58%. Results in the Appendix 1 show REE and Sc data for this 20 m interval of regolith.

Scandium, is an important critical metal with applications ranging from hydrogen fuel cells to light alloys used in aircraft frames. As it occurs in the same Group of the Periodic Table (Gp 3) it has been called the "runt of the rare earth litter"10. As Sc occurs at potentially at economic levels in the North Stanmore regolith, discussions have been initiated with Core Metallurgy to further refine the leaching protocol to recover this additional valuable bi-product.

The potential value of regolith REE deposits is predominantly controlled by the abundances of the magnet REEs (MREE) i.e., NdPr, and DyTb and by the presence or absence of Sc. Felsic alkaine systems are generally dominated by NdPr and are Sc poor e.g., the Caldiera deposit in Brazil (ASX:MEI). By contrast, mafic and ultramafic dominated alkaline source lithologies, like those at North Stanmore, are richer in the very high value elements, DyTb and Sc.

Figure 4 shows the contrast in proportions of the MREEs and Sc2O3 between the infill drilling results from the MRE area, and from the step-out hole NEX-003, north of the MRE. The difference clearly illustrates the compositional variation between the alkaline lithologies that underlie the exploration area and those that occur 8.8km to the north. This is interpreted to reflect lithological control by the underlying source alkaline inrusion. Importantly, the regolith sampled by MEX003 north of the MRE has an average Nb/Ta ratio of 19.5 similar to that of the MRE (average Nb/Ta 16.1) and typical of alkaline igneous rocks, confirming the northward continuity of the North Stanmore Intrusion. This significant extension has important implications to the potential size of Victory's DyTb and Sc resource at North Stanmore.

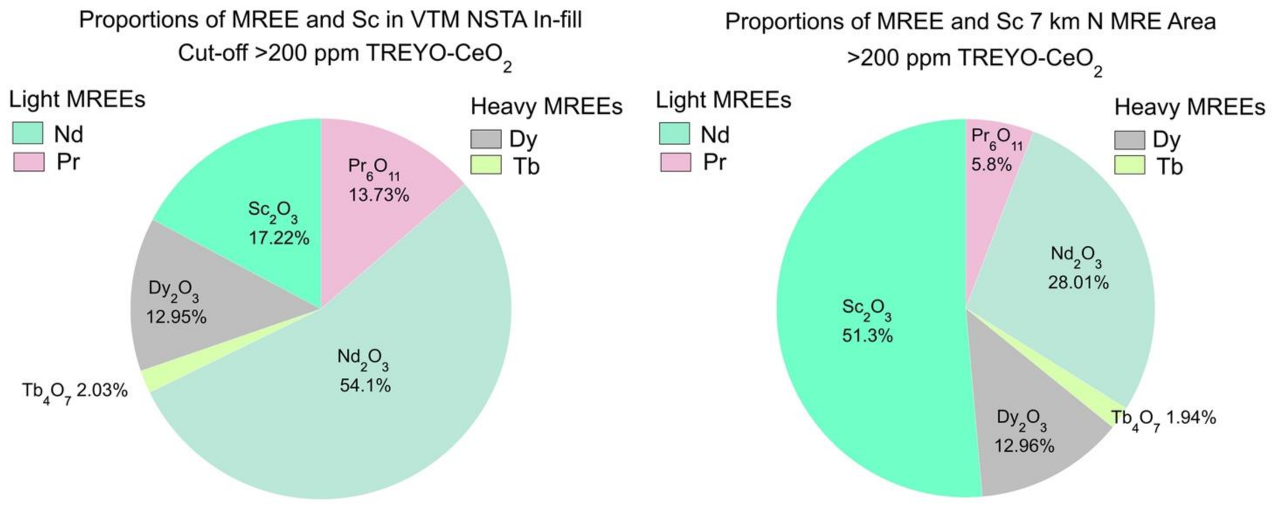

Figure 4: Pie charts comparing relative proportions of the magnet REEs (MREEs), NdPr and DyTb and Sc ("the runt of the REE litter") in confirmed by in-fill drilling in the North Stanmore MRE area and identified by recent assays from RC drilling 7 km north of the MRE area.

[10] Williams-Jones, A.E. & Vasyukova, O.V. (2018) The Economic Geology of Scandium, the Runt of the Rare Earth Element Litter. Economic Geology, 113: 973-988.

This announcement has been authorised by the Board of Victory Metals Limited.

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Victory Metals Limited

Victory is focused upon the exploration and development of its Rare Earth Element (REE) and Scandium Discovery in the Cue Region of Western Australia. Victory's key assets include a portfolio of assets located in the Midwest region of Western Australia, approximately 665 km from Perth. Victory's Ionic clay REE discovery is rapidly evolving with the system demonstrating high ratios of Heavy Rare Earth Oxides and Critical Magnet Metals NdPr + DyTb.

Competent Person Statements - Professor Ken Collerson

Statements contained in this report relating to exploration results, scientific evaluation, and potential, are based on information compiled and evaluated by Professor Ken Collerson. Professor Collerson (PhD) Principal of KDC Consulting, and a Fellow of the Australasian Institute of Mining and Metallurgy (AusIMM No. 100125), is a geochemist/geologist with sufficient relevant experience in relation to rare earth element and critical metal mineralisation being reported on, to qualify as a Competent Person as defined in the Australian Code for Reporting of Identified Mineral resources and Ore reserves (JORC Code 2012). Professor Collerson consents to the use of this information in this report in the form and context in which it appears.

Figure 5. *Regional Map showing Victory Metals tenement* package *and pending tenements.*

Appendix 1 - Aircore (AC) Drill Results > 400ppm cut off grade

Sample ID	Hole ID	From	To	La2O3	CeO2	Pr6O11	Nd2O3	Sm2O3	Eu2O3	Gd2O3	Tb2O3	Dy2O3	Ho2O3	Er2O3	Tm2O3	Yb2O3	Lu2O3	Y2O3	Sc2O3	TREYO	HREYO	HREO/TREO	Ce/Ce*	MREO	TREYO-CeO2	Th	U
		m	m	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	ppm	ppm
319633	IF004	27	28	562	61	148	633	135	30	117	16	95	19.8	60	9.3	59.9	8.8	571	49	2526	988	0.39	0.04	892	2465	8.5	7.1
319634	IF004	28	29	143	30	28	117	31	9	48	7	48	11.0	33	5.2	31.2	5.3	392	35	940	591	0.63	0.10	201	910	6.0	4.0
319635	IF004	29	30	68	27	12	54	15	5	27	4	29	6.7	21	3.2	18.5	3.1	253	58	549	372	0.68	0.20	100	522	1.6	2.9
319535	IF006	23	24	192	234	52	205	41	9	33	4	20	3.1	8	1.0	5.6	0.8	74	52	883	158	0.18	0.47	282	649	3.7	1.7
319543	IF006	31	32	216	455	54	191	33	7	22	2	12	2.0	5	0.6	3.9	0.6	72	36	1076	128	0.12	0.86	259	621	67.9	11.1
319544	IF006	32	33	168	377	42	152	27	6	18	2	10	1.8	5	0.6	3.9	0.6	67	41	881	114	0.13	0.92	206	504	63.3	7.9
319536	IF006	24	25	95	161	25	103	22	5	22	3	19	3.8	11	1.5	9.6	1.4	113	35	595	190	0.32	0.67	150	434	5.0	2.0
319378	IF009	70	71	95	46	19	77	21	8	42	9	63	14.7	45	5.9	31.7	5.2	665	26	1148	890	0.77	0.22	168	1102	4.8	1.8
319377	IF009	69	70	125	59	27	104	27	10	42	8	51	10.7	32	4.1	22.0	3.5	414	53	940	597	0.64	0.21	189	881	3.1	1.9
319292	IF010	68	69	68	136	15	59	12	4	17	3	28	8.3	28	3.7	21.7	3.5	433	30	840	550	0.65	0.86	106	704	19.7	2.6
319282	IF010	58	59	108	150	25	105	22	6	27	4	26	5.3	16	2.1	13.2	2.0	145	38	657	246	0.38	0.60	160	507	4.9	2.5
319278	IF010	54	55	119	386	40	166	35	7	22	3	18	3.3	10	1.3	9.1	1.2	65	33	885	140	0.16	1.11	226	499	7.0	2.0
319277	IF010	53	54	108	373	39	167	35	7	20	2	14	2.5	7	1.0	7.1	1.0	48	34	832	110	0.13	1.11	223	458	6.7	1.9
318097	IF021	22	23	78	195	19	78	17	4	20	4	24	4.9	15	2.1	13.4	2.3	157	29	632	245	0.39	1.03	124	438	2.4	1.8
317926	IF026	40	41	90	146	21	94	22	6	25	4	24	5.1	15	2.0	13.6	2.2	156	29	625	253	0.40	0.69	143	479	5.4	2.5
317920	IF026	34	35	105	232	35	150	33	8	26	3	17	2.9	7	0.9	5.2	0.7	61	40	688	132	0.19	0.76	206	456	5.2	2.5
317925	IF026	39	40	75	135	19	84	18	5	21	4	25	5.2	15	2.1	14.7	2.3	152	33	578	246	0.43	0.73	131	443	5.5	2.4
317922	IF026	36	37	94	203	31	130	28	8	24	3	17	2.6	7	1.0	6.1	0.7	60	33	616	129	0.21	0.75	181	413	4.7	2.4
317921	IF026	35	36	83	179	26	117	26	7	21	3	18	3.4	9	1.3	8.5	1.2	84	37	589	157	0.27	0.76	165	410	5.1	2.2
323408	IF028	33	34	175	468	50	197	41	11	40	7	37	7.4	20	3.4	20.3	3.0	210	15	1289	359	0.28	1.01	290	821	6.6	1.8
323407	IF028	32	33	82	213	26	98	20	6	22	4	26	5.9	18	3.0	18.2	2.7	206	30	750	311	0.42	0.91	154	537	7.0	2.0
329449	IF036	41	42	2404	1726	650	2368	457	114	367	46	262	47.8	135	17.4	109.2	13.9	1270	59	9986	2381	0.24	0.32	3326	8260	6.6	8.8
329450	IF036	42	43	1788	823	396	1470	296	83	294	42	266	52.7	160	22.6	149.2	20.6	1537	40	7400	2627	0.35	0.22	2174	6577	7.1	6.5
329452	IF036	44	45	564	646	138	574	128	36	155	23	151	33.8	102	13.0	80.6	11.3	1218	43	3874	1824	0.47	0.53	886	3228	4.6	2.7
329451	IF036	43	44	157	114	39	151	35	10	48	8	65	15.9	54	7.7	52.3	7.8	575	31	1340	844	0.63	0.33	263	1226	6.1	1.8
329454	IF036	46	47	86	110	18	73	14	4	22	3	22	5.1	16	2.1	12.6	1.9	206	27	597	296	0.50	0.63	116	487	5.9	1.8
329455	IF036	47	48	107	118	17	70	14	4	20	3	17	3.9	13	1.5	8.9	1.3	177	25	575	249	0.43	0.58	107	457	5.4	2.0
329448	IF036	40	41	96	317	28	106	24	6	20	3	19	3.5	11	1.6	11.0	1.4	89	43	735	164	0.22	1.42	156	418	6.3	2.6
319810	IF039	36	37	94	157	25	99	22	5	19	3	18	3.8	11	1.8	11.5	1.7	107	17	580	183	0.32	0.66	146	423	14.5	1.3
319755	IF040	35	36	164	70	44	188	57	15	89	17	118	25.4	76	10.2	62.4	9.1	775	59	1719	1196	0.70	0.17	366	1649	3.7	1.2
319756	IF040	36	37	167	17	35	163	42	12	75	12	84	18.6	54	7.7	46.2	7.1	627	27	1366	943	0.69	0.05	293	1349	15.0	2.0
319754	IF040	34	35	222	262	61	239	53	11	51	8	48	9.0	26	3.3	22.1	3.2	236	62	1256	418	0.33	0.45	356	994	2.5	1.0
319757	IF040	37	38	38	14	7	35	11	3	23	4	28	6.7	21	2.8	17.0	2.7	267	36	480	375	0.78	0.19	74	466	12.9	1.1
319753	IF040	33	34	124	474	35	134	31	6	24	3	18	2.8	7	1.1	7.7	1.1	51	58	919	122	0.13	1.46	189	445	2.2	0.9
319687	IF041	23	24	265	124	82	320	78	13	64	9	52	9.0	24	3.4	23.7	3.8	213	49	1286	416	0.32	0.17	464	1161	5.5	3.7
319688	IF041	24	25	159	227	42	162	40	7	46	7	45	8.7	24	3.7	24.1	3.8	247	19	1047	417	0.40	0.57	256	820	12.7	2.9
319689	IF041	25	26	130	155	34	140	32	6	38	6	37	7.3	20	2.8	19.0	3.2	203	16	834	342	0.41	0.48	217	679	12.6	2.8
320877	IF046	19	20	63	173	20	81	20	5	21	4	26	5.3	17	2.6	17.3	2.4	147	44	604	248	0.41	0.97	131	432	4.8	1.3
320848	IF047	14	15	80	398	25	98	23	6	21	4	26	5.4	16	2.5	16.3	2.4	151	65	875	251	0.29	1.76	153	477	2.1	1.2
320756	IF049	19	20	207	412	49	195	43	12	41	6	39	7.6	23	3.3	21.4	2.7	206	62	1267	362	0.29	0.84	290	856	1.3	1.9
320762	IF049	25	26	186	341	42	166	30	7	26	3	17	3.4	9	1.4	7.8	1.2	130	31	970	205	0.21	0.80	228	629	58.3	8.2
320763	IF049	26	27	184	375	45	180	31	6	22	3	13	2.6	7	1.0	5.8	0.8	92	37	968	154	0.16	0.84	240	594	66.8	8.2
320761	IF049	24	25	127	190	27	109	21	5	22	3	18	4.2	13	1.7	10.7	1.6	149	42	700	227	0.32	0.67	156	510	34.2	6.0
320754	IF049	17	18	95	582	29	107	24	6	20	3	20	4.4	12	1.9	13.3	1.7	104	51	1024	187	0.18	2.23	160	442	2.2	1.7
320712	IF050	36	37	94	269	31	142	30	11	32	5	35	8.0	24	3.4	22.7	3.4	251	20	961	396	0.41	0.98	213	692	7.0	2.6
320711	IF050	35	36	79	254	29	132	28	11	30	5	35	8.2	25	3.7	24.1	3.6	263	23	930	408	0.44	1.04	201	675	6.0	2.5
320713	IF050	37	38	86	332	28	123	28	9	30	5	30	5.9	18	2.4	18.3	2.5	170	18	887	291	0.33	1.35	186	556	6.1	2.2
320710	IF050	34	35	72	224	27	118	26	9	24	4	24	5.5	16	2.3	16.2	2.3	172	25	741	275	0.37	0.99	173	517	6.8	2.3

320441	IF054	40	41	196	240	40	149	29	7	27	4	24	4.3	12	1.6	9.9	1.3	110	27	856	201	0.24	0.60	217	615	7.4	2.3
320442	IF054	41	42	145	176	27	107	24	6	27	4	27	4.9	14	2.0	13.2	1.8	145	24	724	245	0.34	0.62	165	547	6.4	2.1
320440	IF054	39	40	163	230	35	125	23	5	19	3	15	2.5	7	0.9	6.1	0.8	65	36	700	125	0.18	0.68	178	471	8.2	2.1
320438	IF054	37	38	189	235	40	131	23	5	15	2	11	1.8	4	0.5	3.1	0.4	44	27	704	86	0.12	0.60	184	469	12.4	2.4
320437	IF054	36	37	165	171	34	114	19	4	13	2	10	1.4	4	0.4	2.8	0.4	36	31	575	73	0.13	0.51	159	404	13.3	2.4
320356	IF055	31	32	352	762	82	293	54	14	40	6	33	5.3	13	1.6	10.4	1.2	131	41	1798	256	0.14	0.92	414	1037	9.7	3.8
320357	IF055	32	33	292	583	67	246	48	12	37	6	30	4.8	12	1.7	10.0	1.3	123	131	1473	237	0.16	0.86	349	890	6.7	4.5
320358	IF055	33	34	213	384	44	153	30	9	29	5	27	4.8	13	1.7	10.4	1.3	130	67	1056	231	0.22	0.82	229	671	8.4	3.7
320359	IF055	34	35	177	280	34	131	27	7	25	4	27	5.0	13	1.7	10.6	1.2	147	27	891	243	0.27	0.75	196	611	8.3	2.6
320360	IF055	35	36	151	249	31	135	27	8	24	4	25	4.7	13	1.5	9.6	1.0	130	29	813	220	0.27	0.75	194	564	7.6	2.4
320292	IF056	30	31	86	179	22	88	19	5	21	3	21	4.5	13	1.9	12.9	2.0	128	23	607	212	0.35	0.85	135	428	12.2	2.1
320293	IF056	31	32	83	163	20	80	18	5	21	3	21	4.5	13	1.9	13.0	1.9	129	19	578	214	0.37	0.82	124	416	12.1	1.9
320291	IF056	29	30	89	211	22	91	19	5	18	3	18	3.7	11	1.7	11.1	1.7	109	25	615	183	0.30	0.96	134	404	12.4	1.9
320001	IF060	29	30	29	56	8	33	10	4	19	4	34	9.5	35	5.6	42.5	6.4	406	67	702	567	0.81	0.75	79	646	8.0	2.7
320015	IF060	43	44	105	45	17	72	19	7	32	6	37	7.9	24	3.2	20.8	3.0	262	23	661	403	0.61	0.22	132	616	4.3	2.8
320013	IF060	41	42	139	46	33	136	26	7	19	3	15	2.6	8	1.1	8.7	1.2	59	16	504	124	0.25	0.14	187	458	5.2	2.0
320010	IF060	38	39	124	455	32	128	25	6	17	2	15	2.7	8	1.2	8.7	1.2	65	22	892	127	0.14	1.46	178	438	6.5	2.6
320009	IF060	37	38	124	628	33	129	25	6	18	2	15	2.4	7	1.1	7.9	1.0	61	25	1060	121	0.11	1.97	179	433	6.2	2.3
320011	IF060	39	40	104	259	29	116	23	6	17	3	16	2.9	8	1.3	9.6	1.3	63	24	660	128	0.19	0.95	164	400	5.9	2.2
319942	IF062	36	37	205	812	46	183	36	10	37	5	26	5.1	13	2.1	13.7	1.8	133	28	1530	248	0.16	1.72	260	718	5.1	2.2
319944	IF062	38	39	165	60	31	122	28	8	41	5	29	6.2	15	2.1	13.9	1.9	190	28	720	313	0.43	0.17	188	660	4.5	1.5
319943	IF062	37	38	163	118	33	135	29	8	37	4	23	4.9	12	1.7	12.4	1.5	147	29	730	252	0.35	0.33	196	612	4.4	1.4
319946	IF062	40	41	103	60	20	76	19	5	28	4	26	5.7	15	2.1	14.1	2.0	177	29	557	279	0.50	0.27	126	497	4.0	1.4
319945	IF062	39	40	101	56	21	81	19	5	26	4	24	5.0	13	1.9	12.6	1.8	151	28	522	244	0.47	0.25	129	466	4.1	1.4
319194	IF138	24	25	56	349	15	60	17	7	20	4	28	5.7	18	2.7	17.9	2.6	149	12	752	255	0.34	2.43	108	403	4.8	2.5
319003	IF141	22	23	75	125	18	68	16	4	19	3	20	4.5	14	2.0	11.7	1.8	160	21	541	240	0.44	0.69	109	416	4.0	1.3
319120	IF164	19	20	127	344	35	127	26	5	22	4	24	4.5	14	2.0	13.0	1.7	130	54	880	221	0.25	1.04	191	536	8.6	3.9
319122	IF164	21	22	95	235	24	92	21	4	22	4	25	5.2	16	2.4	16.7	2.5	145	32	711	244	0.34	1.00	146	476	5.8	2.1
319057	IF165	16	17	215	523	59	227	53	11	49	8	51	10.9	33	4.6	28.0	4.0	306	26	1584	506	0.32	0.94	346	1061	5.5	4.1
319058	IF165	17	18	105	225	26	100	24	5	28	5	34	7.4	23	3.2	19.2	3.1	227	26	836	355	0.42	0.89	165	611	5.1	2.5
319056	IF165	15	16	147	382	45	162	35	7	25	4	25	4.5	14	1.9	12.0	1.6	114	23	980	209	0.21	0.94	236	598	5.8	2.5
318513	IF166	20	21	453	242	124	430	82	18	59	9	45	6.9	18	2.5	15.4	2.0	156	18	1662	332	0.20	0.21	608	1420	5.1	1.7
318512	IF166	19	20	415	326	124	428	87	18	58	9	46	7.2	18	2.5	15.6	2.1	150	24	1706	327	0.19	0.29	607	1381	5.8	1.5
318514	IF166	21	22	236	147	53	194	41	10	40	7	44	8.1	24	3.8	24.7	3.6	213	34	1048	378	0.36	0.27	297	901	4.0	1.1
318516	IF166	23	24	165	672	40	150	32	8	32	5	35	6.7	20	3.1	21.9	3.1	173	22	1369	310	0.23	1.70	230	697	6.5	1.3
318521	IF166	28	29	133	49	32	120	26	6	28	5	29	6.0	18	2.4	13.7	2.3	232	18	702	342	0.49	0.15	186	653	4.8	1.7
318515	IF166	22	23	174	147	36	138	28	6	25	4	26	4.8	14	2.1	14.5	2.1	115	29	737	213	0.29	0.38	205	590	5.7	1.0
318517	IF166	24	25	111	138	23	88	19	5	23	4	29	6.3	19	2.9	20.4	3.3	184	18	677	298	0.44	0.56	144	538	5.4	1.3
318511	IF166	18	19	148	295	43	149	29	6	20	3	18	3.0	8	1.3	8.8	1.3	78	21	813	148	0.18	0.74	214	518	6.1	1.2
318518	IF166	25	26	65	51	14	56	14	4	18	3	26	5.9	19	2.9	19.5	3.0	205	19	506	306	0.60	0.34	100	455	4.6	1.0
318519	IF166	26	27	54	53	11	44	10	3	16	3	23	5.3	16	2.5	15.7	2.6	199	23	460	287	0.62	0.45	82	407	4.5	1.4
318470	IF167	33	34	534	860	141	546	111	26	105	16	100	20.7	62	9.1	61.8	9.0	669	25	3271	1079	0.33	0.64	804	2411	6.0	4.8
318475	IF167	38	39	346	246	74	285	57	14	68	11	66	14.5	44	5.8	37.9	5.5	546	29	1820	813	0.45	0.32	435	1574	7.5	3.1
318469	IF167	32	33	373	999	109	398	80	19	69	11	64	12.1	36	5.3	36.2	4.7	315	31	2530	572	0.23	0.99	582	1532	6.6	4.1
318471	IF167	34	35	276	494	61	227	45	10	41	6	36	7.0	20	2.9	19.4	2.7	215	20	1463	361	0.25	0.78	330	970	5.0	3.0
318476	IF167	39	40	131	68	28	105	20	5	27	4	25	6.3	18	2.4	15.3	2.3	267	25	725	373	0.51	0.23	162	657	5.2	1.1
318474	IF167	37	38	123	240	29	99	21	6	26	5	33	7.3	23	3.2	23.0	3.1	245	36	883	373	0.42	0.83	165	644	7.3	3.7
318467	IF167	30	31	165	306	43	151	28	5	21	3	18	3.7	11	1.5	10.7	1.5	122	31	892	199	0.22	0.73	216	586	6.5	1.9
318468	IF167	31	32	134	224	35	127	24	5	20	3	18	3.4	10	1.3	9.5	1.3	99	29	715	170	0.24	0.66	183	491	6.2	1.9
318472	IF167	35	36	88	499	21	79	18	4	20	4	24	5.1	16	2.3	15.6	2.2	184	19	982	277	0.28	2.36	128	483	5.4	2.6
318466	IF167	29	30	132	127	36	122	22	4	16	3	15	3.0	9	1.4	10.0	1.3	98	30	601	162	0.27	0.37	177	474	5.9	1.7
318392	IF168	17	18	262	548	100	371	82	18	58	9	52	9.4	28	3.9	26.1	3.6	245	30	1815	452	0.25	0.65	531	1267	6.8	4.1

318394	IF 168	19	20	128	478	37	149	33	7	28	5	33	6.8	20	3.3	20.7	3.0	181	27	1134	309	0.27	1.40	225	656	6.0	3.5
318395	IF 168	20	21	151	168	40	164	32	7	23	3	19	3.6	10	1.5	9.8	1.4	98	24	734	177	0.24	0.44	227	565	5.9	1.7
318393	IF 168	18	19	101	404	28	113	26	6	25	5	27	5.7	17	2.6	16.6	2.4	155	27	933	262	0.28	1.54	172	529	6.7	3.8
318396	IF 168	21	22	107	62	26	108	22	5	19	3	14	2.8	8	1.1	6.5	1.0	86	25	471	145	0.31	0.24	151	409	6.3	1.2
318339	IF 169	26	27	385	636	116	483	97	20	74	9	48	8.8	22	3.1	18.0	2.4	219	38	2141	425	0.20	0.60	656	1504	5.1	3.3
318340	IF 169	27	28	198	366	68	259	52	12	41	6	37	7.2	21	3.1	20.5	2.6	204	36	1298	354	0.27	0.62	370	932	5.5	3.0
318347	IF 169	34	35	132	59	25	114	27	7	41	6	40	9.6	28	4.0	22.8	3.6	353	19	872	515	0.59	0.21	185	812	4.3	3.8
318341	IF 169	28	29	105	166	29	123	26	6	23	3	20	4.3	12	1.8	11.8	1.8	130	25	663	214	0.32	0.60	176	497	5.4	1.8
318343	IF 169	30	31	78	178	19	82	19	5	22	3	23	4.9	14	2.1	13.7	2.1	151	26	616	241	0.39	0.94	128	439	5.3	2.0
318342	IF 169	29	30	86	149	24	97	21	5	19	3	18	3.6	10	1.7	9.8	1.5	105	21	554	177	0.32	0.67	141	405	4.8	1.6
318294	IF 170	36	37	194	136	42	210	49	14	81	13	89	19.7	60	8.0	46.1	6.9	787	25	1756	1125	0.64	0.31	354	1620	4.3	3.4
318292	IF 170	34	35	201	371	72	322	65	15	54	8	48	9.1	25	3.5	21.7	3.2	247	29	1466	435	0.30	0.60	450	1095	4.5	1.9
318287	IF 170	29	30	312	599	70	238	42	8	28	4	25	4.8	14	1.9	11.8	1.8	143	43	1505	244	0.16	0.84	337	906	5.1	1.6
318293	IF 170	35	36	126	286	43	197	42	10	39	7	43	8.5	26	3.7	22.8	3.4	244	23	1102	407	0.37	0.76	290	816	4.7	2.0
318234	IF 171	50	51	187	242	33	137	30	8	43	7	49	10.2	29	4.1	23.3	3.7	400	23	1208	579	0.48	0.63	227	966	8.2	3.9
318235	IF 171	51	52	74	86	13	54	13	4	24	4	30	6.9	21	2.8	15.8	2.7	338	21	689	450	0.65	0.58	101	602	7.5	3.0
318233	IF 171	49	50	115	147	25	99	22	6	26	4	25	4.7	13	1.7	10.0	1.6	154	30	655	246	0.38	0.56	153	508	5.3	2.7
318223	IF 171	39	40	134	165	36	132	27	5	17	3	13	2.3	6	0.9	5.2	0.7	55	27	601	109	0.18	0.48	183	436	9.1	2.0
317835	IF 172	20	21	184	832	71	252	47	10	28	4	23	4.2	11	1.5	11.1	1.6	84	22	1563	179	0.11	1.40	349	731	5.4	1.9
317725	IF 174	38	39	161	193	29	121	24	6	31	5	34	7.3	23	3.4	21.3	3.2	267	22	931	402	0.43	0.58	190	738	10.9	2.5
317721	IF 174	34	35	128	563	29	106	22	5	20	3	21	4.1	12	1.8	13.6	2.0	106	27	1037	189	0.18	1.90	159	475	10.1	3.4
317723	IF 174	36	37	140	215	32	121	23	4	18	3	16	3.2	10	1.4	9.2	1.3	93	22	690	159	0.23	0.66	172	475	9.8	2.0
317722	IF 174	35	36	138	362	31	112	22	5	18	3	16	3.1	9	1.4	9.3	1.5	84	28	816	150	0.18	1.14	162	454	12.6	2.4
317724	IF 174	37	38	118	141	24	94	17	4	17	2	16	3.3	10	1.4	9.4	1.3	105	17	566	170	0.30	0.55	137	424	9.7	1.9
317645	IF 175	18	19	147	70	35	130	26	4	21	3	17	3.6	10	1.7	11.8	1.7	113	19	595	188	0.31	0.20	186	526	6.1	2.7
317515	IF 177	24	25	338	240	86	349	72	12	53	6	33	5.8	15	2.1	13.2	1.9	177	24	1404	319	0.23	0.29	474	1163	9.4	4.2
317516	IF 177	25	26	358	58	79	337	65	11	50	5	21	3.5	9	1.0	5.6	0.9	116	39	1121	224	0.20	0.07	442	1063	4.8	3.0
317514	IF 177	23	24	157	274	40	163	35	6	29	4	25	4.9	15	2.1	13.2	1.8	140	19	908	241	0.26	0.71	232	635	7.9	2.3
317461	IF 178	27	28	145	198	33	133	27	5	22	3	18	3.5	11	1.5	10.1	1.4	112	15	724	187	0.26	0.58	187	526	13.8	2.5
317462	IF 178	28	29	134	147	28	111	23	4	23	3	19	3.8	12	1.7	11.0	1.6	125	16	646	203	0.31	0.50	160	498	12.5	2.8
317463	IF 178	29	30	113	112	25	103	22	5	24	4	21	4.3	13	1.8	12.4	1.8	144	21	606	230	0.38	0.43	153	494	9.8	2.7
317459	IF 178	25	26	110	243	25	92	22	4	19	3	17	3.1	10	1.3	9.4	1.4	99	18	659	166	0.25	0.94	137	415	12.3	2.3
317458	IF 178	24	25	85	303	20	78	21	4	21	3	22	4.3	13	1.9	12.9	1.9	125	26	716	209	0.29	1.49	124	413	8.3	3.5
317457	IF 178	23	24	80	221	21	80	20	3	20	3	20	4.0	12	1.9	12.9	1.9	126	26	628	205	0.33	1.09	125	407	10.0	3.5
317411	IF 179	34	35	220	356	49	205	48	8	54	8	52	11.3	33	4.2	27.3	4.1	410	29	1490	612	0.41	0.71	314	1134	14.6	5.8
317410	IF 179	33	34	169	230	41	168	37	7	37	6	35	6.8	19	2.6	17.5	2.6	204	26	982	336	0.34	0.56	249	752	10.2	4.4
317406	IF 179	29	30	147	265	40	163	35	6	28	4	20	3.5	9	1.4	9.1	1.4	98	27	831	181	0.22	0.70	227	565	13.6	3.5
317405	IF 179	28	29	145	274	41	160	35	6	24	3	17	2.7	7	1.0	6.4	1.0	70	35	794	139	0.17	0.72	221	520	10.6	6.7
317408	IF 179	31	32	113	217	29	113	23	4	20	3	15	2.9	8	1.1	7.7	1.2	84	16	644	148	0.23	0.78	160	426	17.0	3.1
317407	IF 179	30	31	107	216	27	106	24	4	19	3	16	2.9	8	1.1	7.7	1.1	83	18	627	146	0.23	0.82	152	411	13.4	3.4
317344	IF 180	17	18	272	689	89	304	61	10	34	5	30	5.9	17	2.5	16.1	2.5	157	27	1696	281	0.17	0.88	429	1007	10.0	2.8
317345	IF 180	18	19	174	356	42	164	38	6	35	6	37	7.7	23	3.5	24.0	3.8	231	27	1151	377	0.33	0.85	250	795	8.2	2.8
317343	IF 180	16	17	187	437	58	194	39	7	26	4	27	5.7	16	2.5	17.1	2.6	154	30	1178	262	0.22	0.83	284	741	11.9	2.8
317349	IF 180	22	23	169	345	43	162	38	6	31	5	29	5.6	16	2.4	16.1	2.5	166	27	1036	279	0.27	0.83	238	691	8.5	2.0
317355	IF 180	28	29	106	200	27	112	27	5	33	6	36	7.9	25	3.4	22.9	3.4	246	21	860	388	0.45	0.76	181	660	6.8	2.9
317347	IF 180	20	21	130	247	33	123	29	6	26	5	32	7.0	21	3.1	20.7	3.1	218	27	902	340	0.38	0.77	193	655	8.8	2.0
317351	IF 180	24	25	147	269	36	142	33	7	31	5	31	6.1	17	2.6	17.5	2.5	174	25	922	295	0.32	0.76	214	653	8.8	2.1
317353	IF 180	26	27	139	203	33	134	34	7	31	5	31	6.4	19	2.8	17.8	2.7	187	23	852	309	0.36	0.61	203	649	7.7	2.1
317346	IF 180	19	20	132	262	34	125	29	5	23	4	25	5.4	16	2.5	17.0	2.6	160	26	842	261	0.31	0.79	188	581	7.2	1.9
317354	IF 180	27	28	108	154	25	101	25	5	24	4	26	5.6	16	2.3	15.7	2.3	171	26	685	273	0.40	0.60	156	531	6.9	1.8
317350	IF 180	23	24	109	239	27	103	26	5	24	4	25	5.1	16	2.3	15.9	2.4	150	27	754	249	0.33	0.89	159	515	6.7	1.8
317348	IF 180	21	22	89	176	22	84	20	4	18	3	21	4.4	13	2.0	13.6	2.0	135	27	607	216	0.36	0.80	130	432	7.3	1.7

317352	IF 180	25	26	70	182	18	72	18	4	20	3	22	4.7	16	2.3	15.0	2.2	143	27	592	232	0.39	1.05	115	410	6.9	1.9
317249	IF 182	22	23	64	271	16	60	15	5	19	4	26	6.3	22	3.4	23.8	4.1	244	32	784	358	0.46	1.76	106	512	8.6	2.2
317251	IF 182	24	25	99	214	22	85	18	5	19	3	21	4.8	16	2.3	16.1	2.8	166	41	692	255	0.37	0.96	130	478	6.7	2.4
317248	IF 182	21	22	64	295	16	59	14	4	18	3	24	5.9	20	3.0	21.7	3.8	217	25	769	321	0.42	1.90	103	475	8.4	2.1
317257	IF 182	30	31	41	124	9	42	11	4	18	3	26	6.7	22	3.3	22.4	3.8	257	30	595	367	0.62	1.30	81	471	7.5	1.8
317250	IF 182	23	24	47	238	13	52	13	4	17	3	22	5.5	19	2.8	19.6	3.5	204	36	665	301	0.45	1.96	90	426	7.6	2.3
317252	IF 182	25	26	76	162	16	64	15	4	18	3	21	4.7	15	2.3	15.7	2.7	162	55	581	248	0.43	0.96	103	418	6.9	2.0
317259	IF 182	32	33	41	72	9	44	12	4	18	3	22	5.4	19	2.7	17.8	3.1	213	32	485	308	0.63	0.76	78	413	5.0	1.9
317195	IF 183	43	44	232	101	40	180	38	11	56	9	55	13.2	40	5.5	30.1	5.3	523	16	1341	750	0.56	0.22	283	1240	11.8	2.3
317196	IF 183	44	45	109	93	15	62	13	4	22	4	25	6.4	21	2.7	16.1	2.8	304	15	701	408	0.58	0.47	106	607	11.3	2.6
317197	IF 183	45	46	105	88	15	59	12	4	21	4	24	6.2	20	2.7	14.9	2.6	287	13	665	386	0.58	0.46	102	577	10.7	2.4
317194	IF 183	42	43	128	110	28	116	23	6	19	3	17	3.4	10	1.4	9.4	1.4	99	17	573	169	0.30	0.38	164	463	13.3	1.9
317136	IF 184	46	47	371	93	93	359	80	23	69	11	62	10.8	28	3.9	24.7	3.2	254	28	1485	489	0.33	0.10	525	1392	4.7	1.8
317128	IF 184	38	39	362	556	63	227	46	12	45	7	43	9.1	28	3.8	24.5	3.3	268	13	1699	444	0.26	0.76	341	1143	11.8	3.4
317135	IF 184	45	46	246	94	64	243	56	17	51	9	48	8.9	24	3.4	22.6	2.8	217	17	1106	403	0.36	0.15	364	1012	7.0	1.7
317127	IF 184	37	38	378	597	70	247	44	10	33	5	25	4.4	12	1.6	9.5	1.4	112	11	1550	213	0.14	0.76	347	953	19.7	3.1
317137	IF 184	47	48	238	100	61	234	52	14	45	7	38	7.1	19	2.5	16.2	2.1	192	33	1030	343	0.33	0.17	341	930	5.3	2.1
317130	IF 184	40	41	206	283	38	144	30	8	31	5	36	8.4	27	4.0	26.1	3.6	273	13	1123	421	0.38	0.66	224	840	12.2	2.5
317138	IF 184	48	49	179	80	50	197	43	12	39	6	37	7.3	23	3.1	20.1	2.7	219	44	918	369	0.40	0.17	291	839	4.6	2.5
317131	IF 184	41	42	187	258	43	164	33	9	30	5	28	5.9	18	2.6	17.0	2.3	181	13	985	298	0.30	0.59	241	727	9.4	2.6
317129	IF 184	39	40	212	301	39	145	28	7	27	4	26	5.5	17	2.5	15.8	2.5	177	12	1009	285	0.28	0.68	214	708	15.9	2.3
317126	IF 184	36	37	223	650	45	163	31	8	28	4	21	4.1	11	1.4	8.7	1.1	106	13	1303	192	0.15	1.35	233	653	18.4	2.3
317124	IF 184	34	35	251	665	50	169	29	7	23	3	17	3.2	8	1.1	6.5	0.9	82	13	1316	152	0.12	1.22	239	651	12.0	1.8
317125	IF 184	35	36	206	751	43	153	29	7	28	4	21	4.0	11	1.4	8.4	1.0	103	12	1371	189	0.14	1.65	221	620	18.5	2.0
317139	IF 184	49	50	116	60	30	117	27	7	25	4	26	5.3	17	2.3	15.5	2.2	166	27	618	269	0.44	0.21	176	559	11.4	2.3
317123	IF 184	33	34	150	733	29	104	19	5	20	3	19	4.5	14	2.1	14.5	2.0	154	17	1274	238	0.19	2.32	155	540	15.5	2.3
317134	IF 184	44	45	168	173	35	128	25	6	20	3	17	3.4	10	1.5	9.6	1.4	103	14	703	174	0.25	0.46	183	530	21.5	2.0
317121	IF 184	31	32	346	526	36	80	9	1	4	1	4	0.8	3	0.5	3.7	0.5	24	12	1038	42	0.04	0.94	120	513	14.9	1.3
317142	IF 184	52	53	126	78	26	100	22	7	23	4	23	4.6	14	2.0	12.8	1.9	147	21	591	238	0.40	0.28	152	512	7.3	1.9
317133	IF 184	43	44	155	152	26	96	18	5	17	3	17	3.7	11	1.6	11.0	1.6	107	13	623	177	0.28	0.50	141	471	10.3	2.3
317141	IF 184	51	52	91	58	17	66	16	5	20	3	23	5.1	16	2.3	14.8	2.3	178	17	519	271	0.52	0.30	110	461	5.1	2.2
317064	IF 185	30	31	197	72	45	177	38	11	33	5	26	4.7	12	1.9	12.3	1.7	99	38	734	206	0.28	0.16	252	663	2.5	1.4
317061	IF 185	27	28	186	246	31	100	20	5	16	3	19	3.6	11	1.5	10.7	1.5	85	43	739	156	0.21	0.67	153	494	4.7	4.2
317069	IF 185	35	36	46	79	12	53	14	4	21	4	25	6.4	19	2.8	16.2	2.8	264	29	569	366	0.64	0.69	94	490	2.4	1.0
317067	IF 185	33	34	56	72	14	62	15	5	22	4	25	6.3	19	2.8	16.5	2.7	236	33	558	339	0.61	0.52	106	486	4.3	1.2
317063	IF 185	29	30	160	78	37	131	26	6	17	3	13	2.2	6	0.9	5.6	0.8	40	33	527	95	0.18	0.21	184	449	4.2	1.9
316991	IF 186	26	27	169	205	45	156	32	9	26	4	23	4.4	13	1.9	12.8	1.9	126	18	829	221	0.27	0.48	228	624	7.5	1.5
316992	IF 186	27	28	188	76	47	170	33	9	26	4	18	3.1	8	1.1	7.4	1.1	73	19	665	151	0.23	0.17	239	589	8.0	1.3
316994	IF 186	29	30	150	60	34	135	29	9	30	4	23	4.4	12	1.5	9.7	1.4	119	20	622	214	0.34	0.17	196	563	7.0	1.5
316993	IF 186	28	29	166	70	38	149	27	7	22	3	15	2.6	7	1.0	6.1	0.8	63	16	578	128	0.22	0.18	205	507	7.7	1.2
316885	IF 188	30	31	259	105	49	177	40	11	41	6	38	7.1	20	2.9	17.6	2.5	197	17	973	344	0.35	0.19	270	868	10.0	3.4
316884	IF 188	29	30	191	166	53	194	40	10	33	5	28	4.9	13	1.9	12.2	1.9	122	17	874	232	0.26	0.33	279	709	10.6	3.9
316806	IF 189	25	26	164	28	31	132	27	8	31	4	24	5.0	13	2.0	12.0	1.8	200	29	682	300	0.44	0.08	190	654	5.4	4.3
316807	IF 189	26	27	107	65	18	67	15	5	22	4	23	5.7	17	2.4	14.5	2.5	290	31	659	386	0.59	0.31	112	594	6.0	5.0
316801	IF 189	20	21	182	299	37	136	23	5	17	3	16	3.5	10	1.7	11.2	1.9	89	25	834	157	0.19	0.75	192	535	4.2	3.4
316802	IF 189	21	22	167	268	33	120	20	5	17	3	17	3.8	12	1.7	12.3	1.9	111	29	793	185	0.23	0.75	172	525	4.9	4.1
316800	IF 189	19	20	135	572	28	104	18	5	14	3	19	3.8	12	1.9	13.5	2.1	97	25	1028	170	0.17	1.91	154	456	4.8	4.2
316799	IF 189	18	19	137	652	26	99	17	4	13	2	16	3.4	11	1.8	12.8	1.9	92	27	1089	158	0.14	2.25	143	436	5.3	5.3
316736	IF 190	18	19	361	661	79	313	64	14	73	12	76	16.1	49	7.2	44.5	7.2	522	24	2299	822	0.36	0.81	480	1638	9.7	4.0
316737	IF 190	19	20	170	442	34	139	31	8	46	8	59	13.4	44	6.4	38.5	6.5	477	31	1522	706	0.46	1.21	239	1080	7.3	3.6
316735	IF 190	17	18	164	295	45	171	37	7	31	5	29	6.2	18	2.8	18.8	2.6	182	30	1014	303	0.30	0.70	249	719	8.0	2.2
316734	IF 190	16	17	139	274	39	150	32	6	24	3	19	3.7	11	1.6	9.7	1.4	96	37	810	176	0.22	0.75	212	537	10.9	2.2

316666	IF 191	14	15	94	392	23	88	22	5	26	5	35	7.5	26	3.8	23.7	3.6	236	20	990	372	0.38	1.74	151	598	5.5	2.1
316362	IF 192	17	18	133	478	36	126	26	6	20	4	22	3.8	10	1.5	9.6	1.2	94	23	970	172	0.18	1.41	187	492	6.7	3.6
316361	IF 192	16	17	152	317	42	146	27	5	18	3	16	2.6	7	0.9	5.9	0.7	61	25	806	121	0.15	0.80	207	489	7.3	3.3
316366	IF 192	21	22	106	185	23	86	17	4	20	4	24	4.7	14	2.1	13.3	1.8	157	17	662	245	0.37	0.77	137	477	7.3	3.4
316365	IF 192	20	21	101	170	22	82	17	4	18	3	22	4.3	13	2.0	12.2	1.7	145	17	617	226	0.37	0.75	129	448	6.6	3.2
316363	IF 192	18	19	106	305	28	101	20	5	17	3	18	3.3	9	1.3	8.5	1.0	79	14	705	146	0.21	1.13	150	401	6.9	3.0
316611	IF 193	28	29	249	324	47	186	40	11	60	10	73	17.0	53	7.6	50.4	7.7	617	17	1753	908	0.52	0.62	316	1429	12.8	6.7
316609	IF 193	26	27	198	291	55	205	41	8	27	4	22	3.5	10	1.3	8.1	1.1	73	23	948	158	0.17	0.56	286	657	6.7	4.5
316610	IF 193	27	28	124	193	27	102	22	5	21	3	22	4.6	14	2.0	13.8	1.9	127	34	682	214	0.31	0.69	154	489	7.1	3.7
316546	IF 194	28	29	231	323	67	248	49	12	38	6	34	6.2	17	2.5	16.7	2.3	160	21	1214	295	0.24	0.52	356	891	8.3	2.0
316547	IF 194	29	30	148	77	40	152	33	8	31	5	31	5.7	16	2.3	16.4	2.3	154	21	723	273	0.38	0.20	229	647	6.9	1.7
316548	IF 194	30	31	159	71	34	134	27	7	30	5	30	6.3	18	2.6	18.7	2.7	171	19	716	291	0.41	0.20	203	645	6.7	1.5
316545	IF 194	27	28	166	369	50	181	36	7	25	4	19	3.4	9	1.4	9.0	1.4	74	29	954	153	0.16	0.81	254	586	5.7	1.8
316549	IF 194	31	32	113	57	20	81	17	4	21	3	23	5.0	15	2.2	14.9	2.3	159	18	538	249	0.46	0.25	127	481	6.0	1.4
316552	IF 194	34	35	112	86	22	88	19	5	20	3	19	3.7	10	1.4	9.1	1.5	132	47	532	206	0.39	0.36	132	446	3.8	1.5
316551	IF 194	33	34	92	184	15	61	11	3	16	3	18	4.1	12	1.6	10.3	1.6	160	29	594	230	0.39	1.04	97	410	8.4	1.7
316421	IF 196	12	13	366	163	42	116	11	2	5	1	5	0.9	3	0.4	2.9	0.4	22	62	740	42	0.06	0.27	164	577	5.6	1.6
316427	IF 196	18	19	138	155	27	114	22	5	20	3	17	3.3	10	1.3	8.5	1.2	107	29	632	176	0.28	0.52	162	477	7.8	1.2
316433	IF 196	24	25	45	361	13	55	15	3	18	4	28	6.3	21	3.1	20.6	2.8	203	29	800	310	0.39	2.95	100	439	7.4	2.5
316306	IF 197	26	27	805	1058	245	962	175	36	123	18	89	15.3	40	5.7	34.4	4.5	364	27	3974	730	0.18	0.47	1315	2917	8.9	3.8
316308	IF 197	28	29	298	146	79	336	73	18	84	15	89	19.0	54	7.9	47.1	6.6	571	23	1843	912	0.49	0.19	518	1697	6.9	2.6
316307	IF 197	27	28	386	720	109	449	91	20	77	12	67	12.6	35	5.4	34.4	4.8	325	27	2348	593	0.25	0.71	638	1628	8.9	3.6
316309	IF 197	29	30	196	60	43	189	39	11	55	10	61	14.1	42	6.0	36.1	5.6	470	20	1238	711	0.57	0.13	304	1178	6.6	2.0
316310	IF 197	30	31	88	54	14	58	11	3	18	3	18	4.5	14	1.9	11.6	1.7	194	21	495	271	0.55	0.32	92	441	5.7	1.6
316171	IF 198	31	32	427	556	119	456	87	20	79	13	83	17.6	54	8.2	54.3	8.2	593	47	2576	930	0.36	0.50	671	2019	7.7	3.1
316172	IF 198	32	33	347	226	83	349	75	18	78	11	67	12.9	36	5.1	32.2	4.7	366	38	1711	631	0.37	0.27	510	1484	6.7	3.2
316175	IF 198	35	36	314	405	83	339	69	16	66	10	58	11.4	33	4.6	30.1	4.3	330	35	1774	562	0.32	0.51	490	1368	7.0	2.7
316174	IF 198	34	35	265	412	74	295	61	14	55	9	52	9.7	29	4.1	26.6	3.6	286	36	1595	489	0.31	0.59	430	1183	7.3	2.6
316176	IF 198	36	37	202	238	53	211	42	10	42	7	43	8.7	27	3.8	24.5	3.7	277	34	1193	446	0.37	0.47	314	954	6.4	2.6
316167	IF 198	27	28	263	290	75	255	45	10	29	3	15	2.3	5	0.7	4.5	0.6	47	34	1046	118	0.11	0.42	349	756	7.0	2.7
316170	IF 198	30	31	81	575	28	103	22	5	20	4	30	6.5	22	3.3	23.5	3.6	208	36	1135	326	0.29	2.35	166	560	8.7	2.3
316177	IF 198	37	38	108	86	25	99	20	5	23	4	22	4.9	15	2.2	13.4	2.1	179	26	607	270	0.45	0.34	149	521	6.1	2.4
316239	IF 199	29	30	598	1203	153	562	104	20	70	10	51	9.2	25	3.3	19.7	2.7	253	30	3084	464	0.15	0.81	776	1882	6.3	4.4
316242	IF 199	32	33	152	173	29	115	22	5	22	4	22	4.8	15	2.3	14.3	2.1	148	20	730	239	0.33	0.54	170	557	7.3	2.2
316241	IF 199	31	32	140	414	36	131	25	5	16	3	13	2.4	7	1.0	6.5	0.9	58	25	859	113	0.13	1.19	183	445	7.6	1.9
316084	IF 200	23	24	116	353	25	93	23	6	27	5	32	6.5	19	2.9	18.9	2.8	185	27	913	305	0.33	1.36	154	561	7.1	3.2
316085	IF 200	24	25	114	146	22	84	20	5	22	3	23	4.8	15	2.1	13.9	2.3	159	20	637	250	0.39	0.60	133	491	6.8	2.2
316086	IF 200	25	26	100	88	21	79	17	4	22	3	22	5.2	15	2.1	14.7	2.2	177	32	573	267	0.47	0.40	126	485	6.6	2.2
316082	IF 200	21	22	115	681	33	118	29	6	24	4	25	4.6	13	2.0	13.3	1.8	94	27	1163	188	0.16	2.24	179	483	7.6	4.0
316088	IF 200	27	28	71	63	10	36	9	3	18	3	23	5.5	17	2.4	15.7	2.5	220	24	499	310	0.62	0.49	72	436	7.6	2.0
316024	IF 201	23	24	155	681	39	133	29	6	21	4	23	4.6	13	2.0	14.1	2.1	125	29	1250	214	0.17	1.78	198	570	13.2	3.9
316022	IF 201	21	22	164	479	45	150	29	5	19	3	19	3.5	10	1.6	11.3	1.6	95	53	1037	170	0.16	1.13	217	558	11.9	5.0
316025	IF 201	24	25	99	190	19	70	17	4	18	3	22	4.4	15	2.1	14.5	2.3	140	21	620	225	0.36	0.91	114	430	10.4	3.3
321123	IF 203	54	55	167	496	51	208	43	10	33	5	27	5.1	15	1.9	13.2	2.0	133	55	1210	246	0.20	1.07	292	714	3.6	1.2
321124	IF 203	55	56	128	451	38	157	31	8	25	4	21	3.9	11	1.5	10.4	1.6	97	65	988	183	0.18	1.30	220	537	2.9	1.0
321125	IF 203	56	57	100	289	30	121	26	6	21	3	18	3.2	9	1.3	8.9	1.5	78	62	718	152	0.21	1.05	173	429	2.7	0.9
321059	IF 205	64	65	31	60	8	40	15	7	33	6	48	10.8	35	4.8	27.9	4.6	461	62	792	639	0.81	0.85	102	733	1.3	0.9
321050	IF 205	55	56	121	190	34	141	34	9	34	5	31	5.5	17	2.4	18.0	2.3	147	81	793	272	0.34	0.68	211	603	2.8	1.9
321052	IF 205	57	58	55	84	14	61	16	5	21	3	25	5.2	18	2.6	17.5	2.9	163	77	495	264	0.53	0.70	104	410	2.9	1.8
318001	IF 208	42	43	590	83	132	594	156	46	256	42	265	58.2	173	21.9	137.8	20.0	1911	38	4485	2930	0.65	0.06	1033	4402	2.6	2.6
318000	IF 208	41	42	549	844	169	701	163	39	161	27	174	35.9	114	16.5	113.6	15.4	909	36	4031	1605	0.40	0.55	1071	3187	1.8	3.2
318002	IF 208	43	44	267	53	71	328	102	31	174	31	201	45.0	139	17.4	103.8	14.2	1384	52	2961	2140	0.72	0.08	631	2908	1.8	1.4

318002	IF 208	43	44	264	54	70	325	98	30	173	30	200	44.3	134	17.2	101.5	14.0	1371	49	2927	2116	0.72	0.08	625	2874	1.6	1.4
318003	IF 208	44	45	263	36	45	189	40	11	60	9	60	13.3	42	5.4	34.2	4.7	470	40	1283	709	0.55	0.07	303	1246	2.5	1.8
318010	IF 208	51	52	215	189	45	192	46	14	63	9	58	13.1	37	4.9	30.9	4.6	505	28	1426	740	0.52	0.40	304	1237	6.3	2.5
317999	IF 208	40	41	117	1165	45	185	52	13	53	12	84	17.6	55	8.4	62.6	8.4	432	39	2311	746	0.32	3.08	326	1146	2.0	2.2
318005	IF 208	46	47	135	122	31	125	30	8	40	7	43	9.8	29	3.9	24.4	3.8	364	17	978	534	0.55	0.38	206	856	10.2	1.8
318006	IF 208	47	48	95	174	27	106	27	6	29	6	38	9.0	27	4.0	26.6	4.0	301	14	880	451	0.51	0.70	177	705	21.2	1.7
318008	IF 208	49	50	100	96	31	123	28	6	25	4	23	4.6	13	1.9	12.1	1.8	129	14	599	220	0.37	0.34	181	502	9.7	1.2
318009	IF 208	50	51	92	105	25	102	24	6	26	4	24	5.0	14	1.9	12.6	1.7	157	12	601	253	0.42	0.44	155	496	8.9	1.4
318008	IF 208	49	50	94	92	30	120	28	6	25	4	23	4.3	12	1.7	11.7	1.7	124	13	578	213	0.37	0.34	177	486	8.8	1.2
318177	IF 213	26	27	130	80	30	115	26	7	27	5	30	6.7	22	3.4	22.1	3.7	218	52	725	345	0.48	0.27	180	645	4.4	1.0
318178	IF 213	27	28	61	27	11	46	11	4	21	4	27	6.1	18	2.5	14.5	2.4	231	50	485	330	0.68	0.22	87	459	1.7	0.7
321598	IF 231	60	61	121	96	39	162	40	11	43	8	49	10.8	33	4.4	28.0	3.7	366	39	1014	557	0.55	0.33	257	918	3.2	0.6
321458	IF 232	40	41	150	384	46	207	51	14	48	8	47	9.3	28	4.0	24.7	3.7	298	42	1323	485	0.37	1.07	308	939	3.8	2.8
321455	IF 232	37	38	123	226	40	159	35	9	27	4	24	4.4	13	1.8	12.0	1.8	138	79	819	236	0.29	0.75	227	593	4.6	2.7
321463	IF 232	45	46	61	80	13	59	16	6	29	5	35	7.6	22	3.0	19.2	2.7	260	25	619	390	0.63	0.64	112	539	4.2	1.9
321457	IF 232	39	40	104	248	32	136	31	8	26	4	21	3.7	10	1.3	8.9	1.3	106	47	742	191	0.26	1.00	193	494	3.5	2.2
318704	IF 234	21	22	64	143	18	75	16	5	20	3	24	5.1	17	2.2	15.4	2.4	147	19	557	241	0.43	0.86	120	414	6.7	1.7
318777	IF 235	32	33	208	388	48	184	36	5	33	4	25	4.4	11	1.5	10.5	1.5	127	53	1090	225	0.21	0.79	262	701	6.9	2.5
318846	IF 236	28	29	667	196	116	461	102	25	124	19	109	22.2	64	8.5	49.8	7.1	766	17	2735	1194	0.44	0.15	704	2539	7.5	2.3
318845	IF 236	27	28	507	185	99	379	87	21	93	14	80	14.9	41	5.5	33.4	4.7	429	19	1993	737	0.37	0.17	572	1808	7.8	2.2
318847	IF 236	29	30	177	174	36	140	30	7	30	4	26	5.0	14	1.9	11.7	1.8	167	13	823	268	0.33	0.45	205	650	6.2	1.8
320953	IF044	23	24	93	134	21	91	22	6	35	6	39	9.2	26	3.9	24.1	3.7	320	46	835	473	0.57	0.62	158	702	5.1	2.3
326053	IF070	40	41	145	25	23	94	23	8	45	8	43	10.3	29	3.8	22.1	3.7	490	65	974	663	0.68	0.09	168	948	1.9	2.5
326046	IF070	33	34	196	205	56	225	50	13	36	4	21	3.6	9	1.5	10.1	1.4	66	64	897	166	0.19	0.45	306	692	1.7	1.3
326052	IF070	39	40	52	27	11	50	15	6	31	6	41	10.3	29	4.3	26.4	4.3	372	34	686	531	0.77	0.25	109	660	4.3	1.9
326047	IF070	34	35	108	152	33	134	32	10	31	5	28	5.7	17	2.6	18.4	2.9	133	35	710	252	0.35	0.59	199	558	5.2	1.2
326048	IF070	35	36	74	98	22	88	25	9	31	6	35	7.9	25	3.9	27.9	4.5	195	37	652	345	0.53	0.56	151	554	5.0	1.6
326049	IF070	36	37	50	64	14	61	18	7	25	5	35	7.4	24	3.7	25.5	4.4	208	38	553	346	0.63	0.56	115	488	4.6	1.2
326045	IF070	32	33	121	124	33	143	32	9	26	3	17	3.1	9	1.4	10.0	1.7	64	76	597	144	0.24	0.45	196	473	2.0	1.2
326050	IF070	37	38	42	31	11	49	15	5	21	4	31	7.0	23	3.3	24.0	3.9	196	34	468	319	0.68	0.33	96	437	4.8	1.1
326114	IF071	43	44	108	81	26	113	27	10	50	9	72	16.3	53	7.1	46.5	7.2	583	32	1210	855	0.71	0.35	221	1129	12.1	1.6
326109	IF071	38	39	144	264	47	198	51	16	59	10	69	14.3	41	5.3	32.8	4.7	381	64	1337	633	0.47	0.75	324	1073	1.8	0.3
326115	IF071	44	45	77	60	19	82	23	7	37	7	50	12.3	39	5.1	31.4	5.2	477	44	934	673	0.72	0.36	158	873	4.8	1.2
326110	IF071	39	40	125	254	37	156	38	12	41	7	46	9.6	29	3.9	24.7	3.8	247	55	1033	424	0.41	0.87	246	779	2.1	0.5
326111	IF071	40	41	90	183	25	109	30	10	40	7	52	11.6	36	4.9	32.1	4.9	315	61	951	513	0.54	0.88	194	768	2.1	0.4
326112	IF071	41	42	64	91	19	83	25	8	35	7	49	10.9	33	4.4	28.2	4.4	310	56	773	491	0.63	0.60	159	682	1.9	0.5
326108	IF071	37	38	157	123	44	174	38	10	28	4	24	4.4	13	1.8	11.4	1.6	97	64	734	196	0.27	0.34	247	610	2.8	0.4
326113	IF071	42	43	49	48	12	54	17	6	28	6	41	9.3	28	3.8	22.7	3.7	284	49	613	433	0.71	0.45	113	565	1.5	0.5
326116	IF071	45	46	57	61	13	59	15	4	22	4	25	5.6	18	2.2	12.5	2.1	233	38	532	328	0.62	0.51	100	471	4.3	0.9
326246	IF073	41	42	202	131	53	201	50	12	50	9	50	9.7	28	4.4	26.6	4.4	276	10	1108	470	0.42	0.29	313	977	8.5	2.5
326247	IF073	42	43	92	52	17	68	17	5	24	4	24	5.0	15	2.0	13.3	2.2	170	7	510	264	0.52	0.29	113	458	8.7	1.8
326344	IF075	39	40	182	468	54	216	52	12	46	8	41	7.7	20	3.0	18.5	2.8	172	71	1303	331	0.25	1.09	319	835	4.8	1.9
326345	IF075	40	41	130	234	35	139	34	8	35	6	35	7.1	19	3.1	18.3	2.7	173	50	879	308	0.35	0.80	215	645	4.4	1.8
326346	IF075	41	42	78	145	19	79	20	5	23	4	27	5.5	16	2.6	16.0	2.3	157	38	600	259	0.43	0.85	129	455	5.7	1.7
326347	IF075	42	43	71	129	14	62	17	5	23	4	27	5.6	17	2.4	15.1	2.4	177	40	570	277	0.49	0.89	107	441	9.0	1.4
326634	IF079	36	37	151	63	36	151	36	13	61	11	74	18.8	56	7.8	44.5	7.7	734	36	1466	1029	0.70	0.19	272	1403	4.7	2.5
326633	IF079	35	36	213	53	54	220	51	17	65	11	67	16.0	46	6.6	39.3	6.2	517	32	1381	790	0.57	0.11	352	1329	12.6	2.2
326635	IF079	37	38	81	97	19	78	20	6	25	5	28	6.9	20	2.8	16.2	2.6	230	46	637	343	0.54	0.55	129	540	5.6	2.3
326636	IF079	38	39	64	53	17	74	18	5	21	3	22	4.8	15	2.0	13.3	2.1	169	33	485	259	0.53	0.37	117	431	5.3	1.6
327083	IF086	30	31	323	864	79	302	58	18	48	7	40	6.9	19	2.4	15.4	2.1	157	19	1940	315	0.16	1.23	428	1077	8.8	3.1
327084	IF086	31	32	183	393	43	178	38	11	34	6	34	6.7	20	2.7	19.5	2.9	178	21	1151	315	0.27	1.01	261	758	9.5	2.1
327085	IF086	32	33	135	235	25	97	20	6	21	3	20	3.8	11	1.5	10.2	1.6	101	22	691	179	0.26	0.88	145	456	9.7	2.5

327087	IF086	34	35	105	236	19	77	17	5	20	3	22	4.6	15	2.1	13.8	2.2	141	21	683	229	0.34	1.14	122	448	7.4	2.2
324354	IF107	26	27	493	37	87	391	90	32	178	24	171	38.0	118	15.6	102.1	16.1	1721	21	3513	2415	0.69	0.04	672	3476	12.6	4.0
324353	IF107	25	26	48	19	16	67	18	6	22	4	27	5.5	18	2.5	16.7	2.7	180	45	451	284	0.63	0.14	113	432	0.3	0.6
324427	IF109	49	50	78	122	20	82	20	6	27	5	27	5.9	17	2.4	14.6	2.2	194	54	623	300	0.48	0.64	133	500	3.4	1.9
324422	IF109	44	45	90	195	29	112	24	6	22	4	20	4.1	12	1.8	11.4	1.7	102	37	636	185	0.29	0.75	165	441	6.7	2.3
324423	IF109	45	46	57	135	18	70	17	5	19	4	25	5.6	17	2.7	17.1	2.6	158	60	553	256	0.46	0.83	118	418	4.7	2.8
324921	IF117	29	30	466	623	134	506	100	27	77	11	61	10.6	27	3.9	24.4	3.2	241	26	2314	486	0.21	0.50	712	1691	10.1	4.6
324920	IF117	28	29	405	789	106	408	79	21	57	8	47	7.9	20	2.9	18.3	2.3	176	41	2148	362	0.17	0.77	570	1359	8.5	5.0
324922	IF117	30	31	324	493	78	306	65	18	59	9	53	10.6	29	4.4	28.5	4.0	297	23	1778	513	0.29	0.63	446	1285	10.5	3.8
324923	IF117	31	32	240	506	58	236	50	15	55	9	53	10.2	30	4.5	28.8	4.0	314	22	1613	523	0.32	0.88	355	1107	17.8	3.3
324919	IF117	27	28	164	432	62	234	49	13	32	5	28	4.8	13	1.9	12.4	1.7	100	28	1154	212	0.18	0.83	330	721	8.7	5.4
324917	IF117	25	26	237	450	68	238	43	10	26	4	19	3.0	7	1.0	6.3	0.6	57	28	1170	135	0.12	0.71	329	721	8.0	3.0
324918	IF117	26	27	138	354	43	148	27	7	16	2	13	2.1	5	0.8	4.9	0.6	41	25	802	92	0.12	0.91	207	448	8.8	3.4
323900	IF132	44	45	61	124	16	66	17	6	26	5	32	7.1	21	3.0	18.3	2.9	235	65	639	355	0.56	0.81	119	515	7.1	2.3
323969	IF133	47	48	303	219	79	314	73	16	101	18	113	25.2	73	11.6	69.9	10.2	785	16	2210	1223	0.55	0.29	524	1991	12.0	3.2
323966	IF133	44	45	149	301	42	163	33	6	30	5	27	5.3	15	2.4	16.1	2.4	152	24	949	261	0.27	0.77	238	649	13.9	2.8
323965	IF133	43	44	108	270	31	116	24	4	21	3	18	3.7	11	1.8	11.7	1.8	100	24	726	176	0.24	0.93	169	456	14.7	2.8
324084	IF135	23	24	161	458	50	233	62	18	68	12	82	16.2	50	7.2	46.5	6.6	462	19	1733	769	0.44	1.01	376	1275	4.0	3.8
324083	IF135	22	23	103	583	41	175	41	11	33	6	35	6.7	23	3.2	22.2	3.2	178	25	1265	321	0.25	1.71	257	682	4.8	2.0
324085	IF135	24	25	67	418	17	81	23	7	25	5	34	6.4	20	2.8	19.9	2.7	158	20	886	281	0.32	2.49	137	468	4.7	3.2
323813	IF136	25	26	213	349	55	234	53	15	56	9	47	8.9	24	3.2	19.0	2.6	237	21	1326	422	0.32	0.65	346	977	6.4	2.2
323814	IF136	26	27	106	166	25	102	22	6	25	4	28	6.2	21	3.0	20.2	3.1	237	22	773	353	0.46	0.66	159	607	6.6	2.0
323815	IF136	27	28	48	147	12	45	12	4	17	3	25	6.0	19	2.8	18.6	3.1	219	20	580	316	0.55	1.27	85	433	6.4	1.9
323753	IF137	37	38	223	447	64	279	54	13	42	6	38	6.8	18	2.5	16.5	1.9	181	21	1393	326	0.23	0.75	388	946	7.1	2.1
323754	IF137	38	39	180	322	48	185	35	9	33	5	28	5.8	17	2.6	16.3	2.3	187	20	1076	306	0.28	0.71	266	754	6.4	1.9
323756	IF137	40	41	143	166	29	123	26	7	32	5	38	8.2	24	3.3	20.8	2.8	253	15	882	394	0.45	0.54	195	715	6.0	2.7
323755	IF137	39	40	130	290	31	132	27	8	33	5	37	7.6	23	3.3	21.0	2.9	252	20	1003	393	0.39	0.93	205	713	6.1	2.6
316297	IF197	17	18	394	496	72	220	30	5	14	2	8	1.3	3	0.5	3.1	0.4	30	44	1280	68	0.05	0.61	302	784	7.7	2.9
323526	IF210	43	44	285	168	59	211	37	8	32	5	27	5.5	15	2.6	16.7	2.6	162	26	1036	277	0.27	0.27	301	868	5.3	2.0
323527	IF210	44	45	131	121	35	148	33	8	39	6	39	9.2	27	4.4	25.1	4.0	345	34	975	508	0.52	0.36	228	854	5.1	1.8
323525	IF210	42	43	196	215	52	214	46	12	44	7	36	6.7	17	2.7	16.9	2.3	161	32	1027	304	0.30	0.43	309	812	4.9	3.1
323540	IF210	57	58	83	177	21	80	17	2	18	3	18	4.1	12	1.7	9.4	1.5	131	28	579	201	0.35	0.86	122	402	26.4	0.9
Average																						**0.36**	**0.73**	**256**	**805**	**8.0**	**2.5**

Extensional Aircore (AC) Drill Results

Sample ID	Hole ID	From	To	La2O3	CeO2	Pr6O11	Nd2O3	Sm2O3	Eu2O3	Gd2O3	Tb4O7	Dy2O3	Ho2O3	Er2O3	Tm2O3	Yb2O3	Lu2O3	Y2O3	Sc2O3	TREYO	HREYO	HREO/TREO	Ce/Ce*1			Th ppm	U ppm
		m	m	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm						
322114	NEX003	24	25	18.76	50.61	6.44	28.34	8.00	4.70	10.89	2.27	16.12	3.71	12.86	1.84	13.27	2.23	129.53	48.32	309.58	197.43	0.64	1.05			1.96	1.44
322115	NEX003	25	26	28.03	73.70	12.93	65.55	22.84	14.18	32.39	6.05	42.35	9.28	27.67	3.81	25.05	4.17	260.33	43.10	628.34	425.28	0.68	0.93			1.69	1.03
322116	NEX003	26	27	11.73	30.46	4.49	24.03	6.18	4.49	9.37	1.41	9.92	2.25	7.19	1.01	6.80	1.15	70.99	50.77	191.46	114.57	0.60	0.95			1.62	0.97
322117	NEX003	27	28	13.25	33.04	4.54	22.98	6.24	4.48	8.59	1.49	10.63	2.47	7.48	1.19	7.71	1.50	73.40	53.38	199.00	118.94	0.60	0.96			1.62	0.78
322118	NEX003	28	29	12.67	31.45	4.35	20.88	6.09	4.17	7.46	1.38	9.62	2.15	7.03	1.03	6.97	1.16	61.84	53.07	178.24	102.81	0.58	0.97			1.58	0.7
322119	NEX003	29	30	14.89	30.34	4.95	24.14	6.41	3.54	8.58	1.56	10.23	2.26	7.16	0.97	7.15	1.09	68.07	50.77	191.35	110.61	0.58	0.84			1.55	0.99
322120	NEX003	30	31	11.85	29.60	4.24	21.23	6.56	3.90	7.91	1.40	8.31	2.05	6.67	1.02	6.93	1.17	55.37	43.56	168.20	94.72	0.56	0.96			1.61	0.61
322121	NEX003	31	32	15.36	35.26	5.13	23.56	6.20	4.37	9.11	1.60	10.66	2.37	7.16	1.02	7.37	1.16	71.24	49.54	201.57	116.05	0.58	0.93			1.7	0.72
322122	NEX003	32	33	14.54	35.26	4.93	20.76	7.14	3.86	8.51	1.55	10.17	2.22	6.92	0.98	6.83	1.23	68.32	53.22	193.23	110.60	0.57	0.98			2.06	0.71
322123	NEX003	33	34	12.55	30.10	4.10	19.60	5.80	3.26	7.66	1.27	9.03	2.04	6.56	0.93	6.49	1.08	62.86	50.62	173.32	101.19	0.58	0.96			1.83	0.59
322124	NEX003	34	35	10.79	29.11	3.64	16.10	4.93	2.57	6.12	1.11	7.83	1.90	5.56	0.78	5.77	1.03	54.73	47.24	151.97	87.40	0.58	1.06			1.95	0.63
322125	NEX003	35	36	13.72	33.17	4.98	22.74	5.53	3.64	8.08	1.53	10.00	2.25	7.01	0.95	7.46	1.14	63.37	48.16	185.55	105.41	0.57	0.95			1.52	0.37
322126	NEX003	36	37	13.37	34.03	4.83	22.63	6.41	3.40	8.43	1.41	9.63	1.98	6.30	0.94	6.68	1.06	59.30	49.85	180.40	99.13	0.55	0.98			1.64	0.6

322127	NEX003	37	38	21.11	47.17	7.41	38.26	11.25	5.44	14.58	2.42	14.86	3.28	9.49	1.32	9.08	1.61	93.85	48.93	281.13	155.94	0.55	0.88			1.48	0.82
322128	NEX003	38	39	15.48	36.11	5.65	29.86	7.99	4.75	10.20	1.78	11.39	2.39	7.31	1.01	7.22	1.30	67.05	48.47	209.48	114.38	0.55	0.89			2.96	0.81
322129	NEX003	39	40	17.59	39.92	6.68	34.18	9.76	5.68	12.51	2.12	14.06	2.91	8.80	1.26	9.29	1.52	87.62	53.38	253.91	145.77	0.57	0.87			1.18	0.74
322130	NEX003	40	41	14.43	34.03	5.23	24.96	6.73	5.09	9.64	1.56	9.92	2.20	6.84	1.02	6.91	1.27	62.23	35.43	192.04	106.67	0.56	0.92			1.81	1.2
322131	NEX003	41	42	10.79	27.39	4.12	20.30	5.39	4.38	7.80	1.35	8.10	1.92	6.31	0.96	6.63	1.25	56.38	36.20	163.09	95.10	0.58	0.96			1.35	0.78
322132	NEX003	42	43	16.18	36.61	5.94	28.93	7.91	4.52	10.70	1.88	11.71	2.50	7.92	1.14	7.93	1.39	74.29	52.76	219.54	123.97	0.56	0.89			1.09	1.02
322133	NEX003	43	EOH	7.15	17.20	2.69	12.83	4.10	3.27	5.30	0.99	6.85	1.57	5.85	0.86	6.50	1.14	47.24	39.57	123.55	79.57	0.64	0.93			1.22	0.55
Average																						**0.58**	**0.94**			**1.6**	**0.8**

Appendix 2 - List of holes with depths and collars for Aircore (AC) drilling

Hole Id	Easting	Northing	Elevation	Dip	Depth
IF004	588400	6975310	430.187817	90	38
IF006	588700	6975310	430.027626	90	41
IF009	589280	6975310	429.925179	90	73
IF010	589550	6975310	430.610647	90	84
IF021	588400	6975135	431.136298	90	38
IF026	589700	6975560	429.662907	90	73
IF028	589900	6975560	429.613476	90	48
IF036	589900	6975135	432.078637	90	72
IF039	587600	6974670	433.418047	90	66
IF040	587700	6974670	433.280342	90	54
IF041	587800	6974670	433.257533	90	56
IF046	588300	6974670	433.720075	90	42
IF047	588400	6974670	433.812584	90	24
IF049	588600	6974670	433.893354	90	52
IF050	588700	6974670	433.88178	90	61
IF054	589100	6974670	433.835485	90	75
IF055	589200	6974670	433.823911	90	76
IF056	589300	6974670	433.996485	90	63
IF060	589700	6974670	435.121395	90	69
IF062	589900	6974670	435.68385	90	66
IF070	587100	6974140	434.073556	90	58
IF071	587300	6974140	434.342122	90	71
IF073	587500	6974140	434.413638	90	66
IF075	587700	6974140	434.397334	90	66
IF079	588100	6974140	434.364727	90	72
IF086	588800	6974140	436.051005	90	63
IF107	586900	6973710	433.961075	90	50
IF109	587300	6973710	433.509122	90	69
IF117	588100	6973710	433.731943	90	72
IF132	587515	6973490	433.135772	90	66
IF133	587765	6973490	432.754072	90	64
IF135	589300	6973500	436.4016	90	56
IF136	589500	6973500	436.107168	90	68
IF137	589700	6973500	437.202356	90	72
IF138	589500	6973710	436.567325	90	54
IF141	589800	6973710	438.002488	90	60
IF164	588800	6973310	434.596635	90	69
IF165	588900	6973310	434.556528	90	60
IF166	589000	6973310	434.516421	90	63
IF167	589100	6973310	434.835343	90	56
IF168	589200	6973310	435.709549	90	62
IF169	589300	6973310	436.583756	90	62
IF170	589400	6973310	437.457962	90	55
IF171	589500	6973310	438.210794	90	74

IF174	589800	6973310	439.646146	90	56
IF175	585900	6972915	438.120372	90	60
IF177	586100	6972915	439.586599	90	70
IF178	586200	6972915	439.586599	90	57
IF179	586300	6972915	440.566322	90	57
IF180	586400	6972915	440.566322	90	50
IF182	586600	6972915	441.546045	90	65
IF183	586700	6972915	439.862927	90	75
IF184	586800	6972915	439.862927	90	62
IF185	586900	6972915	439.087138	90	56
IF186	587000	6972915	439.087138	90	69
IF188	587200	6972915	438.470261	90	58
IF189	587300	6972915	437.672491	90	74
IF190	588600	6972915	436.99665	90	63
IF191	588700	6972915	436.472126	90	66
IF192	588800	6972915	436.014083	90	64
IF193	588900	6972915	435.846815	90	69
IF194	589000	6972915	435.754303	90	65
IF196	589200	6972915	437.502551	90	61
IF197	589300	6972915	440.124924	90	65
IF198	589400	6972915	439.2508	90	70
IF199	589500	6972915	440.124924	90	70
IF200	589600	6972915	440.282768	90	79
IF201	589700	6972915	440.01274	90	60
IF203	587650	6975310	429.363041	90	76
IF205	587550	6975310.26	429.127899	90	74
IF208	589100	6975135	430.136925	90	62
IF210	588900	6975135	429.721801	90	59
IF213	589400	6975560	429.751002	90	33
IF231	587600	6975560	426.743907	90	74
IF232	587500	6975560	426.398964	90	75
IF233	587400	6975560	426.05402	90	67
IF234	590300	6976410	430.172509	90	62
IF235	590100	6976410	432.240029	90	73
IF236	589900	6976410	434.898578	90	45
NEX003	590900	6984775	424.805143	90	44

JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	• Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. • Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. • Aspects of the determination of mineralisation that are Material to the Public Report. • In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	• Victory Metals Australia (ASX:VTM) completed one Aircore (AC) drilling campaign and a diamond drilling program at North Stanmore during the period September-December 2023. • This drilling will compliment previous drilling to complete the 2024 resource definition drilling program. 13,718m of aircore drilling was completed. • (AC) holes were drilled vertically and spaced 100m apart along 200m - 400m spaced drill lines. • (AC) drilling samples were collected as 1-m samples from the rig cyclone. Each sample was placed into large green drill bags (900mmx600mm) for temporary storage onsite. • Each sample was then split using a 3-tier splitter for homogenizing the sample. • Split samples were then collected from the splitter and placed into calico sample bags for transport to Perth. • These split one-meter samples weighed between 1.5 and 2.5 kg depending on the sample recovery from the drill hole. • A reputable commercial transport company was used to transport the bags. • Sample weights and recoveries of the split sample was recorded on site.

Criteria	JORC Code explanation	Commentary
		• In Victory's sample processing facility in Perth, a handheld pXRF analyzer (Olympus Vanta) was used to determine anomalous REE (Rare earth element) geochemistry from the 1-m calico bags. • pXRF reading times were 75 secs over 3 cycles for multielement and REE assays. • These results are not considered reliable without calibration using chemical analysis from an accredited laboratory. However their integrity was checked using Certified REE-bearing geochemical standards. • The pXRF is used as a guide to the relative presence or absence of certain elements, including REEs vectors (La, Ce, Nd and Y) to help direct the sampling program. • Anomalous 1m samples were then transported to the assay lab for analysis by Victory personnel. • REE anomalism thresholds are determined by VTM technical lead based on historical data analysis.
Drilling techniques	• Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	• (AC) drilling uses a three bladed steel or tungsten drill bit to penetrate the weathered layer of loose soil and rock fragments. The drill rods are hollow and feature an inner tube with an outer barrel (similar to RC drilling). • (AC) drilling uses air compressors (750 cfm/350 psi) to drill holes into the weathered layer of loose soil and fragments of rock. • After drilling is complete, an injection of compressed air is unleashed into the space between the inner tube and the drill rod's inside

Criteria	JORC Code explanation	Commentary
		wall, which flushes the cuttings up and out of the drill hole to the sample cyclone through the rod's inner tube. This causes less cross-contamination between samples. • (AC) drill rigs are lighter in weight than other rigs, meaning they're quicker and more maneuverable in the bush. • (AC) Drilling was performed by Orlando Drilling from Perth, using a Cummins air compressor mounted on a Volvo GM 6x4 truck. • Regularly inspected drilling rigs with automatic rod handlers, with fire and dust suppression systems, mobile and radio communications, qualified and ticketed safety trained operators and offsiders are required by Victory's WHS systems.
Drill sample recovery	• Method of recording and assessing core and chip sample recoveries and results assessed. • Measures taken to maximise sample recovery and ensure representative nature of the samples. • Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse grained material.	• The majority of samples were dry and sample recovery was variable, depending on water flows encountered during drilling. • No defined relationship exists between sample recovery and grade. Sample bias due to preferential loss or gain of fine or coarse material has not been noted. • VTM does not anticipate any sample bias from loss/gain of material from the cyclone.
Logging	• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. • Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.	• All (AC) samples were collected as 1-meter intervals, with corresponding drill chips and clays placed into chip trays and kept for reference at VTM's sample storage facilities. • All (AC) samples in the chip trays were lithologically logged using standard industry

Criteria	JORC Code explanation	Commentary
	• The total length and percentage of the relevant intersections logged.	logging software on a notebook computer. • All (AC) samples have been logged for lithology, alteration, quartz veins, colour, fabrics. • Logging is qualitative in nature. • All (AC) samples have been analysed by a handheld pXRF. • All samples were subjected to a NIR spectrometer for the identification of minerals and the variations in mineral chemistry to detect alteration assemblages and regolith profiles. • All geological information noted above has been completed by a competent person as recognized by JORC.
Sub-sampling techniques and sample preparation	• If core, whether cut or sawn and whether quarter, half or all core taken. • If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. • For all sample types, the nature, quality and appropriateness of the sample preparation technique. • Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. • Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling. • Whether sample sizes are appropriate to the grain size of the material being sampled.	• Air core sampling was undertaken on 1m intervals using a Meztke Static Cone splitter. • Most 1-meter samples were dry and weighed between 1.5 and 2.5 kgms. • Samples from the cyclone were placed into green drill bags in laid out orderly rows on the ground. • Using a hand-held trowel, 1m samples were collected from the one-meter drill bags after splitting of the sample. • These samples were placed into calico bags and weighed between 1.5 and 2.5 kgms. • Quality control of the assaying comprised the collection of a duplicate sample every hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every 20 samples and blanks (beach sand) every 50 samples.

Criteria	JORC Code explanation	Commentary
Quality of assay data and laboratory tests	• The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. • For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. • Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	• Samples were submitted for sample preparation and geochemical analysis by ALS Perth. • All samples were analysed using a hand held Olympus Vanta XRF unit to identify geochemical threholds. These results are not considered reliable without calibration using chemical analysis. They were used as a guide to the relative presence or absence of certain elements, including REEs to help guide the drill program and which samples were submitted for analytical analysis. • All pXRF anomalous samples were sent to ALS Wangarra in Perth. Samples underwent a lithium borate fusion prior to acid dissolution and Ba, La, Ce, Cr, Cs, Pr, Nd, Sm, Eu, Gd, Tb, Dy, Ho, Er, Sc, Sm, Sn, Sr, Ta, Tm, Yb, Lu, Y, Th & U were read by ICP-MS (ALS method ME-MS81). • Ag, As, Cd, Co, Cu, Li, Mo, Ni, Pb, Ti, Zn (base metals) were analysed using a 4 acid digest and read by ICP-AES (ALS method ME-4ACD81). • All samples were crushed and pulverized so that 95% of the sample passed 75µ (ALS methods CRU-31, PUL-31). • Quality control of the assaying comprised the collection of a duplicate sample every hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every 20 samples and blanks (beach sand) every 50 samples.
Verification of sampling and assaying	• The verification of significant intersections by either independent or alternative company personnel. • The use of twinned holes.	• Verification of significant intersection was undertaken by Victory’s independent consultant Prof Kenneth Collerson (PhD, FAusIMM)

Criteria	JORC Code explanation	Commentary
	• Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. • Discuss any adjustment to assay data.	• Quality control of the assaying comprised the collection of a duplicate sample every hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every 20 samples and blanks (beach sand) every 50 samples. • ALS labs routinely re-assayed anomalous assays as part of their normal QAQC procedures. • There has been no adjustments to assay data.
Location of data points	• Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. • Specification of the grid system used. • Quality and adequacy of topographic control.	• All (AC) drill hole coordinates are in GDA94 Zone 50 • All (AC) holes were located by handheld GPS with an accuracy of +/- 5 m. • There is no detailed documentation regarding the accuracy of the topographic control. • Nominal elevation values (Z) were recorded for collars. • There were no Down-hole surveys completed as (AC) drill holes were not drilled deep enough (max to 90m) to warrant downhole surveying.
Data spacing and distribution	• Data spacing for reporting of Exploration Results. • Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. • Whether sample compositing has been applied.	• (AC) drilling at North Stanmore was on a grid spacing of 100 metre between drill holes and a line spacing between 200-400m. • Given the nature of this mineral resource drilling, the spacing is adequate for the purpose intended. • No sample compositing has been applied.
Orientation of data in relation to geological	• Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which	• The relationship between drill orientation and the mineralised structures is not known at this stage

Criteria	JORC Code explanation	Commentary
structure	this is known, considering the deposit type. • If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	as the prospects are covered by a 2-25m blanket of transported cover. • It is concluded from aerial magnetics that any mineralisation trends 010-030. Dips are unknown as the area is covered by a 2-25m blanket of transported cover. • (AC) drilling was vertical as the mineralization is interpreted to be sub parallel to the regolith profile. • Downhole widths of mineralisation are known with (AC) drilling methods to +/- 1 meter.
Sample security	• The measures taken to ensure sample security.	• All samples packaged and managed by VTM personnel. • Larger packages of samples were couriered to ALS from Cue by professional transport companies in sealed bulka bags.
Audits or reviews	• The results of any audits or reviews of sampling techniques and data.	• No sampling techniques or data have been independently audited.

Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. • The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	• North Stanmore Exploration Targets are located within E 20/871. • They form part of a broader tenement package of exploration tenements located in the Cue Goldfields in the Murchison region of Western Australia. • Native Title claim no. WC2004/010 (Wajarri Yamatji #1) was registered by the Yaatji Marlpa Aboriginal Corp in 2004 and covers the entire project area, including Coodardy and Emily Wells. • E20/871 is held 100% by Victory Metals. All tenements are secured by the DMIRS (WA Government). All tenements are granted, in a state of good standing and have no impediments.
Exploration done by other parties	• Acknowledgment and appraisal of exploration by other parties.	• The area has been previously explored for gold by Big Bell Ops, Mt Kersey (1994-1996) and Westgold (2011) and Metals Ex (2013). • Exploration by these companies has been piecemeal and not regionally systematic. • There has been no historical exploration for REEs and base metals in the tenement.
Geology	• Deposit type, geological setting and style of mineralisation.	• Both areas, lie within the Meekatharra – Mount Magnet greenstone belt. The belt comprises metamorphosed volcanic, sedimentary and intrusive

Criteria	JORC Code explanation	Commentary
		rocks. Mafic and ultramafic sills are abundant in all areas of the Cue greenstones. Gabbro sills are often differentiated with basal pyroxenite and/or peridotite and upper leucogabbric units. • The greenstones are deformed by large scale fold structures which are dissected by major faults and shear zones which can be mineralised. Two large suites of granitoids intrude the greenstone belts. • E20/871 occurs within the Cue granite, host to many small but uneconomic gold mines in the Cue area. • The productive gold deposits in the region can be classified into six categories: • Shear zones and/or quartz veins within units of alternating banded iron formation and mafic volcanics e.g. Tuckanarra and Break of Day. • Shear zones and/or quartz veins within mafic or ultramafic rocks, locally intruded by felsic porphyry e.g., Cuddingwarra. Great Fingall. • Banded jaspilite and associated clastic sedimentary rocks and mafics, generally sheared and veined by quartz, e.g. Tuckabianna. • Quartz veins in granitic rocks, close to greenstone contacts, e.g. Buttercup. • Hydrothermally altered clastic sedimentary rocks, e.g. Big Bell. • Eluvial and colluvial deposits e.g. Lake Austin, Mainland. • A post tectonic differentiated alkaline mafic to ultramafic intrusion (North Stanmore Intrusion) cuts

Criteria	JORC Code explanation	Commentary
		the Archaean greenstone belt lithologies.
Drill hole Information	• A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: • easting and northing of the drill hole collar • elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar • dip and azimuth of the hole • down hole length and interception depth • hole length. • If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	• The documentation for completed drill hole locations at the North Stanmore are located in Appendix 1 of this announcement and is considered acceptable by VTM. • Consequently, the use of any data obtained is suitable for presentation and analysis. • Given the early stages of the exploration at the North Stanmore Project, the data quality is acceptable for reporting purposes. • Future drilling programs will be dependent on the assays received. • The exploration results are considered indicative and material to the reader.
Data aggregation methods	• In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. • Where aggregate intercepts incorporate short lengths of high- grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. • The assumptions used for any reporting of metal equivalent values should be clearly stated.	• Raw composited sample intervals have been reported and aggregated where appropriate. • No aggregation methods were used during the September 2023 drilling program. • Weighted averaging of results completed for air core drilling. • There has been no cutting of high grades. • Reporting has included grades greater than 200 ppm TREOs.

Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	• These relationships are particularly important in the reporting of Exploration Results. • If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. • If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	• (AC) drilling was vertical so to intersect the mineralization orthogonally. The clay hosted REE mineralisation is interpreted to be sub parallel to the regolith profile. • As such, reported downhole drillhole widths are interpreted to be near true widths.
Diagrams	• Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	• Diagrams are used in the compilation of the (AC) drilling plans and sections for North Stanmore. Also used to show distribution of drill hole geochemistry.
Balanced reporting	• Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	• Exploration results that may create biased reporting has been omitted from these documents. • Data received for this announcement is located in Appendix 1 of this announcement.
Other substantive exploration data	• Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	Summary of the sighter 2023 Core Resources Testwork • During 2023 VTM engaged Core Resources to undertake Initial bench scale testwork on various composite samples. • The objective of the testwork program was to develop a suitable set of leach parameters to advance further extensive diagnostic leach testwork across a broader range of samples from the North Stanmore project • Testwork conditions were Initially based on typical conditions for Ionic Clay based rare earth systems. During the testwork program lower pH leaching conditions were trialed using both sulphuric acid

Criteria	JORC Code explanation	Commentary
		and hydrochloric acid. • Final test conditions used ammonium sulphate or magnesium sulfate at a concentration of 0.5 M to extract the ionic bound REE, whilst sulphuric acid was utilised to extract REEs from fine grained colloidal mineral aggregated within the samples. • A semi-optimised set of test conditions were applied to a large set of pulp samples. A 50 g sub sample was used in each diagnostic leach test at 25 wt% solids, using 0.5M magnesium sulphate solution, under ambient temperature and 4-hour leach time at pH 1.0 (adjusted with sulphuric acid). The % extractions for both rare earths and impurities are calculated using discharge liquor and discharge solid residue assays (discharge mass basis extraction). • Summary test results for the variability leach program are provided in the published announcement dated 6 November 2023 ‘High Value Mixed Rare earth carbonate produced’, Appendix 1.

Criteria	JORC Code explanation	Commentary
Further work	• The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). • Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	• Further metallurgical testwork will focus on upgrading of REE via beneficiation, optimisation of leach parameters, as well as variability leach testing of individual samples. Variability leach testwork will inform geo-metallurgical variability across the North Stanmore project. • RSC has been employed to conduct a JORC2012 compliant Mineral Resource Estimate. RSC has monitored the drilling programs using supplied SOPs to ensure the acquired data is JORC2012 compliant. • Further drilling targeting gold, scandium, base metals. PGM's and REEs is proposed for the Stanmore and Mafeking Well Projects.