UPDATED MINERAL RESOURCE SETS FOUNDATION FOR UPCOMING SCOPING STUDY AND MINE DEVELOPMENT

Scoping Study starter zone contains 350Mt of rare earth mineralisation

Highlights

- JORC 2012 compliant updated Mineral Resource Estimate (MRE) defines starter zone of **350Mt @ 778ppm TREO** strengthening the foundation parameters of the scoping study
- Starter zone contains 36% or **126Mt @ 772ppm TREO** in the **Indicated** category
- Starter zone represents only **14%** of the available tenement area
- Starter zone MRE to underpin Scoping Study and Ema Project economics
- Further conversion of remaining starter zone Inferred material to Indicated category planned pending finalisation of all drilling results during Q1
- Scoping Study is being finalised pending release during Q1
- Mineralisation is close to surface and amenable to the widely used in-situ recovery mining methods currently supplying the majority of the **world's ionic clay rare earth production**
- Updated total Interim Mineral Resource Estimate is **977Mt @ 729ppm TREO**

Andrew Reid, Managing Director, commented:

"Today's announcement is a crucial step on our path to developing the Ema project. Over the last 6 months we have been focusing on drilling the central starter zone and have now defined a 350Mt MRE with 36% of the volume in the higher confidence Indicated Category, reaffirming the technical robustness and marketable attractiveness of the Ema Project.

We expect the majority of the remaining starter zone Inferred material to be converted to the Indicated category once all final assays are received. We are now focused on finalising the Scoping Study and commencing the important permeability field trials ahead of feasibility study commencement.

The Ema Scoping Study has been developed to leverage the project's major competitive advantages, focusing on a low-capital start-up strategy. It will outline a long-life, low-cost and low risk start-up rare earth project that has potential to maintain solid cashflow margins throughout the rare earth price cycle once Ema is in production."

Brazilian Critical Minerals Limited (**ASX: BCM**) ("**BCM**" or the "**Company**") is pleased to announce an update Mineral Resource Estimate (MRE) for the Ema project, forming part of the Company´s wholly owned REE projects, Apuí, Amazon, Brazil. At a cut-off of 500ppm the starter zone MRE contains **350Mt @ 778 ppm TREO.**

Table 1. Ema REE Project 2025 starter zone Mineral Resource Estimate-@COG 500ppm TREO

JORC Category	cut-off ppm TREO	Tonnes Mt	TREO ppm	NdPr ppm	DyTb ppm	MREO ppm	MREO:TREO %
Indicated	500	126	772	178	16	194	25
Inferred	500	224	793	188	17	205	26
Total	**500**	**350**	**778**	**184**	**17**	**201**	**26**

Table 2. Ema REE Project 2025 Global Mineral Resource Estimate-@COG 500ppm TREO

JORC Category	cut-off ppm TREO	Tonnes Mt	TREO ppm	NdPr ppm	DyTb ppm	MREO ppm	MREO:TREO %
Indicated	500	135	763	174	16	190	25
Inferred	500	842	724	172	16	188	26
Total	**500**	**977**	**729**	**172**	**16**	**188**	**26**

Notes:

1. TREO = total rare earth oxides (CeO_2, Dy_2O_3, Er_2O_3, Eu_2O_3, Gd_2O_3, Ho_2O_3, La_2O_3, Lu_2O_3, Nd_2O_3, Pr_6O_{11}, Sm_2O_3, Tb_4O_7, Tm_2O_3, Yb_2O_3) + Y_2O_3
2. NdPr=Pr_6O_{11}+Nd_2O_3
3. DyTb= Dy_2O_3 + Tb_4O_7
4. Totals may not balance due to rounding of figures.
5. The estimate of Mineral Resources are not Ore Reserves as they have not demonstrated economic viability and may be materially affected by environmental, permitting, legal, title, taxation, socio-political, marketing, or other relevant factors.
6. Mineral resources were classified as Indicated and Inferred only.
7. Mineral Resources were prepared in accordance with Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012) incorporating drilling data acquired by 2023 and 2024.
8. Blocks estimated by ordinary kriging at support of 100 m × 100 m × 4 m with sub-blocks 25 m × 25 m × 2m.
9. The results are presented in-situ and undiluted, are constrained within optimized open pit shell, and are considered to have reasonable prospects of economic viability, using the following parameters:
   a. Pit slope angle: 25°.
   b. Selling Prices: estimated by element oxide.
   c. Costs: Mining: 2.13US$/t mined; Process: 7.23 US$/t processed; Royalties: 2% of revenue; Selling costs: 7.03US$/kg REO.
   d. Metallurgical Efficiencies estimated by element.

Project Summary

The Ema project is located in the State of Amazonas in Brazil (Figure 1). The discovery of rare earths at the Ema project was announced in May 2023, with the maiden MRE announced in April 2024.

Figure 1. Location of the Ema project in Brazil

Mineral Resource Estimate Update

The updated Mineral Resource Estimate was undertaken by GE21 Consultaria Mineral in Brazil and incorporates the assay results from the priority 1 area only of the recently completed 2024, 270-hole drill program (Figure 2).

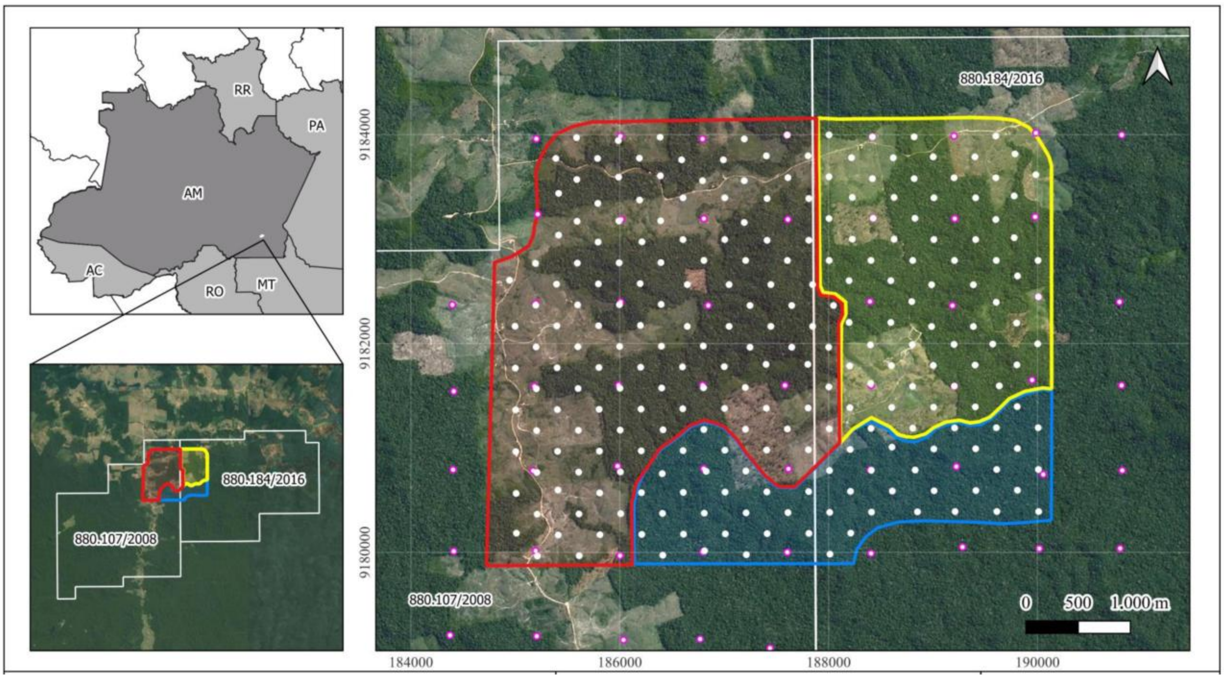

Figure 2. Central infill drilling program 2024. Red = Priority 1, Yellow = Priority 2, Blue = Priority 3. White dots = 270-hole 2024 drilling program. Pink dots represent 2023 drilling program.

This updated Mineral Resource Estimate for the Ema project highlights significant progress and enhanced confidence in the resource base. Key takeaways include:

1. **Starter Zone Mineral Resource**:
   - Approximately **350Mt @ 778ppm TREO**, using a cut-off of 500ppm.
   - Sufficient for underpinning a **long mine life**, critical for scoping and feasibility studies.
2. **Resource Classification**:
   - **Indicated Resources** now account for **135Mt (14%)** of the total global MRE.
   - Within the starter zone (Figure 2), **36%** of the total is classified as Indicated, enhancing confidence in initial project stages.
3. **Outstanding Assays**:
   - Awaiting final assay results from Priority 2 and 3 areas.
   - Expect large proportion incorporation into the **Indicated category**, supported by mineralisation style and consistency with Priority 1 results.
4. **Impact on Project Development**:
   - The inclusion of the Indicated portion bolsters confidence in the Scoping Study outcomes.
   - Strengthens the foundation for establishing a **future Ore Reserve**.
   - Facilitates more precise project design and economic evaluations during the feasibility study phase.

This progress underscores the potential for long-term development and a strong start for the Ema project.

The EMA ionic REE project stands out as a unique and highly promising Mineral Resource in Brazil's rare earth element (REE) sector, offering several key highlights:

- **Analogous to China's iREE Deposits**: The project's similarity to the world-renowned ionic clay REE deposits in southwest China, formed over felsic volcanic rocks, sets it apart from other Brazilian REE projects.
- **World-Class Potential**: China's deposits are the largest known ionic clay REE sources, emphasizing the strategic importance and potential scale of the EMA project.
- **Extensive Land Area**: The project spans a vast **189 km^2** of felsic volcanic terrain.
- The **similarity to Chinese iREE deposits** strengthens the confidence in the project's potential for economically viable development.
- The **extensive area yet to be explored** (55%) indicates the possibility of significant resource expansion as additional drilling is undertaken.
- The project holds strategic importance for Brazil's REE sector, potentially positioning it as a major player in the global supply chain.

The EMA project's unique characteristics and ongoing exploration success underline its potential to contribute meaningfully to the global demand for rare earth elements.

This announcement has been authorised for release by the Board of Directors.

Enquiries

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Geology and Mineralisation

The rare earth element (REE) mineralisation is hosted within a tropical lateritic weathering profile developed atop felsic volcanic and volcaniclastic rocks, including rhyolites and ignimbrites. This weathering profile has facilitated the enrichment of REEs, making the deposit a valuable target for extraction.

The REE mineralisation occurs primarily in the weathered portions of the profile. In these zones, REEs originally contained in primary minerals such as monazite and xenotime are released through weathering processes. The dissolved REEs migrate downward through the regolith profile and are subsequently adsorbed onto newly forming fine aluminosilicate clay particles, including kaolinite, illite, and smectite.

The Ema deposit is characterised as an undulating ionic clay-hosted deposit, conforming to the rise and fall of the local topography. The mineralisation has been geologically interpreted as a singular, contiguous deposit spanning an area of approximately $82km^2$. This interpretation was developed through a systematic approach aimed at ensuring the MRE was both well-constrained and reflective of expected subsurface conditions.

Key steps in the process included the use of both factual and interpreted geological data to guide the development of the mineralisation model. Geological matrices were developed to aid in interpretation, facilitating the definition and construction of estimation domains. This approach ensured that the resource estimation was firmly rooted in the underlying geology, delivering a robust and representative MRE for the deposit.

The methodologies employed demonstrate a thorough understanding of the deposit's geologic characteristics, enhancing confidence in the accuracy and reliability of the MRE. All of the data used in the MRE has been gathered from hand auger drilling. This clay core is geologically logged and subsequently sub-sampled prior to analysis. The sampling intervals are domained by geological constraints (e.g. rock type, and alteration). All geology input is logged and validated by the relevant area geologists, incorporating an assessment of sample recovery. No defined relationship exists between sample recovery and grade.

Drilling

Drilling was conducted with hand-held augers, which offers the advantage of low-cost, rapid deployment and mobility. Drill results for the priority 1 area, previously announced[1], were the only results to be incorporated into this interim MRE update (Figure 3 &4). Once all outstanding assays are received from priority areas 1-3, an additional MRE update will be completed.

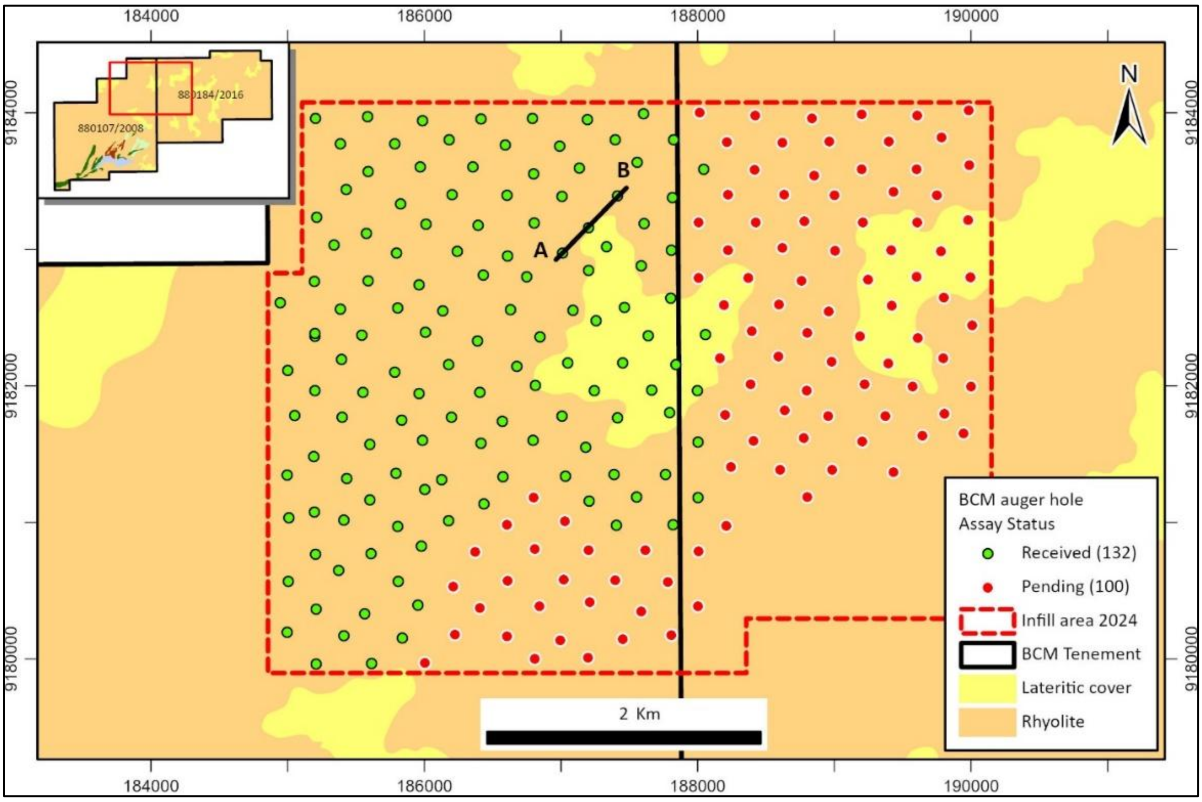

Figure 3 - Location map of the auger infill holes with assay results received from priority 1 area.

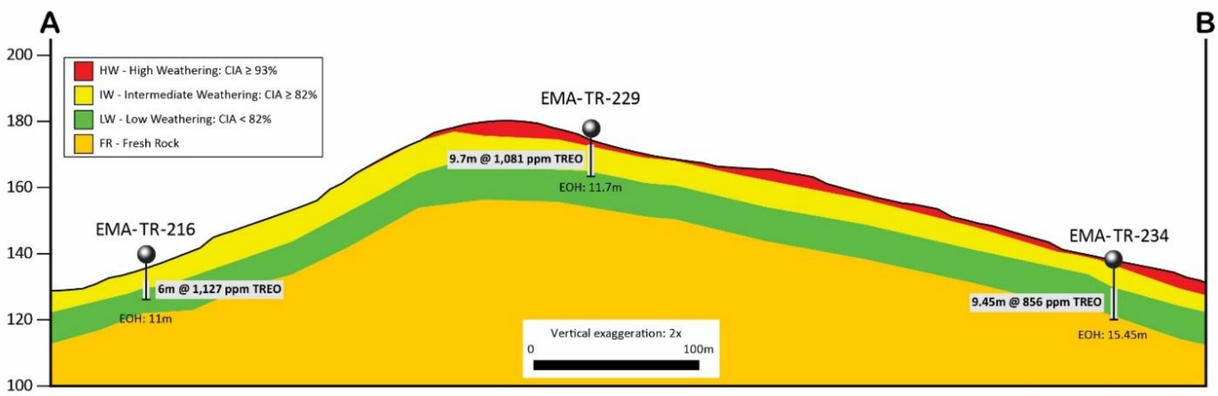

Figure 4 - Cross section from EMA-172 to 192

One key constraint of auger drilling is the depth limitation, with the deepest holes, drilled to ~20m depth, however this is sufficient to intercept the higher-grade lower zones of the mineralisation which lie directly above the basal fresh rock.

Topography is moderately undulating across most of the project area with holes within the starter zone (Priority 1-3) drilled on a nominal 300m grid spacing. Prior drilling programs were conducted at 800m spacing.

The entire enriched zone at Ema is generally contained within the 10 metres of regolith sitting directly above the saprock/fresh rock interface, which display a clear increase in grades with depth.

The leach test results from standard assays at SGS (magnesium sulphate and ammonium sulphate) confirm high recoveries of the four most important rare earth elements, neodymium, praseodymium, dysprosium and terbium, with some individual elements producing recoveries of up to 85% within the lower regolith portion of the profile.

The recovery data indicates a significant proportion of the REE's are present as ionically adsorbed clays, confirming that Ema, which currently stretches over 82km^2 has the potential to become one of the largest ionic clay hosted deposits defined outside of China.

Weathering Model – Chemical Index of Alteration (CIA)

The mineralised horizons were constrained by a weathering model constructed using the Chemical Index of Alteration (CIA; Nesbitt & Young, 1982), which showed high reliability, made possible by the availability of major oxide assays for each interval (Figure 5, 6 & 7).

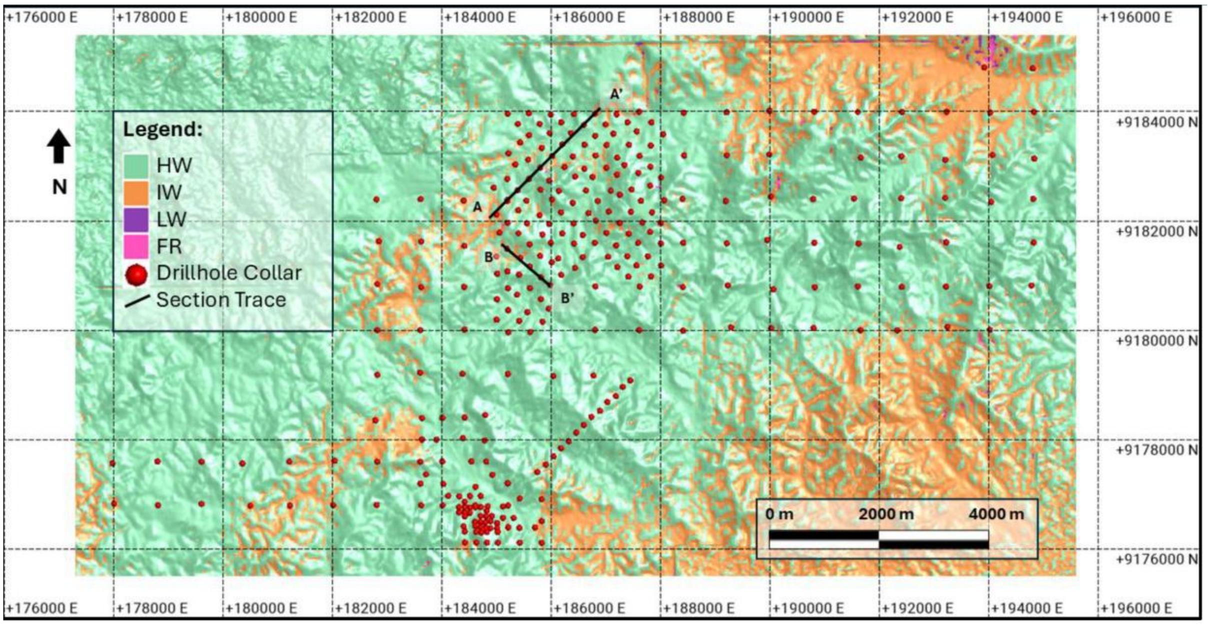

Figure 5. Weathering Model Plan View and Section Location (A-A[1], B-B[1]) over entire global resource area. HW = high weathering, IW = Intermediate weathering, LW = low weathering, FR = fresh rock.

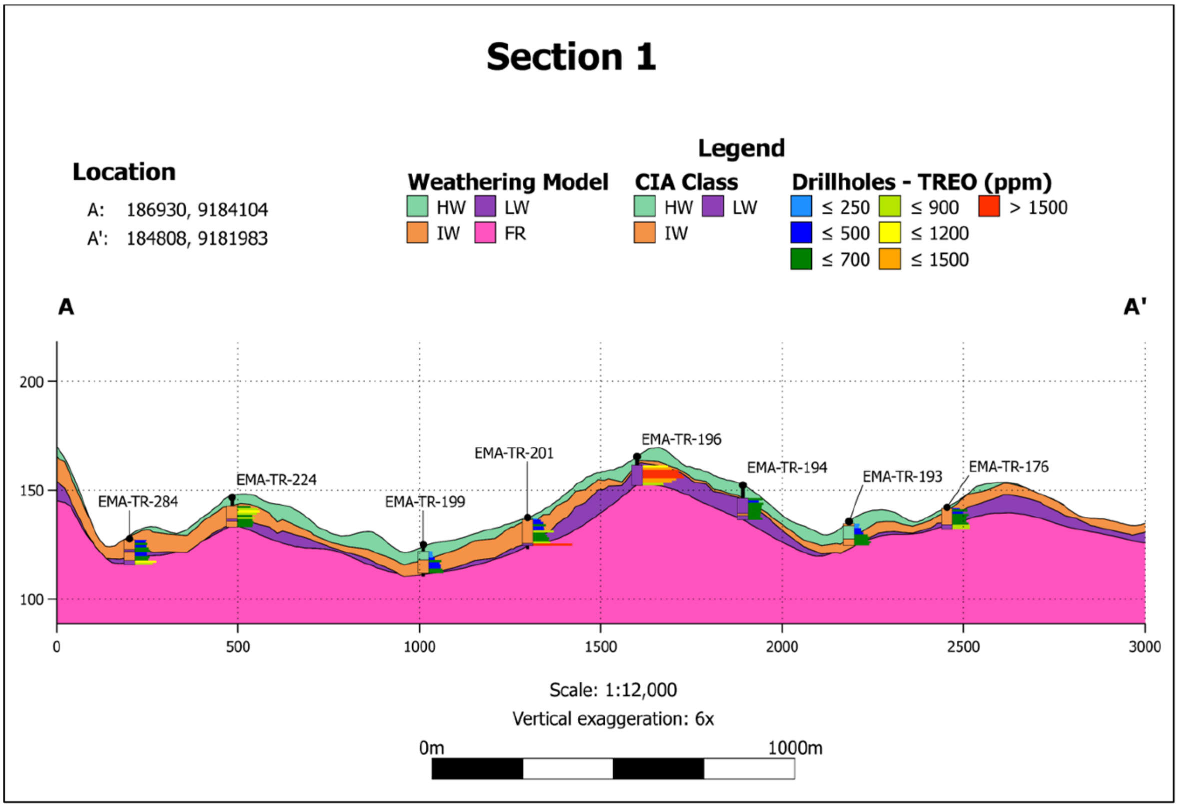

Figure 6. Weathering Model section A-A[1].

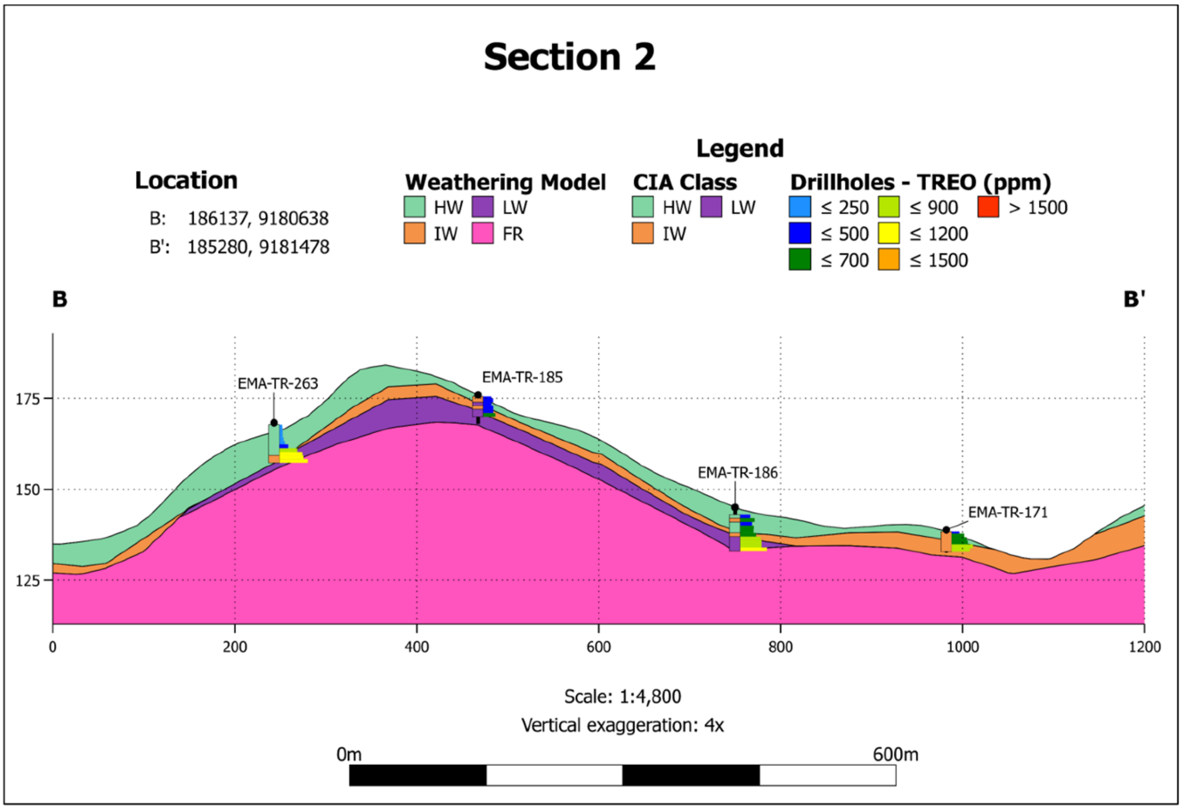

Figure 7. Weathering Model section B-B[1].

Sampling and Sub-sampling Techniques

Holes were sampled by BCM´s exploration team, with sampling being supervised by a GE21 geologist and field assistants. Every 1-metre sample was collected in a plastic bag in the field and transported to the exploration shed to be oven dried prior to homogenisation.

Samples were homogenised and subsequently riffle split with about 1 kg sent to SGS for analysis and a similar amount stored.

Additional sample preparation for the auger samples was conducted at SGS Vespasiano (greater Belo Horizonte) comprising oven drying, crushing of entire sample to 75% < 3mm followed by rotary splitting and pulverisation of 250 to 300 grams at 95% minus 150#.

The <3mm rejects and the 250-300 grams pulverised sample were returned to BCM for storage.

All samples generated have identification that is registered in internal spreadsheets. This identification is linked to the name of the hole and interval to which the sample belongs.

Sample Analysis Method

The assay technique used for REE analysis was Lithium Metaborate Fusion ICP-MS (SGS code ICP95A and IMS95A). This is a recognised industry standard analysis technique for REE suite and associated elements. Elements analysed at ppm levels included the following minerals and elements:

Ba	Ce	Co	Cs	Dy	Er	Eu	Ga
Gd	Hf	Ho	La	Lu	Nb	Nd	Pr
Rb	Sm	Sn	Sr	Ta	Tb	Th	Tm
U	V	W	Y	Yb	Zr	Zn	Co
Cu	Ni						

The sample preparation and assay techniques used are industry standard and provide total analysis.

The ICP95A reports the major elements oxides used to calculate the Chemical Index of Alteration (CIA) at % levels included:

Al2O3	CaO	Cr2O3	F2O3
K2O	MgO	MnO	Na2O
P2O5	SiO2	TiO2	

Estimation Methodology

Geological modelling classified weathering domains based on the Chemical Index of Alteration (CIA; Nesbitt & Young, 1982). GE21 used Leapfrog Geo and Edge software for 3D modelling, with domains based on weathering horizons defined as follows (figure **Error! Reference source not found.**):

- High Weathering: CIA ≥ 93%
- Intermediate Weathering: CIA ≥ 82%
- Low Weathering: CIA < 82%
- Fresh Rock: EOH of auger drilling

Most drillholes did not cross the complete weathering profile; with some holes stopping in the pedolith or saprolite domains due to the depth limitations of the auger semi-compact rocks. The top of fresh rock horizon was assumed at the end of each auger hole. Figure 9 shows a cross-section view of the geological model.

Quality assurance and quality control

One certified blank sample (ITAK-QG-01), 2 certified reference material (standard) sample (ITAK-713 and ITAK-714) and 3 field duplicate sample were inserted by BCM into each 50-sample sequence.

Standard laboratory QA/QC procedures were followed, including inclusion of standard, duplicate and blank samples.

The assay results of the standards fall within acceptable tolerance limits and no material bias is evident.

Data analysis

GE21 developed data analyses, including descriptive statistics for light and heavy REE's by domain, exploratory data analysis, and geostatistical analysis. They identified outliers as breaks in probability plot distribution curves for each element by domain (Table 4).

Bulk density

Average bulk density values for each weathering zone type were defined based on 57 sand replacement *in situ* density assays executed by the BCM technical team. Samples were collected in pits adjacent to auger holes at 2 metre depth intervals. Density values were correlated to a specific weathering zone type based on assay results (CIA) for average density definition. The bulk density applied in the block model was dry based.

Block model and Grade Estimation

The block model dimensions were based on average drill spacing, with sub-blocks used for adhesion between modelled solids and the selective mining unit.

The 3D block model was constructed for resource estimation purposes in Leapfrog EdgeTM software. The parent block dimensions were 100m x 100m x 4m, sub-blocked to 25m (X) x 25m (Y) x 2m (Z).

Variographic analysis was performed for grouped domains (HW, IW and LW) and elements (TREO), with experimental variograms constructed in different directions. No continuity differences were observed in different directions in the horizontal plane, therefore, horizontal/omnidirectional experimental variograms were chosen (Table 3 Table 3). The mineral resource was estimated using ordinary kriging (Table 4

Table 4.) and validated the grade estimate through visual analysis and global and local bias analysis using the nearest neighbour as the comparison estimate.

Table 3. Variogram Parameters for HW, IW and LW domains

Structure		Normalized Sill	Model	Range (Major)	Range (Semi Major)	Range (Minor)
Nugget		0.08	-	-	-	-
Structure 1		0.92	Spherical	200	200	10
Total sill		1	-	-	-	-

Table 4. Ordinary Kriging Strategy

Kriging Pass	Horizontal Range (m)	Vertical Range (m)	Max Samples per DH	Max Samples	Min Samples
P1	100	10	2	12	3
P2	200	20	2	12	3
P3	400	40	2	12	3
P4	>400	>40	2	12	1

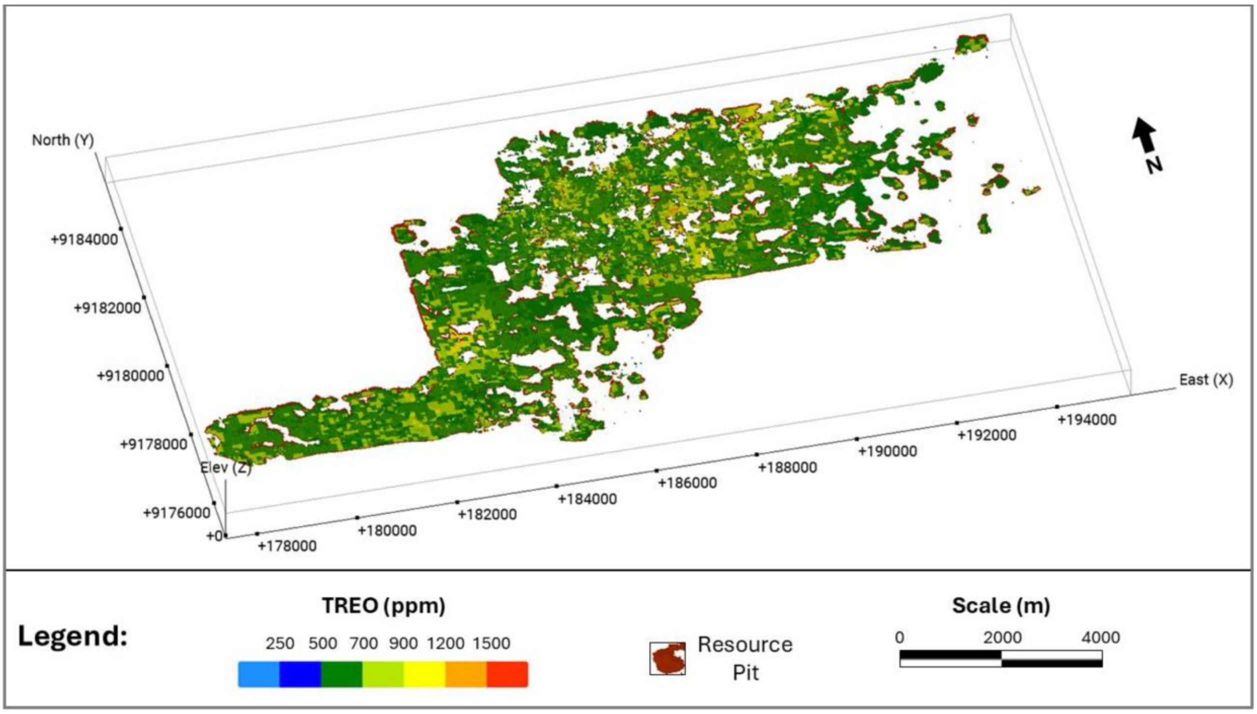

Figure 8. Mineral Resource blocks colour coded by grade.

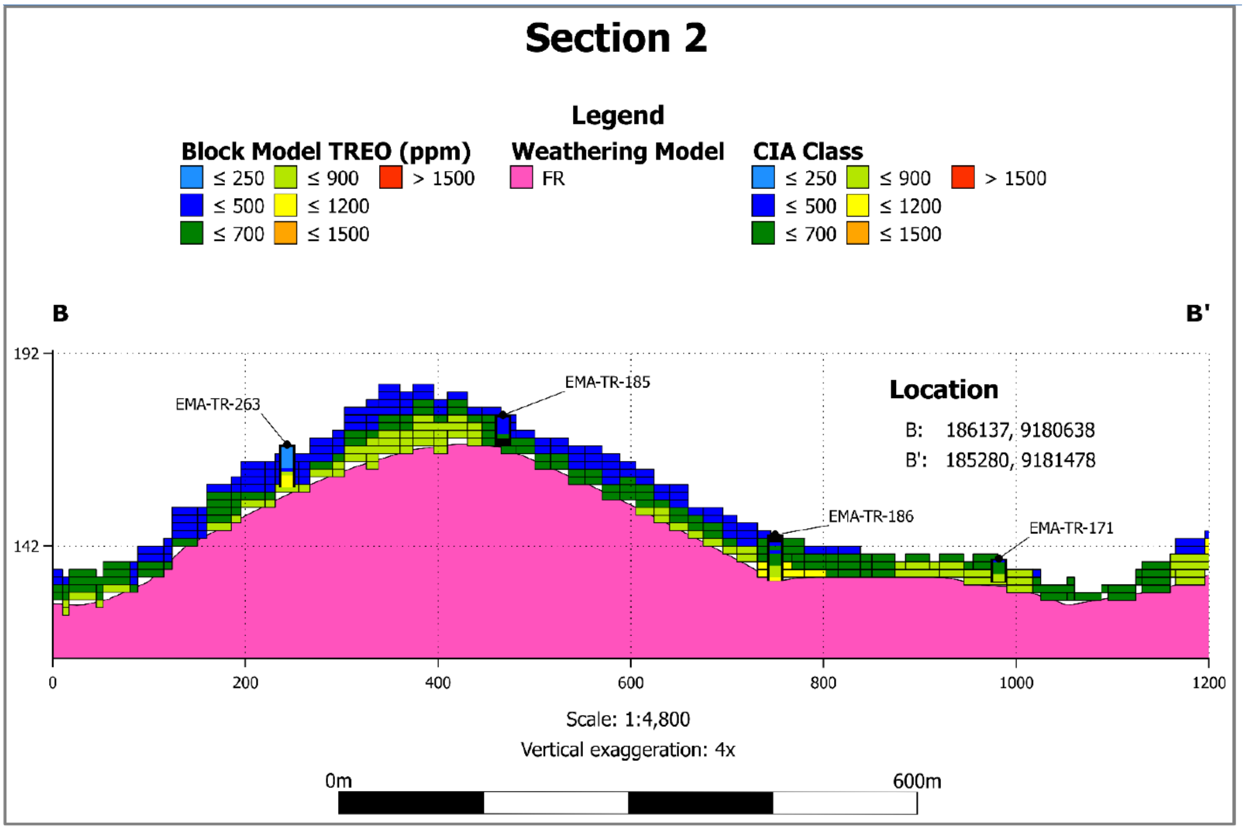

Figure 9. Block Model Grades and Drill Holes section B-B[1] (refer Figure. 5)

Cut-off grades, including basis for the selected Cut-off Grade

The selection of the TREO cut-off grade (500ppm) used for reporting was based on the experience of the Competent Person. Given the Mineral Resource and the absence of any development studies, this cut-off grade was selected based on a peer review of publicly available information from more advanced projects with comparable mineralisation styles (i.e. clay-hosted rare earth mineralisation) and comparable conceptual processing methods.

Mining and metallurgical methods / material modifying factors

No specific mining or metallurgical methods or parameters were incorporated into the modelling process.

Mineral Resource classification and reporting

The Mineral Resource Estimate for Ema Project has been classified as Inferred and Indicated.

The Competent Persons are satisfied that the classification is appropriate based on the current level of confidence in the data, drill hole spacing, geological continuity, variography, and bulk density data available for the project.

References

[1]Brazilian Critical Minerals (ASX:BCM) – Infill Drilling Confirms Ema Resource 8th October 2024

About Brazilian Critical Minerals Ltd

Brazilian Critical Minerals Limited (BCM) is a mineral exploration company listed on the Australian Securities Exchange.

Its major exploration focus is Brazil, in the Apuí region, where BCM has discovered a world class Ionic Adsorbed Clay (IAC) Rare Earth Elements deposit. The Ema IAC project is contained within the 781 km² of exploration tenements within the Colider Group.

BCM has defined an inferred MRE of 977mt of REE's with metallurgical recoveries averaging 68% MREO, representing some of the highest for these types of deposits anywhere in the world.

The Company is currently converting this MRE from Inferred into the Indicated category with an extensive drill program which will inform the scoping study and economic analysis due for completion Q1 2025.

Ema REE Global Mineral Resource Estimate @COG 500ppm TREO

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Total	**500**	**977**	**729**	**172**	**16**	**188**	**26**

Competent Persons Statement

The information in this announcement relates to previously reported exploration results for the Ema Project released by the Company to ASX on 22 May 2023, 17 July 2023, 19 July 2023, 31 July 2023, 13 Sep 2023, 19 Oct 2023, 06 Dec 2023, 06 Feb 2024, 22 Feb 2024, 13 Mar 2024, 02 Apr 2024, 08 Oct 2024 and 19 Nov 2024. The Company confirms that is not aware of any new information or data that materially affects the information included in the above-mentioned releases.

The information in this announcement that relates to the Ema/Ema East Mineral Resource is based on and fairly represents information compiled by Mr. Antonio de Castro (acts as BCM´s Senior Consulting Geologist through the consultancy firm, ADC Geologia Ltda) and Mr. Leonardo Rocha, (employee of GE21 Consultoria Mineral Ltda). Mr. de Castro is a member of the Australasian Institute of Mining and Metallurgy, and Mr. Rocha is a member of Australasian Institute of Geoscientists. Both have sufficient experience of relevance to the styles of mineralisation and types of deposits under consideration, and to activities undertaken to qualify as Competent Persons as defined in the 2012 Edition of the Joint Ore Reserve Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Specially, Mr. de Castro is the Competent Person for the database (including all drilling information), the geological and mineralisation model plus completed the site visits with Mr. Rocha. Mr. Rocha is the Competent Person for the construction of the 3D geology/mineralisation model plus the mineral resource estimation. Mr. de Castro and Mr. Rocha consent to the inclusion in this report of the matters on their information in the form and context in which they appear.

Appendix 1 – Full List of Drill Hole Collars

Hole ID	East	North	RL (m)	Depth (m)	Azimuth	Dip
EML-TR-001	193913.28	9184807.52	107.81	6	0	-90
EML-TR-002	194797.42	9184792.72	121.22	10	0	-90
EML-TR-007	188419.61	9183978.33	118.08	8	0	-90
EML-TR-008	189201.69	9183986.57	125.28	15	0	-90
EML-TR-009	189985.24	9184015.87	131.52	17	0	-90
EML-TR-010	190807.85	9183996.67	149.63	7	0	-90
EML-TR-011	191600.67	9183989.87	170.44	6	0	-90
EML-TR-012	192406.83	9183992.03	176.58	17	0	-90
EML-TR-013	193221.55	9183997.12	123.11	20	0	-90
EML-TR-014	194021.32	9183981.42	122.86	20	0	-90
EML-TR-015	194823.94	9183993.70	118.93	11	0	-90
EML-TR-021	188427.26	9183198.76	125.83	10	0	-90
EML-TR-022	189208.42	9183194.85	174.36	10	0	-90
EML-TR-023	189977.35	9183212.51	173.00	9	0	-90
EML-TR-025	191657.67	9183157.31	198.35	20	0	-90
EML-TR-026	192396.98	9183179.70	127.70	20	0	-90
EML-TR-027	193200.32	9183114.49	134.43	20	0	-90
EML-TR-028	194065.48	9183207.29	116.01	7	0	-90
EML-TR-029	194825.94	9183137.56	119.21	18	0	-90
EML-TR-035	188396.29	9182401.25	153.41	11	0	-90
EML-TR-036	189186.54	9182362.37	167.61	18	0	-90
EML-TR-037	190009.27	9182446.25	143.32	8	0	-90
EML-TR-038	190785.83	9182397.52	130.79	20	0	-90
EML-TR-039	191531.61	9182407.63	120.53	14	0	-90
EML-TR-040	192393.74	9182412.38	174.80	11	0	-90
EML-TR-041	193198.71	9182416.39	166.63	6	0	-90
EML-TR-042	194034.59	9182348.07	127.18	18	0	-90
EML-TR-043	194809.34	9182400.79	121.55	16	0	-90
EML-TR-049	188407.43	9181598.50	135.67	7	0	-90
EML-TR-050	189205.18	9181589.90	138.70	18	0	-90
EML-TR-051	189949.61	9181649.88	143.96	12	0	-90
EML-TR-052	190805.51	9181598.30	137.28	16	0	-90
EML-TR-053	191615.02	9181586.31	227.14	19	0	-90
EML-TR-054	192363.46	9181523.85	174.01	12	0	-90
EML-TR-055	193216.98	9181607.76	168.46	12	0	-90
EML-TR-057	194816.53	9181603.92	127.17	15	0	-90
EML-TR-063	188407.15	9179989.16	135.58	11	0	-90
EML-TR-064	188402.20	9180787.55	139.90	3	0	-90

EML-TR-065	189223.73	9180820.92	171.05	20	0	-90
EML-TR-066	190056.19	9180746.24	121.26	10	0	-90
EML-TR-067	190812.97	9180784.29	141.28	20	0	-90
EML-TR-068	191601.07	9180799.69	175.08	16	0	-90
EML-TR-069	192405.24	9180792.24	138.47	16	0	-90
EML-TR-070	193212.02	9180795.78	138.84	16	0	-90
EML-TR-071	194003.83	9180805.70	223.41	4	0	-90
EML-TR-072	194774.97	9180815.52	141.48	16	0	-90
EML-TR-078	189283.09	9180050.76	135.57	12	0	-90
EML-TR-079	190018.46	9180035.76	145.96	16	0	-90
EML-TR-080	190792.01	9180036.97	143.53	17	0	-90
EML-TR-081	191647.74	9179997.75	124.41	6	0	-90
EML-TR-082	192321.45	9179996.27	123.77	14	0	-90
EML-TR-083	193241.35	9180060.83	125.05	9	0	-90
EML-TR-084	194012.01	9180008.13	186.08	11	0	-90

Hole ID	East	North	RL (m)	Depth (m)	Azimuth	Dip
EMA-TR-008	185745.97	9177402.82	164.16	20	0	-90
EMA-TR-009	185900.31	9177539.18	138.84	17	0	-90
EMA-TR-010	186037.86	9177691.37	129.10	15	0	-90
EMA-TR-011	186177.80	9177843.90	127.59	11	0	-90
EMA-TR-012	186316.92	9177968.47	165.92	7	0	-90
EMA-TR-013	186455.87	9178124.06	183.17	20	0	-90
EMA-TR-014	186593.57	9178263.20	201.31	21	0	-90
EMA-TR-015	186731.54	9178409.15	208.53	18	0	-90
EMA-TR-016	186888.45	9178522.38	179.28	15	0	-90
EMA-TR-017	187024.11	9178683.36	162.09	10	0	-90
EMA-TR-018	187177.87	9178794.70	143.09	18	0	-90
EMA-TR-019	187304.82	9178963.33	129.03	15	0	-90
EMA-TR-020	187439.70	9179081.17	121.15	9	0	-90
EMA-TR-021	184606.82	9176795.11	125.91	12	0	-90
EMA-TR-022	184837.00	9176775.57	122.77	12	0	-90
EMA-TR-023	184807.29	9176594.69	135.83	22	0	-90
EMA-TR-024	184798.65	9176379.43	138.75	21	0	-90
EMA-TR-025	184607.03	9176415.04	140.97	16	0	-90
EMA-TR-026	184395.10	9176408.92	154.80	14	0	-90
EMA-TR-027	184416.63	9176594.06	134.41	13	0	-90
EMA-TR-028	184410.57	9176758.63	126.17	14	0	-90
EMA-TR-029	184611.99	9177128.56	122.94	13	0	-90
EMA-TR-030	185201.26	9177198.48	158.12	4	0	-90
EMA-TR-031	185207.70	9176793.11	118.44	10	0	-90
EMA-TR-032	185213.32	9176392.66	125.92	15	0	-90
EMA-TR-033	185700.35	9176391.55	117.40	6	0	-90
EMA-TR-034	184011.86	9176794.06	131.63	20	0	-90
EMA-TR-035	183618.85	9176796.19	146.88	16	0	-90
EMA-TR-036	183607.08	9177193.44	125.82	12	0	-90
EMA-TR-037	184024.62	9177185.30	122.13	11	0	-90
EMA-TR-038	184809.77	9177596.38	136.71	19	0	-90
EMA-TR-039	184536.82	9177599.38	122.83	10	0	-90
EMA-TR-040	184006.83	9177599.11	130.93	15	0	-90
EMA-TR-041	183604.80	9177591.88	162.69	25	0	-90

EMA-TR-042	183634.49	9177999.52	136.76	14	0	-90
EMA-TR-043	183897.03	9177996.60	124.06	12	0	-90
EMA-TR-044	184381.40	9178023.30	126.58	14	0	-90
EMA-TR-045	184781.11	9177982.03	144.90	6	0	-90
EMA-TR-046	184791.40	9178446.68	179.92	10	0	-90
EMA-TR-047	184414.54	9178404.01	147.48	18	0	-90
EMA-TR-048	184006.58	9178394.08	130.46	15	0	-90
EMA-TR-049	183635.42	9178391.84	124.06	13	0	-90
EMA-TR-050	182805.91	9176803.38	149.80	13	0	-90
EMA-TR-051	182010.93	9176799.63	134.05	12	0	-90
EMA-TR-052	181221.53	9176789.42	142.58	15	0	-90
EMA-TR-053	180498.89	9176788.37	189.59	28	0	-90
EMA-TR-054	179605.11	9176819.69	174.49	10	0	-90
EMA-TR-055	178809.10	9176796.66	180.81	16	0	-90
EMA-TR-056	178002.48	9176827.72	179.47	15	0	-90
EMA-TR-057	182814.92	9177594.65	178.46	29	0	-90
EMA-TR-058	182037.28	9177611.95	149.21	20	0	-90
EMA-TR-059	181206.20	9177596.59	188.79	17	0	-90
EMA-TR-060	180351.97	9177560.74	188.42	11	0	-90
EMA-TR-061	179606.07	9177593.92	204.52	22	0	-90
EMA-TR-062	178800.52	9177598.18	175.95	13	0	-90
EMA-TR-063	177978.86	9177561.12	195.28	16	0	-90
EMA-TR-064	182781.52	9178348.41	135.73	10	0	-90
EMA-TR-065	182818.96	9179184.21	138.99	13	0	-90
EMA-TR-066	182816.43	9180002.25	157.66	25	0	-90
EMA-TR-067	182816.35	9180841.20	177.04	18	0	-90
EMA-TR-068	182845.26	9181627.58	176.12	19	0	-90
EMA-TR-069	182803.35	9182392.88	207.62	18	0	-90
EMA-TR-070	183601.54	9179223.38	143.12	15	0	-90
EMA-TR-071	183603.20	9179999.76	156.55	18	0	-90
EMA-TR-072	183618.79	9180787.59	179.39	17	0	-90
EMA-TR-073	183617.52	9181622.86	194.53	13	0	-90
EMA-TR-074	183610.04	9182396.56	196.76	31	0	-90
EMA-TR-075	184375.09	9179205.37	151.14	23	0	-90
EMA-TR-076	184410.05	9180010.27	150.18	15	0	-90
EMA-TR-077	184403.59	9180791.36	151.64	16	0	-90
EMA-TR-078	184410.22	9181541.98	147.07	14	0	-90
EMA-TR-079	184396.54	9182369.71	144.39	16	0	-90
EMA-TR-080	185204.82	9179196.34	145.00	19	0	-90
EMA-TR-081	185194.31	9180014.35	151.15	17	0	-90
EMA-TR-082	185170.49	9180781.52	161.10	16	0	-90
EMA-TR-083	185183.26	9181589.55	150.35	15	0	-90
EMA-TR-084	185196.60	9182383.12	141.59	10	0	-90
EMA-TR-085	185214.65	9183237.23	138.35	8	0	-90
EMA-TR-086	185201.33	9183959.48	141.70	12	0	-90
EMA-TR-087	186036.27	9179160.96	159.45	8	0	-90
EMA-TR-088	186002.78	9179968.36	142.70	20	0	-90
EMA-TR-089	185978.85	9180825.30	168.31	14	0	-90
EMA-TR-090	185989.34	9181599.09	139.86	16	0	-90
EMA-TR-091	186008.85	9182396.40	187.56	21	0	-90
EMA-TR-092	186014.72	9183188.14	137.33	18	0	-90
EMA-TR-093	186006.12	9183984.73	138.16	19	0	-90

EMA-TR-094	186770.14	9179168.85	135.66	12	0	-90
EMA-TR-095	186797.54	9180003.66	137.68	12	0	-90
EMA-TR-096	186804.10	9180800.56	178.84	14	0	-90
EMA-TR-097	186793.74	9181599.40	132.54	12	0	-90
EMA-TR-098	186847.24	9182363.64	134.35	16	0	-90
EMA-TR-099	186806.09	9183194.89	121.36	11	0	-90
EMA-TR-100	186792.73	9183958.36	128.16	12	0	-90
EMA-TR-101	187605.18	9180000.22	146.56	20	0	-90
EMA-TR-102	187615.76	9180798.82	147.98	14	0	-90
EMA-TR-103	187582.69	9181598.22	155.54	19	0	-90
EMA-TR-104	187610.78	9183187.74	157.11	7	0	-90
EMA-TR-105	187604.04	9183996.58	121.71	9	0	-90
EMA-TR-106	184792.59	9176481.24	134.34	19	0	-90
EMA-TR-107	184884.20	9176502.65	126.44	13	0	-90
EMA-TR-108	184884.88	9176375.46	133.90	21	0	-90
EMA-TR-110	184818.03	9176304.31	153.06	20	0	-90
EMA-TR-111	184718.89	9176295.33	172.34	16	0	-90
EMA-TR-112	184624.18	9176304.05	152.76	14	0	-90
EMA-TR-113	184707.50	9176394.15	152.90	8	0	-90
EMA-TR-114	184704.73	9176495.62	147.89	10	0	-90
EMA-TR-115	184604.56	9176490.83	143.57	18	0	-90
EMA-TR-116	184413.89	9176862.22	124.73	14	0	-90
EMA-TR-117	184509.79	9176755.81	129.76	17	0	-90
EMA-TR-118	184312.15	9176764.14	122.54	8	0	-90
EMA-TR-119	184415.54	9176659.74	132.96	19	0	-90
EMA-TR-120	184312.37	9176662.55	134.54	14	0	-90
EMA-TR-121	184509.45	9176657.15	132.53	14	0	-90
EMA-TR-123	184703.67	9176599.17	133.03	9	0	-90
EMA-TR-124	184909.48	9176596.73	133.84	21	0	-90
EMA-TR-126	184815.63	9176695.51	127.55	15	0	-90
EMA-TR-127	184610.06	9176758.85	121.66	11	0	-90
EMA-TR-128	184710.97	9176762.40	124.35	13	0	-90
EMA-TR-129	185007.45	9176469.15	120.08	6	0	-90
EMA-TR-130	185007.49	9176378.01	127.11	6	0	-90
EMA-TR-131	185018.64	9176305.50	133.63	18	0	-90
EMA-TR-132	184113.63	9176968.73	123.37	10	0	-90
EMA-TR-133	184317.13	9176958.81	122.56	9	0	-90
EMA-TR-134	184513.21	9176963.66	127.72	17	0	-90
EMA-TR-135	184707.92	9176966.06	128.78	18	0	-90
EMA-TR-138	185423.13	9176918.24	131.56	17	0	-90
EMA-TR-140	185115.25	9176773.47	121.26	12	0	-90
EMA-TR-141	185310.94	9176563.76	118.16	8	0	-90
EMA-TR-142	185115.60	9176563.11	118.89	8	0	-90
EMA-TR-143	185413.88	9176383.93	124.63	14	0	-90
EMA-TR-144	185420.61	9176109.87	133.55	18	0	-90
EMA-TR-145	185022.35	9176108.71	164.71	24	0	-90
EMA-TR-146	184820.80	9176111.93	183.63	15	0	-90
EMA-TR-147	184629.75	9176111.66	168.25	7	0	-90
EMA-TR-148	184419.36	9176115.14	128.27	3	0	-90
EMA-TR-149	184415.02	9176313.58	141.52	12	0	-90
EMA-TR-150	185822.85	9176106.46	124.90	15	0	-90
EMA-TR-151	185822.73	9176508.07	117.17	10	0	-90

EMA-TR-152	185819.56	9176907.47	123.15	4	0	-90
EMA-TR-153	183706.55	9177360.69	121.97	8	0	-90
EMA-TR-156	184921.60	9177352.14	120.17	8	0	-90
EMA-TR-157	185614.94	9179966.06	152.53	15	0	-90
EMA-TR-158	185209.13	9180365.92	142.16	12	0	-90
EMA-TR-159	185409.75	9180168.54	140.42	19	0	-90
EMA-TR-160	185006.80	9180566.19	147.63	14	0	-90
EMA-TR-161	185838.72	9180152.62	135.11	5.25	0	-90
EMA-TR-162	185562.19	9180329.27	134.18	12.5	0	-90
EMA-TR-163	185372.01	9180649.99	142.32	15	0	-90
EMA-TR-164	185009.36	9181032.91	150.64	12	0	-90
EMA-TR-165	185204.58	9180766.47	155.31	15	0	-90
EMA-TR-166	185195.70	9181075.78	182.33	6.55	0	-90
EMA-TR-167	185410.68	9181016.95	186.24	14	0	-90
EMA-TR-168	185210.68	9179963.31	148.56	19.8	0	-90
EMA-TR-169	184997.34	9180193.56	148.74	19	0	-90
EMA-TR-170	185051.52	9181785.00	158.25	6	0	-90
EMA-TR-171	185432.52	9181322.03	150.42	6.35	0	-90
EMA-TR-172	185392.43	9182194.24	146.81	10	0	-90
EMA-TR-173	185542.26	9182369.43	139.76	12	0	-90
EMA-TR-174	184945.07	9182606.71	134.91	12	0	-90
EMA-TR-175	185963.20	9181940.96	132.30	10.75	0	-90
EMA-TR-176	185198.22	9182364.65	143.01	10	0	-90
EMA-TR-177	184994.63	9181345.74	143.02	13	0	-90
EMA-TR-178	185608.47	9180769.43	155.33	18	0	-90
EMA-TR-179	185808.22	9180567.72	163.53	14	0	-90
EMA-TR-180	185951.16	9180392.86	140.36	16	0	-90
EMA-TR-181	185199.69	9181965.99	185.84	6.5	0	-90
EMA-TR-182	185190.22	9181484.46	147.58	14	0	-90
EMA-TR-183	184998.61	9182114.38	149.21	9.2	0	-90
EMA-TR-184	185398.64	9181772.15	194.35	11.4	0	-90
EMA-TR-185	185806.26	9180968.08	191.70	8	0	-90
EMA-TR-186	185603.74	9181164.91	158.82	12	0	-90
EMA-TR-187	185600.80	9181571.24	185.27	7	0	-90
EMA-TR-188	185793.98	9181358.94	163.04	10	0	-90
EMA-TR-189	186005.74	9181240.66	155.52	17	0	-90
EMA-TR-190	186179.35	9181012.69	154.98	14.4	0	-90
EMA-TR-191	185195.78	9182766.67	137.06	14	0	-90
EMA-TR-192	185802.95	9182571.69	154.04	10	0	-90
EMA-TR-193	185384.47	9182560.47	137.25	11	0	-90
EMA-TR-194	185589.86	9182768.85	153.65	16	0	-90
EMA-TR-195	185339.92	9183030.53	132.63	11	0	-90
EMA-TR-196	185796.76	9182974.47	167.01	13.3	0	-90
EMA-TR-197	185386.78	9183772.91	146.68	11.5	0	-90
EMA-TR-198	185575.36	9183118.48	136.69	15.5	0	-90
EMA-TR-199	186203.19	9183401.46	126.25	14.7	0	-90
EMA-TR-200	185429.97	9183439.30	133.63	12.5	0	-90
EMA-TR-201	186012.16	9183185.88	137.70	14.5	0	-90
EMA-TR-202	185785.53	9183774.25	142.49	11.7	0	-90
EMA-TR-203	185970.22	9183603.57	132.72	9.9	0	-90
EMA-TR-204	185586.03	9183971.01	142.35	7	0	-90
EMA-TR-205	185988.09	9183943.80	136.82	8.45	0	-90

EMA-TR-206	185589.46	9183568.90	133.67	11.2	0	-90
EMA-TR-207	185783.83	9182100.90	147.23	5	0	-90
EMA-TR-208	185826.48	9183334.49	128.03	11.45	0	-90
EMA-TR-209	185550.81	9181954.61	175.66	6	0	-90
EMA-TR-210	185833.97	9181746.37	152.21	15.5	0	-90
EMA-TR-211	186199.77	9181771.07	139.70	15.2	0	-90
EMA-TR-212	186181.23	9183801.97	128.31	10	0	-90
EMA-TR-213	186357.67	9183601.22	123.42	8.75	0	-90
EMA-TR-214	186392.45	9183175.15	135.86	14.8	0	-90
EMA-TR-215	186607.77	9183393.17	126.79	10.75	0	-90
EMA-TR-216	187006.75	9182971.77	131.42	11	0	-90
EMA-TR-217	186603.47	9182953.66	131.33	12.85	0	-90
EMA-TR-218	187198.46	9182846.39	137.86	5.8	0	-90
EMA-TR-219	187826.64	9183801.97	120.00	8	0	-90
EMA-TR-220	187604.48	9183996.83	121.84	8	0	-90
EMA-TR-221	185988.34	9181599.91	140.16	14	0	-90
EMA-TR-222	186414.17	9181582.69	142.40	19.5	0	-90
EMA-TR-223	186413.68	9183956.01	141.61	10.35	0	-90
EMA-TR-224	186593.42	9183756.50	132.37	13.6	0	-90
EMA-TR-225	186800.25	9183551.78	123.10	11.3	0	-90
EMA-TR-226	187817.60	9183379.01	128.50	8	0	-90
EMA-TR-227	187560.24	9183634.74	123.53	14.4	0	-90
EMA-TR-228	187008.86	9183387.37	122.96	8	0	-90
EMA-TR-229	187202.72	9183156.83	169.19	11.7	0	-90
EMA-TR-230	187395.69	9183802.65	119.78	9	0	-90
EMA-TR-231	187190.94	9183949.80	128.14	13.5	0	-90
EMA-TR-232	186988.43	9183762.66	118.05	6.8	0	-90
EMA-TR-233	187133.49	9183593.77	121.36	10	0	-90
EMA-TR-234	187416.88	9183391.54	140.67	15.45	0	-90
EMA-TR-235	187810.30	9182991.47	136.84	18.2	0	-90
EMA-TR-236	187334.69	9183017.28	200.51	20	0	-90
EMA-TR-237	187587.37	9182876.64	180.46	19.4	0	-90
EMA-TR-238	187804.88	9182643.32	180.49	12.75	0	-90
EMA-TR-239	188058.10	9182374.56	218.61	22	0	-90
EMA-TR-240	186127.05	9181310.48	148.78	11.2	0	-90
EMA-TR-241	186573.77	9181335.29	153.09	12.65	0	-90
EMA-TR-242	186433.15	9181136.75	149.08	14	0	-90
EMA-TR-243	187406.58	9180979.57	150.35	14.4	0	-90
EMA-TR-244	187207.47	9181156.90	145.77	8	0	-90
EMA-TR-245	187035.66	9181340.24	148.97	14.6	0	-90
EMA-TR-246	186793.96	9181599.54	132.57	11.8	0	-90
EMA-TR-247	186573.82	9181740.14	128.70	7.85	0	-90
EMA-TR-248	186406.03	9181953.74	132.64	16	0	-90
EMA-TR-249	186175.62	9182155.17	141.02	17	0	-90
EMA-TR-250	187387.54	9181350.89	143.63	12.7	0	-90
EMA-TR-251	186753.82	9182801.45	123.37	9	0	-90
EMA-TR-252	187086.91	9182552.35	160.12	7.5	0	-90
EMA-TR-253	186009.10	9182395.43	187.07	16.45	0	-90
EMA-TR-254	187464.49	9182572.18	223.80	23.5	0	-90
EMA-TR-255	187252.18	9182479.59	190.33	6.7	0	-90
EMA-TR-256	187452.44	9182164.56	230.62	15.5	0	-90
EMA-TR-257	187662.88	9181970.39	217.42	11	0	-90

EMA-TR-258	187800.73	9181800.06	199.06	18	0	-90
EMA-TR-259	187839.27	9182153.73	230.79	16	0	-90
EMA-TR-260	187636.83	9182367.80	232.13	20.35	0	-90
EMA-TR-261	187999.37	9181966.53	185.13	8	0	-90
EMA-TR-262	188000.98	9181586.78	154.98	18	0	-90
EMA-TR-263	185979.86	9180824.97	168.19	11	0	-90
EMA-TR-264	188003.48	9181183.42	142.15	11	0	-90
EMA-TR-265	187583.84	9181598.22	155.12	14	0	-90
EMA-TR-266	187818.08	9180982.22	139.24	8.65	0	-90
EMA-TR-267	187554.87	9181187.75	137.31	7.85	0	-90
EMA-TR-268	187181.99	9181551.15	147.18	13.65	0	-90
EMA-TR-269	187006.30	9181777.72	147.51	11.3	0	-90
EMA-TR-270	186811.98	9182002.43	160.45	9.45	0	-90
EMA-TR-271	186678.67	9182141.08	137.95	19.55	0	-90
EMA-TR-272	186390.73	9182327.85	134.53	15	0	-90
EMA-TR-273	185962.41	9182738.36	191.08	17.7	0	-90
EMA-TR-274	187766.38	9181350.62	141.52	9	0	-90
EMA-TR-275	187415.11	9181765.93	139.68	5.3	0	-90
EMA-TR-276	187244.99	9181963.03	194.75	7.5	0	-90
EMA-TR-277	186632.50	9182556.92	130.04	14	0	-90
EMA-TR-278	187049.66	9182169.47	174.33	15	0	-90
EMA-TR-279	186431.81	9182810.50	142.84	16	0	-90
EMA-TR-280	186846.40	9182361.73	134.47	11.8	0	-90
EMA-TR-281	186805.98	9183193.35	121.36	8	0	-90
EMA-TR-282	187611.39	9183186.30	157.33	7	0	-90
EMA-TR-283	186239.26	9182983.73	145.21	6	0	-90
EMA-TR-284	186792.75	9183957.27	128.14	12	0	-90
EMA-TR-285	188042.33	9183584.81	122.44	11	0	-90
EMA-TR-286	188014.03	9183999.77	114.63	6	0	-90
EMA-TR-287	188212.88	9183784.54	123.77	13	0	-90
EMA-TR-288	188222.42	9183401.02	131.77	15.6	0	-90
EMA-TR-289	188427.36	9183197.39	125.94	8.5	0	-90
EMA-TR-290	186135.13	9182549.34	159.28	13.4	0	-90
EMA-TR-291	185198.16	9182382.92	141.58	7.45	0	-90
EMA-TR-292	185213.63	9183236.56	138.48	6.55	0	-90
EMA-TR-293	185200.86	9183960.47	141.63	10	0	-90
EMA-TR-294	187615.07	9180797.35	148.22	11	0	-90
EMA-TR-295	186003.25	9179969.55	142.42	20	0	-90
EMA-TR-296	188008.26	9183195.13	128.01	14.25	0	-90
EMA-TR-297	188420.76	9183978.65	118.29	7	0	-90
EMA-TR-298	188418.90	9183579.03	128.83	17	0	-90
EMA-TR-299	188372.04	9182788.99	193.76	12.35	0	-90
EMA-TR-300	188005.00	9182791.29	137.70	10.4	0	-90
EMA-TR-301	188384.66	9182011.55	139.95	14	0	-90
EMA-TR-302	188835.49	9183959.35	122.25	15.35	0	-90
EMA-TR-303	188853.18	9183539.21	127.71	12.5	0	-90
EMA-TR-304	188782.61	9183203.98	118.03	6.5	0	-90
EMA-TR-305	188761.26	9182770.47	124.91	12.3	0	-90
EMA-TR-306	188802.58	9182387.45	131.32	17	0	-90
EMA-TR-307	188798.35	9181966.41	131.22	8.2	0	-90
EMA-TR-308	188775.79	9181619.07	144.26	15.7	0	-90
EMA-TR-309	188395.39	9182400.97	153.80	10.2	0	-90

EMA-TR-310	188804.20	9181183.75	146.28	17.5	0	-90
EMA-TR-311	188220.99	9182992.55	132.98	8	0	-90
EMA-TR-312	188193.42	9182592.06	197.25	9	0	-90
EMA-TR-313	188202.16	9181785.61	145.63	9	0	-90
EMA-TR-314	188163.06	9182200.23	163.65	6.5	0	-90
EMA-TR-315	188245.44	9181404.26	138.67	9	0	-90
EMA-TR-316	188603.72	9181386.78	138.68	9	0	-90
EMA-TR-317	188638.16	9181819.78	136.67	14	0	-90
EMA-TR-318	188591.50	9182212.68	147.47	23	0	-90
EMA-TR-319	188596.69	9182595.46	143.42	17	0	-90
EMA-TR-320	188618.78	9183009.81	132.51	13	0	-90
EMA-TR-321	188618.91	9183779.50	119.22	8	0	-90
EMA-TR-322	188632.86	9183399.57	120.27	8	0	-90
EMA-TR-323	188962.54	9183787.60	123.27	5.5	0	-90
EMA-TR-324	189001.09	9183394.74	137.47	14.8	0	-90
EMA-TR-325	189006.08	9182990.41	131.57	8.5	0	-90
EMA-TR-326	188958.57	9182544.31	134.18	12	0	-90
EMA-TR-327	188981.07	9182176.95	137.95	13	0	-90
EMA-TR-328	188953.84	9181779.71	178.48	7	0	-90
EMA-TR-329	189201.67	9183989.07	125.29	17.5	0	-90
EMA-TR-330	189208.64	9183196.05	174.21	8.5	0	-90
EMA-TR-331	189205.25	9181590.33	138.63	18	0	-90
EMA-TR-332	189371.61	9181777.41	133.90	13	0	-90
EMA-TR-333	189398.55	9183788.43	123.66	9	0	-90
EMA-TR-334	189431.98	9183420.65	145.61	7.5	0	-90
EMA-TR-335	188407.86	9181598.39	135.72	8.5	0	-90
EMA-TR-336	188982.75	9181383.39	149.88	13.6	0	-90
EMA-TR-337	189198.81	9183584.35	132.90	14.65	0	-90
EMA-TR-338	189188.75	9182363.22	167.73	11.5	0	-90
EMA-TR-339	189245.17	9182776.78	167.64	11	0	-90
EMA-TR-340	189221.12	9182009.40	159.63	15.4	0	-90
EMA-TR-341	189434.34	9181366.80	132.12	10.4	0	-90
EMA-TR-342	189394.28	9182165.95	188.08	17	0	-90
EMA-TR-343	189418.81	9182588.03	221.34	18	0	-90
EMA-TR-344	189607.93	9183978.63	127.98	11	0	-90
EMA-TR-345	189601.53	9183585.03	139.97	12.7	0	-90
EMA-TR-346	189414.23	9182992.18	210.99	19	0	-90
EMA-TR-347	189607.00	9183196.44	183.81	16	0	-90
EMA-TR-348	189784.20	9183818.91	121.76	9	0	-90
EMA-TR-349	189748.75	9183394.42	146.60	7	0	-90
EMA-TR-350	189803.12	9181794.00	178.42	21	0	-90
EMA-TR-351	189797.58	9182201.13	151.64	10	0	-90
EMA-TR-352	190002.28	9181994.17	129.74	9.5	0	-90
EMA-TR-353	190009.95	9182445.25	143.18	6.5	0	-90
EMA-TR-354	189943.12	9181651.52	145.23	9	0	-90
EMA-TR-355	189984.36	9184018.89	132.36	17.3	0	-90
EMA-TR-356	189989.36	9183617.75	123.83	13	0	-90
EMA-TR-357	189802.48	9182644.86	183.31	25	0	-90
EMA-TR-358	189572.65	9181995.05	158.97	11	0	-9106
EMA-TR-359	189644.84	9181633.12	143.88	20	0	-90
EMA-TR-360	186372.00	9180782.00	200.00	11.8	0	-90
EMA-TR-361	189995.89	9182793.74	225.63	22.5	0	-90

EMA-TR-362	186809.00	9180804.00	222.00	7	0	-90
EMA-TR-363	189977.40	9183211.82	173.12	7	0	-90
EMA-TR-364	189603.21	9182800.67	230.36	20	0	-90
EMA-TR-365	189608.89	9182351.05	165.32	11	0	-90
EMA-TR-366	186608.00	9180573.00	170.00	8.45	0	-90
EMA-TR-367	189780.69	9182987.19	211.22	12.3	0	-90
EMA-TR-368	186405.00	9180374.00	170.00	14	0	-90
EMA-TR-369	186799.00	9181181.00	192.00	9	0	-90
EMA-TR-370	186606.00	9180984.00	200.00	11.7	0	-90
EMA-TR-371	186212.00	9180528.00	162.00	18	0	-90
EMA-TR-372	187028.00	9181007.00	171.00	11	0	-90
EMA-TR-373	186224.00	9180178.00	165.00	15	0	-90
EMA-TR-374	187203.00	9180796.00	168.00	18	0	-90
EMA-TR-375	187395.00	9180576.00	158.00	14	0	-90
EMA-TR-376	187020.00	9180580.00	201.00	11.8	0	-90
EMA-TR-377	186844.00	9180386.00	174.00	15.5	0	-90
EMA-TR-378	186607.00	9180167.00	170.00	17.5	0	-90
EMA-TR-380	187199.00	9180010.00	133.00	20	0	-90
EMA-TR-381	187450.00	9180146.00	172.00	16.7	0	-90
EMA-TR-382	187587.00	9180349.00	203.00	10.3	0	-90
EMA-TR-383	187781.00	9180562.00	179.00	12	0	-90
EMA-TR-384	187209.00	9180414.00	195.00	21	0	-90
EMA-TR-385	187599.00	9180005.00	168.00	18.5	0	-90
EMA-TR-386	188004.00	9180384.00	167.00	9	0	-90
EMA-TR-387	186995.00	9180137.00	154.00	11	0	-90
EMA-TR-388	186810.00	9180000.00	153.00	15	0	-90
EMA-TR-389	188005.00	9180786.00	158.00	10	0	-90
EMA-TR-390	187807.00	9180176.00	206.00	5.6	0	-90
EMA-TR-396	188211.00	9180974.00	173.00	11.4	0	-90

Appendix 2 - The following Table and Sections are provided to ensure compliance with JORC Code (2012 Edition).

JORC (2012) Table 1 – Section 1: Sampling Techniques and Data

Item	JORC code explanation	Comments
Sampling Techniques	• Nature and quality of sampling (eg cut channels. random chips. or specific specialised industry standard measurement tools appropriate to the minerals under investigation. such as down hole gamma sondes. or handheld XRF instruments. etc). These examples should not be taken as limiting the broad meaning of sampling. • Include reference to measures taken to ensure sample representativity and the appropriate calibration of any measurement tools or systems used. • Aspects of the determination of mineralisation that are Material to the Public Report. • In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required. such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	• Holes were sampled using a powered auger drill machine (open hole) conducted by BCM´s exploration team for 2023 auger drilling campaign. 2024 infill auger drilling campaign was conducted by BCM´s exploration team and supervised by GE21 technical team. • Sampling was executed and supervised by BCM technical team for 2023 drilling campaign. Sampling was executed by BCM technical team and supervised by GE21 technical team (one geologist and two mining technicians) for 2024 campaign. • Every 1-metre sample was collected in a raffia bag in the field and transported to the exploration shed to be dried in the sun prior to homogenisation for the 2023 campaign. Every 1-metre sample was collected in a plastic bag in the field and transported to the exploration shed to be oven-dried prior to homogenisation for the 2024 campaign. • Samples were homogenised and subsequently riffle split with about 1 kg sent to SGS for analysis and a similar amount stored. • 1 certified coarse blank sample, 2 certified reference material (standard) samples and 3 field duplicate samples were inserted into the sample sequence for each 50 samples.
Drilling Techniques	• Drill type (eg core. reverse circulation. open-hole hammer. rotary air blast. auger. Bangka. sonic. etc) and details (eg core diameter. triple or standard tube. depth of diamond tails. face-sampling bit or other type. whether core is oriented and if so. by what method. etc).	• Auger drilling was completed with a handheld-mechanical auger with a 3" auger bit. The drilling is an open hole meaning there is a significant chance of contamination from surface and other parts of the auger hole. Holes are vertical and not oriented or surveyed down dip. • The maximum depth achieved with the powered auger was 25m. Deep auger holes (> 15m) are only achievable if fragments of rocks/boulders etc. sitting within the weathered profile and/or the water table are not in the drillhole path. Auger drilling advances were measured using a measuring tape.
Drill Sample Recovery	• Method of recording and assessing core and chip sample recoveries and results assessed. • Measures taken to maximise sample recovery and ensure representative nature of the samples. • Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	• No recoveries are recorded. • The operator observes the volume of each metre and notes any discrepancy. • When recovery is below 75% in two sequential one metre interval, the field crew stops the drill hole. • No relationship is believed to exist between recovery and grade.
Logging	• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation. mining studies and metallurgical studies.	• All holes from 2023 drilling campaign were logged by BCM geologists. Holes from 2024 infill campaign were logged by GE21 geologist or field technicians. Logging for both campaigns detailed the colour, weathering, hydrothermal alteration, texture and any geological observations. Care was taken to identify transported cover from in-situ saprolite/clay zones and the moisture

<table>
<tr><th>Item</th><th>JORC code explanation</th><th>Comments</th></tr>
<tr><td></td><td>Whether logging is qualitative or quantitative in nature. Core (or costean. channel. etc) photography.
The total length and percentage of the relevant intersections logged.</td><td>content. Logging was done to a level that supports a Mineral Resource Estimate.
Qualitative logging with systematic photography of the stored box.
The entire auger hole is logged.</td></tr>
<tr><td>Sub-Sampling Techniques and Sampling Procedures</td><td>If core. whether cut or sawn and whether quarter. half or all core taken.
If non-core. whether riffled. tube sampled. rotary split. etc and whether sampled wet or dry.
For all sample types. the nature. quality and appropriateness of the sample preparation technique.
Quality control procedures adopted for all sub-sampling stages to maximise representativity of samples.
Measures taken to ensure that the sampling is representative of the in-situ material collected. including for instance results for field duplicate/second-half sampling.
Whether sample sizes are appropriate to the grain size of the material being sampled.</td><td>Auger sampling procedure is completed at the exploration shed in Apuí-AM.
The entire one metre sample is bagged on site in a raffia bag (2023 campaign) or plastic bag (2024 infill campaign) and transported to the exploration shed where it was naturally dried at the sun (2023 campaign) or oven dried (2024 infill campaign) prior to homogenisation and then quartered to about 1kg to go to SGS and another 1kg to store on site.
Sample preparation for the auger samples was conducted at SGS Vespasiano (near Belo Horizonte, MG, Brazil) comprising oven drying, crushing of entire sample to 75% < 3mm followed by rotary splitting and pulverisation of 250 to 300 grams at 95% minus 150#
The <3mm rejects and the 250-300 grams pulverised sample were returned to BCM for storage.</td></tr>
<tr><td>Quality of Assay Data and Laboratory Tests</td><td>The nature. quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.
For geophysical tools. spectrometers. handheld XRF instruments. etc. the parameters used in determining the analysis including instrument make and model. reading times. calibrations factors applied and their derivation. etc.
Nature of quality control procedures adopted (eg standards. blanks. duplicates. external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established</td><td>1 blank sample. 1 certified reference material (standard) sample and 1 field duplicate sample were inserted by BBX into each 25-sample sequence.
Standard laboratory QA/QC procedures were followed. including inclusion of standard. duplicate and blank samples.
The assay results of the standards fall within acceptable tolerance limits and no material bias is evident.
The assay technique used for REE was Lithium Metaborate Fusion ICP-MS determination (SGS code ICP95A and IMS95A). This is a recognised industry standard analysis technique for REE suite and associated elements. Elements analysed at ppm levels:
<table>
<tr><td>Ba</td><td>Ce</td><td>Cr</td><td>Cs</td><td>Dy</td><td>Er</td><td>Eu</td><td>Ga</td></tr>
<tr><td>Gd</td><td>Hf</td><td>Ho</td><td>La</td><td>Lu</td><td>Nb</td><td>Nd</td><td>Pr</td></tr>
<tr><td>Rb</td><td>Sm</td><td>Sn</td><td>Sr</td><td>Ta</td><td>Tb</td><td>Th</td><td>Tm</td></tr>
<tr><td>U</td><td>V</td><td>W</td><td>Y</td><td>Yb</td><td>Zr</td><td>Zn</td><td>Co</td></tr>
<tr><td>Cu</td><td>Ni</td><td></td><td></td><td></td><td></td><td></td><td></td></tr>
</table>
The sample preparation and assay techniques used are industry standard and provide total analysis.

The ICP95A reports the major elements oxides used to calculate the Chemical Index of Alteration (CIA) at % levels included:
<table>
<tr><td>Al2O3</td><td>CaO</td><td>Cr2O3</td><td>F2O3</td></tr>
<tr><td>K2O</td><td>MgO</td><td>MnO</td><td>Na2O</td></tr>
<tr><td>P2O5</td><td>SiO2</td><td>TiO2</td><td></td></tr>
</table></td></tr>
</table>

Item	JORC code explanation	Comments
		• The SGS laboratory used for the RRE assays is ISO 9001 and 14001 and 17025 accredited. • Analytical standard for REE ITAK-713 and 714 were used as CRM material in the batches sent to SGS. • The assay results for the standards were consistent with the certified levels of accuracy and precision and no bias is evident. • The certified blanks used (ITAK-QG-01) may contain traces of REE, with critical elements (Ce, Nd, Dy and Y) present in detectable quantities. • Duplicate samples were allocated separate sample numbers and submitted with the same analytical batch as the primary sample. Variability between duplicate results is considered acceptable and no sampling bias is evident. • Laboratory inserted standards. blanks and duplicates were analysed as per industry standard practice. There is no evidence of bias from these results.
Verification of Sampling and Assaying	• The verification of significant intersections by either independent or alternative company personnel. • The use of twinned holes. • Documentation of primary data. data entry procedures. data verification. data storage (physical and electronic) protocols. • Discuss any adjustment to assay data.	• Due to the style of mineralization, no significant intersections were individually assessed. • Apart from the routine QA/QC procedures by the Company and the laboratory there was no independent or alternative verification of sampling and assaying procedures for the 2023 drilling campaign. 2024 infill drilling campaign sampling and assaying were supervised by GE21 technical team. • 2023 and 2024 drilling campaigns auger drillholes were only assayed for the deepest 10 metres of each auger drillhole. • Analytical results for REE were supplied digitally directly from the SGS laboratory in Vespasiano to the BCM´s Exploration Manager in Rio de Janeiro. • 31 twin holes were executed at the infill area during the 2024 drilling campaign, supervised by GE21. • All twined auger drillholes were totally sampled and assayed. • Geological data was logged onto paper and transferred to Excel spreadsheets at end of the day and then transferred into the drill hole database for 2023 drilling campaign. Geological data was logged digitally on a tablet application and directly imported into the drill hole database for 2024 infill drilling campaign. Microsoft Access was used for database storage and management and incorporates numerous data validation and data integrity checks. All assay data is imported directly into the Microsoft Access database. • No adjustments were made to the data. • All REE assay data received from the laboratory in element form is unadjusted for data entry. • Conversion of elements analysis (REE) to stoichiometric oxide (REO) was undertaken by using defined conversion factors.

Item	JORC code explanation	Comments
		• (Source:https://www.jcu.edu.au/advanced-analytical-centre/resources/element-to-stoichiometric-oxide-conversion- factors).

Element ppm	Conversion Factor	Oxide Form
Ce	1.2284	CeO2
Dy	1.1477	Dy2O3
Er	1.1435	Er2O3
Eu	1.1579	Eu2O3
Gd	1.1526	Gd2O3
Ho	1.1455	Ho2O3
La	1.1728	La2O3
Lu	1.1371	Lu2O3
Nd	1.1664	Nd2O3
Pr	1.2082	Pr6O11
Sm	1.1596	Sm2O3
Tb	1.1762	Tb4O7
Tm	1.1421	Tm2O3
Y	1.2699	Y2O3
Yb	1.1387	Yb2O3

Rare earth oxide is the industry accepted form for reporting rare earths. The following calculations are used for compiling REO into their reporting and evaluation groups:

TREO (Total Rare Earth Oxide) = La2O3 + CeO2 + Pr6O11 + Nd2O3 + Sm2O3 + Eu2O3 + Gd2O3 + Tb4O7 + Dy2O3 + Ho2O3 + Er2O3 + Tm2O3 + Yb2O3 + Y2O3 + Lu2O3

LREO (Light Rare Earth Oxide) = La2O3 + CeO2 + Pr6O11 + Nd2O3

HREO (Heavy Rare Earth Oxide) = Sm2O3 + Eu2O3 + Gd2O3 + Tb4O7 + Dy2O3 + Ho2O3 + Er2O3 + Tm2O3 + Yb2O3 + Y2O3 + Lu2O3

CREO (Critical Rare Earth Oxide) = Nd2O3 + Eu2O3 + Tb4O7 + Dy2O3 + Y2O3

(From U.S. Department of Energy. Critical Material Strategy. December 2011)

MREO (Magnetic Rare Earth Oxide) = Nd2O3 + Pr6O11 + Tb4O7 + Dy2O3

NdPr = Nd2O3 + Pr6O11

DyTb = Dy2O3 + Tb4O7

In elemental from the classifications are:

TREE: La+Ce+Pr+Nd+Sm+Eu+Gd+Tb+Dy+Ho+Er+Tm+Tb+Lu+Y

HREE: Sm+Eu+Gd+Tb+Dy+Ho+Er+Tm+Tb+Lu+Y

CREE: Nd+Eu+Tb+Dy+Y

LREE: La+Ce+Pr+Nd

Item	JORC code explanation	Comments
Location of Data Points	• Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys). trenches. mine workings and other locations used in Mineral Resource estimation.	• Auger collar locations were surveyed initially by handheld GPS receiver, at an estimated accuracy of 10m. • Posterior to the end of the drilling campaign, the collar locations were picked up by a licensed surveyor using a

Item	JORC code explanation	Comments
	• Specification of the grid system used. • Quality and adequacy of topographic control.	Trimble total station (+/- 5cm), referenced to a government survey point. All drill holes have been checked spatially in 3D. • The grid system used for all data types in a UTM projection is SIRGAS Zone 21 Southern Hemisphere. No local grids were used. • The auger holes collar coordinates for the holes used in the resource estimation were surveyed to sub-decimetre accuracy by a licenced surveyor.
Data Spacing and Distribution	• Data spacing for reporting of Exploration Results. • Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. • Whether sample compositing has been applied.	• Auger holes were 300 metres apart inside the infill area (2024 drilling campaign) and over 200m to 800m apart (2023 drilling campaign) designed for testing ionic clay REE mineralization in the regolith over the mapped Proterozoic volcanic rocks (rhyolites and ignimbrites). • The data spacing and distribution is sufficient to establish the level of REE elements present in the target area and its continuity along the regolith profile. Data spacing and distribution are appropriate for a Mineral Resource estimation. • Sample composition was applied within the modelled weathering horizons.
Orientation of Data in relation to Geological Structure	• Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known. considering the deposit type. • If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias. this should be assessed and reported if material.	• The location, orientation, and depth of the sampling is appropriate for the deposit type. • Relevant REE values are compatible with the exploration model for ionic REEs. • No relationship between mineralisation and drilling orientation is known at this stage.
Sample security	• The measures taken to ensure sample security.	• The auger samples in sealed plastic bags were sent directly to SGS by bus and then airfreight. The Company has no reason to believe that sample security poses a material risk to the Commentary integrity of the assay data.
Audit or Reviews	• The results of any audits or reviews of sampling techniques and data.	• The sampling techniques and data have been reviewed by the Competent Person and are found to be of industry standard.

JORC (2012) Table 1 - Section 2: Reporting of Exploration Results

Criteria	JORC code explanation	Commentary
Mineral Tenement and Land Tenure Status	• Type. reference name/number. location and ownership including agreements or material issues with third parties such as joint ventures. partnerships. overriding royalties. native title interests. historical sites. wilderness or national park and environmental settings. • The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	• The EMA and EMA EAST leases are 100% owned by BCM with no issues in respect to native title interests. historical sites. wilderness or national park and environmental settings. • The company is not aware of any impediment to obtain a licence to operate in the area.
Exploration done by Other Parties	• Acknowledgment and appraisal of exploration by other parties.	• No exploration by other parties has been conducted in the region.
Geology	• Deposit type. geological setting and style of mineralisation.	• The REE mineralisation at EMA is contained within the tropical lateritic weathering profile developed on top of felsic rocks. rhyolites as per the Chinese deposits. • The REE mineralisation is concentrated in the weathered profile where it has dissolved from the primary mineral, such as monazite and xenotime, then migrates downwards where REE are adsorbed on to the neo-forming fine particles of aluminosilicate clays (e.g. kaolinite, illite, smectite) forming what is known as Ionic Clay Deposits. • This adsorbed iREE is the target for extraction and production of REO.

Drill Hole Information	• A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:
	  ◦ easting and northing of the drill hole collar
	  ◦ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar
	  ◦ dip and azimuth of the hole
	  ◦ down hole length and interception depth
	  ◦ hole length.
	• If the exclusion of this information is justified on the basis that the information is not material and this exclusion does not detract from the understanding of the report. the Competent Person should clearly explain why this is the case.
		• Drill results and hole locations relating to the current mineral resource estimate have been released by BCM on 22 May 2023, 17 July 2023, 19 July 2023, 31 July 2023, 13 Sep 2023, 19 Oct 2023, 06 Dec 2023, 06 Feb 2024, 22 Feb 2024, 13 Mar 2024, 02 Apr 2024, 08 Oct 2024 and 19 Nov 2024.
		• All Drill-holes are vertical and did not have a down-hole survey down hole length and interception dept due the total length of less than 50m hole length.
		• Full drill hole collars for all holes (see appendix 1)

Data aggregation methods	• In reporting Exploration Results. weighting averaging techniques. maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated. • Where aggregate intercepts incorporate short lengths of high-grade results and longer	• Weighted averages were calculated for all material intercepts aggregation and disclosed as reported in the releases by BCM on 22 May 2023, 17 July 2023, 19 July 2023, 31 July 2023, 13 Sep 2023, 19 Oct 2023, 06 Dec 2023, 06 Feb 2024, 22 Feb 2024, 13 Mar 2024, 02 Apr 2024, 08 Oct 2024 and 19 Nov 2024.

Criteria	JORC code explanation	Commentary
	lengths of low-grade results. the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. • The assumptions used for any reporting of metal equivalent values should be clearly stated.	• 500ppm TREO cut-off grade was applied to define the relevant • The assumptions used for any reporting of metal equivalent values intersections. • No metal equivalent values reported.
Relationship between mineralization widths and intercepted lengths	• These relationships are particularly important in the reporting of Exploration Results. • If the geometry of the mineralisation with respect to the drill hole angle is known. its nature should be reported. • If it is not known and only the down hole lengths are reported. there should be a clear statement to this effect (eg 'down hole length. true width not known').	• Significant values of REE were reported for the auger samples. • Mineralisation orientation is not known at this stage. although assumed to be flat. • The downhole depths are reported. true widths are not known at this stage.
Diagrams	• Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include. but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	• Maps and tables of the auger holes location and target location are inserted. • Drillhole locations and diagrams are presented in this announcement and were also detailed in the relevant previous ASX announcements reported.
Balanced reporting	• Where comprehensive reporting of all Exploration Results is not practicable. representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	• Relevant REE mineralisation with grades higher than 500ppm TREO in auger holes was reported with confirmation of IAC (Ionic Adsorbed Clay) type mineralisation obtained in almost all the auger holes.
Other substantive exploration data	• Other exploration data. if meaningful and material. should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density. groundwater. geotechnical and rock characteristics; potential deleterious or contaminating substances.	• No other significant exploration data has been acquired by the Company.
Further Work	• The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). • Diagrams clearly highlighting the areas of possible extensions. including the main geological interpretations and future drilling areas. provided this information is not commercially sensitive.	• Resume the current infill drilling across the 1000-hectare area, focusing on TREO high -grade zones. Incorporate deeper drilling to target these high-grade zones in the Mineral Resource Estimate (MRE). • Maintain the execution of twin drillholes of 2023 campaign drillholes inside the infill area. • Further metallurgical leaching tests.

JORC (2012) Table 1 – Section 3: Estimation and Reporting of Mineral Resources

Criteria	JORC code explanation	Commentary
Database integrity	• Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. • Data validation procedures used.	• The Ema drilling database was received in CSV format, and GE21 inputted the Database into Leapfrog Geo and Edge. • GE21 carried out an electronic validation of the databases with Leapfrog Geo software. No errors, such as gaps or overlapping data, or other material inconsistencies were found.
Site visits	• Comment on any site visits undertaken by the Competent Person and the outcome of those visits. • If no site visits have been undertaken indicate why this is the case.	• A site visit was undertaken by Mr Leonardo Rocha to the Ema/Ema East Project between July 11th to 15th 2024. • Competent Person, Mr de Castro has planned, managed and/or conducted work programmes, including the drilling, for the Ema/Ema East Project. He has visited site on numerous occasions.
Geological interpretation	• Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. • Nature of the data used and of any assumptions made. • The effect, if any, of alternative interpretations on Mineral Resource estimation. • The use of geology in guiding and controlling Mineral Resource estimation. • The factors affecting continuity both of grade and geology.	• Confidence on the geological interpretation of the rare earth mineralization in saprolite rocks is very high as exploration activities were made using a regular drill spacing and conducted the assays in additional of the REE of the major oxides (ICP95A) required to define the Chemical Index of Alteration (CIA). • Supergene alteration (weathering) zones were set up using Leapfrog™ Geo software implicit method based on a geological code on the database, applying the CIA as a reference index. • GE21 interpreted the following weathering zones (which are correlated to ore grade zones): HW (High Weathering) with CIA • >93, IW (Intermediate Weathering) with CIA >82, LW (Low weathering) with CIA<82 and FR (Fresh Rock) at the EOH (End of Hole). • For the REE mineralisation hosted by clays, which is difficult to visually identify in the drilling, the CIA is critical. • Alternative interpretations are unlikely to have a material impact on the global resource volumes. • All wireframes from geological model were cut by the topographic surface.
Dimensions	• The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.	• The mineralisation has been restrained in depth considering the EOH of the auger drilling as reference.
Estimation and modelling techniques	• The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used. • The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.	• Weathering zones modelling was conducted using Leapfrog™ Geo software's implicit methods. The weathering zones were defined based on the drilling information. Where no drilling information is available the topographic morphology was used as a reference for the wireframe construction. • A 3D block model was constructed for resource estimation purposes. The block dimensions were defined as 100m x 100m x 4m and minimum sub-block dimensions were defined as 25 x 25 x 2m to assure a good adherence between the geological model and block model. The average sample spacing is 300 metres apart for the infill area and 200 to 800 metres apart for the rest.

Criteria	JORC code explanation	Commentary
	• The assumptions made regarding recovery of by-products. • Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation). • In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed. • Any assumptions behind modelling of selective mining units. • Any assumptions about correlation between variables. • Description of how the geological interpretation was used to control the resource estimates. • Discussion of basis for using or not using grade cutting or capping. • The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.	• Rare Earth Element grades were estimated individually using Ordinary Kriging in the Block Model parent cells. Leapfrog Edge™ software was used for this process. • The visual and volumetric comparison between the geological wireframes and the block model shows a good fit for modelled units, with volumetric ratio (wireframe volume/block model volume) values inside the acceptable variation limit (98% to 103%). • No top-cuts (capping) or cut-offs were applied based on the results of an exploratory data analysis (EDA). • Search ellipse ranges were based on the results of the variography along with consideration of the drillhole spacing, with the same search neighbourhood parameters used for all elements to maintain the metal balance and correlations between elements. A three-pass search strategy was used (i.e. if initial search criteria are not met, an expanded search ellipse is used). A minimum of 3 and maximum of 12 samples, considering a maximum of 2 samples by drillhole, was applied on the neighbour search strategy for ordinary kriging interpolation. • Grade estimates were validated against nearest neighbouring composites. The nearest neighbour was applied as the comparative value for the kriging estimates using NN-Check statistical analysis and Swath Plots along three coordinate axes. Global biases and local biases were checked, and values were considered inside acceptance limits. • A combined TREO grade was calculated using the estimated individual grades. • There is no operating mine, and no production data is currently available.
Moisture	• Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.	• All tonnages have been estimated as dry tonnages.
Cut-off parameters	• The basis of the adopted cut-off grade(s) or quality parameters applied	• A set of cut-offs were applied on sample assay results and considered on the mineralisation zone modelling interpretation. Internal waste grades were locally included in mineralised intercepts. • The Mineral Resource has been reported with cut-off grade of 500ppm TREO application directly over the block model. A pit optimisation with assumptions based on REO prices, metallurgical recoveries and operating costs was applied as the limit of mineral resource classification.
Mining factors or assumptions	• Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should	• A conceptual mining study has been completed to support the open cut for the Ema. • Mining of the open cut deposit is assumed to use conventional equipment without the need of blasting. • The table below presents the mining factors applied on the definition of the RPEEE. <table><tr><td>Selling Price</td><td>US$/kg</td><td>By element</td></tr><tr><td>Discount Rate</td><td>%</td><td>8</td></tr></table>

<table>
<tr><th>Criteria</th><th>JORC code explanation</th><th>Commentary</th></tr>
<tr><td></td><td>be reported with an explanation of the basis of the mining assumptions made.</td><td>
<table>
<tr><td>Mining Recovery</td><td>%</td><td>100%</td></tr>
<tr><td>Mining Dilution</td><td>%</td><td>0</td></tr>
<tr><td>Metallurgical Efficiency</td><td>%</td><td>By element</td></tr>
<tr><td>Concentrate Purity</td><td>%</td><td>92.7</td></tr>
<tr><td>Overall Wall Slope Angle</td><td>deg</td><td>25</td></tr>
<tr><td>Mining Cost</td><td>US$/t mined</td><td>2.13</td></tr>
<tr><td>Processing Cost</td><td>US$/t processed</td><td>7.23</td></tr>
<tr><td>Royalties</td><td>% of revenue</td><td>2.00</td></tr>
<tr><td>Selling Cost</td><td>US$/t REO</td><td>7.03</td></tr>
</table>
<table>
<tr><th>REE</th><th>%</th><th>US$/kg REO</th></tr>
<tr><td>Y</td><td>97.0</td><td>2.66</td></tr>
<tr><td>La</td><td>97.6</td><td>0.68</td></tr>
<tr><td>Ce</td><td>86.5</td><td>0.69</td></tr>
<tr><td>Pr</td><td>96.7</td><td>144.18</td></tr>
<tr><td>Nd</td><td>91.7</td><td>150.75</td></tr>
<tr><td>Sm</td><td>91.2</td><td>2.39</td></tr>
<tr><td>Eu</td><td>90.1</td><td>27.45</td></tr>
<tr><td>Gd</td><td>89.8</td><td>71.55</td></tr>
<tr><td>Tb</td><td>90.1</td><td>1789.25</td></tr>
<tr><td>Dy</td><td>92.2</td><td>477.25</td></tr>
<tr><td>Ho</td><td>92.2</td><td>137.25</td></tr>
<tr><td>Er</td><td>89.1</td><td>59.10</td></tr>
<tr><td>Tm</td><td>88.7</td><td>0.00</td></tr>
<tr><td>Yb</td><td>87.8</td><td>19.85</td></tr>
<tr><td>Lu</td><td>88.3</td><td>834.75</td></tr>
</table>
</td></tr>
<tr><td>Metallurgical factors or assumptions</td><td>• The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</td><td>• Metallurgical test work is ongoing. Assumptions related to the metallurgical recoveries for the Mineral Resource grades were based on Aclara’s Technical Report NI 43-101, 2023, and this value was applied for the pit optimisation study for Mineral Resource classification.</td></tr>
<tr><td>Environmental factors or assumptions</td><td>• Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a</td><td>• It is assumed that mine waste and tailings can be stored on site, however no environmental or mining studies have been conducted at this stage.
• The Company will be required to obtain the necessary environmental permits and comply with environmental laws. GE21 does not have information about any factors that could affect the acquisition of environmental licences.</td></tr>
</table>

Criteria	JORC code explanation	Commentary
	greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	
Bulk density	• Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples. • The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vughs, porosity, etc), moisture and differences between rock and alteration zones within the deposit. • Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.	• Average bulk density values for each weathering zone type were defined based on 57 sand replacement in situ density assays executed by BCM technical team. Samples were collected in survey pits along auger holes, usually spaced 2 metres in depth. Density values were correlated to a specific weathering zone type based on assay results (CIA) for average density definition. • The bulk density applied in the block model was dry based.
Classification	• The basis for the classification of the Mineral Resources into varying confidence categories. • Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data). • Whether the result appropriately reflects the Competent Person's view of the deposit.	• Basis for the mineral classification was the QAQC results, style and geometry of mineralisation, sampling grid size and density of information and mining process optimisation for mineral resources. • The Mineral Resource has been classified as an Indicated and Inferred Resource based on the anisotropic average distance to samples on ordinary kriging estimation and it has been limited in depth to represent depths assessed by auger drilling. • The Mineral Resource classification appropriately reflects the view of the Competent Person, who recommends a further infill drillhole campaign to increase the confidence level of the geological model and grade estimate. The Mineral Resource Grade Tonnage table is included in the body of this announcement.
Audits or reviews	• The results of any audits or reviews of Mineral Resource estimates.	• The current model has not been audited by an independent third party but has been subject to GE21 and BCM's internal peer review processes.
Discussion of relative accuracy/ confidence	• Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate. • The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic	• The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the 2012 JORC Code. • The statement relates to global estimates of tonnes and grade. • The Mineral Resource has been validated both globally and locally against the input composite data using nearest neighbour estimate. The Indicate and Inferred Resource estimate are considered globally accurate. Closer spaced drilling is required to improve the confidence of the short-range grade continuity. • No production data is available for comparison with the Mineral Resource estimate at this stage.

BRAZILIAN CRITICAL MINERALS

Criteria	JORC code explanation	Commentary
	evaluation. Documentation should include assumptions made and the procedures used. • These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	