VICTORY METALS

UPDATED MRE IDENTIFIES HREO/TREO RATIOS UP TO 83%

Victory Metals Ltd (**ASX:VTM, Victory** or the **Company**) is pleased to announce a significant upgrade to the Mineral Resource Estimate (**MRE**) at its flagship North Stanmore Heavy Rare Earth Element Project in Western Australia. The upgraded MRE will be used for the 2025 Prefeasibility study planned for release later in 2025.

The MRE incorporates results from a targeted 79 drillhole 3,221m, air-core drilling campaign, delivering a 29.5% increase in contained tonnage. With leading ratios of heavy rare earth elements, including Dysprosium (**Dy**) and Terbium (**Tb**), compared with other Australian clay hosted project at this scale, Victory continues to emerge as the Australian answer as a low-cost heavy rare earth element producer.

HIGHLIGHTS

- **Ultra-high Heavy Rare Earth Ratios zones identified from across the North Stanmore Mineral Resource area including:**
    - **83% HREO/TREO @ 1,726ppm (Hole IF159)**
    - **81% HREO/TREO @ 3,584ppm (Hole IF155)**
    - **80% HREO/TREO @ 10,179ppm (Hole NSE028)**
    - **76% HREO/TREO @ 2,890ppm (Hole DD002)**
    - **75% HREO/TREO @ 4,423ppm (Hole NSTAC180)**
- **29.5% increase to the North Stanmore MRE to 320.6 million metric tonnes @ 510 ppm Total Rare Earth Oxide & high HREO/TREO of 39% (TREOSc_2O_3) (Inferred and Indicated)**
- **A high-grade shallow zone of 50 million metric tonnes has been identified @1,050ppm TREOSc_2O_3 (Inferred and Indicated)**
- **Mineralisation remaining open with the opportunity to target the Ultra-High Heavy Rare Earth Ratio zones through satellite pits**
- **Victory's latest drilling program has proven a low-cost significant resource increase equating to $3,500 all in exploration costs per 1 million tonnes of resource added (inferred & indicated)**
- **The Updated MRE will assist ongoing funding discussions for the development of North Stanmore and will underpin the Prefeasibility Study (PFS)**

Victory's CEO and Executive Director Brendan Clark commented: *"This resource upgrade reinforces the immense scale and strategic importance of North Stanmore. To deliver a 29.5% increase from a small, low-cost 3,221m air core program, speaks volumes about this deposit."*

"Mineralisation remains open in multiple directions, with consistently thick and high-grade intercepts continuing to be identified. While we see strong potential for further resource growth, the Company's

priority is progressing development, as there is already sufficient material to support a mine life exceeding 30 years."

"The drill program was intentionally limited out of deep respect for the Traditional Owners, following the unfortunate passing of a respected Wajarri Yamaji Elder. In line with our heritage protocols, we paused drilling as the presence of a heritage monitor is required when clearing new drill lines. We extend our sincere condolences to the Wajarri Yamaji People and thank them for their ongoing guidance and support."

Updated August MRE Information

The August 2025 MRE has been estimated by MEC Mining Group Pty Ltd (**MEC**) within the boundaries of twelve tenements; E20/0544, E20/0871, E20/971, E20/1016, E20/2468, E20/2469, P20/0543, P20/2007, P20/2153, P20/2331, P20/2352, and P20/2403, with all tenure held by Victory Cue Pty Ltd, a wholly owned subsidiary of Victory (Figure 1).

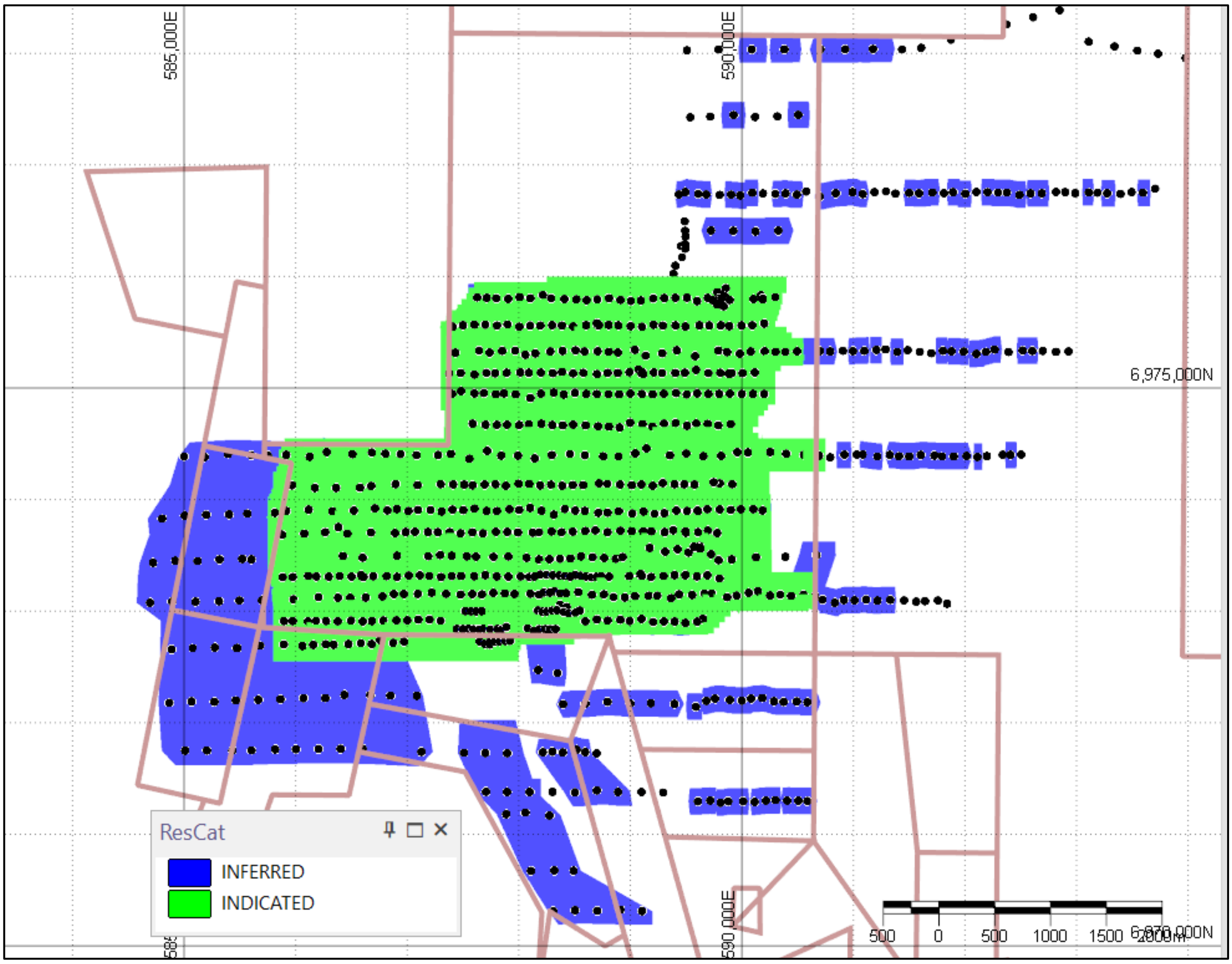

Figure 1: North Stanmore MRE by Resource category

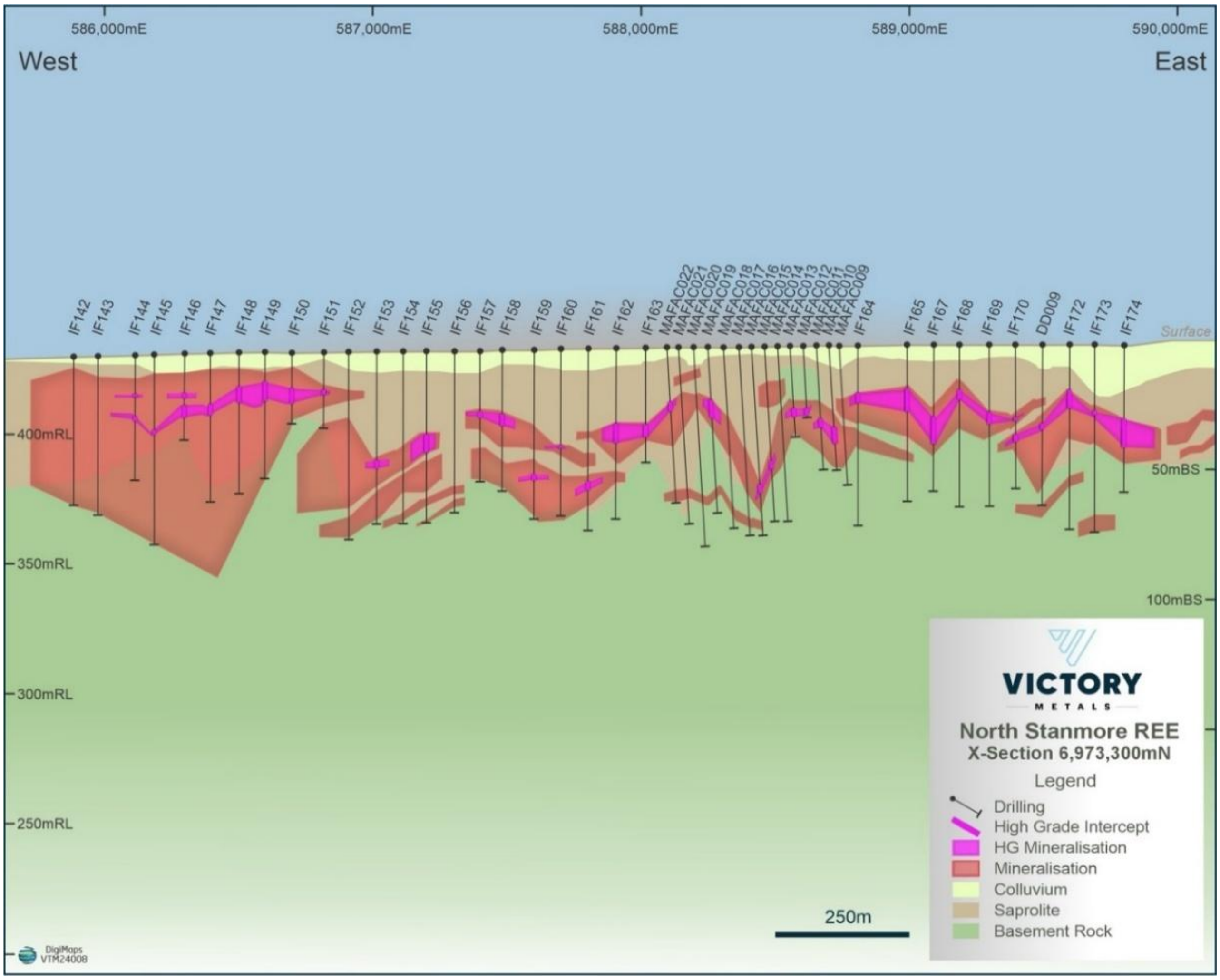

Figure 2: Cross section 6,973,900mN, looking north, 5x vertical exaggeration and showing the High-Grade intercept.

A site visit was conducted on May 30, 2024, by MEC Manager of Resources, Mr Dean O'Keefe and MEC Resource Geologist, Mr Issam Digais, accompanied by Victory Metals personnel including Mr Savvas Hagiantoniou, Exploration Site Supervisor. Dean O'Keefe is an MEC Competent Person for the North Stanmore MRE. During the site visit the general layout of the area and project location was checked. MEC also conducted a check survey of drillhole collar locations, the surveyed locations were confirmed as being in close proximity, to the planned drillhole locations, all within 3m. No production had occurred at North Stanmore at the time of the site visit.

The North Stanmore MRE occurs in regolith above an alkaline intrusion (Figure 2). Despite its magnetic signature, the North Stanmore intrusion had not been recognised previously on regional geological maps. Petrological data for samples of diamond core confirm its alkaline character and indicate that the intrusion is post-tectonic and hence, post-Archean in age.

The North Stanmore Intrusion is a large (approximately 16km by 5km) differentiated ultramafic to felsic intrusion. Lithologies identified in thin section include kaersutite- and carbonate-bearing peridotite, orthopyroxenite, clinopyroxenite, leuco- and leuco-gabbro (ijolite), diorite, monzonite and syenite. Some regolith samples are strongly LREE enriched indicating that the intrusion also contains carbonatite. However, the uniformly high HREO/TREO of the regolith (of approximately 34% to 38%) indicates that carbonatite represents a subordinate phase in the intrusion.

The North Stanmore Intrusion is interpreted to be associated with an early Proterozoic plume track that was responsible for alkaline magmatism extending in a broad belt from Mt Weld carbonatite near Laverton through Leonora to Cue.

The rare earth element mineralisation occurs in a relatively flat-laying saprolite-rich clay horizon beneath a veneer of unconsolidated colluvium that ranges in thickness from 0–36m. The uniformity of Nb/Ta ratios (Nb/Ta 16±4) in the regolith above the North Stanmore Intrusion indicates that the regolith developed *in situ*. Importantly, studies indicate that Nb/Ta ratio of regolith over carbonatites and other alkaline intrusions closely resembles the Nb/Ta ratio of their source plume generated lithologies.

REEs are adsorbed onto kaolinite or form secondary REE phosphates, rhabdophane (after monazite), churchite (after xenotime), and florencite. QEMSCAN mineralogical studies show that the REEs are mainly hosted by <20µm particles.

Scandium oxide (Sc_2O_3) is enriched throughout the regolith profile due to the breakdown of pyroxene in the North Stanmore source lithologies. Scandium oxide is generally considered to behave differently to the REEs, which are adsorbed as outer-sphere complexes on clay surfaces, found in $Al(OH)_2SiO$ sites, or occur as hydrated REE bearing phosphates. However, Sc^{3+} behaves like the transition metals (Ni^{2+}, Co^{2+}, Cu^{2+}) and, due to its smaller ionic radius, it adsorbs onto vacancy sites in clay lattices or attaches to the surface of Mn oxides.

Scandium is a highly valuable critical element occurring in the same Group of the Periodic Table (Gp. 3B) as the lanthanides. It occurs predominantly in HREE bearing ultramafic and mafic igneous rocks like the North Stanmore Intrusion. By contrast, felsic alkaline rocks and granitoids are more LREE enriched and contain negligible amounts of Scandium. The chemical properties of Scandium are distinct from the other REO's and Scandium has recently been recognised to have superconducting properties. Scandium has been deemed a critical mineral due to current Chinese and Russian control of the supply chain.

Yttrium is classified as a REO because of its similar ionic radius to the lanthanides, and similar chemical properties to the HREEs.

A geological cut-off grade of 150ppm TREO + Sc_2O_3 was used to separate mineralised material (MIN) from weakly mineralised material (WMM). A high-grade mineralisation (HGMIN) domain was additionally modelled above a geological cut-off grade of 600ppm TREO + Sc_2O_3. Ordinary block kriging with no top-cut was used for estimation separately of lodes within the high-grade zone and then lodes within the mineralised zone.

Logging was completed for 90% of the sample intervals and used to produce surfaces to delineate the colluvium, upper saprolite, saprolite, sap rock, slightly weathered fresh, and fresh rock.

The North Stanmore database used for the August 2025 MRE includes eight hundred and thirty-four (834) drillholes for 45,339.9m, inclusive of 773 Air-core (AC) drillholes for 41,409m, 50 Reverse Circulation (RC) drillholes for 3,166m, and 11 diamond drill holes for 764.9m. Drillhole depths range from 10m to 222m. All drillholes were completed by Victory from 2022 to 2025. The drillhole spacing at North Stanmore (MRE area) ranges from 50m x 50m to 250m x 100m.

Eleven percussion (air core and RC) drillholes were twinned with diamond drilling (DD001 to DD011). Samples were submitted to the laboratory for analysis only where the initial screening by handheld XRF generated a mineralised value, whereas the diamond drilling was sampled and assayed along the entire length of the drillhole. There is good spatial correlation between the air core and diamond assays for the twin drilling. Yttrium (Y) values obtained by handheld XRF (pXRF) is an excellent indicator of zones of mineralisation within the percussion holes.

Local validation was completed by comparing the composite grades used to estimate the block values against the estimated block values. There was close correlation between composite assays and estimated block grades, with some small differences resulting from the smoothing effect of ordinary kriging. Min/max checks were utilised to ensure all blocks were populated. OBM validation functions were used to check for overlapping blocks, there were no incidence of overlapping blocks.

The Mineral Resource has been classified as Indicated and Inferred categories, in accordance with the 2012 Australasian Code for Reporting of Mineral Resources and Ore Reserves (JORC Code). Unclassified material based on sparse exploration data has not been reported as part of the Mineral Resource. A range of criteria has been considered in determining this classification including:

- Geological continuity
- Data quality
- Drill hole spacing

An Indicated Mineral Resource classification was based on drillhole spacing (250m x 100m, closing to 50m x 50m), in addition to acceptable underlying QAQC, and an RTK/DGPS survey of drillhole collars. An Inferred Mineral Resource classification was based on a drill spacing of ~500m x 100m. Approximately 55% by tonnage of the August 2025 MRE is classified as Indicated Mineral Resources and approximately 45% is classified as Inferred Mineral Resources.

Three stages of metallurgical test work have been completed for the North Stanmore Project, focusing on beneficiation, and leach test work to establish potential recoveries and processing options.

Core Resources (**Core**) located in Brisbane completed the third stage of test work including beneficiation test work in March of 2024 and reported that the REE feed grade increased by 63% by rejecting the +53µm feed material from across all samples. Core also completed leach test work on the beneficiated material.

The leach test work program involved diagnostic metallurgical testing on a composite blend of the beneficiated samples with a head grade of 1,283 ppm TREO. This was sourced from 23 samples and 13 drillholes from North Stanmore. The initial atmospheric leach test work program was trialled at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and heavy rare earth elements Tb (91%), and Dy (92%) with a combined recovery of 93% Magnet Rare Earth Elements ("MREE").

Scandium oxide (Sc_2O_3) recoveries of 50% had previously been achieved, with optimisation work occurring in parallel. These assays were conducted by Australian Laboratory Services, Brisbane. The objective of the diagnostic test work was to recover REE and Scandium oxide from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).

The August 2025 MRE includes a Mineral Resource estimate is shown in Table 1.

Table 1: North Stanmore August 2025 MRE (≥330ppm TREO + Sc_2O_3 cut-off grade)

CLASSIFICATION	MRE TONNES (t)	TREOSc (ppm)	TREO (ppm)	HREO (ppm)	LREO (ppm)	HREO/TREO (%)	Sc_2O_3 (ppm)	Ga_2O_3 (ppm)
INDICATED	176,522,000	532	505	190	316	39	26	26
INFERRED	144,118,000	484	463	166	297	37	21	25
TOTAL	**320,640,000**	**510**	**486**	**179**	**307**	**38**	**24**	**26**

Numbers are rounded to reflect they are an estimate. Numbers may not sum due to rounding.

The sensitivity of the Mineral Resource estimate to the reporting cut-off grade is shown in Figure 3.

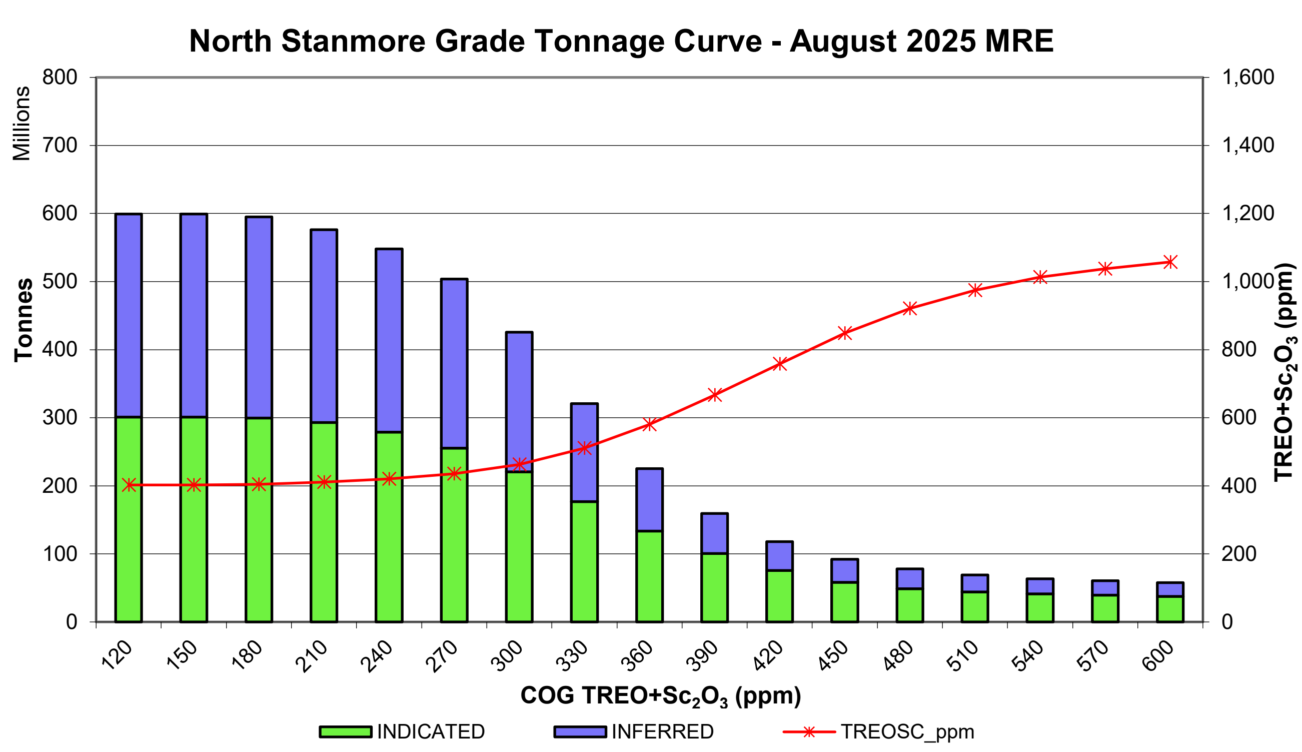

Figure 3: Grade tonnage curve for the North Stanmore TREO + Sc2O3 MRE (Indicated and Inferred)

Table 2 shows the HREO within the HGMIN domain by classification, and Table 3 shows the HREO within the MIN domain by classification.

Table 2: North Stanmore August 2025 MRE HREO within the HGMIN domain (≥330ppm TREO + Sc_2O_3 cut-off grade)

CLASSIFICATION	MRE TONNES (t)	TREO + Sc_2O_3 (ppm)	TREO (ppm)	HREO (ppm)	Eu_2O_3 (ppm)	Gd_2O_3 (ppm)	Tb_4O_7 (ppm)	Dy_2O_3 (ppm)	Ho_2O_3 (ppm)	Er_2O_3 (ppm)	Tm_2O_3 (ppm)	Yb_2O_3 (ppm)	Lu_2O_3 (ppm)	Y_2O_3 (ppm)
INDICATED	35,500,000	1,039	1,008	338	8.0	32.5	5.3	32.5	6.8	20.1	2.9	18.6	2.7	209
INFERRED	19,600,000	1,093	1,067	347	8.2	33.1	5.4	32.5	6.8	20.3	2.9	18.4	2.7	217
TOTAL	**55,025,000**	**1,059**	**1,029**	**341**	**8.1**	**32.7**	**5.3**	**32.5**	**6.8**	**20.2**	**2.9**	**18.6**	**2.7**	**212**

Numbers are rounded to reflect they are an estimate.
Numbers may not sum due to rounding.

Table 3: North Stanmore August 2025 MRE HREO within the MIN domain (≥330ppm TREO + Sc_2O_3 cut-off grade)

CLASSIFICATION	MRE TONNES (t)	TREO + Sc_2O_3 (ppm)	TREO (ppm)	HREO (ppm)	Eu_2O_3 (ppm)	Gd_2O_3 (ppm)	Tb_4O_7 (ppm)	Dy_2O_3 (ppm)	Ho_2O_3 (ppm)	Er_2O_3 (ppm)	Tm_2O_3 (ppm)	Yb_2O_3 (ppm)	Lu_2O_3 (ppm)	Y_2O_3 (ppm)
INDICATED	141,000,000	404	379	152	2.6	12.6	2.2	14.2	3.1	9.5	1.4	9.4	1.4	95.5
INFERRED	124,600,000	389	368	138	2.4	11.5	2.0	12.8	2.8	8.7	1.3	8.7	1.3	86.5
TOTAL	**265,615,000**	**397**	**374**	**145**	**2.5**	**12.1**	**2.1**	**13.6**	**3.0**	**9.1**	**1.4**	**9.1**	**1.4**	**91.3**

Numbers are rounded to reflect they are an estimate.
Numbers may not sum due to rounding.

The economic cut-off grade for the AugustAugust 2025 MEC MRE (Table 1) was ≥330ppm TREO + Sc_2O_3. This cut-off grade was selected based on the evaluation of other like regolith hosted rare earth Mineral Resources.

The MIN domain grade and tonnage is exclusive of the HG grade and tonnage (Table 3).

Table 4 shows the LREO by domain and classification above 330ppm TREO + Sc_2O_3.

Table 5 shows gallium, and hafnium grades above 330ppm TREO + Sc_2O_3.

Table 4: North Stanmore August 2025 MRE LREO Grades by Domain and Classification (≥330ppm TREO + Sc_2O_3 cut-off grade)

DOMAIN	CLASSIFICATION	TONNES (t)	TREO+Sc_2O_3 (ppm)	LREO (ppm)	La_2O_3 (ppm)	CeO_2 (ppm)	Pr_6O_{11} (ppm)	Nd_2O_3 (ppm)	Sm_2O_3 (ppm)
HGMIN	INDICATED	35,485,000	1,039	669	162.3	281.8	39.5	153.0	32.8
HGMIN	INFERRED	19,540,000	1,093	720	182.3	300.2	42.4	161.8	33.7
HGMIN	TOTAL	**55,025,000**	**1,059**	**688**	**169.4**	**288.3**	**40.6**	**156.2**	**33.1**
MIN	INDICATED	141,037,000	404	227	50.9	102.2	12.5	49.9	11.5
MIN	INFERRED	124,578,000	389	230	53.8	102.5	12.9	49.8	11.1
MIN	TOTAL	**265,615,000**	**397**	**228**	**52.2**	**102.4**	**12.7**	**49.8**	**11.3**
Total	TOTAL	**320,640,000**	**510**	**307**	**72.3**	**134.3**	**17.5**	**68.1**	**15.1**

Numbers are rounded to reflect they are an estimate. Numbers may not sum due to rounding.

Table 5: North Stanmore August 2025 MRE Hf, Ga_2O_3 (≥330ppm TREO + Sc_2O_3 cut-off grade)

DOMAIN	CLASSIFICATION	Tonnes (t)	Hf (ppm)	Ga_2O_3 (ppm)
HGMIN	INDICATED	35,485,000	6	26
HGMIN	INFERRED	19,540,000	5	25
HGMIN	TOTAL	**55,025,000**	**6**	**26**
MIN	INDICATED	141,037,000	7	26
MIN	INFERRED	124,578,000	6	26
MIN	TOTAL	**265,615,000**	**6**	**26**
Total	TOTAL	**320,640,000**	**6**	**26**

Numbers are rounded to reflect they are an estimate. Numbers may not sum due to rounding.

The January 2025 MRE compared to the August 2025 MRE has the same Indicated Mineral Resources tonnage of 176.5Mt, however, the TREOSc ppm grade has increased from 503 to 532 ppm. The January 2025 Inferred Mineral Resources tonnage has increased from 70.9Mt to 144.1Mt for the August 2025 MRE. The Inferred Mineral Resources TREOSc ppm grade has decreased from 561 to 484 ppm.

The January 2025 Mineral Resources tonnage has increased from 274.5Mt to 320.6Mt for the August 2025 MRE. The Total Mineral Resources TREOSc ppm grade has changed from 520 to 510 ppm.

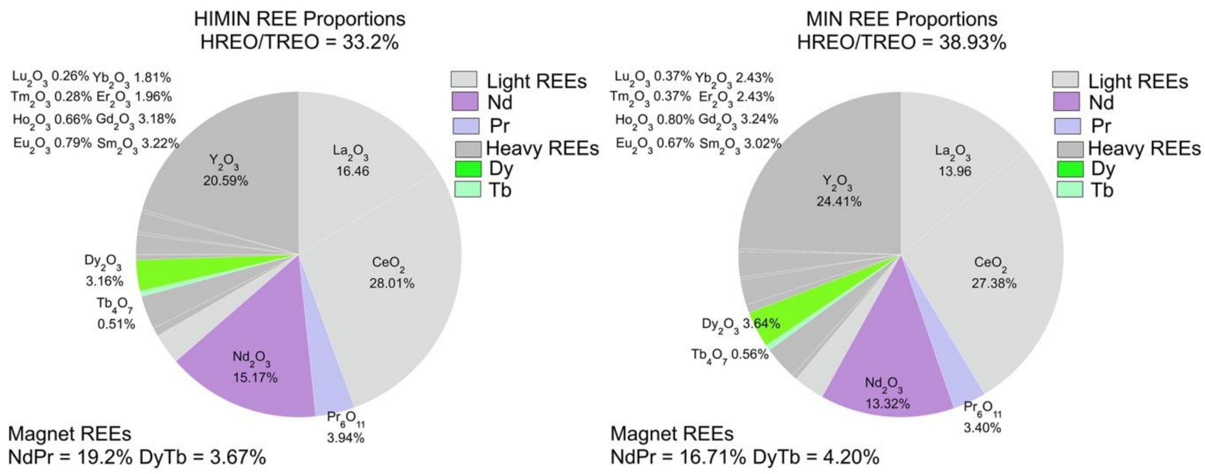

Figure 4: North Stanmore August August updated MRE composition by percentage in 55Mt and 265Mt resource domains

The high HREYO/TREYO ratios indicate that the North Stanmore Mineral Resource contains a significant percentage of the rare, and valuable, HREE's Dysprosium (Dy) and Terbium (Tb) (Figure 4).

Regional Geology

Victory's tenements lie north of Cue, within the centre of the Murchison Province, which comprises the Archaean gneiss-granitoid-greenstone north-western Yilgarn Block. The Archean greenstone belts in the Murchison Province, the Warda Warra and Dalgaranga greenstone belts, and the southern parts of the Meekatharra-Mount Magnet and Weld Range belts are dominated by metamorphosed supracrustal mafic volcanic rocks, as well as sedimentary and intrusive rocks. Thermo-tectonism resulted in development of large-scale fold structures that were subsequently disrupted by late-stage faults. The greenstone belts are intruded by two suites of granitoids. The first, most voluminous suite, comprises granitoids that are recrystallised with foliated margins and massive cores, typically containing large enclaves of gneiss. The second suite consists of relatively small, post tectonic intrusions. Two large Archaean gabbroic intrusions occur south of Cue. These are the Dalgaranga-Mount Farmer gabbroid complex in the southwest, and the layered Windimurra gabbroic complex in the southeast.

Project Geology

Victory's REE, Sc and Ga discovery occurs in regolith above the North Stanmore alkaline intrusion, discovered north of Cue. Despite its magnetic signature, the North Stanmore intrusion had not been recognised previously on regional geological maps. Petrological data[1] for samples of diamond core indicate that the intrusion is post-tectonic and hence post-Archean in age.

[1] Refer VTM ASX release dated 10 August 2022, *Major Alkaline Igneous Complex Discovered*

The North Stanmore Intrusion is a large (approximately 16km by 5km) differentiated ultramafic to felsic intrusion. Lithologies identified in thin section include kaersutite and carbonate-bearing peridotite, orthopyroxenite, clinopyroxenite, leuco- and leuco-gabbro, ijolite, diorite, monzonite and syenite. Some regolith samples are strongly LREE enriched indicating that the intrusion also contains carbonatite. However, the uniformly high HREO/TREO of the regolith (of approximately 34% to 38%) indicates that carbonatite represents a subordinate phase in the intrusion.

The North Stanmore Intrusion is interpreted to be associated with an early Proterozoic plume track that was responsible for alkaline magmatism extending in a broad belt from Mt Weld carbonatite near Laverton through Leonora to Cue[2].

Deposit Type

The rare earth element mineralisation occurs in a relatively flat-laying saprolite-rich clay horizon beneath a veneer of unconsolidated colluvium that ranges in thickness from 0m to 36m. The uniformity of Nb/Ta ratios (Nb/Ta 16±4) in the regolith above the North Stanmore Intrusion indicates that the regolith developed *in situ.* Importantly, studies have shown that Nb/Ta ratio of regolith over carbonatites and other alkaline intrusions closely resembles the Nb/Ta ratio of their source plume generated lithologies[3].

Mineralised REE saprolite horizons above the North Stanmore Intrusion occur at depths between 12m and 77m. Ce/Ce* tracks regolith oxidation, and the upper parts of regolith enrichment zones have Ce/Ce* >1 reflecting gain of mobile Ce^{4+}, while the lower parts of enrichment zones have Ce/Ce* <1. Leachable clay REE deposits all have Ce/Ce* <1. The Ce/Ce* of the MRE in the Indicated category is 0.86.

REEs are complexed with carbonate ions [CO_3^{2-}] and bicarbonate ions [HCO_3^-] or occur as REE^{3+} ions in soil as groundwater migrates downwards during tropical weathering. Based on Ce/Ce*systematics[4] and TREO concentrations, there appear to be four zones of REE enrichment at North Stanmore. These are 15m to 25m, 28m to 37m, 41m to 46m and a deeper zone between 53m and 77m. The regolith is complex and importantly some cores exhibit two zones of REE enrichment.

REEs are adsorbed onto kaolinite or form secondary REE phosphates, rhabdophane (after monazite), churchite (after xenotime), and florencite. QEMSCAN mineralogical studies show that the REEs are mainly hosted by <20-µm particles.

Scandium is enriched throughout the regolith profile due to the breakdown of pyroxene in the North Stanmore source lithologies. Sc is generally considered to behave differently to the REEs, which are adsorbed as outer-sphere complexes on clay surfaces, found in $Al(OH)_2SiO$ sites, or occur as hydrated REE bearing phosphates. However, Sc^{3+} behaves like the transition metals (Ni^{2+}, Co^{2+}, Cu^{2+}) and, due to its smaller ionic radius, it adsorbs onto vacancy sites in

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[2] Fiorentini et al., (2020) Nature Sci. Repts. 10:19729
[3] Cornelius et al, (2005) Geochemistry: Exploration, Environment, Analysis, Vol. 5, 291–310; Zhukova et al., (2021) Ore Geology Reviews 139, 104539
[4] $Ce/Ce^* = (2*(Ce_N)/(La_N+Pr_N))$, where Ce_N, La_N and Pr_N are chondrite normalised values; La_N = La concentration /0.237, Ce_N =Ce concentration /0.613 and Pr_N =Pr concentration/0.0928; Ce/Ce* ratios >1 reflect the gain of Ce^{4+} at shallower regolith depths while Ce/Ce* ratios <1 reflect the loss of mobile Ce^{4+} from deeper parts of weathering profiles that contain Ce^{3+}.

clay lattices or attaches to the surface of Mn oxides[5]. Sc is enriched throughout the regolith profile.

REO and Gallium Terminology

Yttrium is included as a REE because of its similar ionic radius to the lanthanides and has similar chemical properties to the HREEs [holmium (Ho) and erbium (Er)].

Scandium, a highly valuable critical element occurs in the same Group of the Periodic Table (Gp. 3) as the lanthanides. It occurs predominantly in HREE bearing ultramafic and mafic igneous like the North Stanmore Intrusion. By contrast, felsic alkaline rocks and granitoids are more LREE enriched and contain negligible amounts of Sc contents. The chemical properties of Sc are distinct from the other REEs, and Sc has recently been recognised to have superconducting properties. Sc has been deemed a critical mineral due to current Chinese and Russian control of the supply chain.

Gallium is a chemical element with the symbol Ga and atomic number 31. It is a soft, silvery metal that is solid at room temperature but melts just above it, making it unique among metals. Gallium is primarily used in the production of semiconductors, particularly in devices like light-emitting diodes (LEDs) and solar panels. It forms important compounds such as gallium arsenide (GaAs), which is widely used in electronics due to its excellent semiconductor properties. Additionally, gallium is known for its ability to form binary compounds with elements like phosphorus and arsenic, which are crucial in various technological applications.

Analytical data was determined by ALS using the ME-MS81 technique of fusion digestion followed by ICPMS analysis. Results were returned in elemental form and were converted to oxides.

TREO (Total Rare Earth Oxides), LREO (Light Rare Earth Oxides), HREO (Heavy Rare Earth Oxides), MREO (Magnet Rare Earth Oxides), and the ratio of HREO/TREO were calculated as follows:

- **TREO** is the sum of La_2O_3, CeO_2, Pr_6O_{11}, Nd_2O_3, Sm_2O_3, Eu_2O_3, Gd_2O_3, Tb_4O_7, Dy_2O_3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, and Y_2O_3,. This follows the protocol recommended by the International Union of Pure and Applied Chemistry.[6] Yttrium and Scandium are included as they share Group IIIA properties in the Periodic Table with the lanthanides. Importantly, yttrium exhibits similar geochemical properties to the HREOs.

- **TREOS** is the sum of La_2O_3, CeO_2, Pr_6O_{11}, Nd_2O_3, Sm_2O_3, Eu_2O_3, Gd_2O_3, Tb_4O_7,Dy_2O_3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, Y_2O_3, and Sc_2O_3.

- **HREO** is the sum of Eu_2O_3, Gd_2O_3, Tb_4O_7, Dy_2O3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, and Y_2O_3.

[5] Zhang et al., (2024) Am. Mineralogist
[6] Williams Jones and Vasyukova (2018) Economic Geology

- **LREO** is the sum of La_2O_3, CeO_2, Pr_6O_{11}, Nd_2O_3, and Sm_2O_3.
- **MREO** (Magnet Rare Earth Oxides) are the rare earths used in the production of magnets predominantly, Nd_2O_3, Pr_6O_{11} (**NdPr**) and Dy_2O_3, Tb_4O_7 (**DyTb**).
- HREO/TREOS is the ratio of the sum of Eu_2O_3, Gd_2O_3, Tb_4O_7,Dy_2O3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, and Y_2O_3/sum of La_2O_3, CeO_2, Pr_6O_{11}, Nd_2O_3, Sm_2O_3, Eu_2O_3, Gd_2O_3, Tb_4O_7,Dy_2O3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, Y_2O_3, and Sc_2O_3.

Mineralisation controls

Paleoplate tectonics

The small disparity between the equator and polar temperature gradients during the North Stanmore deposit formation was the absence of polar ice caps during the deposit formation period. Australia was geographically located further south, proximate to the current position of Antarctica. Continental drift resulted in the migration of Australia over 50 million years to its current latitude.

The North Stanmore regolith formed 40-50 Ma ago when WA was located close to the South Pole. This coincided with the Eocene Thermal maximum, a period of global warming when tropical and sub-tropical forests occurred from pole to pole. The Eocene thermal maxima also coincided with a massive increase in global chemical weathering.

This unique period of global climate and intense chemical weathering led to the formation of a thick saprolite-rich regolith at North Stanmore, up to ~80 metres deep.

The REO mineralisation is situated higher in the regolith profile at North Stanmore and is generally contained within the saprolite and to a lesser extent the sap rock. This is favourable for economic development as it potentially allows for free dig of the saprolite and assists with process recovery, with easier classification to obtain the fine fractions.

Source Intrusion

The basement geology map was compiled from logging of slightly weathered rock that retained some rock fabric and from fresh rock where some drillholes were drilled to basement (Figure 5). Most drillholes were air core and were drilled to refusal which was often at top of fresh or sometimes in slightly weathered fresh.

The geochemistry of the regolith preserves inherited signatures from the underlying alkaline igneous protoliths.

The western alkaline mafic rocks represent a different mineralised system to the alkaline felsic rocks of the central and eastern zones. The mafic schist are interpreted to have been derived from Archean meta basaltic protoliths.

The host rock is a strong control of mineralization, with higher grade located within the weathered alkaline felsic rock (Figure 6).

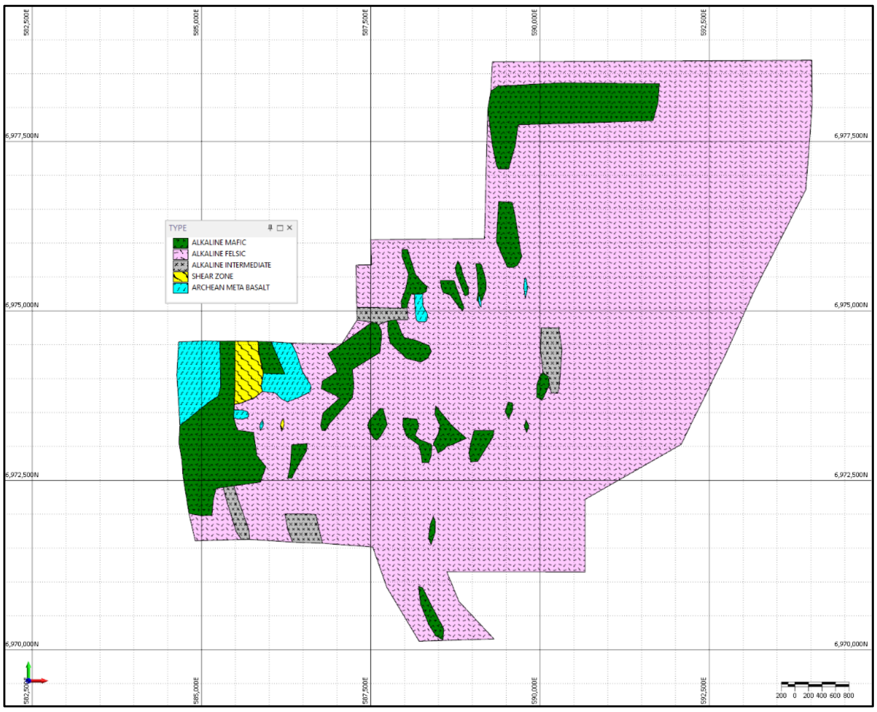


Figure 5: Plan view Basement geological map

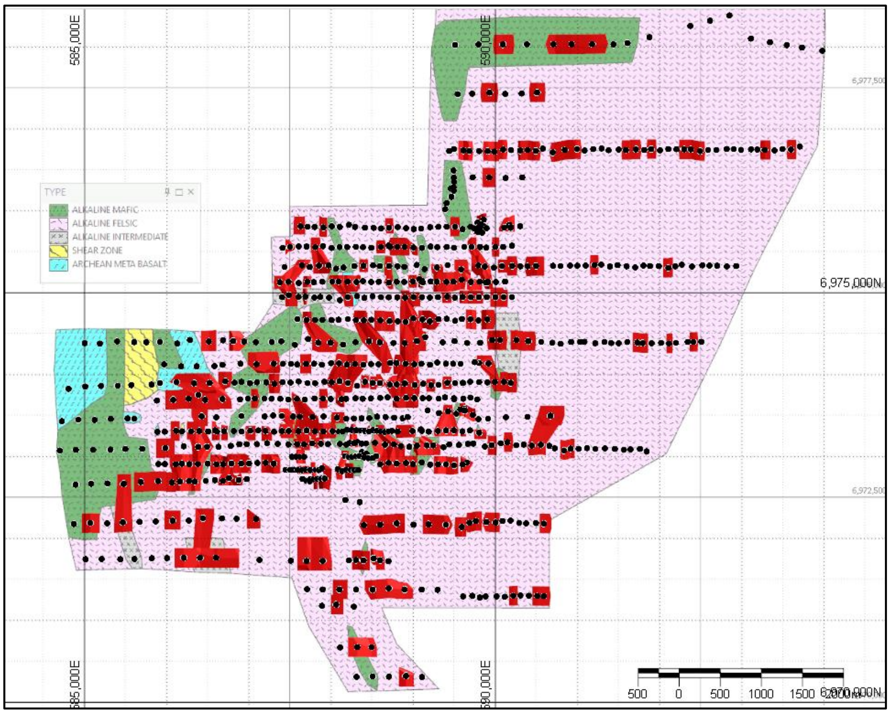


Figure 6: Plan view High grade lodes (Red) and geological map

Paleo water tables and ground water

Sub-horizontal higher-grade lodes are accompanied or contained within lower grade mineralised lodes that occur in larger haloes

Stacked lodes at different elevations equate to paleo water tables. The water table refers to the upper surface of groundwater, where saturated soil or rock meets unsaturated conditions. This level fluctuates based on rainfall, soil permeability, and geological formations. The water table specifically refers to the upper boundary of groundwater, whereas groundwater includes all water stored underground.

Subsequent supergene alteration has mobilised soluble elements, particularly REE in the upper parts of the regolith, to re-precipitate as secondary deposits, including the main REE concentrations (Figure 7). The REE have formed concentrated layers whilst less mobile elements such as scandium are less concentrated.

The changing water table over time has resulted in concentrated REE at different elevations. When the water table changed and was fixed at a different elevation for a prolonged period of time, it formed a concentrated REO lode at this level. As a result, there are multiple stacked levels of lodes. The elevations are consistent, however, the lodes may be broken or disjointed across strike (east – west) likely due to properties of the source rock and other factors that influence the movement of water into and through the subsurface (Figure 8).

High grade lodes were interpreted as sub-horizontal correlating with the paleo water table. The mineralisation interpreted lodes often correlated closely with the boundaries of the rock units (Figure 9).

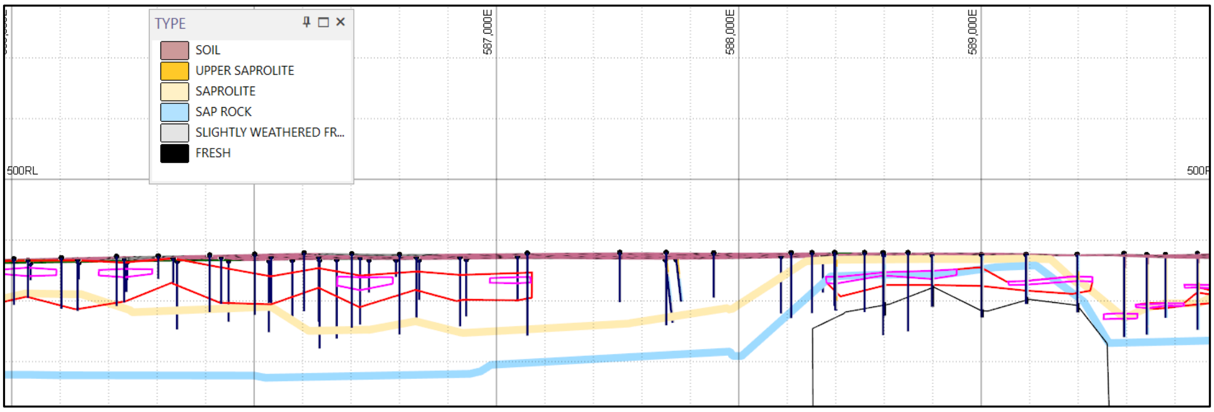


Figure 7: Cross section looking north, showing the basement high at 589,000 east, purple high grade lodes, red mineralised lodes

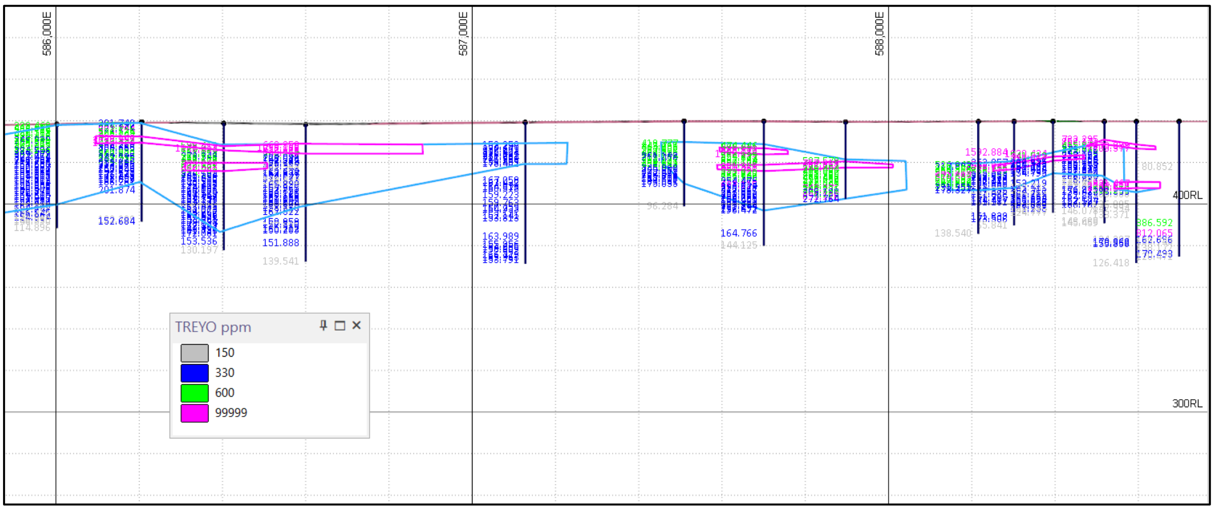


Figure 8: Cross section 6,971,800N,High grade lodes (purple lodes)are generally at the top of the profile, looking north, x5VE

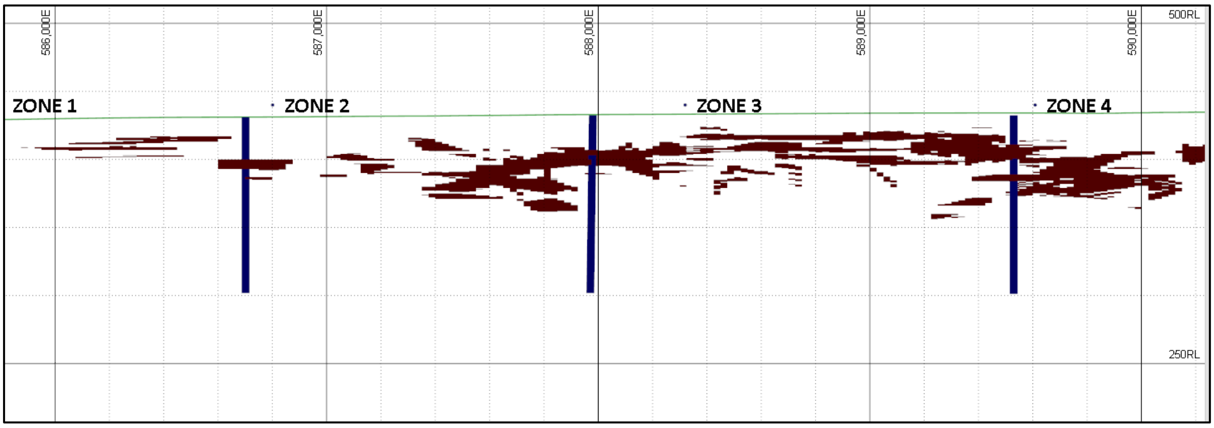


Figure 9: Cross section through the entire model for blocks above 1,000ppm TREO, showing relative levels of the four zones that correlate to paleo water tables, looking north, x5VE

Mineralisation controls and MRE

The understanding of the origins and control of the North Stanmore mineralisation has been incorporated into the modelling and Mineral Resource estimation methodology. This included:

- REE mineralisation formed *in situ*,
- Intense chemical weathering led to the formation of a thick saprolite-rich regolith,
- Host rock is a strong control of mineralisation, with higher grade located within the weathered alkaline felsic rock,
- Stacked high grade lodes at different elevations equate to paleo water tables and the haloes to the ground water.

Lodes have been interpreted and domained based on paleo water table origins, the high grade lodes occur within the alkaline felsics, and the bulk of mineralisation occurs within the saprolite and to a lesser extent sap rock lithotypes.

Sampling and sub-sampling techniques

Air-core drilling samples were collected as 1m samples from the rig cyclone. Each sample was placed into large green drill bags (900mmx600mm) for temporary storage onsite. Each sample was then split using a 3-tier (87.5% - 12.5%) splitter and the sample split was placed into calico sample bags for transport to Perth.

Sample weights and recoveries were recorded on site and weighed 1.5 - 2.5kg depending on the sample recovery from the drill hole. The mean bulk sample weight was 8.45kg.

A handheld pXRF analyzer (Olympus Vanta) was used to determine anomalous REO (Rare earth element) geochemistry (La, Ce, Pr, Nd, and Y) from the 1m sample piles. pXRF reading times were 45 secs over 3 cycles for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their integrity was checked using Certified REO -bearing geochemical standards. The handheld pXRF is used as a guide to the relative presence or absence of certain elements, including REOs vectors (specifically Y but also including La, Ce, and Nd) to help direct the sampling program. Anomalous 1m samples were then transported to the assay lab for analysis by Victory personnel. REO anomalism thresholds are determined by VTM technical lead based on historical data analysis

Victory attended North Stanmore to collect the green sample bag which was transported by Victory to Victory's secure warehouse in Perth.

Measures taken to ensure sample representivity included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight.

Drilling techniques

Drilling at North Stanmore to support the August 2025 MRE includes eight hundred and thirty-four (834) drillholes for 45,339.9m, inclusive of 773 Air-core (AC) drillholes for 41,409m, 50 Reverse Circulation (RC) drillholes for 3,166m, and 11 diamond drill holes for 764.9m. Drillhole depths range from 10m to 222m. All drillholes were completed by Victory from 2022 to 2025.

The drillhole spacing at North Stanmore ranges from 50 x 50m to 250 x 100m.

Mineral Resource estimation

The estimation methodology was ordinary block kriging (OK) with inverse distance weighting to a cubed power used for validation (IDW3). Block model dimensions used are 50 metres (east) by 50 metres (west) by 1 metre (elevation) with sub-blocking down to 25 metres (east) by 25 metres (north) by 0.5 metres (elevation).

The estimation was constrained within explicitly generated wireframe solids using the resource drill hole dataset. Wireframe solids were created to group zones of mineralisation (MIN) and high-grade mineralisation (HGMIN). The wireframe solids were assigned to the assay file and the ore block model file (OBM). The assay file was then composited to 1m interval lengths, starting and stopping on the mineralisation wireframe boundaries.

The 1m composite assay file was used to model the experimental variograms with two components to fit spherical models for the HREO and LREO groups (Table 6).

Table 6: North Stanmore Modelled Variograms by REO Group

REO GROUP	ORIENTATION			
	AXIS	AZIMUTH °	PLUNGE °	ROTATION °
HREO	1	150	0	
	2	240	10	0
	3	180	-90	
MIN	1	150	0	
	2	240	10	0
	3	180	-90	

REO GROUP	MODEL STRUCTURE ɣ				RANGES (m)		
	TOTAL SILL	NUGGET C0	C1	C2	MAJOR	INTERMEDIATE	MINOR
HREO	39,120	24,050	C1	620	720	382	0.9
			C2	14,450	2,100	1,720	3.5
MIN	108,330	53,700	C1	8,170	270	860	2.6
			C2	46,460	875	1,120	3.8

Ordinary block Kriging (OK) was used to estimate all rare earth oxides as individual analytes. Inverse Distance to a cubed Power was used to estimate potential credit elements (scandium oxide, gallium oxide, nickel, cobalt, copper, and hafnium). The estimation used hard boundaries. The estimation employed a three-pass search strategy (Table 7). All blocks were populated by the third search pass.

Table 7: North Stanmore Estimation Search Parameters

REO GROUP	RUN	RADIUS D1 (m)	RADIUS D2 (m)	RADIUS D3 (m)	SECTORS	MAX SAMPLES	MIN DRILLHOLES	STRIKE °	PITCH °	DIP °
HREO	1	600	400	25	8	48	3	0	0	-90
HREO	2	1,000	800	50	8	48	3	0	0	-90
HREO	3	1,500	1000	75	1	NA	1	0	0	-90
MIN	1	600	400	25	8	48	3	0	0	-90
MIN	2	1,000	800	50	8	48	3	0	0	-90
MIN	3	1,500	1,000	75	1	NA	1	0	0	-90

The following variables were estimated using ordinary kriging: La_2O_3, CeO_2, Pr_6O_{11}, Nd_2O_3, Sm_2O_3, Eu_2O_3, Gd_2O_3, Tb_4O_7, Dy_2O_3, Ho_2O_3, Er_2O_3, Tm_2O_3, Yb_2O_3, Lu_2O_3, and Y_2O_3.

The following variables were estimated using inverse distance cubed: Sc_2O_3, Ga_2O_3, Ni, Co, Cu and Hf.

To determine density values, regression analysis was divided into domains based on rock type. Within each domain, a regression factor was calculated by dividing the geophysical density by the diamond core density at each percentile, then taking the mean of these values. This value is the regression factor, which was then applied back to the downhole geophysical density. The mean of these regressed values was taken as a representative nominal density value for each domain. Tonnage estimation was based on dry density values for colluvium of 1.70 t/m^3, saprolite of 1.71 t/m^3, sap rock of 2.18 t/m^3, slightly weathered fresh of 2.2 t/m^3 and fresh of 2.3 t/m^3,

Mineral Resource Classification

A range of criteria has been considered in determining this classification including:

- Geological continuity and lode geometry
- Data quality
- Drill hole spacing

An Indicated Mineral Resource classification was based on drillhole spacing (250m x 100m, closing to 50m x 50m), acceptable underlying QAQC, and an RTK/DGPS survey of drillhole collars. An Inferred Mineral Resource classification was based on a drill spacing of ~500m x 100m.

Approximately 55% by tonnage of the August 2025 MRE is classified as Indicated Mineral Resources and approximately 45% by tonnage is classified as Inferred Mineral Resources.

Sample analysis method

Samples were assayed by ALS Laboratories in Perth, a NATA Accredited Testing Laboratory. The assay methods used include:

- ME-4ACD81: Four acid digestion followed by ICP-AES measurement
- ME-MS81: Lithium borate fusion followed by acid dissolution and ICP-AES measurement
- ME-ICP06: Fusion decomposition followed by ICP-AES measurement

REOs were all analysed by ME-MS81 (four acid digestion followed by ICP-AES measurement) with results returned in their elemental form. Elements were then converted to oxides using the appropriate stoichiometric conversion factors.

Base metals are assayed by ME-ICP06: Fusion decomposition.

Non-ferrous metals are assayed by ME-4ACD81: Four acid digestion.

Using a riffle splitter, 1m composite samples were collected from the individual sample bags.

Quality control of the assaying comprised the collection of a bulk repeat sample every hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every 20 samples and blanks (beach sand) every 50 samples. The repeat sample was collected by passing the bulk reject obtained from the first split stage through the riffle splitter once more. The repeat sample is not a duplicate.

Validation

All ore block models were validated globally and locally. Global validation compared the wireframe volume and grade with the ore block model volume and grade, at a zero-cut-off grade. The global volume comparison between the wireframes and the sub celled ore block models was close. The global grade comparisons of grade within the low grade and high-grade wireframes compared to their respective modelled grades is within 5%, with small differences occurring due to the clustering of grades within the wireframes. Local validation was completed by comparing the composite grades used to estimate the block values against the estimated block values. There was close correlation between composite assays and estimated block grades, with some small differences resulting from the smoothing effect of ordinary kriging. Min/max checks were utilised to ensure all blocks were populated. OBM validation functions were used to check for overlapping blocks, there were no incidence of overlapping blocks.

Cut-off grade

The economic cut-off grade for the August 2025 MEC MRE was ≥330ppm TREO +Sc_2O_3. This cut-off grade was selected based on the evaluation of other like regolith hosted rare earth Mineral Resources.

Metallurgical Testwork

Four stages of metallurgical test work have been completed on the North Stanmore Project, focusing on beneficiation, and leach test work to establish potential recoveries and processing options.

Core Resources (**Core**) located in Brisbane completed the third stage of test work including beneficiation test work in March of 2024 and reported that the REE feed grade increased 63% by rejecting the +53µm feed material from across all samples. Core also completed leach test work on the beneficiated material[7]

The leach test work program involved diagnostic metallurgical testing on a composite blend of the beneficiated samples with a head grade of 1,283 ppm TREO. This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trailed at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) as well as the less valuable light rare earth elements Pr (94%), Nd (94%), with a combined recovery of 93% MREO.

Scandium recoveries of 50% had previously been achieved, with optimisation work occurring in parallel. These assays were conducted by Australian Laboratory Services Brisbane. The objective of the diagnostic test work was to recover REE and Sc from the beneficiated sample

[7] Williams Jones and Vasyukova (2018) Economic Geology
ore Sets Benchmark of 93% Magnet Metal Metallurgical Recoveries Refer VTM ASX release dated 14 May 2024, North Stanmore Sets Benchmark of 93% Magnet Metal Metallurgical Recoveries

using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).

The most recent metallurgical test work, conducted by Core, utilised a composite sample derived from 12 individual samples across 7 drill holes distributed throughout the North Stanmore project area. This composite had an average Total Rare Earth Oxide (TREO) grade of 873ppm, with a Heavy Rare Earth Oxide (HREO) to TREO ratio of 29%.

The leach test was performed over a 4-hour duration at 90°C. The results demonstrated impressive metallurgical recoveries across a wide range of elements: La: 91%, Ce: 94%, Pr: 97%, Nd: 97%, Sm: 98%, Eu: 97%, Gd: 96%, Tb: 94%, Dy: 87%, Ho: 77%, Er: 82%, Tm: 76%, Yb: 77%, Lu: 71%, Y: 72%, Ga: 34%.

Reasonable Prospects for Eventual Economic Extraction

Clause 20 of the JORC (2012) Code requires that all reported Mineral Resources have reasonable prospects for eventual economic extraction. MEC has confirmed the reasonable prospects for eventual economic extraction in relation to the North Stanmore Project based on the following:

- **Shallow Mineralisation:** North Stanmore Mineral Resources occur close to surface and are believed to be amenable to an opencut mining operation.
- **Favourable Metallurgical Results:** Metallurgical testwork has returned favourable processing recoveries.
- **Proximity to Cue:** The North Stanmore Project is situated approximately 6km from the Cue township
- **Excellent connectivity:** Via the Great Northern Highway, a major arterial road linking the project to Geraldton Port (420 km).

This announcement has been authorised by the Board of Victory Metals Limited.

For further information please contact:

Brendan Clark CEO and Executive Director b.clark@victorymetalsaustralia.com	Ben Creagh Investor and Media Relations benc@nwrcommunications.com.au

Victory Metals Limited

Victory is dedicated to the exploration and development of its flagship North Stanmore Heavy Rare Earth Elements (HREE), Scandium, Gallium and Hafnium Project located in the Cue Region of Western Australia. The Company is committed to advancing this world-class project to unlock its significant potential.

Competent Person Statement

Competent Person Statement – Dean O'Keefe

The information in this announcement that relates to the Mineral Resource estimate is derived from, and fairly represents information compiled by Mr Dean O'Keefe, a Fellow of the Australasian Institute of Mining and Metallurgy (FAusIMM #112948). Mr O'Keefe is Competent Person for this style of mineralisation and is a consultant to Victory Metals Limited. Mr O'Keefe is a full time employee of MEC Technical Services Pty Ltd, an independent mining and exploration consultancy. Mr O'Keefe has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which they are undertaking to qualify as Competent Person as defined in the 2012 edition of the Australasian Code for the Reporting of Exploration Results, Mineral Resources, and Ore Reserves (JORC Code). The Competent Persons is not aware of any new information or omission of data that may materially affect the stated Mineral Resource estimate. Mr O'Keefe consents to the inclusion in this announcement of the matters based on his information in the form and context in which it appears.

APPENDIX 1: 2012 JORC CODE - TABLE 1

Section 1: Sampling Techniques and Data

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr>
<td>Sampling techniques</td>
<td>

Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as downhole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.
Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.
Aspects of the determination of mineralisation that are Material to the Public Report. In cases where ‘industry standard’ work has been done this would be relatively simple (e.g. ‘reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay’). In other cases, more explanation may

</td>
<td>

The North Stanmore drilling that contributed to the August 2025 MRE is shown as follows -

<table>
<tr><th>Compiled by</th><th>Year</th><th>Hole Type</th><th>Hole Prefix</th><th>Number</th><th>Total Depth (m)</th><th>Avg Depth (m)</th></tr>
<tr><td rowspan="6">RSC</td><td rowspan="4">2022</td><td rowspan="4">AC</td><td>MAFAC</td><td>45</td><td>2,726</td><td>61</td></tr>
<tr><td>NSE</td><td>96</td><td>5,080</td><td>53</td></tr>
<tr><td>NSTAC</td><td>223</td><td>13,015</td><td>58</td></tr>
<tr><td>Subtotal</td><td>364</td><td>20,821</td><td>57</td></tr>
<tr><td>2023</td><td>RC</td><td>23NSTRC</td><td>50</td><td>3,166</td><td>63</td></tr>
<tr><td colspan="3">Subtotal</td><td>414</td><td>23,987</td><td>58</td></tr>
<tr><td rowspan="6">MEC</td><td rowspan="5">2023</td><td rowspan="3">AC</td><td>IF</td><td>226</td><td>13,540</td><td>60</td></tr>
<tr><td>NEX</td><td>10</td><td>187</td><td>19</td></tr>
<tr><td>Subtotal</td><td>236</td><td>13,727</td><td>58</td></tr>
<tr><td>DH</td><td>DD</td><td>11</td><td>764.9</td><td>70</td></tr>
<tr><td colspan="2">Subtotal</td><td>247</td><td>14,492</td><td>59</td></tr>
<tr><td>2024</td><td>AC</td><td>AC</td><td>94</td><td>3,640</td><td>39</td></tr>
<tr><td></td><td>2025</td><td>AC</td><td>EX25AC</td><td>79</td><td>3,221</td><td>41</td></tr>
<tr><td rowspan="4">All</td><td colspan="3">AC</td><td>773</td><td>41,409</td><td>58</td></tr>
<tr><td colspan="3">RC</td><td>50</td><td>3,166</td><td>63</td></tr>
<tr><td colspan="3">DH</td><td>11</td><td>764.9</td><td>70</td></tr>
<tr><td colspan="3">Total</td><td>834</td><td>45,339.90</td><td>56</td></tr>
</table>

(AC) holes were drilled vertically and spaced 100m apart along 200m - 400m spaced drill lines.
(AC) drilling samples were collected as 1-m samples from the rig cyclone. Each sample was placed into large green drill bags (900mmx600mm) for temporary storage onsite.
Each sample was then split using a 3-tier (87.5% - 12.5%) splitter and the split sample was placed into calico sample bags for transport to Perth.
Sample weights and recoveries were recorded on site and weighed 1.5 - 2.5 kg depending on the sample recovery from the drill hole. The mean bulk sample weight was 8.45kg.
A reputable commercial transport company was used to transport the bags.
A handheld pXRF analyzer (Olympus Vanta) was used to determine anomalous REO (Rare earth element) geochemistry (La, Ce, Pr, Nd and Y) from the 1-m sample piles. pXRF reading times were 45 secs over 3 cycles for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their integrity was checked using Certified REO -bearing geochemical standards.
The handheld pXRF is used as a guide to the relative presence or absence of certain elements, including REOs vectors (La, Ce, Pr, Nd and Y) to help direct the sampling program. Anomalous 1m samples were then transported to the assay lab for analysis by Victory personnel. REO anomalism thresholds are determined by VTM technical lead based on historical data analysis
Victory attended North Stanmore to collect the green sample bag which was transported by Victory to Victory’s secure warehouse in Perth.
Measures taken to ensure sample representivity included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight.
RC drill samples were collected as 1-m samples from the rig cyclone and placed on top of black plastic, that was laid on the natural ground surface to prevent contamination, in separate piles and in orderly rows. A hand-held trowel was used to collect 4-m composite samples from the 1-m piles. Compositing did not account for lithology changes. These composite samples weighed between 2 and 3 kg.

</td>
</tr>
</table>

Criteria	JORC Code explanation	Commentary
	be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information	
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	• (AC) drilling uses a three bladed steel or tungsten drill bit to penetrate the weathered layer of loose soil and rock fragments. The drill rods are hollow and feature an inner tube with an outer barrel (similar to RC drilling). • (AC) drilling uses small compressors (750 cfm/250 psi) to drill holes into the weathered layer of loose soil and fragments of rock. • (RC) Drilling used a 5½" face sampling hammer with 1,350cfm/500 psi onboard compressor, which was occasionally supplemented with an additional booster (2,100cfm/1,000 psi). • After drilling is complete, an injection of compressed air is unleashed into the space between the inner tube and the drill rods inside wall, which flushes the cuttings up and out of the drill hole through the rod's inner tube, causing less chance of cross-contamination. • (AC) Drilling was performed by Seismic Drilling Pty Ltd and Orlando Drilling Pty Ltd, and the RC drilling was performed by Orlando Drilling Pty Ltd. • The drill rigs were inspected daily by VTM personnel for safety and rig hygiene
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• The majority of samples were dry and sample recovery was variable, where excessive water flows were encountered during drilling. • Representative percussion drillhole samples were collected as 1-metre intervals, with corresponding chips placed into chip trays and kept for reference at VTM's facilities. • Measures taken to ensure sample representivity and recovery included regular cleaning of the rig between drill holes using compressed air and weighing the bulk sample to ensure reasonable sample return against an expected target weight.

Criteria	JORC Code explanation	Commentary
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	• All percussion samples in the chip trays were lithologically logged using standard industry logging software on a notebook computer. • All (AC) samples have been logged for lithology, alteration, quartz veins, colour, fabrics. • All (AC) samples have been analysed by a handheld pXRF. • All samples were subjected to a NIR spectrometer for the identification of minerals and the variations in mineral chemistry to detect alteration assemblages and regolith profiles. • All geological information noted above has been reviewed by a competent person as recognised by JORC.
	• *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.*	• Logging is qualitative in nature. • (AC) samples have been photographed.
	• *The total length and percentage of the relevant intersections logged.*	• 90% of the sample intervals were logged.
Subsampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.*	• Diamond drilling was PQ core. • Half core samples were taken, with the exception of when twin samples were collected and then the samples were quarter core.
	• *If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.*	• Air core and RC sampling was undertaken on 1m intervals using a Meztke Static Cone splitter. In the Sampling techniques section above it mentions Riffle Splitter was used – This is contradictory • Most 1-metre samples were dry and weighed between 1.5 and 2.5 kgs. • Samples from the cyclone were placed into green drill bags in laid out in orderly rows on the ground. • Using a hand-held trowel, 1m samples were collected from the one-metre drill bags after splitting of the sample. • These samples were placed into calico bags and weighed between 1.5 and 2.5 kgs.

	• *For all sample types, the nature, quality and appropriateness of the sample preparation technique.*	• Samples were assayed by ALS Laboratories in Perth, a NATA Accredited Testing Laboratory. The assay methods used include:
		  ○ ME-4ACD81: Four acid digestion followed by ICP-AES measurement
		  ○ ME-MS81: Lithium borate fusion followed by acid dissolution and ICP-AES measurement
		  ○ ME-ICP06: Fusion decomposition followed by ICP-AES measurement
		• REOs were all analysed by ME-MS81 (four acid digestion followed by ICP-AES measurement) with results returned in their elemental form. Elements were then converted to oxides using the appropriate stoichiometric conversion factors.
		• Base metals are assayed by ME-ICP06: Fusion decomposition.
		• Non-ferrous metals are assayed by ME-4ACD81: Four acid digestion.

	• *Quality control procedures adopted for all*	• Using a riffle splitter, 1m composite samples were collected from the individual sample bags.

Criteria	JORC Code explanation	Commentary
	subsampling stages to maximise representivity of samples.	• Quality control of the assaying comprised the collection of a bulk repeat sample every hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every 20 samples and blanks (beach sand) every 50 samples. The repeat sample was collected by passing the bulk reject obtained from the first split stage through the riffle splitter once more. The repeat sample is not a duplicate.
	• *Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.*	• Fourteen twin samples of quarter core (diamond PQ) were compared to the original sample for each REO element and results were found to be acceptable.
	• *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Composite samples weighed between 1 and 2 Kg's. • Sample sizes are considered appropriate to the grain size of the material being sampled.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	• All samples were analysed in the field using a handheld Olympus Vanta XRF unit to identify geochemical thresholds. These results are not considered dependable without calibration using chemical analysis. They were used as a guide to the relative presence or absence of certain elements, including REOs to help guide the drill program and which samples were submitted for analytical analysis. • All pXRF anomalous samples were sent to ALS Wangara in Perth for analysis. Over time the mineralised sample criteria has evolved from an initial sampling threshold value of La+Ce+Nd+Pr+Y > 200ppm (for the RSC MRE), to Ce>30ppm (for the post RSC to July 2024 MRE), and most recently Y>30ppm (POST July 2024 to January 2025 MRE). • Samples were submitted for sample preparation and geochemical analysis by ALS in Wangara, Perth, a NATA accredited laboratory. All samples were crushed and pulverized to generate a pulp aliquot sample with 95% of the aliquot sample passing 75µ (ALS methods CRU-31, PUL-31). Aliquots were analysed using the following methods: ○ Lithium borate fusion prior to acid dissolution and ICP-AES (ALS method ME-MS81, a total assay technique) for Ba, Ce, Cr, Cs, Dy, Er, Eu, Ga, Gd, Hf, Ho, La, Lu, Nb, Nd, Pr, Rb, Sc, Sm, Sn, Sr, Ta, Tb, Th, Ti, Tm, U, V, W, Y, Yb, and Zr. ○ Lithium borate fusion prior to acid dissolution and ICP-AES (ALS method ME-ICP06, a total assay technique) for Al2O3, BaO, CaO, Cr2O3, Fe2O3, K2O, MgO, MnO, Na2O, P2O5, SiO2, SrO, TiO2, and Total. ○ 4-acid digest and read by ICP-AES (ALS method ME-4ACD81, a partial assay technique) for Ag, As, Cd, Co, Cu, Li, Mo, Ni, Pb, Sc, Tl, and Zn (base metals). ○ Thermogravimetric analysis to determine loss on ignition (LOI) content. • The sample preparation and analysis are considered appropriate for the analytes. • As a result of the pXRF analysis leading the selection criteria for assaying by a laboratory, only 16,620 metres of drilling of the total 45,340 drill metres (or 37% of total metres) has been assayed.

Criteria	JORC Code explanation	Commentary
	• *For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*	• At Victory's Perth facility spot checks were completed on selected samples using a handheld Olympus Vanta XRF unit. The pXRF device was used to determine anomalous REO geochemistry (La, Ce, Nd, Pr and Y) from the 1-m sample piles. • pXRF reading times were 45 secs over 3 beams for multielement and REO assays. These results are not considered dependable without calibration using chemical analysis from an accredited laboratory. However, their analytical accuracy was checked using REO -bearing geochemical standards. • The pXRF results were not used for estimation.

	• *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	• Sample weights were measured for 174 of the AC drillholes, and recovery was measured for 7 of the diamond drillholes. Sample recovery for the diamond drillholes recovery was 100 %. Based on the information available, sample recovery is acceptable for the diamond holes. The discrepancy between the target weight and the measured weight for the air-core samples indicates potential for bias, however, there may have been an issue with the target weight, and this should be reassessed.
		• Assay analytical precision was established by laboratory repeats and was deemed acceptable to the Competent Person/s.
		• The overall performance of standards was deemed to be acceptable
		  ○ It was noted that La, Pr, Ce and Eu in the CRM OREAS464 have expected values above the detection limits of the lab method ME_MS81.
		  ○ It was noted that Co and Ni in the CRMs OREAS461 and OREAS464 are over reported against the expected values using the lab method ME_4ACD81.
		  ○ It was noted that Cu and Sc in the CRM OREAS464 are under reported against the expected values using the lab method ME_4ACD81.
		• The overall performance of the blanks was deemed to be acceptable
		• Field diamond duplicate data points taken from the same drillholes is available only for 14 samples from diamond drill core. The mean grade of the original sample was generally reproduced by the duplicate for the various analytes and is acceptable to the Competent Person/s.
		• In April 2024, 37 samples were submitted to an umpire laboratory, Intertek Genalysis in Perth. The results were compared to the original assay results from ALS laboratories for the key analytes of interest to the project. There was no observable bias between the original assays completed by ALS and the checks completed by Intertek Genalysis Perth.
		• Twinned hole results are discussed in the relevant section below.
		• There are only 14 duplicates collected over the entire project drilling campaign. MEC recommends that future drilling campaigns will require an increase in duplicate samples to be collected to demonstrate the lack of sample bias in the rig-mounted splitter.

Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.*	• Victory's representative Prof Kenneth Collerson (PhD, FAusIMM) undertook verification of significant intersections.
	• *The use of twinned holes.*	• Eleven percussion (air core and RC) drillholes have been twinned with diamond drilling (DD001 to DD011). Samples were submitted to the laboratory for analysis

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td></td><td>only if the initial screening by handheld pXRF satisfied the anomalous value threshold as set by company policy, whereas the diamond drilling was sampled and assayed along the entire length of the drillhole.
• QQ plots were prepared between the percussion and diamond assays paired at 5m, with good correlation between the two drillhole types.</td></tr>
<tr><td></td><td>• Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</td><td>• ALS laboratories routinely re-assayed anomalous assays as part of their normal QAQC procedures</td></tr>
<tr><td></td><td>• Discuss any adjustment to assay data.</td><td>• REO assay results were adjusted to convert elemental values to the oxide equivalent for REOs. The stoichiometric conversion factors used are provided below:
<table>
<tr><th>Element</th><th>Oxide</th><th>Element to stoichiometric oxide conversion factor</th></tr>
<tr><td>Ce (Cerium)</td><td>CeO_2</td><td>1.2284</td></tr>
<tr><td>Dy (Dysprosium)</td><td>Dy_2O_3</td><td>1.1477</td></tr>
<tr><td>Er (Erbium)</td><td>Er_2O_3</td><td>1.1435</td></tr>
<tr><td>Eu (Europium)</td><td>Eu_2O_3</td><td>1.1579</td></tr>
<tr><td>Ga (Gallium)</td><td>Ga_2O_3</td><td>1.3442</td></tr>
<tr><td>Gd (Gadolinium)</td><td>Gd_2O_3</td><td>1.1526</td></tr>
<tr><td>Ho (Holmium)</td><td>Ho_2O_3</td><td>1.1455</td></tr>
<tr><td>La (Lanthanum)</td><td>La_2O_3</td><td>1.1728</td></tr>
<tr><td>Lu (Lutetium)</td><td>Lu_2O_3</td><td>1.1371</td></tr>
<tr><td>Nd (Neodymium)</td><td>Nd_2O_3</td><td>1.1664</td></tr>
<tr><td>Pr (Praseodymium)</td><td>Pr_6O_{11}</td><td>1.2082</td></tr>
<tr><td>Sc (Scandium)</td><td>Sc_2O_3</td><td>1.5338</td></tr>
<tr><td>Sm (Samarium)</td><td>Sm_2O_3</td><td>1.1596</td></tr>
<tr><td>Tb (Terbium)</td><td>Tb_4O_7</td><td>1.1762</td></tr>
<tr><td>Tm (Thulium)</td><td>Tm_2O_3</td><td>1.1421</td></tr>
<tr><td>Y (Yttrium)</td><td>Y_2O_3</td><td>1.2699</td></tr>
<tr><td>Yb (Ytterbium)</td><td>Yb_2O_3</td><td>1.1387</td></tr>
</table></td></tr>
<tr><td>Location of data points</td><td>• Accuracy and quality of surveys used to locate drillholes (collar and downhole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</td><td>• 51% of the drillholes were surveyed by RTK/DGPS. The remaining holes were surveyed by handheld GPS with a horizontal accuracy of +/- 5 m. Elevation values (Z) were assigned from the topography surface where no DGPS data was available.
• There were no downhole surveys completed. Drillholes were both vertical (92%) and inclined (8%). The majority of drill intervals (99%) were less than a drill hole depth of 100m.</td></tr>
<tr><td></td><td>• Specification of the grid system used.</td><td>• All coordinates are in GDA94 Zone 50.</td></tr>
<tr><td></td><td>• Quality and adequacy of topographic control.</td><td>• A three second SRTM Digital Elevation Model was used to represent the topographical surface sourced from Geoscience Australia. The topography was adjusted by using the DGPS surveyed collar coordinates to model a more accurate topographical surface. It is recommended that a LiDAR based DEM is used in future.</td></tr>
<tr><td>Data spacing and distribution</td><td>• Data spacing for reporting of Exploration Results.</td><td>• The drillhole spacing at North Stanmore ranges from 50 x 50m to 250 x 100m.</td></tr>
</table>

Criteria	JORC Code explanation	Commentary
	• *Whether the data spacing, and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.*	• Given the nature of the exploration programs, the spacing of the exploration drilling is appropriate for understanding the exploration potential and the identification of structural controls on the mineralisation. In areas of closer spaced drilling the spacing demonstrates grade and geological continuity sufficient to support Indicated Mineral Resources. Where drillhole spacing increases, grade and geological continuity can be implied and has been classified as an Inferred Mineral Resource. Areas where the drillhole spacing is such that grade and geological continuity cannot be implied, have been excluded from the Mineral Resource. • The applied Mineral Resource classification is commensurate with the grade continuity demonstrated.
	• *Whether sample compositing has been applied.*	• Percussion samples were collected as 1.0 m samples. Core was collected at a nominal 1.0 m samples. Air core samples were collected as 1.0 m and 4.0 m samples.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	• Mineralisation is sub horizontal, as such the vertical drillholes are suitable to test mineralisation thickness. • It is concluded from aerial magnetics that the mineralisation trends 010°-030°. • Air core drilling was vertical as the mineralisation is interpreted to be sub parallel to the regolith profile. RC percussion drilling was angled. • Downhole widths of mineralisation are known with percussion drilling methods to +/- 1 metre.
	• *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Mineralisation is sub-horizontal. Azimuths and dips of drilling was designed to intersect the strike of the rocks at right angles.
Sample security	• *The measures taken to ensure sample security.*	• All samples were packaged and managed by VTM personnel. • Larger packages of samples were couriered to Core from Cue by professional transport companies in sealed bulka bags. • Unused samples from the percussion drilling are stored at Victory's secure warehouse in Perth.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• MEC conducted an audit of the project data and the historic MRE in April of 2024. The findings were as follows - ○ Several validation issues have now been corrected in the drillhole database, and the data is of sufficient quality to inform an Indicated and Inferred mineral resource. ○ There are no downhole surveys so there is a risk of the hole paths deviating from planned, particularly with the deeper drillholes >100m which account for less than 1% of all drilled metres.

Criteria	JORC Code explanation	Commentary
		• MEC completed a further review upon the completion of the 2025 drilling which focussed on the adequateness of lithological logging procedures in order to produce accurate bottom of hole (bedrock) lithology map and to qualify the rock hardness to allow a rock model to be generated.

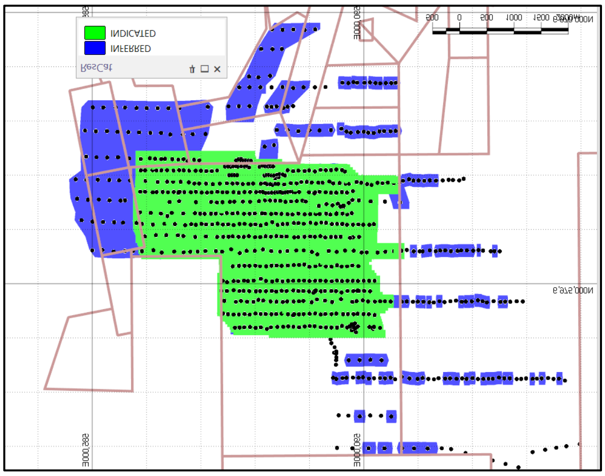
Section 2: Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• The North Stanmore REO Project MRE comprises ten tenements E20/0544, E20/0871, E20/0971, E20/1016, E20/2468, E20/2469, P20/0543, P20/2007, P20/2153, and P20/2403. All tenements are held by Victory Cue Pty Ltd, a wholly owned subsidiary of Victory Metals Ltd. MEC has verified that at the time of the report date that all tenements are currently in good standing. • Native Title claim WC2004/010 (Wajarri Yamatji #1) was registered by the Yaatji Marlpa Aboriginal Corp in 2004 and covers the entire project area, including Coodardy and Emily Wells.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• The area has been previously explored by Harmony Gold (2007-2010) in JV with Big Bell Ops, Mt Kersey (1994- 1996), and Westgold (2011), and Metals X (2013). • Exploration by these companies has been piecemeal and not regionally systematic. • Harmony Gold intersected 3m @ 2.5 g/t Au and 2m @ 8.85 g/t Au in the Mafeking Bore area but did not follow up these intersections. • Other historical drill holes in the area commonly intersected > 100 ppb Au. • There has been no historical exploration for REOs in the tenement.
Geology	• *Deposit type, geological setting and style of mineralisation*	• Victory's tenements lie north of Cue, within the centre of the Murchison Province, which comprises the Archaean gneiss-granitoid-greenstone north-western Yilgarn Block. The Archean greenstone belts in the Murchison Province, the Warda Warra and Dalgaranga greenstone belts, the southern parts of the Meekatharra-Mount Magnet and Weld Range belts are dominated by metamorphosed supracrustal mafic volcanic rocks, as well as sedimentary and intrusive rocks. Thermo-tectonism resulted in development of large-scale fold structures that were subsequently disrupted by late faults. The greenstone belts were intruded by two suites of granitoids. The first, most voluminous suite, comprises granitoids that are recrystallised with foliated margins and massive cores, typically containing large enclaves of gneiss. The second suite consists of relatively small, post tectonic intrusions. • Two large Archaean gabbroid intrusions occur south of Cue. These are the Dalgaranga-Mount Farmer gabbroid complex in the southwest, and the layered Windimurra gabbroid complex in the southeast. The North Stanmore alkaline

Criteria	JORC Code explanation	Commentary
		intrusion, north of Cue, was not recognised on regional geological maps. The petrological and geochemical data indicate that it is post-tectonic and post Archean in age. Similar alkaline intrusions in the vicinity of Cue are interpreted to be related to the early Proterozoic plume track responsible for alkaline magmatism, that extends in a belt from Mt Weld through Leonora to Cue. • Mafic and ultramafic sills are abundant in all areas of the Cue greenstones. Gabbro sills are often differentiated with basal pyroxenite and/or peridotite and upper leucogabbric units. • The greenstones are deformed by large scale fold structures which are dissected by major faults and shear zones which can be mineralised. Two large suites of granitoids intrude the greenstone belts. • The western margin of the project has a signature reflecting a rhyolite, rhyolite-dacite and/or dacitic rock (predominantly acid or felsic rock type). This coincides with an area of elevated TREO/LREO/HREO grades and greater average mineralisation thickness. • The deposit type is regolith-hosted REO mineralisation overlying the North Stanmore alkaline intrusion. The REO mineralisation at North Stanmore is predominantly hosted within a relatively flat-laying saprolite-clay horizon and partially extends into the Sap rock. The Saprolite is covered by 0–36m of unconsolidated colluvium. The saprolite thickness ranges from 14–58m, and overlies a basement of granite, mafic rocks, and other felsic rocks. Mineralogy studies demonstrate that the REOs are mainly hosted by sub-20-µm phases interpreted to be churchite (after xenotime) and rhabdophane (after monazite). The mineralisation is hosted in the saprolite zone of the weathering profile, between the basement granite and surface colluvium.

Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*
	  ○ *easting and northing of the drill hole collar*
	  ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar*
	  ○ *dip and azimuth of the hole*
	  ○ *down hole length and interception depth*
	  ○ *hole length.*
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract*
		• Eight hundred and thirty four (834) drill holes for 45,339.9m, inclusive of 773 Air-core (AC) drillholes for 41,409m, 50 Reverse Circulation (RC) drillholes for 3,166m, and 11 diamond drill holes for 764.9m. Drillhole depths range from 3m to 222m. All drillholes were completed by Victory from 2022 to 2025.
		• Drillhole coordinates are shown in **APPENDIX 2**.
		• Drillhole intersections are reported in **APPENDIX 3**.

Criteria	JORC Code explanation	Commentary
	from the understanding of the report, the Competent Person should clearly explain why this is the case.	
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g., cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• No top cuts were applied as few extreme values were identified. • Samples were composited to 1 m intervals based on the dominant raw sample length. • A geological cutoff grade of 150ppm TREO + Sc representing the on-set of mineralisation was used during interpretation to separate mineralised from unmineralised material for the MIN domain. A high-grade (HGMIN) domain was modelled above a TREO + Sc 600ppm cut-off. • All MRE were reported above an economic cut-off grade of 330ppm TREO + Sc.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	• The clay regolith hosted REO mineralisation is interpreted to be sub horizontal. • 88% of the drillholes are vertical, and the remaining are drilled at a dip of -60˚. As such intersections approximate the true width of mineralised lodes.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views*	• Drillhole collars and tenements are shown below –  2025 Drillhole collar locations are listed in APPENDIX **2**.

Criteria	JORC Code explanation	Commentary
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• All exploration results have been reported above a 150ppm TREO + Sc cut-off.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances*	• Metallurgical testwork: o Three stages of metallurgical test work have been completed on the North Stanmore project, focusing on beneficiation, and on leach test work to establish potential recoveries o Core Resources ("Core") in Brisbane completed Stage 3 test work including beneficiation test work in March of 2024 and reported an increase, to the Rare Earth Element ("REO") feed grade of 63% by rejecting the +53µm feed material from across all samples. Core also completed leach test work on the beneficiated material. o The Leach test work program involved Core conducting diagnostic metallurgical testing on a composite blend of the beneficiated samples which had a head grade of 1,283 ppm Total Rare Earth Oxide plus Yttrium (TREO). This was sourced from 23 samples and 13 drill holes from North Stanmore. The initial atmospheric leach test work program was trialled at elevated temperatures and variable leaching conditions compared to previous work. These test conditions yielded high recoveries of Pr (94%), Nd (94%) and valuable and critical heavy rare earth elements Tb (91%), and Dy (92%) with a combined recovery of 93% Magnet Rare Earth Elements ("MREO"). o Additionally, Scandium oxide (Sc_2O_3) recoveries of (50%) were achieved. These assays were conducted by Australian Laboratory Services (ALS) Brisbane. The objective of the diagnostic test work was to recover REO and Sc_2O_3 from the beneficiated sample using alternative conditions to previous metallurgical programs, that successfully demonstrated increased extractions at higher temperature (from 25°C to 100°C).
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future*	• Further metallurgical testwork will focus on further beneficiation.. Additional variability leach testing of individual samples is also planned. Variability leach testwork will inform geo-metallurgical variability across the North Stanmore project. • Mincore Melbourne have been appointed to conduct a Pre Feasibility Study on the North Stanmore Project

Criteria	JORC Code explanation	Commentary
	drilling areas, provided this information is not commercially sensitive.	

Section 3: Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*	• *An initial Database was supplied to MEC by RSC, the database was then integrated with newly acquired data by MEC for a data audit before commencing an MRE. All validation issues relating to data were identified and remedied prior to MRE.*
	• *Data validation procedures used.*	• *Drillhole collar, downhole survey, assay, geology, and recovery data were imported into Micromine software.* • *The imported data was then compared to the database values with no discrepancies identified.* • *The data was then desurveyed in Micromine and reviewed spatially with no discrepancies identified.*
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*	• *Dean O'Keefe, the Competent Person for this Mineral Resource Estimate visited the North Stanmore project site on May 30, 2024.*
	• *If no site visits have been undertaken indicate why this is the case.*	• *A site visit has been conducted by Dean O'Keefe.*
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.*	• *Confidence in the interpretation of the transported colluvium that truncates the saprolite is commensurate with the drillhole spacing and ranges from low to moderate confidence.* • *The mineralisation is hosted within the saprolite, with some mineralisation extending into the bedrock.* • *There is reasonable confidence in the interpretation of the saprolite commensurate with the available drilling.*
	• *Nature of the data used and of any assumptions made.*	• *Surface AC, RC, as well as diamond drilling, have been used to inform the MRE.*
	• *The effect, if any, of alternative interpretations on Mineral Resource estimation.*	• *The potential for alternate interpretations at a prospect scale is considered unlikely. However, there is a likelihood of variation at the local scale, and this has been reflected in the Mineral Resource classification.*
	• *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	• *The MRE has been interpreted as mineralised domains (MIN) representing the on-set of REO mineralisation at 150ppm TREO + Sc_2O_3, and high-grade pods (HGMIN) within the mineralised domains where the mineralisation grade is greater than 600ppm TREO + Sc_2O_3.*
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• *The North Stanmore deposit extends over 8km across and along strike and is around 70m thick; mineralisation varies between 4m to 60m in true thickness.* • *The southwestern part of the deposit is thicker than the remainder of the deposit.*
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters*	• *The final interpretational wireframes and estimation work was completed using Micromine v2025.5.* • *The estimation was constrained by hard domain boundaries generated from mineralisation wireframes.* • *The available samples were coded by domains (HGMIN, MIN), and 1.0m composites were created honouring these boundaries.*

Criteria	JORC Code explanation	Commentary
	and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.	• *The REO analyte grades were estimated using ordinary kriging of the 1.0m composite grades each of the individual REO grades: HREO, and LREO.* • *The estimation for credit elements was completed using Inverse Distance Cubed for Cu, Ni, Co, Hf, Sc_2O_3, and Ga_2O_3.* • *There were no extreme values observed that required topcuts to be applied.* • *For estimation purposes, all boundaries were treated as hard boundaries.* • *The primary search was 500 m in the direction of maximum continuity, 400 m along the intermediate direction of continuity, and 25 m in the minor direction of continuity. Up to 5 samples per octant sector (maximum number of informing samples was 40 samples) were used.* • *The secondary search was 1,000 m in the direction of maximum continuity, 800 m along the intermediate direction of continuity, and 50 m in the minor direction of continuity, up to 5 samples per octant sector (maximum of 40 informing samples) was used.* • *The third search was 1,500 m in the direction of maximum continuity, 1,200 m along the intermediate direction of continuity, and 75m in the minor direction of continuity, with a maximum of 150 informing samples (no octant search applied).* • *The maximum distance for extrapolation for the Inferred Mineral Resource was 1,500 m.* • *Values were calculated for HREO, LREO, and TREO + Sc by summing the respective REO estimated grades and Scandium oxide for each OBM block.*
	• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*	• *The January 2025 MRE compared to the August 2025 MRE has the same Indicated Mineral Resources tonnage of 176.5Mt, however, the TREOSc ppm grade has increased from 503 to 532 ppm. The January 2025 Inferred Mineral Resources tonnage has increased from 70.9Mt to 144.1Mt for the August 2025 MRE. The Inferred Mineral Resources TREOSc ppm grade has decreased from 561 to 484 ppm. The January 2025 Total Mineral Resources tonnage has increased from 274.5Mt to 320.6Mt for the August 2025 MRE. The Total Mineral Resources TREOSc ppm grade has changed from 520 to 510 ppm.* • *An economic cutoff grade of TREO + Sc ≥330ppm was applied to the MEC August 2025 MRE due to scandium oxide, being a potential credit element along with the presence of hafnium, nickel, cobalt, and copper.* • *The August 2025 MEC Indicated and Inferred Mineral Resource for the North Stanmore Project is estimated at ~321 Mt of REE-bearing saprolite and bedrock at 510 ppm TREO + Sc2O3, for 163,660 tonnes of contained TREO + Sc2O3.*
	• *The assumptions made regarding recovery of by-products.*	• *Test work has demonstrated that Scandium is recoverable and may become a byproduct.* • *Test work has demonstrated that Gallium is recoverable and may become a byproduct.* • *Available metallurgical test work has demonstrated that likely processing will be able to recover significant proportions of Scandium, Gallium, Nickel, Cobalt, Copper and Hafnium.*
	• *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).*	• *Test work completed by Victory Metals included analysis of Uranium (U) and Thorium (Th) levels across the project.* • *The assessed levels of uranium and thorium were very low values across the project. Due to the low values within both ore and waste the uranium and thorium were not estimated,*

Criteria	JORC Code explanation	Commentary
		however, both values may be estimated in the future if required for integration into processing studies. ***Waste*** *U Max = 24ppm, Mean = 1.7ppm* *Th Max = 67ppm, Mean = 7.9ppm* ***MIN Domain (≥150ppm TREO + Sc_2O_3)*** *U Max = 12ppm, Mean = 2.11ppm* *Th Max = 61ppm, Mean = 7.15ppm* ***HGMIN Domain (≥600ppm TREO + Sc_2O_3)*** *U Max = 11ppm, Mean = 1.8ppm* *Th Max = 68ppm, Mean = 6.9ppm* • *Metallurgical recovery to date of deleterious Uranium (U) 2.4ppm and Thorium (Th) 5ppm are less than average abundances in the upper continental crust (U) 3ppm (Th) 10ppm.* • *Scandium oxide, Gallium oxide, Hafnium, Copper, Cobalt, and Nickel were estimated within this MRE and are considered significant.* • *Sulphur (S) has not been analysed by the laboratory and cannot currently be estimated.*
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*	• *Drillhole spacing is consistent and varies in the East and North-East of the deposit. Nominal drillhole spacing is 50 x 50m expanding to ~250 north by 100m east across strike.* • *The block size used for the estimation 50m east x 50m north and 1 mRL, with sub celled blocks to 25m east x 25m north and 0.5mRL.*
	• *Any assumptions behind modelling of selective mining units.*	• *No support correction was applied to allow for selective mining units at this stage of the project life.*
	• *Any assumptions about correlation between variables*	• *No assumptions were made regarding correlations between variables.*
	• *Description of how the geological interpretation was used to control the resource estimates.*	• *A geological cutoff grade of 150ppm was chosen to distinguish the mineralised material from poorly unmineralised material.* • *The mineralised domain MIN was then Interpreted at 150ppm TREO Sc_2O_3 reflecting the on-set of mineralisation.* • *The interpretation was carried out in section lines and a high-grade mineralised domain HGMIN was delineated at 600ppm TREO + Sc_2O_3.*
	• *Discussion of basis for using or not using grade cutting or capping.*	• *Few extreme values were present and no topcuts were applied.*

	• *The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.*	• *The OBM estimate was validated, validation approaches included:*
		  ○ *Visual checks for composite grades versus estimated block grades.*
		  ○ *Comparison of global mean grades of composites versus blocks for each Domain. This check ensures that the global statistics for each estimated variable represent the composited statistics in that domain.*
		  ○ *Histograms of composites versus block distributions to check preservation of the distribution post-estimate.*

Criteria	JORC Code explanation	Commentary
		○ *Swath plots (also known as trend plots) to compare the spatial variation of grades between composites and blocks across the block model.* ○ *On completion of the OBM, checks were conducted for overlapping or missing blocks, and none were found.* • *Primary relevant elements of interest were estimated individually (Dy_2O_3, Er_2O_3, Eu_2O_3, Gd_2O_3, Ho_2O_3, La_2O_3, Lu_2O_3, Nd_2O_3, Pr_6O_{11}, Sm_2O_3, Tb_4O_7, Tm_2O_3, Y_2O_3, Yb_2O_3, Sc_2O_3, Ga_2O_3).*
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• *Tonnages were estimated on a dry basis.*
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• *The MRE was reported at a 330ppm TREO + Sc_2O_3 cutoff grade.* • *The RSC August 2023 MRE economic cut-off grade was ≥400 ppm TREO, inclusive of Yttrium. The economic cut-off grade for the August 2025 MEC MRE was ≥330ppm TREO + Sc_2O_3, inclusive of Yttrium oxide and Scandium oxide. Asra Minerals Limited (ASX: ASR) reported in an ASX Announcement, 16 April 2024, a maiden JORC (2012) Mineral Resource Estimate (MRE) for its 100%-owned Yttria Rare Earth Element (REE) deposit, located on its Mt Stirling Project near Leonora in the northern Goldfields region of Western Australia. The MRE was reported above an economic cut-off grade of 200 ppm TREO, inclusive of Yttrium, minus CeO_2. Asra Minerals Ltd commented that this cut-off grade was selected based on the evaluation of other clay hosted rare earth Mineral Resources.*
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources* • • *not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• *The Competent Person/s deem that there are reasonable prospects for eventual economic extraction using open pit mining methods as a function of:* ○ *The relative shallow depth of the mineralisation and presence of loosely consolidated transported Colluvium above the mineralisation.* ○ *Proximity to significant existing infrastructure (located adjacent to the Gt Northern Highway and the township of Cue).* • *Future pit optimisation studies will confirm the designation of the blocks for RPEEE.*
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider*	• *For a summary of the prior metallurgical testwork refer to Victory Metals Press Releases dated 12th Feb 2024, 5th Dec 2023, 6th Nov 2023, 19th Mar 2024.* • *The objective of the current programme was to produce a mixed rare earth oxide from a representative bulk sample of North Stanmore REE rich clay regolith* • *Leaching was conducted on the composite sample with 4 hour leach time and low temperature.*

Criteria	JORC Code explanation	Commentary
	potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	• *Leaching was carried out in a large baffled glass reactors using an overhead stirrer. The volume of slurry in the test was maintained as constant throughout the test via the addition of DI water to counter volume loss through evaporation. At the conclusion of the test, the slurry was pressure filtered and washed with DI water. Residues were dried overnight in an oven at low temperatures.* • *Assays on feed samples and final residues were conducted at ALS Perth using a combination of ICP-MS and XRF.* • *Combined extractions of REEs Nd, Pr, Dy and Tb were found to be 94%.* • *Extraction of Sc for the composite blend was 50.8% due to incorporation of some Sc in a refractory secondary Zr-bearing mineral in the leach residue* • *Leach of feed solids below 100 degrees Celsius. Slurry filtered with the solids containing Hf, Zr and Sc. Filtrate moved forward for further processing of rare earths.* • *Leachate is neutralized in solution, followed by Fe precipitation and conversion of ferrous to ferric. Slurry filtered with iron solids going to waste and filtrate moves forward for further processing of rare earths.* • *Between 60-70% of Al is precipitated out of solution, while minimizing co-precipitation of rare earths at the appropriate pH. Slurry filtered with Al solids going to waste and filtrate moves forward for further processing of rare earths.* • *Rare earths in solution and remaining Al are precipitated out of solution as a crude MREC solids. Slurry filtered with MREC solids moving forward for further processing and filtrate being recycled.* • *Crude MREC solids are re-leached at the appropriate pH to leach all the rare earths into solution, while rejecting Mn and some Al. Slurry filtered with Al solids going to waste and filtrate moves forward for further processing of rare earths.* • *A clean rare earth solid precipitated out of solution at ambient temperature.* • *The precipitated rare earth phase was then calcined to produce a clean REO product.* • *The composition of the oxide was determined by XRF and ICPMS at ALS.*
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of*	• *The North Stanmore prospect is located in the Murchison of Western Australia, a mining district with considerable mining history and well understood environmental standards and protocols.* • *No environmental assumptions were made for the MRE. Scoping studies will assess these requirements in the future.*

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td>early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</td><td></td></tr>
<tr><td rowspan="3">Bulk density</td><td>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</td><td>Downhole geophysical density is available for 10 diamond drillholes at 10cm depth increments, for a total of 5,896 readings.
Core length, diameter and weight are available for 8 of the diamond drillholes for 50 readings
Regression analysis was performed to compare the two different approaches to measuring density.
A single density value was applied to each geology domain regardless of mineralisation profile. Densities were used to estimate the MRE tonnage.</td></tr>
<tr><td>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.</td><td>Downhole density measurements were obtained from 10 diamond drillholes at 10cm depth increments, for 5,896 readings. No anomalous density readings were observed in the data. Downhole geophysical density measurements were taken in rod, then corrected to account for this, using a factor calculated from a calibration drillhole (DD004).</td></tr>
<tr><td>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</td><td>Core length, diameter and weight are available for 8 of the diamond drillholes for a total of 50 readings. From this information, density was calculated using the formula:
$$Density = \frac{m}{\pi r^2 h}$$
Where “r” is the radius of the PQ core (0.0425m), “h” is the length of the core in metres, and “m” is the mass in kilograms. The density was converted from kg/m3 to g/cm3 for consistency with units used for downhole geophysical density. Four anomalous calculated density values were identified where density <1 g/cm3. Regression analysis was applied to calculate the density from geophysical measurements for the high grade and low-grade domains. The mean density from regression analysis for the High-grade domain is 1.75t/m3, and for the low-grade domain 2.02t/m3.
The following densities have been applied to the MRE.
<table>
<tr><th>Geology domain</th><th>Dry bulk density
(t/m^3)</th></tr>
<tr><td>Colluvium</td><td>1.7</td></tr>
<tr><td>Saprolite (LG & HG)</td><td>1.71</td></tr>
<tr><td>Sap Rock (LG & HG)</td><td>2.18</td></tr>
<tr><td>Slightly Weathered (LG & HG)</td><td>2.2</td></tr>
<tr><td>Basement (LG & HG)</td><td>2.3</td></tr>
</table></td></tr>
<tr><td>Classification</td><td>The basis for the classification of the Mineral</td><td>Mineral Resources were classified as Indicated and Inferred. Material not classified as either indicated or inferred Material remains unclassified and has been reported as an Exploration</td></tr>
</table>

Criteria	JORC Code explanation	Commentary
	Resources into varying confidence categories.	*Target. Indicated Mineral Resource classification was based on drillhole spacing (250 x 100m closing to 50 x 50m in some areas), acceptable underlying QAQC, and RTK/DGPS survey of drillhole collar. The DGPS survey provided increased certainty regarding the drillhole collar location and compensated for a low-resolution topography survey. The topographical surface was adjusted to include the DGPS surveyed drillhole collar coordinates.* • *55% (by tonnage) of the MRE is classified as Indicated Mineral Resources, 45% (by tonnage) is classified as Inferred Mineral Resources.*
	• *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).*	• *Grade and tonnage estimation has been considered for the MRE classification.* • *The Competent Person/s have considered all relevant factors*
	• *Whether the result appropriately reflects the Competent Person's view of the deposit.*	• *The MRE classification of Inferred and Indicated MRE reflects the Competent Persons understanding of the deposit.*
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• *MEC has conducted an internal review of the RSC August 2023 MRE.* • *MEC conducted an audit in May 2025 of the geological logging by reviewing the chip trays. Several drillholes were selected and the chips checked. The audit found that there was strong agreement between the logging and the chip trays. The quality of logging from a limited test program was found to be good.*
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.*	• *No statistical test of the accuracy and confidence in the MRE has been undertaken. The low variability of the mineralisation grades, the relatively consistent mineralisation geometry, the geometry and large areal extent of the mineralisation provide qualitative confidence in the MRE.*
	• *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should*	• *The estimate is considered a good global estimate, and the relative confidence in the underlying data (QAQC), drillhole spacing, geological continuity and interpretation, has been appropriately reflected by the Competent Person/s in the Resource Classification.*

Criteria	JORC Code explanation	Commentary
	include assumptions made and the procedures used.	
	• *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• *There has been no production at the North Stanmore project.*

APPENDIX 2: 2025 Drillhole collar coordinates

HoleID	East	North	RL	Depth	Grid	Azimuth	Dip	HoleType	DateDrilled
AC0001	588308.8	6970311.9	446.9	52.0	MGA94_50	90	-90	AC	Sept 2024
AC0002	588504.4	6970319.8	445.5	48.0	MGA94_50	90	-90	AC	Sept 2024
AC0003	588702.9	6970314.8	445.1	50.0	MGA94_50	90	-90	AC	Sept 2024
AC0004	588910.0	6970310.0	444.8	54.0	MGA94_50	90	-90	AC	Sept 2024
AC0005	589105.2	6970311.5	444.5	43.0	MGA94_50	90	-90	AC	Sept 2024
AC0006	587707.0	6971382.5	441.5	52.0	MGA94_50	90	-90	AC	Sept 2024
AC0007	587896.1	6971379.8	441.5	54.0	MGA94_50	90	-90	AC	Sept 2024
AC0008	588098.4	6971380.2	441.0	50.0	MGA94_50	90	-90	AC	Sept 2024
AC0009	588302.8	6971380.3	441.7	41.0	MGA94_50	90	-90	AC	Sept 2024
AC0010	588504.0	6971376.3	441.2	53.0	MGA94_50	90	-90	AC	Sept 2024
AC0011	588700.3	6971393.8	440.8	55.0	MGA94_50	90	-90	AC	Sept 2024
AC0012	588891.3	6971379.8	440.7	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0013	589101.2	6971379.0	440.7	67.0	MGA94_50	90	-90	AC	Sept 2024
AC0014	589294.6	6971375.6	440.2	26.0	MGA94_50	90	-90	AC	Sept 2024
AC0015	588397.8	6972166.6	438.1	46.0	MGA94_50	90	-90	AC	Sept 2024
AC0016	588597.5	6972171.7	437.9	51.0	MGA94_50	90	-90	AC	Sept 2024
AC0017	588796.3	6972187.7	437.9	43.0	MGA94_50	90	-90	AC	Sept 2024
AC0018	589001.1	6972171.1	438.1	52.0	MGA94_50	90	-90	AC	Sept 2024
AC0019	589185.0	6972175.2	438.3	41.0	MGA94_50	90	-90	AC	Sept 2024
AC0020	589395.9	6972169.7	438.3	48.0	MGA94_50	90	-90	AC	Sept 2024
AC0021	585878.0	6973686.2	428.8	54.0	MGA94_50	90	-90	AC	Sept 2024
AC0022	586077.2	6973695.7	429.2	64.0	MGA94_50	90	-90	AC	Sept 2024
AC0023	586265.3	6973707.8	429.4	60.0	MGA94_50	90	-90	AC	Sept 2024
AC0024	586464.7	6973695.2	429.8	55.0	MGA94_50	90	-90	AC	Sept 2024
AC0025	586676.1	6973705.4	430.2	16.0	MGA94_50	90	-90	AC	Sept 2024
AC0026	585915.9	6973899.7	428.1	46.0	MGA94_50	90	-90	AC	Sept 2024
AC0027	586117.4	6973910.9	428.4	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0028	586330.1	6973897.1	429.0	45.0	MGA94_50	90	-90	AC	Sept 2024
AC0029	586521.0	6973902.4	429.3	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0030	586711.4	6973921.6	429.4	52.0	MGA94_50	90	-90	AC	Sept 2024
AC0031	585967.5	6974128.1	427.1	43.0	MGA94_50	90	-90	AC	Sept 2024
AC0032	586172.6	6974105.3	428.0	49.0	MGA94_50	90	-90	AC	Sept 2024
AC0033	586362.9	6974105.2	428.3	51.0	MGA94_50	90	-90	AC	Sept 2024
AC0034	586578.1	6974107.5	428.6	48.0	MGA94_50	90	-90	AC	Sept 2024
AC0035	585916.3	6974402.3	426.4	14.0	MGA94_50	90	-90	AC	Sept 2024
AC0036	586125.6	6974383.8	427.1	31.0	MGA94_50	90	-90	AC	Sept 2024
AC0037	586280.0	6974426.6	427.1	65.0	MGA94_50	90	-90	AC	Sept 2024
AC0038	589538.7	6977427.4	422.0	19.0	MGA94_50	90	-90	AC	Sept 2024
AC0039	589716.5	6977433.3	421.8	25.0	MGA94_50	90	-90	AC	Sept 2024
AC0040	589926.5	6977446.8	421.8	47.0	MGA94_50	90	-90	AC	Sept 2024
AC0041	590118.4	6977429.9	422.1	74.0	MGA94_50	90	-90	AC	Sept 2024
AC0042	590318.1	6977435.1	422.1	63.0	MGA94_50	90	-90	AC	Sept 2024
AC0043	590506.1	6977447.9	422.0	57.0	MGA94_50	90	-90	AC	Sept 2024
AC0044	588001.0	6978641.5	419.3	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0045	588595.8	6978641.0	419.4	3.0	MGA94_50	90	-90	AC	Sept 2024
AC0046	589469.8	6978632.4	419.6	5.0	MGA94_50	90	-90	AC	Sept 2024
AC0051	588188.0	6979233.8	419.3	51.0	MGA94_50	90	-90	AC	Sept 2024

HoleID	East	North	RL	Depth	Grid	Azimuth	Dip	HoleType	DateDrilled
AC0052	589112.2	6979232.2	419.6	47.0	MGA94_50	90	-90	AC	Sept 2024
AC0053	589424.8	6979227.5	419.8	47.0	MGA94_50	90	-90	AC	Sept 2024
AC0054	589701.6	6979230.6	420.0	48.0	MGA94_50	90	-90	AC	Sept 2024
AC0055	589991.9	6979234.5	420.1	36.0	MGA94_50	90	-90	AC	Sept 2024
AC0056	590288.7	6979241.5	420.3	41.0	MGA94_50	90	-90	AC	Sept 2024
AC0058	587991.8	6979829.7	419.4	66.0	MGA94_50	90	-90	AC	Sept 2024
AC0059	588605.8	6979820.4	419.1	59.0	MGA94_50	90	-90	AC	Sept 2024
AC0060	589422.8	6979831.9	419.9	62.0	MGA94_50	90	-90	AC	Sept 2024
AC0061	589489.9	6981957.0	420.8	5.0	MGA94_50	90	-90	AC	Sept 2024
AC0062	590705.7	6981962.3	420.5	5.0	MGA94_50	90	-90	AC	Sept 2024
AC0063	591304.4	6981949.7	422.6	6.0	MGA94_50	90	-90	AC	Sept 2024
AC0065	590381.3	6982401.3	420.4	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0066	590918.6	6982405.2	420.6	3.0	MGA94_50	90	-90	AC	Sept 2024
AC0067	589499.7	6982866.4	420.7	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0068	590700.0	6982847.1	420.9	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0069	591300.0	6982840.0	422.0	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0070	589386.3	6983320.3	421.1	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0071	589978.3	6983304.4	421.2	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0072	591148.0	6983321.1	421.4	20.0	MGA94_50	90	-90	AC	Sept 2024
AC0073	589685.9	6983770.9	421.8	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0074	590274.5	6983775.4	421.8	5.0	MGA94_50	90	-90	AC	Sept 2024
AC0075	591495.7	6983769.9	421.7	6.0	MGA94_50	90	-90	AC	Sept 2024
AC0076	590287.4	6984234.3	422.3	7.0	MGA94_50	90	-90	AC	Sept 2024
AC0077	590886.9	6984265.2	422.4	6.0	MGA94_50	90	-90	AC	Sept 2024
AC0078	591489.5	6984259.1	422.2	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0079	589994.7	6984778.0	422.8	12.0	MGA94_50	90	-90	AC	Sept 2024
AC0080	590585.4	6984781.5	423.0	6.0	MGA94_50	90	-90	AC	Sept 2024
AC0081	591191.6	6984781.0	423.1	4.0	MGA94_50	90	-90	AC	Sept 2024
AC0082	591700.5	6984785.3	423.0	43.0	MGA94_50	90	-90	AC	Sept 2024
AC0083	590922.7	6984772.5	423.1	29.0	MGA94_50	90	-90	AC	Sept 2024
AC0084	586587.6	6973323.5	431.4	50.0	MGA94_50	90	-90	AC	Sept 2024
AC0085	586609.4	6973307.1	431.4	42.0	MGA94_50	90	-90	AC	Sept 2024
AC0086	589620.9	6973585.4	433.6	58.0	MGA94_50	90	-90	AC	Sept 2024
AC0087	589105.1	6975146.5	428.3	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0088	589630.1	6973563.7	433.7	51.0	MGA94_50	90	-90	AC	Sept 2024
AC0089	589091.7	6973334.4	434.3	45.0	MGA94_50	90	-90	AC	Sept 2024
AC0090	589116.2	6975127.4	428.5	56.0	MGA94_50	90	-90	AC	Sept 2024
AC0091	589103.5	6973315.9	434.4	57.0	MGA94_50	90	-90	AC	Sept 2024
AC0092	588699.5	6975581.5	427.1	81.0	MGA94_50	90	-90	AC	Sept 2024
AC0093	588719.4	6975563.9	427.1	77.0	MGA94_50	90	-90	AC	Sept 2024
AC0094	589882.3	6975129.1	428.6	71.0	MGA94_50	90	-90	AC	Sept 2024
AC0095	590909.3	6984795.7	423.2	24.0	MGA94_50	90	-90	AC	Sept 2024
AC0096	590188.5	6975802.5	426.8	45.0	MGA94_50	90	-90	AC	Sept 2024
AC0097	589910.5	6975133.4	428.5	72.0	MGA94_50	90	-90	AC	Sept 2024
AC0098	589822.1	6975808.7	426.5	41.0	MGA94_50	90	-90	AC	Sept 2024
AC0099	590169.5	6975832.2	426.7	32.0	MGA94_50	90	-90	AC	Sept 2024
AC0100	589803.8	6975768.7	426.6	52.0	MGA94_50	90	-90	AC	Sept 2024

APPENDIX 3: 2025 DRILLHOLE INTERSECTIONS > 330ppm TREO + Sc_2O_3

HoleID	From (m)	To (m)	Interval (m)	TREO ppm	LREO ppm	HREO ppm	MREO ppm	CREO ppm
AC0003	9.0	15.0	6.0	362.3	259.6	102.6	85.8	136.0
AC0004	6.0	12.0	6.0	529.9	364.8	165.1	104.8	188.9
AC0005	13.0	15.0	2.0	471.5	339.7	131.8	114.8	176.9
AC0006	19.0	20.0	1.0	755.2	676.6	78.6	142.1	154.6
AC0006	27.0	30.0	3.0	408.0	287.9	120.2	86.1	146.1
AC0007	14.0	23.0	9.0	520.6	381.5	139.1	98.9	167.1
AC0008	2.0	5.0	3.0	647.1	548.1	99.0	153.0	170.1
AC0008	27.0	28.0	1.0	316.3	212.7	103.6	62.5	116.8
AC0010	22.0	26.0	4.0	725.5	543.7	181.8	156.7	241.5
AC0011	23.0	29.0	6.0	1264.2	892.7	371.5	258.0	448.3
AC0011	44.0	47.0	3.0	534.9	459.9	75.1	132.2	153.0
AC0012	27.0	30.0	3.0	686.7	408.2	278.4	121.4	286.9
AC0015	18.0	25.0	7.0	848.0	637.6	210.4	208.8	296.5
AC0015	26.0	27.0	1.0	326.6	184.5	142.1	73.0	157.1
AC0016	14.0	22.0	8.0	633.4	454.5	179.0	135.6	223.3
AC0017	13.0	21.0	8.0	713.8	488.4	225.5	142.5	268.5
AC0018	10.0	14.0	4.0	417.8	294.7	123.0	67.1	134.0
AC0018	15.0	18.0	3.0	465.6	311.4	154.3	137.1	211.7
AC0019	22.0	27.0	5.0	664.0	501.4	162.6	125.3	202.3
AC0020	18.0	22.0	4.0	556.3	382.4	173.8	123.9	211.2
AC0021	13.0	14.0	1.0	322.3	160.7	161.6	56.2	150.7
AC0021	15.0	38.0	23.0	414.2	229.3	184.9	84.0	189.4
AC0021	43.0	49.0	6.0	389.7	218.9	170.7	80.2	176.8
AC0022	12.0	13.0	1.0	356.9	198.5	158.3	66.9	158.0
AC0022	14.0	17.0	3.0	487.3	326.8	160.6	107.4	189.7
AC0022	19.0	38.0	19.0	535.7	343.6	192.1	124.6	225.6
AC0022	39.0	46.0	7.0	394.0	207.5	186.5	80.2	188.1
AC0022	51.0	52.0	1.0	384.1	203.1	180.9	77.3	183.1
AC0022	54.0	55.0	1.0	413.7	223.0	190.6	84.7	194.8
AC0022	60.0	61.0	1.0	365.9	188.5	177.3	72.7	177.2
AC0022	62.0	63.0	1.0	407.1	240.2	166.9	86.1	179.1
AC0023	10.0	26.0	16.0	441.5	240.2	201.2	91.3	207.9
AC0023	27.0	35.0	8.0	463.0	270.4	192.6	98.3	206.3
AC0023	36.0	37.0	1.0	367.5	151.8	215.7	67.7	201.0
AC0023	38.0	40.0	2.0	344.8	158.3	186.5	66.1	179.4
AC0023	41.0	42.0	1.0	365.4	163.4	202.0	68.9	192.5
AC0023	44.0	46.0	2.0	760.6	538.6	222.0	193.5	295.1
AC0023	47.0	57.0	10.0	380.8	200.4	180.4	77.6	184.0
AC0023	58.0	59.0	1.0	363.5	204.7	158.8	78.2	168.5
AC0024	19.0	30.0	11.0	734.5	583.6	150.9	153.4	216.4
AC0024	31.0	38.0	7.0	474.1	290.1	184.0	118.4	215.6
AC0024	39.0	40.0	1.0	368.8	215.4	153.5	83.1	169.0
AC0024	49.0	53.0	4.0	434.0	226.5	207.5	86.5	205.6
AC0024	54.0	55.0	1.0	369.2	173.0	196.2	69.9	187.0
AC0025	11.0	14.0	3.0	792.1	365.5	426.6	161.1	417.8
AC0026	14.0	15.0	1.0	480.5	322.4	158.1	121.6	202.1
AC0026	21.0	22.0	1.0	317.8	174.6	143.2	67.6	150.6

HoleID	From (m)	To (m)	Interval (m)	La2O3 ppm	CeO2 ppm	Pr6O11 ppm	Nd2O3 ppm	Sm2O3 ppm
AC0003	9.0	15.0	6.0	68.7	105.4	15.7	58.5	11.4
AC0004	6.0	12.0	6.0	72.9	193.2	17.5	67.3	13.9
AC0005	13.0	15.0	2.0	115.4	108.5	21.9	78.3	15.6
AC0006	19.0	20.0	1.0	228.7	301.0	32.1	98.2	16.6
AC0006	27.0	30.0	3.0	77.5	126.4	16.0	55.9	12.1
AC0007	14.0	23.0	9.0	82.5	203.0	17.3	65.5	13.2
AC0008	2.0	5.0	3.0	150.9	240.6	25.8	107.4	23.5
AC0008	27.0	28.0	1.0	45.9	107.2	10.5	40.8	8.3
AC0010	22.0	26.0	4.0	132.7	255.0	29.2	106.9	19.9
AC0011	23.0	29.0	6.0	182.5	457.8	45.8	171.5	35.1
AC0011	44.0	47.0	3.0	103.4	217.0	25.0	99.0	15.3
AC0012	27.0	30.0	3.0	90.2	210.5	18.7	73.4	15.4
AC0015	18.0	25.0	7.0	162.1	264.5	38.3	143.7	29.0
AC0015	26.0	27.0	1.0	65.6	50.4	11.7	47.4	9.5
AC0016	14.0	22.0	8.0	99.7	220.1	24.6	90.7	19.5
AC0017	13.0	21.0	8.0	124.9	224.3	26.2	94.5	18.5
AC0018	10.0	14.0	4.0	43.8	188.6	10.7	42.0	9.6
AC0018	15.0	18.0	3.0	103.4	70.1	24.1	95.9	17.9
AC0019	22.0	27.0	5.0	91.2	287.6	22.7	83.6	16.4
AC0020	18.0	22.0	4.0	84.7	176.0	21.8	82.5	17.5
AC0021	13.0	14.0	1.0	25.1	88.3	7.0	31.3	9.0
AC0021	15.0	38.0	23.0	48.4	103.8	12.7	51.3	13.0
AC0021	43.0	49.0	6.0	46.1	98.6	12.0	49.8	12.4
AC0022	12.0	13.0	1.0	51.8	87.0	10.5	39.0	10.3
AC0022	14.0	17.0	3.0	75.6	145.2	19.3	71.0	15.7
AC0022	19.0	38.0	19.0	81.2	139.9	20.8	83.0	18.7
AC0022	39.0	46.0	7.0	43.9	91.2	11.8	48.6	12.1
AC0022	51.0	52.0	1.0	42.2	91.0	11.7	46.3	11.9
AC0022	54.0	55.0	1.0	46.6	99.7	12.6	50.9	13.3
AC0022	60.0	61.0	1.0	39.5	85.1	10.6	42.6	10.7
AC0022	62.0	63.0	1.0	49.1	109.2	13.3	54.6	14.0
AC0023	10.0	26.0	16.0	52.7	103.5	13.2	56.4	14.3
AC0023	27.0	35.0	8.0	57.6	120.5	14.5	62.4	15.4
AC0023	36.0	37.0	1.0	30.8	66.3	8.9	35.5	10.3
AC0023	38.0	40.0	2.0	31.8	68.6	8.5	38.6	10.8
AC0023	41.0	42.0	1.0	33.3	71.9	9.0	38.8	10.4
AC0023	44.0	46.0	2.0	128.0	215.6	32.2	133.8	29.0
AC0023	47.0	57.0	10.0	43.1	87.6	11.0	47.2	11.5
AC0023	58.0	59.0	1.0	45.5	86.5	11.2	49.7	11.9
AC0024	19.0	30.0	11.0	111.2	316.3	28.9	105.5	21.8
AC0024	31.0	38.0	7.0	86.3	88.3	19.6	77.4	18.4
AC0024	39.0	40.0	1.0	45.0	90.5	12.5	53.1	14.3
AC0024	49.0	53.0	4.0	44.9	103.9	12.8	51.5	13.4
AC0024	54.0	55.0	1.0	35.5	78.7	9.7	39.3	9.7
AC0025	11.0	14.0	3.0	63.9	159.7	21.0	95.3	25.6
AC0026	14.0	15.0	1.0	86.8	114.0	19.9	84.3	17.4
AC0026	21.0	22.0	1.0	37.8	75.1	9.9	41.6	10.2

HoleID	From (m)	To (m)	Interval (m)	Eu2O3 ppm	Gd2O3 ppm	Tb4O7 ppm	Dy2O3 ppm	Ho2O3 ppm
AC0003	9.0	15.0	6.0	3.0	10.7	1.7	10.0	2.0
AC0004	6.0	12.0	6.0	3.8	15.0	2.6	17.4	3.6
AC0005	13.0	15.0	2.0	3.8	14.8	2.3	12.3	2.6
AC0006	19.0	20.0	1.0	3.8	12.9	2.2	9.5	1.8
AC0006	27.0	30.0	3.0	2.7	12.5	2.1	12.1	2.4
AC0007	14.0	23.0	9.0	3.1	13.4	2.3	13.8	3.0
AC0008	2.0	5.0	3.0	6.1	27.1	3.7	16.1	2.3
AC0008	27.0	28.0	1.0	2.1	9.5	1.4	9.7	2.4
AC0010	22.0	26.0	4.0	4.9	19.7	2.8	17.9	3.6
AC0011	23.0	29.0	6.0	8.2	33.2	5.5	35.1	7.5
AC0011	44.0	47.0	3.0	3.7	12.0	1.4	6.7	1.3
AC0012	27.0	30.0	3.0	4.3	19.9	3.7	25.5	5.4
AC0015	18.0	25.0	7.0	6.6	25.5	3.9	22.9	4.3
AC0015	26.0	27.0	1.0	2.6	11.8	1.9	12.1	2.7
AC0016	14.0	22.0	8.0	4.8	18.8	3.0	17.4	3.7
AC0017	13.0	21.0	8.0	4.4	19.5	3.2	18.6	4.2
AC0018	10.0	14.0	4.0	2.4	10.6	1.8	12.6	2.5
AC0018	15.0	18.0	3.0	4.2	16.6	2.5	14.7	2.9
AC0019	22.0	27.0	5.0	4.1	16.8	2.7	16.3	3.4
AC0020	18.0	22.0	4.0	4.3	16.8	2.7	17.0	3.5
AC0021	13.0	14.0	1.0	1.7	12.9	2.3	15.6	3.6
AC0021	15.0	38.0	23.0	3.0	14.8	2.6	17.3	3.8
AC0021	43.0	49.0	6.0	2.8	13.7	2.3	16.0	3.6
AC0022	12.0	13.0	1.0	2.1	12.1	2.3	15.1	3.4
AC0022	14.0	17.0	3.0	3.1	14.3	2.5	14.6	3.3
AC0022	19.0	38.0	19.0	3.5	17.9	2.9	17.8	3.9
AC0022	39.0	46.0	7.0	2.7	14.7	2.6	17.2	3.9
AC0022	51.0	52.0	1.0	2.6	13.8	2.6	16.8	3.6
AC0022	54.0	55.0	1.0	2.8	15.2	2.7	18.6	3.9
AC0022	60.0	61.0	1.0	1.9	13.2	2.5	17.0	3.7
AC0022	62.0	63.0	1.0	1.8	14.5	2.4	15.8	3.4
AC0023	10.0	26.0	16.0	2.8	16.5	2.9	18.7	4.1
AC0023	27.0	35.0	8.0	2.7	16.8	2.9	18.4	4.0
AC0023	36.0	37.0	1.0	2.6	14.6	3.1	20.3	4.5
AC0023	38.0	40.0	2.0	2.4	13.4	2.5	16.4	3.8
AC0023	41.0	42.0	1.0	2.5	14.4	2.8	18.3	4.6
AC0023	44.0	46.0	2.0	5.0	27.7	4.0	23.4	4.6
AC0023	47.0	57.0	10.0	2.2	13.6	2.5	16.9	3.6
AC0023	58.0	59.0	1.0	2.2	12.7	2.2	15.1	3.3
AC0024	19.0	30.0	11.0	3.0	18.5	2.8	16.2	3.0
AC0024	31.0	38.0	7.0	3.5	20.3	3.2	18.2	3.7
AC0024	39.0	40.0	1.0	2.7	14.8	2.4	15.1	3.1
AC0024	49.0	53.0	4.0	1.7	16.0	2.9	19.3	4.4
AC0024	54.0	55.0	1.0	1.0	12.7	2.7	18.2	4.3
AC0025	11.0	14.0	3.0	7.5	34.2	6.0	38.9	8.5
AC0026	14.0	15.0	1.0	3.0	15.0	2.3	15.0	3.3
AC0026	21.0	22.0	1.0	2.0	11.1	2.0	14.0	3.0

HoleID	From (m)	To (m)	Interval (m)	Er2O3 ppm	Tm2O3 ppm	Yb2O3 ppm	Lu2O3 ppm	Y2O3 ppm
AC0003	9.0	15.0	6.0	5.8	0.8	5.1	0.7	62.8
AC0004	6.0	12.0	6.0	11.6	1.6	10.2	1.5	97.8
AC0005	13.0	15.0	2.0	6.8	0.9	7.1	0.9	80.2
AC0006	19.0	20.0	1.0	3.8	0.4	3.1	0.3	40.9
AC0006	27.0	30.0	3.0	6.8	0.9	6.6	0.8	73.3
AC0007	14.0	23.0	9.0	9.0	1.3	9.5	1.2	82.4
AC0008	2.0	5.0	3.0	4.3	0.4	2.0	0.2	36.8
AC0008	27.0	28.0	1.0	6.4	1.1	7.3	1.0	62.7
AC0010	22.0	26.0	4.0	9.9	1.6	10.7	1.6	109.1
AC0011	23.0	29.0	6.0	22.8	3.5	23.9	3.8	227.9
AC0011	44.0	47.0	3.0	3.7	0.5	3.1	0.5	42.2
AC0012	27.0	30.0	3.0	18.2	2.5	16.3	2.7	179.9
AC0015	18.0	25.0	7.0	12.7	1.7	11.7	1.6	119.4
AC0015	26.0	27.0	1.0	8.1	1.1	7.6	1.1	93.2
AC0016	14.0	22.0	8.0	10.9	1.6	10.0	1.4	107.4
AC0017	13.0	21.0	8.0	13.1	1.9	11.1	1.8	147.7
AC0018	10.0	14.0	4.0	8.1	1.1	7.7	1.0	75.3
AC0018	15.0	18.0	3.0	8.9	1.2	7.8	1.1	94.4
AC0019	22.0	27.0	5.0	10.6	1.5	10.3	1.4	95.5
AC0020	18.0	22.0	4.0	11.0	1.7	10.5	1.6	104.8
AC0021	13.0	14.0	1.0	11.4	1.6	11.1	1.5	99.8
AC0021	15.0	38.0	23.0	12.3	1.9	12.3	1.8	115.2
AC0021	43.0	49.0	6.0	11.4	1.8	11.6	1.7	105.8
AC0022	12.0	13.0	1.0	10.1	1.6	10.7	1.4	99.6
AC0022	14.0	17.0	3.0	10.8	1.6	10.3	1.5	98.5
AC0022	19.0	38.0	19.0	12.6	1.7	11.7	1.7	118.3
AC0022	39.0	46.0	7.0	12.6	1.8	12.1	1.9	116.9
AC0022	51.0	52.0	1.0	11.8	1.7	11.7	1.6	114.9
AC0022	54.0	55.0	1.0	12.4	1.6	12.0	1.7	120.0
AC0022	60.0	61.0	1.0	11.6	1.6	11.0	1.7	113.1
AC0022	62.0	63.0	1.0	10.3	1.7	10.7	1.8	104.5
AC0023	10.0	26.0	16.0	12.6	1.8	12.6	2.0	127.1
AC0023	27.0	35.0	8.0	11.9	1.8	12.4	1.8	119.9
AC0023	36.0	37.0	1.0	13.7	1.9	13.3	2.0	139.7
AC0023	38.0	40.0	2.0	11.9	2.0	12.7	1.9	119.5
AC0023	41.0	42.0	1.0	12.7	2.0	12.5	2.1	130.2
AC0023	44.0	46.0	2.0	13.0	2.0	11.7	1.7	128.8
AC0023	47.0	57.0	10.0	11.5	1.8	11.2	1.9	115.2
AC0023	58.0	59.0	1.0	10.8	1.5	10.0	1.7	99.3
AC0024	19.0	30.0	11.0	8.7	1.2	7.4	1.1	88.9
AC0024	31.0	38.0	7.0	10.6	1.4	8.6	1.3	113.2
AC0024	39.0	40.0	1.0	9.1	1.3	8.2	1.1	95.8
AC0024	49.0	53.0	4.0	13.8	2.1	14.9	2.2	130.1
AC0024	54.0	55.0	1.0	13.1	2.1	14.1	2.3	125.8
AC0025	11.0	14.0	3.0	26.9	3.9	26.8	3.9	270.1
AC0026	14.0	15.0	1.0	9.5	1.5	9.4	1.7	97.4
AC0026	21.0	22.0	1.0	8.7	1.3	8.8	1.4	90.9

HoleID	From (m)	To (m)	Interval (m)	Sc2O3 ppm	Th ppm	U ppm	Nb ppm	Ta ppm
AC0003	9.0	15.0	6.0	22.9	7.3	1.6	5.5	0.4
AC0004	6.0	12.0	6.0	21.2	6.2	1.2	4.5	0.4
AC0005	13.0	15.0	2.0	20.1	5.2	1.3	3.8	0.4
AC0006	19.0	20.0	1.0	38.2	10.6	3.6	12.4	0.6
AC0006	27.0	30.0	3.0	27.5	9.5	4.6	7.0	0.6
AC0007	14.0	23.0	9.0	26.3	8.5	3.7	6.6	0.6
AC0008	2.0	5.0	3.0	33.4	12.9	2.0	5.3	0.4
AC0008	27.0	28.0	1.0	22.2	7.5	2.0	5.8	0.4
AC0010	22.0	26.0	4.0	22.1	9.5	2.2	6.2	0.6
AC0011	23.0	29.0	6.0	26.4	8.5	3.9	6.9	0.6
AC0011	44.0	47.0	3.0	29.2	37.6	6.3	11.0	0.6
AC0012	27.0	30.0	3.0	20.1	10.3	2.8	6.4	0.5
AC0015	18.0	25.0	7.0	20.7	6.1	2.7	6.5	0.5
AC0015	26.0	27.0	1.0	20.7	5.2	2.0	4.5	0.4
AC0016	14.0	22.0	8.0	22.4	6.4	1.8	5.2	0.4
AC0017	13.0	21.0	8.0	20.9	4.9	1.4	4.6	0.4
AC0018	10.0	14.0	4.0	21.0	5.0	1.5	4.9	0.4
AC0018	15.0	18.0	3.0	18.4	5.0	1.0	4.5	0.4
AC0019	22.0	27.0	5.0	17.0	10.1	2.6	6.0	0.7
AC0020	18.0	22.0	4.0	22.0	7.4	1.5	6.2	0.5
AC0021	13.0	14.0	1.0	17.2	7.9	3.0	10.1	0.8
AC0021	15.0	38.0	23.0	17.1	8.1	2.8	9.9	0.8
AC0021	43.0	49.0	6.0	17.1	7.5	3.1	9.7	0.8
AC0022	12.0	13.0	1.0	14.0	8.5	1.8	7.9	0.6
AC0022	14.0	17.0	3.0	17.6	10.4	2.2	8.6	0.7
AC0022	19.0	38.0	19.0	16.7	7.6	2.5	8.5	0.6
AC0022	39.0	46.0	7.0	16.9	7.2	2.7	9.0	0.7
AC0022	51.0	52.0	1.0	16.0	6.8	2.0	8.7	0.6
AC0022	54.0	55.0	1.0	14.6	7.1	2.2	8.9	0.7
AC0022	60.0	61.0	1.0	16.4	6.5	1.9	7.9	0.6
AC0022	62.0	63.0	1.0	14.3	6.3	2.1	8.5	0.7
AC0023	10.0	26.0	16.0	17.2	6.3	2.0	8.2	0.6
AC0023	27.0	35.0	8.0	16.8	6.6	2.1	8.2	0.7
AC0023	36.0	37.0	1.0	21.9	6.1	2.2	8.8	0.7
AC0023	38.0	40.0	2.0	17.5	6.1	2.4	8.2	0.7
AC0023	41.0	42.0	1.0	14.4	6.5	2.6	8.2	0.7
AC0023	44.0	46.0	2.0	37.9	10.2	3.4	7.3	0.6
AC0023	47.0	57.0	10.0	18.3	6.4	2.0	9.0	0.7
AC0023	58.0	59.0	1.0	18.4	6.2	1.5	9.0	0.6
AC0024	19.0	30.0	11.0	55.8	10.9	5.9	6.3	0.4
AC0024	31.0	38.0	7.0	59.3	11.5	4.0	6.2	0.4
AC0024	39.0	40.0	1.0	54.0	10.9	3.3	4.8	0.3
AC0024	49.0	53.0	4.0	19.1	12.5	2.7	12.8	0.9
AC0024	54.0	55.0	1.0	7.5	11.8	2.5	12.9	0.9
AC0025	11.0	14.0	3.0	24.0	5.8	3.8	6.8	0.5
AC0026	14.0	15.0	1.0	11.8	5.3	1.7	7.4	0.6
AC0026	21.0	22.0	1.0	13.0	5.5	1.9	8.5	0.7

HoleID	From (m)	To (m)	Zr ppm	Hf ppm	Co ppm	Cu ppm	Ni ppm
AC0003	9.0	15.0	170.0	4.4	11.0	43.7	41.0
AC0004	6.0	12.0	151.0	3.6	18.2	25.8	45.7
AC0005	13.0	15.0	135.0	2.9	41.0	30.0	48.5
AC0006	19.0	20.0	246.0	5.9	1.0	20.0	8.0
AC0006	27.0	30.0	209.0	5.2	20.3	113.3	47.0
AC0007	14.0	23.0	199.0	5.6	25.8	32.6	37.8
AC0008	2.0	5.0	190.0	5.3	5.0	27.7	106.7
AC0008	27.0	28.0	195.0	5.0	11.0	34.0	42.0
AC0010	22.0	26.0	184.0	5.1	41.0	48.3	41.8
AC0011	23.0	29.0	178.0	4.8	14.5	60.3	34.3
AC0011	44.0	47.0	281.0	7.0	35.7	90.0	92.7
AC0012	27.0	30.0	161.0	4.2	17.0	34.7	31.7
AC0015	18.0	25.0	226.0	6.0	14.1	28.0	31.7
AC0015	26.0	27.0	125.0	3.3	37.0	30.0	59.0
AC0016	14.0	22.0	165.0	4.1	24.0	28.3	34.9
AC0017	13.0	21.0	134.0	3.5	21.9	36.6	58.5
AC0018	10.0	14.0	142.0	4.0	24.0	47.3	40.3
AC0018	15.0	18.0	150.0	4.0	31.7	20.0	43.7
AC0019	22.0	27.0	161.0	4.5	14.2	29.8	37.4
AC0020	18.0	22.0	162.0	4.4	29.0	30.3	49.8
AC0021	13.0	14.0	284.0	7.0	15.0	51.0	5.0
AC0021	15.0	38.0	339.0	9.6	4.9	8.5	3.7
AC0021	43.0	49.0	337.0	9.3	5.5	8.5	2.8
AC0022	12.0	13.0	217.0	5.9	1.0	3.0	2.0
AC0022	14.0	17.0	260.0	7.2	0.8	8.0	6.3
AC0022	19.0	38.0	263.0	7.3	4.8	9.0	5.5
AC0022	39.0	46.0	289.0	8.0	4.0	1.0	3.3
AC0022	51.0	52.0	276.0	8.0	2.0	1.0	3.0
AC0022	54.0	55.0	280.0	8.4	3.0	1.0	2.0
AC0022	60.0	61.0	245.0	7.3	1.0	1.0	4.0
AC0022	62.0	63.0	276.0	7.0	1.0	1.0	3.0
AC0023	10.0	26.0	238.0	6.6	5.8	2.9	7.9
AC0023	27.0	35.0	261.0	7.1	2.1	1.1	5.6
AC0023	36.0	37.0	377.0	10.4	2.0	7.0	5.0
AC0023	38.0	40.0	283.0	7.4	3.5	1.3	0.8
AC0023	41.0	42.0	262.0	7.1	3.0	1.0	3.0
AC0023	44.0	46.0	243.0	6.7	13.5	41.5	24.0
AC0023	47.0	57.0	291.0	7.7	4.2	1.6	3.6
AC0023	58.0	59.0	284.0	7.4	2.0	1.0	3.0
AC0024	19.0	30.0	185.0	5.0	30.3	133.1	76.0
AC0024	31.0	38.0	199.0	5.5	40.3	57.6	55.6
AC0024	39.0	40.0	221.0	5.8	31.0	37.0	74.0
AC0024	49.0	53.0	342.0	10.2	12.5	23.3	49.5
AC0024	54.0	55.0	261.0	8.2	1.0	3.0	4.0
AC0025	11.0	14.0	201.0	5.3	5.7	4.7	2.2
AC0026	14.0	15.0	225.0	6.2	5.0	13.0	5.0
AC0026	21.0	22.0	258.0	6.5	4.0	2.0	3.0

HoleID	From (m)	To (m)	Interval (m)	TREO ppm	LREO ppm	HREO ppm	MREO ppm	CREO ppm
AC0026	25.0	27.0	2.0	342.4	189.8	152.6	73.2	160.6
AC0026	36.0	37.0	1.0	314.7	160.3	154.3	63.1	154.0
AC0027	16.0	20.0	4.0	759.4	567.5	191.9	186.4	269.4
AC0027	21.0	38.0	17.0	402.0	223.9	178.1	82.8	185.0
AC0027	40.0	43.0	3.0	367.8	189.7	178.1	72.2	177.1
AC0027	44.0	46.0	2.0	407.6	239.7	167.9	88.1	182.2
AC0027	48.0	49.0	1.0	357.5	212.5	145.0	76.1	156.2
AC0027	50.0	51.0	1.0	422.7	258.2	164.6	91.4	181.0
AC0027	52.0	54.0	2.0	359.0	212.9	146.1	74.8	157.7
AC0028	11.0	21.0	10.0	727.1	481.8	245.3	168.1	292.6
AC0028	23.0	25.0	2.0	332.3	179.8	152.5	70.6	158.0
AC0028	27.0	29.0	2.0	421.3	232.8	188.5	84.1	192.5
AC0028	30.0	34.0	4.0	430.3	256.0	174.3	96.2	189.4
AC0028	35.0	44.0	9.0	570.5	389.6	180.9	128.9	220.6
AC0029	13.0	23.0	10.0	637.5	356.6	280.9	113.5	283.3
AC0029	25.0	31.0	6.0	504.5	281.8	222.6	101.7	231.1
AC0029	32.0	34.0	2.0	367.7	163.9	203.8	68.3	193.5
AC0029	35.0	37.0	2.0	394.5	212.1	182.4	80.0	188.0
AC0029	38.0	41.0	3.0	468.7	301.5	167.3	102.4	190.5
AC0029	44.0	51.0	7.0	511.8	317.0	194.7	110.2	214.9
AC0029	52.0	56.0	4.0	342.1	148.9	193.2	61.2	181.6
AC0030	21.0	28.0	7.0	704.2	290.6	413.6	132.0	395.9
AC0030	30.0	36.0	6.0	346.4	178.9	167.4	66.3	167.3
AC0030	38.0	39.0	1.0	383.2	190.5	192.7	68.7	187.6
AC0031	10.0	11.0	1.0	340.7	180.2	160.5	71.2	166.8
AC0031	17.0	19.0	2.0	351.0	182.5	168.5	71.9	169.9
AC0031	29.0	30.0	1.0	370.7	218.9	151.8	79.6	165.4
AC0031	34.0	41.0	7.0	343.0	168.3	174.7	70.8	174.4
AC0032	18.0	28.0	10.0	453.7	285.8	167.9	101.0	190.3
AC0032	47.0	48.0	1.0	336.9	177.8	159.2	66.8	159.4
AC0033	16.0	44.0	28.0	408.0	228.6	179.5	84.9	187.3
AC0033	45.0	47.0	2.0	349.6	169.8	179.8	68.3	175.7
AC0034	18.0	20.0	2.0	398.2	252.9	145.3	78.7	157.0
AC0034	21.0	26.0	5.0	456.6	309.9	146.7	109.0	181.0
AC0034	27.0	28.0	1.0	485.3	309.6	175.6	102.0	197.0
AC0034	31.0	33.0	2.0	394.9	234.4	160.5	83.2	173.2
AC0034	34.0	35.0	1.0	417.0	260.6	156.4	93.4	177.0
AC0036	18.0	19.0	1.0	321.7	140.9	180.8	47.5	160.9
AC0036	20.0	29.0	9.0	444.2	267.2	177.1	93.5	191.9
AC0037	14.0	15.0	1.0	340.2	179.7	160.4	63.7	158.5
AC0037	25.0	27.0	2.0	348.2	201.4	146.8	53.7	136.8
AC0037	29.0	30.0	1.0	445.6	283.5	162.1	105.2	184.9
AC0037	31.0	32.0	1.0	468.4	264.0	204.4	98.7	211.8
AC0037	36.0	37.0	1.0	938.9	561.6	377.3	201.4	416.7
AC0037	38.0	41.0	3.0	372.7	198.6	174.1	78.2	175.6
AC0037	42.0	44.0	2.0	422.5	260.6	161.9	98.4	179.8
AC0037	49.0	50.0	1.0	380.7	223.7	156.9	83.8	170.6

HoleID	From (m)	To (m)	Interval (m)	La2O3 ppm	CeO2 ppm	Pr6O11 ppm	Nd2O3 ppm	Sm2O3 ppm
AC0026	25.0	27.0	2.0	39.1	83.5	10.4	45.6	11.1
AC0026	36.0	37.0	1.0	33.7	70.0	8.7	37.9	10.0
AC0027	16.0	20.0	4.0	122.0	251.1	34.4	130.7	29.2
AC0027	21.0	38.0	17.0	49.1	98.5	12.8	50.9	12.6
AC0027	40.0	43.0	3.0	39.2	85.3	10.5	43.0	11.6
AC0027	44.0	46.0	2.0	48.3	107.1	13.9	56.3	14.1
AC0027	48.0	49.0	1.0	45.4	95.6	11.9	47.7	11.9
AC0027	50.0	51.0	1.0	54.7	116.5	14.7	57.9	14.6
AC0027	52.0	54.0	2.0	43.0	98.6	11.8	48.2	11.3
AC0028	11.0	21.0	10.0	114.1	202.3	27.6	111.9	26.0
AC0028	23.0	25.0	2.0	39.5	74.6	10.3	44.4	11.0
AC0028	27.0	29.0	2.0	53.1	103.7	12.5	51.2	12.3
AC0028	30.0	34.0	4.0	54.1	109.4	14.6	61.8	16.2
AC0028	35.0	44.0	9.0	80.1	181.9	22.2	86.7	18.7
AC0029	13.0	23.0	10.0	64.3	190.5	17.5	68.2	16.1
AC0029	25.0	31.0	6.0	68.8	120.1	15.8	62.7	14.4
AC0029	32.0	34.0	2.0	33.0	73.0	9.3	39.0	9.7
AC0029	35.0	37.0	2.0	44.2	94.8	12.0	49.5	11.7
AC0029	38.0	41.0	3.0	64.5	137.9	17.0	66.8	15.3
AC0029	44.0	51.0	7.0	69.1	142.8	18.1	70.4	16.6
AC0029	52.0	56.0	4.0	29.0	68.8	8.4	33.6	9.1
AC0030	21.0	28.0	7.0	64.4	115.0	17.1	74.4	19.6
AC0030	30.0	36.0	6.0	38.7	80.5	9.9	39.9	10.0
AC0030	38.0	39.0	1.0	42.2	87.2	10.1	40.2	10.7
AC0031	10.0	11.0	1.0	36.0	78.7	10.0	44.3	11.2
AC0031	17.0	19.0	2.0	34.5	83.6	9.8	43.1	11.5
AC0031	29.0	30.0	1.0	49.0	94.0	11.9	51.3	12.6
AC0031	34.0	41.0	7.0	33.1	71.9	9.7	42.3	11.3
AC0032	18.0	28.0	10.0	63.9	124.2	16.7	65.6	15.4
AC0032	47.0	48.0	1.0	36.5	81.7	10.2	39.5	9.9
AC0033	16.0	44.0	28.0	48.6	101.6	12.9	52.5	13.0
AC0033	45.0	47.0	2.0	34.5	75.6	9.5	39.8	10.4
AC0034	18.0	20.0	2.0	46.7	131.5	13.4	49.7	11.5
AC0034	21.0	26.0	5.0	74.3	127.5	19.3	72.8	16.0
AC0034	27.0	28.0	1.0	72.1	140.0	17.5	64.6	15.4
AC0034	31.0	33.0	2.0	50.6	106.0	13.1	52.6	12.1
AC0034	34.0	35.0	1.0	55.0	116.2	14.6	60.9	14.0
AC0036	18.0	19.0	1.0	17.4	89.1	5.2	22.6	6.6
AC0036	20.0	29.0	9.0	56.5	122.4	15.0	59.1	14.1
AC0037	14.0	15.0	1.0	40.1	82.7	10.3	36.5	10.2
AC0037	25.0	27.0	2.0	65.6	91.0	8.0	29.1	7.7
AC0037	29.0	30.0	1.0	66.6	116.0	16.6	69.2	15.1
AC0037	31.0	32.0	1.0	58.1	117.7	14.7	58.9	14.7
AC0037	36.0	37.0	1.0	137.8	234.0	31.7	128.3	29.8
AC0037	38.0	41.0	3.0	42.6	87.3	11.1	46.8	10.9
AC0037	42.0	44.0	2.0	56.6	109.3	15.1	62.6	16.9
AC0037	49.0	50.0	1.0	48.4	97.2	12.6	52.6	12.9

HoleID	From (m)	To (m)	Interval (m)	Eu2O3 ppm	Gd2O3 ppm	Tb4O7 ppm	Dy2O3 ppm	Ho2O3 ppm
AC0026	25.0	27.0	2.0	2.0	12.4	2.3	14.8	3.3
AC0026	36.0	37.0	1.0	2.0	11.8	2.3	14.2	3.2
AC0027	16.0	20.0	4.0	5.0	21.5	3.1	18.2	3.8
AC0027	21.0	38.0	17.0	2.6	13.7	2.5	16.6	3.7
AC0027	40.0	43.0	3.0	2.6	13.2	2.5	16.2	3.9
AC0027	44.0	46.0	2.0	2.6	14.3	2.4	15.4	3.6
AC0027	48.0	49.0	1.0	1.7	12.6	2.3	14.2	3.3
AC0027	50.0	51.0	1.0	2.4	14.6	2.6	16.2	3.4
AC0027	52.0	54.0	2.0	2.0	11.9	2.1	12.7	3.0
AC0028	11.0	21.0	10.0	5.1	26.5	4.1	24.5	5.0
AC0028	23.0	25.0	2.0	2.8	13.7	2.2	13.7	3.1
AC0028	27.0	29.0	2.0	2.9	15.0	2.7	17.7	4.1
AC0028	30.0	34.0	4.0	3.5	17.2	2.9	17.0	3.6
AC0028	35.0	44.0	9.0	3.5	18.3	2.8	17.2	3.7
AC0029	13.0	23.0	10.0	2.0	19.6	3.6	24.2	5.5
AC0029	25.0	31.0	6.0	1.7	17.6	3.1	20.1	4.4
AC0029	32.0	34.0	2.0	1.0	12.5	2.4	17.6	4.1
AC0029	35.0	37.0	2.0	1.4	13.5	2.5	16.1	3.6
AC0029	38.0	41.0	3.0	1.2	15.9	2.6	16.0	3.4
AC0029	44.0	51.0	7.0	1.7	17.5	3.1	18.6	4.0
AC0029	52.0	56.0	4.0	0.8	12.8	2.6	16.6	4.1
AC0030	21.0	28.0	7.0	5.2	29.2	5.3	35.2	8.4
AC0030	30.0	36.0	6.0	1.7	12.2	2.1	14.5	3.2
AC0030	38.0	39.0	1.0	1.3	12.2	2.3	16.1	3.6
AC0031	10.0	11.0	1.0	2.1	11.6	2.1	14.7	3.4
AC0031	17.0	19.0	2.0	2.4	13.5	2.6	16.5	3.5
AC0031	29.0	30.0	1.0	2.6	13.4	2.1	14.2	3.1
AC0031	34.0	41.0	7.0	2.7	13.3	2.4	16.5	3.7
AC0032	18.0	28.0	10.0	2.9	15.2	2.5	16.2	3.4
AC0032	47.0	48.0	1.0	2.0	12.0	2.4	14.7	3.3
AC0033	16.0	44.0	28.0	2.7	14.0	2.5	17.0	3.7
AC0033	45.0	47.0	2.0	1.7	12.1	2.4	16.6	3.8
AC0034	18.0	20.0	2.0	1.4	11.0	2.0	13.5	3.2
AC0034	21.0	26.0	5.0	2.0	13.9	2.4	14.5	3.1
AC0034	27.0	28.0	1.0	2.1	16.0	3.0	16.9	3.6
AC0034	31.0	33.0	2.0	1.5	13.3	2.5	15.0	3.6
AC0034	34.0	35.0	1.0	1.7	14.8	2.5	15.6	3.2
AC0036	18.0	19.0	1.0	1.6	10.0	2.3	17.4	3.8
AC0036	20.0	29.0	9.0	3.0	14.4	2.6	16.8	3.6
AC0037	14.0	15.0	1.0	2.1	12.0	2.0	14.9	3.6
AC0037	25.0	27.0	2.0	1.8	9.6	1.8	14.8	3.0
AC0037	29.0	30.0	1.0	3.5	17.2	2.5	16.9	3.4
AC0037	31.0	32.0	1.0	2.8	16.1	3.0	22.1	4.2
AC0037	36.0	37.0	1.0	6.4	36.1	5.8	35.6	7.4
AC0037	38.0	41.0	3.0	2.7	14.6	2.4	18.0	3.5
AC0037	42.0	44.0	2.0	3.3	18.7	2.9	17.8	3.3
AC0037	49.0	50.0	1.0	3.0	15.6	2.6	16.0	3.4

HoleID	From (m)	To (m)	Interval (m)	Er2O3 ppm	Tm2O3 ppm	Yb2O3 ppm	Lu2O3 ppm	Y2O3 ppm
AC0026	25.0	27.0	2.0	9.8	1.5	9.1	1.5	95.9
AC0026	36.0	37.0	1.0	10.4	1.6	9.8	1.5	97.7
AC0027	16.0	20.0	4.0	12.2	1.8	12.1	1.8	112.4
AC0027	21.0	38.0	17.0	11.7	1.7	11.5	1.7	112.5
AC0027	40.0	43.0	3.0	12.1	1.7	11.4	1.8	112.7
AC0027	44.0	46.0	2.0	10.6	1.6	10.2	1.6	105.5
AC0027	48.0	49.0	1.0	8.7	1.3	9.1	1.5	90.3
AC0027	50.0	51.0	1.0	10.3	1.5	9.8	1.7	102.0
AC0027	52.0	54.0	2.0	9.4	1.3	9.5	1.4	92.8
AC0028	11.0	21.0	10.0	14.8	2.0	14.2	2.0	147.1
AC0028	23.0	25.0	2.0	9.5	1.4	9.6	1.5	94.9
AC0028	27.0	29.0	2.0	12.1	1.8	12.2	2.0	118.0
AC0028	30.0	34.0	4.0	11.0	1.6	11.5	1.8	104.3
AC0028	35.0	44.0	9.0	11.0	1.6	10.7	1.7	110.4
AC0029	13.0	23.0	10.0	18.1	2.5	17.5	2.7	185.3
AC0029	25.0	31.0	6.0	14.1	2.0	13.9	2.2	143.6
AC0029	32.0	34.0	2.0	13.9	2.0	14.5	2.2	133.5
AC0029	35.0	37.0	2.0	11.6	1.6	11.7	1.8	118.6
AC0029	38.0	41.0	3.0	10.7	1.5	10.3	1.6	103.8
AC0029	44.0	51.0	7.0	12.6	1.8	12.5	1.8	121.1
AC0029	52.0	56.0	4.0	12.2	1.9	12.4	1.8	127.9
AC0030	21.0	28.0	7.0	25.5	3.6	22.2	3.2	275.7
AC0030	30.0	36.0	6.0	10.8	1.6	10.5	1.7	109.2
AC0030	38.0	39.0	1.0	12.9	1.9	12.9	1.9	127.6
AC0031	10.0	11.0	1.0	9.7	1.6	10.2	1.6	103.5
AC0031	17.0	19.0	2.0	10.6	1.6	10.8	1.6	105.4
AC0031	29.0	30.0	1.0	8.9	1.5	9.3	1.6	95.1
AC0031	34.0	41.0	7.0	10.8	1.7	11.3	1.7	110.5
AC0032	18.0	28.0	10.0	10.8	1.6	10.5	1.6	103.0
AC0032	47.0	48.0	1.0	10.7	1.5	10.1	1.8	100.7
AC0033	16.0	44.0	28.0	11.8	1.8	11.7	1.8	112.5
AC0033	45.0	47.0	2.0	12.1	1.8	12.4	1.8	115.1
AC0034	18.0	20.0	2.0	9.9	1.7	10.7	1.6	90.4
AC0034	21.0	26.0	5.0	9.4	1.4	9.4	1.4	89.3
AC0034	27.0	28.0	1.0	11.5	1.6	9.2	1.3	110.5
AC0034	31.0	33.0	2.0	10.5	1.5	9.6	1.5	101.6
AC0034	34.0	35.0	1.0	10.1	1.5	9.4	1.5	96.4
AC0036	18.0	19.0	1.0	12.4	1.8	12.8	1.8	117.1
AC0036	20.0	29.0	9.0	11.5	1.7	11.4	1.7	110.4
AC0037	14.0	15.0	1.0	10.3	1.6	9.4	1.6	103.0
AC0037	25.0	27.0	2.0	10.4	1.8	12.2	2.0	89.3
AC0037	29.0	30.0	1.0	10.7	1.6	11.6	1.7	92.8
AC0037	31.0	32.0	1.0	12.7	2.3	14.1	2.2	125.0
AC0037	36.0	37.0	1.0	21.7	3.0	18.1	2.5	240.6
AC0037	38.0	41.0	3.0	11.6	1.8	12.0	1.8	105.8
AC0037	42.0	44.0	2.0	9.8	1.4	10.0	1.5	93.3
AC0037	49.0	50.0	1.0	8.8	1.3	8.5	1.3	96.5

HoleID	From (m)	To (m)	Interval (m)	Sc2O3 ppm	Th ppm	U ppm	Nb ppm	Ta ppm
AC0026	25.0	27.0	2.0	16.0	5.6	1.6	10.0	0.7
AC0026	36.0	37.0	1.0	16.6	7.0	2.5	9.7	0.8
AC0027	16.0	20.0	4.0	20.4	7.4	3.6	9.1	0.7
AC0027	21.0	38.0	17.0	18.2	7.4	2.8	9.5	0.7
AC0027	40.0	43.0	3.0	14.9	8.0	2.6	10.4	0.8
AC0027	44.0	46.0	2.0	13.9	7.1	2.2	9.1	0.7
AC0027	48.0	49.0	1.0	12.0	5.0	1.5	8.3	0.6
AC0027	50.0	51.0	1.0	12.1	5.8	1.8	8.6	0.6
AC0027	52.0	54.0	2.0	11.1	5.6	1.6	8.7	0.7
AC0028	11.0	21.0	10.0	19.4	7.1	1.7	8.5	0.6
AC0028	23.0	25.0	2.0	17.5	6.9	1.7	8.8	0.7
AC0028	27.0	29.0	2.0	15.2	7.0	1.8	8.5	0.6
AC0028	30.0	34.0	4.0	18.8	7.6	2.0	8.9	0.7
AC0028	35.0	44.0	9.0	20.8	8.2	2.8	10.1	0.7
AC0029	13.0	23.0	10.0	14.9	14.3	2.0	14.1	1.0
AC0029	25.0	31.0	6.0	15.5	14.5	1.9	14.3	1.0
AC0029	32.0	34.0	2.0	14.9	13.3	2.7	13.4	1.1
AC0029	35.0	37.0	2.0	11.7	11.8	1.7	12.0	0.9
AC0029	38.0	41.0	3.0	11.7	14.4	1.7	11.4	0.9
AC0029	44.0	51.0	7.0	10.0	10.6	1.8	11.0	0.8
AC0029	52.0	56.0	4.0	8.5	8.2	1.5	11.3	0.8
AC0030	21.0	28.0	7.0	17.5	9.2	1.5	9.8	0.7
AC0030	30.0	36.0	6.0	13.7	9.6	1.6	10.8	0.8
AC0030	38.0	39.0	1.0	8.9	10.4	1.7	10.0	0.8
AC0031	10.0	11.0	1.0	19.3	9.3	3.0	9.5	0.6
AC0031	17.0	19.0	2.0	16.8	6.6	2.3	8.9	0.6
AC0031	29.0	30.0	1.0	14.0	5.9	1.5	8.4	0.6
AC0031	34.0	41.0	7.0	16.1	7.4	3.0	9.5	0.7
AC0032	18.0	28.0	10.0	14.4	8.7	1.8	8.7	0.7
AC0032	47.0	48.0	1.0	15.2	6.6	2.4	9.3	0.6
AC0033	16.0	44.0	28.0	20.8	9.0	2.0	9.9	0.7
AC0033	45.0	47.0	2.0	16.3	6.5	1.6	9.5	0.7
AC0034	18.0	20.0	2.0	15.0	13.0	2.2	12.2	1.1
AC0034	21.0	26.0	5.0	11.7	15.0	1.7	11.9	1.0
AC0034	27.0	28.0	1.0	12.9	12.1	1.9	9.6	0.9
AC0034	31.0	33.0	2.0	10.2	10.6	2.3	9.9	0.9
AC0034	34.0	35.0	1.0	8.6	10.3	2.0	10.7	0.8
AC0036	18.0	19.0	1.0	22.2	11.2	2.4	10.3	0.7
AC0036	20.0	29.0	9.0	16.4	7.5	2.7	9.0	0.6
AC0037	14.0	15.0	1.0	10.9	8.8	1.3	9.4	0.6
AC0037	25.0	27.0	2.0	18.8	10.4	1.6	10.7	0.7
AC0037	29.0	30.0	1.0	19.6	10.3	1.5	10.5	0.8
AC0037	31.0	32.0	1.0	20.2	10.3	2.1	10.5	0.7
AC0037	36.0	37.0	1.0	16.1	10.7	2.1	12.9	0.8
AC0037	38.0	41.0	3.0	20.2	8.7	1.5	10.1	0.7
AC0037	42.0	44.0	2.0	16.6	9.8	1.9	10.9	0.8
AC0037	49.0	50.0	1.0	12.6	8.0	2.0	10.4	0.7

HoleID	From (m)	To (m)	Zr ppm	Hf ppm	Co ppm	Cu ppm	Ni ppm
AC0026	25.0	27.0	227.0	6.4	6.0	1.0	2.0
AC0026	36.0	37.0	285.0	8.4	4.0	7.0	1.0
AC0027	16.0	20.0	340.0	8.6	3.0	63.8	12.5
AC0027	21.0	38.0	300.0	8.1	4.8	26.2	7.4
AC0027	40.0	43.0	326.0	9.0	2.3	6.3	2.7
AC0027	44.0	46.0	280.0	7.5	2.0	2.5	3.5
AC0027	48.0	49.0	199.0	5.4	2.0	1.0	2.0
AC0027	50.0	51.0	232.0	6.8	2.0	1.0	3.0
AC0027	52.0	54.0	247.0	6.6	1.0	1.5	2.0
AC0028	11.0	21.0	256.0	7.1	6.4	8.0	10.1
AC0028	23.0	25.0	271.0	6.5	4.0	16.5	3.0
AC0028	27.0	29.0	299.0	7.5	2.5	19.5	3.5
AC0028	30.0	34.0	291.0	8.3	2.3	12.0	2.5
AC0028	35.0	44.0	283.0	7.0	10.6	17.0	25.3
AC0029	13.0	23.0	306.0	9.6	6.9	10.9	13.1
AC0029	25.0	31.0	340.0	10.7	3.5	4.8	14.2
AC0029	32.0	34.0	373.0	12.0	2.0	3.0	5.5
AC0029	35.0	37.0	259.0	8.7	3.5	5.5	20.0
AC0029	38.0	41.0	262.0	8.8	5.3	4.3	12.0
AC0029	44.0	51.0	265.0	7.8	2.7	2.4	7.9
AC0029	52.0	56.0	251.0	6.9	1.5	1.8	8.3
AC0030	21.0	28.0	290.0	7.8	3.3	6.4	9.4
AC0030	30.0	36.0	248.0	7.3	5.3	2.2	10.8
AC0030	38.0	39.0	299.0	9.2	14.0	3.0	30.0
AC0031	10.0	11.0	290.0	7.5	5.0	20.0	7.0
AC0031	17.0	19.0	229.0	6.4	2.5	12.5	3.5
AC0031	29.0	30.0	230.0	6.3	1.0	0.5	0.5
AC0031	34.0	41.0	316.0	8.7	1.7	9.0	1.1
AC0032	18.0	28.0	280.0	7.7	3.3	21.5	3.6
AC0032	47.0	48.0	262.0	7.2	4.0	4.0	2.0
AC0033	16.0	44.0	309.0	8.9	2.3	5.4	3.9
AC0033	45.0	47.0	276.0	7.7	1.0	2.0	0.8
AC0034	18.0	20.0	335.0	8.9	3.5	39.5	9.5
AC0034	21.0	26.0	305.0	8.8	2.4	9.4	3.2
AC0034	27.0	28.0	245.0	6.9	10.0	16.0	9.0
AC0034	31.0	33.0	297.0	8.0	7.0	74.5	12.5
AC0034	34.0	35.0	275.0	7.5	3.0	36.0	3.0
AC0036	18.0	19.0	407.0	10.2	1.0	43.0	3.0
AC0036	20.0	29.0	314.0	8.1	2.7	28.6	3.1
AC0037	14.0	15.0	233.0	6.0	2.0	4.0	4.0
AC0037	25.0	27.0	404.0	12.1	3.5	60.5	6.5
AC0037	29.0	30.0	382.0	11.2	1.0	26.0	3.0
AC0037	31.0	32.0	427.0	12.1	3.0	58.0	3.0
AC0037	36.0	37.0	361.0	10.0	2.0	8.0	1.0
AC0037	38.0	41.0	365.0	10.4	2.3	1.7	2.0
AC0037	42.0	44.0	431.0	11.4	2.0	2.5	2.0
AC0037	49.0	50.0	358.0	9.2	3.0	3.0	0.5

HoleID	From (m)	To (m)	Interval (m)	TREO ppm	LREO ppm	HREO ppm	MREO ppm	CREO ppm
AC0037	51.0	53.0	2.0	468.0	289.1	178.9	106.1	201.1
AC0037	54.0	57.0	3.0	412.8	239.6	173.2	86.9	184.0
AC0037	58.0	61.0	3.0	438.7	259.8	178.8	91.1	190.3
AC0040	30.0	40.0	10.0	640.7	266.4	374.3	137.8	376.4
AC0043	42.0	43.0	1.0	2425.6	2037.4	388.2	777.4	839.3
AC0043	44.0	51.0	7.0	876.7	641.4	235.4	225.1	332.1
AC0082	26.0	27.0	1.0	437.8	230.4	207.4	99.0	216.8
AC0082	33.0	40.0	7.0	471.6	284.9	186.6	96.6	194.1
AC0083	21.0	27.0	6.0	651.0	234.5	416.5	126.1	392.1
AC0084	9.0	26.0	17.0	693.5	347.4	346.1	136.6	348.5
AC0084	36.0	38.0	2.0	341.4	183.8	157.6	67.5	160.3
AC0085	11.0	16.0	5.0	685.5	280.1	405.4	139.8	393.2
AC0086	32.0	33.0	1.0	552.6	441.2	111.4	144.8	179.2
AC0086	36.0	38.0	2.0	593.9	327.9	266.0	117.2	278.8
AC0087	45.0	56.0	11.0	1077.4	731.8	345.7	170.5	375.0
AC0088	31.0	37.0	6.0	1196.6	746.5	450.1	258.5	516.9
AC0089	26.0	29.0	3.0	1714.4	1290.9	423.5	513.9	671.7
AC0089	30.0	35.0	5.0	572.6	353.3	219.3	99.1	226.0
AC0090	51.0	52.0	1.0	326.6	260.3	66.3	121.0	133.5
AC0091	23.0	25.0	2.0	482.9	384.0	98.9	100.4	141.0
AC0091	31.0	38.0	7.0	902.1	658.4	243.7	200.3	313.7
AC0092	55.0	59.0	4.0	297.1	185.0	112.1	73.1	127.8
AC0092	75.0	77.0	2.0	999.1	338.3	660.8	226.6	644.9
AC0093	57.0	58.0	1.0	312.0	208.5	103.5	85.0	122.7
AC0093	59.0	60.0	1.0	338.4	220.5	117.9	81.7	125.5
AC0093	61.0	75.0	14.0	484.5	182.5	302.0	104.6	289.7
AC0094	43.0	52.0	9.0	920.8	616.7	304.2	218.6	368.5
AC0095	21.0	24.0	3.0	492.8	178.8	314.0	102.0	297.6
AC0096	29.0	35.0	6.0	1048.0	707.7	340.4	239.6	412.7
AC0097	38.0	48.0	10.0	1437.9	711.4	726.6	333.8	776.7
AC0097	49.0	50.0	1.0	332.9	187.7	145.2	59.3	155.9
AC0098	26.0	29.0	3.0	739.4	527.5	211.9	198.4	290.9
AC0098	33.0	36.0	3.0	434.2	195.9	238.3	85.8	240.8
AC0099	22.0	26.0	4.0	698.9	394.8	304.1	173.3	337.9
AC0100	20.0	23.0	3.0	1561.9	1445.1	116.7	424.2	384.4
AC0100	28.0	35.0	7.0	785.1	486.3	298.7	179.3	338.4

HoleID	From (m)	To (m)	Interval (m)	La2O3 ppm	CeO2 ppm	Pr6O11 ppm	Nd2O3 ppm	Sm2O3 ppm
AC0037	51.0	53.0	2.0	59.3	128.1	15.8	68.8	17.2
AC0037	54.0	57.0	3.0	51.2	106.1	13.3	55.0	14.0
AC0037	58.0	61.0	3.0	57.7	116.7	13.9	57.3	14.2
AC0040	30.0	40.0	10.0	82.2	61.5	19.6	82.5	20.5
AC0043	42.0	43.0	1.0	557.1	648.6	152.2	570.4	109.1
AC0043	44.0	51.0	7.0	137.9	274.3	39.5	157.4	32.3
AC0082	26.0	27.0	1.0	56.5	82.1	15.6	61.1	15.1
AC0082	33.0	40.0	7.0	41.9	152.2	13.2	60.6	17.1
AC0083	21.0	27.0	6.0	34.7	95.6	14.1	69.5	20.7
AC0084	9.0	26.0	17.0	76.1	148.6	19.9	82.3	20.5
AC0084	36.0	38.0	2.0	38.1	84.4	10.2	41.1	10.1
AC0085	11.0	16.0	5.0	45.3	113.2	16.9	81.6	23.1
AC0086	32.0	33.0	1.0	98.6	194.1	26.8	101.7	19.9
AC0086	36.0	38.0	2.0	101.2	120.9	17.9	73.0	15.0
AC0087	45.0	56.0	11.0	100.5	470.4	27.4	108.7	24.8
AC0088	31.0	37.0	6.0	166.1	330.9	42.7	170.5	36.3
AC0089	26.0	29.0	3.0	354.2	404.1	95.6	365.5	71.5
AC0089	30.0	35.0	5.0	64.9	198.9	15.2	60.6	13.7
AC0090	51.0	52.0	1.0	80.6	52.0	22.7	89.0	16.2
AC0091	23.0	25.0	2.0	73.8	207.6	19.4	69.0	14.2
AC0091	31.0	38.0	7.0	131.7	328.0	36.5	134.7	27.5
AC0092	55.0	59.0	4.0	43.7	72.1	11.8	47.6	9.9
AC0092	75.0	77.0	2.0	123.7	23.4	32.3	124.5	34.4
AC0093	57.0	58.0	1.0	33.4	92.3	13.8	55.3	13.8
AC0093	59.0	60.0	1.0	35.9	106.4	13.2	49.9	15.1
AC0093	61.0	75.0	14.0	54.3	40.0	14.5	58.0	15.8
AC0094	43.0	52.0	9.0	143.2	260.1	38.0	144.9	30.4
AC0095	21.0	24.0	3.0	22.9	70.1	10.7	57.5	17.7
AC0096	29.0	35.0	6.0	127.6	346.0	40.5	159.1	34.5
AC0097	38.0	48.0	10.0	223.0	182.9	52.7	206.8	46.1
AC0097	49.0	50.0	1.0	56.2	75.2	9.6	38.0	8.7
AC0098	26.0	29.0	3.0	91.6	234.8	32.4	137.8	30.9
AC0098	33.0	36.0	3.0	44.6	74.0	11.5	53.0	12.9
AC0099	22.0	26.0	4.0	63.7	166.1	23.8	113.5	27.8
AC0100	20.0	23.0	3.0	444.3	551.6	94.7	307.5	47.1
AC0100	28.0	35.0	7.0	83.2	232.1	25.6	118.4	27.0

HoleID	From (m)	To (m)	Interval (m)	Eu2O3 ppm	Gd2O3 ppm	Tb4O7 ppm	Dy2O3 ppm	Ho2O3 ppm
AC0037	51.0	53.0	2.0	3.7	18.9	3.0	18.6	3.8
AC0037	54.0	57.0	3.0	3.0	14.7	2.4	16.1	3.4
AC0037	58.0	61.0	3.0	2.3	15.9	2.6	17.3	3.7
AC0040	30.0	40.0	10.0	6.1	27.6	4.7	30.9	6.9
AC0043	42.0	43.0	1.0	23.6	69.7	9.5	45.3	7.7
AC0043	44.0	51.0	7.0	8.1	27.5	4.1	24.1	4.6
AC0082	26.0	27.0	1.0	5.2	19.1	3.2	19.1	4.3
AC0082	33.0	40.0	7.0	6.4	20.5	3.4	19.5	4.2
AC0083	21.0	27.0	6.0	11.2	30.2	5.4	37.1	8.1
AC0084	9.0	26.0	17.0	5.9	24.8	4.3	30.1	6.5
AC0084	36.0	38.0	2.0	1.6	11.5	2.1	14.2	3.0
AC0085	11.0	16.0	5.0	7.7	31.5	5.3	36.1	7.8
AC0086	32.0	33.0	1.0	5.4	18.4	2.4	13.8	2.5
AC0086	36.0	38.0	2.0	4.5	19.1	3.4	22.9	4.9
AC0087	45.0	56.0	11.0	7.6	27.5	4.5	29.9	6.5
AC0088	31.0	37.0	6.0	10.2	39.6	6.3	39.0	8.8
AC0089	26.0	29.0	3.0	15.5	59.8	8.4	44.5	8.3
AC0089	30.0	35.0	5.0	3.6	16.7	3.0	20.4	4.6
AC0090	51.0	52.0	1.0	3.9	11.4	1.6	7.8	1.4
AC0091	23.0	25.0	2.0	3.0	10.5	1.7	10.3	2.0
AC0091	31.0	38.0	7.0	6.5	24.9	4.0	25.0	5.3
AC0092	55.0	59.0	4.0	2.5	10.9	1.9	11.8	2.6
AC0092	75.0	77.0	2.0	9.9	47.2	8.4	61.4	12.9
AC0093	57.0	58.0	1.0	3.3	11.7	2.1	13.8	2.9
AC0093	59.0	60.0	1.0	3.6	12.3	2.4	16.2	3.2
AC0093	61.0	75.0	14.0	4.6	22.9	4.0	28.2	6.3
AC0094	43.0	52.0	9.0	10.3	31.0	4.9	30.8	6.2
AC0095	21.0	24.0	3.0	10.3	24.5	4.4	29.5	6.1
AC0096	29.0	35.0	6.0	10.0	33.9	5.5	34.5	7.2
AC0097	38.0	48.0	10.0	14.2	56.5	9.7	64.7	13.8
AC0097	49.0	50.0	1.0	2.4	10.9	1.5	10.1	2.3
AC0098	26.0	29.0	3.0	7.7	27.2	4.2	24.0	4.5
AC0098	33.0	36.0	3.0	4.2	18.9	2.9	18.4	4.3
AC0099	22.0	26.0	4.0	8.4	31.1	5.1	30.9	6.6
AC0100	20.0	23.0	3.0	8.4	25.7	3.7	18.2	2.7
AC0100	28.0	35.0	7.0	5.5	28.4	4.7	30.6	6.4

HoleID	From (m)	To (m)	Interval (m)	Er2O3 ppm	Tm2O3 ppm	Yb2O3 ppm	Lu2O3 ppm	Y2O3 ppm
AC0037	51.0	53.0	2.0	10.6	1.6	10.0	1.6	107.1
AC0037	54.0	57.0	3.0	10.9	1.6	11.8	1.7	107.5
AC0037	58.0	61.0	3.0	11.4	1.6	11.5	1.8	110.8
AC0040	30.0	40.0	10.0	21.5	2.8	19.1	2.6	252.1
AC0043	42.0	43.0	1.0	20.5	2.6	16.8	2.0	190.5
AC0043	44.0	51.0	7.0	13.4	1.8	11.7	1.6	138.3
AC0082	26.0	27.0	1.0	12.6	1.8	11.9	1.9	128.3
AC0082	33.0	40.0	7.0	12.2	1.9	12.4	1.9	104.3
AC0083	21.0	27.0	6.0	25.8	3.4	22.7	3.7	268.9
AC0084	9.0	26.0	17.0	21.4	3.2	20.8	3.2	225.9
AC0084	36.0	38.0	2.0	10.1	1.5	10.6	1.5	101.4
AC0085	11.0	16.0	5.0	25.1	3.5	22.3	3.6	262.5
AC0086	32.0	33.0	1.0	6.5	0.9	4.9	0.7	55.9
AC0086	36.0	38.0	2.0	17.1	2.2	14.6	2.3	174.9
AC0087	45.0	56.0	11.0	20.5	3.0	19.1	2.7	224.4
AC0088	31.0	37.0	6.0	26.2	3.6	22.0	3.5	290.9
AC0089	26.0	29.0	3.0	22.7	3.3	20.3	2.9	237.9
AC0089	30.0	35.0	5.0	14.1	2.1	14.3	2.2	138.5
AC0090	51.0	52.0	1.0	3.9	0.5	4.0	0.5	31.2
AC0091	23.0	25.0	2.0	6.2	0.8	6.5	0.9	57.0
AC0091	31.0	38.0	7.0	15.4	2.2	14.8	2.1	143.5
AC0092	55.0	59.0	4.0	7.8	1.2	8.2	1.3	64.0
AC0092	75.0	77.0	2.0	38.0	5.2	32.5	4.8	440.7
AC0093	57.0	58.0	1.0	8.8	1.3	9.8	1.6	48.3
AC0093	59.0	60.0	1.0	10.3	1.9	12.9	1.8	53.5
AC0093	61.0	75.0	14.0	19.1	2.8	16.5	2.7	194.9
AC0094	43.0	52.0	9.0	19.2	2.9	18.8	2.6	177.5
AC0095	21.0	24.0	3.0	18.9	2.7	18.6	3.0	196.0
AC0096	29.0	35.0	6.0	21.0	2.9	19.0	2.7	203.6
AC0097	38.0	48.0	10.0	41.6	5.6	34.2	5.0	481.4
AC0097	49.0	50.0	1.0	6.7	0.9	5.7	0.9	103.9
AC0098	26.0	29.0	3.0	12.6	1.7	11.2	1.6	117.2
AC0098	33.0	36.0	3.0	12.8	1.7	11.0	1.7	162.3
AC0099	22.0	26.0	4.0	19.1	2.8	17.4	2.6	180.1
AC0100	20.0	23.0	3.0	5.9	0.7	4.3	0.6	46.5
AC0100	28.0	35.0	7.0	19.0	2.9	19.1	2.9	179.2

HoleID	From (m)	To (m)	Interval (m)	Sc2O3 ppm	Th ppm	U ppm	Nb ppm	Ta ppm
AC0037	51.0	53.0	2.0	17.9	7.8	2.2	10.3	0.7
AC0037	54.0	57.0	3.0	13.1	7.0	1.8	9.4	0.7
AC0037	58.0	61.0	3.0	11.5	6.6	2.2	8.9	0.7
AC0040	30.0	40.0	10.0	42.0	0.8	0.6	1.2	0.1
AC0043	42.0	43.0	1.0	37.7	5.6	3.1	6.3	0.4
AC0043	44.0	51.0	7.0	19.9	5.7	2.2	5.9	0.4
AC0082	26.0	27.0	1.0	13.7	6.2	2.4	7.6	0.8
AC0082	33.0	40.0	7.0	25.5	7.7	3.5	9.6	0.7
AC0083	21.0	27.0	6.0	70.6	1.3	2.2	9.2	0.5
AC0084	9.0	26.0	17.0	25.2	6.1	3.1	8.3	0.5
AC0084	36.0	38.0	2.0	10.6	9.7	2.0	9.7	0.7
AC0085	11.0	16.0	5.0	35.1	5.4	2.6	7.1	0.5
AC0086	32.0	33.0	1.0	38.7	4.4	2.9	4.7	0.4
AC0086	36.0	38.0	2.0	22.7	11.5	2.7	9.1	0.6
AC0087	45.0	56.0	11.0	55.0	2.4	1.5	4.2	0.3
AC0088	31.0	37.0	6.0	28.1	4.8	2.2	5.1	0.2
AC0089	26.0	29.0	3.0	22.9	6.9	2.3	7.0	0.4
AC0089	30.0	35.0	5.0	15.1	5.0	1.9	5.3	0.3
AC0090	51.0	52.0	1.0	21.9	2.3	1.1	5.3	0.3
AC0091	23.0	25.0	2.0	40.9	11.1	2.2	6.8	0.5
AC0091	31.0	38.0	7.0	17.9	5.5	2.2	5.5	0.3
AC0092	55.0	59.0	4.0	65.8	6.0	1.8	4.9	0.4
AC0092	75.0	77.0	2.0	54.2	4.0	1.5	2.6	0.3
AC0093	57.0	58.0	1.0	45.4	9.4	1.8	6.6	0.5
AC0093	59.0	60.0	1.0	52.1	7.4	2.5	7.4	0.5
AC0093	61.0	75.0	14.0	48.8	10.5	1.8	5.4	0.6
AC0094	43.0	52.0	9.0	20.9	5.4	1.6	6.7	0.4
AC0095	21.0	24.0	3.0	61.5	1.5	1.2	7.0	0.4
AC0096	29.0	35.0	6.0	21.0	5.8	3.0	7.1	0.5
AC0097	38.0	48.0	10.0	37.2	6.8	1.7	6.0	0.5
AC0097	49.0	50.0	1.0	21.9	6.4	1.1	7.6	0.5
AC0098	26.0	29.0	3.0	18.7	3.7	3.8	7.4	0.4
AC0098	33.0	36.0	3.0	15.2	3.3	1.4	7.5	0.4
AC0099	22.0	26.0	4.0	18.2	5.9	1.3	7.4	0.5
AC0100	20.0	23.0	3.0	51.3	5.4	3.0	7.3	0.5
AC0100	28.0	35.0	7.0	17.9	13.1	4.1	9.2	0.6

HoleID	From (m)	To (m)	Zr ppm	Hf ppm	Co ppm	Cu ppm	Ni ppm
AC0037	51.0	53.0	344.0	8.6	3.0	1.0	3.0
AC0037	54.0	57.0	292.0	7.7	2.0	7.3	7.7
AC0037	58.0	61.0	253.0	6.7	1.7	9.3	4.7
AC0040	30.0	40.0	36.0	1.1	204.2	97.2	389.9
AC0043	42.0	43.0	225.0	5.2	7.0	31.0	21.0
AC0043	44.0	51.0	195.0	4.7	12.0	28.0	17.1
AC0082	26.0	27.0	216.0	5.0	5.0	32.0	21.0
AC0082	33.0	40.0	311.0	8.0	89.4	59.9	57.1
AC0083	21.0	27.0	455.0	8.9	31.8	25.2	12.8
AC0084	9.0	26.0	262.0	6.8	9.8	9.7	7.1
AC0084	36.0	38.0	219.0	6.7	3.0	4.0	4.0
AC0085	11.0	16.0	191.0	5.3	21.4	8.4	4.8
AC0086	32.0	33.0	134.0	3.5	5.0	43.0	22.0
AC0086	36.0	38.0	215.0	6.0	38.0	50.5	32.0
AC0087	45.0	56.0	140.0	3.5	123.6	114.8	37.5
AC0088	31.0	37.0	197.0	4.8	5.7	26.0	14.3
AC0089	26.0	29.0	237.0	5.8	16.7	54.7	32.3
AC0089	30.0	35.0	168.0	4.3	32.0	36.4	25.6
AC0090	51.0	52.0	226.0	4.9	8.0	33.0	16.0
AC0091	23.0	25.0	279.0	7.3	3.5	40.0	22.5
AC0091	31.0	38.0	189.0	4.6	27.1	29.7	30.4
AC0092	55.0	59.0	124.0	3.6	76.8	100.3	48.3
AC0092	75.0	77.0	67.0	2.0	67.0	121.5	145.0
AC0093	57.0	58.0	257.0	7.4	17.0	69.0	18.0
AC0093	59.0	60.0	208.0	5.7	27.0	89.0	31.0
AC0093	61.0	75.0	100.0	3.1	44.2	92.2	45.0
AC0094	43.0	52.0	242.0	6.0	9.6	55.0	55.4
AC0095	21.0	24.0	417.0	8.7	30.7	18.3	5.7
AC0096	29.0	35.0	239.0	5.4	8.7	24.5	15.3
AC0097	38.0	48.0	202.0	4.5	7.1	53.6	42.7
AC0097	49.0	50.0	264.0	5.8	11.0	19.0	31.0
AC0098	26.0	29.0	237.0	5.5	20.3	22.3	17.0
AC0098	33.0	36.0	271.0	5.8	32.0	14.7	8.7
AC0099	22.0	26.0	231.0	5.3	12.8	18.5	14.5
AC0100	20.0	23.0	260.0	6.4	5.0	20.0	34.7
AC0100	28.0	35.0	351.0	9.9	13.7	28.9	15.4