ASX ANNOUNCEMENT

12 September 2025

ANNUAL MINERAL RESOURCE AND ORE RESERVE STATEMENT

- **Mineral Resources:**
  - **Total Mineral Resource estimate is 26.8 Mt @ 2.4 g/t for 2.11 Moz, an increase of 160 koz after mining 108 koz from 1 June 2024, including:**
    - Riverina Underground Resource increased 25% to 7.0 Mt at 2.6 g/t for 586 koz, up from 468 koz after mining 92 koz from 1 June 2024.
    - Sand King Underground Resource increased 14% to 3.9 Mt at 2.8 g/t for 348 koz, up from 306 koz after mining 17 koz.
- **Ore Reserves:**
  - **Total Ore Reserve estimate increased 24% to 3.0 Mt at 2.4 g/t for 236 koz. Underground Ore Reserves increased 24% to 1.66 Mt at 3.3 g/t for 176 koz, up from 142 koz after mining 108 koz from 1 June 2024 including:**
    - Sand King Underground Ore Reserve increased 54% to 829 kt at 3.2 g/t for 84 koz, up from 55 koz after mining 17 koz.
    - Riverina Underground Ore Reserve increased 5% to 825 kt at 3.5 g/t for 92 koz, up from 87 koz after mining 92 koz from 1 June 2024.
  - **Cut-off grades for Underground Ore Reserve are based on a A$2,500/oz[1] gold price to ensure focus remains on conversion of higher margin ounces.**
- **The Resource and Reserve estimates do not include recent drilling results from Little Gem, Waihi, Round Dam and step-out extensions of Sand King. These are expected to be updated in H2 FY26 as part of the FY26 drill program of 329km ($73 million) allocated to exploration and resource development drilling compared to 64km drilled in FY25 (Figure 1).**

Table 1 - Combined Davyhurst Gold Project Mineral Resource estimate, as at 1 July 2025 [2]

MINERAL RESOURCE ESTIMATE	MEASURED		INDICATED		INFERRED		TOTAL MATERIAL		
	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000 oz.)
Total Project	900	1.4	16,900	2.3	9,100	2.6	26,800	2.4	2,110

Table 2 - Combined Davyhurst Gold Project Ore Reserve Estimate, as at 1 July 2025

ORE RESERVE ESTIMATE	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
Mining Project	105	4.3	14	1,857	3.1	185	1,961	3.2	200
Low Grade & Stockpiles	752	1.0	25	299	1.2	11	1,051	1.1	36
TOTAL	**857**	**1.4**	**39**	**2,156**	**2.8**	**196**	**3,013**	**2.4**	**236**

[1] Sand King and Riverina Underground Ore Reserves are based on A$2,500/oz. Waihi open pit Ore Reserve are based on A$2,400/oz; Underground low grade and stockpile Ore Reserves are based on A$4,400/oz and Waihi Low grade A$3,400/oz.

[2] Inclusive of Ore Reserve

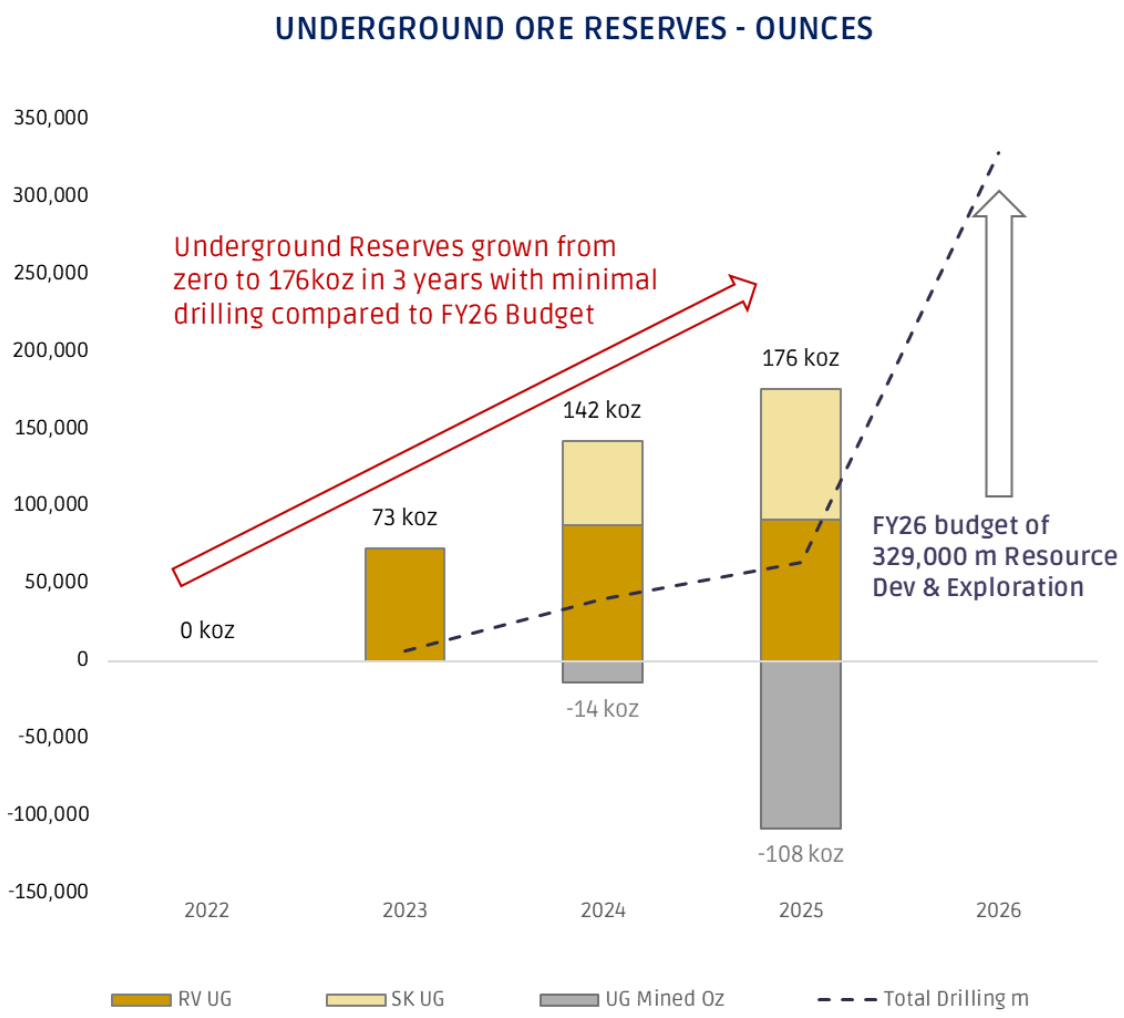

Figure 1 - ORE ounce growth & drilling[3]

Ora Banda's Managing Director, Luke Creagh commented:

"The rapidly improving underground Resources and Reserves after depletion is testament to the continuity and quality of the Riverina and Sand King underground mines, both of which remain open at depth and laterally.

"Riverina and Sand King underground drill platforms are currently being developed, which puts us in a position to drill significant extensional programs to extend and convert mineralisation at both mines in FY26.

"The most exciting element to this Resource and Reserve growth story is that the recent successful programs announced at Waihi, Round Dam and Little Gem have not been included in this announcement. However, the Company will provide an update on these deposits upon the completion of meaningful follow-up drilling as part of our $73 million Exploration and Res Dev drilling program in FY26"

[3] 2023-2025 are actual Resource Development drill metres & 2026 are planned/budgeted FY26 drill metres. Resource Development & Exploration drilling, not including Grade Control drilling. UG mined ounces are all reconciled ounces mined from underground mines, including outside of ORE designs.

This announcement was authorised for release to the ASX by the Ora Banda Board of Directors. For further information about Ora Banda and its projects please visit the Company's website at www.orabandamining.com.au.

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Table 3 - Davyhurst Gold Project Mineral Resource Estimates for deposits with Ore Reserves

DEPOSIT	MEASURED		INDICATED		INFERRED		TOTAL MATERIAL		
	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000oz.)
RIVERINA									
Open Pit	476	1.7	2,118	1.6	117	1.5	2,711	1.6	138
Underground	266	3.3	3,953	2.7	2,826	2.4	7,046	2.6	586
SUB TOTAL	**742**	**2.3**	**6,071**	**2.3**	**2,943**	**2.4**	**9,757**	**2.3**	**724**
SAND KING									
Open Pit	-	-	-	-	-	-	-	-	-
Underground	108	3.2	1,900	2.7	1,901	2.9	3,909	2.8	348
SUB TOTAL	**108**	**3.2**	**1,900**	**2.7**	**1,901**	**2.9**	**3,909**	**2.8**	**348**
WAIHI									
Open Pit	-	-	2,057	2.3	95	2.0	2,152	2.3	157
Underground	-	-	278	3.6	324	3.5	602	3.5	68
SUB TOTAL	**-**	**-**	**2,335**	**2.5**	**419**	**3.5**	**2,754**	**2.5**	**225**
TOTAL	**900**	**2.2**	**10,300**	**2.4**	**5,300**	**2.6**	**16,400**	**2.5**	**1,300**

Notes:

1. *This Mineral Resource estimate comprises 3 individual projects.*
2. *This Mineral Resource estimate is inclusive of in-situ Ore Reserves and is exclusive of surface stockpiles*
3. *The values in the above table have been rounded.*
4. *Further details on the makeup and preparation of this Mineral Resource can be found in the body of this report.*
5. *Refer to "Other Mineral Resource Estimates" section of this report for the full MRE statement*

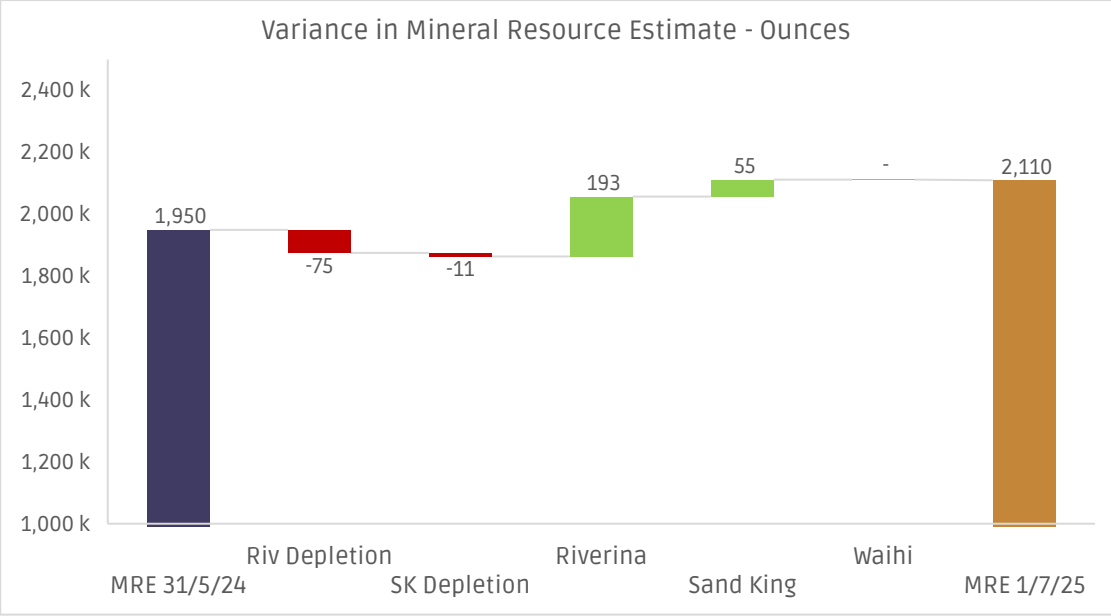

Figure 2 - Change to company MRE ounces 31/5/24 to 1/7/25

Table 4 – Davyhurst Gold Project Ore Reserve by deposit, as at 1 July 2025

AREA	PROJECT	PROVED			PROBABLE			TOTAL		
		('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
Riverina	Riverina Underground	53	4.7	8	773	3.4	84	825	3.5	92
Siberia	Sand King Underground	52	3.9	7	777	3.1	78	829	3.2	84
	Sub-Total	**105**	**4.3**	**14**	**1,550**	**3.2**	**161**	**1,655**	**3.3**	**176**
Davyhurst	Waihi Open Pit				307	2.4	24	307	2.4	24
Low Grade	All mines				299	1.2	11	299	1.2	11
Stockpiles	Davy / Sib / Riv	752	1.0	25				752	1.0	25
	Sub-Total	**752**	**1.0**	**25**	**606**	**1.8**	**35**	**1,358**	**1.4**	**60**
TOTAL		**857**	**1.4**	**39**	**2,156**	**2.8**	**196**	**3,013**	**2.4**	**236**

Notes:

1. *The table contains rounding adjustments to reflect accuracy and may not total exactly.*
2. *This Ore Reserve was estimated from practical mining envelopes and the application of modifying factors for mining dilution and ore loss.*
3. *For the underground mine Ore Reserve, dilution skins were applied to the Mineral Resource estimate. Dilution was included at the background grade estimated into each model. The Riverina dilution is estimated to average 57% while Sand King is estimated to average 32%, reflecting mining shapes and orebody widths appropriate for each deposit.*
4. *At Riverina overall recovery is estimated to be 85%.: The rib and sill pillars equate to 88% mining recovery with both development and stoping activities. Consistent with reconciled performance, an additional 5% stope ore loss was also included for operational losses. At Sand King overall recovery is estimated to be 84%: Sill pillars have been considered via a stope recovery of 72% where stoping extends more than 4 levels down dip on a mineralised lode. A 5% stope ore loss was also included for operational losses*
5. *The underground mine Ore Reserve was estimated using a cut-off grade of 2.4 g/t Au for Riverina and 2.5 g/t Au for Sand King, based on a gold price of A$2,500/oz, stopes were further spatially optimised. Costs used in the cut-off grade calculation allow for ore transport, processing, site & corporate overheads and royalties as well as process recovery specific to the location. Process recoveries range for the project were estimated to be 87% or above, based on recent metallurgical test work.*
6. *For the open pit Ore Reserve, dilution skins were applied to the undiluted Mineral Resource estimate. The method also included internal and edge dilution resulting from forming practical mineable shapes. Dilution was incorporated in the model at the background grades estimated into the model: The average grade of dilution for Waihi was 0.16 g/t Au. The estimated average dilution at Waihi was estimated to be 27%. Ore loss was incurred in the Auto Stope Designer (ASD) Deswik™ process due to variation between mineralised lode geometry and practical dig block geometry. In addition, a nominal 5% loss was applied for further mining losses occurring through normal operations.*
7. *The Waihi open pit Ore Reserve was primarily estimated using a cut-off grade of 1.2 g/t Au based on a gold price of A$2,400/oz. Low Grade Ore Reserve was based on A$3,400/oz for a cut-off grade of 0.8 g/t. Costs used in the cut-off grade calculation allow for ore transport, processing, site overheads and selling costs as well as a weight average recovery of 90% for oxide, transition and fresh. The mining and disposal of existing in-pit tailings were also considered and allowed for.*
8. *The Inferred Mineral Resource within the mining envelope was considered as waste when defining limits of these envelopes; however, minor amount of Inferred material was included within the Riverina Underground and Sand King Underground mine plan due to practical mining geometries and orebody characteristics. Inferred material within total Underground Mine Ore Reserve equates to 50,000t at a grade of 2.4 g/t Au. This material is included at the edges of the mining envelope and equate to 2.2% of the underground mine Ore Reserve inventories.*
9. *The Ore Reserve is inclusive of surface stockpiles above cut-off. Cut-off grade for stockpiles was 0.7 g/t Au based on A$4,400/oz. All surface stockpiles were classified as Proved.*
10. *All low grade material is in situ.*
11. *Costs were derived from the FY26 budget estimate including underground contract pricing current at the date of this Ore Reserve and budget level contract pricing for Waihi. Unit costs for haulage, processing and site overheads were estimated based on scheduled process plant throughput of ORE material.*

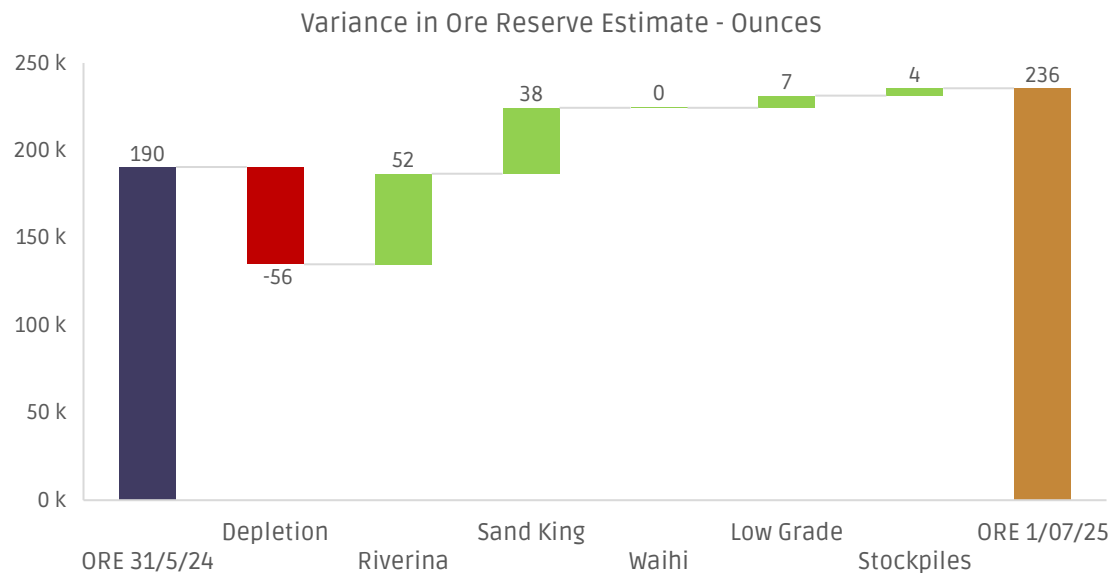

Figure 3 - Change to company ORE ounces 31/5/24 to 1/7/25

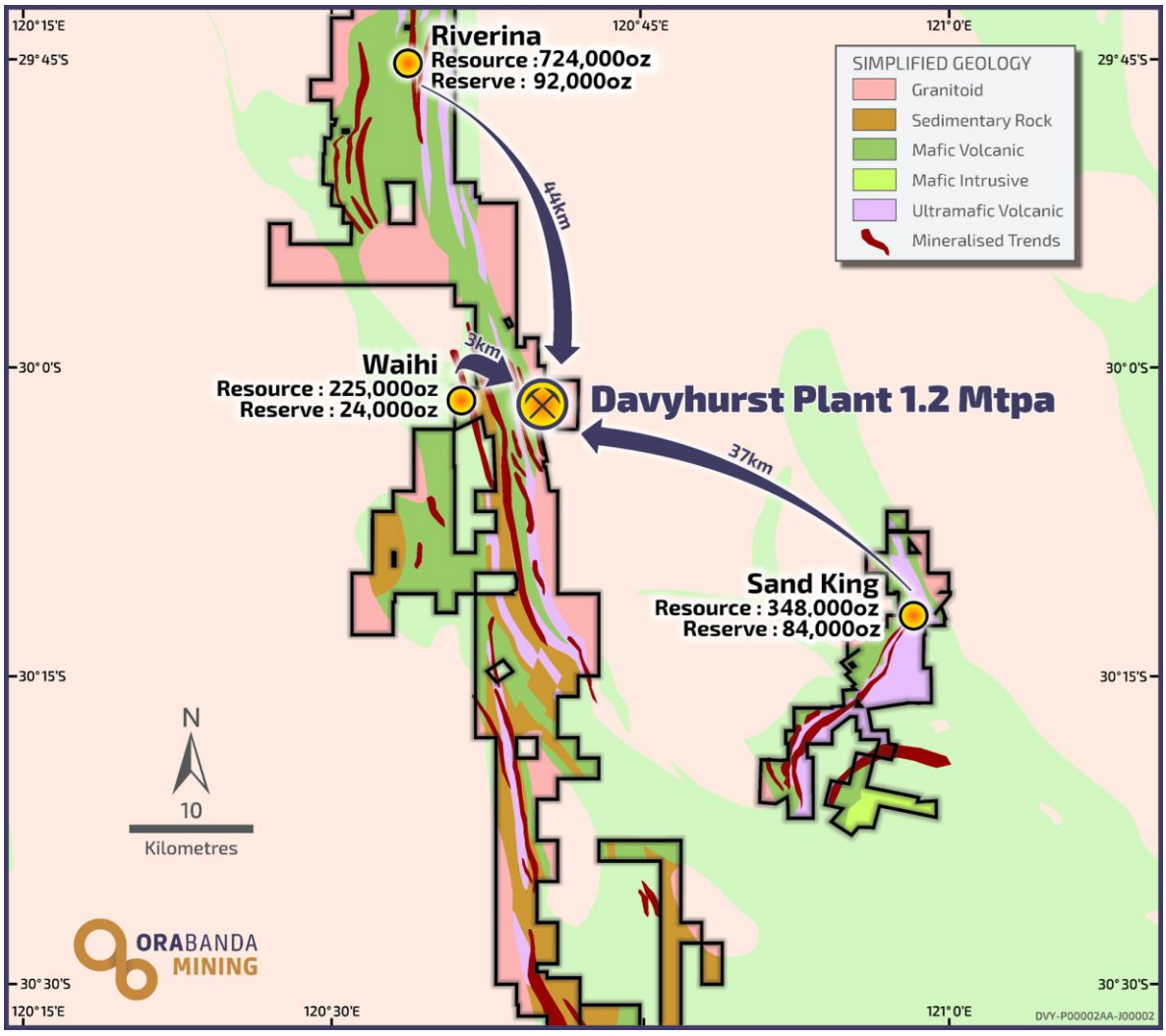

Figure 4 - Deposit locations

COMPETENT PERSONS STATEMENTS

The information in this announcement that relates to the Waihi, Sand King and Riverina Mineral Resources is based on and fairly and accurately represents information and supporting documentation compiled under the supervision of Mr Ross Whittle-Herbert, an employee of Ora Banda Mining Limited, who is Member of the Australian Institute of Geoscientists. Mr Whittle-Herbert has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Whittle-Herbert consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears.

The Missouri, Sand King, Riverina Area, British Lion, Waihi, Callion, Forehand and Silver Tongue Mineral Resources have been updated in accordance with all relevant aspects of the JORC code 2012, and released to the market on 2 December 2019, 26 May 2020, 5 June 2020, 9 October 2020, 1 August 2022 & 16 February 2023 (Riverina Area), 4 February 2020 and 26 October 2023 (Waihi), 3 January 2017, 26 May 2020 and 2 July 2024 (Sand King), 15 December 2016, 1 May 2022 and 26 October 2023 (Missouri), 15 May 2020 & 29 June 2020 (Callion), 29 July 2021 (Forehand, Silver Tongue & British Lion). Further details on Riverina and Sand King are provided in this release.

Mineral Resources other than Missouri, Sand King, Riverina Area, British Lion, Waihi, Callion, Forehand and Silver Tongue were first reported in accordance with the JORC 2004 code in the Swan Gold Mining Limited Prospectus released to the market on 13 February 2013. Mineral Resources other than Sand King, Missouri, Riverina Area, Forehand, Silver Tongue, British Lion, Waihi and Callion have not been updated to comply with JORC Code 2012 on the basis that the information has not materially changed since it was last reported. The Company is not aware of any new information or data that materially affects the information in that Prospectus and confirms all material assumptions and technical parameters underpinning the estimates continue to apply and have not materially changed.

The information in this announcement that relates to Ore Reserves for Riverina and Sand King Underground is based on, and fairly and accurately represents, information and supporting documentation compiled by Mr Leroy Savage, who is an employee of Ora Banda Mining Limited, and has sufficient relevant experience on matters relating to mine design, mine scheduling, mining methodology and mining costs. Mr Savage is a member of the Australian Institute of Mining and Metallurgy. Mr Savage is satisfied that the information provided in this announcement has been determined to a pre-feasibility level of accuracy or better. Mr Savage consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears.

The information in this report that relates to Open Pit Ore Reserves is based on, and fairly and accurately represents, information and supporting documentation compiled by Mr Geoff Davidson, who is a mining engineering consultant and employed by Mining and Cost Engineering Pty Ltd, and has sufficient relevant experience to advise Ora Banda Mining Limited on matters relating to mine design, mine scheduling, mining methodology and mining costs. Mr Davidson is a Fellow member of the Australian Institute of Mining and Metallurgy. Mr Davidson currently holds shares in Ora Banda purchased independently of the company. Mr Davidson is satisfied that the information provided in this announcement has been determined to a pre-feasibility level of accuracy or better, based on the data provided by Ora Banda Mining Limited. Mr Davidson consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears.

FORWARD-LOOKING STATEMENTS

This announcement contains forward-looking statements which may be identified by words such as "forecast", "guidance", "target", "outlook", "estimates", "believes", "expects", "anticipates", "intends", "may", "will", "would", "could", or "should" and other similar words that involve risks and uncertainties. These statements are based on an assessment of present economic and operating conditions, and on a number of assumptions regarding future events and actions that, as at the date of this announcement, are expected to take place.

Such forward-looking statements are provided as a general guide only, are not guarantees of future performance and involve known and unknown risks, uncertainties, assumptions and other important factors, many of which are beyond the control of the Company, the Directors and management of the Company. When forecasting or providing guidance on costs and production the Company has taken into account current operating costs, design, plans for the mine, cost escalation, required personnel numbers and inputs including capital estimates, submitted tender rates from contractors and suppliers, and average industry productivity and mining specification metrics. These and other factors could cause actual results to differ materially from those expressed or implied in any forward-looking statements.

The Company has no intention to update or revise forward-looking statements, or to publish prospective financial information in the future, regardless of whether new information, future events or any other factors affect the information contained in this announcement, except where required by law (including the ASX Listing Rules).

The Company cannot and does not give assurances that the results, performance or achievements expressed or implied in the forward-looking statements contained in this announcement will actually occur and investors are cautioned not to place undue reliance on these forward-looking statements.

Abbreviations

The following abbreviations are used in this report unless otherwise defined within the body of the report and which are specific to the relevant technical discussion in which they are used.

Abbreviation	Definition
ASD	Auto Stope Designer
SO or MSO	Stope Optimiser/Mineable Shape Optimiser
CIL	Carbon in Leach
DEMIRS	The Department of Energy, Mines, Industry Regulation and Safety
DGP	Davyhurst Gold Project
HV	High voltage
NSR	Net Smelter Return
OBM, Ora Banda or Company	Ora Banda Mining Limited
RoM	Run of Mine
TSF or IPTFS	Tailings Storage Facility
WRL	Waste Rock Landform
RESCAT	Resource classification category
ORE	Ore Reserve Estimate
MRE	Mineral Resource Estimate
mbs	Metres below surface
RL	Reduced level

Asset Fundamentals

The Davyhurst project area has over 140 km of combined strike of mineralised trends inside the 1,135 km^2 tenement package (Figure 5). The tenements cover the highly prospective ground at the convergence of two regionally significant deep-seated structures, the Zuleika Shear and the Ida Fault. Ora Banda Mining (OBM) is the registered holder to 37 Mining Leases, 21 Exploration Licences, 10 Prospecting Licences, has access agreements for 35 Miscellaneous Licences and 4 General Purpose Leases.

Gold ore is treated at its 1.2 Mtpa centrally located Davyhurst processing facility. This facility is supported by multiple workshops and stores along with administration offices. A 7.5 MW gas power station provides power for the Davyhurst central hub and is supported by a connection to mains grid power. Two villages are established: the Davyhurst Village with 259 person capacity and the Riverina Village with 158 person capacity. Support infrastructure includes several bore fields and pipelines, haul roads, access to nearby airstrips, two TSF cells along with in pit storage (IPTSF) with +3 years capacity. Both Riverina and Siberia have established mine site offices and workshops.

Location

OBM's Davyhurst Gold Project is in the eastern goldfields, 125 km from Kalgoorlie via roads, 67 km sealed road to Ora Banda and 58 km of unsealed public and private haul roads. The tenement package extends from 44 km north of Coolgardie at the southern extent to 20 km north of Menzies at the northern extent. The tenements are well connected with rural roads from Coolgardie, Menzies, Ora Banda and Canegrass with most roads established from the 1890- early 1900's gold rush.

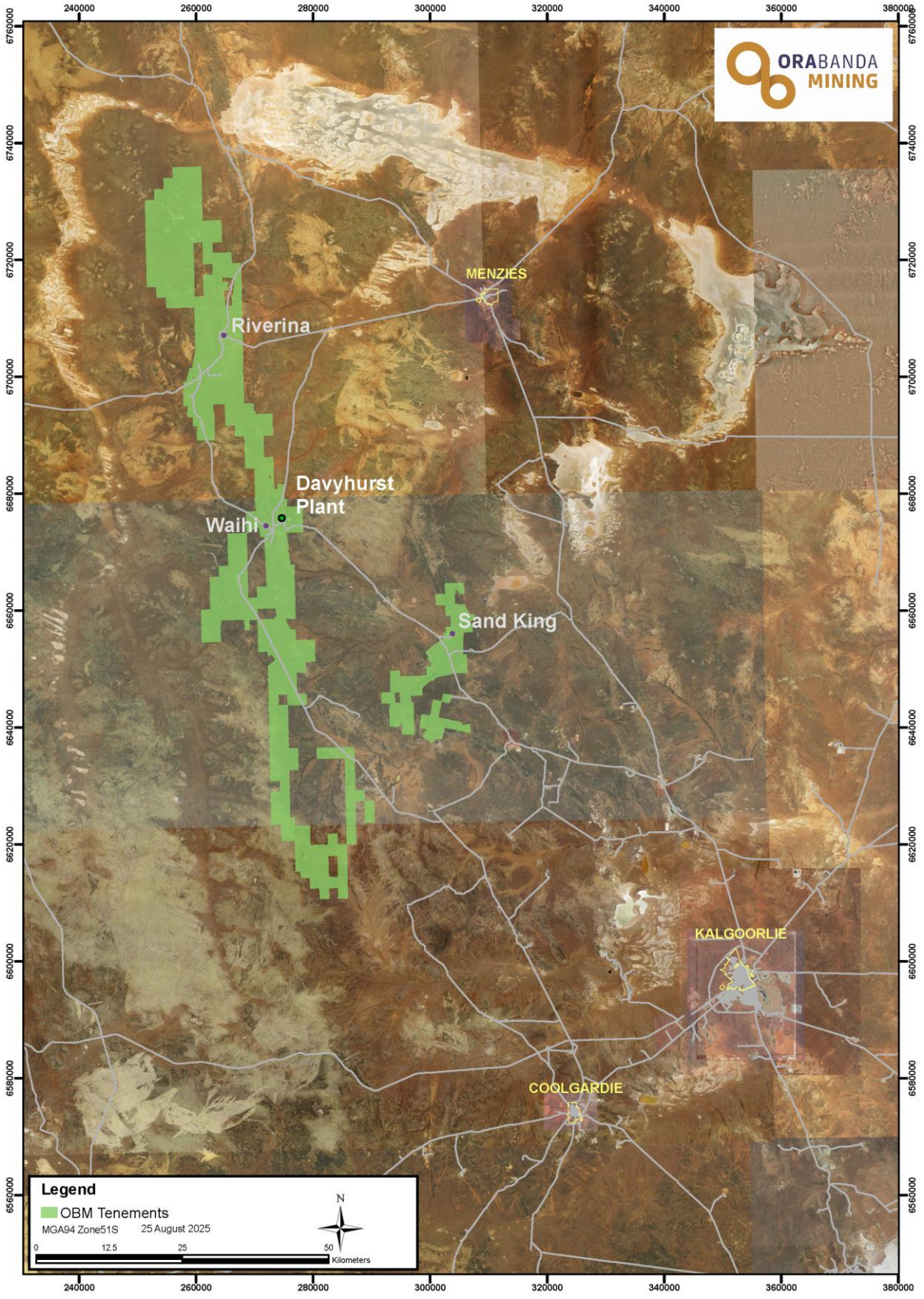

Figure 5 - Regional map, OBM tenements and deposits

RIVERINA RESOURCE AND RESERVE

SUMMARY

As of and including 30 June 2025, underground operations at Riverina had mined 875 k tonnes at 3.8 g/t for 106 k ounces including low grade since commencement in May 2023. Of the 106 k ounces mined 48 k ounces were Ore Reserve equivalent and as such represent the depletion in Figure 6. Geological drilling and mining have improved the orebody knowledge and has, as a result, contributed to the 52 k ounces of growth to the ORE resulting in a post depletion increase of 4 k ounces or 5%. The ORE grade has decreased to 3.5 g/t from 4.2 g/t with the increase in stope dilution from 5% to 20% resulting in 0.4 g/t reduction to the overall grade. The FY25 reconciliation to the ORE shows a 14% positive grade reconciliation.

A summary of the Riverina Mineral Resource and Ore Reserve as at 1 July 2025 are shown in Table 5 and Table 6 respectively.

Table 5 - Riverina Gold Project Mineral Resource Estimate

RIVERINA GOLD PROJECT MINERAL RESOURCE ESTIMATE[1]:									
	MEASURED		INDICATED		INFERRED		TOTAL MATERIAL		
	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	266	3.2	3,953	2.7	2,826	2.4	7,046	2.6	586
OPEN PIT	476	1.7	2,118	1.6	117	1.5	2,711	1.6	138
TOTAL	**742**	**2.2**	**6,071**	**2.3**	**2,943**	**2.4**	**9,757**	**2.3**	**724**

Table 6 - Riverina Gold Project Ore Reserve Estimate

RIVERINA GOLD PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	53	4.7	8	773	3.4	84	825	3.5	92
LOW GRADE	-	-		144	1.2	5	144	1.2	5
TOTAL	**-**	**-**		**917**	**3.0**	**89**	**970**	**3.1**	**97**

[1] Inclusive of Ore Reserve

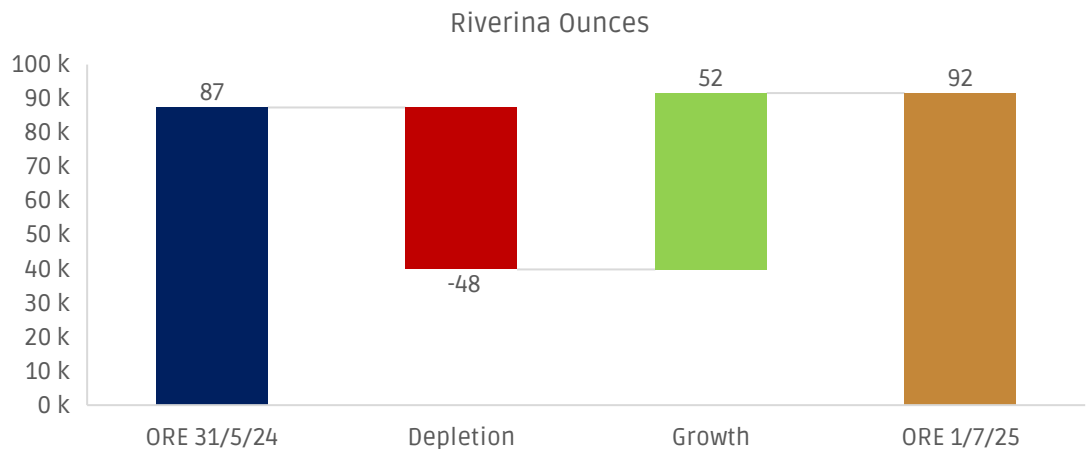

Figure 6 - Change in Riverina ORE ounces

INTRODUCTION

Tenement

The Riverina gold project is located on the granted mining tenement M30/256, which is 100% owned by Carnegie Gold Pty Ltd, a wholly owned subsidiary of Ora Banda Mining Limited. OBM holds rights to gold and its byproducts over this tenement. There are no known heritage or native title issues within the tenement. The tenement is in good standing with DEMIRS with no known title risk.

Permits and Licenses

The required environmental approvals to operate the Riverina Underground mine are in place. The operations remain compliant with all the current permitting requirements which remain in full force. A rehabilitation obligation remains at Riverina post open pit mining.

- Riverina Gold Operations Mining Proposal (Reg Id 128331, Approved September 2024)
- Riverina Gold Operations Mine Closure Plan for the Mining Proposal (Reg Id 98123)
- "Prescribed Premise Licence 9402/2023/1
- Groundwater Well Licence GWL108490 (3)
- Clearing Permit 8854-3

Infrastructure

The Riverina Underground mine commenced in May 2023, establishing declines, raises, ventilation and escapeway infrastructure. Eight production levels have been accessed, and stope production commenced on these levels up to 30 June 2025 with development and stoping ongoing. A 5 MW power station supplies HV power via a service hole to underground substations and distribution network. A dewatering capacity of 60 l/s is currently in place along with 2,526 ML in pit storage capacity. Permitted waste rock storage capacity remains as well as pit backfilling opportunities.

The Riverina office, workshop, communications and surface facilities are sufficient for the ongoing underground operation. Approved waste storage is sufficient for the Ore Reserve mine design.

The Riverina village is 2.8 km from the mine offices and was built in 2021. Additional rooms were made available in FY25 for a total of 158 person capacity.

The Davyhurst processing facility is located 46 km via well-established public roads to the south of Riverina. Road trains are used to haul ore from the mine ore pad at Riverina to the Davyhurst RoM pad.

MINERAL RESOURCES

Mineral Resource Estimation: Summary Information as required under Australian Securities Exchange (ASX) Listing Rule 5.8.1 follows.

GEOLOGY & GEOLOGICAL INTERPRETATION

Lithology

Mafic and ultramafic volcanics and volcanogenic sedimentary lithologies (wacke, siltstone, shales) are found in the main Riverina resource area. The Riverina deposit sits on the western limb of a regional significant syncline with the mine sequence generally dipping steeply (approximately 80-70°E) to the east.

Mafic basalts are the dominant rock type and host the Main Lodes within the Riverina deposit. Narrow, tightly constrained shear zones within the basalt host mineralised quartz veining with relatively tight alteration halos. Immediately to the west of the host basalt at Riverina is a thick body of peridotite (ultramafic). Several discrete, narrow ultramafic bodies have also been identified in the Riverina mine area. These narrow ultramafic bodies are interleaved with the mafic and sediment units proximal to the orebody in the Murchison and Reggie Lodes.

Metasedimentary bodies are host to mineralisation within both the Murchison and Reggie Lodes. Originally fine-grained greywackes and siltstone, they are now represented as moderately foliated to highly deformed felsic schists with zones that appear mylonitic in nature. The widths of the metasedimentary units range from very thin discontinuous lenses to more robust strike extensive units locally up to 15 m wide. A thinly bedded/laminated interflow sediment horizon lies in close proximity to the Main Lode ore zones in the southern portion of the deposit area. Semi-massive and massive sulphide zones are found within carbonaceous shale beds in the Murchison and Reggie Lode areas. These black shales are typically gold poor.

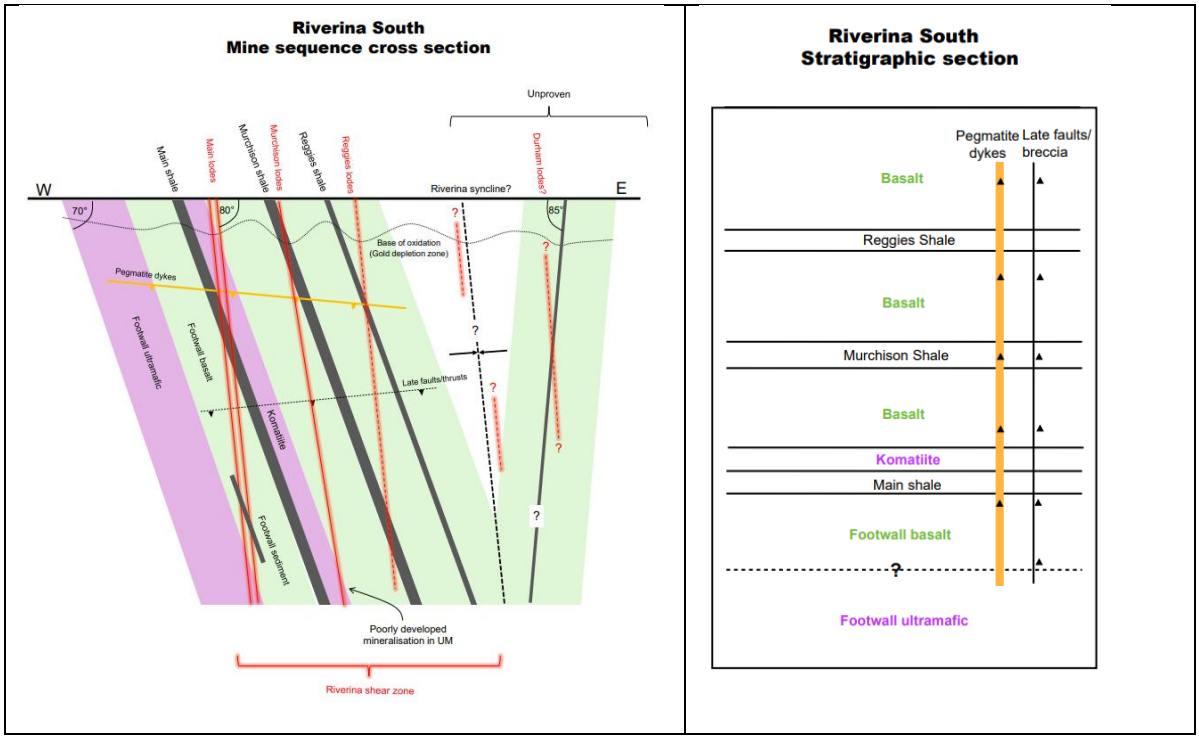

Figure 7 - Diagrammatic cross section of the defined mine sequence of the Riverina Deposit and indicative stratigraphic section

Late pegmatite dykes form a shallow S-SW dipping dyke swarm that cross-cut all lithologies including alteration related to gold mineralisation. Narrow, steep east and north dipping dykes are also visible in the open pit. Dykes can be up to several metres true thickness but are more commonly 1 m or less and often pinch out/terminate on late structures.

Structure

The Riverina deposit is interpreted to lie in a low strain zone of a several kilometre long macro shear boudin, bounded to the east and west by thick ultramafic bodies. This macro boudin has developed around the core of a regional syncline that has been rotated and deformed within a ductile stress regime. The deposit is located within the western limb of this tightly folded syncline, with the stratigraphy within the limb dipping at approximately 70°E. Major shear zones have developed on this steep east dipping fold limb and control the line of historic workings north and south of the deposit.

There are three main mineralised horizons which make up the Riverina Deposit, namely Main Lodes, Murchison Lodes and Reggie Lodes. The Main Lode is defined as several discrete steep dipping to sub-vertical structures striking between 340° and grid north, running parallel while maintaining a separation of between 5 m and 15 m. These structures are remarkably consistent in their strike and dip continuity and have been consistently intersected in drilling for over 1.7 km of strike and over 1 km vertical metres down dip.

The Murchison Lodes are a series of parallel/sub-parallel mineralised structures that strike more north-south and also dip steeply to the east. The tenor of the mineralisation is influenced by the different lithologies that these steep shears cross-cut. The mineralised structures are generally narrow, displaying tight alteration halos.

The Reggie Lodes make a minor contribution to the overall MRE but remain under-drilled and form a high priority exploration target.

The Riverina area is dominated by tight to isoclinal folding (F1) that has an overall plunge of ~30° to the south. This mirrors the average plunge of mineralisation across the deposit, although observations from drill core show there are localised areas where the plunge is measured as sub-horizontal (5-10^0) to the south and possibly coincides with an increased tenor of grade and width.

An early extensional deformation event led to emplacement of N-S steep dipping extensional quartz veins with initial Au deposition. A later structural event involved ENE-WSW shortening and continued intense strike slip shearing over a period of time. In zones of high strain and low stress, early quartz veins were boudinaged and in places mylonitised, and gold was remobilised and redeposited. A strong ductile S-C fabric is developed with the intersection of the S and C fabrics plunging gently to the south. This is coincident with measurements of the plunge of well-developed quartz boudin necks, which range from sub-horizontal to up to 35^0 to the south.

The rocks at Riverina exhibit a diverse range of deformation over short distances. Only metres from mineralised shear zones, where rocks are intensely deformed and often mylonitic, pillow basalts are relatively undeformed, showing their distinctive flat bases and domal tops (younging direction to east). Undeformed sediment units also exhibit fine graded bedding and laminations. Pegmatite dykes, although weakly deformed by later structural events, tend to remain fairly pristine.

The post-mineralisation structural architecture based on pit mapping, drill core logging and underground mapping, highlights the presence of multiple shallow south-dipping thrust faults that transect the entire Riverina area. In the Riverina North pit, one such thrust is marked by a 30-40 cm thick zone of fault gouge (cataclasite) and saccharoidal quartz. Associated ramp structures, back thrusts and antithetic shears form a complex structure array in the Riverina North pit. N-S sub-vertical mineralised shear zones have also been reactivated and acted as transfer faults associated with the late-stage thrusting. Several of these structures have been intersected in underground development. An additional structural event, post north-south shortening and thrust development, resulted in conjugate strike slip faulting. Faults are steep ENE dipping (sinistral) and moderate SE dipping (dextral). Fault offsets are from a few metres to several metres. The steep ENE dipping set are open spaced structures and act as a fractured aquifers and transfer meteoric water into the mine.

Alteration & Mineralisation

Mineralisation at Riverina is hosted within three distinct mineralised shear systems; from west to east they are the Main Lodes, the Murchison Lodes and the Reggie Lodes.

The Main Lode mineralised zone is hosted within pillowed basalts, the dominant rock type in the area and comprises several continuous discreet lodes running sub-parallel to each other, although only two form the bulk of the mineralisation. The individual ore zones range from <0.5 m to up to 3 m wide with the high-grade core characterised by intense shearing/mylonitisation of boudinaged quartz-sulphide veins and surrounding strong banded silica-biotite-sericite alteration of the mafic host. The Main Lodes exist within a broader shear zone characterised by weaker shearing and alteration. High gold grades are occasionally noted in the broader shear, associated with localised stronger silica alteration/veining, but are discontinuous. High grade mineralisation has a shallow southerly plunge consistent with geological observations (boudin neck plunge and S-C fabric intersection.

The dominant sulphide minerals are pyrrhotite and pyrite, with arsenopyrite and galena observed in the highest gold grade intervals. Highest concentration of sulphide tends to be within intensely altered wallrock adjacent to quartz veining. Visible gold is present as fine discreet flakes, however in very high-grade zones, forms small foliation parallel accumulations.

The Murchison Lodes comprise several parallel/sub-parallel mineralised zones ranging from <1 m to several metres thick with variable grades. Lodes are hosted within both strongly sheared and altered basalts, and finely bedded volcanogenic sediments (wacke, siltstone, shale). Basalt hosted ore zones exhibit strong shearing and boudinaged quartz-sulphide veining with associated strong silica-biotite-sulphide alteration. Strong shearing with boudinaged quartz-sulphide veining and associated silica-sericite alteration characterise the mineralisation with the sediment hosted ore zones in the Murchison. Sulphides are dominantly pyrite and pyrrhotite with localised arsenopyrite, galena and chalcopyrite.

Reggie Lodes are similar in character to the Murchison, comprising several sub-parallel, semi-continuous mineralised zones within both basalt and sediment host rocks.

Weathering

The weathering profile at Riverina is highly variable. Weathering increases significantly within shear zones and depth to fresh rock reaches vertical depths of 80 m in the centre of Riverina deposit and 40 to 50 m on the flanks of the main shear structures. The base of complete oxidation can extend to depths of up to 50 m vertical metres within the main shear zones. The base of complete oxidation over unaltered, massive mafic and ultramafic lithologies can be as shallow as 3–5 m below the current ground surface, as is evident in the north of the Riverina open pit. In places, possible zones of depletion in the upper saprolite are interpreted, where weaker mineralised shears appear to terminate ~20 m below surface. Stronger shears project to surface, although some redistribution of gold may have taken place from these shears as well. Significant areas of supergene enrichment are not evident.

DRILLING AND SAMPLING, AND SAMPLE ANALYSIS TECHNIQUES

Modern exploration in the Riverina area began in the mid 1980's. Numerous operators have held the tenure since. Although a proportion of drilling data is from previous operators, it is generally well documented and to industry standards of the time. In addition, OBM has added significant drilling to the Riverina deposit. All RC and diamond drilling at the deposit is deemed suitable for resource estimation purposes. Previous operators include Riverina Gold NL, Riverina Gold Mines, Greater Pacific Gold NL, Barminco, Barra Resources Ltd, Riverina Resources Ltd, Monarch Gold Ltd and Eastern Goldfields.

RC holes drilled by most operators were typically at least 5 inches in diameter. RC hole diameters from drilling by Riverina Gold NL and Barra Resources are unknown. Diamond holes were all HQ or NQ in diameter.

Early RC and diamond hole locations (Riverina Gold NL, Riverina Gold Mines, Greater Pacific Gold NL) were surveyed on an early Riverina local grid which is oriented to true north. The origin for this grid is 10,000N, 10,000E located at the south-west corner of surveyed tenement M30/98. These coordinates were transformed to MGA94 Zone 51 using well-established grid transformation

parameters. Drilling by other operators was surveyed by mine surveyors or contractors using DGPS or RTKGPS in either AMG84 Zone 51 or MGA94 Zone 51 coordinates. Surface collars drilled by OBM were all picked up by the mine surveyor in MGA94 Zone 51 coordinates.

Generally shallow RC holes by Riverina Gold NL and Riverina Gold Mines were not down hole surveyed. Other early operators downhole surveyed RC holes by Eastman camera. Diamond drill holes were downhole surveyed by Eastman camera or gyro. Riverina Resources employed Eastman camera, electronic multi-shot or gyro for surveying. Electronic multishot was used by Monarch Gold and north seeking gyro was used by OBM. All grade control holes drilled by OBM are surveyed by the mine surveyor and downhole surveyed by rig north seeking gyro.

UG diamond drill rig alignment is via surveyed collar locations and the DeviAligner tool, downhole surveys via DeviGyro-OX tool. Underground face sample locations measured via laser distometer to known surveyed control points and development surveys via theodolite.

RC sampling protocols for some early operators (Riverina Gold NL., Riverina Gold Mines, Greater Pacific Gold NL, Barminco) are unknown. A riffle splitter was employed by Riverina Gold Mines and ¼ was sent for analysis. Later operators collected samples through a cyclone and split using either a riffle splitter or cone splitter. Barra Resources, Riverina Resources and Monarch Gold submitted 4 m composites for analysis. These were taken using a spear or flour scoop. Anomalous intervals were then re-split using a riffle splitter and submitted for analysis. OBM sampled every meter with a 2-3 kg split taken from a cone splitter. OBM occasionally submitted 4 m composite samples by spearing the 1 m sample piles. If anomalous gold values were returned, the individual 1 m samples from the rig cone splitter were submitted as a separate batch.

Diamond core was generally sampled to geological boundaries and or mineralised intervals. Generally, half core was sampled though Barra Resources Ltd submitted whole core for analysis. Core sampling or resource drilling by Ora Banda was defined by a geological or mineralisation boundary with ½ core submitted for analysis. Frequently underground drill core was whole core sampled. All drill samples were logged by qualified geologists.

Historical assay QAQC protocols used by companies prior to Monarch Gold's ownership (pre-2007) have not been documented in any detail. Monarch Gold submitted Certified Reference Material every 20th sample in RC drilling programs. Duplicate samples were submitted every 25th sample for RC drilling. The protocol adopted by OBM required CRM standards and blanks be inserted every 20 to 25 samples for RC and diamond drilling. The frequency rate of RC field duplicate samples was nominally 1 every 30 m.

The current resource update follows an extensive surface RC and surface and UG diamond drill program completed after the previous MRE released in July 2024. An additional 4 RC holes, 30 diamond holes and 29 RCDD holes were included in this resource update. In addition, there are 471 UG diamond holes and 2145 faces included in the current MRE.

Assay QAQC for the additional drilling was analysed. Assay precision was acceptable, performance of certified reference material was good and overall results were generally acceptable.

Sample Analysis Methods

Historical assay QAQC protocols used by companies prior to Monarch Gold's ownership (pre-2007) have not been documented in any detail. Monarch Gold submitted Certified Reference Material

every 20th sample in RC drilling programs. Duplicate samples were submitted every 25th sample for RC drilling. The protocol adopted by OBM required CRM standards and blanks be inserted every 25 samples for RC and surface diamond drilling. The frequency rate of RC field duplicate samples was nominally 1 every 25 m. All underground diamond drill and face sample submissions include routine CRM and blank insertions at rate of 1:20. Diamond core is sampled to geological intervals with a minimum length of 0.3 m. Initially OBM drilling and face samples were prepared in the SGS on-site sample preparation laboratory and pulps sent to SGS in Kalgoorlie for analysis. A 50 g charge was taken and analysed by fire assay Microwave Plasma-Atomic Emission Spectroscopy (MP-AES). Since early March 2025 all underground grade control and face sampling was crushed in the SGS on-site laboratory and the samples sent to SGS Kalgoorlie for gold analysis by Photon assay method. In April all samples from surface drilling were assayed by Photon assay method. Transfer of analytical method from fire assay to Photon assay followed a program of comparison assaying whereby Photon assay analysis was done on the crush reject of samples already assayed by fire assay.

ESTIMATION METHODOLOGY

Mineralised domains were interpreted to assay grade boundaries corresponding to geological observations in core and face photographs, and geology logging, including structure. All drilling and face sampling from underground development was used to aid the interpretation. RC, diamond drilling and face sampling assay data was used in the estimation of grades. Sample intervals were manually defined using Leapfrog™ software, on a section-by-section basis. The narrow but variable width of the mineralisation precluded the utilisation of fixed length composite samples as no one composite length was satisfactory for all locations. This led to the adoption of full width compositing, using Leapfrog™, which compiles the entire drillhole intersection across the mineralisation into a single full width composite of variable length. Leapfrog™ also calculates the true width of the sample interval using its distance function. The distance from the sample interval mid-point to the footwall and hangingwall surface of the lodes is determined and the two values are added to get the full width.

A 2-dimensional estimation technique was adopted where the lodes are projected onto a 2D northing-elevation plane with a nominal easting. The 2D estimation method accounts for the different sample supports by estimating an 'accumulation' variable, which is defined as the product of the assayed grade and the true width of the lode. The lode width is also estimated, and the final gold grade is back-calculated from the estimated accumulation and width variables. The 2D estimation method, with a single grade across the full width of the mineralised vein, assumes full horizontal extraction.

Prior to estimation, the easting value of the centre point of each domain composite and each block were set to an arbitrary but constant value.

Spatial continuity, using Supervisor™ software, of accumulation and width variables was evaluated using variography in the 2D plane and the parameters defined were applied in the estimation process. Search neighbourhoods were defined using Kriging Neighbourhood Analysis implemented in Supervisor™. Top cuts were applied to the accumulation variable where appropriate.

Estimation of gold accumulation and true width was by ordinary kriging with exactly the same parameters, using Micromine™ software into a parent block size of 5mN x 5mRL in the areas with mine development or close-spaced drilling, and 10mN x 20mRL elsewhere. After estimation in the

2D plane the back-calculated gold grade values were pressed across the full width of the corresponding domain in the final 3D model. The domain wireframes were then used to constrain volumes by removing blocks outside the domains, using suitable sub-celling.

The bulk density values for ore were assigned based on the weathering state of the rock and determined from over 3,459 drill core density measurements. The model has been depleted to account for existing mining, both underground (including in-situ pillars and 'skins' proximal to open stope voids) and open pit.

CRITERIA USED FOR CLASSIFICATION

Wireframe solids were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, Measured, Indicated or Inferred:

- Measured – Near surface areas defined by close spaced RC grade control drilling and an area between two development drives with significant face sampling
- Indicated – Areas with:
    - drill spacing in long section up to approximately 40mN x 40mRL and with reasonable confidence in the geological interpretation and grade continuity.
    - reasonable estimation quality as defined by the conditional bias slope > 0.5
- Inferred – Areas with:
    - drill spacing in long section in excess of 40mN x 40mRL and where grade continuity is poorer as defined by a lower sample density, even though geological continuity may be apparent.
    - poorer estimation quality as defined by the conditional bias slope > 0.2 and < 0.5

Areas of some lodes, particularly at depth have fairly low/no sample support and were not classified.

CUT-OFF GRADES AND MODIFYING FACTORS

The Mineral Resources have been reported from fresh material at a diluted cut-off of 0.9 g/t Au inside Mine Stope Optimiser (MSO) derived solids with dimensions of 10mN x 10mRL and a minimum width of 1.6 m. Individual MSO blocks were assessed and removed if above the top of fresh DTM surface and if above the $2400/ oz optimised pit shell from within which the remaining Riverina open pit resources are reported.

ORE RESERVES

Material Assumptions and Outcomes, Criteria for Classification

This ORE for Riverina was derived from technical studies, data and knowledge gained from the recent underground mining, incorporating project-specific costs as well as geotechnical analysis, dilution and recovery parameters and was based on the 2025 MRE current at the time and described in this announcement. Processing parameters were based on test work that has been combined with recent processing performance. Hydrogeological conditions were determined from recent mining at Riverina.

The Riverina Underground Ore Reserve was estimated using a gold price of A$2,500/ oz.

The dilution skin method was employed to reflect the selective mining method proposed for Riverina Underground. Dilution parameters were subjectively determined based on a geotechnical assessment of the expected mining environment. A cut-off grade of 2.4 g/t was applied to determine economic mining envelopes, further spatial optimisation was done to ensure all economic ounces were included.

Mining recovery for the underground Ore Reserve is dependent upon the dimensions and spacing of pillars throughout the orebody. The Riverina mine design assumed 40 m open stopes (along strike) and pillars of 5.0 m by 17.5 m. The 40 m stope strike extents were considered a practical distance over which to successfully operate remote loaders to recover ore from open stopes. 3 m high dilution control sill pillars were designed where stoping extends more than 4 levels down dip on a mineralised lode. The rib and sill pillars equate to 88% mining recovery with both development and stoping activities. Consistent with reconciled performance, an additional 5% stope ore loss was also included for operational losses. The overall mining recovery was estimated to be 85%.

Mining Method

The underground mine design utilises conventional narrow vein up-hole benching using longhole open stoping mining methods. This method is commonly used in the Western Australian Goldfields for this style of mineralisation.

Mining equipment is mechanised, with equipment that includes electric-hydraulic drills for development and production, and rubber tyred loaders and trucks for load and haul activities. Stope production loading incorporates a combination of conventional loading and tele-remote loading for non-entry mining stopes.

Based on the geotechnical assessment, which identified good ground conditions and favourable stress environment, as would be expected at mining depths less than 500mbs, no stope backfill is contemplated.

Cut-off Grades

The estimation of the cut-off grades for the Riverina Underground Ore Reserve were estimated to be 2.4 g/t for production stoping. The cut-off grade calculation was estimated at a gold price of A$2,500/oz, and is inclusive of mining, transport, processing, overheads, sustaining capital and royalties.

A cut-off grade of 2.0 g/t was applied to the underground development based on the incremental cost of developing hauling and processing of the ore. The calculation was estimated at a gold price of A$2,500/oz.

Low Grade insitu material is 0.7 g/t to 2.0 g/t, based on the surface SP cut-off 0.7 g/t where haulage, processing, admin costs are applicable and using a gold price of A$4,400/oz.

Recent Riverina mine contractor costs and OBM budget costings were used.

The standard WA state royalty of 2.5% NSR plus a 1% NSR third party royalty was applied.

Processing Method

The process for treating ore at the DGP is conventional CIL with some gold recovered via a gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. The process plant has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm. The process plant has been successfully operated at this rate with recent improvements made. The processing recovery applied to Riverina Underground was 88% and was based on metallurgical test work. The recovery performance was 88.1% through Davyhurst plant in FY25 of which 76% was Riverina Underground feed.

Estimation Methodology, and Modifying Factors

The ore drive widths were designed to be 4.5 m allowing access for larger mechanised mining equipment. A combination of full face and split firing development methods will be used. Split firing within the 4.5 m wide ore drives will be undertaken as part of the development cycle. It has been assumed split firing will be used for 45% of ore drive advance. Given the nature of the mineralisation, this practice will reduce ore development dilution from 83% to 61% for each cut with an average orebody width of 0.75 m. The practice has been successfully undertaken at Riverina in FY25 and is a continuing practice.

Given the narrow vein nature of the mineralisation, the global dilution, inclusive of stoping and ore drive development, was estimated to be 57% of material. Background grades were estimated into the block model and were included in the dilution modelling. Dilution grades varied between zero and 0.5 g/t depending on the nature of the alteration halo. The global average grade of dilution was estimated to be 0.22 g/t. Dilution being all included material less than 0.7 g/t[1].

Delineation of economic stoping areas was completed using Deswik™ software. Mineable "stope" shapes were created to simulate fully diluted stope blocks, as described below. The optimisation field used a cut-off grade of 2.4 g/t. The stope shapes are then depleted by development ore drives and modifying factors are applied in the mine schedule. Scheduled stopes below 2.4 g/t are spatially optimised and incremental stope cut-off grades were used where development is in place and planned to access stopes >2.4 g/t. Spatial optimisation and use of incremental COG of 2.0 g/t ensures all economic ounces are included.

A minimum stope mining width of 1.6 m was applied in the dilution modelling process, with an additional 0.6 m dilution skin applied to all valid stope shapes (0.3 m hanging wall and 0.3 m footwall). Therefore, all stoping analytics have been completed on a minimum mining width including dilution of 2.2 m wide. In addition, a nominal provision for unplanned dilution of 20% at 0 g/t was also included in a scheduling adjustment as a contingency to all stoping panels.

Inferred material was not considered in defining the stoping envelopes; however, due to practical mining geometries a small portion of Inferred material was included within the Underground Ore Reserve. This material was included at the edges of the mining envelope and equates to approximately 1.5% of the Riverina Underground Ore Reserve inventories. The Inferred inventory was not considered material to the economics of the project. The RESCAT for each scheduled task was attributed with the RESCAT of the dominant mass of material above 0.5 g/t.

[1] 0.7 g/t represents the surface stockpile cut off for development ore.

The economic viability of the Riverina Underground was confirmed using current commercial parameters in a project evaluation cash flow model. This model also considered project phasing, stockpiling, project capital and the effect of fixed costs. The cash flow modelling was based on a gold price of A$3,300/oz. The mine demonstrated a positive net cash flow with acceptable returns. Overall unit mining costs for the underground was estimated to be A$171/t ore, inclusive of sustaining capital

Mine Design

The Riverina Underground design on which this Ore Reserve was based is shown in Figure 8. The mine entries for the Riverina Underground consists of a main access portal, primary return ventilation rise and an escapeway rise. All entries are located in the fresh rock portion of the existing Riverina pit. The decline is 5.5 m wide x 5.7 m high with a typical gradient of 1:7. Ore drives are designed to be 4.5 m wide x 4.5 m high.

Underground pump stations are in place and have been allowed for in the design with ~100 vertical metres between pump stations. Mine dewatering is further pumped 15 km to a water storage pit with 1,870,000 kl capacity remaining. Dewatering pipelines and pumps are capable of 60 l/s.

Primary ventilation is via a 4.5 m diameter raise bore from underground to the open pit. Return air drives are designed 5 m x 5 m with vertical rises ~6 m x 4 m. The system can meet the demand at various stages including the Ore Reserve design and schedule.

The average floor to floor slope distance between levels is set at 22 m with an average stope panel height of approximately 17.5 m. Stope parameters used in the Riverina mine design are shown in Table 7.

Table 7 - Riverina Stope Parameters

Stoping Parameters		
Sub-Levels	22	m
Stope Width	1.6	m
Dilution FW	0.3	m
Dilution HW	0.3	m
Stope Length	~40	m
Ave Stope Width	2.2	m
Rib Pillar Width	5	m
Sil Pillar thickness	3	m
Sil Pillar frequency	~85	m
COG	2.4	g/t
Schedule Dilution	20%	0 g/t Dilution
Schedule Recovery	95%	

The current ground control management plan provides stope and pillar analysis and guidance in line with the stope parameters used.

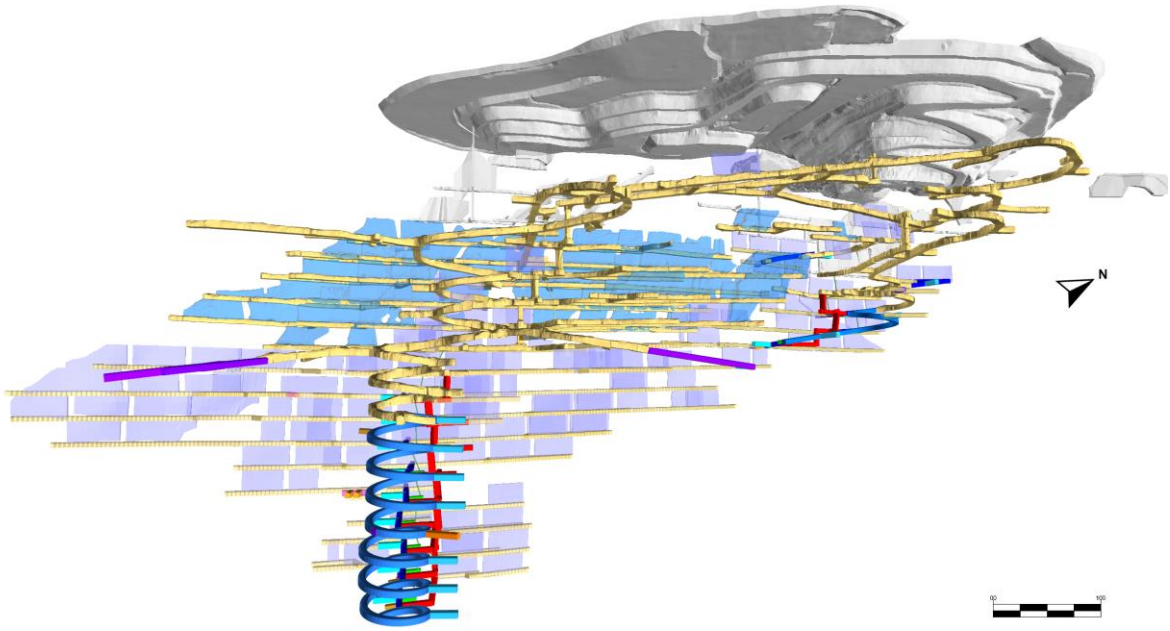

Figure 8 - Isometric view looking north-west of Riverina Underground Ore Reserve mine design with existing OBM underground workings (as built yellow drives, blue mined stopes as at 30 June 2025) and future Ore Reserve stoping areas (purple), Riverina pit and historical underground working (light grey)

Riverina Underground Mine Schedule

A mine schedule for the Riverina Underground Ore Reserve was developed, with productivity rate assumption in line with contractor expectations.

The mining sequence assumes top-down retreat mining with no current plans to backfill stopes. The mining equipment resource levels on which the mine schedule was based are shown in Table 8. The ORE schedule was used in the economic assessment.

Table 8 - Riverina mining equipment levels

Equipment		
2x Jumbo	Sandvik DD421	Twin Boom
2x Long Hole Drill	Sandvik DL431	76mm holes
3x Loader	Sandvik LH517	17T
3x Truck	Sandvik TH663	60T

Economic Assessment

An economic assessment was carried on the Riverina Underground to validate the Ore Reserve. The cash flow was modelled in real terms on a pre-tax basis. Costs, recovery and revenue parameters used were as described above.

Costs were derived from the FY25 budget estimate including contract pricing current at the date of this Ore Reserve. Unit costs for mining were estimated based on fully resourced contracted scope of work.

Mining overheads were based on OBM budget provisions for supervision and technical support, as well as contractor fixed costs, general operating expenses, FIFO flights and accommodation. Dayworks provisions were also included for miscellaneous works during operations as well as closing of the site.

Unit costs for haulage, processing and head office overheads were calculated using the combined project cost model with the Ore Reserve mine schedules and stockpiles.

An allowance for capital has been used in the economic modelling and based on recent actuals and budget forecasts. The allowance covers:

- Additional underground sub stations,
- Power station purchase,
- Primary vent controls, and
- Underground dewatering.

The ORE is based on a feasibility level of accuracy. A gold price of A$3,300/oz was used for financial assessment and the competent person is satisfied that the mine demonstrated a positive net cash flow with acceptable returns.

Ore Reserve

On the basis of the outcomes of the analysis described above, the estimated economic mining inventory was classified as an Ore Reserve under the 2012 JORC code. All of the ORE was derived from the economic portion of the Measured and Indicated Mineral Resource. Measured Mineral Resource within the economic mining envelope was classified at Proved Ore Reserve Estimate. Indicated Mineral Resource within the economic mining envelope was classified at Probable Ore Reserve Estimate. Low grade was all classified as Probable Ore Reserve Estimate. The Ore Reserve is shown in Table 9.

Table 9 - Riverina Underground Ore Reserve, as at 1 July 2025

RIVERINA GOLD PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	53	4.7	8	773	3.4	84	825	3.5	92
LOW GRADE	-	-		144	1.2	5	144	1.2	5
TOTAL	**-**	**-**		**917**	**3.0**	**89**	**970**	**3.1**	**97**

SAND KING RESOURCE AND RESERVE

SUMMARY

The Sand King Underground portal was fired in August 2024 and in FY25, 182 k tonnes at 2.9 g/t for 17 k ounces were mined from 3 levels with both development and stoping contributing. Of the 17 k ounces mined 8 k ounces were Ore Reserve equivalent and as such represent the depletion in Figure 9. The FY25 reconciliation to the ORE shows a 10% positive grade reconciliation. Geological drilling and mining have improved the orebody knowledge and as a result contributed to the 38 k ounces of growth to the ORE resulting in an increase of 30 k ounces or 54%.

A summary of the Sand King Mineral Resource and Ore Reserve as at 1 July 2025 are shown in Table 10 and Table 11.

Table 10 - Sand King Gold Project Mineral Resource Estimate

SAND KING GOLD PROJECT MINERAL RESOURCE ESTIMATE[1]:									
	MEASURED		INDICATED		INFERRED		TOTAL MATERIAL		
	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	108	3.2	1,900	2.7	1,901	2.9	3,909	2.8	348
OPEN PIT	-	-	-	-	-	-	-	-	-
TOTAL	**108**	**3.2**	**1,900**	**2.7**	**1,901**	**2.9**	**3,909**	**2.8**	**348**

Table 11 - Sand King Gold Project Ore Reserve Estimate

SAND KING GOLD PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	52	3.9	7	777	3.1	78	829	3.2	84
LOW GRADE	-	-		96	1.2	4	96	1.2	4
TOTAL	**52**	**3.9**	**7**	**874**	**2.9**	**81**	**926**	**3.0**	**88**

[1] Inclusive of Ore Reserve

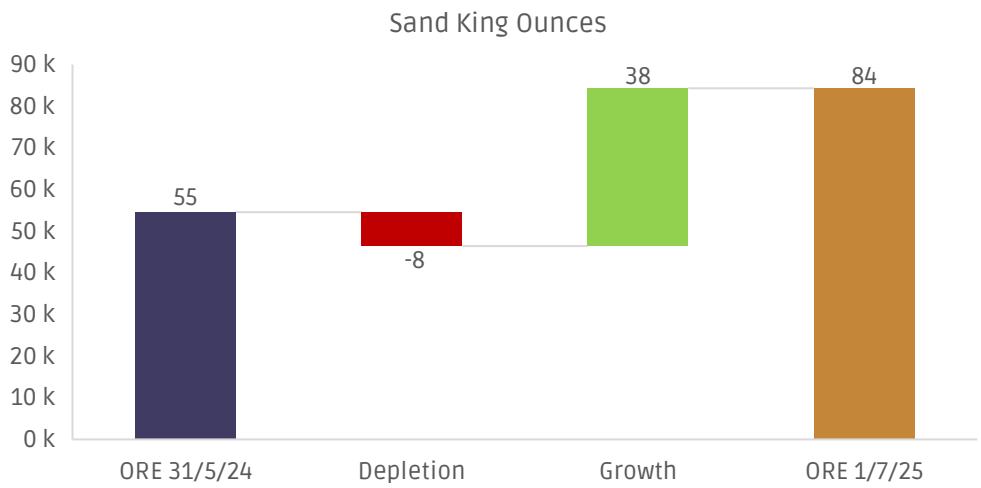

Figure 9 - Change in Sand King ORE ounces

INTRODUCTION

Tenement

The Sand King deposit is located on the granted mining tenement M24/960, which is 100% owned by Siberia Mining Corporation Pty Ltd, a wholly owned subsidiary of Ora Banda Mining Limited. OBM holds rights to gold and its byproducts over all this tenement. There are no known heritage or native title issues. The tenement is in good standing with no known title risk. Tenement M24/39 is held by Robert Gardner, Gardner granted Siberia the right to explore for Gold Minerals (gold and silver mineralisation in any form) (entire tenement). In relation to the "Reduced Area", Siberia has continued exclusive and overriding rights to carry out exploration and mining operations. Robert Gardner has priority of rights over the "Remaining Area" of M24/39. Various infrastructure is in place or planned in the M24/39 tenement including haul roads, an open pit ramp, a section of decline and a WRL.

Permits and Licenses

The required environmental approvals to operate the Sand King Underground mine are in place:

- Siberia Gold Operations Mining Proposal Amendment (Reg Id 500381)
- Siberia Gold Operations Mine Closure Plan for Mining Proposal (Reg Id 121808)
- Mine Dewatering Works approval number W6904/2024/1
- Clearing Permit 6968/4

The works approval permits the construction of dewatering infrastructure from Sand King to the nearby Palmerston Pit and/or Missouri Pit for water storage. A construction certificate was submitted in November 2024 which completes the application for a Category 6 Dewatering Prescribed Premise Licence which is being assessed. The operations remain compliant with all the current permitting requirements, and as such they remain in full force. A rehabilitation obligation remains at Siberia post open pit mining.

Mine Infrastructure

The Siberia Gold Operation is an established mining centre with extensive offices, workshops and communications. ROM pads, waste rock landforms and haul roads are established along with bore fields and water storage dam and pits. The facilities are sufficient for operation of the Ore Reserve mine design. The mine is located in the Siberia Gold Operation 37 km to the south east of Davyhurst processing facility

The Sand King underground mine commenced in August 2024, establishing declines, rises, ventilation and escapeway infrastructure. Three production levels have been accessed up to 30 June 2025 with development and stoping ongoing. A 5 MW diesel power station supplies HV power via a service hole to underground substations and distribution network. A dewatering capacity of 30 l/s is currently in place along with 3,265 ML in nearby pit storage capacity. Permitted waste rock storage capacity remains as well as pit backfilling opportunities.

The Davyhurst village is 35 km from the mine offices. Additional rooms were constructed in FY25 for a total of 259 person capacity.

The Davyhurst processing facility is located 37 km via well-established public and private roads to the north west of Siberia. Road trains are used to haul ore from the mine ore pad at Sand King to the Davyhurst RoM pad.

MINERAL RESOURCES

Mineral Resource Estimation: Summary Information as required under Australian Securities Exchange (ASX) Listing Rule 5.8.1 follows.

GEOLOGY & GEOLOGICAL INTERPRETATION

Lithology

Mafic rocks of the Siberia area have been assigned to the Wongi and Missouri Basalt Units of the Pole Group, while the ultramafics to their south and east are assigned to the Walter Williams Formation. Gold mineralisation associated with the Sand King deposit is hosted entirely within Missouri basalt, immediately west of the boundary with the komatiite-dominated Walter Williams Formation. Within the Missouri Basalt are two distinct units, a pillowed unit and a younger feldspar phyric, columnar jointed unit. Stratigraphic layering in the Siberia area strikes NE-SW and dips moderately towards the south-east and forms part of the western limb of the regional-scale Kurrawang Syncline. Numerous examples of younging direction in pillows are observable in the pit. The pillowed unit is more massive (competent) than the columnar basalt and is the preferred host for gold mineralisation. Two narrow interflow sediments and two narrow ultramafic units with limited continuity have been observed in core logging within the mafic package. A thin dolerite is also present.

Aplite dykes form a NE-trending, NW dipping dyke swarm that cuts both the western and eastern units of the Missouri Basalt. The dykes are up to 5 m thick. The composition of the dykes is probably equivalent to that of monzogranite. Aplite dykes predate mineralisation and are occasionally mineralised where proximal to mineralised structures.

Structure

There are several structural styles and orientations associated with Sand King gold mineralisation. The current structural history includes development of early conjugate, ductile shear structures striking ~010° and 330° and dipping moderately to the east. Subsequently brittle tension veins striking 060° and 090 ° developed and introduced the bulk of the gold mineralisation.

Kinematics show dextral movement on the 010° and sinistral movement on the 330° shears. 010° shears are frequently exploited by the later aplite dykes. Shears are sometimes quartz filled with weak boudinage and sometimes dry with no observable quartz or alteration. Quartz deposition and gold precipitation at Sand King is dominantly associated with later tension veins in either 060° or 090° orientation and dipping steeply north. 060° striking veins tend to have the greatest continuity while the 090° veins tend to form linking structures between the 060° veins and have shorter continuity. Movement along the tension vein structures is primarily strike-slip, supported by sub-horizontal slicken lines on exposed planes. Later dextral movement along 060° tension veins is evident, and an extreme example is in the north-east of the pit. Here shearing has formed en-echelon quartz arrays. Tension vein mineralisation presents as linear en-echelon veins, sigmoidal vein arrays and laminated quartz veins.

When the tension veins intersect the 330° and 010° shears the ore bearing fluids migrate up and down the shear, causing grade and volume "blowouts". The intersection of the steep north dipping tension veins with the moderate east dipping 330° and 010° shears give a steep north plunge to the high-grade blowouts. The blowouts form pipe-like features.

Alteration & Mineralisation

There are two alteration events at Sand King, including an initial pervasive greenschist alteration event related to regional metamorphism, and a later hydrothermal alteration event related to gold mineralisation. Gold mineralisation typically occurs in a series of quartz veined, biotite-albite-calcite-pyrite-pyrrhotite lodes. Typically, the lode alteration extends for only 1-1.5 m away from the quartz veining although at times, zones of alteration up to 5m from veining have been noted. Pyrite is the dominant sulphide as disseminations in wall rock and clusters within veins. Pyrrhotite (FeS) is noted to replace pyrite (FeS_2), infilling pressure shadows around pyrite euhedra. This suggests an evolution of the mineralising hydrothermal fluid from a S_2 rich to S_2 depleted composition. Other sulphide minerals, observed in hand specimen and/or polished thin sections include, galena, altaite (Pb telluride), chalcopyrite, molybdenite, Ilmenite, bismuth tellurides and sphalerite with arsenopyrite notably absent. Tungsten, in the form of scheelite is commonly present.

Weathering

The oxidation profile at Sand King is also thin (<20 m) outside the main deformation corridor that hosts mineralisation. Within the mineralised corridor weathering extends to approximately 40 m below surface at which point the transition to unweathered material occurs over an average distance of 20 m.

DRILLING AND SAMPLING, AND SAMPLE ANALYSIS TECHNIQUES

Modern exploration in the Siberia area commenced in the 1980s by Western Mining Corporation (WMC) and was followed by numerous operators who held the tenure for various periods. Although a significant proportion of drilling data is from previous operators, it is generally well documented and to industry standards of the time. In addition, OBM has added significant drilling to the Siberia

deposits. All RC and diamond drilling at the deposit is deemed suitable for resource estimation purposes.

Previous operators include WMC, Gilt-Edged Mining, Gold Fields Ltd, Siberia Mining Corporation (SMC), Monarch Gold Ltd and Eastern Goldfields.

RC drilling was completed by all operators. Hole diameters for WMC, Gilt-Edged Mining and Gold Fields Ltd are unknown. All other operators drilled either 4 inch (Monarch Gold) or >5 inch diameter holes (Ora Banda). Diamond core holes were generally HQ or NQ diameter, though WMC drilled some BQ diameter holes. Diamond core by WMC was not oriented, other operators oriented the core. Collar locations were surveyed by various contractors and methods including theodolite (WMC), Differential GPS (Gilt-Edged Mining, GoldFields Ltd, SMC, EGS) and RTKGPS (Monarch Gold, OBM). Underground diamond collars are surveyed by mine surveyors.

RC holes by WMC were generally not downhole surveyed. RC holes by other operators were downhole surveyed by magnetic methods such as Eastman single shot or electronic multi shot. Early diamond holes by WMC were downhole surveyed by Eastman single shot or multi-shot camera approximately every 30 m. Later operators surveyed RC holes with electronic multiple shot, Eastman single shot (SMC, EGS) or Gyro (OBM). Diamond holes by more recent operators (Siberia Mining Corporation - Ora Banda) were north seeking gyro surveyed. Underground GC holes are downhole surveyed by Devi rate gyro.

All RC grade control holes drilled by OBM were surveyed by the mine surveyor and downhole surveyed by rig north seeking gyro.

Percussion samples were generally collected at 1 m intervals, split in the field, generally using a riffle splitter to produce a 2-3 kilogram subsample. Some operators composited the 1 m samples to either 2 m, 4 m or 5 m intervals using a spear or scoop to sample from the split reject. The bagged, split 1 m samples were submitted for assay if anomalous composite assay results were returned. Core was generally cut in half and sampled at geological boundaries (Gold Fields Ltd, OBM) or 1 m intervals (SMC). RC samples from Delta Gold were collected through a cyclone in large plastic bags at 1 m intervals. Underground GC core was sampled to geological boundaries with a minimum sample length of 0.3 m. GC core was whole core sampled. All drill holes were logged by qualified geologists.

OBM RC drill sample recovery is monitored and visually checked for recovery, moisture and contamination. RC sample weights were recorded at the laboratory and monitored.

Historical QAQC protocols used by companies prior to Gilt Edged Mining's ownership have not been documented in any detail. Gilt Edged Mining routinely used standards, field duplicate samples and check analyses at a second laboratory to monitor analytical quality. SMC used standards and field duplicates (1 in 20) during drilling campaigns to provide a reference material to monitor laboratory performance. Monarch Gold submitted Certified Reference Material every 20th sample in both RC drilling programmes. Duplicate samples were submitted every 25th sample for RC drilling. The protocol adopted by OBM required CRM standards and blanks be inserted every 25 samples for RC and diamond drilling. The frequency rate of duplicate samples was nominally 1 every 25 m. Underground diamond drilling and face CRM standards and blanks were inserted at a rate of 1:20.

Post the 2024 MRE Ora Banda completed 6 surface diamond holes (1,452 m), 307 UGGC holes (36,042 m) and sampling of 405 faces (1935 m). This significant program of drilling and face sampling is included in the current MRE.

Sample Analysis Methods

All WMC samples were analysed at the WMC exploration division laboratory by 25g Aqua Regia with AAS finish. Gilt Edged mining analysed composite samples by MinLab, Kalgoorlie using 25g Aqua Regia, AAS finish. Individual 1 m samples from composite results >0.2 g/t were submitted to Genalysis in Perth for fire assay with a 50 g charge. RC and diamond samples collected by Gold Fields Ltd were dried, crushed, split, pulverised and a 50 g charge taken for fire assay at Australian Laboratory Services in Kalgoorlie. All assaying by SMC was done by either SGS Analabs in Kalgoorlie or Ultratrace using a 50 g charge taken for fire assay. Monarch gold assayed by 50g fire assay with AAS finish. Samples were submitted to both ALS Laboratories and Ultratrace.

Eastern Goldfields utilised Intertek-Genalysis in Kalgoorlie, Kalassay in Kalgoorlie, SGS in Kalgoorlie and Nagrom Laboratories in Perth for sample analysis. A 50gm charge was taken and analysed by fire assay ICP-OES. Drilling completed in 2020 by Ora Banda utilised Nagrom Laboratories in Perth and SGS in Kalgoorlie for sample analysis. A 50 g charge was taken and analysed by fire assay ICP-OES. For 2023 and 2024 drilling Ora Banda utilised the SGS on-site facility for sample preparation with pulps sent to SGS in Kalgoorlie for analysis. A 50 g charge was taken and analysed by fire assay MP-AES. Initial underground drilling and face sampling was assayed by SGS, Kalgoorlie by fire assay MP-AES. From December 2024 underground sample submissions were sent to SKS Kalgoorlie for sample preparation and assay by Photon assay method. Transfer of analytical method from fire assay to Photon assay followed a program of comparison assaying whereby Photon assay analysis was done on the crush reject of samples already assayed by fire assay. Underground diamond core is predominantly whole core sampled.

ESTIMATION METHODOLOGY

All lode interpretations and block models were created in Sand King Mine Grid (SMG). This grid is rotated through 60° so that 060° (MGA) is 000° in SMG. 4000 m is added to AHD elevations. The block model was also prepared in SMG so that the long axis of blocks is parallel to the strike of the dominant mineralisation.

Ore lode interpretation was based on a ~1 g/t cut-off, determined from a log-probability of raw assays from resource drilling, and influenced by the presence and intensity of quartz veining and the dominantly biotite+sulphide rich alteration. Sub 1 g/t intervals were included in the interval selection if alteration was observed in core photos and logging. Generally, there was no restriction to internal grade dilution. Domain/waste boundaries were treated as hard boundaries and for estimation purposes the mineralised domains were not separated into oxide, transitional and fresh sub domains. Lodes were generally interpreted on E-W sections in Leapfrog™ software using structural measurements to help determine whether a drill intercept should be in a 090 or 060 (MGA Grid) lode or in a shear orientation. All RC and diamond drill samples and face sampling were used to inform the interpretation.

One metre composites were calculated from the raw assay data with a minimum length of 0.3 m. Residual intervals were distributed across the composited interval. Supervisor™ software was used to establish spatial grade continuity. Top cuts were applied to the composite data on a domain basis to reduce the influence of occasional extreme gold grades.

Block model block size is 4mE x 10mN x 10mRL (SMG) with sub-celling to 0.5mE x 1.0mN x 1.0mRL. Estimation was done into the parent blocks. Kriging Neighbourhood Analysis (KNA) was used to define the estimation neighbourhood parameters, including search distances, minimum and maximum samples and discretisation. Estimation was completed using three runs, each with less restrictive search and minimum sample parameters. Search anisotropy was established from the geostatistical evaluation. Grade thresholds were used for certain lodes to limit the influence of high grade composites at significant distances from the block being estimated. Grade thresholds are applied when distances exceed a given percentage of the search distance.

Oxidation was applied based in DTM surfaces defined from geological drill logs and observations of the pit walls. Values were applied according to oxidation state. Density values were established from 2311 drill core measurements (water immersion method) and referencing historic results from bulk metallurgical samples.

Surface topography was established by recent completion of mining pit surveys completed by the Mine Survey department and a regional Arvista survey completed in 2017.

Underground mining depletion is applied as at 30 June 2025 from solid wireframes produced by the mine survey department.

CRITERIA USED FOR CLASSIFICATION

Wireframe solids were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, measured, indicated or inferred:

- Measured - Close spaced grade control drilling where geological and grade continuity is well established.

Areas classified as Indicated are defined by:

- Good support from drilling, averaging a nominal 40 mN x 40 mRL
- Reasonable confidence in the mineralised lode interpretation.

Inferred Resources are defined where there is a lower confidence in geological and grade continuity as defined by a lower concentration of drilling data. Inferred resources are defined by:

- Drill spacing typically greater than 40 mN x 40 mRL
- Lodes defined by three or less drillholes

Inferred Resources are generally located around the periphery of ore lodes, particularly at depth at Sand King where drilling is sparse.

CUT-OFF GRADES AND MODIFYING FACTORS

The Mineral Resources have been reported from fresh material at a diluted cut-off of 0.9 g/t Au inside Mine Stope Optimiser (MSO) derived solids with dimensions of 10mN x 10mRL and a minimum width of 1.6 m. Individual MSO blocks were assessed and removed if above the 350RL (base of current as-mined pit).

ORE RESERVES

Material Assumptions and Outcomes, Criteria for Classification

The Ore Reserve was derived from technical studies incorporating project-specific costs as well as geotechnical analysis, dilution and recovery parameters and is based on the current 2025 MRE. Processing parameters were based on recent test work combined with historical recent processing recoveries. Hydrogeological conditions were determined from recent mining of the Sand King pit and underground, as well as information obtained from extensive Resource drilling.

Costs were derived from the FY26 budget estimate including contract pricing current at the date of this Ore Reserve. Unit costs for mining were estimated based on fully resourced contracted scope of work of which this Ore Reserve forms a portion. Unit costs for haulage, processing, site administration and head office overheads were calculated using the combined project cost model with the Ore Reserve mine schedules and stockpiles.

The Sand King Underground Ore Reserve was estimated using a gold price of A$2,500/oz.

The dilution skin method was employed to reflect the selective mining method proposed for Sand King Underground. Dilution parameters were based on a geotechnical assessment of the expected mining environment. A cut-off grade of 2.5 g/t was applied to determine economic mining envelopes using Deswik™ ASD. Costs derived from the FY26 budget including contract pricing current at the time were used to validate the Ore Reserve cut-off grades.

Mining extraction ratios for the underground Ore Reserve is dependent upon the dimensions and spacing of pillars throughout the orebody. The Sand King mine design assumes 40 m open stopes (along strike) and pillars of 5 m by 17.5 m. The 40 m stope strike extents are considered a practical distance over which to successfully operate remote loaders to recover ore from open stopes. Sill pillars have been considered via a stope recovery of 72% where stoping extends more than 4 levels down dip on a mineralised lode A 5% stope ore loss was also included for operational losses. The overall mining recovery was estimated to be 84%.

Mining Method

The underground mine design is premised on a conventional longhole open stoping mining method, commonly used in the Western Australian Goldfields.

Mining equipment will be mechanised, with equipment to include electric-hydraulic drills for development and production, and rubber tyred loaders and trucks for load and haul activities. Production loading will incorporate conventional and tele-remote loading for non-entry mining stopes.

Based on the geotechnical assessment, which identified favourable ground conditions and low stress environment, as would be expected at the shallow mining depths of no more than 250mbs, no stope backfill is contemplated.

Cut-off Grades

The Sand King cut-off grade was calculated to be 2.5 g/t for production stoping ore. The cut-off grade calculation was estimated at a gold price of A$2,500/oz, and is inclusive of mining, transport, processing, overheads, sustaining capital and royalties.

A cut-off grade of 2.0 g/t was applied to the underground development based on the incremental cost of developing hauling and processing of the ore. The calculation was estimated at a gold price of A$2,500/oz.

Low Grade insitu material is 0.7 g/t to 2.0 g/t, based on the surface SP cut-off where haulage, processing, admin costs are applicable and using a gold price of A$4,400/oz.

Recent Sand King mine contractor costs and OBM budget costings were used.

The WA state royalty of 2.5%NSR plus a 1%NSR Private company royalty apply.

Processing Method

The process for treating ore at the DGP is conventional CIL with some gold recovered via gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. The process plant has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm. The process plant has been successfully operated at this rate with recent improvements made. The processing recovery applied to Sand King Underground was 87% and was based on metallurgical test work. The recovery performance was 88.1% through Davyhurst plant in FY25 of which 13% was Sand King underground feed.

Estimation Methodology, and Modifying Factors

The ore drive width is designed at 4.5 metres allowing access for larger mechanised mining equipment. A combination of full face and split firing will be undertaken. Split firing is suitable in the south and far north zones where the mineralisation is ~ 1m. Given the nature of the mineralisation 12% of ore drive advance has been assumed to be split fired which will further reduce dilution. The practice has been successfully undertaken at Ora Banda mines with similar styles of mineralisation.

Given the nature of the mineralisation, the global dilution, inclusive of stoping and ore drive development, equates to 32% of material. Background grades were estimated into the block model and were included in the dilution modelling. Dilution grades varied between zero and 0.5 g/t depending on the nature of the alteration halo. The global average grade of dilution was estimated to be 0.15 g/t. Dilution being all included material less than 0.7 g/t.

Delineation of economic stoping areas was completed using Deswik™ software. Mineable “stope” shapes were created to simulate fully diluted stope blocks. The stope shapes are then depleted by development ore drives and modifying factors are applied in the mine schedule. Stope selection was optimised using a cut-off grade of 2.5 g/t.

A minimum stope mining width of 1.6 m was applied in the dilution modelling process, with an additional 0.6 m dilution skin applied to all valid stope shapes (0.3 m hanging wall and 0.3 m footwall). In addition, a nominal provision for unplanned dilution of 5% @ 0 g/t was also included as a contingency to all stoping panels.

Inferred material was not considered in defining the stoping envelopes; however, due to practical mining geometries a small portion of Inferred material is included within the Underground Ore Reserve. This material was included at the edges of the mining envelope and equates to 36,064 t at a grade of 2.04 g/t, representing 2.6% of the Sand King Underground Ore Reserve ounces. The Inferred inventory was not considered material to the economics of the project. The RESCAT for each scheduled task was attributed with the RESCAT of the dominant mass of material above 0.5 g/t.

The economic viability of the Sand King Underground was confirmed using current commercial parameters in a project evaluation cash flow model inside the greater multiple mine company model. This model also considered project phasing, stockpiling, sustaining capital and the effect of fixed costs. The cash flow modelling was based on a gold price of A$3,300/oz. The mine demonstrated a positive net cash flow with acceptable returns. Overall unit mining costs for the underground was estimated to be A$168/t ore, inclusive of sustaining capital.

Mine Design

The mine design for the Sand King Underground on which this Ore Reserve was based is shown in Figure 10. The mine entries consists of a main access portal and primary ventilation portal. Both are located in the fresh rock portion of the existing Sand King pit.

The primary ventilation is via a vent portal to the Sand King open pit. Return air drives are designed 5 m x 5 m with vertical rises ~6 m x 4 m. The system can meet the demand at various stages of mine life including the Ore Reserve design and schedule.

Underground pump stations are in place and have been allowed for in the design. Mine dewatering is further pumped 500 m to a water storage pit with 175,000 kl capacity. Dewatering pipelines are capable of 40 l/s and pumps to suit demand.

The decline is 5.5 m wide x 5.7 m high with a typical gradient of 1:7. Ore drives are designed to be 4.5 m wide x 4.5 m high. The average floor to floor slope distance between levels is set at 22 metres, with an average stope panel height of approximately 17.5 metres. Stope parameters used in the Riverina mine design are shown in Table 12.

The current Ground Control Management Plan provides stope and pilar analysis and guidance in line with the stope parameters used.

Table 12 - Sand King stope parameters

Stoping Parameters		
Sub-Levels	22	m
Stope Width	1.6	m
Dilution FW	0.3	m
Dilution HW	0.3	m
Stope Length	~40	m
Ave Stope Width	3.2	m
Pillar Width	5	m
Sil Pillar Recovery	72	%
Sil Pillar frequency	~88	m
COG	2.5	g/t
Schedule Dilution	5%	0g/t Dilution
Schedule Recovery	95%	

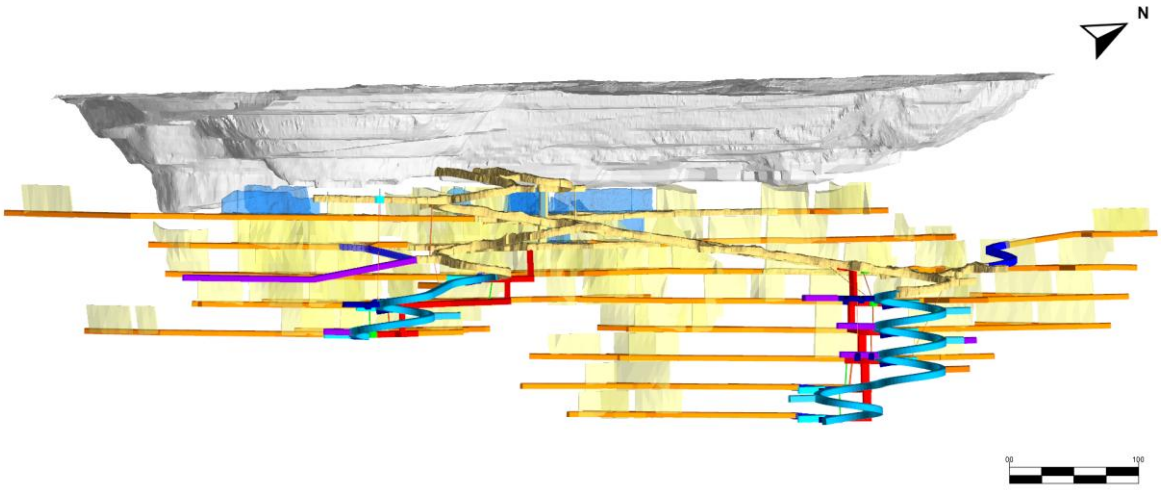

Figure 10 - Sand King Underground Ore Reserve mine design with Sand King pit (looking north west)

Sand King Underground Mine Schedule

A mine schedule for the Sand King Underground Ore Reserve was developed, with productivity rate assumption in line with contractor expectations.

The mining sequence assumes top-down echelon mining with no current plans to backfill stopes. The primary mining equipment levels on which the mine schedule was based are shown in Table 13. The ORE schedule was used in the economic assessment.

Table 13 - Sand King primary mining equipment levels

Equipment		
2x Jumbo	Sandvik DD421	Twin Boom
2x Long Hole Drill	Sandvik DL431	76mm holes
3-2x Loader	Cat 2900XE	17T
2-3x Truck	Sandvik TH663	60T

Economic Assessment

An economic assessment was carried on the Sand King Underground to validate the Ore Reserve Financials. The cash flow was modelled in real terms on a pre-tax basis. Recovery and revenue parameters used were as described above.

Costs were derived from the FY26 budget estimate including contract pricing current at the date of this Ore Reserve. Unit costs for mining were estimated based on fully resourced contracted scope of work.

Mining overheads were based on OBM budget provisions for supervision and technical support, as well as contractor fixed costs, general operating expenses, FIFO flights and accommodation. Dayworks provisions were also included for miscellaneous works during operations as well as closing of the site.

Unit costs for haulage, processing, site administration and head office overheads were calculated using the combined project cost model with the Ore Reserve mine schedules and stockpiles.

An allowance for capital has been used in the economic modelling and based on recent actuals and budget forecasts. The allowance covers:

- UG sub stations with HV cabling,
- Power station payments,
- Dewatering and mine water pipeline and pump stations,
- Escapeway ladders, and
- Primary ventilation controls and concrete works.

The ORE is based on a feasibility level of accuracy. A gold price of A$3,300/oz was used for financial assessment and the competent person is satisfied that the mine demonstrated a positive net cash flow with acceptable returns.

Ore Reserve

On the basis of the outcomes of the analysis described above, the estimated economic mining inventory was classified as an Ore Reserve under the 2012 JORC code. All of the Ore Reserve Estimate was derived from the economic portion of the Measured & Indicated Mineral Resource. Measured Mineral Resource within the economic mining envelope was classified at Proved Ore Reserve Estimate. Indicated Mineral Resource within the economic mining envelope was classified at Probable Ore Reserve Estimate. Low grade was all classified as Probable Ore Reserve Estimate. The Ore Reserve is shown in Table 14.

Table 14 - Sand King Ore Reserve, as at 1 July 2025

SAND KING GOLD PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	52	3.9	7	777	3.1	78	829	3.2	84
LOW GRADE[1]	-	-		96	1.2	4	96	1.2	4
TOTAL	**52**	**3.9**	**7**	**874**	**2.9**	**81**	**926**	**3.0**	**88**

1 Insitu material

WAIHI RESOURCE AND RESERVE

SUMMARY

The Waihi Gold project is a high grade open pit reserve within 4 km of the Davyhurst processing facility. Waihi offers a high grade option in the longer-term schedule. There has been no material change to the reserve, cost changes have been considered and the Ore Reserve has been estimated using a gold price of A$2,400/oz representing a decrease of A$200/oz from previous years Ore Reserve due to revised cost model.

A summary of the Waihi Mineral Resource and Ore Reserve estimates as at 1 July 2025, are shown in Table 15 and Table 16.

Table 15 - Waihi Gold Project Mineral Resource Estimate

WAIHI GOLD PROJECT MINERAL RESOURCE ESTIMATE[8]:									
	MEASURED		INDICATED		INFERRED		TOTAL MATERIAL		
	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	-	-	278	3.6	324	3.5	602	3.5	68
OPEN PIT	-	-	2,057	2.3	95	2.0	2,152	2.3	157
TOTAL	**-**	**-**	**2,335**	**2.5**	**419**	**3.5**	**2,754**	**2.5**	**225**

Table 16 - Waihi Gold Project Ore Reserve Estimate

WAIHI GOLD PROJECT ORE RESERVE ESTIMATE:							
	PROVED		PROBABLE		TOTAL MATERIAL		
	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000oz.)
OPEN PIT	-	-	307	2.4	307	2.4	24
LOW GRADE[9]	-	-	58	1.0	58	1.0	2
TOTAL	**-**	**-**	**365**	**2.2**	**365**	**2.2**	**26**

Notes:

1. *The table contains rounding adjustments to reflect accuracy and may not total exactly.*
2. *This Ore Reserve was estimated from practical mining envelopes and the application of modifying factors for mining dilution and ore loss, including consideration of mining and disposal of tailings.*
3. *For the open pit Ore Reserve, dilution skins were applied to the undiluted Mineral Resource estimate. The method also included internal and edge dilution resulting from forming practical mineable shapes. Dilution was incorporated in the model at the background grades estimated into the model: The average grade of dilution for Waihi was 0.16 g/t Au. The estimated average dilution at Waihi was estimated to be 27%. Ore loss was incurred in the Auto Stope Designer (ASD) Deswik™ process due to variation between mineralised lode geometry and practical dig block geometry. In addition, a nominal 5% loss was applied for further mining losses occurring through normal operations.*
4. *The Inferred Mineral Resource within the mining envelope was considered as waste when defining limits of these envelopes.*
5. *The Waihi open pit Ore Reserve was primarily estimated using a cut-off grade of 1.2 g/t Au based on a gold price of A$2,400/oz. Low Grade reserve was based on A$3,400/oz for a cut-off grade of 0.8 g/t. Costs used in the cut-off grade calculation allow for ore transport, processing, site overheads and selling costs as well as a weight average recovery of 90% for oxide, transition and fresh.*

[8] Inclusive of Ore Reserve

[9] Insitu material

INTRODUCTION

Tenement

The Waihi gold project is located on the granted mining tenement M30/255, which is 100% owned by Carnegie Gold Pty Ltd, a wholly owned subsidiary of Ora Banda Mining Limited. OBM holds rights to gold and its byproducts over this and all its tenement package. There are no known heritage or native title issues in relation to the project. The tenement is in good standing with DEMIRS and with no known title risk.

Permits and License

The required environmental approvals to operate the Waihi open pit mine are in place. The project remains compliant with all the current permitting requirements, and as such they remain in full force.

- Waihi Gold Operations Mining Proposal and Mine Closure plan (Reg Id 120936).
- GWL 180490 (3)
- Clearing permit 8882-1

Mine Infrastructure

Waihi gold project is located 120 km northwest of Kalgoorlie, 3.5 km to the west of Davyhurst processing plant and 5 km from the Davyhurst village and 120 km northwest of Kalgoorlie.

The existing features of the Waihi project consists of 3 adjoining in-pit tailings storages over the historic Waihi and Golden Pole underground mines. These underground mines were developed in the early 1900's and the open pits were mined from mid 1980's to late 1990's by various companies. The pits mined in the mid 1980's were later filled with tailings from the Davyhurst plant in the 2000's. There is an approved pipeline corridor and haul road from Davyhurst to Waihi.

The site contains a rehabilitated waste rock landform and a smaller legacy waste rock landform along with ROM pads and various access and haul roads. The rehabilitated waste rock landform is under post closure monitoring.

Figure 11 - Waihi Existing Surface Features.

MINERAL RESOURCES

Waihi Open Pit Resources are unchanged from last year.
Mineral Resource Estimation: Summary Information as required under Australian Securities Exchange (ASX) Listing Rule 5.8.1 follows.

GEOLOGY & GEOLOGICAL INTERPRETATION

Lithology

Waihi's rock pile is dominated by two main units, a high-Mg basalt and fine to medium grained tholeiitic basalt. Both rock types are variably foliated. Instances of minor interbedded discontinuous ultramafics within and proximal of the mined rockpile exist. All lithologies have been cut by a series of late stage, narrow lepidolite-bearing pegmatite dykes striking ~075° and 170°. The tholeiitic basalt is fine-medium grained, massive to weakly foliated and composed of pyroxene and white plagioclase feldspar of equigranular texture. The High-Mg basalt is weak to strongly foliated, fine to medium grained and composed of actinolite within a fibrous Mg chlorite. Komatiite units within the mine area have always remained difficult to differentiate from the high-Mg metamorphosed basalts. Historical petrographic studies and recent pXRF geochemical analysis

have a population of samples reporting to ultramafic or a protolith indicative of one. The pegmatite dykes are medium to very course-grained, quartz-feldspar-muscovite +/-lepidolite +/-tourmaline bearing units with smooth planar contacts. Metamorphism is amphibolite facies.

Structure

The most pervasive deformation event observed at Waihi is a steep westerly-dipping penetrative NNW-trending foliation attributed by a phase of intense ENE-WSW crustal shortening synonymous with the regional D2 event of the Eastern Goldfields. This event resulted in major regional-scale upright folds with parasitic S and Z folds. Early quartz veins were emplaced during this event, commonly along the basalt/high Mg basalt contact and have been folded with the rock pile. Sub-vertical ductile mineralised shears trending NNW transect the rock pile with better gold deposition occurring along the basalt/high Mg contact and where the early folded quartz is itself a host.

Alteration & Mineralisation

Mineralisation at Waihi is characterised by multiple lodes displaying alteration haloes with silica flooding and strongly deformed quartz veins and boudins sub-parallel to the regional fabric. Mineralisation is hosted in the lower amphibolite facies metamorphic suite of mafic to ultramafic rocks including tholeiitic basalts, high-Mg amphibolites and minor intercalated komatiites. Mineralisation would appear to be controlled by deep-seated ductile shear zones associated with progressive strong K-metasomatism and is typified by a biotite-altered schist. The deep-seated ductile shear zone also provides a natural conduit for high-temperature metamorphic fluids which have locally overprinted the biotite schist as prograde calc-silicate skarn-like assemblages comprising diopside – tremolite/actinolite ± microcline. Strongly biotite-altered zones contain disseminated sulphides, mainly pyrrhotite associated with pyrite and chalcopyrite and appear to have a direct relationship with mineralisation. Other sulphides such as arsenopyrite, galena and sphalerite are uncommon.

Weathering

The weathering profile in the area is poorly developed with most of the area covered by thin soils or fresh, outcropping amphibolite. In the old Waihi pit saprolite and weathered bedrock occur to a depth of approximately 15 m within the exposed ore zones. In the Homeward Bound pit, weathering is negligible. Pisolitic laterite has developed over the sedimentary rocks to the west and a veneer of laterite clay covers the east.

DRILLING AND SAMPLING, AND SAMPLE ANALYSIS TECHNIQUES

Modern exploration at Waihi commenced in the early 1980s by WMC and Billiton Australia and was followed by numerous operators who held the tenure at various periods since. Although a significant proportion of drilling data is from previous operators, it is generally well documented and to industry standards of the time. In addition, OBM has added significant drilling to the Siberia deposits. All RC and diamond drilling at the deposit is deemed suitable for resource estimation purposes. Previous operators include WMC, Billiton, Consolidated Exploration (Consex), Consolidated Gold (Consgold), Croesus, Eastern Goldfields Ltd (EGS) and Ora Banda Mining Limited.

RC drilling was completed by all operators with diameters up to 5.5 inch. Diamond drilling was completed by Billiton, Consgold, Croesus, EGS and OBM, using NQ diameter for resource drilling. EGS and OBM conducted HQ drilling for metallurgical and/or geotechnical purposes.

Early drilling conducted was surveyed using a Waihi local grid or AMG84 Zone51. Historical collars have all been converted to MGA94 Zone 51 using well established grid transformation parameters. Billiton holes were surveyed in AMG84 grid. WMC holes were located using tape and compass from surveyed north-south AMG84 baselines. Consex initially drilled on Waihi local grid and later changed to AMG84. Consgold holes were surveyed by licenced surveyors. Croesus surveyors picked up all prior drilling, apart from some early WMC holes, at Waihi using DGPS or theodolite. EGS and OBM used a contract surveyor (RTKGPS) or DGPS to locate collars in MGA94 grid. Recent collars from 2020 onwards are picked up by OBM mine surveyors in MGA grid.

Downhole survey methods for early operators (WMC, Billiton and Consex) are unknown. Consgold employed either wireline multi-shot camera, Eastman single shot camera using an aluminium barrel to minimise magnetic interference, or electronic gyro compass. Croesus holes were downhole surveyed every 10 m by electronic multi-shot or other unrecorded method. EGS downhole surveys were recorded every 30 m using a Reflex digital downhole survey instrument. Some RC holes were not downhole surveyed if they were short. Drill-hole downhole surveys are recorded every 18-30 m using a reflex digital downhole camera (2019 RC) or Gyro tool (subsequent RC and DD). At completion of drilling in-run or out-run surveys are collected every 10 m.

Sample Analysis Methods

RC samples from Billiton drilling were collected and assayed every metre. The assay method employed is unknown but is assumed to be aqua regia digest. No information is available for drilling by WMC. Phase 1 composite 2 m RC samples by Consex were analysed by multi-acid digestion and AAS. Later phase samples were pre roasted. Any results of >1 g/t Au or samples in proximity to ore grade intersections were re-assayed by fire assay using a 50 g charge. Croesus RC composite, 1 m split samples and diamond drill samples were analysed for gold (fire assay/ICP-OES) by Ultratrace Laboratories in Perth. EGS utilised Intertek-Genalysis in Kalgoorlie, SGS in Kalgoorlie and Nagrom Laboratories in Perth for sample analysis. At all 3 laboratories, a 50 g charge was taken and analysed by fire assay with an ICP-OES finish. Early drill programs by OBM utilised primarily Nagrom Laboratories in Perth for sample analysis, although a small proportion of samples went to Intertek-Genalysis in Kalgoorlie. All samples were analysed by fire assay with an ICP-OES finish. From March 2025 drill programs adopted the Photon assay method.

ESTIMATION METHODOLOGY

The resource model is for the most part interpreted to a 0.4 g/t cut-off grade guided by geological observation. A minimum of 2 m downhole width above 0.5 g/t defined a potential bedrock lode. Sometimes lodes were pushed through drillholes with grades below 0.4 g/t in order to maintain continuity. All wireframing was completed using LeapfrogTM modelling software. Ore/waste boundaries could be treated as hard boundaries for the estimation.

One metre sample composites were calculated from the raw assay data. SupervisorTM software was used to establish spatial grade continuity. The plunge is moderate (39°) towards the north and is consistent with observed geological structures (fold hinges and boudin necks) in diamond core and field mapping. Selected lodes with high variability and high maximum grades were selected for top cutting to reduce the influence of the high grade composites.

Block model block sizes are 2mE x 10mN x 10mRL with sub-celling to 0.5mE x 1.0mN x 1.0mRL. SupervisorTM software was used for Kriging Neighbourhood Analysis (KNA) to assist with defining

the estimation neighbourhood. Parameters defined by KNA were optimal block size and search distances, minimum samples and discretisation. Estimation was completed in 3 passes with an expanded search and reduced minimum/maximum samples for each successive pass.

Density readings were taken from diamond core samples. 411 readings were collected and results were applied according to oxidation state; 1.9 t/m3 (oxidised), 2.5 t/m3 (transitional) and 2.94 t/m3 (fresh).

CRITERIA USED FOR CLASSIFICATION

Existing mining at Waihi has confirmed steep west dipping to sub vertical north-west striking mineralised lodes. Where lodes are defined by two or fewer drillholes, they have been classified as inferred.

Areas classified as Measured are defined by:

- Areas covered by the grade control RC drilling completed by Croesus.

Areas classified as Indicated are defined by:

- Areas covered by closer spaced drilling where drill pierce point spacing <=30 m.

Inferred resources are defined by:

- Areas covered by wider spaced drilling where drill pierce point spacing >=30 m.

CUT-OFF GRADES AND MODIFYING FACTORS

Reasonable prospects for eventual economic extraction for the updated Waihi Open Pit Resources was confirmed by applying a conceptual A$2,400 optimised pit shell. Pit slopes used in the conceptual optimisation were based on typical slope parameters used in the Western Australian goldfields for oxide, transition and fresh respectively. Allowance was made for in-pit ramps. Assumed mining costs were applied on a progressive bench by bench basis using contractor supplied budget quotations for the DGP received in October 2019 for the DGP. Dilution factors of 15% to 20% were applied and mining recovery was 95%.

The Open Pit Mineral Resources within the A$2,400 pit shell were reported using a cut-off grade of 0.5 g/t. The portions of the Mineral Resource that exists below the pit shells was reported using a 2.0 g/t cut-off grade, being an approximate estimate of the cut off for narrow vein underground open stoping.

ORE RESERVES

Overview of Assumptions, Outcomes and Criteria for Classification

The Ore Reserve was estimated from the Mineral Resource estimates referred to in this announcement. Aside from historical mining, no depletion of the Waihi Mineral Resources was required.

The Ore Reserve is reported as at 1 July 2025.

The Ore Reserve was generated from design studies using current costs, geotechnical parameters and dilution and recovery parameters.

Costs were derived from the FY26 budget process and recent preliminary contract pricing specific to the Waihi open pit. Unit costs for haulage, processing and site overheads were estimated based on scheduled process plant throughput using material above the economic cut-off grade.

The open pit Ore Reserve was estimated using a cut-off grade derived from a gold price of A$2,400/oz. Low Grade Ore and Stockpiles were incorporated based on a gold price of A$3,400/oz. There are no existing economic surface stockpiles at Waihi.

No Measured economic Mineral Resource occurs within the Waihi mining envelope. All Indicated economic Mineral Resource within the mining envelope was classified as Probable within the Waihi open pit Ore Reserve following the application of modifying factors. No downgrading of the Ore Reserve classification was considered necessary.

Dilution parameters were validated through mining reconciliations of current DGP operations. The resource model used as a basis for the Ore Reserve estimate was a sub-celled Ordinary Kriged model. The dilution skin method was used to reflect the selective mining method used at DGP.

A weight average process recovery of 90% was used in the estimate. This process recovery was based metallurgical test work for oxide, transition and fresh.

Mining Method

The Waihi deposit will be mined by open pit methods using selective mining techniques. Ore and waste will be mined using conventional mining methods typically used in the Eastern Goldfields. Load and haul will be done by 120 tonne class excavators and 90 tonne dump trucks. This mining approach was successfully used for the load and haul of ore and waste on other Ora Banda open pit projects. Drill and blast will be carried out using conventional diesel hydraulic blasthole drills and blasting practices, typical of the West Australian Goldfields.

Selective mining of the ore will be in the across strike direction and entail separating the blasted waste from the ore at the hanging wall contact, excavating the ore, then separating the ore from the waste at the footwall contract. Ore mining will be directly supervised by Ora Banda personnel. Personnel designated as ore spotters will be present during the ore mining process and will be in direct contact with excavator operators.

A key nuance of mining the Waihi pit is the excavation and storage of tailings. Tailings will be mined by conventional load and haul fleet in combination with low ground pressure dozer (swamp dozer). Surface storage will be developed using a sequence of placing tails and waste rock to complete a landform whereby the tailings are fully encapsulated.

Processing Method

Ore is treated at the DGP using conventional carbon-in-leach (CIL) with some gold recovered via gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. The process plant currently has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm.

Test work on Waihi ores was conducted during the feasibility study in 2020. The test work showed the material to be similar in nature to ores already treated through the Davyhurst process plant. Based on the process plant design criteria (106 µm, 24 hr leach) recoveries between oxide, transition and fresh ranged from 94%, 92% and 90% respectively, with on average 57% of the gold being recovered through gravity. The overall recovery was estimated to be approximately 90% due to 93% of the ounces from fresh rock material.

Cut-off Grades

The cut-off grade used to define the economic material within the mining envelope allows for ore haulage, crusher loading, processing, site G&A and corporate overhead contributions. Standard state royalties and third party royalties were included. The cut-off grade for high grade at Waihi is estimated to be 1.2 g/t. The cut-off grade for Low Grade and Surface stockpiles is estimated to be 0.8 g/t.

A gold price of A$2,400 per ounce was used in the high grade cut-off calculation and using A$3,400 for low grade cut-off calculation.

Estimation Methodology, and Modifying Factors

Dilution modelling for open pit Ore Reserves were completed using Auto Stope Designer (**ASD**) functionality in Deswik™ software. Mineable "stope" shapes are created to simulate practical dig blocks. Dilution skins were added to both hanging wall and footwall of the mineralisation and internal and edge dilution is included resulting from forming practical mineable shapes.

A minimum ore mining width of 1.5 m was applied in the dilution modelling process. A 0.5 m dilution skin was applied to both hanging wall and footwall at Waihi for all of weathering classifications, resulting in the SMU of 2.5m wide. The average dilution is estimated to be 27% at Waihi. The dilution parameters were determined from a subjective assessment of operational performance at other DGP pits (e.g. Missouri and Riverina).

The ASD optimisation shapes with an average grade below 1.2 g/t and above 0.8 g/t were classified as Low Grade.

Background grades were estimated into the resource model and were included in the dilution modelling. Dilution grades were estimated to be 0.16 g/t for Waihi.

Ore loss was applied in the ASD process as a result of the variation between mineralised lode geometry and practical dig block geometry. In addition, a nominal 5% loss was applied in the mining schedule, to account for further mining losses occurring through normal operations.

Pit Optimisation

Pit optimisations using Whittle or similar software were carried out to inform pit design and was considered still to be a reasonable representation of the economic envelope at the revised input parameters.

Validation of Waihi's economics was based on the ultimate pit achieving the target cash costs described above (A$3,000 per ounce).

Pit Design

The pit design for Waihi was informed by previous pit optimisations and assessment of the local conditions and features, as well as current geotechnical parameters. The pit optimisation and design were validated against updated cost and revenue inputs for this Ore Reserve estimate.

The proposed pit cutback final depth will be approximately 70 m. The batter angles will vary between 50^0 and 85^0 (excluding tailings). Berms will be between 5 m and 7 m in width, with the batter face heights of 15 m to 25 m. The parameters used were based on geotechnical assessment. Detailed tailings geotechnical test work and modelling was done to determine the excavation geometry in the insitu tailings. Based on the study results, the stable overall slope angles of in the insitu tailings were designed to be no more than 9.5^0. The pit ramp width will be single lane 15 m wide ramp to accommodate Komatsu HD-785 trucks. Passing bays will be located at switch backs and berms.

The Waihi ultimate pits (North Pit and Central Pit) are shown in Figure 12.

Geotechnical test work and modelling was carried out on the relocation and storage of the insitu in-pit tailings. From this analysis, a detailed methodology for constructing stable Waste Rock Landforms (WRL) was developed whereby the majority of mined tailings are stored on top of the existing in-pit tailings and then encapsulated with co-mingled tailings and fresh rock. The proposed WRL has been approved by the regulator (Waihi Mining Proposal Reg ID 120936).

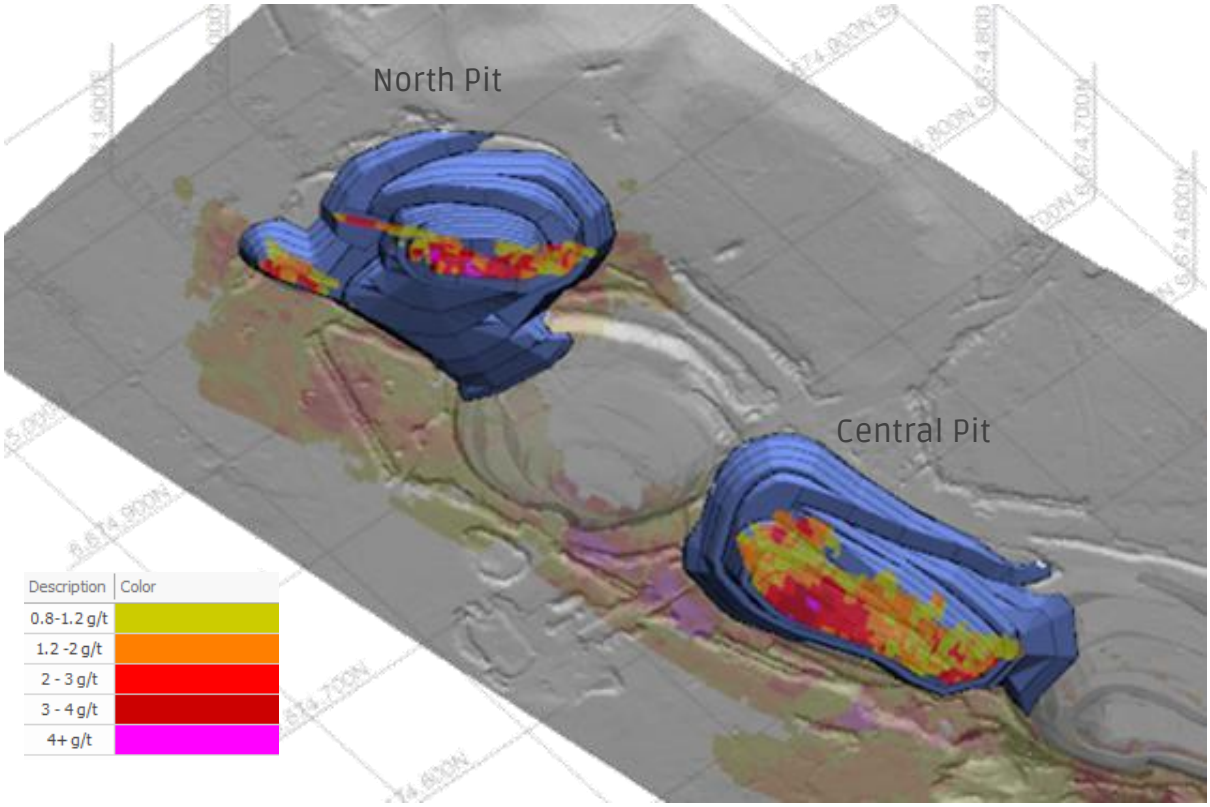

Figure 12 - Waihi open pit designs showing diluted block model >0.8 g/t

Open Pit Mine Schedule

The project comprises the Central Pit and North Pit. Both pits are currently backfilled with tailings from an earlier mining episode. The removal and disposal of tails formed part of the operational considerations and costing. The Central pit will be prioritised in the first 3 months to enable regulation of the tailings movement and accelerate ore delivery to the ROM. Management of the tailings handling, deposition and sequencing will be an important consideration for the project. The Waihi pit will be mined over a period of approximately nine months.

The cash flow modelling was based on a gold price of A$3,400/oz. All pits demonstrated a positive net cash flow with acceptable returns.

STOCKPILES

Stockpile inventories consist of ROM stocks and low-grade stocks mined under ownership of Ora Banda as of 1 July 2025 and above the economic cut-off grade are shown in Table 17. The cut-off grades vary based on location and allows for ore haulage, crusher loading, processing, site G&A and corporate overhead contributions. The total of these costs was estimated to no more than A$89 per tonne depending on mining location. Recoveries used were based on metallurgical test results of the source deposit. The cut-off grades estimated are no less than 0.7 g/t for surface stockpiles.

Table 17 - Ore Reserve stockpiles

Location	Stockpile ID	Grade Bin	Material Type	Dry Tonnes	Grade	Ounces
Davyhurst	DH-RV-HG	HG	Fresh	1,305	4.98	209
Davyhurst	DH-RV-MG	MG	Fresh	1,221	2.99	117
Davyhurst	DH-RV-LG	LG	Fresh	16,914	1.31	712
Davyhurst	DH-RV-SKY	LG	Fresh	1,418	0.76	35
Davyhurst	DH ROM L (LG)	LG	Oxide	15,509	0.92	459
Davyhurst	DH-SK-HG	HG	Fresh	1,985	3.94	251
Davyhurst	DH-SK-LG	LG	Fresh	8,767	1.42	400
Davyhurst	DH-Crushed	MG	Crushed	12,822	2.95	1216
Davyhurst	FOS A	MG	Crushed	12,734	1.60	655
Davyhurst	FOS C	MG	Crushed	8,347	2.40	644
Davyhurst	FOS D1	HG	Crushed	753	4.71	114
Riverina	RV-HG1	HG	Fresh	1,588	5.45	278
Riverina	RV-MG1	MG	Fresh	1,005	2.98	96
Riverina	RV-LG1	LG	Fresh	52,028	1.28	2,141
Riverina	RV-MG2	MG	Fresh	6,844	2.60	572
Riverina	RV-MG3	MG	Fresh	7,143	3.64	836
Riverina	RV-LG2	LG	Fresh	1,426	1.40	64
Riverina	RV SKY	LG	Oxide	169,268	0.76	4,136
Riverina	RV SKY	LG	Fresh	56,423	0.76	1,379
Siberia	SK-LG1	LG	Fresh	22,906	1.43	1,053
Siberia	SK-MG1	MG	Fresh	1,664	2.25	120
Siberia	SK-MG2	MG	Fresh	135	2.72	12
Siberia	SK-HG1	HG	Fresh	2,965	4.42	421
Siberia	SK-HG2	HG	Fresh	841	3.74	101
Siberia	MS-LG 1	LG	Fresh	85,956	0.79	2,183
Siberia	MS-LG 2	LG	Fresh	243,043	0.77	5,993
Siberia	MS-LG01 O/S	LG	Fresh	1,858	0.79	47
Siberia	SK - LG -OX	LG	Oxide	15,000	0.79	381
Sub Total			Fresh	517,436	1.0	17,023
Sub Total			Oxide	199,777	0.8	4,976
Sub Total			Crushed	34,656	2.4	2,629
Total				**751,869**	**1.0**	**24,628**

OTHER MINERAL RESOURCE ESTIMATES

The DGP Mineral Resource Estimate totals 2.11 M ounces, compared to 1.95 M ounces in FY24.

Some Mineral Resources from other areas of OBM tenure have been determined by previous operators and reported under JORC 2004 and guidelines. These Mineral Resources have not been recently updated in accordance with JORC Code 2012 on the basis that the information has not materially changed since it was last reported. These include all Round Dam Trend resources, Black Rabbit and Palmerston/Camperdown from Siberia area, Sunraysia and Lady Gladys from Riverina-Mulline areas and Lights of Israel/Makai from the Central Davyhurst area. These Mineral Resources total 524 K ounces or 25% of the total DGP Mineral Resource Estimate.

All other Resources in the DGP Mineral Resource Estimate, are updated under the JORC 2012 code.

Existing surface stockpiles are not included in the Mineral Resources.

Table 18 - Total Mineral Resource Estimate by deposit

PROJECT		MEASURED		INDICATED		INFERRED		TOTAL MATERIAL		
		('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000oz.)
LIGHTS OF ISRAEL		-	-	74	4.3	180	4.2	**254**	**4.2**	**34**
MAKAI SHOOT		-	-	1,985	2.0	153	1.7	**2,138**	**2.0**	**136**
WAIHI	Open Pit	-	-	2,057	2.3	95	2.0	**2,152**	**2.3**	**157**
	Underground	-	-	278	3.6	324	3.5	**602**	**3.5**	**68**
	TOTAL	-	-	2,335	2.5	419	3.5	**2,754**	**2.5**	**225**
Central Davyhurst Subtotal		**-**	**-**	**4,394**	**2.3**	**752**	**3.3**	**5,146**	**2.4**	**396**
LADY GLADYS		-	-	1,858	1.9	190	2.4	**2,048**	**1.9**	**125**
RIVERINA AREA	Open Pit	476	1.7	2,118	1.6	117	1.5	**2,711**	**1.6**	**138**
	Underground	266	3.3	3,953	2.7	2,826	2.4	**7,046**	**2.6**	**586**
	TOTAL	742	2.3	6,071	2.3	2,943	2.4	**9,757**	**2.3**	**724**
BRITISH LION	Open Pit	-	-	386	1.6	17	1.6	**403**	**1.6**	**21**
	Underground	-	-	36	3.2	3	3.8	**39**	**3.2**	**4**
	TOTAL	-	-	422	1.7	20	2.0	**442**	**1.7**	**25**
FOREHAND	Open Pit	-	-	-	-	691	1.5	**691**	**1.5**	**33**
	Underground	-	-	-	-	153	2.5	**153**	**2.5**	**12**
	TOTAL	-	-	-	-	844	1.7	**844**	**1.7**	**46**
SILVER TONGUE	Open Pit	-	-	-	-	127	2.3	**127**	**2.3**	**9**
	Underground	-	-	-	-	77	4.5	**77**	**4.5**	**11**
	TOTAL	-	-	-	-	204	3.1	**204**	**3.1**	**21**
SUNRAYSIA		-	-	175	2.1	318	2.0	**493**	**2.0**	**32**
Riverina-Mulline Subtotal		**742**	**1.1**	**8,526**	**2.1**	**4,519**	**2.3**	**13,788**	**2.2**	**972**
SAND KING	Open Pit	-	-	-	-	-	-	-	-	-
	Underground	108	3.2	1,900	2.7	1,901	2.9	**3,909**	**2.8**	**348**
	TOTAL	108	3.2	1,900	2.7	1,901	2.9	**3,909**	**2.8**	**348**
MISSOURI	Open Pit	-	-	-	-	-	-	-	-	-
	Underground	-	-	464	3.4	246	4.9	**710**	**3.9**	**89**
	TOTAL	-	-	464	3.4	246	4.9	**710**	**3.9**	**89**
PALMERSTON / CAMPERDOWN		-	-	118	2.3	174	2.4	**292**	**2.4**	**23**
BLACK RABBIT		-	-	-	-	434	3.5	**434**	**3.5**	**49**
Siberia Subtotal		**108**	**3.2**	**2,482**	**2.8**	**2,755**	**3.1**	**5,345**	**3.0**	**508**
CALLION	Open Pit	-	-	241	3.7	28	1.6	**269**	**3.5**	**30**
	Underground	-	-	255	6.0	156	5.5	**411**	**5.8**	**77**
	TOTAL	-	-	496	4.9	184	4.9	**680**	**4.9**	**107**
Callion Subtotal		**-**	**-**	**496**	**4.9**	**184**	**4.9**	**680**	**4.9**	**107**
FEDERAL FLAG		32	2	112	1.8	238	2.5	**382**	**2.3**	**28**
SALMON GUMS		-	-	199	2.8	108	2.9	**307**	**2.8**	**28**
WALHALLA		-	-	448	1.8	216	1.4	**664**	**1.7**	**36**
WALHALLA NORTH		-	-	94	2.4	13	3.0	**107**	**2.5**	**9**
MT BANJO		-	-	109	2.3	126	1.4	**235**	**1.8**	**14**
MACEDON		-	-	-	-	186	1.8	**186**	**1.8**	**11**
Walhalla Subtotal		**32**	**2.0**	**962**	**2.1**	**887**	**2.0**	**1,881**	**2.1**	**125**
Davyhurst Total		**900**	**1.4**	**16,900**	**2.3**	**9,100**	**2.6**	**26,800**	**2.4**	**2,110**

1. The Riverina Area, British Lion, Callion, Forehand and Silver Tongue Mineral Resources have been updated in accordance with all relevant aspects of the JORC code 2012, and initially released to the market on 2 December 2019, 26 May 2020, 5 June 2020, 9 October 2020, 1 August 2022 & 16 February 2023 (Riverina Area), 15 May 2020 & 29 June 2020 (Callion), 29 July 2021 (Forehand, Silver Tongue & British Lion)
2. The Sand King, Missouri and Waihi Mineral Resources have previously been updated in accordance with all relevant aspects of the JORC code 2012 and initially released to the market on 3 January 2017 (Sand King),15 December 2016 (Missouri) and 4 February 2020 (Waihi). Subsequent MRE updates were released on 26 May 2020 and 2 July 2024 (Sand

King) and & 1 May 2022, 26 October 2023 (Missouri). Further updates to Sand King and Riverina are provided in this report.

3. All Mineral Resources listed above, with the exception of the Missouri, Sand King, Riverina Area, British Lion, Waihi, Callion, Forehand and Silver Tongue were prepared previously and first disclosed under the JORC Code 2004 (refer Swan Gold Mining Limited Prospectus released to the market on 13 February 2013). These Mineral Resources have not been updated in accordance with JORC Code 2012 on the basis that the information has not materially changed since it last reported.
4. The Riverina, British Lion, Waihi, Callion, Forehand and Silver Tongue Open Pit Mineral Resource Estimates are reported within a A$2,400/oz pit shell above 0.5 g/t. The British Lion, Waihi, Missouri, Callion, Forehand and Silver Tongue Underground Mineral Resource Estimates are reported from material outside a A$2,400 pit shell and above 2.0 g/t. Riverina Underground Mineral Resource Estimates are reported from fresh material below the A$2,400/oz pit shell within Mine stope optimised solids of dimensions 10 m x 10 m x 1.6 m minimum width at a diluted cut-off grade of 0.9 g/t. Sand King Underground Mineral Resource Estimates are reported from fresh material below 350mRL (base of open pit) within Mine stope optimised solids of dimensions 10 m x 10 m x 1.6 m minimum width at a diluted cut-off grade of 0.9 g/t.
5. Resources are inclusive of in-situ ore reserves and are exclusive of surface stockpiles
6. The values in the above table have been rounded.

APPENDIX - JORC CODE, 2012 EDITION –REPORT TEMPLATE

Section 1 Sampling Techniques and Data – Riverina

Information for historical (Pre Ora Banda Mining Limited from 1980's to 2010) drilling and sampling has been extensively viewed and validated where possible. Information pertaining to historical QAQC procedures and data is incomplete but of a sufficient quality and detail to allow drilling and assay data to be used for resource estimations. Further Ora Banda Mining Limited has undertaken extensive infill and confirmation drilling which confirm historical drill results. Sections 1 and 2 describe the work undertaken by Ora Banda Mining Limited and only refer to historical information where appropriate and/or available.

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample retrospectivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information*	• Croesus Mining N.L; All samples were dried, crushed and split to obtain a sample less than 3.5kg, and finely pulverised prior to a 50gm charge being collected for analysis by fire assay. • Monarch Gold Mining Company Ltd; Industry standard work. RC samples collected and sent to certified laboratories for crushing, pulverising and assay by fire assay (RC) and aqua regia (RAB). • Pancontinental Mining Ltd; Samples (>2kg) were crushed to 1mm, 1kg split taken and pulverised to 90% minus 20 mesh from which a 50gm aliquot was taken for assay by aqua regia or fire assay. • Consolidated Gold N.L/DPPL (Davyhurst Project PTY LTD); Industry standard work, RAB samples crushed, pulverised and a 50g charge taken for fire assay. 200gm soil samples oven dried, and pulverised, 50g charge taken for aqua regia assay. • Riverina Resources Pty Ltd; Industry standard work. RAB samples taken every metre, composited to 4m using a spear. Samples crushed, pulverised and 50g charge taken for fire assay. RC four metre composite samples were collected using a sample spear. RC and diamond samples crushed, pulverised and 50g charge taken for fire assay and/or 4 acid digest. Any gold anomalous 4m composite samples were re-sampled over 1m intervals using a riffle splitter and also sent to Kalgoorlie Assay Laboratory for gold analysis by 50g fire assay. • Barra Resources Ltd; Industry standard work. The entirety of each hole was sampled. Each RC and RAB hole was initially sampled by 4m composites using a spear or scoop. To obtain a representative sample, the entire 1m sample was split using a riffle splitter into a calico bag. Whole diamond core samples for ore zones were sampled. Entire samples were pulverised before splitting and a 50g charge taken for fire assay. • Greater Pacific Gold; Core sampling method unknown, assumed to be cut half core. RC sampling method unknown. Analysis method unknown. However, work completed by accredited laboratories, Analabs and Genalysis. • Carpentaria Exploration Company Pty Ltd; Samples were collected over 1m intervals. 1m, 2m and 4m composite samples taken depending on the rock type. Composite samples were collected using a sample spear. About 2kg samples were despatched for analysis. Samples crushed, pulverised and a 50g charge taken for fire assay. • Malanti Pty Ltd; Industry standard work. 1m samples were collected via a cyclone and passed through a triple splitter giving a 12.5% split of about 2kg. A trowel was used to scoop the samples for composites over 4m and 6m intervals. Samples for assay were then taken with composite intervals based on geology. Many of the single splits were selected for assay in the first instance. Samples packed in poly weave bags were freighted for analysis. Sample crushed, pulverised and a 50g charge taken for fire assay. • Riverina Gold Mines NL; Industry standard work, Composited RAB and 1m RC samples assayed by laboratory. Samples crushed, pulverised and a 50g charge taken for aqua regia analysis. • Riverina Gold NL; RAB samples were bulked at 2m intervals. RC holes were sampled at 1m intervals. Diamond core samples were taken at geological boundaries, sample method unknown. All samples crushed, pulverised and a charge taken for fire assay (Au) and perchloric acid digest/AAS for other elements.

		• Ora Banda Mining Limited (OBM) - 1m RC samples using face sampling hammer with samples collected under cone splitter. 4m composite RC samples collected using a PVC spear from the sample piles at the drill site. For drilling up to April 2020, RC samples were dispatched for pulverising and 50g charge Fire Assay. For drillholes RVRC20036 to RVRC20104 inclusive, 1m and 4m composite samples were dispatched to the lab, crushed to a nominal 3mm, split to 500 grams and analysed by PhotonAssay method at MinAnalytical in Kalgoorlie. 4m composite samples with gold values greater than 0.2 g/t Au were re-sampled as 1m split samples and submitted to the lab for PhotonAssay analysis. Half-core samples, cut by automated core saw. Core sample intervals selected by geologist and defined by geological boundaries. Samples are crushed, pulverized and a 40g charge is analysed by Fire Assay. For all drilling in 2022, - 1m RC samples using face sampling hammer with samples collected under cone splitter. 4m composite RC samples were taken outside of mineralised zone, collected using a scoop from the sample piles at the drill site. 1m cone spilt samples were taken within the expected mineralised zones. Core sample intervals selected by geologist and defined by geological boundaries. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay. Underground diamond drilling - Core sample intervals selected by geologist and defined by geological boundaries. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay. Underground face sample (rock chips by hammer) intervals selected by geologist and defined by geological boundaries. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay.
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Croesus Mining N.L; Auger samples were drilled by Prodrill Pty Ltd using Toyota mounted auger rig. RAB holes were drilled by either Kennedy, or Arronika or Challenge Drilling of Kalgoorlie. Challenge drilling employed a custom built RAB/AC rig. RC holes were drilled by Ausdrill Pty Ltd and diamond holes were drilled by Sandersons. Core was oriented. • Monarch Gold Mining Company Ltd; Aircore and RAB holes were drilled by Challenge Drilling. All RC holes were drilled by Kennedy Drilling Contractors with $5^{1/2}$" hammer. • Pancontinental Mining Ltd; Drilling was undertaken by Davies Drilling of Kalgoorlie using a Schramn T64 rig. • Consolidated Gold N.L/DPPL; Auger samples were collected using a power auger fitted to a 4WD vehicle. RAB drilling was undertaken by Bostech Drilling Pty Ltd. • Riverina Resources Pty Ltd; RC holes drilled with $5^{1/4}$" hammer. Unknown diamond core diameter. • Barra Resources Ltd; Holes were drilled by Resource Drilling Pty Ltd using a Schramm 450 drill rig. • Greater Pacific Gold; Schramm RC Rig with face sampling hammer, $5^{1/8}$" diameter. NQ core, Edson Rig • Carpentaria Exploration Company Pty Ltd; RC drilling by Robinson contractors. Face sampling hammer used. • Malanti Pty Ltd; Holes were drilled by Redmond Drilling of Kalgoorlie using a truck mounted Schramm rig with a compressor rated at 900 cfm 350 psi. • Riverina Gold Mines NL; Vacuum holes were drilled by G & B Drilling using a Toyota Landcruiser mounted Edsom vacuum rig fitted with a 2 inch (5.08cm) diameter blade. RAB holes were drilled by PJ and RM Kennedy using a Hydro RAB 50 drill rig mounted on a 4 wheel Hino truck with 600 cfm/200 PSI air capacity. A 51/4 inch hammer and blade were used. RC holes were drilled by either Civil Resources Ltd using an Ingersoll Rand T4W heavy duty percussion rig fitted with a 900 cfm at 350 PSI air compressor and a 51/4 inch (13,34cm diameter) RC hollow hammer or by Swick Drilling using an Ingersoll Rand TH 60 reverse circulation drill rig with 750 cfm/350 PSI air capacity and a 51/4 inch RC hollow hammer or by B. Stockwell of Murray Black's Spec Mining Services using a rig mounted on an 8 x 4 Mercedes. • Riverina Gold NL; RC hole were drilled by Green Drilling using Schramm T66 rig. Diamond holes were drilled by Longyear. Diamond holes were sometimes drilled with a RC pre-collar, HQ core and a NQ2 core drilled. • Ora Banda Mining Limited (OBM) – 5.25 to 5.5 inch diameter RC holes using face sampling hammer with samples collected under cone splitter. HQ and HQ3 coring to approx. 40m, then NQ2 to BOH. Metallurgical and geotechnical core holes drilled using HQ3 exclusively. All core oriented by reflex instrument. All core drilled in 2022 was orientated by Axis instrument. Underground diamond drilling – NQ2 coring with standard tubing (triple tubing for geotechnical), all core is oriented by Axis Champ Ori tool, rig alignment via DeviAligner tool, downhole surveys via DeviGyro-Ox tool.

Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• Auger, RAB and RC drill recoveries were not recoded by Croesus Mining N.L, Monarch Gold Mining Company Ltd, Pancontinental Mining Ltd, Consolidated Gold N.L/DPPL, Riverina Resources Pty Ltd, Barra Resources Ltd, Carpentaria Exploration Company Pty Ltd, Malanti Pty Ltd, Riverina Gold Mines NL or Riverina Gold Mines NL. However Monarch, in a Riverina resource report state that "Good recoveries for RMRC series RC drilling were observed. Minor water was encountered in 27 of the RMRC series drillholes" • Diamond Core recoveries are very high due to the competent ground. Any core recovery issues are noted on core blocks and logged. • Ora Banda Mining Limited (OBM - Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks). Underground diamond drilling – Diamond drill recoveries are recorded as a percentage calculated from measured core against metre marks and noted core loss blocks from driller's rod counts. Underground face sampling domains marked up, with chip samples taken along the sample line per domain to reduce sampling bias. • There is no known relationship between sample recovery and grade.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Croesus Mining N.L; RAB drill logs were recorded both on paper and later electronically by a Casiopia datalogger. Diamond core was geologically, geotechnically and magnetic susceptibility logged. Qualitative: alteration, colour, contact, grainsize, joint, matrix, texture, rocktype, mineral, structure, sulphide, percent sulphide, vein type, percent vein, weathering. Quantitative; percent sulphide, percent vein. Diamond core was photographed. • Monarch Gold Mining Company Ltd; Qualitative: lithology, mineralisation code, alteration, vein code, sulphide code. Quantitative; percent mineralisation, alteration intensity, percent vein, percent sulphide. • Pancontinental Mining Ltd; All drill data was recorded on computer forms and the lithological descriptions were produced by Control Data' Bordata program. Qualitative: colour, weathering, minerals, grainsize, rock, structure, alteration. Quantitative: alteration intensity. • Consolidated Gold N.L/DPPL; Holes were logged at 1m intervals using a standard logging sheet directly onto a palmtop logger. Qualitative: colour, weathering, minerals, grainsize, rock, structure, alteration. Quantitative: alteration intensity. • Riverina Resources Pty Ltd; Qualitative: lithology, minerals, oxidation, colour, grain, texture, texture intensity, alteration, sulphide, comments. Quantitative: alteration intensity, percent sulphide, percent quartz veins. • Barra Resources Ltd; Each meter from all RC drillholes was washed, sieved and collected in chip trays and stored at the Barminco First Hit Mine office. These rock chips were geologically logged using the Barminco Pty Ltd geological logging codes. This data was manually recorded on logging sheets or captured digitally using a HP Jornada hand held computer utilising the Micromine Field Marshall program and entered into a digital database at the Barminco First Hit Mine office. Each diamond drillholes was recovered according to the driller's core blocks and metre marked. The core was logged to the centimetre, and samples were marked up accordingly. The core was geologically logged using the Barminco Pty Ltd geological logging codes. This data was manually recorded on logging sheets in the field and entered into a digital database at the Barminco First Hit Mine office. Qualitative: qualifier, lithology, mineralisation, alteration, grain size, texture, colour, oxidation. Quantitative; percentage of quartz and sulphide. Core was photographed. • Greater Pacific Gold; Qualitative logging of lithology, oxidation, alteration and veining. • Carpentaria Exploration Company Pty Ltd; Qualitative: description. Quantitative; percent oxidation, percent quartz, percent pyrite. • Malanti Pty Ltd; Qualitative: description. Quantitative; percent quartz. Logged on a metre basis. • Riverina Gold Mines NL; Qualitative for Vacuum holes: colour, grain size, alteration minerals, rock type, structure, vein type, sulphides, oxidation and comments. Quantitative for Vacuum holes; percent veins, percent sulphides. Qualitative for RAB holes and RC holes from RV110 to RV295: colour, grain size, alteration minerals, rock type, fabric, vein type, sulphides, oxidation and comments. Quantitative RAB holes and RC holes from RV110 to RV295; percent veins, percent sulphides. Qualitative for RC holes from RV296 to RV350: geology, oxidation, colour and description. Quantitative for RC holes from RV296 to RV350; percent quartz. • Riverina Gold NL; Qualitative: RQD, lithology, mineralisation, alteration, weathering, veining, fracturing. Quantitative: percent quartz. • Ora Banda Mining Limited (OBM - Field logging was conducted using Geobank Mobile™ software on Panasonic Toughbook CF-31 ruggedized laptop computers. Qualitative logging: Lithology, colour, oxidation, grainsize, texture, structure, hardness, regolith. Quantitative: estimates are made of quartz veining, sulphide and alteration percentages. Core photographed both wet and dry. Magnetic susceptibility and RQD were also recorded for core holes. Underground diamond drilling – Qualitative logging: Lithology, texture, alteration, mineralisation/sulphides, structure, veining. Quantitative: estimates are made of veining, sulphide and

		alteration percentages, RQD measurements, core density measurements, core recovery per metre, fractures per metre. Core photographed both wet and dry. Underground face sampling domain logging of lithology, veining, alteration, mineralisation/sulphides with each face mapped and photographed • All holes were geologically logged in their entirety to a level of detail to support mineral resource estimation.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Croesus Mining N.L; Auger samples were taken from an average depth of 1.5m to 2m. RAB and Aircore samples were collected in buckets below a free standing cyclone and laid out at 1m intervals in rows of tens adjacent to the drill collar. Composite analytical samples (~3.5kg) were initially collected over 5m intervals for each hole and a 1m bottom of hole analytical sample. Analytical composite samples were formed by taking a representative scoop through each 1m drill sample. RC drill samples were collected in large plastic retention bags below a freestanding cyclone at 1m intervals, with analytical samples initially formed by composite sampling over 5m intervals. Where samples were dry, analytical composites were formed by spear sampling, using a 50mm diameter plastic pipe pushed through the drill cuttings in the sample retention bag to the base of the bag. The pipe is removed carefully with the contents of the pipe containing a representation of the retained metre. Wet RC drill samples where thoroughly mixed in the sample retention bag and 'scoop' sampled to form a 5m composite sample. HQ diamond core was cut into halves and sampled on geological boundaries, to a minimum of 20cm samples or on a metre basis on site. The diamond core was cut using a diamond saw, with half core being submitted to the laboratory for analysis and the other stored. Field samples were taken for RAB, RC and diamond core samples at a rate of 1 in 20. Composite analytical samples returning values greater than 0.1 g/t Au were re-sampled at 1m intervals. • Monarch Gold Mining Company Ltd; Drillhole samples were collected at 4m and 3m composite intervals. All samples at ALS Kalgoorlie were sorted, dried, split via a riffle splitter using the standard splitting procedure laboratory Method Code SPL-21, pulverised in a ring mill using a standard low chrome steel ring set to >85% passing 75 micron. If sample was >3 kg it was split prior to pulverising and the remainder retained or discarded. A 250g representative split sample was taken, the remaining residue sample stored and a 50gm sample charge was taken for analysis. All samples at Ultra Trace Pty Ltd were sorted, dried, a 2.5 – 3kg sample was pulverized using a vibrating disc, was split into a 200-300g subsample and the residue sample stored. A 40grm charge was taken for analysis. Composite samples returning anomalous values were sampled at 1m intervals using a scoop. For both RC and RAB drilling a duplicate sample was collected at every 25th sample, and a standard sample was submitted every 20th sample. • Pancontinental Mining Ltd; RC samples were collected in plastic bags directly from the cyclone at 1m intervals, split twice through a sample splitter before splitting off a 2kg sample for analysis. Samples were crushed to 1mm, 1kg split taken and pulverised to 90% minus 20 mesh from which a 50gm aliquot was taken. Field samples were taken at a rate of 1 in 10 and results show a good correlation with the original values. Samples sent to SGS were dried, jaw and roll crushed, split and pulverised in a chromium steel mill. • Consolidated Gold N.L/DPPL; Auger samples were collected at a nominal depth of 1.5m or blade refusal. Approximately 200gm of material was placed into pre-numbered paper geochemical bags. Sample numbers were entered into a datalogger linked to the GPS unit to ensure accuracy. RAB samples were collected a 1m intervals and used to create a 4m composite sample. Samples were oven dried, pulverised in a single stage grinding bowl until about 90% of the material passed 75 micron. A 50gm split sample was taken for analysis. Composite samples returning values greater than 0.19 Au g/t were sampled at 1m intervals. • Riverina Resources Pty Ltd; Auger soil samples were collected from a depth of 1.8m or blade refusal. RAB and RC 4m composites were taken using a sample spear. Samples were dried, crushed, split, pulverised and a 50gm charge taken. Composite samples returning anomalous gold values were sampled at 1m intervals using a sample spear. • Barra Resources Ltd; Every metre of the drilling was collected through a cyclone into a large green plastic bag and lined up in rows near the hole in rows of 20. The entirety of each hole was sampled. Each hole was initially sampled by 4m composites using a spear or scoop. Once each hole was logged, intervals considered to be geologically significant were re-sampled at 1m intervals. To obtain a representative sample, the entire 1m sample was split using a riffle splitter into a calico bag. Whole diamond core samples for ore zones were sampled. Samples greater than 2.5kg were riffle split to <2.5kg using a Jones riffle splitter. The entire sample was then pulverised in a Labtechnics LM5 to better than 85% passing 75 microns. A 50gm pulp was taken for assaying in appropriately numbered satchels. Composite samples that returned gold assays greater than 0.1 g/t Au and that had not been previously sampled at 1m intervals, were re-sampled at 1m intervals. In addition, any highly anomalous 1m samples were also sampled again to confirm their assay results. • Greater Pacific Gold; Sample preparation for RC and core sample unknown.

		• Carpentaria Exploration Company Pty Ltd; Samples were collected over 1m intervals. 2m and 4m composite samples were collected using a sample spear. About 2kg samples were despatched for analysis. Samples were dried, crushed, split, pulverised and a charge taken for analysis. • Malanti Pty Ltd; 1m samples were collected in plastic bags via a cyclone and passed through a triple splitter giving a 12.5% split of about 2kg which was placed in a calico bag and marked with the drillhole number and interval sampled. The 87.5% was returned to the similarly numbered large plastic bag and laid in rows on site. A trowel was used to scoop the samples for composites over 4m and 6m intervals. Samples for assay were then taken with composite intervals based on geology. Many of the single splits were selected for assay in the first instance. Samples packed in poly weave bags were freighted for analysis. Samples were dried, crushed, split, pulverised and a 50gm charge taken. RC Samples with anomalous composite assays were split and submitted for analysis. • Riverina Gold Mines NL; Vacuum hole samples were collected every metre and split. RAB samples were taken every metre through a cyclone and riffle split to a quarter and composited to 4m intervals. RC samples were taken every metre through a cyclone after being riffle split to a quarter and some composited to 4m. The residue remained on site in plastic bags whilst the quarter split was sent for analysis. For vacuum holes RVV70 to RVV125, a 30grm was taken. RC samples from holes RV110 to RV164 and vacuum hole samples were dried, crushed to nominal 3mm and a 1,000 gram split was taken for pulverising until 90% passed minus 75 microns. A 25grm charge was taken. RC samples from holes RV230 to RV350 were totally pulverised and a 50 grm charge taken. 4m RAB composite samples returning anomalous values greater than 0.1 g/t Au were sampled at 1m intervals. • Riverina Gold NL; RAB samples were bulked at 2m intervals. RC holes were sampled at 1m intervals. Diamond core samples were taken at geological boundaries. Samples were crushed, split, pulverised and a charge taken for analysis. • Ora Banda Mining Limited (OBM) – RC samples were submitted either as individual 1m samples taken onsite from cone splitter or as 4m composite samples speared from the onsite drill sample piles. Half core samples, cut by saw. Core sample intervals selected by geologist and defined by geological boundaries. For drilling up to April 2020, RC samples were dried, crushed, split, pulverised and a 50gm charge taken. For drillholes RVRC20036 to RVRC20104 inclusive, 1m and 4m composite samples were dispatched to the lab, crushed to a nominal 3mm, split to 500 grams and analysed by PhotonAssay method at MinAnalytical in Kalgoorlie. 4m composite samples with gold values greater than 0.2 g/t Au were re-sampled as 1m split samples and submitted to the lab for PhotonAssay analysis. For all drilling in 2022, - RC samples were submitted either as individual samples taken from the onsite cone splitter or as four metres composite samples taken by metal scoop. Core sample intervals selected by geologist and defined by geological boundaries, cut by saw and submitted as half core. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) MP-AES finish. Field duplicates, blanks and standards were submitted for QAQC analysis. Underground diamond drilling – Core sample intervals selected by geologist and defined by geological boundaries, selected holes cut by saw and submitted as half core and remainder of holes are whole-core sampled. All samples were dispatched to the SGS laboratory at the Davyhurst site for crushing and pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) MP-AES finish. Flushes, blanks and standards were submitted for QAQC analysis. Underground face samples as per diamond drilling, including field duplicates, rock chip samples taken via hammer sampling per geology domain. • Repeat assays were undertaken on pulp samples at the discretion of the laboratory.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable*	• Croesus Mining N.L; Auger samples were sent to Ultratrace Laboratories, Perth, to be assayed for gold using the Aqua Regia method with a detection limit of 1ppb. RAB, aircore, RC and diamond samples were sent to Ultratrace Laboratories in Perth to be analysed for gold using Fire assay/ICP Optical Spectrometry. Diamond core check samples were analysed at Genalysis of Perth. Some diamond core samples were also analysed for platinum and palladium by fire assay. • Monarch Gold Mining Company Ltd; RC samples were sent to ALS Kalgoorlie to be analysed gold by fire assay (lab code Au-AA26). This was completed using a 50grm sample charge that was fused with a lead concentrate using the laboratory digestion method FA-Fusion and digested and analysed by Atomic Absorption Spectroscopy against matrix matched standard. RC samples were also sent to Ultra Trace Pty Ltd, Canning Vale Western Australia for gold analysis by lead collection fire assay. Samples were also analysed for palladium and platinum. The Quality control at ALS involved 84 pot fire assay system. The number and position of quality control blanks, laboratory standards and repeats were determined by the batch size. Three repeat samples were generally at position 10, 30, 50 of a batch and the control blanks (one blank) at the start of a batch of 84 samples. The laboratory standards were inserted randomly and usually two certified internal standards were analysed with a batch, but it was at the discretion of the 'run builder' as

	levels of accuracy (ie lack of bias) and precision have been established.	to how many standards to add to the batch and where to place them in the run. QAQC at Ultra Trace Pty Ltd was undertaken for every 27th sample. At random, two repeat samples were chosen, one laboratory standard was inserted and one check sample was taken. The check sample was chosen if the first pass of fire assay shows anomalous value. • Pancontinental Mining Ltd; Samples were sent to Genalysis Laboratory Services Pty Ltd in Perth to be analysed for gold with a detection limit of 0.01 ppm. They were also analysed for gold at SGS laboratory using aqua regia with AAS finish. A number of samples with an assay greater than 0.2 ppm were re-assayed by fire assay. Laboratory standards indicated reasonable accuracy. • Consolidated Gold N.L/DPPL; Auger samples were submitted to ALS Pty Ltd in Perth to be analysed for gold to a detection limit of 0.001ppm using ALS's PM2005 graphite furnace/AAS technique. Samples were also analysed for calcium, magnesium and arsenic using ALS's IC205 technique. RAB samples were submitted to Minlab Pty Ltd Kalgoorlie to be analysed for gold by fire. Some samples were also sent to Amdel Laboratories Ltd Kalgoorlie for gold analysis by fire assay method FAI. • Riverina Resources Pty Ltd; Auger soil samples were sent to Ultra Trace in Perth to be analysed for gold and arsenic using an aqua regia digest and determination by ICP-MS. RC samples were submitted to Kalgoorlie Assay Laboratory for gold analysis by 50gm fire assay. Samples from holes GNRC012 to GNRC020 were also sent Kalgoorlie Assay Laboratory for gold and nickel analysis using a four-acid digest and gold analysis by 50g fire assay. Martin Zone samples were to Kalgoorlie Assay Laboratories to be assayed Ni, Co, Cr, Cu, Mg, Mn, Fe, S, As, Al, Ca, and Zn using a four acid digest with ICP-OES finish and for Au using a 50gm fire assay digest with flame AAS finish. Some samples were also sent to Ultra Trace in Perth for analysis. 312 end of hole RAB samples from the Forehand Prospect were sent to AusSpec International in Sydney for HyChips spectral analysis developed by AusSpec International and CSIRO capable of analysing dry samples stored in chip trays at a rate of at least 1,600 per day. This was undertaken to identify alteration minerals, weathered clays, Fe oxides, and weathering intensity as well as sample mineralogy including mineral crystallinity and mineral composition. (Results are in appendix 4 of Riverina Project Combined ATR 2006.pdf). Down Hole Electro-Magnetic (DHEM) surveys were conducted in RC drillholes GNRC001, GNRC003 and GNRC004 and three diamond drillholes. These surveys were completed by Outer Rim Exploration Services using a Crone Pulse EM probe. (Southern Geoscience Consultants were contracted to plan the DHEM surveys and interpret the results). • Barra Resources Ltd; Auger samples were sent to Ultra Trace Analytical Laboratories in Perth to be analysed for gold and arsenic. Gold was determined by Aqua Regia with ICP-Mass Spectrometry to a detection limit of 0.2ppb. All RC pulp samples were sent to Kalgoorlie Assay Laboratories or Australian Laboratory Services Pty Ltd (ALS) in Kalgoorlie for gold analysis. Gold analysis was completed using the 50gm fire assay technique with an AAS finish to a detection limit of 0.01ppm. Each was weighed and data captured, with the charge then intimately mixed with flux. Mixed sample and flux were fused in a ceramic crucible at 1100° C in a reducing furnace. Molten mass was then poured into moulds and allowed to cool. Lead button removed and placed in a cupellation furnace. The resultant dore bead was parted and digested, being made up to volume with distilled water. The analyte solution was aspirated against known calibrating standards using AAS. All diamond core sample pulps were sent to Leonora Laverton Assay Laboratory Pty Ltd to be assayed for gold by fire with an AAS finish to a detection limit of 0.01ppm Au. Some drillhole samples were analysed for gold (Fire assay/ICP Optical Spectrometry) by Ultratrace Laboratories in Perth. • Greater Pacific Gold; 1m RC samples submitted to Analabs for Au, Ag, Cu, Pb, Zn, As and Ni analysis. Core samples submitted to Genalysis for Au, Ag, Cu, Pb, Zn, As and Ni analysis. Ore zone samples submitted to Minlab for re-assay. Screen fire assay performed on ore zone pulps. • Carpentaria Exploration Company Pty Ltd; Samples were sent to Australian Assay Laboratories Group in Leonora to be analysed for gold with a detection limit of 0.01 g/t Au by fire assay. Repeat assays undertaken for about 1 sample in 20. Field duplicates and standards routinely submitted with assay batches. • Malanti Pty Ltd; RC samples from RRC1 to RRC7 holes were sent to Aminya Laboratories Pty Ltd, Ballarat, Victoria, to be analysed for gold by fire assay with a detection limit of 0.01 g/t Au. RC samples from holes RRC8 to RRC12 submitted to Minesite Reference Laboratories, Wangara, Western Australia to be analysed for gold by Fire Assay of 50g charge (code FA50) with a 0.01ppm lower detection limit. About 1 in 20 assays was either a repeat or duplicate. • Riverina Gold Mines NL; RC samples from holes RV110 to RV164 and vacuum hole samples were sent to Leonora Laverton Assay Laboratory Pty Ltd, Leonora, to be analysed for gold. The charge was dissolved in aqua-regia/solvent digest with a double ketone backwash and then assayed using AAS techniques with a detection limit of 0.02ppm. RC samples from holes RV230 to RV350, vacuum samples from holes RVV126 to RVV204 and RAB composite samples were sent to Multilab Pty Ltd in Kalgoorlie to be analysed for gold. The 50grm samples were digested in aqua regia and assayed by AAS techniques with a detection limit of 0.01ppm. Other RC samples were sent to Minlab in Perth to be analysed for gold using the aqua regia digest and AAS finish. For vacuum and RAB samples, about

		1 in 10 assays was a repeat. For RC holes from RV110 to RV164 and vacuum holes, at least 10 percent of a bulk order was repeated as a laboratory duplicate for quality control. • Riverina Gold NL; RAB samples were analysed for gold, silver, arsenic, lead, zinc, copper and nickel. RC samples were despatched to Genalysis to be analysed for gold by Aqua Regia/ AAS method. Diamond samples were set to Analabs in Kalgoorlie to be analysed for gold by fire with fusion AAA, copper, lead and silver by ASS with perchloric acid digestion and, arsenic by ASS with vapour generation and density using an air pycnometer. • Ora Banda Mining Limited (OBM) – Up to April 2020, all samples were sent to an accredited laboratory (Nagrom Laboratories in Perth, Intertek-Genalysis in Kalgoorlie or SGS in Kalgoorlie). The samples have been analysed by firing a 50gm portion of the sample. This is the classical fire assay process and will give total separation of gold. An ICPOES finish is used. Commercially prepared standard samples and blanks are inserted in the sample stream at a rate of 1:12. Sizing results (percentage of pulverised sample passing a 75µm mesh) are undertaken on approximately 1 in 40 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. For drillholes RVRC20036 to RVRC20104, 1m and 4m composite RC samples were sent to MinAnalytical Laboratory Services in Kalgoorlie. Sample prep involves drying and a -3mm crush, of which 500 grams is linear split into assay jars for analysis. Samples are analysed by the PhotonAssay method which utilises gamma radiation to excite the nucleus of the target atoms (gold). The excited nucleus then emits a characteristic photon, which is counted to determine the abundance of gold in the sample. For all drilling in 2022, All samples were sent to the accredited onsite SGS laboratory at Davyhurst for sample preparation. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) with MP-AES finish. Commercially prepared standard samples and blanks are inserted in the sample stream at an average rate of 1:25. Sizing results (percentage of pulverised sample passing a 75µm mesh) are undertaken on approximately 1 in 20 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. Standards and blanks were inserted into the sample stream at a rate of approximately 1:12. Duplicates were submitted at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are acceptable. Underground diamond drilling – All samples pre-April 2025 were sent to the accredited onsite SGS laboratory at Davyhurst for sample preparation. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) with MP-AES finish. Commercially prepared standard samples and blanks are inserted in the sample stream at an average rate of 1:20. Sizing results (percentage of pulverised sample passing a 75µm mesh) are undertaken on approximately 1 in 20 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. The accuracy (standards) and precision (repeats) of assaying are acceptable. Face samples assayed as per diamond core, including a field duplicate per face. From April 2025 all face sample, and UG diamond samples were assayed by PhotonAssay analysis. From March 2024 surface RC and diamond samples were analysed by PhotonAssay. Samples are crushed at the SGS onsite laboratory using dedicated Orbis crushers and analysed at SGS Kalgoorlie. • Fire assay is considered a total technique, Aqua Regia is considered partial. The PhotonAssay method is considered a total technique and is non-destructive.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• Holes are not deliberately twinned. • Monarch Gold Mining Company Ltd; Geological and sample data was logged digitally and .csv or .xls files imported into Datashed SQL database with in-built validation. Samples bags were put into numbered plastic bags and then cable tied. Samples collected daily from site by laboratory. • OBM - Geological and sample data logged directly into field computer at the drill rig or core yard using Field Marshall or Geobank Mobile. Data is transferred to Perth via email or through a shared server and imported into Geobank SQL database by the database administrator (DBA). Assay files are received in .csv format and loaded directly into the database by the DBA. Hardcopy and/or digital copies of data are kept for reference if necessary. • Data entry, verification and storage protocols for remaining operators is unknown. • No adjustments have been made to assay data.
Location of data points	• *Accuracy and quality of surveys used to locate drillholes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.*	• Croesus Mining N.L; All drilling was located using a Trimble/Omnistar DGPS with an accuracy of plus or minus 1m. Down hole surveys were either as planned or taken using electronic multi shot camera. The gird system used is AGD 1984 AMG Zone 51. • Monarch Gold Mining Company Ltd; The collar co-ordinates of aircore and RAB holes and RC holes RMRC001 to RMRC085 were surveyed using GPS. The co-ordinates of holes RMRC086 to RMRC177 were surveyed using the RTKGPS. All surveying was undertaken

	• *Quality and adequacy of topographic control.*	by staff of Monarch Gold Mining Company Ltd. Down hole surveys were undertaken every 5m by Ausmine using electronic multi-shot (EMS). The gird system used is GDA94 MGA Zone 51. • Pancontinental Mining Ltd; RC drilling at Mulwarrie was surveyed by McGay Surveys. The grid system used is AMG Zone 51. RAB drilling at Riverina South – holes drilled on local Riverina grid and transformed to MGA using 2 point transformation. Holes were not routinely downhole surveyed. • Consolidated Gold N.L/DPPL; Auger holes located on AMG grid. Some RAB holes were drilled on an AMG grid installed by Kingston Surveys Pty Ltd of Kalgoorlie. Each 40m grid peg had an accurate (plus or minus 10 cm) northing, easting and elevation position. Other RAB holes drilled on local grid. Holes located using compass and hip chain from surveyed baselines. The grid system used is AMG Zone 51. RAB holes not down hole surveyed. • Riverina Resources Pty Ltd; Collar co-ordinates were surveyed using a DGPS. Collar azimuth and inclination were recorded. Downhole surveys for most GNRC holes were by single shot and on rare occasions by gyro. Diamond holes surveyed by electronic multishot. The gird system used is AGD 1984 AMG Zone 51. • Barra Resources Ltd; Collar co-ordinates for northings, eastings and elevation have been recorded. Collar azimuth and inclination were recorded. Drillhole collar data was collected by the First Hit mine surveyor and down hole data was collected by the drilling company and passed onto the supervising geologist. The gird system used is AGD84 Zone 51. • Greater Pacific Gold; Collars surveyed on Riverina local Mine grid. 2 point grid transformation translates coordinates into MGA91 zone 51. Holes downhole surveyed by gyro (Ace Drilling). • Carpentaria Exploration Company Pty Ltd; A local Riverina South grid was employed to record collar coordinates. Holes were not downhole surveyed. Local co-ordinates were transferred to the AMG and MGA grids using a 2-point transformation. • Malanti Pty Ltd; Collar locations of re-sampled RAB holes were noted using a GPS. Holes were not downhole surveyed. Two grid systems were employed; a local Riverina grid and AGD 1996 AMG Zone 51. Local co-ordinates were transferred to the AMG and MGA grids using a 2-point transformation. • Riverina Gold Mines NL; Collar co-ordinates for northings and eastings and have been recorded. Collar inclination was recorded. The grid used was the Riverina grid which is oriented to true north. The origin for this grid is 10,000N, 10,000E located at the south west corner of surveyed M30/98. • Riverina Gold NL; For diamond holes, down hole surveys were either assumed or taken using an Eastman camera or gyro. Diamond hole locations surveyed on Riverina local grid. RC and RAB holes located on surveyed Riverina local grid. • Topography has been surveyed by recent operators. Collar elevations are consistent with surrounding holes and the natural surface elevation. • Ora Banda Mining Limited (OBM) (RC, DD) MGA94, zone 51. Drillhole collar positions were picked up by a contract surveyor using RTKGPS subsequent to drilling. Drill-hole, downhole surveys are recorded every 30m using a reflex digital downhole camera. Some RC holes not surveyed if holes short and/or drilling an early stage exploration project. Diamond drillholes completed in 2019 and 2020 by OBM were surveyed using a Gyro tool. For all drilling in 2022 Drillhole collar positions were picked up by an OBM mining surveyor using RTKGPS subsequent to drilling. All downhole surveys were taken every 10m by Gyro. Underground diamond drilling – diamond drilling collar locations picked up by mine surveyors via theodolite and known survey control points. UG diamond drill rig alignment via surveyed collar locations and DeviAligner tool, downhole surveys via DeviGyro-Ox tool. Underground face sample locations measured via laser distometer to known surveyed control points and development surveys via theodolite.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Exploration results are reported for single holes only. • Drillhole spacing is adequate for the current resources reported externally. (Examples are discussed below) • Croesus Mining N.L; Auger samples were collected to infill a 250m x 100m grid, Riverina South RAB samples were collected to infill a 400m x 80m grid and Sunraysia RC drilling was completed on a 40m x 200m grid. • Monarch Gold Mining Company Ltd; RAB holes were drilled on 200m x 40m grids and RC holes were drilled on a 20m x 20m and 40m x 20m grids. • Riverina Resources Pty Ltd; Auger soil sampling program was taken over 50m x 50m, 50m x 100m and 50m x 200m spaced grids, Silver Tongue RAB and RC holes were drilled on 25m x 25m, 25m x 50m and 50mx 50m spaced grids and Corporate James RAB holes were drilled on 50m x 100m and 25m x 100m spaced grids.

		• Barra Resources Ltd; Auger soil sampling program was taken over 50m x 50m, 50m x 100m and 50m x 200m spaced grids, Silver Tongue RAB and RC holes were drilled on 25m x 25m, 25m x 50m and 50m x 50m spaced grids, Corporate James RAB holes were drilled on 50m x 100m and 25m x 100m spaced grids, Forehand RAB and RC holes were drilled on 50m x 100m, 50m x 50m or 25m x 50m spaced grids and Cactus RC holes were drilled on 10m x 10m, 20m x 20m and 40m x50m spaced grids. • Ora Banda Mining Limited (OBM) – underground diamond drilling – typical spacing for grade control purposes is 20m x 20m. Underground face samples are taken each 3m/4m ore development cut. • Drill intercepts are length weighted, 1.0g/t lower cut-off, not top-cut, maximum 2m internal dilution.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Drilling was oriented at 90° to the strike of mineralisation and inclined at 60°. Examples are discussed below. • Croesus Mining N.L; Holes were either vertical or inclined at 60° and oriented towards the west. • Monarch Gold Mining Company Ltd; Holes were inclined at 60o and oriented towards the west. • Consolidated Gold N.L/DPPL; Holes were inclined at 60° and oriented towards either the west or east. • Riverina Resources Pty Ltd; Holes were inclined at 60° and oriented towards either the west or east. • Barra Resources Ltd; Holes were either vertical or inclined at 60° and oriented towards the west. • Greater Pacific Gold; Holes drilled to the east inclined at -58 to -60. Suitable for sub vertical N-S striking mineralisation. • Carpentaria Exploration Company Pty Ltd; Holes were inclined at 60° and oriented towards either the west or east. • Malanti Pty Ltd; Holes were inclined at 60° and oriented towards either the west or east. • Riverina Gold Mines NL; Vacuum holes from RVV1 to RVV69 and from RVV126 to RVV204 were drilled vertically. Vacuum holes from RVV70 to RVV125 were inclined at 60° and oriented either east or west. RAB and RC holes were inclined at 60° and oriented either east or west. • Riverina Gold NL; RC holes were inclined at 60° and oriented either east or west. • Ora Banda Mining Limited (OBM) – RC drilling is predominately inclined at between -50 and -60 degrees towards the west. Drilling inclined to the east is only done when lodes are deemed to be vertical or if local landforms prevent access. Underground diamond drilling – collared from decline cuddies in sub-horizontal and inclined fans cutting across sub-vertical lodes, holes are designed to optimise intersection angles and reduce bias for Main Lode East and West. Some bias is present for the Murchison lodes, given their close proximity to the drill cuddies and this impact is mitigated through detailed wall/backs mapping of Murchison lode intersections in underground workings and future targeted grade control drilling
Sample security	• *The measures taken to ensure sample security.*	• Unknown for all drilling except for the following; • Barra Resources Ltd. Samples received at the laboratory were logged in ALS Chemex's unique sample tracking system. A barcode was attached to the original sample bag. The label was then scanned and the weight of sample recorded together with information such as date, time, equipment used and operator name. • Monarch; Sample calicos were put into numbered plastic bags and cable tied. Any samples that going to SGS were collected daily by the lab. Samples sent to ALS were placed into sample crates and sent via courier on a weekly basis. • OBM - Samples were bagged, tied and stored in a secure yard on site. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• OBM has reviewed historic digital data and compared it to hardcopy and digital (Wamex) records, noting that no issues were found.

Section 1 Sampling Techniques and Data – Sand King

Information for historical (Pre Ora Banda Mining Limited from 1980's to 2010) drilling and sampling has been extensively viewed and validated where possible. Information pertaining to historical QAQC procedures and data is incomplete but of a sufficient quality and detail to allow drilling and assay data to be used for resource estimations. Further Ora Banda Mining Limited has undertaken extensive infill and confirmation drilling which confirm historical drill results. Sections 1 and 2 describe the work undertaken by Ora Banda Mining Limited and only refer to historical information where appropriate and/or available.

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	• Goldfields Group; Auger holes were drilled to a maximum depth of 1.5m. RC samples were routinely collected at 1m intervals. Diamond drill core samples were taken at geological boundaries and sawn in half. Samples pulverised at laboratory. • Monarch Gold Mining Company Ltd; RAB samples were collected at 2m and 4m composites via a scoop method at 1m intervals. RC samples were collected at 1m, 2m to 5m intervals. 1m samples were riffle split. • WMC; In early drilling by WMC, samples were "panned' for visible gold. Percussion samples were collected at 1m intervals, split in the field. Diamond core samples were cut in half or quartered. • Gilt Edged Mining NL; All RAB and RC holes were collected through a cyclone and sampled at 1m intervals, pipe or spear sampled, composited over 5m intervals. The composite samples weighing about 3kg were despatched for analysis. 5m composites with assays greater than 0.2 g/t Au were resampled by riffle-splitting the whole of each 1m sample down to about 3kg prior to being despatched for analysis. • Siberia Mining Corporation Ltd; RAB samples were collected at 1m intervals from the drillhole collar using a plastic bucket and laid on the ground. A scoop sample was taken from each sample to form a 5m composite. RC samples were collected at 1m intervals and passed through a cyclone and split using a two tiered, 75:25 riffle splitter. The split sample (approximately 2-3kg) was stored in a drawn calico bag, which was then placed next to the split sample reject (approximately 10-15kg), which was contained in UV resistant PVC bags. A representative scoop sample was then taken from each split sample reject bags to form a 4m composite sample. Diamond half core sampled at 1m intervals. • Ora Banda Mining; RC samples were routinely collected at 1m intervals and cone split. RC samples are collected at 1m intervals in calico bags directly from a cone splitter. Sample size of at least 2kg is targeted. Diamond drilling. Core sample intervals selected by geologist and defined by geological boundaries. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay.
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Goldfields Group; Auger holes were using an auger rig on the back of a Toyota Landcruiser from Snap Drilling. RC holes were drilled by Western Diamond Drillers using a Schramm Rig. Diamond holes were drilled by Mundy Drilling services using a KL1200 rig. Diamond holes were oriented. • Monarch Gold Mining Company Ltd; RC holes were drilled by Kennedy Drilling using a 4 inch blade. • WMC; RC percussion holes were drilled using a Schram Rig. RC holes were drilled using blades and hammer. The RC drilling diameter is unknown. Diamond drillholes for NQ core were drilled and reduced to BQ core at depth if necessary. Some diamond holes commenced with a percussion pre-collar. Diamond core generally not oriented. • Gilt Edged Mining NL; RC holes were drilled by either Sing Drilling or McKay Drilling. Both Kalgoorlie companies used a booster and auxiliary compressor. The RC drilling diameter is unknown. • Siberia Mining Corporation Ltd; RAB holes were drilled by ProDrill Pty Ltd of Kalgoorlie using an open hole RAB drill rig. All holes were drilled dry. RC holes were drilled by Premium Drilling Pty Ltd of Kalgoorlie using a 350/750 Schram RC drill rig and a 5.25" face sampling hammer. An auxiliary booster was used on holes deeper than 75m. • EGL; RC drilling using 5.25 inch face sampling hammer. PQ, HQ and NQ diamond core. PQ drilled from surface until fresh rock encountered, then changed to NQ for geotechnical holes. Resource holes drilled HQ from surface to fresh rock, then changed to NQ. • Ora Banda Mining Limited – 5.5 – 5.625 inch diameter RC holes using face sampling hammer with samples collected under cone splitter. Core holes have RC pre-collars, then NQ_2, HQ_3 or PQ_3 coring to BOH. All core oriented by Axis instrument. RC grade control rig is 5.5 inch diameter hammer with samples collected from a rig mounted cone splitter into calico bags which are submitted for assay. GC Drilling was carried out by Australian Surface Drill Contractors, Rock on Ground, Orlando Drilling and JDC Drilling.

Criteria	JORC Code explanation	Commentary
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• Quantitative auger, RAB and RC drill recoveries were not recoded by Goldfields Group, Monarch Gold Mining Company Ltd, WMC, Gilt Edged Mining NL, Siberia Mining Corporation, Maitland Mining NL, Newcrest Mining Ltd, Julia Mines NL, Placer Dome Asia Pacific Ltd, Goongarrie Gold Pty Ltd, Australian Consolidated Equities Ltd, Centaur Mining and Exploration Ltd, EGL, Britannia Gold NL, Glengarry Resources NL, Sundowner Minerals NL and Gutnick Resources NL. • EGL - Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks). RC sample recoveries not recorded. • Ora Banda Mining Limited – RC drilling recoveries, including Grade control RC were recorded on a pre metre basis based on sample size. Diamond Core recoveries are very high due to the competent ground. Any core recovery issues are noted on core blocks and logged. Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks). • There is no known relationship between sample recovery and grade.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Goldfields Group; Qualitative: colour, oxidation, hardness, shearing, texture, grain size, rock, alteration, minerals and Quantitative: alteration intensity, mineralisation intensity, structure intensity, vein percent. • Monarch Gold Mining Company Ltd; Qualitative: colour, oxidation, hardness, shearing, texture, grain size, rock, alteration, minerals. Quantitative: alteration intensity, mineralisation intensity, structure intensity, vein percent. • WMC; RC and diamond logging describes the dominant and minor rock types, mineralisation, oxidation, alteration, texture, vein type and basic structure. Quantitative values assigned to amounts of sulphides, alteration and veining. • Gilt Edged Mining NL; Qualitative: rock code, alteration, sulphides, weathering. • Siberia Mining Corporation Ltd; Qualitative: alteration, colour, lithology, oxidation, mineralogy, vein style, vein assemblage, remarks. Quantitative: mineralisation intensity. • EGL; Qualitative: alteration, colour, grain size, lithology, oxidation, mineralogy, structure, texture, vein style, vein assemblage, remarks. Quantitative: mineralisation intensity, vein percent. • Ora Banda Mining Limited – Field logging was conducted using Geobank MobileTM software on Panasonic Toughbook CF-31 ruggedized laptop computers. Qualitative logging: Lithology, colour, oxidation, grainsize, texture, structure, hardness, regolith. Quantitative: estimates are made of quartz veining, sulphide and alteration percentages. Core photographed both wet and dry. Magnetic susceptibility and RQD were also recorded for core holes. • All holes were geologically logged in their entirety to a level of detail to support mineral resource estimation
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Goldfields Group; RC samples were routinely collected at 1m intervals and riffle split. Diamond drill core samples were taken at geological boundaries and sawn in half. RC and diamond samples were dried, crushed, split, pulverised and a 50 gm charge taken. All sampling of resource drilling incorporated a system of standards and blanks to keep strict control on assay reliability. • Monarch Gold Mining Company Ltd; RAB samples were collected at 1m intervals and 2m and 4m composites taken via a scoop method. RC samples were collected at 1m, 2m and 5m intervals. 1m samples were riffle split. Samples were prepared with a single stage mix and grind from which an assay charge was taken Composite samples with assays greater than 0.2 g/t Au were split at 1m intervals and re-analysed. Field duplicate samples were taken and analysed every 20 samples. Blanks and standards were routinely submitted with assay batches to evaluate sample preparation and assay accuracy. • WMC; In early drilling by WMC, samples were "panned' for visible gold. Percussion samples were collected at 1m intervals, split in the field. Diamond core samples were cut in half or quartered. Samples were dried in fan forced ovens at 80°C for paper packets and 140°C for samples in calico bags, sieved using a nylon mesh. Oversize samples crushed in Jacques jaw crusher to produce -6mm sample, split employing either a rotary or riffle splitter and pulverised using Tema Swing mills prior to analysis, except for soil and stream sediment samples finer than 80 mesh. A 25grm charge was taken for assaying. • Gilt Edged Mining NL; All RAB and RC holes were collected through a cyclone and sampled at 1m intervals, pipe or spear sampled, composited over 5m intervals. The composite samples weighing about 3kg were despatched for analysis. 5m composites with assays greater than 0.2 g/t Au were resampled by riffle-splitting the whole of each 1m sample down to about 3kg prior to being despatched for analysis. Samples were despatched to MinLab in Kalgoorlie where they were dried, pulverised to a nominal 90% minus 200 mesh (75 microns) and a 25 gm aliquot taken to be analysed for gold. Comprehensive QA/QC and check sampling reports were produced. Umpire assay checks were completed using a second laboratory (Genalysis). • Siberia Mining Corporation Ltd; RAB samples were collected at 1m intervals from the drillhole using a plastic bucket and laid on the ground. A scoop sample was taken from each sample to form a 5m composite. RC samples were collected at 1m intervals and passed through a cyclone and split using a two teared, 75:25 riffle splitter. The split sample (approximately 2-3kg) was stored in a drawn calico bag, which was then placed next to the split sample reject (approximately 10-15kg), which was contained in UV resistant PVC bags. A

Criteria	JORC Code explanation	Commentary
		representative scoop sample was then taken from each split sample reject bags to form a 4m composite sample. Diamond half core was sampled at 1m intervals. Samples were dried, crushed, split, pulverised until 80% passed minus 75 microns and a 50 gm charge taken. Field duplicates were submitted. Composites with assays greater than 0.2 g/t Au were re-assayed using individual 1m re-split samples. • EGL & Swan Gold; RC samples were routinely collected at 1m intervals from a cone splitter and submitted for analysis. Samples were crushed, pulverised and a 50gm charge taken for analysis. Field duplicates, blanks and standards were submitted for QAQC analysis. Diamond core in sampled at 1m intervals or to zones of geological interest. Core samples are sawn in half. Minimum sample length in NQ core or 0.3m. • Ora Banda Mining Limited – RC samples were submitted as individual 1m split samples (cone splitter) or composited to 4m by PVC spear. Half-core samples, cut by automated core saw. Core sample intervals selected by geologist and defined by geological and/or mineralisation boundaries. RC samples were dried, crushed, split, pulverised and a 50gm charge taken. Field duplicates, blanks and standards were submitted for QAQC analysis. Grade control samples are prepared in the SGS on-site laboratory or at the SGS Kalgoorlie laboratory. GC samples are dried, crushed, split, pulverised and a 50gm charge taken for fire assay. Core sample intervals selected by geologist and defined by geological boundaries, cut by saw and submitted as half core. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) MP-AES finish. Field duplicates, blanks and standards were submitted for QAQC analysis. From December 2024 all UG diamond and face samples were analysed by PhotonAssay analysis. All samples were dispatched to the SGS laboratory at the Davyhurst site for crushing in dedicated Orbis crusher. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for PhotonAssay.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	• Goldfields Group; Auger samples were set to Analabs (Welshpool) to be assayed for gold to 1ppb by graphite furnace P605 and arsenic to 1ppm by aqua regia hydride H605. RC samples were submitted to Australian Laboratory Services (ALS) in Kalgoorlie for gold and arsenic analysis. Fire assay methods were used for gold analysis with 50gm charge, detection limit of 0.01ppm Au, while Aqua Regia methods, with detection limits of 5ppm As, were used for arsenic analysis. Diamond drill core samples were despatched to Genalysis in Kalgoorlie and analysed for gold using 50gm fire assay to 0.01ppm. A system of standards and blanks were incorporated in all sample despatches to keep a strict control on assay reliability. QA/QC re-assaying of mineralised RC intersections and interpreted structures was undertaken later in the reporting period. • Monarch Gold Mining Company Ltd; Samples submitted to ALS for 50g Fire Assay with AAS finish. Samples were also analysed at Ultratrace for gold, palladium and platinum. Submitted field duplicates, blanks and standards for QAQC analysis. • WMC; All samples were sent to WMC Exploration Division Kalgoorlie Laboratory to be analysed for gold using wet method, aqua regia leach, reading by AAS; a 25gm sample was digested with aqua regia, the gold extracted using aliquot DIBK and the solvent backwashed. The gold concentration was determined by Atomic Absorption. • Gilt Edged Mining NL; All samples were submitted to Minlab of Kalgoorlie to be assayed for gold; 5m composites were analysed by aqua regia/AAS with a detection limit of 0.01ppm and 1m samples assayed by Fire/AAS with a detection limit of 0.01ppm. Certified reference material standards were employed. Duplicate samples, analytical standards, and check analyses at a second laboratory were used to monitor analytical quality. • Siberia Mining Corporation Ltd; All samples were submitted to SGS Analabs in Kalgoorlie to be assayed for gold using 50gm Fire Assay with detection limit at 0.01ppm Au and for sulphur. Samples were also analysed at Ultratrace. Standards and repeats (1 in 20) were used during the first phase drilling campaign to provide a reference to the internal lab standards. There was a strong correlation between standard (client) and laboratory results. Repeats of composite samples showed no problems with technique or dependability with the laboratory. • EGL& Swan; Samples were sent to Intertek Assay Laboratories to be analysed for gold by 50gm fire assay. Certified reference material standards were employed for a gold range of 0.32 to 48.55ppm. Blanks were also employed. Satisfactory results were obtained for both. Field duplicates were routinely taken from RC sampling. • Ora Banda Mining Limited - All samples were sent to the accredited onsite SGS laboratory at Davyhurst for sample preparation. Prior to December 2024 samples were crushed and pulverised for fire analysis. After December 2024 samples were only crushed for PhotonAssay analysis. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for either a 50g charge Fire Assay (GO_FAP50V10) with MP-AES finish or PhotonAssay analysis. Commercially prepared standard samples and blanks are inserted in the sample stream at an average rate of 1:25. Sizing results (percentage of pulverised sample passing a 75µm mesh) are undertaken on approximately 1 in 20 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. Standards and blanks were inserted into the sample stream at a rate of approximately 1:12. Duplicates were submitted at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are acceptable.

Criteria	JORC Code explanation	Commentary
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• Selected drill intersections from WMC, Goldfields and Siberia Mining Corporation diamond core have been inspected by EGL/OBM geologists. Some WMC holes have been re-logged by EGL geologists and mineralisation identified at the reported intervals. • Drill intersections from WMC and Goldfields diamond core were inspected by Siberia Mining Corporation geologists in 2005 and mineralization was visible in core at the expected intervals. Mineralisation widths and styles are very comparable with NQ2 drilling by SMC in 2004. • Holes are not deliberately twinned. • WMC; Hand written geology logs and assays were digitally captured. • EGL; Data has been verified by reviewing original drill and assay logs. Print outs of computerized sample intervals and assays generated by WMC were used to verify the intercepts reported. Geological and sample data logged directly into field computer at the core yard. Data is transferred to Perth via email and imported into GBIS SQL database by the database administrator (DBA). Assay files are received in .csv format and loaded directly into the database by the DBA. Hardcopy and/or digital copies of data are kept for reference if necessary. • Monarch Gold Mining Company Ltd; Geological and sample data was logged digitally and .csv or .xls files imported into Datashed SQL database with in-built validation. • Ora Banda Mining Limited - Geological and sample data logged directly into field computer (Panasonic Toughbook CF-31) at the core yard or at the drill rig using Geobank Mobile. Data is exported from the logging computer, copied onto the company servers and imported into Geobank SQL database by the database administrator (DBA). Assay files are received in .csv format and loaded directly into the database by the DBA. Hardcopy and/or digital copies of data are kept for reference if necessary. • Data entry, verification and storage protocols for remaining operators is unknown. • No adjustments have been made to assay data.
Location of data points	• *Accuracy and quality of surveys used to locate drillholes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• Goldfields Group; Collar co-ordinates for RC and DD holes, including elevation were surveyed with DGPS. RAB holes were located with GPS. Downhole surveys were taken every 10m for RC and DD holes, method unknown. RAB holes not downhole surveyed. The gird system used is AGD 1984 AMG Zone 51. • Monarch Gold Mining Company Ltd; Drillhole collars were surveyed by Spectrum Surveys of Kalgoorlie using RTK GPS. Downhole surveys were undertaken by electronic multiple shot (EMS) or Eastman single shot. The gird system used is GDA1994 MGA Zone 51. • WMC; Drillhole collars were surveyed by Electronic Distance Meter (EDM) theodolite by the Kalgoorlie Gold Operations' mine surveyor. Holes also surveyed using theodolite by McGay Surveys as well as by WMC mine surveyors. WMC RC holes were generally not downhole surveyed. Diamond holes down hole surveyed by Eastman single shot camera or multishot approximately every 30m. The gird system used is AGD 1984 AMG Zone 51. • Gilt Edged Mining NL; Contract surveyors were engaged for siting of drillholes prior to drilling, pick-up of accurate drillhole co-ordinates after drilling and down-hole plunge and azimuth readings. All holes drilled after 1998 were picked up by Fugro Survey Pty Ltd of Kalgoorlie using differential GPS. The gird system used is AGD 1984 AMG Zone 51. • Siberia Mining Corporation Ltd; Collar co-ordinates for northings, eastings and elevation were recorded by Fugro Spatial Solutions Pty Ltd. The grid system used is AGD 1984 AMG Zone 51. Diamond holes were down hole surveyed by gyro. RC holes generally not downhole surveyed. If surveyed, then done by Digital electronic multishot (DEMS) • EGL and Swan; Collar locations were surveyed by DGPS and downhole surveys were collected using electronic multishot by the drillers. Subsequent to drilling holes were open hole gyro surveyed by ABIMS where possible. The gird system used is GDA1994 MGA Zone 51. • Ora Banda Mining Limited (RC, DD) MGA94, zone 51. Holes are picked up using RTK GPS the mine surveyors. Drill-hole downhole surveys are recorded using an Axis digital tool. Surface grade control holes are all surveyed by the mine surveyors by RTKGPS. Grade control holes are all downhole surveyed with north seeking gyro. Underground diamond drilling – diamond drilling collar locations picked up by mine surveyors via theodolite and known survey control points. UG diamond drill rig alignment via surveyed collar locations and DeviAligner tool, downhole surveys via DeviGyro-Ox tool. Underground face sample locations measured via laser distometer to known surveyed control points and development surveys via theodolite. • At close of mining in January 2024, OBM mine surveyors surveyed the Sand King pit area. Topographical control is considered adequate for resource modelling
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and*	• Drilling is predominantly on a 20mN X 20mRL grid, increasing to 40mN X 40mRL at depth. Surface grade control drilling was carried out on a nominal 5m X 5m grid. Underground grade control drilling is at a nominal 15m X 15m spacing when targeting the major lodes. • At Sand King the data spacing and distribution is sufficient to establish geological and grade continuity to support the definition of Mineral Resource and classifications as defined under the JORC 2012 code.

Criteria	JORC Code explanation	Commentary
	classifications applied. • *Whether sample compositing has been applied.*	• Composites of drill intercepts are length weighted, 1g/t lower cut-off, not top-cut, maximum 2m internal dilution. • Samples are composited for resource calculations.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• At Sand King resource drilling is predominantly inclined to the south, optimal for the predominantly ENE (060°) striking, north dipping mineralisation. UG diamond drilling is from cuddy's in fan patterns which does lead to less than optimal intersection angles of the outermost holes. • It is not known whether there is any introduced sample bias due to drill orientation.
Sample security	• *The measures taken to ensure sample security.*	• Unknown for earlier operators. • EGL – Samples are bagged, tied and in a secure yard on site. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS. • Monarch - Pre-numbered sample bags were put into numbered plastic bags. These numbers were written on the submission forms which were checked by the geologist. Plastic bags were then securely cable tied and placed in a secure location. Samples were then picked up by the Lab in Kalgoorlie or deliver to Perth via courier. A work order conformation was emailed to Monarch personnel for each sample submission once samples were received by the Laboratory. • Ora Banda Mining Limited - Samples were collected on the day of drilling and bagged into cable tied polyweave bags. Polyweave bags are stored into bulka bags on pallets in a secure yard on-site. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• Digital data from the SQL database has been reviewed by OBM and is consistent with hard copy and digital WAMEX data. • Siberia Mining Corporation conducted a due diligence on the data and core in 2005 and were "comfortable with the quality and integrity of the data". Digital data has been reviewed and is consistent with hard copy data. • Monarch Gold Mining Company Ltd; Monthly QAQC reports were produced to monitor accuracy and precision.

Section 1 Sampling Techniques and Data – Waihi

Information for historical (Pre Ora Banda Mining Limited from 1980's to 2010) drilling and sampling has been extensively viewed and validated where possible. Information pertaining to historical QAQC procedures and data is incomplete but of a sufficient quality and detail to allow drilling and assay data to be used for resource estimations. Further Ora Banda Mining Limited has undertaken extensive infill and confirmation drilling which confirm historical drill results. Sections 1 and 2 describe the work undertaken by Ora Banda Mining Limited and only refer to historical information where appropriate and/or available.

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that*	• Billiton - RAB and RC 1m samples with RAB being composited to 2m. Diamond core of NQ size. Assay sample techniques undocumented • Consolidated Exploration (ConsEx) – RAB 1m samples usually dispatched as 3m composites but occasional 1m. RC a mix of 1m sampling or 2m composites. Lady Eileen programs RC drilling made use of roller, Blade or hammer with crossover sub all nominally 5.5 inch diameter to obtain 2-3kg sample. Composite 2m samples were hammer milled, mixed and split to 200g then pulverised. 1m samples single stage mix and ground. Sub –samples taken for aqua regia and fire assay. • Cons Gold (Consolidated Gold) – RC 1m samples where alteration is visible. Remainder of hole composited to 4m. 2 to 3 kg samples, including core, sent to laboratory for crushing, pulverising and 50g Fire Assay. • Croesus – RC 1m samples collected under cyclone. 5m comps assayed for gold by 50g Fire assay. NQ diamond except for geotechnical purposes (HQ triple). • DPPL (Davyhurst Project Pty Ltd)- 4.25 to 5.5 inch RC drilling with face hammer. Potential mineralisation sampled and assayed on a metre basis otherwise 4m composites. Samples jaw crushed and pulverised before taking a 50gm charge for fire assay.

Criteria	JORC Code explanation	Commentary
	are Material to the Public Report. • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	• Ora Banda Mining Limited (OBM) - RC samples collected from the levelled cone splitter directly off rig into calico bags. Splitter maintained on level site to ensure sample representivity. 1m samples are dried, crushed, pulverised and a 50g charge is analysed by Fire Assay. Half core samples, cut by saw. Core sample intervals selected by geologist and defined by geological and/or mineralisation boundaries, or sampled to 1m. Samples are crushed, pulverized and a 40g or 50g charge is analysed by Fire Assay. • WMC - RC Sampling on 1m basis, assayed by aqua regia method, unknown laboratory.
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Billiton RAB and RC (Conventional hammer) diameter undocumented with use of roller/blade and hammer. NQ Diamond core • ConsEx - RC drilling with roller, blade or hammer with crossover sub. • Cons Gold – NQ diamond and HQ (triple) for geotechnical holes. RAB and RC. 4.25 to 5.5 inch RC drilling with stabilisers and face sampling hammers. • Croesus – Diamond holes NQ2 diameter. RC and RAB details undocumented but assumed to be industry standard at the time being 5.5 inch face sampling hammers and 4 inch diameter respectively. • Delta – RAB - details undocumented • DPPL - NQ core and HQ for geotechnical holes. RC drilling with stabilisers and face sampling hammers. • OBM - HQ3 coring to approx. 40m, then NQ2 to BOH. All core oriented by reflex instrument. RC drilled with face sampling hammer, 5.5" – 5.625" diameter. RC pre-collars used for some DD holes • WMC – Conventional RC hammer, diameter unknown and RAB drilling details undocumented.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• RC drill recoveries were not recorded by Aberfoyle/Bardoc, Annaconda, Ashton, Consolidated Gold, Croesus, Delta, DPPL, Hill Minerals, Intrepid, Monarch, Mt Kersey, Normandy, Pancontinental, Texas Gulf, West coast holdings or WMC. • Billiton – Recoveries for some RC drilling programs were examined in 1986 but raw data not available. • ConsEx – 2 m plastic pipe inserted into cyclone vent. Cyclone washed at the end of each hole or if water injected. Sample weights measured for Homeward bound (no bias observed) and Lady Eileen prospects (generally no bias observed aside from two high grade samples perceived to be due to coarse grained gold) • OBM - Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks). RC sample recoveries are approximated based on the size of the bulk sample and recorded in drill log tables. • It is unknown whether a relationship exists between sample recovery and grade or whether sample bias may have occurred.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Billiton - Qualitative: lithology, alteration for Diamond and RAB. RC logging details unavailable • Consolidated Exploration- Qualitative: lithology, colour, alteration, grainsize (at times). Quantitative: Quartz mineralisation at times • Consolidated Gold/ DPPL - Qualitative: lithology , colour, oxidation, alteration, with grainsize, texture and structure often recorded in diamond drilling. Quantitative: Quartz veining. Core photographed. Logging entered directly into HPLX200 data loggers. • Croesus - Most holes photographed, geologically logged and geotechnical and magnetic susceptibility measurements were taken. Qualitative: Lithology, colour, grainsize, alteration, oxidation, texture, structures, regolith. Quantitative: Quartz veining • OBM - Qualitative: Lithology, colour, oxidation, grainsize, texture, structure, hardness, regolith. Quantitative: estimates are made of quartz veining, sulphide and alteration percentages. Core photographed wet and dry. Magnetic susceptibility recorded for core holes. Bulk density measurements taken at regular intervals for core holes (determined by Archimedes Principle). • WMC RC: Qualitative: Lithology, Colour, Grainsize, Alteration and oxidation. • Some logging detail was lost during translation from one logging system to another. This has been rectified by referring back to original logs. • Entire holes were logged by all operators
Sub-sampling techniques	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and*	• Billiton – Sub-sampling methods undocumented. 1m repeat fire assays of 2m RAB comps at Lady Eileen were done. • Duplicates for RAB and RC inserted however frequency unknown. • ConsEx – RC holes sampled on 1m basis and riffle split to 1-2kg samples for 3m composites or 2-3kg samples for 2m composites. Composite 2m samples were hammer milled, mixed and split to 200g then pulverised to 200#. 1m samples single stage mix and ground to 200#.

Criteria	JORC Code explanation	Commentary
and sample preparation	*appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Consgold - RC Samples collected via cyclone at 1m intervals and passed through 3 stage riffle splitter. A 2-3kg fraction was calico bagged for analysis, the residue collected in plastic bags and stored on site. Potentially mineralised zones were sampled at 1m intervals, the remainder composited to 4m by unknown method. Composite samples returning >0.19g/t were re submitted at 1m intervals. Samples underwent mixermill preparation (2-3kg) by Amdel Laboratories. RAB 4m composite samples using PVC spear. Samples returning >0.19g/t were re submitted at 1m intervals. Diamond drill samples were sawn into half core. One half was jaw crushed, then pulverised using a labtechnics mill. A quartz blank was pulverised between each sample to avoid contamination. Field duplicates from residues at 1 in 20 frequency were submitted. • Croesus RC/RAB - 1m samples collected under cyclone. 5m comps, spear sampled with 50mm PVC pipe. Wet RC drill samples were thoroughly mixed in the sample retention bag and scoop sampled to form a composite sample. 3-5kg five metre composite analytical samples, returning values greater than 0.1g/t gold, were riffle split at 1m intervals, were samples where dry, and grab sampled where wet. RAB 1m resampling method undocumented. • Samples were dried, crushed and split to obtain a sample less than 3.5kg, and then fine pulverised prior to a 50gm charge being collected and analysed. Every 20th sample was duplicated in the field and submitted for analysis. Diamond tails were cut to half core and sampled based on geological boundaries and identified prospective zones. Samples size varied from 0.2m to1m. Core samples were sent to Ultratrace Laboratories of Perth • DPPL – RC 3 stage riffle split then 4m compositing. RAB 4m composites sampled using PVC spear. Both RC and RAB composites returning >0.19ppm Au re-submitted as 1m samples. Field duplicates from residues at 1 in 20 frequency submitted. • OBM – RC samples split into 2 x calico bags each metre using a cone splitter. Wet or moist samples are noted during sampling. Core was cut with diamond saw and half core sampled. All mineralized zones are sampled, including portions of visibly un-mineralised hanging wall and footwall zones. Sample weights range from >1kg to 3.5kg. Samples weighed by laboratory, dried and split to <3kg if necessary and pulverized by LM-5 • WMC - RC Sampling on 1m basis, methods undocumented. Assay by aqua regia method, unknown laboratory.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	• Billiton - Laboratory and methods undocumented. Standards for RAB and RC inserted however frequency unknown. • ConsEx – Genalysis composite 2m samples were hammer milled, mixed and split to 200g then pulverised to 200#. 1m samples single stage mix and ground to 200#. Phase 1 standard wet chemical multi acid digestion and AAS. Second phase were also pre-roasted. Results of >1g/t re-assayed by fire assay. Check assays at umpire lab (Classic labs) for Lady Eileen drilling - significant differences in high grade samples, otherwise considered good. • Consolidated Gold/ DPPL – RC and RAB - Mixermill prep with fire assay 50g charge at AMDEL, Minilab or Analabs Laboratories in Kalgoorlie. Half core was diamond sawn, jaw crushed, milled using LABTECHNICS mill at AMDEL for 50g charge by fire assay. Gannet standards submitted to monitor lab accuracy for infill resource drilling. Pulp umpire analysis was done but frequency unknown (1995). Screen fire assays of selected high grade samples. Quartz blanks submitted between each diamond core sample. • Croesus samples analysed for Au by Fire Assay/ICPOES by Ultratrace in Perth. Gannet standards and blank samples made by Croesus were submitted with split sample submissions. QAQC analysis of repeats was analysed by Croesus Mining NL. for their drilling completed during 2000. • OBM - Samples sent to Nagrom in Perth (2019) and SGS in Kalgoorlie (after 2019). The Nagrom samples have been analysed by Firing a 50gm portion of the sample. Lower sample weights may be employed for samples with very high sulphide and metal contents. This is the classical fire assay process and will give total separation of gold. An ICPOES finish is used. Samples after 2019 and prior to March 2025 were pulverised in the accredited site based SGS lab and assayed by 50g Fire assay, MPAES finish at SGS Kalgoorlie. From March 2025 all drill samples were crushed at the site laboratory in dedicated Orbis crushers and sent to SGS Kalgoorlie for PhotonAssay analysis. Commercially prepared standard samples and blanks are inserted in the sample stream at a rate of 1:25 for standards and 1:25 for blanks. Sizing results (percentage of pulverised sample passing a 75µm mesh or percentage of crushed sample passing a 3.35mm sieve) are undertaken on approximately 1 in 40 samples. Duplicate samples are submitted for RC holes only at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are deemed acceptable. • WMC drill samples were assayed by aqua regia method, unknown laboratory. • Fire assay is considered a total technique and aqua regia is considered a partial technique. • Historic operators assayed by "AAS". This is assumed to be aqua regia.

Criteria	JORC Code explanation	Commentary
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• OBM geologists have viewed selected diamond holes from previous operators at Waihi and verified the location of mineralised intervals. • ConsGold – Each metre interval geologically logged directly into HPLX2000 with standardised logging codes. • Twinned holes were occasionally used by previous operators but this practice was not common. • OBM - Geological and sample data logged directly into field computer (Panasonic Toughbook CF-31) using Geobank Mobile. Data is exported onto company servers and imported into Geobank SQL database by the database administrator (DBA). Assay files are received in .csv format and loaded directly into the database by the DBA. Hardcopy and/or digital copies of data are kept for reference if necessary. • Data entry, verification and storage protocols for remaining operators is unknown. • No adjustments have been made to assay data
Location of data points	• *Accuracy and quality of surveys used to locate drillholes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• RAB and AC holes are/were not routinely collar surveyed or downhole surveyed due to their limited use in resource estimation. To this end, discussion of RAB and AC drilling is omitted from this section. RC/GC (grade control) and shallow RC holes are/were not routinely downhole surveyed due to their shallow nature reducing the chance of significant deviation. Barren exploration RC holes were not routinely downhole surveyed or collar surveyed. DD holes were routinely collar and downhole surveyed by most operators or have been re-surveyed by subsequent operators. • The influence of magnetic rocks on the azimuths of magnetic down hole surveys is minor. Early holes surveyed in AMG zone 51 and converted to MGA using Geobank and or Datashed data management software. • Billiton (RC, DD) Local Lights of Israel grid undergone 2 point transformation. Downhole surveys when performed were by undocumented method with a 25m interval average. • ConsEx (RC). Drilled on local grids (possibly truncated AMG84, zone 51). Holes appear to have been surveyed using AMG, zone 51 grid at a later stage. Numerous vertical holes not down-hole surveyed. Downhole surveys when performed were by undocumented method with a 9m interval average. • Cons Gold/DPPL (RC, DD) Local grids and AMG84 zone 51 used. RC and DD Collars surveyed by licensed surveyors to respective grids. Holes of all types routinely collar surveyed whist RC resource holes routinely downhole surveyed by various methods including gyro and EMS with average intervals ranging between 10-25m. • Croesus (RC, DD) Various local grids and AMG zone 51. RC, DD holes routinely collar surveyed and downhole surveyed using Electronic Multishot (EMS), GRYO, Eastman single shot or combination thereof at 10-15m average interval. • Hills (RC) Local grid used. • OBM (RC, DD) MGA94 Zone 51. Drillhole collars are marked out and collar positions (post-drilling) picked up by a registered contract or mine surveyor using RTK-GPS. Drill-hole downhole surveys are recorded every 18-30m using a reflex digital downhole camera (2019 RC) or Gyro tool (subsequent RC and DD). At completion of drilling in-run or out-run surveys are collected every 10m. • WMC (RC, DD) - Digital data provided by ConsGold. (Wamex report a50226). Downhole surveys when performed were by undocumented method with a 16m interval average
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Data spacing nominally 20m x 20m but down to circa 10m x 10m and grade control drilling at circa 5m x 5m. • Drillhole spacing is adequate to establish geological and grade continuity for the Waihi deposit for the purpose of Mineral Resource and Ore Reserve estimation. • Composites of drill intercepts are length weighted, 1g/t lower cut-off, not top-cut, maximum 2m internal dilution
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Mineralised structures at Waihi are steep dipping and strike circa 320o to 345o Drilling is dominantly oriented to the east on a Waihi local grid which is rotated -14 degrees from the MGA north. Drilling is therefore oriented towards 76o on the MGA grid and to a lesser extent 256o, orthogonal to the mineralisation strike. Drillhole inclinations range from -50 to -90o. At Homeward bound some drillholes were drilled down the structure in an attempt to better define the folding present. • It is unknown whether the orientation of sampling achieves unbiased sampling, though it is considered unlikely as the majority of holes have optimally intersected the mineralised lodes.

Criteria	JORC Code explanation	Commentary
Sample security	• *The measures taken to ensure sample security.*	• Undocumented for most early operators. • ConsGold – RC residues stored onsite. • OBM – Samples are bagged into cable-tied polyweave bags and stored in bulka bags in a secure yard. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• OBM has reviewed historic digital data and compared it to hardcopy and digital (Wamex) records. Changes were made to the SQL database where necessary. • No audits of sampling techniques have been done.

Section 2 Reporting of Exploration Results – Riverina

(Criteria listed in the preceding Missouri & Sand King section also apply to this section.)

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td>Mineral tenement and land tenure status</td><td>• Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.
• The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</td><td>• All tenure pertaining to this report is listed below.
<table>
<tr><th>TENEMENT</th><th>HOLDER</th><th>AGREEMENTS</th></tr>
<tr><td>M30/256</td><td>CARNEGIE GOLD PTY LTD.</td><td>JV BETWEEN DAVYSTON EXPLORATION PTY LTD (68%) AND CARNEGIE GOLD PTY LTD (32%) FOR ALL MINERALS OTHER THAN GOLD AND SILVER

DAVYSTON EXPLORATION PTY LTD HOLDS A CONSENT CAVEAT & A REGISTERED MORTAGE AGANST THE TENEMENT

SOUTH32 LTD HOLDS ROYALTY RIGHTS (PORTION OF TENEMENT ONLY)

HAWKES POINT HOLDINGS L.P HAS A REGISTERED MORTGAGE AGAINST THE TENEMENT</td></tr>
</table>
• Carnegie Gold PTY LTD is a wholly owned subsidiary of OBM.
• There are no known heritage or native title issues.
• There are no known impediments to obtaining a licence to operate on this tenement area.</td></tr>
<tr><td>Exploration done by other parties</td><td>• Acknowledgment and appraisal of exploration by other parties.</td><td>• Drilling, sampling and assay procedures and methods as stated in the database and confirmed from Wamex reports and hard copy records are considered acceptable and to industry standards of the time.</td></tr>
<tr><td>Geology</td><td>• Deposit type, geological setting and style of mineralisation.</td><td>• The geology of the Riverina area consists of an interlayered sequence of meta-basalts, meta-sediments and ultramafics, rarely cross-cut by narrow pegmatite dykes. The local stratigraphy strikes roughly N-S with primarily steep east to sub-vertical dips. The area has been affected by upper greenschist to lower amphibolite grade metamorphism with many minerals exhibiting strong preferred orientations. All rock units exhibit strain via zones of foliation, with strongly sheared zones more common in ultramafic</td></tr>
</table>

		lithologies. Contemporaneous strike faults and late stage thrust and wrench faults have dislocated the stratigraphy and hence, mineralisation. • Gold mineralisation is hosted by quartz-sulphide and quartz-Fe oxide veining primarily in the metabasalts. Metasediments and ultramafics may also contain gold mineralised quartz veining, although much less abundant. Gold mineralisation is also seen in silica-biotite-sulphide and silica-sericite-sulphide alteration zones in the metabasalts.

Drillhole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drillholes:*
	  ○ *easting and northing of the drillhole collar*
	  ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drillhole collar*
	  ○ *dip and azimuth of the hole*
	  ○ *down hole length and interception depth*
	  ○ *hole length.*
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*
		• See list of drill intercepts.

Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Original assays are length weighted. Grades are not top cut. Lower cut off is nominally 1.0g/t. Due to the narrow nature of mineralisation a minimum sample length of 0.2m was accepted when calculating intercepts. Maximum 2m internal dilution. • Metal equivalents not reported.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drillhole angle is known, its nature should be reported.*	• Intercept widths are down hole lengths. True widths are not reported given the varying orientation of drilling and mineralisation at each deposit/prospect mentioned in the report. • The geometry of the mineralisation at Riverina South is approx. N-S and sub vertical. Surface drilling is oriented perpendicular the strike of the mineralisation. UG drilling from drill cuddy with hole radiating in fans. Holes testing strike extremities are at lower angles to the ore lode and therefore not true widths, while those perpendicular to the lode can approximate true widths.

	• *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drillhole collar locations and appropriate sectional views.*	• See plans, cross-sections and long sections.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• The location of drillhole intersections is shown on the plans and 2D/3D diagrams and are coloured according to grade to provide context for the highlighted intercepts

Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Riverina has no known reported metallurgical issues and is currently being successfully mined.
		• Results from previous processing have demonstrated that good gold recovery can be expected from conventional CIL processing methods.
		• Recent baseline metallurgical test work demonstrated the following gold recoveries:
		  ○ Oxide – 90%
		  ○ Transitional – 97%
		  ○ Fresh – 94.3%
		• Additional variation test-work remains ongoing.

Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Further GC drilling at Riverina underground will continue as the access into the mine is deepened. • Further resource definition drilling will be conducted from the surface, when beyond the reach of the underground drills, aimed and continued mineral resource growth and resource conversion.

Section 2 Reporting of Exploration Results – Sand King

(Criteria listed in the preceding Missouri & Sand King section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures,*	• Sand King deposit is on Tenement M24/960 held by Siberia Mining Corporation Pty Ltd, a wholly owned subsidiary of Ora Banda Mining. The tenement is in good standing. • .

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td>land tenure status</td><td>partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.
The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</td><td>
<table>
<tr><th>TENEMENT</th><th>HOLDER</th><th>AGREEMENTS</th></tr>
<tr><td>M24/0960</td><td>SIBERIA MINING CORPORATION PTY LTD</td><td>SIBERIA GRANTED GARDNER THE RIGHT TO EXPLORE FOR NICKEL MINERALS (portion of the tenement only)

ROB MITCHELL AND HANK SHRERS (SURFACE ALLUVIAL RIGHTS TO 2M DEPTH) (portion of the tenement only)

STONEHORSE ENERGY LIMITED HAVE RIGHTS TO EXPLORE FOR NICKEL MINERALS (portion of the tenement only)

JV BETWEEN DAVYSTON EXPLORATION PTY LTD (68%) AND SIBERIA MINING CORPORATION PTY LTD (32%) FOR ALL MINERALS OTHER THAN GOLD AND SILVER

DAVYSTON EXPLORATION PTY LTD HOLDS A CONSENT CAVEAT & A REGISTERED MORTAGE AGAINST THE TENEMENT</td></tr>
<tr><td>M24/39</td><td>CHARLES ROBERT GARDNER</td><td>GARDNER GRANTED SIBERIA THE RIGHT TO EXPLORE FOR GOLD MINERALS (GOLD AND SILVER MINERALISATION IN ANY FORM)(ENTIRE TENEMENT). IN RELATION TO THE “REDUCED AREA”, SIBERIA HAS CONTINUED EXCLUSIVE AND OVERRIDING RIGHTS TO CARRY OUT EXPLORATION AND MINING OPERATIONS. ROBERT GARDNER HAS PRIORITY OF RIGHTS OVER THE “REMAINING AREA” OF M24/39

WMC RESOURCES LTD HOLDS A CAVEAT AGAINST THE TENEMENT

CITY OF KALGOORLIE-BOULDER HOLDS AN ABSOLUTE CAVEAT AGAINST THE TENEMENT

SIBERIA HOLDS A CONSENT CAVEAT AGAINST THE TENEMENT</td></tr>
</table>
There are no known heritage issues
There are no known impediments to operating in the area.
</td></tr>
<tr><td>Exploration done by other parties</td><td>Acknowledgment and appraisal of exploration by other parties.</td><td>Drilling on the tenements was completed by numerous operators, but the majority of work was completed by WMC, Gilt Edged Mining, Siberia Mining Corporation, Monarch Gold and EGS. All work by these companies was to industry standards of the time.</td></tr>
<tr><td>Geology</td><td>Deposit type, geological setting and style of mineralisation.</td><td>Sand King is an orogenic lode style deposit hosted by mafic rocks, predominantly basalt.
Gold mineralisation at Sand King takes the form of stacked quartz-biotite-feldspar-sulphide shear lodes within the basalt. Widths vary from sub 1m to ~ 6m true width. Occasionally blow outs occur with >6m true width. Mineralised structures are NE-SW striking in the south and normally steeply dipping (~80 degrees) to the north-west while in the north-eastern end of the deposit most mineralisation is interpreted to strike E-W and dip steeply to the north (~80 degrees)</td></tr>
<tr><td>Drillhole Information</td><td>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drillholes:
easting and northing of the drillhole collar
elevation or RL (Reduced Level – elevation above sea level in metres) of the drillhole collar
dip and azimuth of the hole
down hole length and interception depth</td><td>See Significant Intercepts in document
The significant intercept table provides details of drillholes with intercepts of >= 1 gram metres. In cases where drilling has intercepted a lode position with grades below this value, NSI (no significant intercept) is listed. This provides context to the number of holes in the project area with significant gold intercepts versus the number of holes with lesser or no significant intercepts.
Widths reported in the Significant Intercepts table are all down hole lengths.</td></tr>
</table>

Criteria	JORC Code explanation	Commentary
	○ *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Original assays are length weighted. Grades are not top cut. Lower cut off grade is nominally 1.0g/t. Maximum 2m internal dilution and minimum width of 0.2m. • No metal equivalents reported.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drillhole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	• Drilling is predominantly angled at -60° to the south, optimally intersecting the steep north dipping mineralisation. This drill orientation does not intersect all lodes at optimal angles and as such some drill intercepts are longer than true widths. • All intercept widths reported are down hole lengths. The geometry of mineralisation is known for the Sand King deposit. However, no attempt has been made to report true widths. • Some drill programs required shallow angle (~30°) diamond drilling to hit specific targets within the constraints of existing mining infrastructure (existing pit and dumps). • UG drilling from drill cuddys with hole radiating in fans. Holes testing strike extremities are at lower angles to the ore lode and therefore not true widths, while those perpendicular to the lode can approximate true widths.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drillhole collar locations and appropriate sectional views.*	• See plans and sections.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• All drill intercepts from recent drilling are reported. • Results reported include both low and high gram metre (g/t x down hole length) values.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Metallurgical and geotechnical work has been completed for Sand King deposit in the past.
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).*	• Additional deep and lateral drilling to grow the UG resource.

Criteria	JORC Code explanation	Commentary
	• *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	

Section 2 Reporting of Exploration Results – Waihi

(Criteria listed in the preceding Golden Eagle section also apply to this section.)

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td>Mineral tenement and land tenure status</td><td>• Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.
• The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</td><td>• All tenure pertaining to this report is listed below
<table>
<tr><th>TENEMENT</th><th>HOLDER</th><th>Expiry Date</th><th>AGREEMENTS</th></tr>
<tr><td>M30/255</td><td>CARNEGIE GOLD PTY LTD.</td><td>10/01/2038</td><td>DAVYSTON EXPLORATION PTY LTD HOLDS A CONSENT CAVEAT & A REGISTERED MORTAGE AGANST THE TENEMENT

HAWKES POINT HOLDINGS L.P HAS A REGISTERED MORTGAGE AGAINST THE TENEMENT</td></tr>
</table>
• Carnegie Gold PTY LTD is a wholly owned subsidiary of OBM.
• There are no known heritage or native title issues.
• There are no known impediments to obtaining a licence to operate in the area.</td></tr>
<tr><td>Exploration done by other parties</td><td>• Acknowledgment and appraisal of exploration by other parties.</td><td>• Modern exploration commenced at the Davyhurst sites in the 1980s. Three companies, Jones Mining, Western Mining Corporation (WMC) and Hill Minerals pegged claims surrounding the historic Davyhurst sites. In 1986, WMC established a 300,000 tonne per annum carbon-in-pulp (CIP) treatment plant at Davyhurst and commenced open pit mining at Golden Eagle and Waihi. In 1988 WMC's and Jones Mining's assets were acquired by Consolidated Exploration Ltd. Consolidated Exploration then developed open cut mines at Great Ophir, Lady Eileen, Lady Eileen South and Homeward Bound. At about the same time Aberfoyle Resources / Hill Minerals commenced open-pit mining at the Lights of Israel Deposit and trucked the ore 80 km to the Bardoc processing plant. During 1995/96 Consolidated Exploration Ltd restructured as Consolidated Gold NL (CGNL) and commenced tenement acquisition and exploration activities in the area. This resulted in the consolidation of holdings in the district. In December 1996 CGNL acquired the assets of Aberfoyle Resources in the area, including the Bardoc Processing plant, in an equity transaction. The Bardoc plant was relocated to the Davyhurst site and upgraded to 1.2 Mt/y. In October 1998 Davyhurst Project Pty Ltd (DPPL), a subsidiary of NM Rothschild and Sons (Australia), acquired the project. In 2000, Croesus Mining NL ("Croesus") acquired the Davyhurst Project and continued operations until 2005. In January 2006, Monarch Gold Mining Company Limited (Monarch) acquired Davyhurst and operated the project until 2008.
• Drilling, sampling and assay procedures and methods as stated in the database and confirmed from Wamex reports and hard copy records are considered acceptable and to industry standards of the time. There is sufficient understanding of drilling, sampling and assay methodologies for the majority of drilling in the Waihi area. The company is confident that previous operators completed work to standards considered acceptable for the time. As part of each resource upgrade, OBM is committed to additional drilling to confirm the style, widths and tenor of mineralisation at each deposit.</td></tr>
<tr><td>Geology</td><td>• Deposit type, geological setting and style of mineralisation.</td><td>• Regional Geology - Rocks of the Coolgardie domain (Kalgoorlie Terrane) are prevalent in the Davyhurst area. Rocks of the Coolgardie Domain are not well exposed at Davyhurst and the distribution of rock types suggests that it is mainly represented by the upper part of the stratigraphic sequence, namely basalts, felsic volcanics and sedimentary rocks. The abundant ultramafic-mafic sills of the Ora Banda Domain do not occur in the Coolgardie Domain. Granitoids in the Davyhurst Project area can be classified by magnetic signature into</td></tr>
</table>

Criteria	JORC Code explanation	Commentary
		three types: low, medium and high magnetic response. Binns et al. (1976) distinguished 'static style' and 'dynamic style' regional metamorphism. Static style areas generally occupy the central, low-strain part of the greenstone regions away from the granitoids and typically have lower metamorphic grades (prehnite–pumpellyite to upper greenschist facies). Strain is concentrated in narrow zones so that textures are well preserved in more massive and competent rocks. Dynamic-style areas of greenstone have higher metamorphic grades (upper greenschist to upper amphibolite facies) and are characterized by more pervasive foliation, particularly along the contacts with large granitoid terrains. There appears to be two major controls on mineralisation in the Davyhurst area. Both mineralisation styles rely on mineralisation taking place during reactivation of earlier ductile shear zones. In the case of the Lights of Israel group of deposits, the early shears are moderately to gently west dipping, whereas in the Federal Flag – Lady Eileen group of deposits, the early shear is steeply west dipping. In the northern portion of the Davyhurst tenements most gold mineralisation is aligned in planar corridors that have N- to NW-trends. The overall dip of the mineralised corridors is mostly steep (>75º) E- or W-dipping with moderate to steep (~60º) and shallow-dipping (~15º) ore zones at the Federal Flag and Lady Gladys deposits, respectively. Within these planar corridors of mineralisation linear trends to gold distribution are mostly shallowly plunging. Internal variations within the corridors at individual deposits are common and discussed later. Mineralisation at the Lights of Israel and Makai deposits differs from the other examined deposits in that mineralisation has a linear form that plunges moderately (~20º) to the NNW. • **Local Geology** - The two major rock types within the Waihi deposit are: ○ ***Tremolite/Actinolite/Chlorite Amphibolite***. Weakly to strongly foliated, fine to medium grained rocks composed of tremolite/actinolite within a fibrous Mg chlorite matrix. High Mg Basalt ○ ***Fine Grained Basalt***. Massive to weakly foliated, very fine grained rock composed of actinolite and plagioclase (albite) with trace magnetite. Tholeiitic basalt Late stage lepidolite bearing pegmatite dykes striking 060° and dipping steeply 75° north cut across the stratigraphy at several places. A quartz felspar porphyry sub parallel to regional foliation has been mapped in the old Homeward Bound pit. Detailed mapping by ConsGold of the Waihi and Homeward Bound pits shows the area is dominated by a strong penetrative foliation striking 347° and dipping 75° to 80° west. A second weaker foliation striking 040° and dipping 75° north was also recognised in both pits. Several post mineralisation faults striking approximately 070° and dipping north have been mapped or inferred from the drilling. The faults have only minor lateral displacement. Several of the faults are infilled by lepidolite pegmatite. • Gold mineralisation at Waihi occurs within both the tholeiitic and high Mg basalts. Mineralisation is characterised by multiple loads and broad alteration haloes. Mineralisation also appears to have a moderate northerly plunge of approximately 40° towards 340°. Folding is common at Waihi and numerous folds and re-folded folds are noted in pit and in in drill core. Fold hinges have a consistent ~40° plunge to the north. Within the deposit there is a pervasive biotite alteration halo. Associated with gold mineralisation, biotite plus silica and quartz veining occur. Higher grade gold mineralisation is generally associated with extreme silica flooding and quartz veining which has destroyed the majority of the rock fabric. Diopside as an alteration mineral also occurs throughout the resource. Quartz veining sub parallel to, or cross cutting the regional fabric also occurs within the deposit. These veins are discontinuous and can form boudins with the ore zone. Grade distribution within these blobs is erratic (Lennartz, 1988). Controls on ore shoots within the resource are not well understood at this stage. From the data available there appears to be a major zone of mineralisation plunging north from the south end of the Waihi pit. From the old stope plans of the Waihi Shaft, it would appear that the higher grade mineralisation has a steeply dipping lensoidal shape, with occasional glory holes, which WMC inferred were fold hinges. Around the Homeward Bound and east lode areas the higher grade mineralisation appears to have a 40° plunge to the north. Pyrrhotite, pyrite and arsenopyrite are the dominant sulphides within the resource. Trace to accessory concentrations of chalcopyrite, pentlandite, gesdorfite, and bismuth have been recognised
Drillhole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drillholes:* ○ *easting and northing of the drillhole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in*	• Individual drill intercepts are previously reported. *For previous announcements relating to Waihi please refer to ASX announcement dated 22 February 2017, 29 July 2019, 14 October 2019, 6 November 2019, 22 November 2019, 24 December 2019, 21 January 2020* • Any widths reported in a Significant Intercepts table are all down hole lengths.

Criteria	JORC Code explanation	Commentary
	metres) of the drillhole collar ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Original assays are length weighted. For reporting exploration results grades are not top cut. Lower cut off grade is nominally 1.0g/t. Maximum 2m internal dilution. • No metal equivalents reported.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drillhole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	• Intercept widths are down hole lengths. True widths are not reported. • Surface drilling is dominantly towards 080° which is approx. perpendicular to the strike of the mineralisation.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drillhole collar locations and appropriate sectional views.*	• See plans and sections provided within this announcement.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• Results reported include both low and high gram metre (g/t x down hole length) values. • The significant intercept table (previously reported – see references in Section on Drillhole Information) provides details of drillhole intercepts shown on diagrams. There is no lower cut-off grade, the holes listed include those with NSI (no significant intercept). Holes in the significant intercept table are shown on diagrams coloured according to gram metre grade bins. This provides spatial context to the number of holes in the project area with significant gold intercepts versus the number of holes with lesser or no significant intercepts
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment;*	• Metallurgical and geotechnical work has been completed for numerous previously mined deposits, including Waihi. • Waihi deposit was previously mined and processed at Davyhurst plant with no known metallurgical issues. • Ongoing geological/ structural evaluation to determine the controls on mineralisation. • New metallurgical holes from Waihi have been drilled and are being tested. Results are pending. • Geotechnical holes have been drilled in 2020 and 2023

Criteria	JORC Code explanation	Commentary
	metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Data evaluation and geological assessment of all deposits, including Waihi, will be followed by additional resource drilling and updated JORC 2012 compliant Mineral Resources. • Exploration targeting extensions to the current resource are ongoing.

Section 3 Estimation and Reporting of Mineral Resources – Riverina

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	• Data from EGL and early OBM drilling captured into Field Marshall logging software. More recent drilling capture in Geobank Mobile. Data sent from site and imported into SQL database via DBMS. Validation checks in SQL database ensure data integrity is not compromised. • The data is verified by company geologists before being sent to the DBA for validation or passing Geobank Software validation protocols. • Historic data has been verified by checking historical reports on the project. • The Competent Person has undertaken a number of validation checks on the database, using Micromine software which include, but are not limited to, checks for overlapping intervals, checks for missing data/records, visual checks on drillhole locations and traces to identify any possible survey issues. No major issues were detected.

Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*
	• *If no site visits have been undertaken indicate why this is the case.*
		• Numerous site visits completed to:
		  ○ View and map geology in existing open pit
		  ○ View and manage drilling operations
		  ○ View and log drill core
		  ○ View Underground exposure

Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	• Mineralised structures are roughly N-S striking, sub-vertical to steeply east dipping. The main lodes have been previously mined and are sub-vertical. Late stage south dipping thrust structures are mapped in the pit and underground workings and would extend east towards the Murchison and Reggie lodes. Minor sinistral offsets of up to 5m are noted in underground workings and are observed as offsets of mineralised drill intercepts. Three late structures have been modelled with offsets, two south dipping pegmatite filled thrusts and a pegmatite filled back thrust known as "The Slide". An additional thrust mapped in the north pit, usually gouge filled, has been modelled without offsetting mineralisation, though in reality minor offsets will occur. An additional lower thrust has been modelled from drill core observations, again without offsetting mineralisation. An increase in drill density will enable potential offsets to be better defined. • Structural data from OBM drilling was used to guide the orientation of mineralised lodes where possible. • Inspection of core and ore shows the mineralisation to be associated with silica sericite alteration and quartz-carbonate veining. Resource interpretations are guided by presence and intensity of veining and/or alteration noted in logging. • Geological continuity of N-S mineralised structures are well defined, although sometimes terminate abruptly, possibly due to the minor offsets caused by the E-W structures and/or structures entering pods of sediment/ultramafic which are poor hosts for gold mineralisation. The main lodes at Riverina are geologically continuous over 1km and limited only by drilling depth.

Criteria	JORC Code explanation	Commentary
		• Mineralisation is also locally stoped by intruding pegmatite dykes along late structured, the location of which are well understood.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The main lodes at Riverina are geologically continuous over 1km in a N-S direction and defined to a depth of 320m below surface. A single deep diamond hole has confirmed main lode mineralisation at a depth of 470m below surface. • The central Murchison and East (Reggie) lodes extend for a similar strike length but are not as depth extensive. The deposit extends for 320m in an E-W direction

Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*
	• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*
	• *The assumptions made regarding recovery of by-products.*
	• *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).*
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*
	• *Any assumptions behind modelling of selective mining units.*
	• *Any assumptions about correlation between variables.*
	• *Description of how the geological interpretation was used to control the resource estimates.*
	• *Discussion of basis for using or not using grade cutting or capping.*
	• *The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.*
		• A 2-dimensional estimation technique was adopted where the lodes are projected on to a nominal 2D northing-elevation plane for estimation. Accumulation and Horizontal Width variables are estimated into a 2-Dimensional block Model and the Au grade is back calculated (Au grade = Accumulation / True Width).
		• Full width composite samples were digitised on-screen using LeapfrogTM software. Composites have different lengths and are therefore at different supports and said to be non-additive and unsuited for ordinary kriging. When grades are weighted by the sample widths they become additive, hence requirement to estimate Accumulation (Grade*Width) and the Width. Lode intervals based on representative geology seen in core/face photos and logging. Internal dilution included if bounded by samples with significant gold grade. True Width of each full width composite is calculated in Leapfrog TM software using its distance function between the composite mid-point and the footwall and hanging-wall wireframes.
		• Ordinary Kriging (OK) using MicromineTM was used to estimate Accumulation and Horizontal Widths into a 2D block model (single block in the E-W direction). Locations of all composite data were transformed on to a single arbitrary Easting (Local Grid coordinate 10000mE) to define the 2D north-Elevation plane. Variography was completed in the 2D plane. Semi variogram parameters defined from the Accumulation variable were also applied to the Width as the two variables are related and correlated. Mineralisation boundaries were treated as hard boundaries.
		• High grade cuts up to 85 gram metres were applied to the Accumulation variable data based on analysis of individual domains. Top-cuts applied on a domain basis. Horizontal Width variable did not require top cutting.
		• The parent block dimensions used were 20m NS by 20m RL. There is only one block in the X (across strike) direction. Drillhole spacing is approximately 20m between section and 20m along section in well drilled areas. A parent block size of 1m x 20m x 20m was selected to account for areas of lower drill density and taking consideration of realistic underground mining selectivity.
		• An orientated ellipsoid search was used to select data and was based on parameters derived from variography defined using SupervisorTM software.
		• Estimation completed in 3 runs each with less restrictive search, and minimum sample parameters. The initial interpolation pass was used with a maximum range equal to the range of the principal direction of the modelled variograms. Maximum number of samples was 12, minimum was 2 (run 3). Search range increased progressively for each subsequent run. Estimates were transformed back to real space from the 2D plane.
		• No estimation of deleterious elements was carried out. Only Au was interpolated into the block model.
		• Previous resource estimates have been completed in 2020, 2021 and 2023
		• No assumptions have been made regarding recovery of by-products.
		• Selective mining units were not modelled in the Mineral Resource.
		• No assumptions have been made regarding correlation between variables
		• The validation was carried out by three methods:
		  ○ Visual comparison of long section block grades with nearby drill assay results.
		  ○ Statistical comparison of estimated grades and composite grades on a domain by domain basis.
		  ○ Trend analysis of estimated block model grades versus composite grades on 10m northing and 5m vertical intervals.

Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages and grades were estimated on a dry in situ basis. No moisture values were reviewed.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The Mineral Resources have been reported at a diluted cut-off of 1.3g/t Au inside simulated Mineable Stope Optimiser (MSO) shapes of 10m x 10m with a minimum width of 1.6m.

Criteria	JORC Code explanation	Commentary
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• Reasonable prospects for eventual economic extraction for the Riverina underground Resource was confirmed by applying a Mine Stope Optimiser (MSO) with dimensions of 10mN x 10mRL, a minimum width of 1.6m and a cut-off grade of 1.3g/t. Individual MSO blocks were assessed and removed if above the top of fresh DTM surface and if above the A$2400 optimised pit shell from within which the Riverina open pit resources are reported.

Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	• Riverina has no known reported metallurgical issues.
		• Results from previous processing have demonstrated that good gold recovery can be expected from conventional CIL processing methods.
		• Recent baseline metallurgical test work demonstrated the following gold recoveries:
		  ○ Oxide – 90%
		  ○ Transitional – 97%
		  ○ Fresh – 94.3%
		• Additional variation test-work remains ongoing.

Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• Riverina Underground is currently being mined and all approvals are currently in place. • All environmental impacts are accounted for in the current approvals
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.*	• Bulk density determinations were derived from 3459 measurements (immersion method) made on core samples drilled by OBM/EGS. • Historic bulk densities for fresh basalt collected from underground in 1988 were analysed. The mean fresh rock density from recent drilling compared closely with the mean density of underground samples. • Bulk density values used in the underground resource were 2.82t/m3 (Main Lodes), 2.89t/m3 (Main Lode bounding shear) and 2.85t/m^3 (Murchison and Reggie Lodes). • It is assumed there are minimal void spaces in the rocks within the Riverina deposit. Values applied in the Riverina block model are similar to other known bulk densities from similar geological terrains.

Criteria	JORC Code explanation	Commentary
	• *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	Mineral Resources were classified in accordance with the Australasian Code for the Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC, 2012). The classification takes account of confidence in the geological interpretation, sample density and assay QAQC. Underground - Wireframe solids were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, measured, indicated or inferred: • Measured – Near surface areas defined by close spaced RC grade control drilling • Indicated – Areas with: o drill spacing in long section of approximately 40mN x 40mRL where there is reasonable confidence in the geological interpretation and grade continuity. o reasonable estimation quality as defined by the conditional bias slope > 0.5 • Inferred – Areas with: o drill spacing in long section in excess of 30mN x 30mRL and where grade continuity is poorer as defined by a lower sample density, even though geological continuity may be apparent. o poorer estimation quality as defined by the conditional bias slope > 0.2 and < 0.5 • The input data is comprehensive and of sufficient quality for use in the MRE's. Significant recent drilling, covering the entire deposit, has confirmed the location and tenor of many historic drill-holes. Assay QAQC is of sufficient quality for the assays to be used in the MRE. There is sufficient understanding of the geology to support the current interpretation in terms of continuity. • The Mineral Resource estimates appropriately reflects the view of the Competent Person.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• The Underground MRE has been internally peer reviewed
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and*	• The Riverina Mineral Resource estimate is reported with a reasonable degree of confidence. The data quality is good and the drillholes from recent drilling have detailed logs produced by qualified geologists. Historic logging has been reviewed. • The Mineral Resource statements relate to global estimates of tonnes and grade. Confidence in the estimate allows reasonable quantification of global metal content. The interpretation is considered globally robust but at a local scale, variations to ore geometry and grade could be expected. • All Measured and Indicated resources are relevant to economic evaluation. • The deposit is currently being mined – Underground. • Production data from current mining is used to calibrate MRE's

Criteria	JORC Code explanation	Commentary
	confidence of the estimate should be compared with production data, where available.	

Section 3 Estimation and Reporting of Mineral Resources – Sand King

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary

Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*
	• *Data validation procedures used.*
		• Data from EGS/OBM drilling captured into Field Marshall or Geobank Mobile logging software. Data sent to Perth for import into SQL database via DBMS. Validation checks in SQL database ensure data integrity is not compromised.
		• Data for use in resource estimation derived directly from SQL via queries (views) and a data warehouse database
		• Data validation included:
		  ○ review of historic digital data versus original hardcopy records
		  ○ Inspection of mineralised intervals in historic core

Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*
	• *If no site visits have been undertaken indicate why this is the case.*
		• Numerous site visits completed to:
		  ○ View and log historic core
		  ○ Map the Sand King pit
		  ○ Log recent drill core
		  ○ View underground exposures

Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	• Sand King pit mapped by structural geological consultants (Model Earth Pty. LTD) Additional mapping completed by OBM geology team. Current pit mapping identifies early 010 and 330 ductile shears and 060 and 090 (semi) steep north dipping brittle extension veins. Extension veins form the bulk of the mineralisation. This structural architecture has been verified during underground mining. • An extensive relog program of historic diamond core was completed to provide consistency with 2016 (EGS) and 2020 (OBM) geological logging. • Inspection of core and pit ore shows the mineralisation to be associated with quartz-carbonate veining and biotite-sulphide alteration either side of the veining. Resource interpretations guided by presence and intensity of veining and/or biotite noted in logging. • Geological continuity of extension structures is well defined, although not strike extensive and can terminate abruptly. Quartz tension veins oriented 090°-100° form stacked lodes and the intersection of these with the shear-lodes and 060° lodes is the most likely control for high grade shoots and plunge steeply towards the N-NNE. Mineralising structures post date locally intruding aplite dykes and these can be (weakly) mineralised.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The Sand King deposit extends for over 800m in NE-SW direction and approximately 300m in a SE-NW direction. The Resource extends for ~400m below the surface RL of 420m AHD. • A mine grid is employed at Sand King. This has a 60° rotation so that 060° (MGA) is 000° (Mine Grid). 4000m is added to the MGA RL.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* • *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes*	• Interpolation was done using Ordinary Kriging (OK) estimation method. • 1m composite samples coded to the mineralised domains were used as inputs to estimation. Only RC (including RC grade control) and diamond drilling samples were used for estimation. • OK was used to estimate gold grades into a 3-dimensional block model. Estimation parameters were derived from modelled semi-variograms. Micromine™ software was used for the OK estimation. • Grade capping was applied on a domain by domain basis due to the usually positively skewed grade populations. High grade cuts up to 60g/t were applied to 1m composite data based on analysis of individual domains. • The parent block dimensions (Mine Grid) for OK estimates were 4m EW by 10m NS by 10m vertical. Sub-cells of 0.5m by 1m by 1m were applied to the OK model. Drillhole spacing in better drilled areas is approximately 20m between section and 20m along section. The parent block size is approx. 50% of data spacing. • An orientated ellipsoid search was used to select data and was based on parameters derived from the variography defined using

Criteria	JORC Code explanation	Commentary

	appropriate account of such data.
	• *The assumptions made regarding recovery of by-products.*
	• *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).*
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*
	• *Any assumptions behind modelling of selective mining units.*
	• *Any assumptions about correlation between variables.*
	• *Description of how the geological interpretation was used to control the resource estimates.*
	• *Discussion of basis for using or not using grade cutting or capping.*
	• *The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.*
		Supervisor™ software.
		• Estimation completed in 3 runs each with less restrictive search, and minimum sample parameters. The initial interpolation pass was used with a maximum range equal to the range of the principal direction of the modelled semi variograms. Maximum number of samples was 20, minimum was 6. Range increased progressively and number of samples required was reduced for each subsequent run.
		• No estimation of deleterious elements was carried out. Only Au was interpolated into the block model.
		• Previous OK resource estimates have been completed in 2017, 2020 2021 and 2022 all tailored for Open Pit MRE's. The 2024 MRE was used to estimate UG reserves.
		• No assumptions have been made regarding recovery of by-products.
		• No assumptions have been made with respect to modelling of selective mining units.
		• Only Au was estimated so correlation analysis was not possible.
		• The deposit mineralisation was constrained by wireframes constructed using an approx. 1 g/t Au cut-off grade (based on inflection point in log probability plot of raw assays) in association with logged geology, particularly the presence of quartz veining and biotite-sulphide alteration. Ore lode continuity is preserved reasonably well at the relatively high interpretation cut-off grade. The wireframes were applied as hard boundaries in the estimate.
		• The validation was carried out by three methods:
		  ○ Visual comparison of block grades with nearby drill assay results on a section by section basis.
		  ○ Comparison of estimated grades and composite grades on a domain by domain basis.
		  ○ Trend analysis of estimated block model grades versus composite grades.

Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages and grades were estimated on a dry in situ basis. No moisture values were reviewed.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The Underground Mineral Resource has been reported at a diluted 0.9 g/t Au cut-off from within Mine Stope Optimiser shapes (MSO) with 10mN x 10mRL dimensions and minimum 1.6m width. All fresh material above cut-off grade within MSO shapes below 350RL are included in the report.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• Reasonable prospects for eventual economic extraction for the Sand King underground Resource was confirmed by applying a Mine Stope Optimiser (MSO) with dimensions of 10mN x 10mRL, a minimum width of 1.6m and a cut-off grade of 0.8 g/t. Costs applied to the MSO process approximate current OBM mining costs and a gold price of A$4000 was used.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical*	• Sand King deposit is currently being mined with underground methods. • Metallurgical test-work was undertaken in 2019/2020 and again in 2023/2024 as part of mining studies. • Gold recovery adopted for the underground mine is 87% (Fresh)

Criteria	JORC Code explanation	Commentary
	assumptions made.	
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• The previous mining operations included the development of waste dumps and tailings at the site. Waste rock from underground is used to cap historic tailings. • The area is not located in an environmentally sensitive area and all environmental approvals are in place
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	• 4069 density measurements (water immersion method) were taken from ore and waste material derived from older and recent OBM drilling. Bulk density values used in the resource were 1.5t/m3, 2.43t/m3 and 2.81t/m3 for oxide, transitional and fresh mineralisation respectively. Densities of 1.57t/m3, 2.61t/m3 and 3.0t/m3 for oxide, transitional and fresh waste were assigned. • A fresh rock ore density of 2.88 g/cm^3 was determined by Oretest laboratory on a bulk ore sample in 1998. • These bulk density estimates are similar to values determined for comparable basalt hosted gold deposits, and in particular Missouri deposit 600m to the south.

Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.*
	• *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).*
	• *Whether the result appropriately reflects the Competent Person's view of the deposit.*
		• Mineral Resources were classified in accordance with the Australasian Code for the Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC, 2012). The Mineral Resource was classified as Indicated and Inferred Mineral Resource on the basis of data quality, sample spacing, and lode continuity.
		• The Indicated portion of the Mineral Resource was defined where:
		  ○ Good support from drilling, averaging a nominal 40mN x 40mE.
		  ○ Areas where the estimation quality is reasonable mainly assessing kriging slope.
		• The remaining portions of the deposit were classified as Inferred Mineral Resource where:
		  ○ Data support is poorer with drilling typically greater than 40m x 40m.
		  ○ Areas where the estimation quality is poorer mainly assessing kriging slope.
		• The definition of mineralised zones is based on sound geological understanding of the controls on mineralisation. This is largely due to recent detailed pit mapping and exposure in underground workings which has produced a robust model of mineralised domains.
		• Inferred resources are typically at the periphery of mineralised domains and at depth where drill density and therefore confidence is generally lower.
		• The Mineral Resource estimate appropriately reflects the view of the Competent Person.

Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• The current MRE has been internally peer reviewed.

Criteria	JORC Code explanation	Commentary
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• The Sand King Mineral Resource estimate is reported with a reasonable degree of confidence. The data quality is good and the drillholes from recent drilling by EGS/OBM have detailed logs produced by qualified geologists. Historic logging has been reviewed. • Confidence in the estimate allows reasonable quantification of global metal content. The interpretation is considered globally robust but at a local scale, variations to ore geometry and/or grade could be expected. • All Measured and Indicated resources are relevant to economic evaluation. • The deposit is currently being mined. • Historical production records are available for the deposit.

Operator	Period	Tonnes Mined	Head Grade	Recovered Grade	Recovery	Ounces Produced
WMC	1980 - 1986	321,853	5.2	4.77	0.92	49,388
	1986 - 1987	Production Suspended				
	1987 - 1991	425,202	3.11	2.85	0.91	38,907
	Total Production	**747,055**	**4.01**	**3.68**	**0.92**	**88,295**
Monarch Gold	2007/2008	48,073		2.27		3,478
EGS*	2018	118,400		1.12		4,233
OBM	2023 - 2024	122,002	1.97			7,710

* Includes Laterite and Low-Grade Stockpile

Section 3 Estimation and Reporting of Mineral Resources – Waihi

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	• Data from EGL/OBM drilling captured into Field Marshall logging software. Data sent from site and imported into SQL database via DBMS. Validation checks in SQL database are carried out to ensure data integrity is not compromised. • The data is verified by company geologists before being sent to the DBA for validation or passing Geobank Software validation protocols • Historic data has been verified by checking historical reports on the project. • The Competent Person has undertaken a number of validation checks on the database, using Micromine software which include, but are not limited to, checks for overlapping intervals, checks for missing data/records, visual checks on drillhole locations and traces to identify any possible survey issues. No major issues were detected.

Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*
	• *If no site visits have been undertaken indicate why this is the case.*
		• Numerous site visits have been completed by the Competent Person with the following objectives:
		  ○ View geology in existing open pit
		  ○ View drilling operations
		  ○ View and log drill core

Criteria	JORC Code explanation	Commentary

Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.*
	• *Nature of the data used and of any assumptions made.*
	• *The effect, if any, of alternative interpretations on Mineral Resource estimation.*
	• *The use of geology in guiding and controlling Mineral Resource estimation.*
	• *The factors affecting continuity both of grade and geology.*
		• Mineralised structures at Waihi strike from 320° to 345° and are steeply west dipping. Mineralised lodes at Homeward Bound strike 325° and are steep east dipping. The main Waihi lodes are interpreted to be the west limbs of a tightly folded antiform. Homeward Bound lodes are the east limbs of the same antiform. Parasitic folds are evident and plunge moderately to the north. This is coincident with the plunge of high grade mineralisation. Mineralisation appears to concentrate in areas of competency contrast between:
		  ○ High-Mg basalt the tholeiitic basalt
		  ○ Coarse grained amphibolite units within tholeiitic basalt
		• Late stage E-W structures have been mapped and may offset the mineralised lodes slightly. These structures have also been exploited by thin pegmatite dykes.
		• Geology model proposed by Model Earth PTY. LTD following a site visit to map pit exposures and selected core.
		• Structural data from OBM drilling was used to guide the orientation of mineralised lodes where possible.
		• Inspection of core, RC chips and pit exposures shows the mineralisation to be associated with biotite and silica alteration and quartz-carbonate veining.
		• Geological continuity of mineralised strictures are well defined, although sometimes terminate abruptly, possibly due to the minor offsets caused by the E-W structures. The main lodes at Waihi are geologically continuous over 0.9 km and are known to extend a further 400m south to the Dexy prospect. Grade continuity is less extensive but well defined at a low cut-off grade (0.4g/t)

Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The main lodes at Waihi are geologically continuous over 0.9 km in a N-S direction and defined to a depth of 200m below surface. • The Homeward Bound Lodes are continuous over 0.3 km in a NW-SE direction and defined from surface to a depth of 230 m below surface.

Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*
	• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*
	• *The assumptions made regarding recovery of by-products.*
	• *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).*
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*
	• *Any assumptions behind modelling of selective mining units.*
	• *Any assumptions about correlation between variables.*
	• *Description of how the geological interpretation was used to control the resource estimates.*
	• *Discussion of basis for using or not using grade cutting or capping.*
	• *The process of validation, the checking process used, the comparison of model data to drillhole*
		• 1m composite samples coded to the mineralised domains were used as inputs to estimation. Only RC and diamond drilling samples used for estimation.
		• Ordinary Kriging (OK) was used to estimate gold grades into a 3-dimensional block model. Estimation parameters derived from modelled semi-variograms. Micromine software was used for the estimation.
		• High grade cuts up to 40 g/t were applied to 1m composite data based on analysis of individual domains.
		• The parent block dimensions used were 10mN by 2mE by 10mRL with sub-cells of 1m by 0.5m by 1.0m. Drillhole spacing is approximately 20m between section and 20m along section. The parent block size was selected (approx. 50% of data spacing) using QKNA.
		• An orientated ellipsoid search was used to select data and was based on Kriging Neighbourhood parameters derived from the variography.
		• Estimation completed in 3 runs (Homeward bound) or 4 runs (Waihi Main) each with less restrictive search, and minimum sample parameters. The initial interpolation pass was used with a maximum range greater than the range of the principal direction of the modelled variograms. Maximum number of samples was 16, minimum was 4. A single sector search was applied. Range increased progressively and the minimum number of samples reduced.
		• No estimation of deleterious elements was carried out. Deleterious elements have not been recorded during mining by previous operators Only Au was interpolated into the block model.
		• Previous resource estimates have been completed in 2001 and 2020
		• The MRE makes use of RC grade control drilling from the previous mining episode in 2003. Production records are not available to make comparisons.
		• No assumptions have been made regarding recovery of by-products. Silver has not been routinely assayed.
		• Selective mining units were not modelled in the Mineral Resource
		• Only Au was estimated so correlation analysis was not possible
		• The deposit mineralisation was constrained by wireframes constructed using a 0.4 g/t Au cut-off grade in association with logged geology, particularly the presence of quartz veining and biotite-sulphide alteration. The wireframes were applied as hard boundaries in the estimate.
		• Grade capping was applied on a domain by domain basis due to the usually highly positively skewed grade populations
		• The validation was carried out by three methods:
		  ○ Visual comparison of block grades with nearby drill assay results on a section by section basis.
		  ○ Statistical comparison of estimated grades and composite grades on a domain by domain basis.
		  ○ Trend analysis of estimated block model grades versus composite grades on 10m northing and 5m vertical intervals.

Criteria	JORC Code explanation	Commentary
	data, and use of reconciliation data if available.	
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages and grades were estimated on a dry in situ basis. No moisture values were reviewed.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The Mineral Resource has been reported at a 0.5 g/t Au cut-off within an optimised pit shell, based on assumptions about economic cut-off grades for open pit mining. • The portions of the Mineral Resource that exists below the pit shell was reported using a 2 g/t cut-off grade, being an approximate estimate of the cut off grade for narrow vein underground open stoping.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• It is intended to adopt a selective open cut mining practise at the deposit. • Reasonable prospects for eventual economic extraction for the Waihi Mineral Resource update was confirmed by applying the conceptual A$2,400/oz pit shell which was generated using the Mineral Resource block model described above. A theoretical economic mining inventory was determined from the Indicated and Inferred material within the unconstrained Mineral Resource. Pit slopes used in the conceptual optimisation were based on preliminary geotechnical assessment of Waihi deposit. Allowance was made in the pit slopes for in-pit ramps. Assumed mining costs were applied on a progressive bench by bench basis using contractor supplied budget quotations for DGP received in October 2018 for the Davyhurst project area. The average mining costs for the pit shell was estimated to be A$4.21 per tonne of material mined which included the cost to remove the existing tailings. A dilution factor of 15% and mining recovery of 95% was applied to define the theoretical economic mining inventory within the pit shell. The conceptual combined haulage, processing and administration cost applied was A$39.33 per tonne processed and process recoveries of between 92% and 93% were applied based on weathering domains. • The underground cut-off was based on a mining cost of A$140 per tonne of ore, a dilution of 15% and mining recovery of 95%. With the exception of the underground cut-off, no other modifying factors were applied to the underground portion of the Mineral Resource.

Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	• Waihi has no known reported metallurgical issues and has been previously mined.
		• Metallurgical test-work has been completed as part of the part of the feasibility study completed in 2020
		  ○ Oxide = 94% extraction
		  ○ Transitional = 92% extraction
		  ○ Fresh = 89.8 % extraction
		Oxide and Trans Values are assumed, Fresh is from test work. Oxide and Trans only make up 4% of the resource ounces.
		• Results from previous processing (using CIP) have demonstrated that good gold recovery can be expected from modern conventional CIL processing methods.

Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• The area is not located in an environmentally sensitive area and environmental approvals are in place for the project and surface waste rock landforms for Waihi.

Criteria	JORC Code explanation	Commentary
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	• Bulk density determinations were derived from measurements (immersion method) made on recent core samples drilled by OBM. Results compared favourably with limited measurements taken by previous operators using the calliper method. • Bulk density values used in the resource were 1.9 t/m3, 2.5 t/m3 and 2.94 t/m3 for oxide, transitional and fresh material, both ore and waste. • It is assumed there are minimal void spaces in the rocks within the Waihi deposit. Values applied in the Waihi block model are similar to other known bulk densities from similar geological terrains.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	Mineral Resources were classified in accordance with the Australasian Code for the Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC, 2012). The classification takes account of confidence in the geological interpretation, sample density and assay QAQC. In order to avoid a mosaic style of classification, solid wireframes were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, measured, indicated or inferred: • Measured – No areas of the current resource attained Measured status. • Indicated – Areas with drill spacing up to approximately 30 mE x 30 mN and with reasonable confidence in the geological interpretation and grade continuity. • Inferred – Areas with drill spacing in excess of 30 mE x 30 mN and where grade continuity is poorer as defined by a lower sample density, even though geological continuity may be apparent. • The input data is comprehensive and of sufficient quality for use in the MRE. Significant recent drilling, covering the entire deposit, has confirmed the location and tenor of many historic drill-holes. Assay QAQC is of sufficient quality for the assays to be used in the MRE. There is sufficient understanding of the geology to support the current interpretation in terms of continuity. • The Mineral Resource estimate appropriately reflects the view of the Competent Person.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• The MRE has not been audited or reviewed in detail. However, personnel from CSA Global have viewed lode interpretations, estimation parameters and classification at a high level of the 2020 MRE.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• The Waihi Mineral Resource estimate is considered to be reported with a reasonable degree of confidence. The data quality is good and the drillholes from recent drilling have detailed logs produced by qualified geologists. Historic logging has been reviewed. • The Mineral Resource statement relates to global estimates of tonnes and grade. Confidence in the estimate allows reasonable quantification of global metal content. The interpretation is considered globally robust but at a local scale variations to ore geometry and/or grade can be expected. • The deposit is not currently being mined. • Waihi Production records up to December 1996 are available. Total ore reserves were 761Kt @ 2.41 g/t for 59,000 ounces. Mill production was 704Kt @ 2.39 g/t for 54,000 ounces.

Section 4 Estimation and Reporting of Ore Reserves

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• *Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.* • *Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.*	• All Mineral Resources were completed by Ora Band Mining (OBM) using Ordinary Kriging and formed the basis for re-estimation of the Ore Reserve. • Where applicable the Mineral Resources were depleted to and including the 30 June 2025. • Mineral Resources are reported inclusive of the in situ Ore Reserves. The total Ore Reserve includes an estimated 752,000 t at 1.0 g/t of economic material in surface stockpiles. • The Riverina Ore Reserve was estimated from a diluted Mineral Resource. The diluted Mineral Resource was created from the undiluted resource by constraining the model to a minimum width of 1.6 m at a cut-off grade of 0.9 g/t with each lode evaluated on a spacing of 10 mN x 10 mRL. • The Sand King Ore Reserve was estimated from a diluted Mineral Resource. The diluted Mineral Resource was created from the undiluted resource by constraining the model to a minimum width of 1.6 m at a cut-off grade of 0.9 g/t with each lode evaluated on a spacing of 10 mN x 10 mRL.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	• The site was initially visited by Mr Geoff Davidson on May 20th, 2020 and on several occasions subsequently. Mr Davidson is the Competent Person for portions of this Ore Reserve estimate relating to the open pit operations. During the site visit representative diamond drill core for each of the deposits was inspected for areas within the proposed mining envelopes. In addition, visits were made to each of the proposed mining locations and inspections were made of the existing plant site and associated infrastructure at Davyhurst. Mr Davidson is satisfied the conditions allowed for in this Ore Reserve estimate is consistent with the observations made during the site visit. • The site has been visited by Mr Leroy Savage on multiple occasions as he was formerly site based at the Siberia mining complex. He is currently part of Ora Banda Mining's corporate mining engineering team. Mr Savage is the Competent Person for Riverina and Sand King Underground Ore Reserve estimate. Mr Savage has inspected representative diamond drill core for the Sand King Underground for areas within the proposed mining envelope. In addition, inspections were made of the existing plant and associated infrastructure at Davyhurst. Mr Savage is satisfied the conditions allowed for Riverina and Sand King Underground Ore Reserve estimate are consistent with the observations made during various site visits. • The Competent persons are satisfied the parameters and modifying factors used to determine their respective Ore Reserve are appropriate.
Study status	• *The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.* • *The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.*	• This Ore Reserve estimate is an update for the DGP; the mining costs used to determine the economic mining envelopes and convert Mineral Resources into Ore Reserves are based on mining costs specific to the locations considered. The evaluation of the Ore Reserves is considered to be at a pre-feasibility level of confidence or better. Technically achievable mine plans were developed for each mining location and determined to be economically viable following the application of appropriate Modifying Factors and practical mining programs. The costs and parameters used are based on existing realised costs and current or recent hard dollar contracts implemented for the project.
Cut-off parameters	• *The basis of the cut-off grade(s) or quality parameters applied.*	• Cut-off grade parameters were determined using realised costs from existing or recent project specific hard dollar contracts, as well as realised internal costs for OBM labour, plant and equipment. Ore haulage costs were based on contracts in place at the time. Processing costs were based on an assessment of realised costs to date and forward projections. Site general costs and administration overheads (G&A) were based on existing realised costs and forward projections specific to the mining operations. Selling costs were based on standard State Royalties and existing third party royalty agreements. Metallurgical process recoveries were based on recent demonstrated process plant performance and the most recent metallurgical test work. • Cut off grades for Sand King Underground reserves and the cut off grade for Riverina Underground reserves were based on a gold price of A$2,500 /oz. The cut off grade for Waihi supports a gold price of A$2,400 /oz for High Grade

Criteria	JORC Code explanation	Commentary
		and A$3,400 /oz for Low Grade. The inclusion of underground mine Low Grade and Surface Stockpiles were based on a cut off grade determined at A$4,400 /oz. • The cut off grade allows for ore haulage, crusher loading, processing, site G&A and corporate overhead contributions. The total of these costs were estimated to range between A$79 to A$89 per tonne depending on mining location. • The weight average processing recovery applied to Waihi material was 90% based on plant performance and metallurgical testwork for oxide, transition and fresh material. The processing recovery applied to Riverina Underground was 88% and was based on recent metallurgical test work. The processing recovery applied to Sand King Underground was 87% and was based on recent metallurgical work. The recovery performance was 88.1% through Davyhurst plant in FY25 using a blend of Open pit stockpiles and Riverina and Sand King undergrounds. • Standard state royalties were included as well as an ad valorem third party royalty of 1% . • The cut off grade for Waihi was estimated to be 1.2 g/t. The cut off grade for Waihi Low Grade was estimated to be 0.8 g/t. • The cut off grade for the Riverina Underground was estimated to be 2.4 g/t. A cut off grade of 2.0 g/t was applied to the underground development. The Riverina Underground reserve comprises approximately 170,000 t at 3.0 g/t of development ore and contemplates 45% of ore drive advance to be via the split-firing method of extraction. • The cut off grade for the Sand King Underground was estimated to be 2.5 g/t. A cut off grade of 2.0 g/t was applied to the underground development. The Sand King Underground reserve comprises approximately 149,000 t at 2.7 g/t of development ore and contemplates 12% of ore drive advance to be via the split-firing method of extraction. • The respective cut-off grades were applied to the diluted Mineral Resource for each project. • The cut -off grade for surface stockpiles was estimated to be no less than 0.7 g/t. • Low Grade insitu material is 0.7 g/t to 2.0 g/t used for both Riverina and Sand King mines.
Mining factors or assumptions	• *The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).* • *The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.* • *The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.* • *The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).* • *The mining dilution factors used.* • *The mining recovery factors used.* • *Any minimum mining widths used.* • *The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.* • *The infrastructure requirements of the selected mining methods.*	Open Pit Mining Factors and Assumptions • A combination of approved and preliminary mine designs were used as the basis for the Ore Reserve estimate. Preliminary designs were derived from economic envelopes determined using Whittle pit optimisation, based on costs from earlier studies, as well as slope parameters determined from site specific geotechnical assessment and modified for ramps and minimum mining widths. Approved mine designs were validated in in a cash flow model. The project average mining cost for Waihi pit was estimated to be A$11.82 per tonne of material mined. These costs include provisions for grade control, drill, blast, load, haul, rehabilitation and OBM mine overheads. Cost were derived from recent contractor quotations for mining the Waihi pit and OBM mine overheads. • Conventional selective mining methods will be used for Waihi. The Waihi operations are primarily planned around using 120 t-class excavators and 90 t dump trucks. Tails mining includes low ground pressure dozing as part of the load and haul system. All material mined, excluding existing in-pit backfill, historical waste dumps and in-pit tailings, allow for drilling and blasting. The Competent Person considers the proposed mining method to be appropriate for the style and nature of the mineralisation. • Minimum mining widths of 20 m were allowed on all wall cutbacks adjacent to existing open pit workings. • The mining methods proposed are well-known and used successfully in the region. • Productivity rates considered historical performance and Industry standards. • Suitable access exists to the mine. • The mining method contemplates selectively separating waste from the ore to minimise dilution and ore loss. Ore faces will be exposed by removing waste to the identified contact prior to removing the ore. • Independent consultants were engaged to conduct a geotechnical analysis of the proposed excavation and waste material storage methods. This analysis formed the basis of pit wall design criteria and tailings disposal methods proposed at Waihi. • Allowance was made for grade control activities, including in-pit reverse circulation drilling and face sampling. • Only the Indicated and Measured portion of the Mineral Resource was used to estimate the Ore Reserve. All Inferred material was treated as waste. Background grades were estimated into the mineral resource model and subsequently included as diluting material. The average grade of dilution included in the reserve were 0.16 g/t for Waihi.

Criteria	JORC Code explanation	Commentary
		• Open pit mining blocks were diluted by applying a dilution skin to both footwall and hanging wall using Auto Stope Designer (ASD) functionality in Deswik™. The method also included internal and edge dilution resulting from forming practical mineable shapes using ASD. A skin thickness of 0.5 m was applied to Waihi to both hanging wall and footwall. A minimum mining width of 1.5 m was applied. The dilution parameters were determined from operational performance. Average dilution factors are 27% at Waihi. • Ore loss was incurred in the ASD process due to the variation between mineralised lode geometry and dig block geometry. In addition, a nominal 5% loss was applied for further mining losses occurring through normal operations. • Practical mine designs were completed for Waihi which formed the basis of scheduling and economic validation of the Ore Reserve. The strip ratio for Waihi was estimated to be 8.3 by mass inclusive of high grade and low grade ore. • Most of the infrastructure required for the operations is already established at the DGP, including a processing plant and associated infrastructure, camp, airstrip, offices, power reticulation, borefields and coreyards. An accommodation camp has been constructed at the Riverina. • Waihi is located approximately 3.5 km from the Davyhurst mill and administration centre and will be managed from there. Nominal provisions were made for site infrastructure. Underground Mining Factors and Assumptions Riverina Underground • The mining method proposed for Riverina is narrow-vein long hole open stoping using up-hole-benching techniques. This method has been successfully implemented at Riverina since 2023 along with similar styled deposits in the West Australian Goldfields region. The decline design parameters are nominally 5.5m wide x 5.7m high with an average design gradient of 1:7 down. Ore development has been planned at 4.5m wide x 4.5m high. The average floor to floor distance between levels will be 22 metres, with an average stope panel height of approximately 17.5 metres. • OBM geotechnical engineer conducted a geotechnical analysis to an appropriate level of detail. This forms the basis of stoping parameters and development ground support requirements. Stopes will be approximately 40m long x 22m high within the stable envelope of the unsupported span determined from geotechnical analysis. Provision is made for full height rib pillars between stopes and sill pillars, which will be reevaluated upon stope performance. This provision equates to a recovery of 88%. An additional 5% stope ore loss was also provisioned for operating losses. The overall mining recovery is estimated to be 85%. • The reserve inventories will be mined in proximity to known historical underground workings. The design has been stood-off an appropriate distance from known voids. Probe drilling and resultant dewatering will be undertaken prior to developing near any known voids. Appropriate procedures will be implemented during the mining episode when mining around historical underground voids. • Split firing methods will be undertaken in the planned 4.5m by 4.5m wide ore drives to minimize dilution. It is estimated for the style of mineralisation (narrow vein), the average dilution for development (for the 45% or ore drive advance where it is used) will reduce to the equivalent to developing a 3.5m wide drive. • Overall unit mining costs for the underground was estimated to be A$171/t ore inclusive of sustaining capital. • Stopes were defined by applying a 2.4 g/t cut-off to the diluted Mineral Resource. The cut-off allows for production stoping activities as well as load and haul downstream processing and sales. • A minimum stope mining width of 1.6m was applied in the dilution modelling process, with a dilution skin then applied. The dilution allows for a skin of 0.3 m on both hanging wall and footwall. In addition, a nominal allowance of 20% dilution at 0g/t was included to account for unidentified dilution sources. The global dilution of the diluted resource was estimated to be 57% of material. Dilution being all included material less than 0.7 g/t. • A cut off grade of 2.0 g/t was applied to ore drive development on a cut by cut basis. This cut-off allows for ore development mining costs, haulage, processing and sales. • Inferred material was not considered in defining the stoping envelopes; however, due to practical stope mining

Criteria	JORC Code explanation	Commentary
		geometries a small portion of Inferred material was included within the Underground Ore Reserve. This material was included at the edges of the mining envelope and equates to approximately 1.5% of the Riverina Underground Ore Reserve inventories. • Grade control will be conducted primarily via face sampling and underground diamond drilling. • Infrastructure required for the underground operations is already established at Riverina. This includes a mining camp, offices, fuel farm, workshops, core shed, water storage & pump stations, diesel generated power and conventional underground mine services. Sand King Underground • The mining method proposed for Sand King is narrow-vein long hole open stoping using up-hole-benching techniques. This method has been successfully implemented at Sand King and similar styled deposits in the West Australian Goldfields region. The decline design parameters are nominally 5.5 m wide x 5.7 m high with an average design gradient of 1:7 down. Ore development has been planned at 4.5m wide x 4.5m high. The average floor to floor distance between levels will be 22 metres, with an average stope panel height of approximately 17.5 metres. • Internal Geotechnical Engineers conducted a geotechnical analysis to an appropriate level of detail. This forms the basis of stoping parameters and development ground support requirements. Stopes will be approximately 40m long x 22m high within the stable envelope of the unsupported span determined from geotechnical analysis. Provision is made for full height rib pillars between stopes, sill pillars will be evaluated upon stope performance. An additional 5% stope ore loss was also provisioned for operating losses. The overall mining recovery is estimated to be 84%. • Split firing methods will be undertaken in the planned 4.5m by 4.5m wide ore drives to minimize dilution. It is estimated for the style of mineralisation (narrow vein), the average dilution for development (for the 12% or ore drive advance where it is used) will reduce to the equivalent to developing a 3.5m wide drive. • Overall unit mining costs for the underground was estimated to be A$168/t ore, inclusive of sustaining capital. • Stopes were defined by applying a 2.5 g/t cut-off to the diluted Mineral. The cut-off allows for production stoping as well as load and haul downstream processing and sales. • A minimum stope mining width of 1.6m was applied in the dilution modelling process, with a dilution skin then applied. The dilution allows for a skin of 0.3m on the hanging wall and 0.3m on the footwall. In addition, a nominal allowance of 5% dilution was included to account for unidentified dilution sources. The global dilution of the diluted resource was estimated to be 32% of material and the global average grade of dilution was estimated to be 0.15 g/t. Dilution being all included material less than 0.7 g/t. • A cut off grade of 2.0g/t was applied to ore drive development on a cut by cut basis. This cut-off allows for ore development mining costs, haulage, processing and sales. • Inferred material was not considered in defining the stoping envelopes; however, due to practical stope mining geometries a small portion of Inferred material was included within the Underground Ore Reserve. This material was included at the edges of the mining envelope and equates to approximately 2.6% of the Sand King Underground Ore Reserve inventories • Grade control will be conducted primarily via face sampling and underground diamond drilling. • Infrastructure required for the underground operations is already established at Sand King Underground this includes the Davyhurst mining camp, site offices, fuel farm, workshops, core shed, water storage & pump stations, diesel generated power and conventional underground mine services.
Metallurgical factors or assumptions	• *The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.* • *Whether the metallurgical process is well-tested technology or novel in nature.* • *The nature, amount and representativeness of metallurgical test work undertaken, the nature of the*	• The process for treating ore is conventional CIL with some gold recovered via gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. • A process recovery of 88% was applied to Riverina Underground based on metallurgical testing of samples taken from within the proposed mining envelope. This is confirmed by the Davyhurst processing performance. • A process recovery of 87% was applied to Sand King Underground based on metallurgical testing of samples taken from within the proposed mining envelope. This is confirmed by the Davyhurst processing performance. • A weight average process recovery of 90% was applied to Waihi open pits based on metallurgical testing of oxide,

Criteria	JORC Code explanation	Commentary
	metallurgical domaining applied and the corresponding metallurgical recovery factors applied. • *Any assumptions or allowances made for deleterious elements.* • *The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.* • *For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?*	transition and fresh samples taken from within the proposed mining envelope. This is inline with historical open pit recovery at Davyhurst processing plant. • The process plant has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm. The process plant has been successfully operated, and further operational improvements are proposed.
Environmental	• *The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.*	• All of the ORE projects have approved Mining Proposals along with clearing permits and appropriate water licences. • All flora and fauna baseline studies have been completed for areas that may potentially be influenced by mining operations contemplated in this Ore Reserve estimate. No conservation significant taxa were identified as being at risk. • Searches of Indigenous and European State Heritage Registers have not identified any sites that require active management. • Both historical and recent geochemical data indicate the majority of waste rock mass is non-acid forming. Sulphidic sedimentary units at Riverina will be intersected occasionally by underground development and will be classed as Potential Acid Forming (PAF) . The storage of PAF waste is being managed through co-mingling with Acid Neutralising Capacity(ANC) waste in accordance with the approved Mine Closure plan. Test work on Waihi tails has determined that there is no PAF risk. Provisions for the management of PAF were allowed for in this estimate. Test work on Sand King underground has reported that there is no PAF risk • Tailings from ore processing will be stored within the existing Tailings Storage Facility (TSF). Allowance has been made for expansions to this facility as required by the mine plan.
Infrastructure	• *The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.*	• The majority of required infrastructure is established and commissioned. Small temporary satellite facilities for Waihi will be required. Preliminary provisions were made within the financial analysis for these facilities. • Additional accommodation camp capacity has been constructed at both Davyhurst and Riverina. Communication is established at all operating locations. • The operation is currently serviced by an existing airstrip adjacent to the Callion mine workings and from Kalgoorlie airport.
Costs	• *The derivation of, or assumptions made, regarding projected capital costs in the study.* • *The methodology used to estimate operating costs.* • *Allowances made for the content of deleterious elements.* • *The source of exchange rates used in the study.* • *Derivation of transportation charges.* • *The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.* • *The allowances made for royalties payable, both Government and private.*	• Initial capital has been fully expensed. Sustaining capital was allowed for in the financial analysis . • Mining and ore haulage costs were estimated from hard dollar contracts for the project current at the date of the Ore Reserve. • Power, diesel and accommodation costs were based on current realised costs and FY26 budget forecasts. Staff costs were based on current employment contracts in place. • Processing operating costs were based on current performance and FY26 budget forecasts. • Unit costs for haulage, processing and site overheads were estimated based on scheduled utilisation of process capacity using material above the economic cut off grade. • Open Pit Mining operations specific overhead costs were included based on inflated costs from FY24 budget. • Riverina Underground overheads and fixed costs applied to the Ore Reserve were factored based on proportion of total contracted material movement estimated month to month being on average 90% of contracted material movement over duration of the reserve case. The contracted material relies on the conversion to reserve of additional Mineral Resource. • Sand King Underground overheads and fixed costs applied to the reserve were factored based on proportion of total contracted material movement estimated month to month being on average 88% of contracted material movement over duration of the reserve case. The contracted material relies on the conversion to reserve of additional Mineral Resource.

Criteria	JORC Code explanation	Commentary
		• Corporate overhead were assigned based on the estimated costs attributable to operations being 50%. • No deleterious elements have been identified or are expected. • All costs were quoted and compiled in Australian dollars. • The standard WA state government royalty for gold was allowed for. Third party royalties of 1% ad valorem were applied in the financial analysis.
Revenue factors	• *The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.* • *The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.*	• Revenue calculations were based on detailed mine plans and mining factors including provision for dilution and ore loss. • A financial analysis was completed on A$3,300/oz before selling costs and is below the current spot price as of the date of this announcement.
Market assessment	• *The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.* • *A customer and competitor analysis along with the identification of likely market windows for the product.* • *Price and volume forecasts and the basis for these forecasts.* • *For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.*	• There are no known major gold producers expecting to influence the global supply of gold over the period of the project. • Demand for gold is expected to be subject to usual global factors.
Economic	• *The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.* • *NPV ranges and sensitivity to variations in the significant assumptions and inputs.*	• The Ore Reserve estimate was validated using a financial model prepared to a budget level of accuracy for the purpose of project evaluation using realised costs to date and existing contract pricing. • All inputs from open pit and underground operations, processing, transportation and sustaining capital as well as contingencies have been scheduled and evaluated to generate a life of mine financial model. • Economic inputs have been sourced from operational budgets, contractors and DGP accounts for internal costs. • Unit costs for haulage, processing and site overheads were estimated based on full utilisation of process plant capacity using material above the economic cut off grade. • No escalation of gold price or costs is included. • A discount rate of 8%pa was applied. • The NPV of the Project is positive at an assumed commodity price of A$3,300/oz and the Competent Persons are satisfied that the project economics retains a suitable margin of profitability based on the reserve assumptions. • Sensitivity analysis ranking of variable factors; gold price, grade, metallurgical recovery followed by operating costs.
Social	• *The status of agreements with key stakeholders and matters leading to social licence to operate.*	• To the best of the Competent Persons knowledge all agreements are in place and current with all key stakeholders including traditional owner claimants.
Other	• *To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:* • *Any identified material naturally occurring risks.* • *The status of material legal agreements and marketing arrangements.* • *The status of governmental agreements and approvals critical to the viability of the project, such*	• Riverina and Sand King are active mines. • A formal process to assess and mitigate naturally occurring risks will be undertaken prior to execution of new mining projects. Currently, all naturally occurring risks are assumed to have adequate prospects for control and mitigation. • All proposed mining operations are contained within granted mining leases 100% owned by Ora Banda Mining. • All approvals are in place for Riverina Underground which is currently producing. • Sand King underground operations are fully permitted pending final assessment of the Category 6 Dewatering Prescribed Premise Licence which there is no known impediment to it being approved.

Criteria	JORC Code explanation	Commentary
	as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.	• All approvals are in place for Waihi open pit mining.
Classification	• *The basis for the classification of the Ore Reserves into varying confidence categories.* • *Whether the result appropriately reflects the Competent Person's view of the deposit.* • *The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).*	• The Proved and Probable Ore Reserves were based on that portion of the Measured and Indicated Mineral Resource respectively within the mine design that may be economically extracted and includes an allowance for dilution and ore loss. • The result appropriately reflects the Competent Person's view of the deposit and how it will be exploited. • The Ore Reserve is inclusive of surface stockpiles above the relevant cut off grade and total 751,869 t at 1.0 g/t . All surface stockpiles were classified as Proved. • Measured material was classified as Proved in the Ore Reserve. • Inferred material within the Riverina Underground Ore Reserve equates to 13,936t at a grade of 3.4g/t. This material is included at the edges of the mining envelope and equate to 1.5% of the Ore Reserve inventories. • Inferred material within the Sand King Underground Ore Reserve equates to 36,064t at a grade of 2.0g/t . This material is included at the edges of the mining envelope and equate to 2.6% of the Ore Reserve inventories.
Audits or reviews	• *The results of any audits or reviews of Ore Reserve estimates.*	• The Ore Reserve estimate, along with the mine design, life of mine plan and modifying factors, has been peer-reviewed internally by Ora Banda Mining Pty Ltd and by independent consultants.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.* • *It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• The design, schedule and financial model on which the Ore Reserve is based was completed to a feasibility level of accuracy for project evaluation purposes. Costs were taken from existing contracts, contractor budget quotations and internal realised costs reported from OBM accounts. • The Ore Reserve is a global estimate based on the Mineral Resource Estimate. • There is a degree of uncertainty associated with geological estimates. The Reserve classifications reflect the levels of geological confidence in the estimates. • There is a degree of uncertainty regarding estimates of impacts of natural phenomena including geotechnical assumptions, hydrological assumptions and the modifying mining factors, commensurate with the current status of the project. The Competent Person is satisfied that the analysis used to generate the modifying factors is appropriate, and that a suitable margin exists under current market conditions to allow for the Reserve estimate to remain economically viable despite reasonably foreseeable negative modifying factor results. • Unit costs for haulage, processing and site overheads were estimated based on schedule utilisation of process plant capacity using material above the economic cut off grade. • There is a degree of uncertainty regarding estimates of commodity prices and exchange rates, however the Competent Person is satisfied that the assumptions used to determine the economic viability of the Ore Reserves are reasonable based on their source. • Where applicable parameters and modifying factors used were calibrated against actual operational data and reconciliations.