

ASX Announcement

25 May 2017

Mineral Resource Update at Mulga Rock Project

Vimy Resources Limited (“**Vimy**” **ASX: VMY**) is pleased to announce the results from a Mineral Resource update on the Ambassador deposit at its Mulga Rock Project (**MRP**). This update relates to the Ambassador East deposit where recent drilling was completed in 4Q 2016, and is part of a larger resource update of the entire Mulga Rock Project which is due for release in June 2016.

The key highlights from the Mineral Resource Estimation (**MRE**) update are:

- **Maiden Measured Mineral Resource for the MRP (12.4Mlb U₃O₈) high-grade, Measured Resource at greater than 0.11% U₃O₈ (1,100ppm)**
- **A 14% increase in contained metal at Ambassador East (from 12.4 to 14.1Mlb U₃O₈)**
- **Further resource work underway indicates a 20-25% uplift in metal in the entire Ambassador Resource**
- **Spectacular drilling results include: 7.5m @ 2,598ppm U₃O₈ and 4.5m @ 2,792ppm U₃O₈**

During the course of the ongoing Definitive Feasibility Study (**DFS**) two open pits were excavated on the Ambassador deposit from which 75 dry tonnes of ore was excavated (see ASX Announcement “Mulga Rock Test Pit Bulk Sample Result” 14 June 2016). The assessment of the material from the test pits confirmed that the contained U₃O₈ in the excavated material was 53% higher than expected from the resource model. The announcement forecast that further drilling, called ‘Optimisation Drilling’, would be conducted which was carried out in 4Q 2016.

The 4Q 2016 drilling program, which was used for this updated MRE, was carried out over part of the Ambassador East deposit which falls inside the current pit designs. Key intersections include:

- NNA7060 (AC) 5m @ 2,090ppm U₃O₈ from 38.5m,
- NNA7092 (AC) 4.5m @ 2,792ppm U₃O₈ from 39.5m,
- NND7108 (DD) 2.3m @ 3,008ppm U₃O₈ from 44.9m,
- NND7304 (DD) 4.9m @ 2,417ppm U₃O₈ from 44.9m,
- NNA7146 (AC) 7.5m @ 2,598ppm U₃O₈ from 43.5m, and
- NND7041 (DD) 2.3m @ 4,059ppm U₃O₈ from 34.5m.

Ambassador East will provide ROM Feed for the first years of production. Significantly, there has been a 92% conversion from Indicated to Measured Status. The MRE geological modelling, variography, and grade estimation was carried out in-house and validated by AMC Consultants. A full description of methodologies and assumptions are provided in the appended JORC Code, Table 1.

Managing Director, Mike Young said, “This resource upgrade is very positive for us, but more importantly, the lessons we’ve learned and applied to our models will result in very improved economics in the DFS. Instead of talking about forward demand for uranium, we’ll be able to compete in today’s market.

“In a nutshell, these results have changed our paradigm from a wannabe to a gonna-be.”

Please consider the environment before printing this announcement past Page 6.

Mulga Rock Project

The Mulga Rock Project is 100% owned and operated by Vimy and lies approximately 240km east-northeast of Kalgoorlie, situated on two granted Mining Leases (ML39/1104 and ML39/1105). Vimy holds title to approximately 750 square kilometres of exploration ground across the Mulga Rock Project (Figure 1).

The Mulga Rock East Mining Centre comprises the Ambassador and Princess resources and will form the first stage of the mine development for the project (Figure 1). The Ambassador resource is a large, flat-lying deposit that is approximately 9km in length and 1km wide. It has been extensively drilled with 1,606 aircore and reverse circulation (AC and RC) holes completed for a combined total depth of 101,174 metres, and 366 diamond drill holes (DDH) for 20,065 metres.

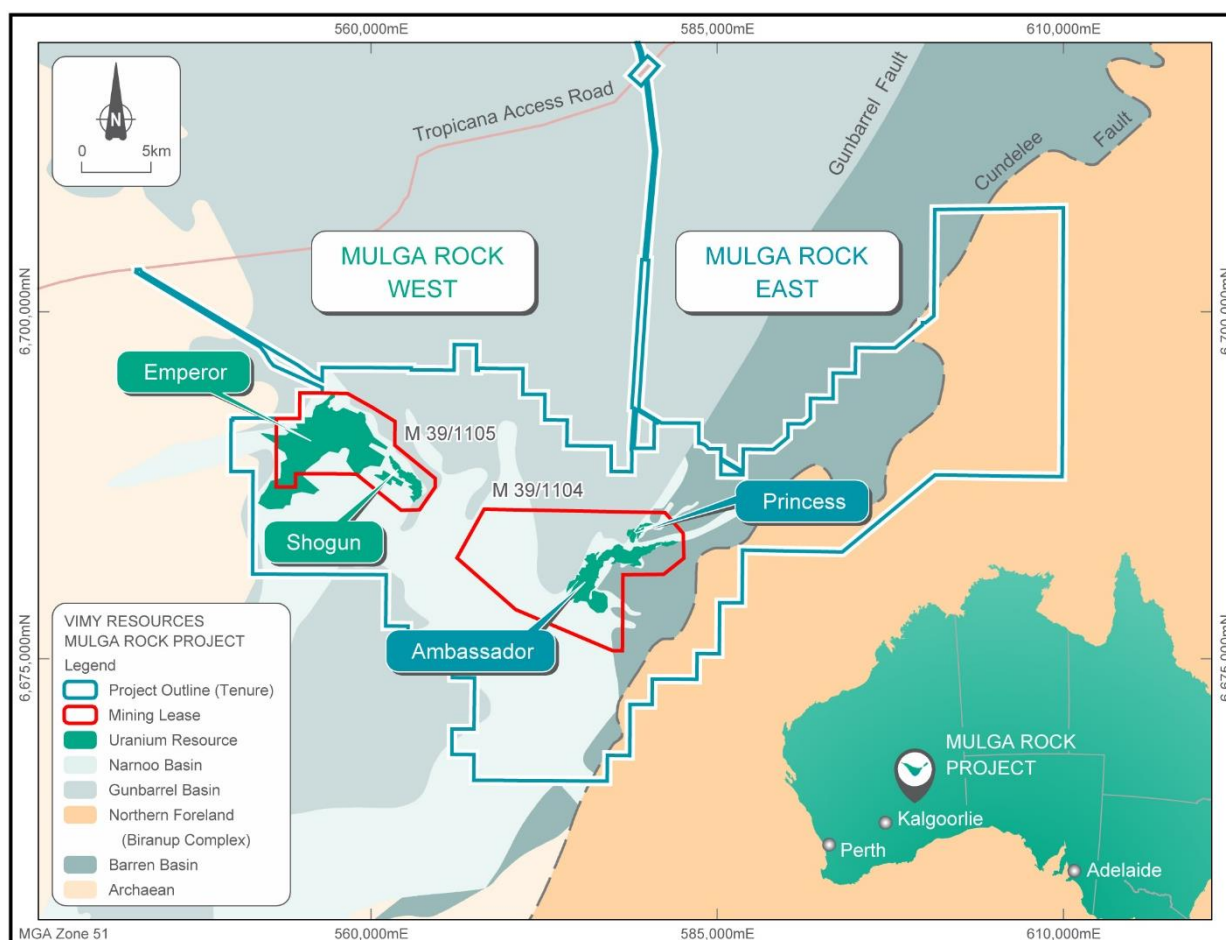


Figure 1: Location of Mulga Rock Uranium Deposits

Resource Estimates at Ambassador East

The 4Q 2016 drilling program, and this mineral resource estimation, was conducted on a 4km long section of the Ambassador East resource (Figure 2) using a drill spacing varying between 50 x 80m and 50 x 40m. A number of improvements were made to sampling procedures in the 4Q 2016 drilling program, including vacuum packing of diamond drill core at the rig to preserve moisture, and two-stage validation of wireline data. Drill intercepts for this drilling program are listed at the end of this release.

The revised 2017 Mineral Resource has increased by 14% in terms of contained U_3O_8 metal compared to the June 2016 estimate (Table 1) comprising an increase in tonnage of 3% and an increase in grade of 11%.

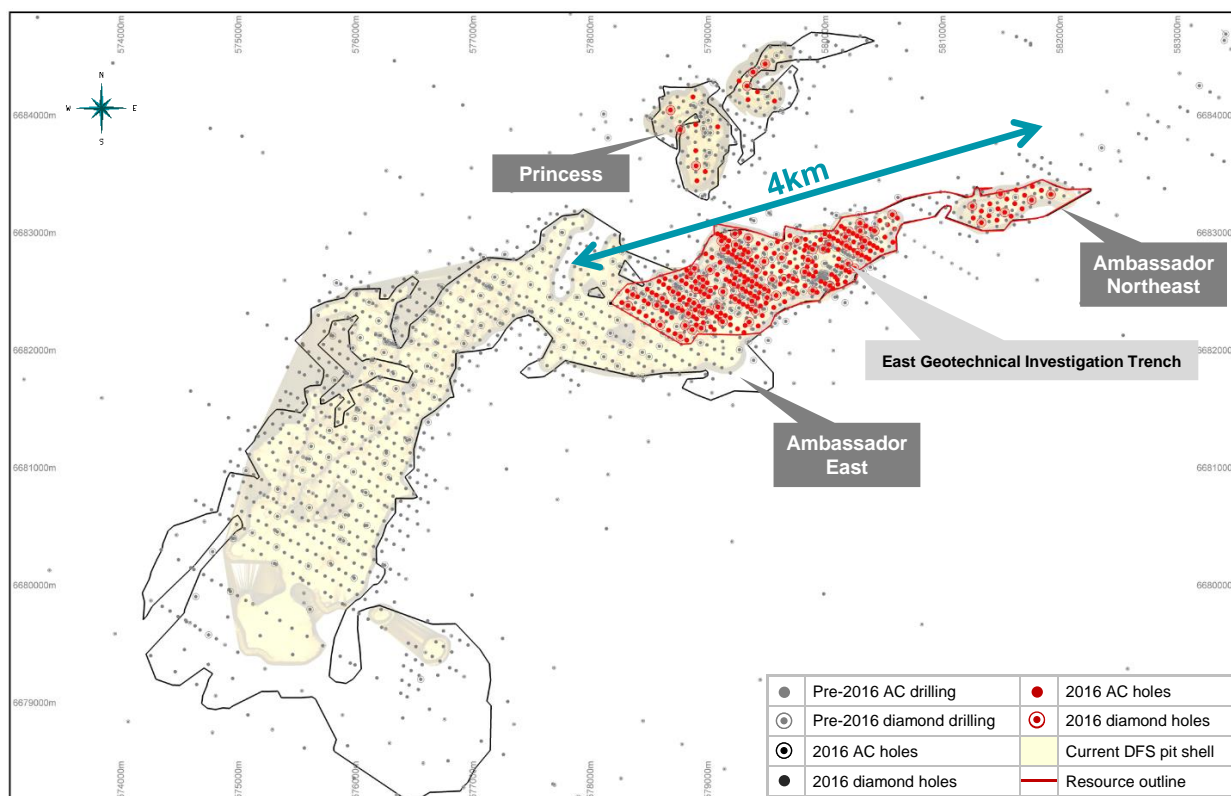


Figure 2: Ambassador and Princess – Collar location map and drill hole type

Overall the Company has identified several areas where the understanding of controls on mineralisation, input data, and resource modelling processes have improved and cumulatively leads to a material increase in the uranium metal:

- Drill hole density: increased drilling density, irrespective of drilling method, increases contained metal (common in supergene deposits),
- DDH versus aircore: DDH shows a slightly thinner ore horizon at much higher uranium grade for similar contained metal as for comparable air core holes,
- Ore densities from diamond core data have increased with improved methodology,
- Detailed twin hole drilling has improved understanding of disequilibrium factors and allows application by geological domain rather than globally, and
- A better understanding of the controls on mineralisation and geological modelling.

Table 1: Ambassador East Deposit Mineral Resource (2017 vs 2016) – infill drill area only ^{1, 2}

Deposit / Resource	Classification	Cut-off Grade (ppm U ₃ O ₈)	Tonnes (Mt) ¹	U ₃ O ₈ (ppm) ²	U ₃ O ₈ (Mlb)
2017 Mineral Resource – Infill area					
Ambassador East	Measured	150	5.1	1,105	12.4
Ambassador East	Indicated	150	0.6	685	0.8
Ambassador East	Inferred	150	1.1	360	0.9
Total			6.7	950	14.1
2016 Mineral Resource – Infill area					
Ambassador East	Measured	150	-	-	-
Ambassador East	Indicated	150	6.4	870	12.2
Ambassador East	Inferred	150	0.2	475	0.2
Sub-Total			6.6	855	12.4
Difference (%)			+3	+11	+14

¹ t = metric dry tonnes; Appropriate rounding has been applied, and rounding errors may occur.

² Using cut combined U₃O₈ composites (combined chemical and radiometric grades).

Table 2 summarises the current global resource of 78.5Mlb U₃O₈ including 12.4Mlb U₃O₈ of Measured material. It is expected that most of this material will convert to Proven Reserves at the completion of the DFS.

While Table 2 is presently up-to-date, the Company is carrying out further work to update the MRP global resource estimates (Princess, all of Ambassador, and Shogun) and expects to provide this to the market in July. The work so far indicates the presence of two distinct, very high-grade (>1,000ppm) zones at Ambassador East and Ambassador West. Furthermore, Vimy considers that the global increase in contained metal at Ambassador and Princess will be in the order of 20 to 25% over the previously announced resource (ASX Announcement 8 November 2017).

Table 2: Mulga Rock Project Mineral Resource, 22 May 2017 ^{1, 2}

Deposit / Resource	Classification	Cut-off Grade (ppm U ₃ O ₈)	Tonnes (Mt) ¹	U ₃ O ₈ (ppm) ²	U ₃ O ₈ (Mlb)
Mulga Rock East					
Princess	Indicated	150	1.3	690	1.9
Princess	Inferred	150	2.5	380	2.1
Ambassador	Measured	150	5.1	1,105	12.4
Ambassador	Indicated	150	14.0	655	20.1
Ambassador	Inferred	150	11.3	335	8.3
Sub-Total			34.2	595	45.0
Mulga Rock West					
Emperor	Inferred	150	30.8	440	29.8
Shogun	Indicated	150	1.9	680	2.9
Shogun	Inferred	150	1.1	390	0.9
Sub-Total			33.7	450	33.6
Total Resource			67.9	525	78.5

¹ t = metric dry tonnes; Appropriate rounding has been applied, and rounding errors may occur.

² Using cut combined U₃O₈ composites (combined chemical and radiometric grades).

Upcoming activities

During the next two quarters the Company will:

- Complete current collation of the Draft DFS and financial model using the June 2016 resource model,
- Complete a global resource estimation model of Ambassador East (this announcement), Ambassador West, Shogun and Princess using new data and principles identified here,
- Complete a new Ore Reserve using the new resource models,
- Re-run financials with new model metal throughputs, and
- Assess all FID Optimisation alternatives such as staged, high-grade implementation.

The activities above will feed into the updated and final DFS to be completed in the September quarter 2017 and published thereafter.

Geology of the Mulga Rock Uranium Deposits

The Mulga Rock uranium deposits are hosted by Late-Eocene to Cretaceous, lacustrine and estuarine sediments comprising fine-grained clastic sands, silts and clays, and carbonaceous matter derived from plants. Uranium and base-metal mineralisation are predominantly associated with supergene enrichment within carbonaceous-rich sediments at, or just below, the weathering horizon.

The sediments have been strongly oxidised by weathering to depths typically between 25-55 metres. The uranium and base metals have been leached from the weathered zone and re-precipitated in horizontal zones at the reduction-oxidation (redox) boundary. The uranium mineralisation is mostly amorphous and has been absorbed onto the carbonaceous material or precipitated as very fine-grained uraninite (UO_2).

The mineralised zones are similar in geology, mineralogy and host rock material across all deposits.

Typical long and cross sections of the portion of the Ambassador East Mineral Resource drilled during the program are shown in Figures 3 and 4. The cross sections show the resource block model with a 150ppm U_3O_8 cut-off grade. The main uranium domain is located directly below the redox boundary that is located predominantly within Eocene sediments, typically 2 to 6 metres thick.

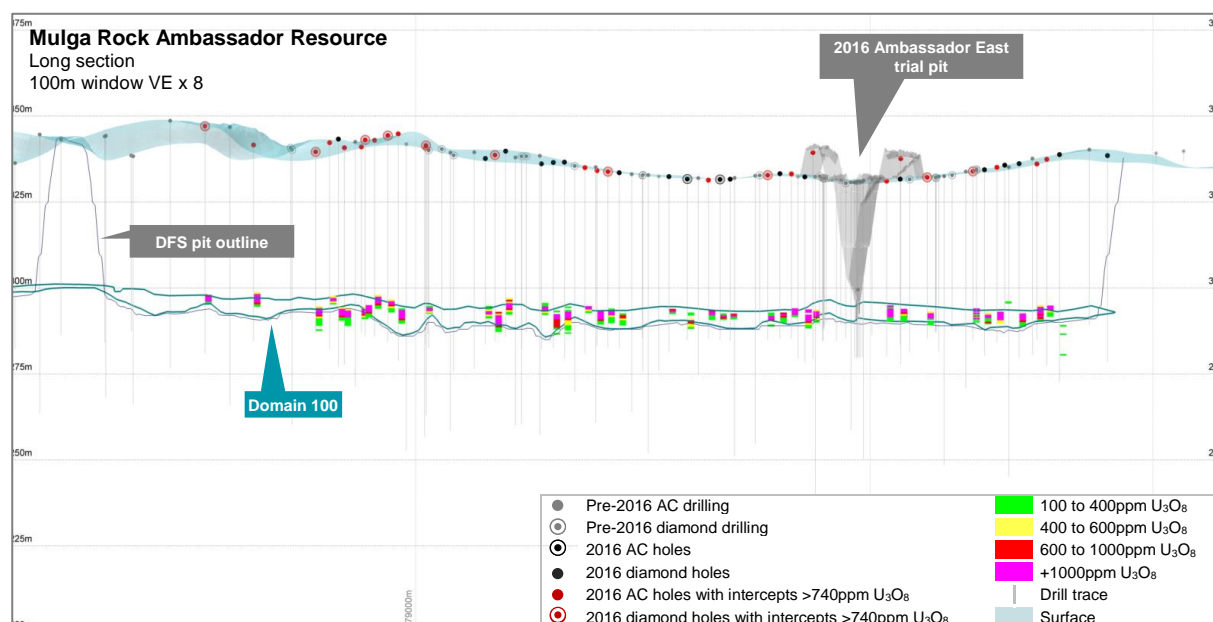


Figure 3: Ambassador Resource – Long section – vertical exaggeration 8x

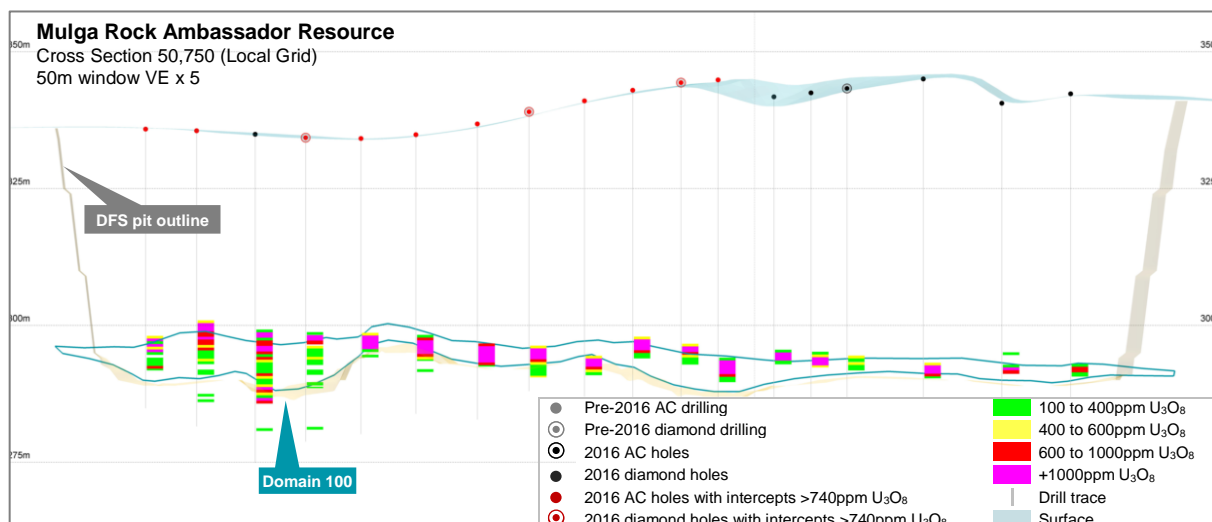


Figure 4: Ambassador Resource – Schematic cross section 50,750N – vertical exaggeration 5x



Mike Young
Managing Director and CEO
Dated: 25 May 2017

The information in this announcement that relates to the Exploration Results for the Mulga Rock Resource Estimate (U_3O_8), are based on information compiled by Xavier Moreau, who is a Member of the Australian Institute of Geoscientists. Mr Moreau is a full-time employee of Vimy Resources. Mr Moreau has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which is being undertaken to qualify as Competent Persons as defined in the 2012 Edition of the JORC 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Moreau consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears.

The information in this announcement that relates to the Mulga Rock Mineral Resource estimates (U_3O_8) is based on information compiled under the supervision of AMC Consultants as consultants to the Company and reviewed by Ingvar Kirchner an employee of AMC Consultants. Mr Kirchner consents to the inclusion, form and context of the relevant information herein as derived from the original resource reports. Mr Kirchner has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which is being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the JORC 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'.

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Mulga Rock Project

Ambassador May 2017 Mineral Resource Update

Executive Summary

Ambassador is one of four uranium deposits comprising the Mulga Rock Project (MRP). The MRP is located approximately 240 km east-northeast of Kalgoorlie in Western Australia. The area of the Ambassador Deposit was subject to uranium exploration by PNC Exploration Australia Pty Ltd (PNC) during 1981 to 1988, which resulted in the discovery of uranium mineralisation. The MRP currently comprises the Emperor, Shogun, Ambassador and Princess uranium deposits which are located within Mining Leases (ML) 39/1104 and 39/1105.

This report documents an updated 2017 Mineral Resource for the portion of the Ambassador deposit subjected to infill drilling in Q4 2016 (Ambassador East). The estimate was completed by Vimy Resources Ltd (Vimy) under the supervision of AMC Consultants Pty Ltd (AMC). The report complies with disclosure and reporting requirements set forth in the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves of December 2012 (the JORC Code¹) as prepared by the Joint Ore Reserves Committee of the Australasian Institute of Mining and Metallurgy, Australian Institute of Geoscientists and Mineral Council of Australia (JORC).

A Mineral Resource for Ambassador was completed in January 2009 following a small drilling programme in 2008 aimed at confirming the tenor of mineralisation at MRP. Uranium data only was examined. Subsequently, a material amount of additional infill drilling has been completed in 2009, 2014, 2015, and 2016 at Ambassador, resulting in several iterations of updated Mineral Resource estimates for Ambassador. The current Mineral Resource covering Ambassador East is interim portion of a study for the Ambassador uranium deposit that will be used in a Definitive Feasibility Study.

The Ambassador deposit is a supergene deposit associated with multiple phases of weathering, the most recent of which have occurred within the last 300,000 years. The mineralogy of the MRP is diverse, with over 50 minerals being recognized at the nearby Shogun Deposit in addition to the common rock-forming minerals. The bulk of the uranium occurs as diffuse concentrations, too fine to be resolved by scanning electron microscopy (SEM), and disseminated evenly throughout the organic rich sediments. The major zone of uranium accumulation within the deposit occurs as a sub-horizontal planar body that is strongly correlated with both the unpressurized groundwater surface and fine textured, carbonaceous sediments such as lignites and lignitic clays. It is theorised that uranium (and other base metals within the deposit) were transported laterally from source materials in oxidized form by acidic, meteoric flow. The metals were then concentrated and eventually fixed (reduced) in the anoxic, capillary fringe at the surface of the water table. Uranium reduction and fixation (U^{6+} to U^{4+}) is thought to be largely biogenic (enzymatically catalysed reduction by U-bacteria). The anoxic (reduced) capillary fringe is much thicker in fine textured sediments (such as lignites) than in coarser textured sediments such as carbonaceous sands. As such, most uranium accumulation in the MRP is similarly correlated with organic-matter rich materials at the water table surface. Uranium accumulation does occur at the water table surface in medium to coarse sands, but is generally too thin to be of commercial value. More redox active metals (such as Cu, Ni and Zn) tend to

¹ Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves, The JORC Code 2012 Edition. Effective 20 December 2012 and mandatory from 1 December 2013. Prepared by the Joint Ore Reserves Committee of the Australasian Institute of Mining and Metallurgy, Australasian Institute of Geoscientists and Minerals Council of Australia (JORC).

reduce and fix at redox interfaces below the water table surface. Mineralisation, therefore, is controlled by the lithological and geochemical properties of the sediments rather than by stratigraphy. Suitable lithological and geochemical environments for significant metal accumulation occur in both remnant carbonaceous Cretaceous sediments and Eocene palaeochannel sediments.

Eocene palaeochannel sediments primarily host the mineralisation in the deposit. Uranium mineralisation commences at depths ranging typically between 30 m and 50 m at Ambassador, reflecting the combination of a slight dip to the mineralised surface and the topography of the area.

Vimy is responsible for the drillhole database and geology used in the Mineral Resource, with data compiled in a Datashed database system.

The Ambassador Mineral Resource for the portion that was infill drilled in Q4 2016, shown in Figure I, contains a total of 643 drillholes (totalling 37.1 km of drilling) of which 446 holes contained either radiometric or assay data.

The holes comprise a mixture of data including:

- Recent radiometric probe data primarily from aircore (AC) and reverse circulation (RC) holes.
- Historical and recent chemical assay data primarily from diamond core holes (DC).
- Some historical radiometric data for PNC drillholes.

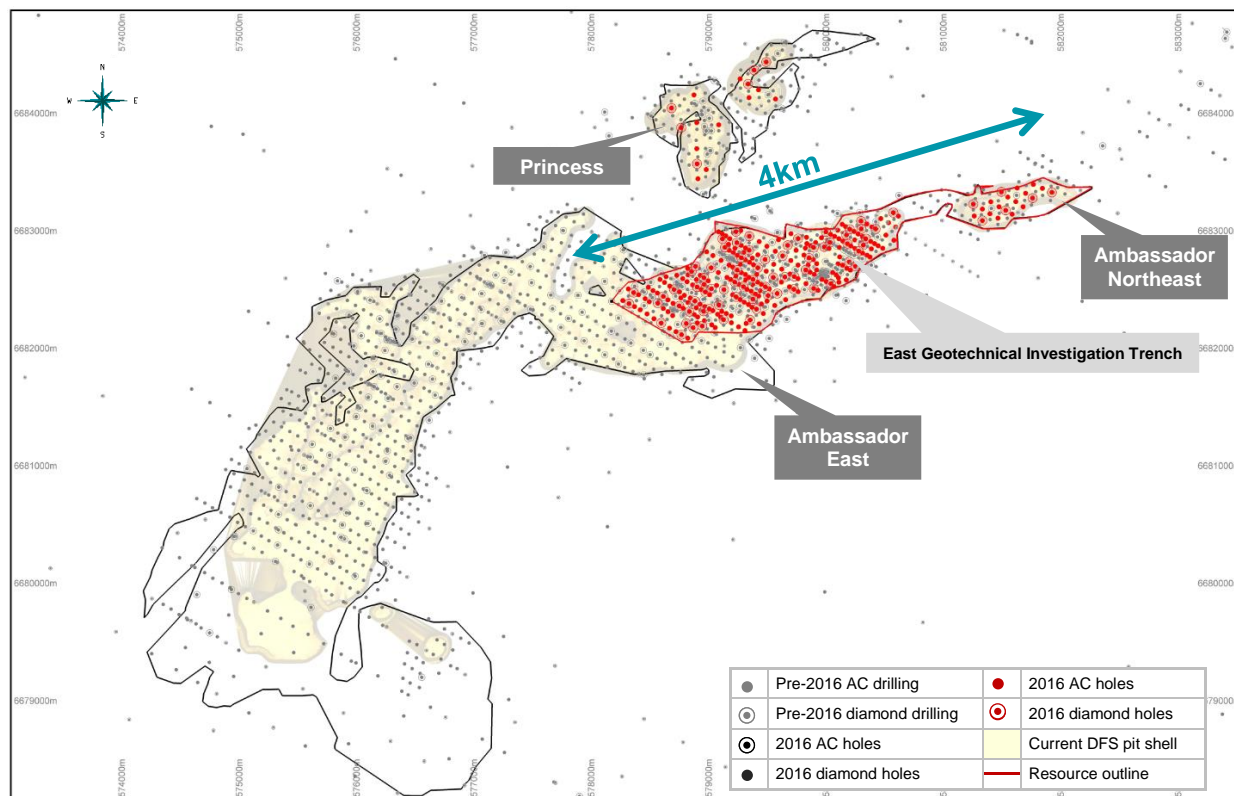
The drillholes within the infilled portion of the Ambassador deposit reported here comprise:

- 418 AC holes (25,213 m total).
- 200 DC holes (10,316 m total).
- 22 RC holes (1,417 m total).
- 3 Sonic holes (161 m total).

Drillholes that were omitted for use in resource estimation tended to lack critical radiometric and/or assay data.

The mineralised zones were defined by interpretation of stratigraphy, geology, and anomalous grades. Using geology and stratigraphic positions, the uranium mineralised zones were defined using a $eU_3O_8 > 100$ ppm cut-off grade (prior to disequilibrium correction, for percussion drilling) and/or chemical $U_3O_8 > 100$ ppm cut-off grade (for diamond drilling). A minimum thickness of 0.5 m and maximum 1 m internal dilution was allowed for in definition of the mineralisation domains. This protocol defined multiple stacked mineralised zones, with the majority of the metal contained in Domain 100 zone, being the most laterally extensive and highest in grade. A schematic long section and cross section of the Domain 100 mineralisation are shown in Figures II and III. The mineralised zones were further refined and constrained by the use of sub-domains related to geology and palaeochannel controls and limits on the uranium mineralisation. Ambassador East sub-domains are shown in Figures IV and V. This is a significant improvement on previous models.

Figure I Drillhole locations and type as of May 2017



In order to address potential disequilibrium and sample quality issues, a large number of diamond drillholes and corresponding AC twin drillholes were drilled in the Ambassador deposit. Detailed studies were completed to assess the following aspects:

- Gamma-derived eU_3O_8 between the DC and AC holes. Outcomes were as follows:
 - Global statistical calculations confirmed earlier studies that the gamma-derived eU_3O_8 from the twin DC and AC holes were comparable despite possible variations in drill hole diameters, casing, hole condition etc. Minor variations between twin holes are noted, but are assumed to be caused by short range geological variability—those assumptions were substantiated by other test work.
- Chemical assay-derived U_3O_8 between the DC and AC holes. Outcomes were as follows:
 - Samples derived from the DC holes are typically of good quality.
 - The effects of sample smearing and non-selective interval dilution in the 2016 study are apparent within a number of the AC holes, although there are also examples where this effect is either minimal or absent.
 - As a result, U_3O_8 values derived from AC holes are likely to be biased low in terms of grade and biased high in terms of interval width.
 - For the purposes of resource estimation, gamma-derived factored eU_3O_8 (referred to as eU_3O_8d when corrected for disequilibrium) should be used in preference to U_3O_8 assays for the AC holes. This would also apply to other drilling techniques such as RC and rotary mud, where the likelihood of sample smearing and/or sample contamination is possibly high.

Figure II Ambassador Mineral Resource – Schematic long section – vertical exaggeration 8x

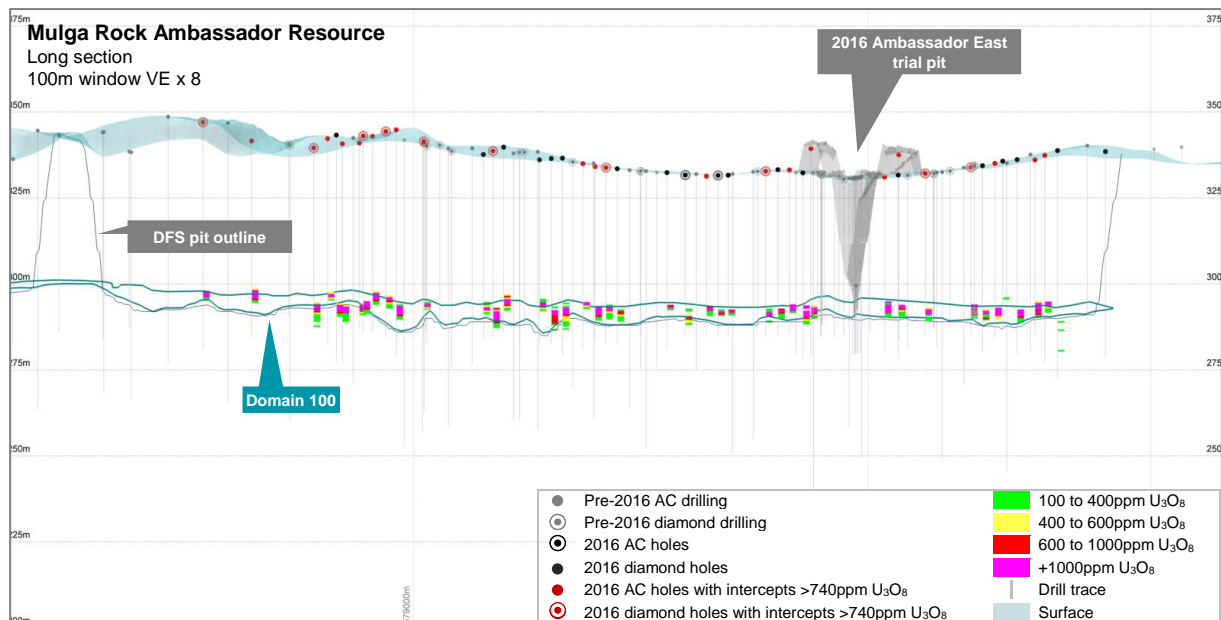


Figure III Ambassador Mineral Resource – Schematic cross section – vertical exaggeration 8x

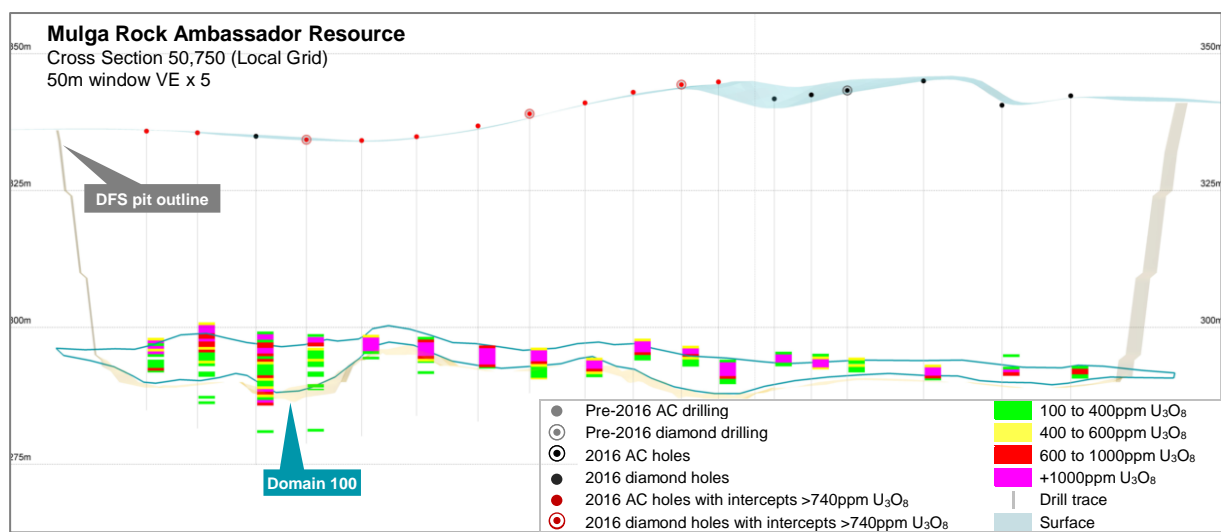


Figure IV Ambassador East domain 100 sub-domains.

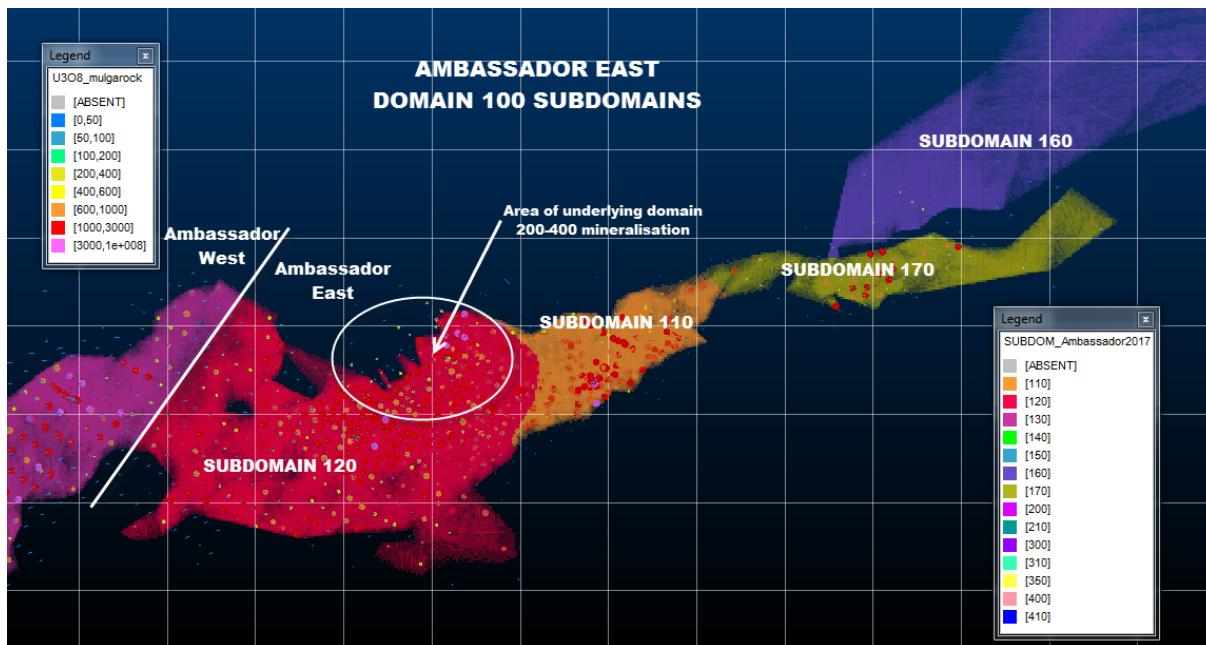
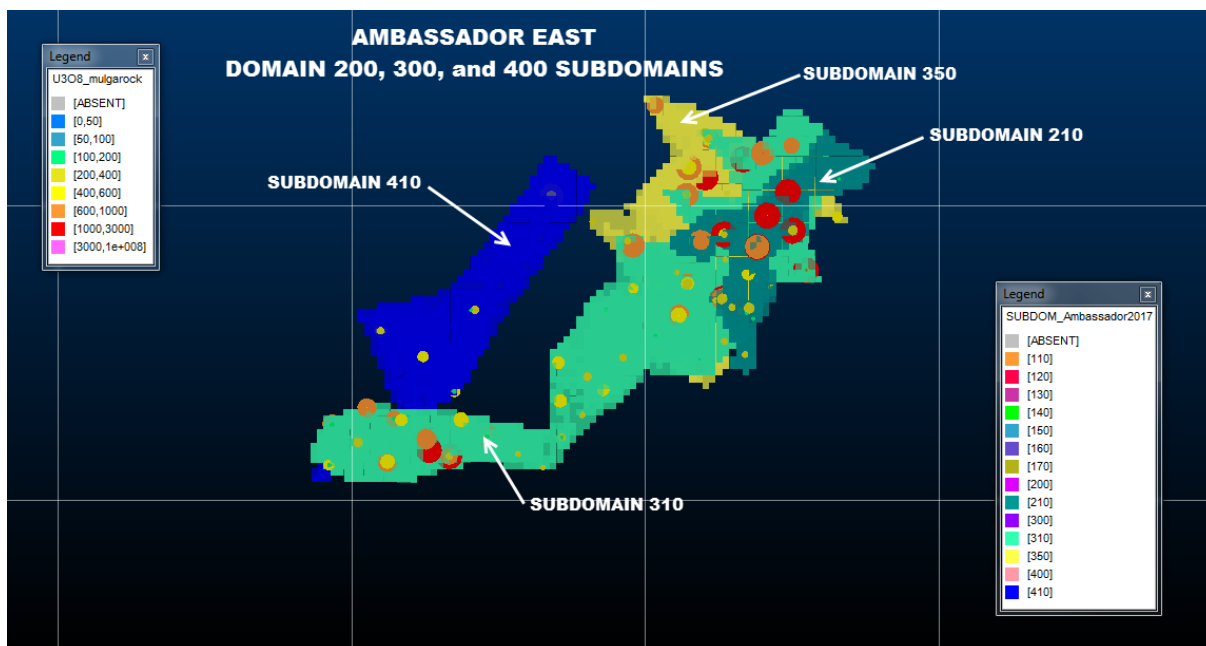


Figure V Ambassador East domain 200-400 sub-domains.



The net conclusions from the twin hole study—as it affects the data used for the Mineral Resource—are as follows:

- AC eU₃O₈ data (corrected for disequilibrium) should be used in preference to the AC chemical assay U₃O₈ data due to sample quality/potential smearing issues where possible.
- Chemical U₃O₈ data should be used from the DC holes where possible.

- As radiometric data is comparable between DC and AC twin holes, the disequilibrium corrections derived from DC eU_3O_8/U_3O_8 sample interval pairs are valid to be extrapolated from the DC holes to the AC holes.

As is normal for most young uranium deposits, the radiometric equivalent U_3O_8 (eU_3O_8) grades require adjustment for radiometric disequilibrium. This was achieved by using regression equations derived from the comparison of paired assay results with composited radiometric logging from the various phases of DC drilling. In the majority of cases at Ambassador, the radiometric eU_3O_8 grades for similar intervals are lower than the corresponding chemical assays for U_3O_8 , requiring general positive adjustments to the radiometric data to emulate the accurate chemical assay data. To obtain a robust global estimate of the disequilibrium, each of the uranium domains was first split into groups (based on the data type/vintage/domain/subdomain) and then further split into distinct grade bins. These grade bins were determined based on apparent “natural breaks” in the dataset identified in both the statistics and Q-Q plots. Specifically, disequilibrium corrections (regression formulae for the Q-Q data) were derived for the infilled portion of Ambassador East based on the 0.5 m downhole composite data and within the mineralised domains and sub-domains:

- Domain 100 (sub-domains 110, 120, and 170) for:
 - PNC data where eU_3O_8 data was derived from digitized logs.
 - PNC data where eU_3O_8 data from recent wireline logs was derived from digitized logs.
 - Vimy data from holes drilled up to and including 2015.
 - Vimy data from holes drilled after 2015.
- Domain 200, 300, and 400 (sub-domains 210, 310, 350, and 410 respectively) combined Vimy data from holes drilled between 2014 and 2016 due to limited data.

Any radiometric data below the lower disequilibrium grade range for the Vimy and PNC data within the uranium domains were not corrected, as the material was considered to be internal dilution, and the corrections applied within that grade range were likely to be both minimal and inaccurate. The disequilibrium adjustments were validated by the sub-domains. When compared to the raw eU_3O_8 dataset, the disequilibrium corrected data (eU_3O_8d) is statistically similar to the assay-derived U_3O_8 data.

All data was composited to 0.5 m downhole intervals within the mineralised domains and sub-domains. For Domains 100 and 200 at Ambassador, which are essentially relatively thin and flat-lying zones, the 0.5 m U_3O_8 composite data (plus any residuals) was also re-composited to the full vertical width of the domains such that a single composite of variable width represents each drillhole. The full width composites were used for parallel accumulation type estimates.

The full block model dimensions at Ambassador cover a region of roughly 9 km x 1 km. The Ambassador East infilled area reported here covers a region of approximately 4 km long and up to 900 m wide. Parent block dimensions for the Ambassador block model are 50 mE x 50 mN x 1 mRL with sub-celling down to 10 mE x 10 mN x 0.25 mRL. Estimation for this Ambassador East update utilizes Ordinary Kriging (OK) and the 0.5 m composite data.

Bulk density data (wet, dry, and moisture) was based upon an analysis of immersion bulk density data, wireline density logs for DC holes, and ultimately a hybrid data set coded for the key lithologies (basement, carbonaceous clay, claystone, conglomerate, carbonaceous sandstone, laterite, lignitic clay, sandstone, and siltstone). Use of the wireline density data in conjunction with the Archimedean methods generated a comprehensive data set across the range of lithologies for use in modelling without some of the biases related to selection of competent units of core for weight/volume measurements. Dry bulk density values range from $0.74t/m^3$ (for lignite-lignitic clay) to $1.55 t/m^3$ (sandstone) in the range of material associated with the uranium mineralisation, excluding basement material ($1.91 t/m^3$). Bulk densities were estimated directly into the block models for the domains and sub-domains using Inverse Distance (Power=1) method, with block densities reflecting the fractions of the main lithologies

discussed above, each assigned a specific moisture and wet but density. Average bulk densities and moistures for the classified portions of the Ambassador domains are given in Table I.

Table I Average density and moisture values for the classified portions of the uranium mineralisation domains within the infill drilled area of Ambassador East

Deposit	Sub-domain	Bulk density dry (t/m ³)	Moisture (% of dry BD)	Bulk density wet (t/m ³)
Ambassador	110	1.11	41.1	1.51
	210	1.30	30.6	1.64
	310/350	1.46	27	1.81
	410	1.20	37	1.61

Note: Appropriate rounding has been applied.

Redox boundary, water table, and stratigraphy were flagged in the block model based on interpreted wireframe surfaces provided by Vimy geologists.

The Mineral Resource has been reported in accordance with the guidelines as set out in the JORC Code. The resource estimate has been classified as a combination of Measured, Indicated and Inferred Resource based on the confidence of the input data, drillhole spacing, geological interpretation, and grade estimation. The resource classification assumes exploitation by conventional open cut mining methods.

The Mineral Resource in Table II is a subset of the Ambassador deposit for the Ambassador East area of infill drilling only, reported using a lower cut-off grade of 150ppm U₃O₈. The model used cut U₃O₈ 0.5m composite data (combined chemical and disequilibrium corrected radiometric grades) and ordinary kriging as the estimation method.

Table II Mineral Resource by uranium domain, May 2017 – Ambassador East area reported at 150ppm U₃O₈ lower cut-off grade

May 2017 Mineral Resource— Ambassador East area of infill drilling												
Uranium Domain	Resource Classification									Total		
	Measured			Indicated			Inferred					
	Tonnage (Mt)	U ₃ O ₈ (ppm)	Metal (Mlb)	Tonnage (Mt)	U ₃ O ₈ (ppm)	Metal (Mlb)	Tonnage (Mt)	U ₃ O ₈ (ppm)	Metal (Mlb)	Tonnage (Mt)	U ₃ O ₈ (ppm)	Metal (Mlb)
100	5.1	1,105	12.4	0.5	720	0.7	0.1	450	0.1	5.7	1060	13.3
200				0.1	540	0.1				0.1	540	0.1
300							0.9	350	0.7	0.9	350	0.7
400							0.01	200	0.01	0.01	200	0.01
Total	5.1	1,105	12.4	0.6	685	0.8	1.1	360	0.9	6.7	950	14.1

The Mineral Resource in Table III combines the updated Ambassador East area of infill drilling with the remainder of the 2016 Ambassador model, and is also reported using a lower cut-off grade of 150ppm U₃O₈. The model uses a combination of accumulation (via ordinary kriging) and ordinary kriging as the estimation methods.

Table III Mineral Resource by uranium domain, May 2017 – total Ambassador area incorporating the infill area in Table II, reported at 150ppm U₃O₈ lower cut-off grade

May 2017 Ambassador Mineral Resource—Ambassador total inclusive of the 2016 infill area shown in Table 2												
Uranium Domain	Resource Classification									Total		
	Measured			Indicated			Inferred					
	Tonnage (Mt)	U ₃ O ₈ (ppm)	Metal (Mlb)	Tonnage (Mt)	U ₃ O ₈ (ppm)	Metal (Mlb)	Tonnage (Mt)	U ₃ O ₈ (ppm)	Metal (Mlb)	Tonnage (Mt)	U ₃ O ₈ (ppm)	Metal (Mlb)
100	5.1	1,105	12.4	9.9	760	16.5	5.4	375	4.5	20.3	740	33.4
200				4.2	400	3.7	0.4	300	0.3	4.6	390	3.9
300							4.7	310	3.3	4.7	310	3.3
400							0.8	205	0.4	0.8	205	0.4
Total	5.1	1,105	12.4	14.0	655	20.1	11.3	335	8.3	30.4	610	40.9

Footnotes for Tables II and III:

- Appropriate rounding has been applied in the tables above, sums may vary slightly.
- The current MRP Ambassador resource drilling database comprises 1764 drillholes. Of these, 357 were diamond holes, 143 were RC, 1249 were AC, 10 were geotechnical holes and five were sonic holes. The infilled portion of Ambassador East reported here contains 643 drillholes. Of these, 418 were AC holes, 200 diamond holes and 22 RC holes and three sonic holes.
- Hole types are a mix of diamond core, RC and air core holes. Due to concerns regarding sample collection quality and recovery, the use of AC chemical assays in the 2017 resource estimate is very limited. Radiometric eU₃O₈ data adjusted for disequilibrium is used in preference for the AC type holes.
- 2008-2016 Vimy and historical PNC chemical data and radiometric data were used in the 2017 resource estimate of U₃O₈.
- AMC note that the quality of the PNC assay data ranges from moderate to good, with many of the diamond drillholes chemical assays having been sourced from hard-copy laboratory certificates. However, it also noted that there is a lack of QA/QC data regarding standards and blanks in particular, as well as little information being available regarding exact laboratory analytical procedures. The laboratories used were well regarded at the time and the use of XRF and ICP-MS for uranium analysis is an industry standard process.
- QA/QC of Vimy assay samples since 2008 are of current industry standard and outlined in the JORC Code 2012 Table 1 Section 1. Field duplicates, standards, and blanks were routinely submitted.
- Radiometric logging of the PNC and Vimy drillholes was conducted. Appropriate post-processing was completed on the data for conversion to a standardized eU₃O₈ value for all drillholes.
- In the majority cases at Ambassador, the radiometric eU₃O₈ grades for similar intervals are lower than the corresponding chemical assays for U₃O₈, requiring positive adjustments to the radiometric data to emulate the accurate chemical assay data. Data was analysed for each of the four uranium domains and sub-domains, splitting the data into groups (based on the data type/vintage) and then distinct grade bins as required. These grade bins were determined based on apparent natural breaks in the dataset identified in Q-Q plots and statistics. Specifically, disequilibrium corrections (regression formulae for the Q-Q data) were derived for:
 - Domain 100 (sub-domains 110, 120, and 170) for:
 - PNC data where eU₃O₈ data was derived from digitized logs.
 - PNC data where eU₃O₈ data from recent wireline logs was derived from digitized logs.
 - Vimy data from holes drilled up to and including 2015.
 - Vimy data from holes drilled after 2015.
 - Domain 200, 300, 350 and 400 each combined Vimy data from holes drilled between 2014 and 2016 due to insufficient data.
 - Any radiometric data below the lowest disequilibrium grade bin within the uranium domains were not corrected.
- As the assay database consists of both chemical U₃O₈ data and radiometric eU₃O₈ data, the combined dataset is used with priority given to chemical assay data from the diamond drillholes; otherwise the corrected radiometric data was used.
- Statistical analyses were completed on the raw sample data and the 0.5 m composite data. High-grade cuts were applied as follows:
 - Sub-domain 110 – 11,000 ppm U₃O₈.
 - Sub-domain 120 – 9,700 ppm U₃O₈.
 - Sub-domain 170 – 3,000 ppm U₃O₈.
 - Sub-domain 210 – 1,700 ppm U₃O₈.
 - Sub-domain 310 – 1,600 ppm U₃O₈.
 - Sub-domain 350 – 1,100 ppm U₃O₈.
 - Sub-domain 410 – no top-cut applied due to consistent low-grade and no outliers.
- Grade variability was generated for the grade estimation by OK. The Ambassador East directional variography was moderately well-

structured for Domain 100 and 200 (and associated sub-domains), and weakly structured for Domains 300 and 400

- Parent blocks of size 50 m (X) x 50 m (Y) x 1 m (Z) with sub-blocks of size 10 m x 10 m x 0.25 m were used to construct the mineralised domains of the estimate. The block XY dimensions are approximately half of the nominal drill spacing.
- The X and Y coordinates correspond to UTM Northing and Easting (Grid GDA94 Zone 51) respectively and Z corresponds to Australian Height Datum.
- Grade estimates were generated by ordinary kriging for all sub-domains, using the sub-domains as hard boundaries. Appropriately cut and composited data were used.
- Bulk density values were derived from analysis of Archimedean data and selective use of corrected gamma probe data as documented by Vimy. Lithology dry bulk densities range from 0.74 t/m³ for lignitic clay material to 1.91 t/m³ for basement material. The uranium domains contained a mix of lithology types, and the domain average densities and spatial variations present in the model reflect that.
- Bulk density data (dry bulk density, wet bulk density, and moisture) were assigned to the simplified lithologies associated with the 0.5 m composite data and estimated directly in the block model.
- The grade estimates for all zones have been classified as Measured, Indicated and Inferred in accordance the JORC Code 2012 guidelines based on the confidence levels of the key criteria that were considered during the resource estimation.
- The reporting block cut-off grade of 150 ppm U₃O₈ currently reflects an expected open pit mining scenario reliant on mechanized strip mining equipment to allow bulk removal of overburden. Feasibility Study level mining studies are currently in progress.

JORC Code, 2012 Edition – Table 1 Ambassador Mineral Resource Estimate, May 2017

Material discussed in Sections 1 and 2 below refer to Q4 2016 drilling. Previous drilling has been addressed in past releases to the ASX.

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> <i>Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i> <i>Include reference to measures taken to ensure sample representativity and the appropriate calibration of any measurement tools or systems used.</i> <i>Aspects of the determination of mineralisation that are Material to the Public Report.</i> <i>In cases where ‘industry standard’ work has been done this would be relatively simple (e.g. ‘reverse circulation drilling was used to obtain 1 m samples from which 3kg was pulverised to produce a 30g charge for fire assay’). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.</i> 	<ul style="list-style-type: none"> Reverse circulation air core (AC) samples were recovered directly from a cyclone and riffle splitter. If wet, the drill cuttings were allowed to dry in the bags before collection. Samples were taken at 0.5m metre intervals from within the uranium mineralised zone and at 1m intervals outside it. The mineralised zone is defined by geology, proximity to the weathering front, and radiometrics. Whole core was sampled from the diamond drill holes to ensure maximum sample size. Due to the rheology of the mineralised zones, the core was vacuum packed at the rig, which also allowed for on-site bulk density measurement on site by immersion. Downhole logging of natural gamma was used to determine the U₃O₈ grade, using gamma probes calibrated for uranium in September 2016 at the South Australian Government’s Department of Water, Land and Biodiversity Conservation calibration facility (test pits and related facilities) in the Adelaide suburb of Frewville. Wireline density probes used to measure in-situ bulk density were also calibrated at the same facility. Daily calibrations on the gamma tools were carried out using a Cs¹³⁷ jig, and additional calibrations done using a calibration bore at Mulga Rock during the drilling program. The following wireline logging tools were run in aircore and diamond drill holes: <ul style="list-style-type: none"> Natural gamma Dual spaced focused resistivity Magnetic deviation Dual spaced induction (conductivity) Single arm calliper Triple-spaced density (using a Cs¹³⁷ source)

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> A dual neutron porosity was used in diamond drill holes, reliant on an Am²⁴¹-Be source. Wireline logs were recorded in open hole configuration, with drilling mud in diamond holes, and post-drilling conditioning with mud for aircore holes.
Drilling techniques	<ul style="list-style-type: none"> Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc). 	<ul style="list-style-type: none"> The drilling program at Ambassador East, North and Princess comprised both aircore and diamond core techniques. A range of aircore drill bits was used due to a wide range of rock hardness, ranging from tungsten carbide blades arranged around an opening in the face of the bit to bits fitted with PCD buttons. The diamond drilling was completed using triple tube, which comprises outer PQ3 diameter (~122mm) drill rods. Core is not oriented as all holes are vertical and the mineralisation is not structurally complex.
Drill sample recovery	<ul style="list-style-type: none"> Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material. 	<ul style="list-style-type: none"> Sample flow from the cyclone was continually monitored during aircore drilling, ensuring high sampling standards. Diamond core loss was recorded as part of logging. Overall core recovery greater than 91%, and 94% within the mineralised zones, with losses occurring primarily in loose sands which, where collected, are sub-economic. Evaluation of gamma log equivalent U₃O₈ grade in areas of core loss allowed the grade bias due to core loss to be assessed on a hole by hole basis.
Logging	<ul style="list-style-type: none"> Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. The total length and percentage of the relevant intersections logged. 	<ul style="list-style-type: none"> Lithological logging of drill samples was carried out to record main lithological, sedimentological, weathering, colour, and reduction-oxidation (redox) features. Stratigraphy is also tentatively assigned while drilling and revised following analysis of wireline data. The stratigraphic boundaries determined from graphic logs and associated cross-sections were used to model deposit geology. Diamond core was logged and photographed before vacuum packing.
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. 	<p>Site Based Work</p> <ul style="list-style-type: none"> Selection of sample composites for chemical analysis was based on current interpretations of mineralised domains for the drill core and adjusted as necessary based on downhole wireline radiometric data. Sample length for

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all sub-sampling stages to maximise representativity of samples. Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. Whether sample sizes are appropriate to the grain size of the material being sampled. 	<p>drill core is nominally 0.5m, but intervals were modified to align with lithological boundaries. Sample length for aircore was 0.5m.</p> <ul style="list-style-type: none"> After drying, the aircore bagged samples over the mineralised zone were weighed then split using a single tier riffle splitter. Duplicates were also taken from the original sample via the riffle splitter. Samples were dispatched and transported in accordance with the Company's Radiation Management Plan. <p>Laboratory Based Work</p> <ul style="list-style-type: none"> Following sorting, weighing and drying at the laboratory, aircore samples were crushed to 3mm, split to produce a 2.2kg fraction and pulverised to 90% passing 75 microns. Moisture content was determined from all vacuum-packed drill core samples, with repeat bulk density measurements by immersion carried out for about 20% of samples. A small mass of the pulverised sample was then split for assay, with the coarse fraction and pulverised residue preserved. Samples from the main mineralised interval were submitted and analysed for uranium and a range of trace and major elements via fused bead laser ablation and XRF, using a combination of atomic emission spectroscopy (ICP-AES) and mass spectroscopy (ICP-MS). The sample was fused with a 12:22 lithium borate flux including 5% LiNO₃.
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established. 	<p>QA/QC of Assay Samples</p> <ul style="list-style-type: none"> A comprehensive QA/QC program was carried out, comprising the use of in-house and external standards, blank, field and laboratory duplicates, and external pulp duplicates (umpire assays). Barren flushes were also inserted between samples at the laboratory on a 1:30 ratio. The in-house standards were manufactured and certified by Geostats Pty Ltd in 2010 using Mulga Rock composites generated from 2009 drill cuttings (matrix matched). Other matrix-matched standards were also used. A 1:17 ratio for standards and 1:20 duplicates were included in the samples despatched, while the laboratory also used in-house standards and performed repeats. Field duplicates for aircore samples were selected based on down-hole gamma and lithology data and collected in the same manner as the original sample. Due to the full sampling of the drill core, 1:20 pseudo-duplicates were collected at the primary crushing stage (10mm) at the laboratory.

Criteria	JORC Code explanation	Commentary
Discussion of relative accuracy/ confidence		<ul style="list-style-type: none"> Past diamond-diamond and diamond-aircore twin holes have been completed in previous years and demonstrated very high levels of confidence in the data collected, notwithstanding short-range geological variability inherent to the host-rocks and supergene nature of the deposit.
Portable XRF Logging		<ul style="list-style-type: none"> All drill cuttings were analysed by portable XRF through ~50-micron plastic bags on site to guide future drilling and for additional sampling purposes. The portable XRF data is not used directly for any purpose other than determining mineralised zones for sampling, and grade variability. Portable XRF data is not used during Mineral Resource estimation.
Verification of sampling and assaying	<ul style="list-style-type: none"> The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes. Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. Discuss any adjustment to assay data. 	<ul style="list-style-type: none"> The depth of down-hole gamma data was checked for discrepancy between the recorded total hole depth and the maximum depth of gamma logging. The difference was less than 1m on average. Correlation of core assay data and probe derived equivalent U_3O_8 grade is used to determine a radiometric disequilibrium correction.
Location of data points	<ul style="list-style-type: none"> Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. Specification of the grid system used. Quality and adequacy of topographic control. 	<ul style="list-style-type: none"> All drill holes were surveyed using a Differential Global Positioning System in Real-Time Kinematics (RTK) mode, with a sub-decimetre horizontal resolution. The MGA94, zone 51 grid system was used. Azimuth and inclination data from wireline tools were used in to calculate the deviation of each drill hole.
Data spacing and distribution	<ul style="list-style-type: none"> Data spacing for reporting of Exploration Results. Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. Whether sample compositing has been applied. 	<ul style="list-style-type: none"> Drill spacing at Ambassador East and Northeast ranges between 50 x 80m and 50 x 40m along WNW-ESE trending traverses, with drill spacing of 100 x 80m at Princess. Data spacing is sufficient for the methods used and resource classification. Sample compositing is not done during drilling and sampling.
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material. 	<ul style="list-style-type: none"> Drilling has adequately tested the tabular nature of the mineralisation at Ambassador. However, steeply-dipping structures may have some control on uranium mineralisation in sands underlying the upper mineralised. These may require angled drilling for full evaluation. However, these zones are minor and the economics of the mineralisation is not materially affected.

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> Aircore and diamond were consistently drilled at least 6m past the base of uranium mineralisation to allow for effective wireline logging of mineralised intervals.
Sample security	<ul style="list-style-type: none"> <i>The measures taken to ensure sample security.</i> 	<ul style="list-style-type: none"> Aircore samples were sealed in drums and transported by a transport contractor from Kalgoorlie to the assay laboratory, with full chain of custody maintained throughout transport. Vacuum packed diamond cores were transported in core trays to the laboratory in a similar fashion.
Audits or reviews	<ul style="list-style-type: none"> <i>The results of any audits or reviews of sampling techniques and data.</i> 	<ul style="list-style-type: none"> AMC Consultants conducted an audit of drilling and sampling processes in November 2016, confirming the appropriateness and robustness of the procedures described above. Golder carried out an independent review of the sensitivity of data input, processing and resource estimation in the second half of 2016 and found the estimation process to be robust. That review also supported more localised factoring of radiometric disequilibrium.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> <i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i> <i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</i> 	<ul style="list-style-type: none"> The Ambassador and Princess Deposits are located about 240 km ENE of Kalgoorlie within Mining Lease M39/1104, held by Narnoo Mining Pty Ltd, a wholly owned subsidiary of Vimy Resources Limited (Vimy). Mining Lease M39/1104 is located on Vacant Crown Land and is not subject to a native title claim.
Exploration done by other parties	<ul style="list-style-type: none"> <i>Acknowledgement and appraisal of exploration by other parties.</i> 	<ul style="list-style-type: none"> The area of the Ambassador Deposit was subject to uranium exploration by PNC Exploration Australia Pty Ltd (PNC) during the 1980's, which resulted in the discovery of the Mulga Rock Deposits. The bulk of PNC's exploration effort was focused on the Ambassador and the eastern side of the Mulga Rock Project between 1982 and 1985.

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> • A trial mining program took place within the Shogun deposit in late 1983 to obtain a bulk sample of mineralised lignite. • During 2008 and 2009, Vimy, then known as Energy and Minerals Australia Ltd (ASX: EMA) carried out a twin drill hole program followed by an extensive infill drilling and sampling program, with statistics as follows: <ul style="list-style-type: none"> ○ 417 aircore drill holes for 27,144m ○ 27 diamond drill holes for 1,693m ○ 5 sonic drill holes for 306m. • During 2014, Vimy carried a further twin and resource drill-out program (primarily at Ambassador East, with some diamond tails drilled at Princess), as follows: <ul style="list-style-type: none"> ○ 144 aircore drill holes for a total of 9,461m ○ 42 diamond drill holes for 2,589m • In 2015, Vimy carried out an additional infill drill-out program, primarily focused on Ambassador West, for the following totals: <ul style="list-style-type: none"> ○ 1035 aircore drill holes for 64,425m ○ 144 reverse circulation drill holes for 9,881m • In late 2015-2016, Vimy completed two trial pits at Ambassador East and West to support open pit, geotechnical and metallurgical studies. Approximately 150 t of ore sample were collected for further analysis and pilot plant studies. • Reconciliation against the resource block model revealed that the bulk sample contained 53% more metal than the resource model predicted (See ASX announcement dated 14 June 2016). • In late 2016, Vimy completed an optimisation drilling program, which is the subject of this update, focused primarily on Ambassador East, as follows: <ul style="list-style-type: none"> ○ 215 aircore drill holes for 11,700m ○ 84 diamond drill holes for 4,333m
Geology	<ul style="list-style-type: none"> • <i>Deposit type, geological setting and style of mineralisation.</i> 	<ul style="list-style-type: none"> • Ambassador is a sediment-hosted, supergene-enriched uranium deposit. The mineralisation that comprises the Ambassador resource is hosted by reduced Late Eocene sediments preserved within the Narnoo Basin. The Narnoo Basin Sequence consists of a multiple fining upwards packages including sandstone, claystone (typically carbonaceous) and lignite which were deposited in alluvial and lacustrine environments. The mineralisation is hosted by reduced sediments of Eocene age preserved within a complex set of sedimentary troughs overlying an extensive long-lived paleodrainage

Criteria	JORC Code explanation	Commentary
		<p>referred to as the Mulga Rock paleochannel, itself likely to represent a dead arm of the Lake Reside regional paleodrainage.</p> <ul style="list-style-type: none"> Overlying the reduced Narnoo Basin sediments is a succession of oxidised sediments which at Ambassador are about 25 to 55m thick. Pre-Eocene basement in the Ambassador area consists of both Cretaceous and Carboniferous sedimentary successions, as well as Paleoproterozoic metasediments to the east of the Gunbarrel fault.
Drill hole Information	<ul style="list-style-type: none"> A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length. If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case. 	<ul style="list-style-type: none"> All relevant drill hole collar data pertaining to this release is provided in the table attached to this announcement. The dip and azimuth of all drill holes is vertical.
Data aggregation methods	<ul style="list-style-type: none"> In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated. 	<ul style="list-style-type: none"> For the purpose of this announcement, the minimum intercept used was 0.5m or greater above 100ppm U_3O_8 (0.01% U_3O_8), with a zero waste length (grades lower than 100ppm U_3O_8). The value of 100ppm represents a natural break in the assay data.

Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	<ul style="list-style-type: none"> These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known'). 	<ul style="list-style-type: none"> Mineralisation is tabular and horizontal and related to un-pressurised groundwater flow. The vertical drill hole intersections represent true mineralisation thickness.
Diagrams	<ul style="list-style-type: none"> Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views. 	<ul style="list-style-type: none"> Two representative sections and a plan view of all drill collars are provided in the main text.
Balanced reporting	<ul style="list-style-type: none"> Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results. 	<ul style="list-style-type: none"> Balanced reporting has been achieved through a comprehensive reporting of sampling and analytical processes followed and complete disclosure of all intercepts.
Other substantive exploration data	<ul style="list-style-type: none"> Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances. 	<ul style="list-style-type: none"> Laboratory checks of field derived bulk densities validated the process followed and further validation is underway using long-spaced density data from wireline data.
Further work	<ul style="list-style-type: none"> The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive. 	<ul style="list-style-type: none"> Additional analysis is underway to: <ul style="list-style-type: none"> Refine the definition of base metal domains. Expand a conditional simulation model to the entire Ambassador, Princess and Shogun Mineral Resources, which collectively form the current MRP Ore Reserve.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

Criteria	JORC Code explanation	Commentary
Database integrity	<ul style="list-style-type: none"> Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. Data validation procedures used. 	<ul style="list-style-type: none"> The resource estimation was based on both the available historical exploration and more recent drill hole database. Vimy manages exploration data in a Datashed database system. Vimy has assumed responsibility for the validity of the drill hole data and geology. The database was reviewed, and validation checks completed prior to commencing the resource estimation study. Changes that were made to the database before loading into mining software included: <ul style="list-style-type: none"> Replacing less than detection samples with a value equal to half the detection level Identifying intervals with no samples/assays/radiometric data and setting appropriate bespoke priorities for those intervals. The deconvolved radiometric eU_3O_8 grades (before disequilibrium factoring) were composited to 0.5m intervals in conjunction with the assay data to make processing, comparison and modelling more efficient. The radiometric data suite allowed for cross-checking of both assay data, geology, and density. A final table of ranked assays data was used for the resource estimation with priority placed on: <ul style="list-style-type: none"> Diamond drilling with chemical data, then Disequilibrium factored radiometric grades.
Site visits	<ul style="list-style-type: none"> Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is the case. 	<ul style="list-style-type: none"> Ingvar Kirchner (Coffey Mining; now AMC Consultants) visited site in November 2014 and November 2016, while Ellen Maidens, Vimy Resource estimation geologist visited site in November 2015 and November 2016. Several other people employed by Coffey Mining visited site during 2012 and 2010. Xavier Moreau undertook multiple site visits during the 2014, 2015 and 2016 drilling programmes and during the sampling phase.
Geological interpretation	<ul style="list-style-type: none"> Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. Nature of the data used and of any assumptions made. The effect, if any, of alternative interpretations on Mineral Resource estimation. 	<ul style="list-style-type: none"> Geology (lithology) was not modelled, but was used in defining the mineralised zones. Stratigraphy was modelled and influences the limits of the interpreted mineralised zones.

Criteria	JORC Code explanation	Commentary																				
	<ul style="list-style-type: none"><i>The use of geology in guiding and controlling Mineral Resource estimation.</i><i>The factors affecting continuity both of grade and geology.</i>	<ul style="list-style-type: none">Diamond drilling has improved the geological understanding of the deposit. Previously the interpretation was complicated by the overprint of oxidation/lithology and stratigraphy. A simplified stratigraphic interpretation has been completed and is the basis for mineralised domain definition.The deposit grades are very closely associated with the reduction-oxidation front and are highest close to this sub-horizontal boundary.For the purpose of the resource estimation, the mineralisation boundaries were based on a nominal 100ppm U₃O₈ lower cut-off grade, defining a mineralised zone of at least 0.5m thickness and honouring, where possible, the geology/stratigraphy. This value was chosen as it represents a natural break in the distribution of grades distinguishing mineralisation from un-mineralised material. Four uranium mineralised zones were defined for the Ambassador deposit defining progressively deeper and lower grade mineralisation—Domains 100, 200, 300, and 400. The domains were subdivided into a number of key sub-domains based on geology, palaeochannel profile and tenor of mineralisation for estimation purposes.																				
Dimensions	<ul style="list-style-type: none"><i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i>	<ul style="list-style-type: none">The block model is not rotated.The block model extents are tabulated below:<table><tr><th colspan="4">Mulga Rock Project – Ambassador Deposit May 2017 Block Model Construction Parameters</th></tr><tr><th></th><th>Origin (m)</th><th>Extent (m)</th><th>Parent/Sub Block Size (m)</th></tr><tr><td>Easting</td><td>573000</td><td>10500</td><td>50/10</td></tr><tr><td>Northing</td><td>6676000</td><td>9000</td><td>50/10</td></tr><tr><td>Elevation</td><td>230</td><td>170</td><td>1.0/0.25</td></tr></table>	Mulga Rock Project – Ambassador Deposit May 2017 Block Model Construction Parameters					Origin (m)	Extent (m)	Parent/Sub Block Size (m)	Easting	573000	10500	50/10	Northing	6676000	9000	50/10	Elevation	230	170	1.0/0.25
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Northing	6676000	9000	50/10																			
Elevation	230	170	1.0/0.25																			
Estimation and modelling techniques	<ul style="list-style-type: none"><i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i><i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i><i>The assumptions made regarding recovery of by-products.</i><i>Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulfur for acid mine drainage)</i>	<ul style="list-style-type: none">Vimy, under AMC Consultants supervision, estimated the Mineral Resource for the Ambassador deposit as at May 2017.U₃O₈ grade estimation was completed using a combination of accumulation process involving OK for the thin, high-grade upper mineralised zones and normal OK for the lower mineralised zones.The estimation was constrained with geological mineralisation interpretations and sub-domains.In the majority of cases at Ambassador and Princess, the radiometric e U₃O₈ grades for similar intervals are lower than the corresponding chemical assays for U₃O₈, requiring positive adjustments to the radiometric data to emulate the accurate chemical assay data. Data for the mineralised subdomains were split into groups based on the data types and then distinctly identified grade																				

Criteria	JORC Code explanation	Commentary
	<p><i>characterisation).</i></p> <ul style="list-style-type: none"> <i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i> <i>Any assumptions behind modelling of selective mining units.</i> <i>Any assumptions about correlation between variables.</i> <i>Description of how the geological interpretation was used to control the resource estimates.</i> <i>Discussion of basis for using or not using grade cutting or capping.</i> <i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i> 	<p>ranges. Separate disequilibrium corrections (regression formulae for Q-Q data) were derived for each data type and sub-domain.</p> <ul style="list-style-type: none"> All samples within the mineralised wireframes were composited to 0.5m samples. High grade cuts were applied to the combined chemical and eU₃O₈d 0.5m composite data for the various uranium domains and sub-domains. High grade cuts ranged from 3,000 to 15,000ppm for high grade sub-domains and 700ppm to no-cut for deeper low grade sub-domains. Accumulation Method Ordinary Kriging (OK) and normal OK estimates were completed using grade variogram models and a set of ancillary parameters controlling the source and selection of composite data from the domains and sub-domains. The sample search parameters were defined based on the estimation methods, variography and the data spacing. A two pass search strategy with hard boundaries was used for all sub-domains belonging to domains 100, 200, 300 and 400. Mining will be by shallow open pit mining. Details are currently the subject of an updated Definitive Feasibility Study. Mining is expected to be more selective than the current drill spacing and supported block estimation size. Block estimates were visually compared to the input composite samples in section views and swath plots. Global average grades for estimates and declustered composite mean grades show a good correspondence. Other than for limited trial mining in two small pits, mining has not commenced so no reconciliation data is available for the deposit. No assumptions were made concerning recovery of by-products as this does not drive the economics of the project. The block size of 50m x 50m x 1m is considered appropriate given the drillhole spacing and style of mineralisation. No assumptions are made regarding the SMU in the model. The 2017 Ambassador Mineral Resource has changed from the previous Mineral Resource for the infill area primarily due to the following items: <ul style="list-style-type: none"> Increased drill spacing and diamond drilling density in the area reported (Ambassador East). Introduction of key sub-domains to better honour local geology, palaeochannel profile, tenor of mineralisation, and disequilibrium characteristics. Changes to interpretations related to infill drilling and improved geological knowledge. Some of the domains have decreased slightly in volume while others have increased.

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> Changes to bulk density values and method of applying the densities according to estimated dominant lithologies for direct estimation. Driven partly by improved moisture estimates, the dry bulk densities for some domains will have increased slightly on average. The use of sub-domains has improved disequilibrium factors generated from DC holes, and has improved the parity between the eU_3O_8 radiometric data and the U_3O_8 assay data, honouring local variations. The disequilibrium studies have been thorough in distinguishing the various radiometric data types, tools, and domains. The purpose of the disequilibrium factors applied to the various data and domains is to get the consistently low biased eU_3O_8 radiometric data to be statistically comparable to the “umpire/correct” chemical assay data. The revised 2017 Mineral Resource for the Ambassador East infill area has increased by approximately 14% in terms of contained U_3O_8 metal compared to the June 2016 estimate. For the larger Ambassador area, the additional data and modelling currently results in an overall 4% increase in contained metal.
Moisture	<ul style="list-style-type: none"> Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content. 	<ul style="list-style-type: none"> Tonnages and metal are reported on a dry basis, requiring a dry in-situ bulk density. Wet density and moisture are also estimated in the block model for mining studies and metallurgical purposes.
Cut-off parameters	<ul style="list-style-type: none"> The basis of the adopted cut-off grade(s) or quality parameters applied. 	<ul style="list-style-type: none"> The nominal 100ppm U_3O_8 lower cut-off used to interpret the mineralisation domains was chosen as it represents a natural break in the assay data. A block cut-off grade of 150ppm U_3O_8 is currently applied for reporting purposes assuming open-pit mining methods. Mining studies are currently in progress.
Mining factors or assumptions	<ul style="list-style-type: none"> Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made. 	<ul style="list-style-type: none"> Relatively shallow open pit mining, incorporating in-pit waste and tailings disposal is assumed for the bulk of the deposit. No mining recovery factor has been applied to the U_3O_8 in the Mineral Resource. Mining is by open pit, and it is assumed that the majority of the mineralisation occurring within the pit design can be recovered for processing.
Metallurgical factors or assumptions	<ul style="list-style-type: none"> The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical 	<ul style="list-style-type: none"> No factors have been applied regarding metallurgy, recovery or processing cost in the Mineral Resource. At Ambassador, spectral, mineralogical, deportment and metallurgical studies

Criteria	JORC Code explanation	Commentary
	<i>methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i>	<p>show that the bulk of the uranium is in a hexavalent ionic state and adsorbed onto organic matter, with a negligible fraction contained in refractory minerals.</p> <ul style="list-style-type: none"> Recent test work at Ambassador has shown potential recoveries greater than 90% for both lignite and sand-hosted mineralised material, using an atmospheric acid leach (tested in a resin-in-pulp configuration).
Environmental factors or assumptions	<ul style="list-style-type: none"> Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made. 	<ul style="list-style-type: none"> The November 2015 Pre-Feasibility Study identified that the most effective management of overburden storage would be to employ strip mining with the majority of waste placed in the mining void as the pit advances. This would minimise the size of above ground overburden storage areas. Additional mining studies part of the MRP DFS have identified that hybrid in-pit and above ground overburden disposal might be suitable and equally cost-effective. The Mulga Rock Project Public Environmental Review (PER) document was lodged and accepted for public comment by the EPA in November 2015. The public comment period closed in March 2016. The Project achieved State and Commonwealth environmental permitting in December 2016 and March 2017 respectively.
Bulk density	<ul style="list-style-type: none"> Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples. The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit. Discuss assumptions for bulk density estimates used in the evaluation process of the different materials. 	<ul style="list-style-type: none"> Bulk density has been determined by using both gamma downhole geophysical logging of diamond drill holes in the Ambassador deposit and Archimedean data from core samples. The Archimedean density measurements have been used to validate and correct the downhole geophysical data where applicable. Downhole gamma data has been selectively used where differences have been identified. Dry bulk density values were determined by converting the wet bulk density using moisture values for the corresponding lithology and mineralised domain type. Bulk densities were estimated directly into the block models using Inverse Distance (Power=1) method, and assigned to the composite intervals according to the main lithologies discussed above, each assigned a specific moisture, wet bulk density and dry bulk density. Those densities were checked using a probability based lithological model and found to be identical. Density values assigned to the Ambassador deposit are consistent with density of similar lithologies for other deposits in the area.
Classification	<ul style="list-style-type: none"> The basis for the classification of the Mineral Resources into varying confidence categories. Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, 	<ul style="list-style-type: none"> The Mineralised Resource has been classified as a combination of Measured, Indicated and Inferred material, in accordance with JORC Code 2012 guidelines based on the confidence levels of the key criteria considered during the resource estimation such as data quality, drilling density, apparent

Criteria	JORC Code explanation	Commentary
	<p><i>reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i></p> <ul style="list-style-type: none"> <i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i> 	<p>grade and spatial continuity of the mineralisation.</p>
Audits or reviews	<ul style="list-style-type: none"> <i>The results of any audits or reviews of Mineral Resource estimates.</i> 	<ul style="list-style-type: none"> AMC have audited the 2017 Ambassador Mineral Resource model and determined that the model is fit for purpose.
Discussion of relative accuracy/ confidence	<ul style="list-style-type: none"> <i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i> <i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i> <i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i> 	<ul style="list-style-type: none"> The resource classification represents the relative confidence in the resource estimate as determined by the Competent Person. Issues contributing to or detracting from that confidence are discussed above. Conditional simulation modelling has been used to help quantify the confidence levels associated with varying drill spacing, and its implications with regards to plant feed variability. All other things being equal, the following criteria were used to support resource classification: <ul style="list-style-type: none"> Measured category is defined as having a +/- 15% relative error at the 90% level against the quarterly production output (~0.75Mlb U₃O₈). Indicated category is defined as having a +/- 15% relative error at the 90% level against the annual production output (~3Mlb U₃O₈). The ordinary kriged estimates are considered to be a global estimate with no further adjustments for Selective Mining Unit (SMU) dimensions. Accurate mining scenarios are yet to be determined by the current Definitive Feasibility Studies. No large-scale production data is available for comparison to the estimate. The local accuracy of the resource is adequate for the expected use of the model in the feasibility study. Due to the nature of the uranium mineralisation, the degree of radiochemical disequilibrium is likely to vary considerably between drill holes and with depth down each drill hole. The disequilibrium factoring applied for the 2017 Resource estimate has resulted in satisfactory global results, but local variations are expected. Diamond drilling and increased drill spacing have improved the geological, physical property (density and moisture) and disequilibrium adjustment confidence in the Ambassador East deposit. Further investigation into suitable grade control methods will be conducted before moving the MRP into production.

List of uranium intercepts - 2017 Mulga Rock East Exploration Results - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7001	580555	6683187	334.7	45	AC	41	44	345
NNA7002	580406	6683166	332.6	45	AC	40	42.5	258
NNA7005	580448	6683025	335.9	54	AC	50.5	51	157
NNA7005	580448	6683025	335.9	54	AC	47.5	50	176
NNA7006	580076	6683116	330.5	45	AC	38.5	40	193
NNA7007	580106	6683098	330.7	41	AC	35.5	38.5	484
NNA7011	580352	6682954	336.1	51	AC	41.5	46.5	772
NNA7012	580422	6682913	338.8	66	AC	51	54	131
NNA7013	580038	6683068	330.3	45	AC	39	41.5	145
NNA7015	580183	6682984	331.7	45	AC	36	41	535
NNA7015	580183	6682984	331.7	45	AC	42	43	130
NNA7019	580048	6682994	330.5	45	AC	34	37	282
NNA7019	580048	6682994	330.5	45	AC	40.5	41	109
NNA7020	580082	6682973	331.0	43	AC	39.5	40.5	169
NNA7020	580082	6682973	331.0	43	AC	34	37.5	339
NNA7022	580149	6682933	332.4	48	AC	37.5	44	433
NNA7023	580183	6682913	333.2	48	AC	39	43.5	720
NNA7023	580183	6682913	333.2	48	AC	44	44.5	131
NNA7025	580251	6682872	334.4	54	AC	42	46	436
NNA7026	580288	6682854	335.1	51	AC	42	46	956
NNA7026	580288	6682854	335.1	51	AC	46.5	47	165
NNA7027	579900	6683003	328.8	42	AC	34	36	927
NNA7029	580052	6682919	331.1	45	AC	35	37	1111
NNA7029	580052	6682919	331.1	45	AC	40.5	41.5	120
NNA7030	579773	6683007	328.0	48	AC	34	37	479
NNA7031	579850	6682962	328.3	45	AC	33	35.5	522
NNA7031	579850	6682962	328.3	45	AC	36	37	193
NNA7033	579965	6682912	330.0	48	AC	34	35	140
NNA7034	580055	6682840	337.6	60	AC	44	48.5	1208
NNA7039	579774	6682954	328.7	42	AC	35	39.5	512
NNA7040	579805	6682936	328.6	42	AC	36	39.5	547
NNA7043	580041	6682781	331.1	51	AC	36.5	37	375

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7043	580041	6682781	331.1	51	AC	37.5	41.5	909
NNA7044	580079	6682769	331.7	48	AC	38	42	441
NNA7044	580079	6682769	331.7	48	AC	43.5	44	126
NNA7045	580115	6682743	333.0	48	AC	39.5	41	839
NNA7046	580146	6682728	334.2	48	AC	38.5	40	328
NNA7048	579761	6682915	329.4	44	AC	37	40.5	712
NNA7054	579683	6682896	330.5	43	AC	38.5	39.5	431
NNA7056	579750	6682856	331.3	45	AC	37.5	40.5	557
NNA7058	579830	6682816	331.4	46	AC	38	41.5	578
NNA7059	579859	6682783	339.4	60	AC	46	50	929
NNA7059	579859	6682783	339.4	60	AC	51	51.5	152
NNA7060	579995	6682708	331.6	54	AC	38.5	43.5	2090
NNA7061	580026	6682685	337.9	57	AC	44.5	48.5	1349
NNA7062	580044	6682662	338.2	54	AC	45	46	469
NNA7063	580112	6682644	335.0	48	AC	38	38.5	117
NNA7071	579786	6682770	332.3	48	AC	40	43.5	623
NNA7072	579857	6682729	332.3	54	AC	39	45.5	695
NNA7074	579212	6683064	349.1	79	AC	52	54.5	1984
NNA7074	579212	6683064	349.1	79	AC	58.5	60	439
NNA7074	579212	6683064	349.1	79	AC	61	62	152
NNA7074	579212	6683064	349.1	79	AC	62.5	64	118
NNA7078	579369	6682970	336.7	51	AC	43	46.5	240
NNA7080	579435	6682930	334.3	48	AC	40	45	513
NNA7080	579435	6682930	334.3	48	AC	45.5	47	368
NNA7082	579506	6682888	332.1	45	AC	38.5	42	293
NNA7086	579638	6682810	331.2	45	AC	39	42	495
NNA7088	579700	6682771	331.9	48	AC	39	43	331
NNA7091	579803	6682709	333.3	48	AC	40	44	407
NNA7092	579837	6682691	333.2	48	AC	39.5	44	2792
NNA7093	579904	6682648	333.2	48	AC	39	44	1181
NNA7094	579940	6682630	333.5	48	AC	40	44.5	2454
NNA7104	579056	6683035	347.5	81	AC	61	63	429

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7104	579056	6683035	347.5	81	AC	63.5	64.5	206
NNA7104	579056	6683035	347.5	81	AC	66	66.5	114
NNA7105	579084	6683019	347.3	78	AC	54.5	57	404
NNA7105	579084	6683019	347.3	78	AC	67	73	349
NNA7105	579084	6683019	347.3	78	AC	73.5	75	136
NNA7106	579119	6682995	345.5	78	AC	55	57	755
NNA7109	579215	6682939	339.0	70	AC	42.5	51	1117
NNA7109	579215	6682939	339.0	70	AC	52	54	295
NNA7109	579215	6682939	339.0	70	AC	55	57	337
NNA7109	579215	6682939	339.0	70	AC	58	59	102
NNA7110	579251	6682916	338.3	75	AC	45	48	722
NNA7110	579251	6682916	338.3	75	AC	49	49.5	115
NNA7113	579357	6682858	334.7	51	AC	40.5	46	282
NNA7113	579357	6682858	334.7	51	AC	46.5	47	105
NNA7117	579493	6682777	331.6	48	AC	38.5	42.5	551
NNA7117	579493	6682777	331.6	48	AC	43	43.5	150
NNA7119	579561	6682735	331.7	45	AC	38.5	42	929
NNA7121	579631	6682695	331.4	46	AC	38	41	902
NNA7123	579699	6682654	331.7	47	AC	39.5	43	406
NNA7125	579767	6682613	332.0	48	AC	39.5	44.5	372
NNA7128	579871	6682555	333.1	48	AC	38	41	561
NNA7128	579871	6682555	333.1	48	AC	42	42.5	147
NNA7131	579108	6682947	340.4	81	AC	46	52	1737
NNA7131	579108	6682947	340.4	81	AC	54	58	474
NNA7131	579108	6682947	340.4	81	AC	61	63	152
NNA7131	579108	6682947	340.4	81	AC	72	73	257
NNA7132	579161	6682914	339.0	78	AC	44	51	707
NNA7132	579161	6682914	339.0	78	AC	51.5	53	152
NNA7132	579161	6682914	339.0	78	AC	53.5	55.5	158
NNA7132	579161	6682914	339.0	78	AC	56	56.5	105
NNA7132	579161	6682914	339.0	78	AC	57.5	59.5	176
NNA7132	579161	6682914	339.0	78	AC	61	62	144
NNA7132	579161	6682914	339.0	78	AC	62.5	64	208
NNA7132	579161	6682914	339.0	78	AC	65	66	126

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7133	579237	6682879	338.2	72	AC	45.5	47.5	542
NNA7133	579237	6682879	338.2	72	AC	48	50	402
NNA7133	579237	6682879	338.2	72	AC	53	54	119
NNA7133	579237	6682879	338.2	72	AC	57	63	202
NNA7134	579310	6682829	335.6	54	AC	40.5	44	432
NNA7146	579114	6682896	339.3	81	AC	43.5	51	2598
NNA7146	579114	6682896	339.3	81	AC	63	63.5	103
NNA7146	579114	6682896	339.3	81	AC	64	64.5	152
NNA7146	579114	6682896	339.3	81	AC	65.5	66	119
NNA7147	579148	6682875	339.3	72	AC	41.5	45	595
NNA7147	579148	6682875	339.3	72	AC	46	57	289
NNA7147	579148	6682875	339.3	72	AC	58	59	104
NNA7148	579183	6682853	339.1	72	AC	43	47.5	812
NNA7150	579251	6682815	337.9	60	AC	44.5	48.5	534
NNA7151	579287	6682794	336.6	60	AC	42	46.5	205
NNA7152	579320	6682773	335.4	57	AC	40	43	194
NNA7155	579428	6682718	332.8	54	AC	41.5	45	276
NNA7158	579558	6682625	332.4	51	AC	39	42	356
NNA7160	579627	6682586	332.5	51	AC	40.5	46	358
NNA7162	579700	6682544	332.6	48	AC	39	43	308
NNA7166	579207	6682776	339.6	66	AC	47	51	551
NNA7167	579348	6682691	334.7	54	AC	40.5	44.5	567
NNA7171	578975	6682852	337.4	59	AC	42	44.5	758
NNA7173	579044	6682811	338.2	63	AC	45	49.5	231
NNA7173	579044	6682811	338.2	63	AC	50	50.5	106
NNA7173	579044	6682811	338.2	63	AC	51	53.5	131
NNA7173	579044	6682811	338.2	63	AC	55	58	188
NNA7173	579044	6682811	338.2	63	AC	58.5	59	113
NNA7173	579044	6682811	338.2	63	AC	59.5	60	141
NNA7175	579112	6682771	338.6	72	AC	44.5	47.5	2238
NNA7175	579112	6682771	338.6	72	AC	53	54	108
NNA7175	579112	6682771	338.6	72	AC	56	57	107
NNA7176	579143	6682753	339.3	69	AC	41.5	43.5	710
NNA7178	579216	6682706	338.6	69	AC	43.5	49	1300

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7179	579252	6682689	337.0	55	AC	42.5	47.5	296
NNA7180	579281	6682667	335.8	54	AC	42.5	43	217
NNA7180	579281	6682667	335.8	54	AC	43.5	47	276
NNA7180	579281	6682667	335.8	54	AC	48	48.5	133
NNA7182	579356	6682625	334.4	51	AC	40	42	1656
NNA7182	579356	6682625	334.4	51	AC	44	45.5	121
NNA7183	579387	6682607	334.1	51	AC	41	45.5	1903
NNA7185	579455	6682568	333.5	51	AC	41.5	45.5	400
NNA7192	579171	6682677	337.8	60	AC	43	48	1015
NNA7193	579251	6682645	335.8	63	AC	41	47	1011
NNA7193	579251	6682645	335.8	63	AC	48.5	49	149
NNA7193	579251	6682645	335.8	63	AC	50.5	51	113
NNA7194	579315	6682601	335.3	54	AC	40.5	43.5	704
NNA7195	579376	6682551	335.0	54	AC	40.5	42.5	776
NNA7201	579020	6682707	337.1	48	AC	39	41	394
NNA7203	579095	6682666	336.8	53	AC	41.5	46	379
NNA7204	579125	6682648	336.4	60	AC	41	46.5	739
NNA7204	579125	6682648	336.4	60	AC	47	48	419
NNA7206	579197	6682606	335.6	57	AC	41	48	593
NNA7208	579264	6682565	336.1	54	AC	41	46	538
NNA7209	579299	6682548	336.5	54	AC	44	51.5	433
NNA7210	579336	6682523	336.6	57	AC	42	42.5	116
NNA7210	579336	6682523	336.6	57	AC	43	50.5	519
NNA7211	579365	6682506	336.4	51	AC	42	46	541
NNA7212	579436	6682464	334.9	51	AC	42.5	46	296
NNA7213	579502	6682426	332.9	49	AC	41	43.5	340
NNA7218	579387	6682439	336.8	54	AC	46.5	52	502
NNA7219	578866	6682682	338.1	51	AC	40	42	310
NNA7221	578935	6682637	338.9	52	AC	43.5	46	188
NNA7223	579005	6682597	338.5	53.5	AC	42.5	47.5	850
NNA7227	579142	6682518	337.7	54	AC	43.5	44	114
NNA7227	579142	6682518	337.7	54	AC	44.5	47	676
NNA7229	579207	6682476	339.8	54	AC	43.5	44	367
NNA7229	579207	6682476	339.8	54	AC	44.5	48	588

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7230	579241	6682454	340.2	57	AC	46.5	55	426
NNA7231	579278	6682434	340.2	56	AC	48.5	52	291
NNA7232	579307	6682411	339.8	54	AC	45.5	46	121
NNA7232	579307	6682411	339.8	54	AC	47.5	52.5	669
NNA7234	579404	6682358	336.6	54	AC	45.5	49	253
NNA7235	578835	6682647	337.2	51	AC	39.5	41.5	750
NNA7236	578899	6682605	338.8	51	AC	44	47.5	290
NNA7242	578875	6682562	338.9	51	AC	43.5	45.5	673
NNA7244	578947	6682518	340.9	54	AC	44	46.5	465
NNA7249	579369	6682269	340.1	54	AC	48.5	49.5	191
NNA7251	579050	6682376	346.9	59.5	AC	52	55.5	711
NNA7251	579050	6682376	346.9	59.5	AC	56	56.5	144
NNA7252	579088	6682358	348.2	60	AC	53	57.5	420
NNA7253	579131	6682338	349.3	63	AC	56	59	294
NNA7255	579258	6682274	342.4	59	AC	49.5	57	260
NNA7256	578904	6682417	343.0	57	AC	45.5	49.5	1541
NNA7258	578974	6682383	344.8	66	AC	51.5	55.5	883
NNA7259	579015	6682351	341.8	57	AC	46.5	50	626
NNA7260	579040	6682328	342.5	62	AC	47.5	52	495
NNA7262	579132	6682280	345.0	60	AC	52	57	652
NNA7263	579193	6682244	340.6	57	AC	48.5	51	586
NNA7264	579248	6682213	342.3	59	AC	50	53	266
NNA7267	579594	6682475	333.1	46	AC	40	42	494
NNA7269	580471	6683130	333.8	48	AC	41.5	42	119
NNA7269	580471	6683130	333.8	48	AC	42.5	43	109
NNA7269	580471	6683130	333.8	48	AC	39	40	278
NNA7270	580532	6683095	335.1	51	AC	44.5	45	106
NNA7270	580532	6683095	335.1	51	AC	50	50.5	107
NNA7271	580286	6683120	331.6	45	AC	39.5	40	150
NNA7271	580286	6683120	331.6	45	AC	40.5	42	491
NNA7272	580329	6683095	332.2	45	AC	39.5	40	108
NNA7272	580329	6683095	332.2	45	AC	40.5	42	274
NNA7274	580177	6683057	332.2	48	AC	40.5	41	231
NNA7274	580177	6683057	332.2	48	AC	35.5	40	390

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7276	580319	6682971	335.1	51	AC	39.5	46	601
NNA7277	580383	6682934	337.4	60	AC	43	46.5	1272
NNA7279	580324	6682908	336.2	56.5	AC	44	49	508
NNA7281	578759	6682743	337.5	57	AC	43.5	44	177
NNA7281	578759	6682743	337.5	57	AC	46	49	112
NNA7281	578759	6682743	337.5	57	AC	52	53	106
NNA7281	578759	6682743	337.5	57	AC	41.5	42.5	162
NNA7284	578667	6682683	336.4	57	AC	36.5	40	1234
NNA7284	578667	6682683	336.4	57	AC	41	41.5	114
NNA7284	578667	6682683	336.4	57	AC	43	44.5	140
NNA7284	578667	6682683	336.4	57	AC	54	56	166
NNA7285	578717	6682654	335.5	57	AC	36.5	38.5	2581
NNA7285	578717	6682654	335.5	57	AC	42.5	44.5	582
NNA7286	578755	6682628	335.3	54	AC	36.5	49	530
NNA7286	578755	6682628	335.3	54	AC	50	51	115
NNA7287	578801	6682602	336.3	54	AC	38	44.5	749
NNA7287	578801	6682602	336.3	54	AC	47.5	48	130
NNA7289	578576	6682671	336.1	51	AC	36.5	38	354
NNA7289	578576	6682671	336.1	51	AC	38.5	39.5	266
NNA7289	578576	6682671	336.1	51	AC	42	43.5	526
NNA7290	578524	6682647	335.9	51	AC	38	39	1406
NNA7290	578524	6682647	335.9	51	AC	39.5	41.5	1143
NNA7290	578524	6682647	335.9	51	AC	42	44	278
NNA7291	578563	6682622	335.6	54	AC	35	43	744
NNA7291	578563	6682622	335.6	54	AC	48	49	156
NNA7292	578607	6682591	334.9	60	AC	36	44.5	361
NNA7292	578607	6682591	334.9	60	AC	45	48	186
NNA7292	578607	6682591	334.9	60	AC	48.5	49.5	136
NNA7294	578690	6682542	334.1	54	AC	36	40	1778
NNA7295	578731	6682513	334.8	51	AC	37	41.5	1485
NNA7296	578782	6682489	336.8	54	AC	40.5	46	1576
NNA7298	578864	6682436	341.0	54	AC	47	50.5	756
NNA7299	578702	6682491	334.4	51	AC	36.5	41.5	1429
NNA7300	578762	6682450	336.7	51	AC	39.5	41	1122

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7300	578762	6682450	336.7	51	AC	42	42.5	269
NNA7301	578833	6682407	340.8	63	AC	47	51	833
NNA7301	578833	6682407	340.8	63	AC	51.5	52	158
NNA7303	578721	6682402	336.9	57	AC	42.5	50	748
NNA7305	578817	6682348	342.3	60	AC	45.5	47.5	801
NNA7305	578817	6682348	342.3	60	AC	48	48.5	125
NNA7306	578845	6682329	343.3	66	AC	49.5	54	609
NNA7307	578902	6682298	336.8	57	AC	41	45.5	831
NNA7307	578902	6682298	336.8	57	AC	46	46.5	165
NNA7308	578964	6682261	338.4	51	AC	41.5	43.5	418
NNA7308	578964	6682261	338.4	51	AC	45	45.5	190
NNA7309	578993	6682238	338.5	54	AC	43	46.5	369
NNA7310	578841	6682278	339.2	51	AC	41.5	47	1632
NNA7310	578841	6682278	339.2	51	AC	48	49	290
NNA7310	578841	6682278	339.2	51	AC	50	51	246
NNA7315	578636	6682444	334.3	54	AC	38	45	697
NNA7316	578592	6682475	333.6	51	AC	35	39.5	1186
NNA7316	578592	6682475	333.6	51	AC	40.5	41	110
NNA7318	578501	6682532	334.9	54	AC	38.5	41.5	614
NNA7319	578464	6682552	336.8	54	AC	36.5	38.5	2045
NNA7319	578464	6682552	336.8	54	AC	41	42.5	143
NNA7319	578464	6682552	336.8	54	AC	43	44.5	158
NNA7320	578424	6682581	338.4	54	AC	38	44	1097
NNA7323	579206	6684354	341.6	57	AC	52	53	124
NNA7323	579206	6684354	341.6	57	AC	50.5	51	110
NNA7325	579364	6684262	340.3	57	AC	49.5	50	143
NNA7326	579508	6684184	344.8	66	AC	54.5	61	361
NNA7327	579282	6684196	340.4	57	AC	45	51.5	464
NNA7328	578813	6684218	343.3	60	AC	41	46.5	689
NNA7328	578813	6684218	343.3	60	AC	47.5	49	240
NNA7329	579024	6683964	339.2	57	AC	39	39.5	440
NNA7329	579024	6683964	339.2	57	AC	40.5	49	443
NNA7331	578837	6683983	340.0	51	AC	36	36.5	117
NNA7331	578837	6683983	340.0	51	AC	37	42.5	795

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7333	578836	6683761	344.1	57	AC	43.5	46	2127
NNA7333	578836	6683761	344.1	57	AC	47	47.5	112
NNA7335	578918	6683583	338.2	51	AC	39.5	45	765
NNA7336	578847	6683505	337.2	51	AC	39	40	1602
NNA7336	578847	6683505	337.2	51	AC	40.5	42.5	537
NNA7337	581704	6683457	336.9	57	AC	42.5	48	251
NNA7337	581704	6683457	336.9	57	AC	48.5	51	142
NNA7337	581704	6683457	336.9	57	AC	53	54	292
NNA7338	581782	6683424	339.4	54	AC	45.5	49	185
NNA7340	581567	6683426	335.3	51	AC	37.5	38.5	128
NNA7341	581638	6683381	336.9	54	AC	41.5	42	232
NNA7344	581488	6683349	336.0	51	AC	35.5	37.5	673
NNA7345	581555	6683310	336.5	51	AC	40	42.5	251
NNA7346	581617	6683266	339.4	54	AC	45	47.5	183
NNA7347	581342	6683309	336.1	51	AC	39.5	40	108
NNA7347	581342	6683309	336.1	51	AC	40.5	41	109
NNA7347	581342	6683309	336.1	51	AC	38	39	148
NNA7348	581413	6683267	336.9	59	AC	43.5	46.5	513
NNA7348	581413	6683267	336.9	59	AC	47	50	346
NNA7348	581413	6683267	336.9	59	AC	50.5	51	108
NNA7350	581524	6683203	339.2	54	AC	45.5	47	244
NNA7352	581270	6683247	335.6	54	AC	39.5	44	336
NNA7353	581335	6683206	335.3	54	AC	40	44	762
NNA7353	581335	6683206	335.3	54	AC	48.5	49	108
NNA7354	581403	6683169	336.1	54	AC	40.5	42.5	1233
NNA7355	581202	6683188	334.2	51	AC	42.5	45	152
NNA7355	581202	6683188	334.2	51	AC	35.5	42	202
NNA7358	578632	6682341	341.6	57	AC	43.5	46	2762
NNA7358	578632	6682341	341.6	57	AC	46.5	48.5	246
NNA7359	578591	6682374	338.3	57	AC	42.5	46.5	802
NNA7360	578552	6682400	337.1	51	AC	38.5	40.5	538
NNA7362	578433	6682458	341.1	60	AC	42.5	50	1520
NNA7363	578397	6682484	340.9	63	AC	41.5	42	131
NNA7363	578397	6682484	340.9	63	AC	43	45.5	1771

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NNA7363	578397	6682484	340.9	63	AC	47	48.5	223
NNA7363	578397	6682484	340.9	63	AC	49	50.5	108
NNA7364	578341	6682518	340.5	60	AC	41	47.5	1294
NNA7364	578341	6682518	340.5	60	AC	48	51	206
NNA7367	578760	6682149	332.6	51	AC	34.5	36	337
NNA7369	578660	6682203	332.9	51	AC	35	39	1442
NNA7370	578605	6682233	335.3	57	AC	37	41.5	1045
NNA7372	578472	6682314	347.6	66	AC	51	51.5	174
NNA7372	578472	6682314	347.6	66	AC	53	57	702
NNA7373	578413	6682355	349.2	63	AC	48	50	1029
NNA7373	578413	6682355	349.2	63	AC	50.5	53.5	1466
NNA7374	578355	6682390	349.0	63	AC	50	52	337
NNA7375	578306	6682417	347.7	60	AC	46.5	47.5	216
NNA7375	578306	6682417	347.7	60	AC	48	52	1671
NNA7377	578207	6682469	343.9	59	AC	43	43.5	111
NNA7377	578207	6682469	343.9	59	AC	44	45	252
NNA7377	578207	6682469	343.9	59	AC	45.5	50	711
NNA7377	578207	6682469	343.9	59	AC	51.5	52	130
NND7000	580513	6683217	334.5	43	DDH	40.55	41.6	1319
NND7003	580237	6683145	330.9	45	DDH	34	34.2	230
NND7003	580237	6683145	330.9	45	DDH	34.45	34.9	218
NND7003	580237	6683145	330.9	45	DDH	36.7	37	316
NND7003	580237	6683145	330.9	45	DDH	37.8	38.4	129
NND7003	580237	6683145	330.9	45	DDH	39.2	39.7	292
NND7003	580237	6683145	330.9	45	DDH	40.25	41	134
NND7004	580360	6683078	332.9	45.5	DDH	37.25	37.4	1100
NND7004	580360	6683078	332.9	45.5	DDH	37.75	38.2	299
NND7008	580140	6683076	331.4	45	DDH	34.25	35	1201
NND7008	580140	6683076	331.4	45	DDH	35.4	35.95	279
NND7008	580140	6683076	331.4	45	DDH	36.35	40.1	727
NND7008	580140	6683076	331.4	45	DDH	40.65	41	133
NND7010	580277	6682994	333.9	48	DDH	37.45	37.7	137
NND7010	580277	6682994	333.9	48	DDH	40.1	41.1	199
NND7010	580277	6682994	333.9	48	DDH	41.65	42.4	313

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NND7014	580113	6683026	331.1	42.3	DDH	34.25	36.2	1304
NND7014	580113	6683026	331.1	42.3	DDH	36.3	37.55	487
NND7014	580113	6683026	331.1	42.3	DDH	38.1	39.3	231
NND7016	579937	6683053	329.2	41	DDH	38	38.4	176
NND7016	579937	6683053	329.2	41	DDH	36.85	37.35	285
NND7021	580120	6682953	331.7	45.3	DDH	35.9	36.3	1427
NND7021	580120	6682953	331.7	45.3	DDH	36.7	37.7	555
NND7021	580120	6682953	331.7	45.3	DDH	37.8	38	623
NND7024	580216	6682890	333.9	49	DDH	39.8	40.9	3803
NND7024	580216	6682890	333.9	49	DDH	41	42.3	886
NND7024	580216	6682890	333.9	49	DDH	42.5	43.05	1268
NND7024	580216	6682890	333.9	49	DDH	43.2	43.4	110
NND7024	580216	6682890	333.9	49	DDH	43.7	44	139
NND7028	579973	6682963	330.0	39.3	DDH	33.45	33.9	494
NND7028	579973	6682963	330.0	39.3	DDH	34.1	34.7	1865
NND7028	579973	6682963	330.0	39.3	DDH	35.25	35.4	116
NND7032	579923	6682925	329.4	41	DDH	31.8	32	153
NND7032	579923	6682925	329.4	41	DDH	32.2	32.4	113
NND7032	579923	6682925	329.4	41	DDH	32.5	32.7	174
NND7032	579923	6682925	329.4	41	DDH	33.15	33.3	575
NND7032	579923	6682925	329.4	41	DDH	34.3	34.5	145
NND7032	579923	6682925	329.4	41	DDH	38.2	38.4	191
NND7035	580135	6682798	332.2	47	DDH	39	41.15	1579
NND7035	580135	6682798	332.2	47	DDH	41.95	43	240
NND7036	580188	6682760	331	46.8	DDH	38.2	38.3	2134
NND7036	580188	6682760	331	46.8	DDH	38.4	38.7	1273
NND7038	579700	6682995	329.0	42	DDH	34.1	35	588
NND7038	579700	6682995	329.0	42	DDH	35.2	35.6	1063
NND7038	579700	6682995	329.0	42	DDH	38.05	38.2	251
NND7038	579700	6682995	329.0	42	DDH	38.6	38.85	236
NND7038	579700	6682995	329.0	42	DDH	39.1	39.35	130
NND7041	579833	6682919	328.9	42	DDH	34.45	36.8	4059
NND7041	579833	6682919	328.9	42	DDH	37.5	38.2	268
NND7052	579612	6682939	330.3	41	DDH	35.9	36.65	552

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NND7052	579612	6682939	330.3	41	DDH	36.8	37	1238
NND7052	579612	6682939	330.3	41	DDH	37.35	37.7	1346
NND7052	579612	6682939	330.3	41	DDH	37.9	39.05	1246
NND7057	579793	6682831	331.5	46.6	DDH	38	39.6	1509
NND7057	579793	6682831	331.5	46.6	DDH	40.2	41.5	458
NND7076	579285	6683015	339.4	54	DDH	42.2	42.65	261
NND7076	579285	6683015	339.4	54	DDH	43.2	44.9	469
NND7076	579285	6683015	339.4	54	DDH	48.85	50.65	147
NND7076	579285	6683015	339.4	54	DDH	51.1	51.5	259
NND7076	579285	6683015	339.4	54	DDH	51.95	52.2	362
NND7076	579285	6683015	339.4	54	DDH	52.5	53.25	162
NND7084	579568	6682849	331.1	46.5	DDH	37.35	37.65	179
NND7084	579568	6682849	331.1	46.5	DDH	38.35	39.7	1443
NND7084	579568	6682849	331.1	46.5	DDH	40.25	41	436
NND7090	579765	6682730	332.8	48	DDH	39.95	40.3	120
NND7090	579765	6682730	332.8	48	DDH	40.5	42.3	1040
NND7090	579765	6682730	332.8	48	DDH	43.4	44	358
NND7095	579979	6682611	333.9	45.3	DDH	36	36.65	1199
NND7097	579171	6683054	350.2	80	DDH	53.15	54.4	2459
NND7097	579171	6683054	350.2	80	DDH	60.65	61.45	809
NND7097	579171	6683054	350.2	80	DDH	62.65	64.25	280
NND7097	579171	6683054	350.2	80	DDH	64.65	66.6	264
NND7097	579171	6683054	350.2	80	DDH	66.8	68	153
NND7097	579171	6683054	350.2	80	DDH	69	69.9	349
NND7097	579171	6683054	350.2	80	DDH	70.5	71.4	307
NND7097	579171	6683054	350.2	80	DDH	71.8	71.9	410
NND7097	579171	6683054	350.2	80	DDH	72	73.4	152
NND7108	579177	6682961	339.7	70.4	DDH	44.9	47.15	3008
NND7108	579177	6682961	339.7	70.4	DDH	47.6	50.2	873
NND7108	579177	6682961	339.7	70.4	DDH	55.4	55.8	970
NND7108	579177	6682961	339.7	70.4	DDH	56.7	57.8	584
NND7108	579177	6682961	339.7	70.4	DDH	58.1	59	461
NND7108	579177	6682961	339.7	70.4	DDH	59.35	65.3	293
NND7108	579177	6682961	339.7	70.4	DDH	66.3	66.65	184

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NND7111	579283	6682896	337.2	54.5	DDH	47.6	50.2	320
NND7111	579283	6682896	337.2	54.5	DDH	50.65	53	736
NND7115	579420	6682818	332.5	46.5	DDH	38.75	38.95	156
NND7115	579420	6682818	332.5	46.5	DDH	39.1	39.25	152
NND7115	579420	6682818	332.5	46.5	DDH	39.5	42.5	1045
NND7122	579668	6682672	331.6	46.8	DDH	39	40.9	651
NND7127	579833	6682571	332.5	46	DDH	37.5	39.1	1359
NND7130	579055	6682993	346.4	74	DDH	61.25	62.2	330
NND7130	579055	6682993	346.4	74	DDH	63.45	64.55	482
NND7130	579055	6682993	346.4	74	DDH	65.85	67	766
NND7130	579055	6682993	346.4	74	DDH	68.6	69.4	530
NND7130	579055	6682993	346.4	74	DDH	69.75	70.5	403
NND7130	579055	6682993	346.4	74	DDH	70.65	71	543
NND7138	579588	6682668	331.7	46.8	DDH	38.8	39.1	165
NND7138	579588	6682668	331.7	46.8	DDH	39.45	39.7	215
NND7138	579588	6682668	331.7	46.8	DDH	40.5	40.7	496
NND7138	579588	6682668	331.7	46.8	DDH	41.15	43.6	596
NND7145	579077	6682921	339.4	69	DDH	42.5	43.75	1083
NND7145	579077	6682921	339.4	69	DDH	47.3	49.7	618
NND7145	579077	6682921	339.4	69	DDH	49.8	50.2	554
NND7145	579077	6682921	339.4	69	DDH	51.85	52.18	1556
NND7145	579077	6682921	339.4	69	DDH	63.35	64.05	567
NND7145	579077	6682921	339.4	69	DDH	66.2	66.5	147
NND7145	579077	6682921	339.4	69	DDH	66.9	67.2	101
NND7149	579217	6682833	338.9	60	DDH	41.5	41.65	671
NND7149	579217	6682833	338.9	60	DDH	41.95	42.15	376
NND7149	579217	6682833	338.9	60	DDH	42.5	43.95	1657
NND7149	579217	6682833	338.9	60	DDH	44.1	44.8	207
NND7153	579357	6682747	334.4	51	DDH	41	43.35	802
NND7157	579488	6682666	332.4	51	DDH	38.7	40.4	494
NND7157	579488	6682666	332.4	51	DDH	40.8	43.65	1980
NND7157	579488	6682666	332.4	51	DDH	43.9	44.35	305
NND7161	579664	6682565	332.5	48.3	DDH	38.9	39.3	425
NND7161	579664	6682565	332.5	48.3	DDH	39.5	41.45	1384

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NND7177	579182	6682727	339.3	54.2	DDH	43.7	46.6	1047
NND7177	579182	6682727	339.3	54.2	DDH	46.7	47.5	164
NND7181	579316	6682648	334.9	52.4	DDH	40.9	45.1	1218
NND7184	579421	6682586	333.8	51.1	DDH	39.8	44.1	1066
NND7187	579522	6682528	333.7	49.8	DDH	40.65	41.4	576
NND7187	579522	6682528	333.7	49.8	DDH	42	42.3	320
NND7187	579522	6682528	333.7	49.8	DDH	42.7	45.3	532
NND7196	579445	6682511	334.6	51.3	DDH	41.1	44.8	559
NND7199	578960	6682748	337.1	49.5	DDH	40	40.2	1003
NND7199	578960	6682748	337.1	49.5	DDH	40.4	40.8	4315
NND7199	578960	6682748	337.1	49.5	DDH	41.4	42.2	1533
NND7199	578960	6682748	337.1	49.5	DDH	42.5	43	311
NND7199	578960	6682748	337.1	49.5	DDH	43.25	43.4	1592
NND7199	578960	6682748	337.1	49.5	DDH	45.25	46.7	263
NND7199	578960	6682748	337.1	49.5	DDH	47	48.85	254
NND7205	579160	6682626	336.0	50	DDH	40.55	42.5	2492
NND7205	579160	6682626	336.0	50	DDH	42.8	43.65	467
NND7207	579235	6682587	335.9	50	DDH	39.5	40.6	316
NND7207	579235	6682587	335.9	50	DDH	41	44.3	900
NND7217	579315	6682481	338.1	55.8	DDH	43.65	44.4	1311
NND7217	579315	6682481	338.1	55.8	DDH	44.8	46.4	435
NND7220	578899	6682662	338.8	51	DDH	43.25	43.45	144
NND7220	578899	6682662	338.8	51	DDH	43.75	45.05	944
NND7220	578899	6682662	338.8	51	DDH	46.9	47.3	265
NND7225	579069	6682561	337.5	49.8	DDH	42.9	46.2	2893
NND7228	579173	6682498	338.7	54.1	DDH	45.6	46.6	635
NND7228	579173	6682498	338.7	54.1	DDH	46.8	49.3	1674
NND7228	579173	6682498	338.7	54.1	DDH	49.6	50.45	534
NND7228	579173	6682498	338.7	54.1	DDH	50.7	51.45	344
NND7233	579346	6682395	338.7	54.2	DDH	45.6	46	114
NND7233	579346	6682395	338.7	54.2	DDH	46.5	50.3	723
NND7237	578962	6682568	340.0	49.6	DDH	44.2	45.9	441
NND7243	578910	6682542	339.9	54.3	DDH	42.7	44.7	782
NND7248	579291	6682303	341.7	56	DDH	47.75	48	331

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NND7248	579291	6682303	341.7	56	DDH	48.2	50.5	502
NND7250	579026	6682431	341.4	58	DDH	46.65	48.9	1177
NND7257	578944	6682397	344.4	60	DDH	47.7	51.5	1491
NND7261	579065	6682305	343.3	57	DDH	48.8	49.7	499
NND7261	579065	6682305	343.3	57	DDH	50	51.5	351
NND7273	580239	6683078	331.7	48	DDH	37.85	39.05	395
NND7278	580256	6682941	333.7	51	DDH	39.35	41.55	1077
NND7278	580256	6682941	333.7	51	DDH	41.7	42.8	148
NND7278	580256	6682941	333.7	51	DDH	42.9	43.7	138
NND7278	580256	6682941	333.7	51	DDH	44	44.15	679
NND7278	580256	6682941	333.7	51	DDH	44.3	44.6	358
NND7288	578840	6682583	337.3	54.3	DDH	38.6	38.8	544
NND7288	578840	6682583	337.3	54.3	DDH	39.05	40.2	1062
NND7288	578840	6682583	337.3	54.3	DDH	42.8	43.2	104
NND7288	578840	6682583	337.3	54.3	DDH	44.65	45	210
NND7293	578644	6682563	334.3	55.5	DDH	35.9	36	1033
NND7293	578644	6682563	334.3	55.5	DDH	36.05	37.75	2102
NND7293	578644	6682563	334.3	55.5	DDH	38	38.25	842
NND7293	578644	6682563	334.3	55.5	DDH	38.6	41.15	341
NND7293	578644	6682563	334.3	55.5	DDH	42.35	43.3	114
NND7293	578644	6682563	334.3	55.5	DDH	44.6	44.85	144
NND7293	578644	6682563	334.3	55.5	DDH	45.05	45.25	147
NND7293	578644	6682563	334.3	55.5	DDH	45.5	45.75	213
NND7293	578644	6682563	334.3	55.5	DDH	52.8	53.3	132
NND7297	578821	6682463	339.0	51	DDH	42.7	48.5	2184
NND7302	578895	6682377	343.1	57	DDH	48.05	50.9	2772
NND7302	578895	6682377	343.1	57	DDH	51.2	51.7	307
NND7304	578773	6682374	339.6	52.8	DDH	44.9	49.8	2417
NND7304	578773	6682374	339.6	52.8	DDH	50.3	50.6	384
NND7304	578773	6682374	339.6	52.8	DDH	51.6	52	196
NND7311	578884	6682251	338.3	48	DDH	44	47.6	906
NND7312	578806	6682238	336.1	48	DDH	38.9	42.2	1770
NND7314	578688	6682422	335.5	48.3	DDH	39.1	41.4	3095
NND7314	578688	6682422	335.5	48.3	DDH	41.6	41.8	108

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NND7317	578552	6682503	333.5	46.8	DDH	35.4	39	1088
NND7321	579428	6684500	345.0	63.4	DDH	51.2	51.85	356
NND7321	579428	6684500	345.0	63.4	DDH	52.05	52.7	157
NND7321	579428	6684500	345.0	63.4	DDH	54.2	55.1	349
NND7321	579428	6684500	345.0	63.4	DDH	55.45	56.35	291
NND7321	579428	6684500	345.0	63.4	DDH	57.05	58.95	191
NND7321	579428	6684500	345.0	63.4	DDH	59.15	60.2	540
NND7321	579428	6684500	345.0	63.4	DDH	61	62.4	122
NND7322	579325	6684430	340.5	56.5	DDH	46.35	46.55	481
NND7322	579325	6684430	340.5	56.5	DDH	47	48.1	602
NND7322	579325	6684430	340.5	56.5	DDH	48.4	49.3	314
NND7324	579274	6684311	340.4	57	DDH	47	48.6	358
NND7330	578622	6684107	341.7	54.3	DDH	39.7	40.1	803
NND7330	578622	6684107	341.7	54.3	DDH	43.8	44.7	294
NND7330	578622	6684107	341.7	54.3	DDH	45.3	46.05	228
NND7330	578622	6684107	341.7	54.3	DDH	51.3	52.8	130
NND7332	578704	6683939	340.1	50.5	DDH	37.25	38.3	304
NND7334	578839	6683633	339.1	48.3	DDH	38.2	40	782
NND7334	578839	6683633	339.1	48.3	DDH	43.7	44.2	262
NND7334	578839	6683633	339.1	48.3	DDH	44.3	45.3	325
NND7339	581863	6683388	341.5	57	DDH	41.65	42.9	402
NND7342	581698	6683341	339.1	56	DDH	47.3	48	2134
NND7342	581698	6683341	339.1	56	DDH	48.5	50.6	527
NND7342	581698	6683341	339.1	56	DDH	51.2	51.5	301
NND7342	581698	6683341	339.1	56	DDH	51.8	52.9	347
NND7342	581698	6683341	339.1	56	DDH	53.6	53.8	351
NND7343	581432	6683393	333.7	48.4	DDH	34.5	35.5	1512
NND7349	581468	6683236	338.0	54.1	DDH	35.6	36.1	131
NND7349	581468	6683236	338.0	54.1	DDH	43.6	44	337
NND7349	581468	6683236	338.0	54.1	DDH	44.1	45.1	1945
NND7351	581194	6683289	337.4	51.3	DDH	39.2	45	198
NND7357	578747	6682273	337.5	51.1	DDH	42.4	43.4	1568
NND7357	578747	6682273	337.5	51.1	DDH	43.6	48.9	1933
NND7357	578747	6682273	337.5	51.1	DDH	49.3	49.6	200

Hole ID	Easting	Northing	RL	Depth	Type ¹	From	To	Grade
NND7357	578747	6682273	337.5	51.1	DDH	50	50.35	124
NND7361	578505	6682446	336.0	48.1	DDH	38.6	41.2	801
NND7365	578299	6682536	339.9	48.1	DDH	39.3	44	1344
NND7365	578299	6682536	339.9	48.1	DDH	44.15	46.6	257
NND7368	578707	6682178	332.4	48.1	DDH	35.5	37.3	930
NND7368	578707	6682178	332.4	48.1	DDH	38	38.3	154
NND7371	578534	6682277	347.1	66	DDH	49.05	51.5	2441
NND7376	578260	6682443	345.7	60.5	DDH	46.4	49.4	1447
NND7376	578260	6682443	345.7	60.5	DDH	50	50.3	192