

8 November 2017

## Discovery of Exceptional High-Grade Shallow Mineralisation at Celtic Tiger Transforms Outlook for Kildare Zinc Project

*Thick high-grade mineralisation including hits up to 25.0% Zn+Pb within 200m of surface at Celtic Tiger, confirming potential for shallower mineralisation across the project*

### Key Points:

- Multiple zones of high-grade zinc mineralisation intersected in the shallow regions of the Celtic Tiger and McGregor prospects in holes Z\_4069\_006, \_007 and \_008 including:
  - 23.95m @ 8.0% Zn+Pb from 166.0m (Celtic Tiger, 007), including:
    - 8.70m @ 12.6% Zn+Pb from 166.0m;
    - 1.05m @ 25.0% Zn+Pb from 177.4m; and
    - 1.55m @ 10.6% Zn+Pb from 184.8m;
  - 3.70m @ 9.16% Zn+Pb from 81.5m (Celtic Tiger, 007)
  - 5.45m @ 13.4% Zn+Pb from 130.2m (Celtic Tiger, 007)
  - 2.60m @ 15.2% Zn+Pb from 156.5m (Celtic Tiger, 007)
  - 3.11m @ 19.6% Zn+Pb from 205.40m (McGregor, 008)\*
  - 2.20m @ 12.1% Zn+Pb from 224.51m (McGregor, 008)\*
  - 11.50m @ 6.1% Zn+Pb from 238m (McGregor, 006)\*
  - 7.97m @ 7.1% Zn+Pb from 266.90m (McGregor, 008)\*
- Base of Reef mineralisation extended further at McGregor, including:
  - 5.36m @ 11.1% Zn+Pb from 366.70m (McGregor, 006)\*
  - 11.19m @ 10.3% Zn+Pb from 423.22m (McGregor, 008, previously reported)\*
- The results confirm the exciting potential of the Celtic Tiger Discovery, where drilling continues.
- Multiple zones of high-grade mineralisation encountered within 200m of the surface, enhancing the prospectivity of the Kildare Project as a whole.
- Potential to upgrade the current Inferred Resource, which stands at **5.2Mt @ 8.6% combined Zn+Pb**.

*\*Calculated True depths and thicknesses*

ZMI's Managing Director, Peter van der Borgh, said: *"These results are a clear game-changer for ZMI and the future of the Kildare Zinc Project. The discovery of thick, high-grade zinc mineralisation within a couple of hundred metres of the surface at both McGregor and Celtic Tiger will have a number of positive impacts for the project.*

*"From an exploration perspective, this means cheaper and quicker drilling for shallower targets, while the presence of shallower, more accessible mineralisation will obviously translate into improved economics when we undertake future financial modelling of the project.*

*"It also brings into play more than 4km of similar geology along the Western Margin of the Graben, as well as similar structural settings that we are identifying elsewhere within the project and beyond. And then of course there's proof of concept for our exploration model, which also has widespread application.*

*"The style of mineralisation at Celtic Tiger has many similarities to the Base of Reef mineralisation at McGregor, and as a consequence, I believe we can be thinking of a substantial Exploration Target at Celtic Tiger which will complement our existing Inferred Mineral Resource at McGregor and Shamrock. In the meantime, the extensions to the Base of Reef mineralisation at McGregor point clearly to the likelihood of an increase in the maiden Inferred Resource.*

*"Lastly, I'd like to thank Dave Blaney and his team at BRG for their expertise and hard work in helping us deliver this terrific result."*

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European base metals explorer Zinc of Ireland NL (ASX: ZMI – "ZMI" or "the Company") is pleased to advise that recent diamond drilling at its 100%-owned **Kildare MVT Zinc Project** in Ireland (Figure 1) has confirmed multiple zones of exceptionally high-grade zinc mineralisation in the shallower regions of the McGregor and newly discovered Celtic Tiger prospects.

The highly significant assay results – from recently completed diamond drill holes Z\_4069\_006 (006), Z\_4069\_007 (007) and Z\_4069\_008 (008) – clearly demonstrate the potential for shallower mineralisation at Kildare, transforming the outlook for the Project and significantly upgrading its discovery and growth potential.

The reported drill holes each intersected multiple zones of mineralisation relating to faulting, brecciation and veining, including zones of massive sulphide development.

The results at Celtic Tiger, which is located ~1km to the west of the main Resource at McGregor, comprise multiple zones of mineralisation between 81.5m and 200m below surface, including **5.45m @ 13.4% Zn+Pb from 130.2m, 2.60m @ 15.2% Zn+Pb from 156.5m, and 8.70m @ 12.6% Zn+Pb from 166.0m.**

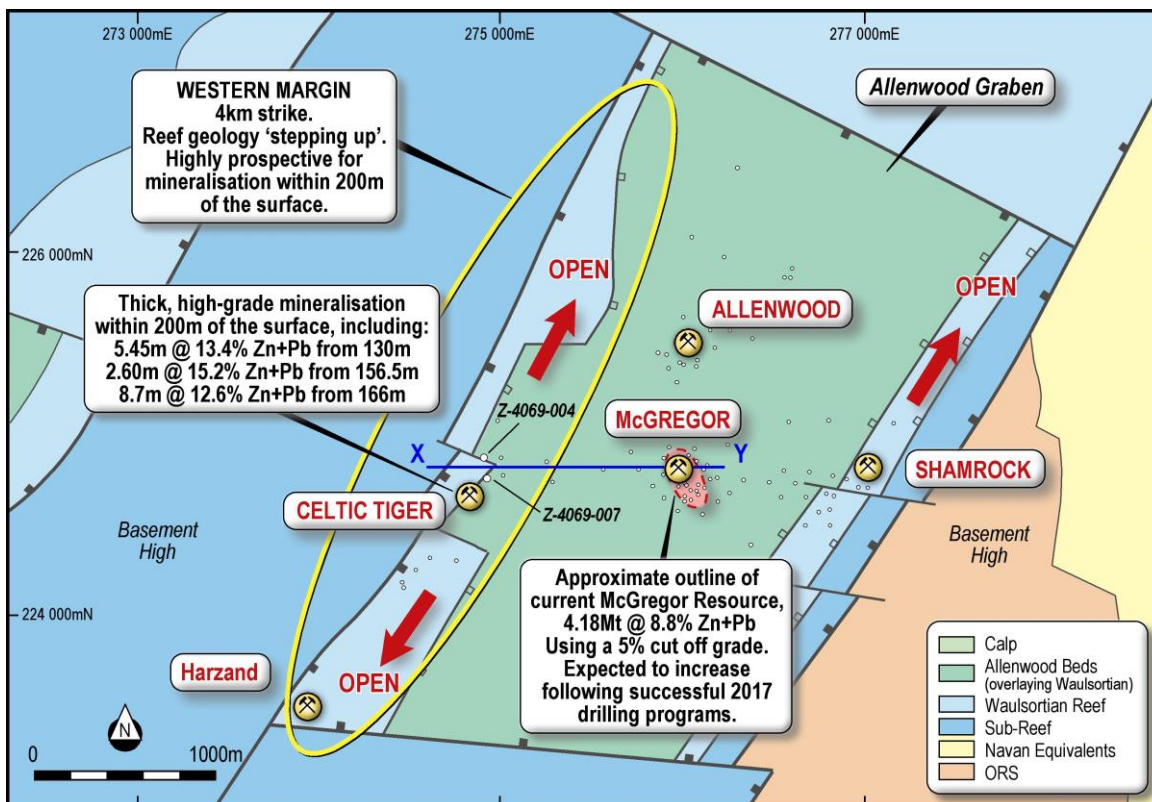


Figure 1. Geology plan of the Allenwood Graben. Note the cross-section line X-Y displayed in Figure 2.

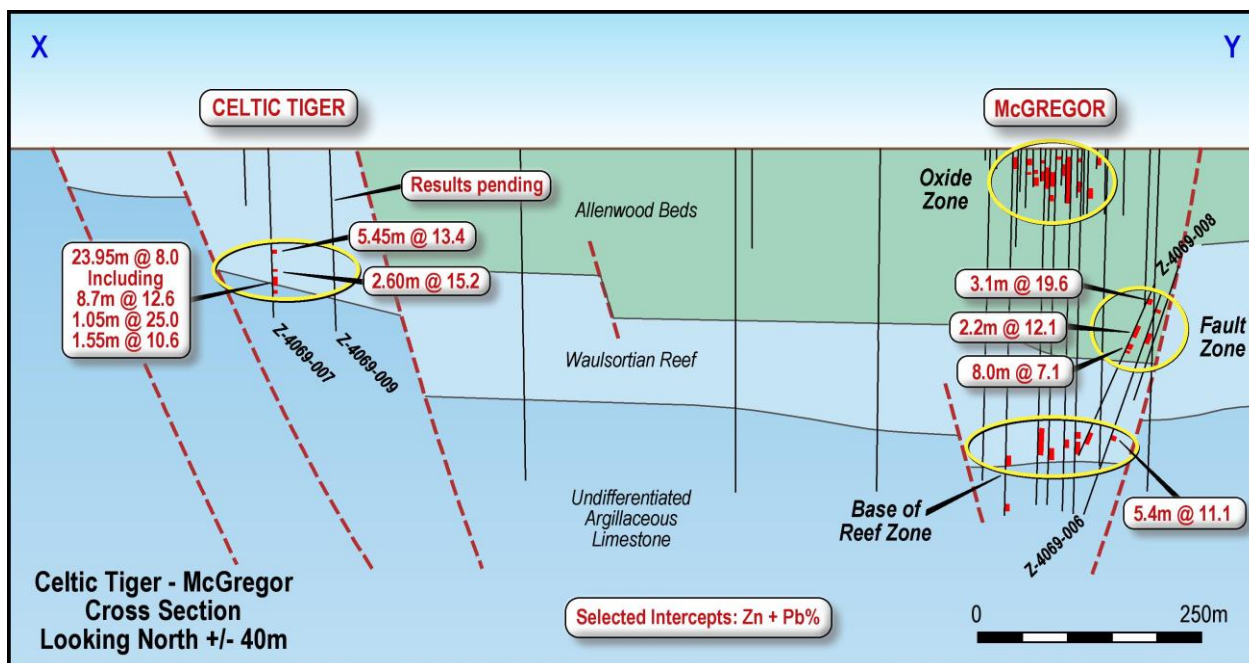


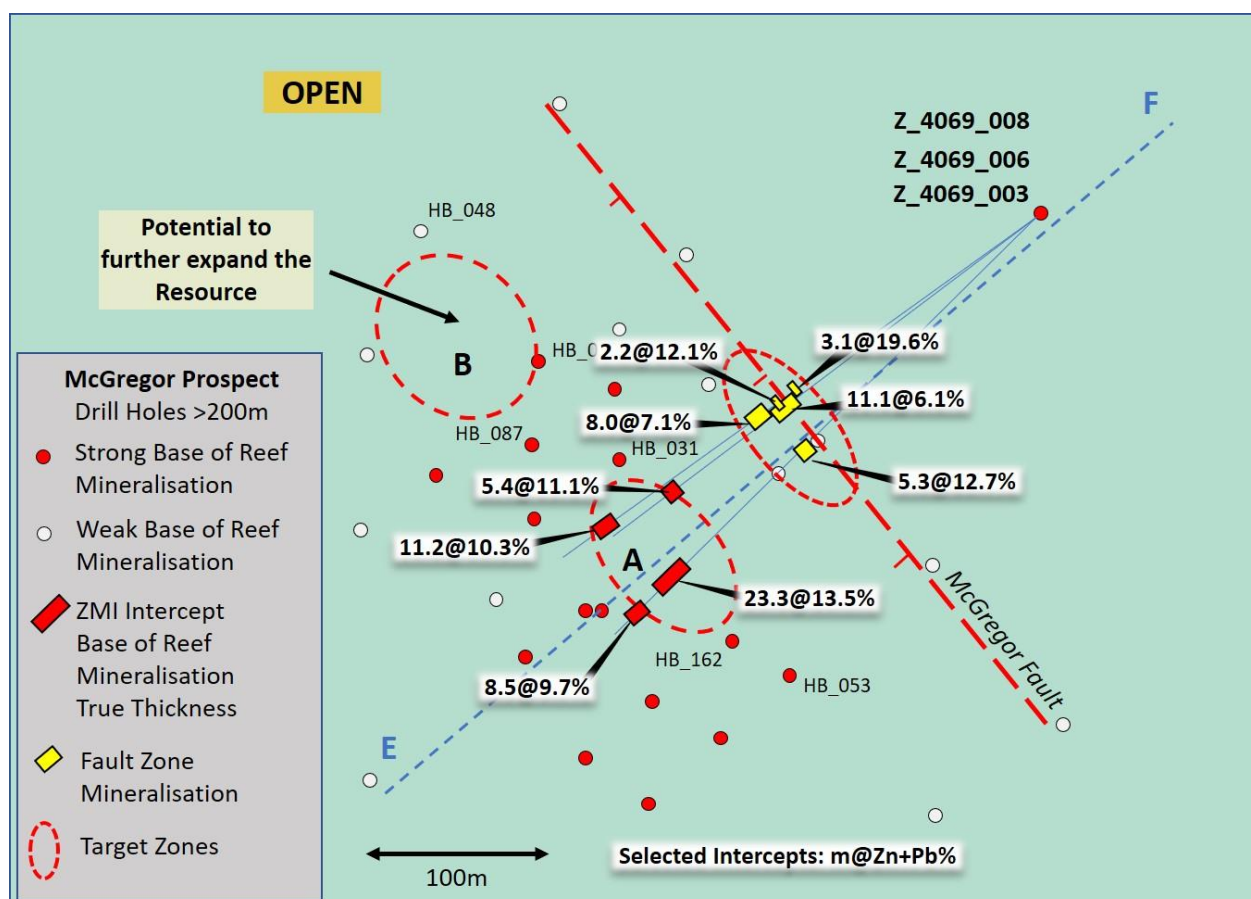
Figure 2. Cross-section from Celtic Tiger to McGregor, highlighting selected intercepts reported in this announcement. Note the Waulsortian Reef stepping up along the western margin of the graben.

The assays from McGregor, including **3.11m @ 19.6% Zn+Pb from 205.4m (008) and 11.35m @ 6.1% Zn+Pb from 238m (006)**, confirm that shallow mineralisation has developed adjacent to the recently discovered McGregor Fault. These shallower intercepts, combined with the successful extensions of the deeper Base of Reef mineralisation reported previously, mean that the Phase 2 and 3 drilling programs are highly likely to have a positive impact on the current JORC Inferred Resource, which comprises **5.2Mt @ 8.6% Zn+Pb**.

### Phase 3 Drilling Update

Phase 3 of ZMI’s diamond drilling is a multi-pronged program designed to extend the Base of Reef mineralisation at McGregor, and follow up on the Company’s previous intercepts of shallow mineralisation at McGregor and Celtic Tiger.

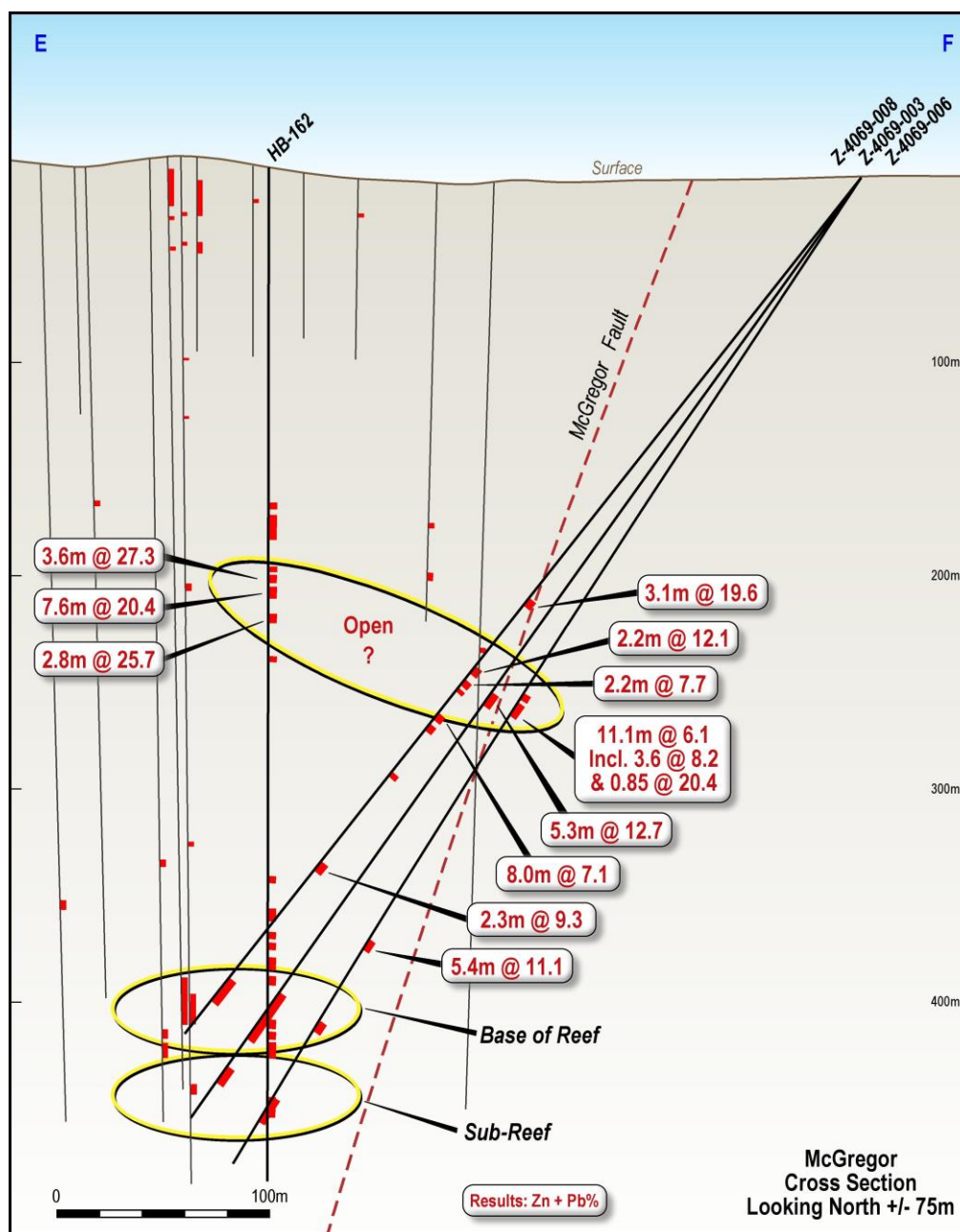
Two holes, Z\_4069\_006 and \_008, were drilled at McGregor. The results from the Base of Reef intercept in Hole 008, comprising **11.19m @ 10.3% Zn+Pb from 423.22m**, were reported on 16<sup>th</sup> October and the remaining assays from hole 008, and those from hole 006, are reported in this announcement.



**Figure 3: Plan of the McGregor Prospect showing the location of drill hole collars, projected hole traces and intercepts. Note the E-F cross-section line shown in Figure 4.**



Of particular significance are the shallower results that appear to be spatially related to the recently discovered McGregor Fault, including **3.11m @ 19.6% Zn+Pb from 205.4m** below surface. Several other zones were intersected within 250m of surface in both drill holes (Figure 4).



**Figure 4. Cross-section through the McGregor Prospect, highlighting the intersected zones of fault related mineralisation in ZMI's recent drill holes, and the potential correlation with zones of mineralisation in historical hole HB162.**

Three contiguous holes have now intersected this mineralisation, which may correlate with high-grade mineralisation in historical hole HB162, some 100m to the south (Figure 4).

Drill hole 006 also intersected mineralisation comprising **5.36m @ 11.1% Zn+Pb from 366.70m** towards the Base of Reef. The Base of Reef contact was faulted in this hole, and a portion of mineralisation is likely to have been displaced.

Drill hole Z\_4069\_007 at the Celtic Tiger prospect was drilled ~100m south of hole Z\_4069\_004 (Figure 1) reported in July, which intersected several zones of mineralisation including **2.85m @ 20.9% Zn+Pb from 193.90m**.

The latest results, including **5.45m @ 13.4% Zn+Pb from 130.2m, 2.60m @ 15.2% Zn+Pb from 156.5m, and 8.70m @ 12.6% Zn+Pb from 166.0m**, are highly encouraging and confirm that the Kildare Project hosts significant zinc-lead mineralisation within 200m of the surface.

The Celtic Tiger mineralisation comprises zones of white matrix breccia (WMB) and calcite veining with abundant tan sphalerite (ZnS), marcasite (FeS<sub>2</sub>), and occasional galena (PbS) towards the base and at the base of the Waulsortian Reef. Replacement of breccia clasts is common in many of the more mineralised horizons.

As such, the mineralisation in Z\_4069\_007 resembles the mineralisation observed towards and at the Base of Reef horizon at McGregor, which hosts a significant component of the 5.2Mt Kildare Inferred Resource. If the geometry of the mineralisation is also similar (i.e. sub-horizontal), it can be assumed that the intercepts in this vertical hole are close to true thickness, although this has yet to be confirmed.

**Table 1. Drill collar details relating to new drill hole information in this report. Irish Grid 65.**

HoleID	mE	mN	Dip	Azimuth	RL	Total Depth (m)
Z_4069_006	257253	224938	-58.5	230	78	583.5
Z_4069_007	274915	224872	-90	360	75	277.4
Z_4069_008	276253	224938	-53.7	233	78	575.1

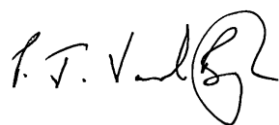
## Looking ahead

Next steps for the Kildare Zinc Project include:

- Ongoing diamond drilling at Celtic Tiger, with a further 2 or 3 holes to be completed before Christmas.
- Completion of an updated Mineral Resource estimate for the Kildare Project plus a maiden Exploration Target for the Celtic Tiger Prospect – planned for Q1 2018.
- Planning for the Phase 4 drilling program at Kildare, aiming to commence in Q1 2018, building on the significant recent breakthroughs achieved in the Company’s geological understanding of the broader potential of the project area.

The Company looks forward to updating shareholders as results come to hand.

Yours faithfully,

A handwritten signature in black ink, appearing to read 'P. J. Van der Borgh', with a large, stylized flourish at the end.

**Peter van der Borgh**  
Managing Director  
Zinc of Ireland NL

**Investor Inquiries:**

Peter van der Borgh  
Zinc of Ireland NL  
Tel: +44 7881 027 036  
Email: [peter@zincofireland.com](mailto:peter@zincofireland.com)

**Media Inquiries:**

Nicholas Read  
Read Corporate  
Tel: +61-8 9388 1474  
Email: [nicholas@readcorporate.com.au](mailto:nicholas@readcorporate.com.au)

**Competent Person Statement**

*The information in this document is based on information compiled by Mr Peter van der Borgh, BSc (Hons, 1<sup>st</sup> Class), a Competent Person who is a Fellow of the Geological Society of London. Mr van der Borgh is a director and shareholder of Zinc of Ireland NL. Mr van der Borgh has sufficient experience, which is relevant to the style of mineralisation and types of deposits under consideration and to the activity which has been undertaken to qualify as a Competent Person as defined in the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code). Mr van der Borgh consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.*

**Disclaimer**

*Certain statements contained in this announcement, including information as to the future financial or operating performance of ZMI and its projects, are forward-looking statements that:*

- *may include, among other things, statements regarding targets, estimates and assumptions in respect of mineral reserves and mineral resources and anticipated grades and recovery rates, production and prices, recovery costs and results, capital expenditures, and are or may be based on assumptions and estimates related to future technical, economic, market, political, social and other conditions;*
- *are necessarily based upon a number of estimates and assumptions that, while considered reasonable by ZMI, are inherently subject to significant technical, business, economic, competitive, political and social uncertainties and contingencies; and,*
- *involve known and unknown risks and uncertainties that could cause actual events or results to differ materially from estimated or anticipated events or results reflected in such forward-looking statements.*

## ADDITIONAL INFORMATION JORC CODE, 2012 EDITION – TABLE 1

The following sections are provided for compliance with requirements for the reporting of exploration results under the JORC Code, 2012 Edition.

### Section 1 Sampling Techniques and Data

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> <li>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</li> <li>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</li> <li>Aspects of the determination of mineralisation that are Material to the Public Report.</li> <li>In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</li> </ul>	<ul style="list-style-type: none"> <li>Sampling is by half core (generally NQ diameter) of mineralised sections only. The entirety of the drill hole has not been sampled and additional samples, if collected, may be reported at a later time.</li> <li>Sampling has occurred within lithological domains and as such does not cross lithological boundaries.</li> <li>Samples are prepared by ALS Loughrea, Co Galway by crushing to 70% passing &lt;2mm with a representative sample then split using a Boyd splitter. The split sample is pulverised to 85% passing &lt;75um. The samples are then assayed by a multi element oxidising digestion with an inductively coupled plasma atomic emission spectroscopy finish (ICP-AES). A selection of samples also have specific gravity (S.G.) measured.</li> </ul>
Drilling techniques	<ul style="list-style-type: none"> <li>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is orientated and if so, by what method, etc).</li> </ul>	<ul style="list-style-type: none"> <li>Diamond drilling, PQ, HQ and NQ sized.</li> <li>Upper portions of the drill holes were triple tubed or tri-coned to increase hole stability.</li> <li>The core was orientated topside using a Reflex ACT tool.</li> </ul>
Drill sample recovery	<ul style="list-style-type: none"> <li>Method of recording and assessing core and chip sample recoveries and results assessed.</li> <li>Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> <li>Whether a relationship exists between</li> </ul>	<ul style="list-style-type: none"> <li>Drill core had recovery lengths and RQD estimated.</li> <li>Triple tubing was used to stabilise the hole.</li> <li>There does not appear to be a relationship between recovery and grade.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<p>sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</p>	
Logging	<ul style="list-style-type: none"> <li>• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> <li>• Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</li> <li>• The total length and percentage of the relevant intersections logged.</li> </ul>	<ul style="list-style-type: none"> <li>• Drill holes have been logged by a competent representative geologist in Ireland. The detailed logging is ongoing and should support addition into a mineral resource estimate at a later date.</li> <li>• A visual estimate of mineral types and amounts and interpreted lithology was completed using a standardised logging template.</li> <li>• Photography of mineralised zones is complete.</li> </ul>
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> <li>• If core, whether cut or sawn and whether quarter, half or all core taken.</li> <li>• If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</li> <li>• For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> <li>• Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</li> <li>• Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</li> <li>• Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul>	<ul style="list-style-type: none"> <li>• Core has been sampled by cutting in half before lab preparation.</li> <li>• The sample preparation is considered "industry standard" for this sample type.</li> <li>• A representative selection of submitted samples comprised duplicates, blanks and standards which were unbeknownst to the assaying laboratory. The laboratory also conducted internal QAQC checks.</li> <li>• Fields duplicates, blanks and standards for the submitted assays have all surpassed internal and ZMI QAQC standards.</li> </ul>
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> <li>• The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</li> <li>• For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</li> <li>• Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</li> </ul>	<ul style="list-style-type: none"> <li>• Samples are assayed by a multi element oxidising digestion with an inductively coupled plasma atomic emission spectroscopy finish (ICP-AES). A selection of samples also have specific gravity (S.G.) measured.</li> <li>• Ore grade analysis for base metals and associated elements by ICPAES, following a strong oxidizing acid digestion. Elements (low reporting limit/upper limit) –units are % unless indicated otherwise: Ag (1/1500 ppm (µg/g)), As (0.005/30.0), Bi (0.005/30.00), Ca (0.01/50.0), Cd (0.001/10.0), Co (0.001/20.0), Cu (0.005/40.0), Fe (0.01/100.0), Hg (8/10000 ppm (µg/g)), Mg (0.01/50.0), Mn (0.005/50.0), Mo (0.001/10.0), Ni (0.001/30.0), P (0.01/20.0), Pb (0.01/30.0), S (0.05/50.0), Sb (0.005/100.0), Ti (0.005/1.0), Zn (0.01/100.0).</li> <li>• Internal QAQC results all appear within limits.</li> <li>• Lab-produced QAQC results all appear within limits.</li> </ul>
Verification of sampling and assaying	<ul style="list-style-type: none"> <li>• The verification of significant intersections by either independent or alternative company personnel.</li> <li>• The use of twinned holes.</li> <li>• Documentation of primary data, data</li> </ul>	<ul style="list-style-type: none"> <li>• Drill hole data is compiled digitally by company representatives.</li> <li>• Samples are yet to be submitted to an umpire laboratory for check analysis.</li> <li>• Holes were not twinned.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p>entry procedures, data verification, data storage (physical and electronic) protocols.</p> <ul style="list-style-type: none"> <li>Discuss any adjustment to assay data.</li> </ul>	<ul style="list-style-type: none"> <li>Assays have been adjusted to represent weighted averages over 1m.</li> <li>Visual mineralisation has been verified by several company representatives.</li> </ul>
Location of data points	<ul style="list-style-type: none"> <li>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</li> <li>Specification of the grid system used.</li> <li>Quality and adequacy of topographic control.</li> </ul>	<ul style="list-style-type: none"> <li>Initial surveys are by hand-held GPS in Irish Grid 65.</li> <li>Collars have been surveyed either by handheld GPS or by a differential GPS: Trimble GPS6000 (RTK GPS accurate to 5mm)</li> <li>Downhole surveys are by Relfex EZ-TRAC and are displayed in Appendix 2.</li> <li>Location of the collar and downhole information is considered appropriate for this stage of exploration.</li> </ul>
Data spacing and distribution	<ul style="list-style-type: none"> <li>Data spacing for reporting of Exploration Results.</li> <li>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</li> <li>Whether sample compositing has been applied.</li> </ul>	<ul style="list-style-type: none"> <li>Drill collars are not at a standard data spacing but are placed to intersect maximum metal grades (see plan view maps above).</li> <li>Data spacing for the results contained in this report are not appropriate for resource estimation alone.</li> <li>Sample compositing has not been applied. Assay compositing (combining individual assays into one reportable length) has however occurred.</li> <li>The results from hole Z_4069_006 and Z_4069_08 are expected to be used in addition to historical data to support a mineral resource estimate but this is as yet to be confirmed.</li> </ul>
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> <li>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</li> <li>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</li> </ul>	<ul style="list-style-type: none"> <li>Calculated vertical depths and thicknesses have been quoted for Z_4069_006 and _008 so as to alleviate any undue bias of drilling results.</li> <li>Calculated vertical thicknesses have not been applied to Z_4069_007, as the orientation of mineralisation is not yet known.</li> <li>Vertical thickness has been calculated using an average of the top and bottom drillhole surveys. This may cause minor under- or over-estimation of the true thickness but this is not expected to be material.</li> <li>Minor rounding due to thickness calculation may have occurred but this is not expected to be material.</li> <li>Mineralisation appears to be horizontal/sub-horizontal.</li> </ul>
Sample security	<ul style="list-style-type: none"> <li>The measures taken to ensure sample security.</li> </ul>	<ul style="list-style-type: none"> <li>Samples were under the custody of company representatives in-country until delivery to the lab.</li> </ul>
Audits or reviews	<ul style="list-style-type: none"> <li>The results of any audits or reviews of sampling techniques and data.</li> </ul>	<ul style="list-style-type: none"> <li>No audits or reviews have taken place.</li> </ul>

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> <li>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</li> <li>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</li> </ul>	<ul style="list-style-type: none"> <li>The Kildare Project is comprised of 7 Licenses, namely PL890, PL3846, PL3866, PL4069, PL4070, PL4072 and PL4073.</li> <li>All tenements are 100% owned by Raptor Resources, a subsidiary of Zinc of Ireland NL.</li> <li>No historical, wilderness or national parks are known to infringe significantly on the tenure.</li> </ul>
Exploration done by other parties	<ul style="list-style-type: none"> <li>Acknowledgment and appraisal of exploration by other parties.</li> </ul>	<ul style="list-style-type: none"> <li>Historical exploration is outlined in GXN Announcement dated 17<sup>th</sup> March 2016 and associated annexes.</li> </ul>
Geology	<ul style="list-style-type: none"> <li>Deposit type, geological setting and style of mineralisation.</li> </ul>	<ul style="list-style-type: none"> <li>The Kildare Project is situated approximately 2km NW of the Lower Paleozoic Kildare Inlier on a northeast-southwest trending reverse fault. Local geology consists of sediments conformably overlying Carboniferous Waulsortian Mudbank. This mudbank overlies a thick succession of carbonates and limestones atop basement volcanics.</li> <li>The area is considered prospective for breccia-hosted Fe-Zn-Pb deposits (a Mississippi Valley-type mineralisation style).</li> </ul>
Drill hole Information	<ul style="list-style-type: none"> <li>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>easting and northing of the drill hole collar</li> <li>elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>dip and azimuth of the hole</li> <li>down hole length and interception depth</li> <li>hole length.</li> </ul> </li> <li>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</li> </ul>	<ul style="list-style-type: none"> <li>Z_4069_006: 275,253mE, 224,938mN, 78mAOD, -58.5° (top), -63.3 (bottom) dip, 230° azimuth, total depth 583.5m.</li> <li>Z_4069_007: 274,915mE, 224,872mN, 75mAOD, -90° dip, 360° azimuth, total depth 277.4m</li> <li>Z_4069_008: 276,253mE, 224,938mN, 78mAOD, -53.7° (top), -58.7 (bottom) dip, 233° azimuth, total depth 575.1m.</li> </ul>
Data aggregation methods	<ul style="list-style-type: none"> <li>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.</li> <li>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used</li> </ul>	<ul style="list-style-type: none"> <li>No minimum cut-off grade has been applied to the reported intersections.</li> <li>Assays have been weighted to 1m intervals.</li> <li>Internal dilution may occur.</li> <li>Reported intersections reflect the highest grade and/or the widest mineralised intersections</li> <li>No metal equivalents have been quoted.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p>for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</p> <ul style="list-style-type: none"> <li>The assumptions used for any reporting of metal equivalent values should be clearly stated.</li> </ul>	
Relationship between mineralisation widths and intercept lengths	<ul style="list-style-type: none"> <li>These relationships are particularly important in the reporting of Exploration Results.</li> <li>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> <li>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').</li> </ul>	<ul style="list-style-type: none"> <li>Relationship between true mineralisation width and reported intercepts appear to be either perpendicular or close to for 90° drill holes.</li> <li>Angled holes have a lower angle of intersection and as such true vertical widths have been calculated.</li> </ul>
Diagrams	<ul style="list-style-type: none"> <li>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</li> </ul>	<ul style="list-style-type: none"> <li>Plans and sections appear throughout this release.</li> </ul>
Balanced reporting	<ul style="list-style-type: none"> <li>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</li> </ul>	<ul style="list-style-type: none"> <li>All drill holes with assays received have been reported in Appendix 1.</li> <li>Reported intervals are those which are of the highest grade and/or greatest width.</li> </ul>
Other substantive exploration data	<ul style="list-style-type: none"> <li>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</li> </ul>	<ul style="list-style-type: none"> <li>N/A</li> </ul>
Further work	<ul style="list-style-type: none"> <li>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</li> <li>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</li> </ul>	<ul style="list-style-type: none"> <li>As summarised at the end of the announcement.</li> </ul>

## APPENDIX 1: Assay Results

Note: All depths are downhole

Hole ID	Sample No.	From_m	To_m	Interval_m	Ag_ppm	Zn_%	Pb_%
Z-4069-006	50245	243.2	244.2	1	<1	0.01	<0.01
Z-4069-006	50246	244.2	244.4	0.2	<1	0.43	0.01
Z-4069-006	50247	244.4	245	0.6	<1	1.68	0.01
Z-4069-006	50248	245	245.45	0.45	<1	2.9	0.05
Z-4069-006	50249	245.45	246.25	0.8	7	15.3	0.28
Z-4069-006	50250	246.25	247	0.75	2	0.03	<0.01
Z-4069-006	50251	277.5	278.7	1.2	2	0.06	<0.01
Z-4069-006	50252	278.7	279.7	1	2	0.37	0.06
Z-4069-006	50253	279.7	280.4	0.7	2	0.10	<0.01
Z-4069-006	50254	280.4	281	0.6	5	6.50	1.21
Z-4069-006	50255	281	282.15	1.15	2	0.28	0.03
Z-4069-006	50256	282.15	282.75	0.6	10	14.75	8.64
Z-4069-006	50258	282.75	283.05	0.3	3	0.91	0.25
Z-4069-006	50259	283.05	283.5	0.45	2	2.95	0.71
Z-4069-006	50260	283.5	284	0.5	6	11.45	3.93
Z-4069-006	50261	284	284.5	0.5	5	6.47	3.49
Z-4069-006	50262	284.5	286	1.5	<1	0.51	0.2
Z-4069-006	50264	286	287	1	1	0.81	0.24
Z-4069-006	50265	287	288	1	<1	1.10	0.04
Z-4069-006	50266	288	288.4	0.4	3	9.38	2.01
Z-4069-006	50267	288.4	289	0.6	8	24.3	2.13
Z-4069-006	50268	289	290	1	<1	0.12	0.02
Z-4069-006	50269	290	290.7	0.7	3	2.89	0.34
Z-4069-006	50270	290.7	291.25	0.55	3	2.39	0.29
Z-4069-006	50271	291.25	291.5	0.25	3	19.2	1.41
Z-4069-006	50272	291.5	292.35	0.85	4	4.63	0.24
Z-4069-006	50273	292.35	293.25	0.9	<1	0.65	0.11
Z-4069-006	50274	293.25	293.75	0.5	11	16.55	3.58
Z-4069-006	50275	293.75	294.75	1	4	2.72	0.11
Z-4069-006	50277	304.9	305.75	0.85	5	0.76	0.03
Z-4069-006	50278	305.75	306.9	1.15	4	4.21	0.04
Z-4069-006	50279	306.9	308.3	1.4	<1	0.03	<0.01
Z-4069-006	50281	308.3	309.1	0.8	2	3.05	0.04
Z-4069-006	50282	309.1	310.4	1.3	3	7.36	0.22
Z-4069-006	50283	310.4	311.5	1.1	6	4.46	0.03
Z-4069-006	50284	311.5	312.5	1	<1	1.35	0.01
Z-4069-006	50285	312.5	313.5	1	<1	0.20	0.01



Z-4069-006	50286	313.5	314.2	0.7	<1	1.63	0.03
Z-4069-006	50287	314.2	314.6	0.4	2	2.40	0.47
Z-4069-006	50288	314.6	315.6	1	<1	1.48	0.02
Z-4069-006	50289	315.6	316.1	0.5	<1	1.78	0.01
Z-4069-006	50290	316.1	317.6	1.5	<1	4.21	0.15
Z-4069-006	50291	317.6	319.1	1.5	1	3.42	0.08
Z-4069-006	50292	319.1	319.5	0.4	<1	3.35	0.19
Z-4069-006	50293	319.5	320.5	1	2	0.48	0.02
Z-4069-006	50294	362.6	363	0.4	<1	0.11	0.01
Z-4069-006	50295	363	363.4	0.4	6	8.09	0.47
Z-4069-006	50296	363.4	364.5	1.1	<1	0.52	0.02
Z-4069-006	50297	391.5	392.4	0.9	1	0.56	0.02
Z-4069-006	50298	392.4	393.4	1	<1	1.21	0.09
Z-4069-006	50299	393.4	394.4	1	1	2.98	0.23
Z-4069-006	50300	394.4	395.95	1.55	2	6.70	0.35
Z-4069-006	50301	395.95	397.05	1.1	<1	2.51	0.13
Z-4069-006	50302	397.05	398.55	1.5	<1	0.97	0.03
Z-4069-006	50303	398.55	399.15	0.6	2	1.29	0.18
Z-4069-006	50304	399.15	399.8	0.65	6	3.34	0.23
Z-4069-006	50305	399.8	400.3	0.5	2	2.01	0.28
Z-4069-006	50306	400.3	401.4	1.1	<1	0.03	0.01
Z-4069-006	50307	401.4	401.65	0.25	<1	0.06	0.16
Z-4069-006	50308	401.65	402.15	0.5	<1	0.01	0.01
Z-4069-006	50309	402.15	402.5	0.35	<1	0.04	0.12
Z-4069-006	50310	402.5	402.95	0.45	<1	0.01	0.01
Z-4069-006	50311	402.95	404.55	1.6	<1	0.54	0.25
Z-4069-006	50312	404.55	405	0.45	<1	0.01	0.04
Z-4069-006	50313	405	405.7	0.7	<1	1.11	0.21
Z-4069-006	50314	405.7	406.2	0.5	1	1.18	0.46
Z-4069-006	50315	406.2	406.7	0.5	<1	0.04	0.01
Z-4069-006	50316	406.7	407.6	0.9	1	0.19	0.21
Z-4069-006	50317	407.6	408.3	0.7	<1	0.01	<0.01
Z-4069-006	50318	408.3	408.8	0.5	<1	0.52	0.08
Z-4069-006	50319	408.8	410.3	1.5	<1	0.04	<0.01
Z-4069-006	50320	410.3	411.1	0.8	<1	0.02	0.01
Z-4069-006	50321	411.1	412	0.9	<1	0.36	0.02
Z-4069-006	50322	412	412.3	0.3	<1	<0.01	<0.01
Z-4069-006	50323	412.3	413.8	1.5	<1	0.01	<0.01
Z-4069-006	50324	413.8	415.1	1.3	<1	0.01	0.05
Z-4069-006	50325	415.1	416.5	1.4	<1	0.01	0.07
Z-4069-006	50326	416.5	417	0.5	1	0.36	0.1
Z-4069-006	50327	417	418.5	1.5	<1	<0.01	<0.01

Z-4069-006	50328	418.5	419	0.5	<1	0.03	0.08
Z-4069-006	50329	419	420	1	<1	0.01	0.01
Z-4069-006	50351	420	421.5	1.5	<1	<0.01	0.06
Z-4069-006	50352	421.5	422.3	0.8	<1	<0.01	0.05
Z-4069-006	50353	422.3	422.75	0.45	3	1.15	0.22
Z-4069-006	50354	422.75	423.45	0.7	<1	0.06	<0.01
Z-4069-006	50355	423.45	424	0.55	3	4.88	0.2
Z-4069-006	50356	424	424.25	0.25	<1	0.02	0.05
Z-4069-006	50357	424.25	424.9	0.65	1	1.87	0.18
Z-4069-006	50359	424.9	425.8	0.9	<1	<0.01	<0.01
Z-4069-006	50360	425.8	426.5	0.7	1	1.89	0.15
Z-4069-006	50361	426.5	427.65	1.15	1	0.75	0.06
Z-4069-006	50362	427.65	428.7	1.05	<1	<0.01	0.02
Z-4069-006	50363	428.7	429.7	1	<1	<0.01	0.01
Z-4069-006	50364	429.7	430.7	1	<1	1.83	0.07
Z-4069-006	50365	430.7	431.4	0.7	<1	0.61	0.07
Z-4069-006	50366	431.4	431.85	0.45	3	8.36	0.67
Z-4069-006	50367	431.85	432.7	0.85	<1	0.01	0.02
Z-4069-006	50368	432.7	433.35	0.65	1	3.49	0.17
Z-4069-006	50369	433.35	434.15	0.8	<1	6.81	0.18
Z-4069-006	50370	434.15	434.75	0.6	2	8.98	0.3
Z-4069-006	50372	434.75	435.3	0.55	<1	0.15	0.04
Z-4069-006	50373	435.3	435.85	0.55	3	18.75	0.77
Z-4069-006	50374	435.85	436.2	0.35	2	6.45	0.54
Z-4069-006	50375	436.2	437.35	1.15	16	26.8	3.89
Z-4069-006	50377	437.35	437.7	0.35	8	16.65	2.42
Z-4069-006	50378	437.7	438.4	0.7	<1	0.83	0.13
Z-4069-006	50379	438.4	438.7	0.3	1	1.58	0.29
Z-4069-006	50380	438.7	439.3	0.6	<1	0.34	0.05
Z-4069-006	50381	439.3	440	0.7	<1	0.22	0.1
Z-4069-006	50382	440	440.5	0.5	<1	0.04	0.03
Z-4069-006	50383	440.5	441.4	0.9	<1	0.10	0.01
Z-4069-006	50384	441.4	442.5	1.1	<1	0.11	0.05
Z-4069-006	50386	442.5	443.5	1	<1	0.41	0.11
Z-4069-006	50387	443.5	445	1.5	<1	0.04	0.01
Z-4069-006	50388	445	446.4	1.4	<1	0.26	0.08
Z-4069-006	50389	446.4	447.4	1	1	0.23	0.05
Z-4069-006	50390	447.4	447.8	0.4	<1	0.10	0.01
Z-4069-006	50391	447.8	448.7	0.9	<1	0.29	0.05
Z-4069-006	50392	448.7	449.7	1	<1	0.01	<0.01
Z-4069-006	50393	459.65	460.65	1	<1	0.03	0.03
Z-4069-006	50394	460.65	460.85	0.2	1	0.64	0.24

Z-4069-006	50395	460.85	461.85	1	<1	0.16	0.04
Z-4069-006	50330	467	468	1	<1	0.09	<0.01
Z-4069-006	50465	468	468.8	0.8	<1	4.00	0.24
Z-4069-006	50331	468.8	469.6	0.8	<1	0.09	0.01
Z-4069-006	50332	469.6	471.05	1.45	<1	0.16	0.02
Z-4069-006	50334	471.05	417.4	-53.65	<1	0.08	0.07
Z-4069-006	50335	471.4	472.25	0.85	<1	0.16	0.04
Z-4069-006	50336	472.25	472.65	0.4	<1	<0.01	0.01
Z-4069-006	50337	472.65	473.4	0.75	1	0.09	0.07
Z-4069-006	50338	473.4	473.8	0.4	<1	0.20	0.02
Z-4069-006	50339	473.8	474.2	0.4	2	0.18	0.1
Z-4069-006	50340	474.2	475.5	1.3	<1	0.05	0.04
Z-4069-006	50341	475.5	476.5	1	<1	<0.01	0.04
Z-4069-006	50342	476.5	477.4	0.9	<1	<0.01	0.03
Z-4069-006	50343	477.4	478.95	1.55	1	1.18	0.14
Z-4069-006	50344	478.95	480.1	1.15	2	0.03	0.01
Z-4069-006	50345	480.1	480.5	0.4	1	1.98	0.24
Z-4069-006	50346	480.5	481	0.5	7	0.32	0.35
Z-4069-006	50347	481	482.3	1.3	1	0.17	0.07
Z-4069-006	50349	482.3	482.85	0.55	<1	0.15	0.05
Z-4069-006	50350	482.85	483.4	0.55	7	7.81	0.6
Z-4069-006	50451	483.4	484.6	1.2	<1	0.04	0.06
Z-4069-006	50452	484.6	485.4	0.8	<1	0.02	0.01
Z-4069-006	50453	485.4	486.1	0.7	3	7.99	0.29
Z-4069-006	50455	486.1	486.9	0.8	<1	<0.01	0.01
Z-4069-006	50456	486.9	488.1	1.2	<1	0.01	0.06
Z-4069-006	50457	488.1	488.75	0.65	3	4.83	0.29
Z-4069-006	50458	488.75	489.25	0.5	<1	0.02	<0.01
Z-4069-006	50459	489.25	490.6	1.35	3	14.7	0.65
Z-4069-006	50460	472.65	473.4	0.75	2	0.14	0.08
Z-4069-006	50461	490.6	491.3	0.7	2	8.78	0.42
Z-4069-006	50462	491.3	491.8	0.5	1	0.01	0.02
Z-4069-006	50463	491.8	493.3	1.5	5	11.2	0.36
Z-4069-006	50464	493.3	494.4	1.1	1	0.04	0.08
Z-4069-006	50396	521.65	522.65	1	2	1.20	0.14
Z-4069-006	50397	522.65	523.5	0.85	3	3.12	0.91
Z-4069-006	50398	523.5	524.2	0.7	3	3.31	0.15
Z-4069-006	50399	524.2	524.85	0.65	3	5.37	0.32
Z-4069-006	50400	524.85	525.85	1	4	5.98	0.11
Z-4069-006	50401	525.85	526.9	1.05	<1	0.11	0.05
Z-4069-006	50466	526.9	527.9	1	1	0.20	0.03
Z-4069-006	50467	527.9	528.35	0.45	<1	0.90	0.08

Z-4069-006	50468	528.35	529.8	1.45	<1	0.04	0.01
Z-4069-006	50469	529.8	531.3	1.5	4	1.01	0.11
Z-4069-006	50470	531.3	532.4	1.1	1	0.05	0.01
Z-4069-006	50471	532.4	533.1	0.7	2	0.33	0.12
Z-4069-006	50472	533.1	534.4	1.3	1	0.02	0.04
Z-4069-006	50473	534.4	535.5	1.1	1	<0.01	0.01
Z-4069-006	50474	535.5	536.4	0.9	<1	<0.01	<0.01
Z-4069-006	50475	536.4	536.9	0.5	10	1.56	0.35
Z-4069-006	50476	158.1	158.4	0.3	<1	<0.01	<0.01
Z-4069-006	50477	536.9	538.5	1.6	<1	0.01	0.01
Z-4069-006	50478	538.5	539.5	1	<1	0.01	0.02
Z-4069-006	50479	539.5	540	0.5	1	<0.01	0.01
Z-4069-006	50480	540	540.4	0.4	1	<0.01	0.01
Z-4069-006	50481	540.4	542	1.6	<1	0.01	0.01
Z-4069-006	50483	542.4	543.2	0.8	2	0.06	0.05
Z-4069-006	50484	547.6	548.6	1	<1	0.01	<0.01
Z-4069-006	50485	548.6	549.2	0.6	<1	0.25	0.05
Z-4069-006	50486	549.2	550	0.8	<1	0.01	<0.01
Z-4069-006	50487	559.6	560.6	1	<1	0.01	<0.01
Z-4069-006	50488	560.6	561.6	1	<1	0.02	0.01
Z-4069-006	50489	561.6	562.5	0.9	1	<0.01	0.03
Z-4069-006	50490	562.5	563.5	1	1	<0.01	<0.01
Z-4069-006	50491	563.5	565	1.5	1	<0.01	0.07
Z-4069-006	50492	565	566.25	1.25	<1	<0.01	0.01
Z-4069-006	51052	566.25	567.3	1.05	<1	<0.01	<0.01
Z-4069-006	50494	567.3	568.9	1.6	<1	0.01	<0.01
Z-4069-006	50495	568.9	570.4	1.5	<1	0.01	<0.01
Z-4069-006	50496	570.4	571.5	1.1	2	<0.01	<0.01
Z-4069-006	50497	571.5	572.6	1.1	1	<0.01	<0.01
Z-4069-006	50498	533.1	534.4	1.3	3	0.05	0.03
Z-4069-006	50499	572.6	574.1	1.5	<1	<0.01	0.02
Z-4069-006	50500	574.1	575.1	1	<1	<0.01	<0.01

Hole ID	Sample No.	From_m	To_m	Interval_m	Ag_ppm	Zn_%	Pb_%
Z_4069_007	50402	77.40	78.60	1.20	<1	0.02	0.01
Z_4069_007	50403	78.60	79.05	0.45	<1	2.99	0.08
Z_4069_007	50404	79.05	80.00	0.95	<1	0.01	0.01
Z_4069_007	50405	80.00	81.50	1.50	<1	0.04	0.01
Z_4069_007	50406	81.50	82.60	1.10	1	4.39	0.70
Z_4069_007	50408	82.60	83.10	0.50	8	17.65	1.69
Z_4069_007	50409	83.10	84.10	1.00	<1	1.45	0.89
Z_4069_007	50410	84.10	85.20	1.10	4	12.90	1.89

Z_4069_007	50411	85.20	86.00	0.80	<1	0.45	0.33
Z_4069_007	50412	86.00	86.85	0.85	<1	0.16	0.05
Z_4069_007	50413	86.85	87.75	0.90	1	1.71	0.07
Z_4069_007	50414	87.75	88.75	1.00	<1	0.01	0.01
Z_4069_007	50415	91.00	92.00	1.00	<1	0.01	<0.01
Z_4069_007	50416	92.00	93.50	1.50	<1	0.35	0.05
Z_4069_007	50417	93.50	95.00	1.50	<1	1.36	0.01
Z_4069_007	50418	95.00	96.50	1.50	<1	0.97	0.01
Z_4069_007	50419	96.50	98.00	1.50	<1	1.42	0.02
Z_4069_007	50420	98.00	99.45	1.45	<1	3.20	0.02
Z_4069_007	50421	99.45	100.25	0.80	<1	0.07	<0.01
Z_4069_007	51221	100.25	101.00	0.75	<1	1.80	0.03
Z_4069_007	51222	101.00	101.80	0.80	<1	0.81	0.01
Z_4069_007	51224	101.80	102.80	1.00	<1	0.07	0.07
Z_4069_007	51226	102.80	104.05	1.25	<1	0.13	<0.01
Z_4069_007	51227	104.05	104.90	0.85	<1	0.13	<0.01
Z_4069_007	51228	104.90	105.70	0.80	<1	0.07	0.02
Z_4069_007	51229	105.70	106.60	0.90	<1	0.01	0.01
Z_4069_007	51230	108.60	109.60	1.00	<1	0.04	0.03
Z_4069_007	51231	109.60	109.85	0.25	<1	0.66	0.03
Z_4069_007	51233	109.85	110.85	1.00	<1	0.01	<0.01
Z_4069_007	51234	113.20	114.25	1.05	<1	0.01	<0.01
Z_4069_007	51235	114.25	114.80	0.55	<1	2.13	0.01
Z_4069_007	51237	114.80	115.80	1.00	<1	0.01	<0.01
Z_4069_007	51238	118.70	119.70	1.00	<1	0.48	0.46
Z_4069_007	51239	119.70	120.40	0.70	1	3.78	0.13
Z_4069_007	51240	120.40	121.80	1.40	<1	0.04	0.01
Z_4069_007	51241	121.80	122.80	1.00	<1	0.02	0.01
Z_4069_007	51242	122.80	123.70	0.90	2	4.10	0.92
Z_4069_007	51243	123.70	124.75	1.05	<1	0.21	0.01
Z_4069_007	51244	124.75	125.05	0.30	2	5.53	0.10
Z_4069_007	51245	125.05	126.05	1.00	1	0.05	0.01
Z_4069_007	50449	129.20	130.20	1.00	<1	0.25	0.01
Z_4069_007	50450	130.20	130.80	0.60	5	17.80	0.85
Z_4069_007	51401	130.80	131.50	0.70	<1	0.85	0.01
Z_4069_007	51403	131.50	132.55	1.05	4	24.30	0.34
Z_4069_007	51404	132.55	133.50	0.95	3	18.55	0.33
Z_4069_007	51405	133.50	134.50	1.00	3	12.90	0.12
Z_4069_007	51406	134.50	135.00	0.50	<1	0.25	0.01
Z_4069_007	51407	135.00	135.65	0.65	2	6.25	0.46
Z_4069_007	51408	136.95	137.20	0.25	<1	1.22	0.04
Z_4069_007	51409	137.20	138.15	0.95	1	0.05	0.01



Z_4069_007	51410	138.15	138.85	0.70	<1	0.01	<0.01
Z_4069_007	51411	138.85	139.55	0.70	2.5	14.20	0.36
Z_4069_007	51412	139.55	140.45	0.90	<1	0.24	0.01
Z_4069_007	51413	140.45	141.00	0.55	<1	0.19	<0.01
Z_4069_007	51414	141.00	141.80	0.80	3	2.66	1.29
Z_4069_007	51415	141.80	142.30	0.50	7	12.25	1.83
Z_4069_007	51416	142.30	143.25	0.95	<1	0.48	0.04
Z_4069_007	51418	143.25	143.55	0.30	3	7.81	0.31
Z_4069_007	51419	143.55	144.40	0.85	<1	3.59	0.91
Z_4069_007	51420	144.40	144.70	0.30	7	28.10	2.11
Z_4069_007	51422	144.70	145.25	0.55	<1	0.46	0.03
Z_4069_007	51423	145.25	145.60	0.35	4	13.95	1.90
Z_4069_007	51424	145.60	146.20	0.60	<1	5.52	0.16
Z_4069_007	51425	146.20	147.00	0.80	<1	0.42	0.03
Z_4069_007	51426	147.00	147.25	0.25	<1	2.56	0.27
Z_4069_007	51427	147.25	147.75	0.50	<1	0.52	0.17
Z_4069_007	51428	147.75	148.45	0.70	<1	0.57	0.14
Z_4069_007	51429	148.45	148.85	0.40	<1	0.36	0.02
Z_4069_007	51431	148.85	149.50	0.65	<1	2.19	0.18
Z_4069_007	51432	149.50	150.40	0.90	<1	2.20	0.45
Z_4069_007	51433	150.40	151.40	1.00	<1	0.02	0.03
Z_4069_007	51434	151.40	152.10	0.70	<1	0.15	0.06
Z_4069_007	51435	152.10	152.95	0.85	<1	0.10	0.06
Z_4069_007	51436	154.80	155.40	0.60	<1	0.32	0.09
Z_4069_007	51437	155.40	156.50	1.10	<1	1.06	0.04
Z_4069_007	51438	156.50	158.00	1.50	1	6.79	0.72
Z_4069_007	51439	158.00	159.10	1.10	4	24.10	1.47
Z_4069_007	51440	159.10	160.60	1.50	<1	0.09	0.01
Z_4069_007	51441	160.60	161.80	1.20	<1	0.39	0.02
Z_4069_007	51443	161.80	162.40	0.60	<1	<0.01	<0.01
Z_4069_007	51444	162.40	163.15	0.75	<1	8.33	0.48
Z_4069_007	51445	163.15	164.45	1.30	<1	0.73	0.01
Z_4069_007	51446	164.45	166.00	1.55	<1	1.91	0.55
Z_4069_007	51447	166.00	167.00	1.00	1	12.70	0.41
Z_4069_007	51448	167.00	167.65	0.65	6	31.30	1.81
Z_4069_007	51450	167.65	168.45	0.80	<1	0.07	0.02
Z_4069_007	51451	168.45	168.70	0.25	<1	3.51	0.02
Z_4069_007	51452	168.70	169.70	1.00	5	23.10	0.46
Z_4069_007	51453	169.70	170.70	1.00	4	14.30	0.65
Z_4069_007	51454	170.70	171.40	0.70	7	19.40	0.47
Z_4069_007	51455	171.40	172.50	1.10	<1	0.51	0.03
Z_4069_007	51456	172.50	172.80	0.30	1	4.39	0.10

Z_4069_007	51457	172.80	174.10	1.30	<1	2.39	0.02
Z_4069_007	51458	174.10	174.70	0.60	11	26.60	2.64
Z_4069_007	51459	174.70	176.00	1.30	<1	0.38	0.02
Z_4069_007	51461	176.00	177.00	1.00	1	0.28	0.07
Z_4069_007	51462	177.00	177.35	0.35	2	1.21	0.06
Z_4069_007	51463	177.35	177.95	0.60	8	38.00	1.42
Z_4069_007	51465	177.95	178.40	0.45	3	6.48	0.19
Z_4069_007	51466	178.40	179.70	1.30	1	0.15	0.11
Z_4069_007	51467	179.70	180.70	1.00	2	1.20	0.13
Z_4069_007	51468	180.70	182.00	1.30	2	3.18	0.10
Z_4069_007	51469	182.00	182.75	0.75	1	1.73	0.10
Z_4069_007	51470	182.75	183.75	1.00	<1	2.23	0.11
Z_4069_007	51472	183.75	184.75	1.00	<1	1.40	0.06
Z_4069_007	51473	184.75	185.90	1.15	3	7.35	0.35
Z_4069_007	51474	185.90	186.30	0.40	2	18.40	0.47
Z_4069_007	51475	186.30	187.50	1.20	<1	0.05	0.01
Z_4069_007	51476	187.50	188.60	1.10	<1	0.06	0.01
Z_4069_007	51477	188.60	189.95	1.35	7	16.75	2.51
Z_4069_007	51478	189.95	191.00	1.05	<1	0.07	0.01
Z_4069_007	51479	191.00	191.60	0.60	<1	4.91	0.14
Z_4069_007	51480	191.60	192.60	1.00	<1	0.02	0.01

Hole ID	Sample No.	From_m	To_m	Interval_m	Ag_ppm	Zn_%	Pb_%
Z-4069-008	51053	216.9	217.9	1	<1	0.04	0.02
Z-4069-008	51054	217.9	218.3	0.4	<1	3.41	0.19
Z-4069-008	51055	218.3	219	0.7	1	0.58	0.03
Z-4069-008	51085	219	219.6	0.6	<1	0.11	0.01
Z-4069-008	51084	219.6	220.3	0.7	<1	0.02	<0.01
Z-4069-008	51056	226.05	226.7	0.65	<1	0.20	0.02
Z-4069-008	51057	226.7	227.15	0.45	4	7.28	0.22
Z-4069-008	51058	227.15	228.15	1	<1	0.04	0.04
Z-4069-008	51059	239.5	240.4	0.9	<1	0.06	0.01
Z-4069-008	51060	240.4	241.65	1.25	<1	0.09	0.02
Z-4069-008	51061	241.65	242.05	0.4	7	13.55	1.08
Z-4069-008	51062	242.05	242.3	0.25	1	2.51	0.18
Z-4069-008	51063	242.3	242.6	0.3	4	8.87	1.51
Z-4069-008	51067	242.6	243.7	1.1	8	25.10	5.4
Z-4069-008	51151	243.7	244.7	1	10	17.95	4.97
Z-4069-008	51065	244.7	244.95	0.25	<1	0.45	0.11
Z-4069-008	51066	244.95	245.4	0.45	4	12.05	3.78

Z-4069-008	51069	245.4	246.1	0.7	<1	0.18	0.04
Z-4069-008	51094	273.8	274.8	1	1	0.01	<0.01
Z-4069-008	51095	274.8	275.8	1	<1	0.20	0.14
Z-4069-008	51096	275.8	276.6	0.8	<1	0.40	0.01
Z-4069-008	51088	276.6	278.1	1.5	<1	0.38	0.04
Z-4069-008	51089	278.1	278.5	0.4	<1	0.15	0.01
Z-4069-008	51090	278.5	279.2	0.7	<1	0.24	0.1
Z-4069-008	51091	279.2	280.7	1.5	<1	1.42	0.8
Z-4069-008	51092	280.7	281.6	0.9	<1	2.09	0.43
Z-4069-008	51093	281.6	282.6	1	1	3.64	0.23
Z-4069-008	51131	282.6	283.9	1.3	<1	0.59	0.23
Z-4069-008	51132	283.9	284.4	0.5	<1	0.3	0.06
Z-4069-008	51133	284.4	285	0.6	<1	0.13	0.01
Z-4069-008	51134	285	285.3	0.3	<1	0.01	<0.01
Z-4069-008	51070	285.3	285.9	0.6	5	12.35	6.62
Z-4069-008	51071	285.9	286.8	0.9	<1	0.18	0.03
Z-4069-008	51072	286.8	288	1.2	7	14.00	3.55
Z-4069-008	51073	288	289	1	1	0.44	0.32
Z-4069-008	51074	292.1	293.1	1	<1	0.02	<0.01
Z-4069-008	51075	293.1	293.5	0.4	1	1.86	0.08
Z-4069-008	51076	293.5	293.9	0.4	5	18.35	14.15
Z-4069-008	51077	293.9	294.5	0.6	<1	0.05	0.02
Z-4069-008	51078	294.5	295.8	1.3	<1	0.04	0.01
Z-4069-008	51079	295.8	296.1	0.3	8	17.45	5.36
Z-4069-008	51081	296.1	296.9	0.8	<1	0.33	0.04
Z-4069-008	51135	298.6	298.85	0.25	2	4.17	0.4
Z-4069-008	51136	298.85	299.1	0.25	8	17.65	5.76
Z-4069-008	51083	299.1	300.5	1.4	<1	0.06	0.01
Z-4069-008	51097	300.5	302	1.5	1	1.19	0.2
Z-4069-008	51099	302	303.3	1.3	<1	0.84	0.14
Z-4069-008	51100	303.3	303.7	0.4	1	0.92	0.51
Z-4069-008	51101	303.7	304.4	0.7	<1	2.35	0.15
Z-4069-008	51102	304.4	305.9	1.5	<1	0.34	0.02
Z-4069-008	51103	305.9	307.4	1.5	<1	0.41	0.03
Z-4069-008	51104	307.4	308.7	1.3	<1	1.16	0.06
Z-4069-008	51105	308.7	310.1	1.4	1	0.28	0.38
Z-4069-008	51106	310.1	311.5	1.4	2	5.06	0.17
Z-4069-008	51107	311.5	312.2	0.7	<1	2.18	0.13
Z-4069-008	51108	312.2	313.7	1.5	2	0.48	0.38
Z-4069-008	51109	313.7	314.4	0.7	1	3.82	0.4
Z-4069-008	51110	314.4	314.7	0.3	5	16.15	1.1

Z-4069-008	51111	314.7	315.2	0.5	<1	1.56	0.22
Z-4069-008	51112	315.2	315.5	0.3	9	28.5	1.03
Z-4069-008	51114	315.5	316.7	1.2	2	3.20	0.09
Z-4069-008	51115	316.7	318.1	1.4	7	13.55	1.01
Z-4069-008	51116	318.1	319	0.9	1	5.44	0.2
Z-4069-008	51117	319	320.2	1.2	<1	0.61	0.04
Z-4069-008	51118	320.2	320.6	0.4	4	7.95	0.41
Z-4069-008	51119	320.6	321	0.4	1	0.45	0.01
Z-4069-008	51129	321	321.6	0.6	4	12.05	0.74
Z-4069-008	51130	321.6	322.1	0.5	<1	0.13	0.02
Z-4069-008	51121	322.1	323.15	1.05	2	1.15	0.27
Z-4069-008	51122	323.15	324	0.85	4	11.30	0.79
Z-4069-008	51123	324	324.7	0.7	<1	1.53	0.08
Z-4069-008	51124	324.7	326.05	1.35	2	2.06	0.27
Z-4069-008	51125	326.05	327.5	1.45	<1	0.54	0.02
Z-4069-008	51126	327.5	329	1.5	<1	1.18	0.1
Z-4069-008	51128	329	330.1	1.1	<1	0.61	<0.01
Z-4069-008	51138	333.3	333.9	0.6	<1	2.17	0.13
Z-4069-008	51139	333.9	334.3	0.4	<1	0.10	0.01
Z-4069-008	51140	334.3	334.6	0.3	3	2.70	0.14
Z-4069-008	51141	334.6	335.2	0.6	2	6.31	0.06
Z-4069-008	51142	335.2	336.2	1	<1	0.48	0.01
Z-4069-008	51144	352.4	353.2	0.8	<1	1.53	0.03
Z-4069-008	51145	353.2	353.7	0.5	<1	1.66	0.01
Z-4069-008	51146	353.7	354.1	0.4	1	11.35	0.09
Z-4069-008	51147	354.1	355	0.9	2	3.61	0.09
Z-4069-008	51148	355	356	1	1	0.81	0.01
Z-4069-008	51149	356	356.4	0.4	1	1.33	0.01
Z-4069-008	51150	356.4	357.9	1.5	<1	0.02	<0.01
Z-4069-008	51152	357.9	359.3	1.4	1	0.21	<0.01
Z-4069-008	51153	359.3	360.3	1	<1	0.02	<0.01
Z-4069-008	51154	360.3	361.25	0.95	1	5.28	0.04
Z-4069-008	51155	361.25	362.25	1	1	0.10	0.01
Z-4069-008	51156	367.4	368.4	1	<1	0.14	0.01
Z-4069-008	51157	368.4	368.9	0.5	1	1.31	0.02
Z-4069-008	51158	368.9	369.7	0.8	2	6.05	0.04
Z-4069-008	51159	369.7	370.1	0.4	1	0.10	<0.01
Z-4069-008	51160	370.1	371.3	1.2	<1	0.05	<0.01
Z-4069-008	51161	371.3	372.3	1	<1	0.11	<0.01
Z-4069-008	51162	372.3	373.3	1	1	0.49	0.01
Z-4069-008	51163	377.25	378.1	0.85	<1	0.05	<0.01
Z-4069-008	51165	378.1	378.55	0.45	1	2.36	0.11

Z-4069-008	51166	378.55	379.55	1	<1	0.07	0.01
Z-4069-008	51167	384	385	1	1	0.01	<0.01
Z-4069-008	51168	385	385.4	0.4	2	1.51	0.06
Z-4069-008	51169	385.4	385.8	0.4	1	0.01	<0.01
Z-4069-008	51171	385.8	386.25	0.45	2	0.04	<0.01
Z-4069-008	51172	386.25	386.55	0.3	1	2.46	0.09
Z-4069-008	51173	386.55	387.55	1	<1	0.01	0.01
Z-4069-008	51174	390.35	391.35	1	<1	0.16	<0.01
Z-4069-008	51175	391.35	391.8	0.45	1	0.85	0.01
Z-4069-008	51176	391.8	393.3	1.5	<1	0.52	0.02
Z-4069-008	51177	393.3	394.7	1.4	1	2.36	0.05
Z-4069-008	51178	394.7	395.55	0.85	2	8.39	0.16
Z-4069-008	51179	395.55	396.3	0.75	<1	0.14	<0.01
Z-4069-008	51180	396.3	396.65	0.35	1	2.40	0.1
Z-4069-008	51181	396.65	397.2	0.55	<1	0.07	0.01
Z-4069-008	51182	397.2	397.85	0.65	1	5.00	0.15
Z-4069-008	51183	397.85	398.9	1.05	3	9.40	0.16
Z-4069-008	51185	398.9	399.2	0.3	<1	0.06	0.01
Z-4069-008	51186	404.4	405.4	1	<1	<0.01	<0.01
Z-4069-008	51187	405.4	406	0.6	2	1.76	0.08
Z-4069-008	51188	406	406.7	0.7	1	<0.01	<0.01
Z-4069-008	51189	406.7	407.4	0.7	2	7.52	0.31
Z-4069-008	51190	407.4	408.3	0.9	<1	0.03	0.02
Z-4069-008	51191	408.3	408.9	0.6	2	8.82	0.43
Z-4069-008	51193	408.9	409.6	0.7	<1	0.10	0.15
Z-4069-008	51194	409.6	410.6	1	<1	0.07	<0.01
Z-4069-008	51195	410.6	411.6	1	1	0.11	0.01
Z-4069-008	51196	411.6	412	0.4	2	3.26	0.07
Z-4069-008	51197	412	412.7	0.7	<1	0.43	<0.01
Z-4069-008	51220	412.7	413.25	0.55	3	4.82	0.13
Z-4069-008	51198	413.25	414.15	0.9	4	4.21	0.03
Z-4069-008	51199	414.15	415	0.85	<1	0.22	<0.01
Z-4069-008	51200	415	415.7	0.7	4	11.05	0.17
Z-4069-008	51202	415.7	416.5	0.8	3	13.75	0.35
Z-4069-008	51203	416.5	417.4	0.9	<1	0.04	0.01
Z-4069-008	51204	417.4	417.65	0.25	5	21.3	0.49
Z-4069-008	51205	417.65	419.25	1.6	<1	0.04	<0.01
Z-4069-008	51206	419.25	419.6	0.35	<1	3.58	0.15
Z-4069-008	51207	419.6	420.05	0.45	<1	0.93	0.06
Z-4069-008	51208	420.05	420.6	0.55	2	9.16	0.11
Z-4069-008	51209	420.6	421.2	0.6	<1	0.07	0.02
Z-4069-008	51211	421.2	421.55	0.35	<1	6.44	0.11



Z-4069-008	51212	421.55	422.1	0.55	1	0.03	0.03
Z-4069-008	51213	422.1	422.7	0.6	1	6.25	0.13