ASX Announcement
26 March 2018

Drilling Reveals High-grade Depth Extensions at Nicolsons

Pantoro Limited (**PNR:ASX**) (**Pantoro**) is pleased to provide an update on its extensional exploration activities at its 100% owned Nicolson's Mine. Nicolsons has been the major contributor to gold production for the project since commencement, with consistent, very high grade mineralisation found along the entire known strike length of the mine.

Highlights

- **Deepest intersection received to date in the Anderson Lode at 410 m below surface and 130 m below current Ore Reserve. Mineralisation remains open at depth.**
- **Very high grade development in the southern Johnston Lode demonstrating substantial overcall to the Ore Reserve.**
- **Depth extension and northerly plunge of the Johnston Lode confirmed.**

Pantoro has focussed its underground exploration on growth of Mineral Resources and Ore Reserves for the past year with two drill rigs operating throughout the period. Outstanding results have been achieved, with new drilling results including:

- **1 m @ 11.80 g/t Au**
- **3.8 m @ 58.36 g/t Au inc. 2.4m @ 91.7 g/t Au**
- **1.10 m @ 51.06 g/t Au**
- **0.95 m @ 37.48 g/t Au**
- **3.6 m @ 9.24 g/t Au**
- **16.9 m @ 7.20 g/t Au (TW 4.56 m) including 8.35 m @ 12.04 g/t Au**
- **2 m @ 12.21 g/t Au**

Commenting on the results, Managing Director Paul Cmrlec said

> "These latest results from Nicolsons clearly demonstrate the high quality of the asset. Mineralisation has been very consistent throughout the mine, which has a strike length approaching 1 kilometre. The current round of drilling has extended the known mineralisation to approximately 410 metres below surface while the current mine depth is only 250 metres.
>
> We will continue to explore deeper at Nicolsons with approved drill programs in place to systematically target the orebody to depths greater than 600 metres below surface. The next Ore Reserve updates for both Nicolsons and Wagtail are expected to be released during the June 2018 quarter.
>
> The mine is currently in an exceptional position to substantially increase production with 10 stoping fronts to be available for production during the first half of 2018. Manning levels are in the process of being increased to achieve the planned ramp up to 25,000 tonnes per month from Nicolsons, and installation works for the ore sorter are progressing in line with schedule. Pantoro is very well positioned to achieve its planned production rate of 80-100,000 ounces per annum late this year."

Enquiries

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Hall/Anderson Lode

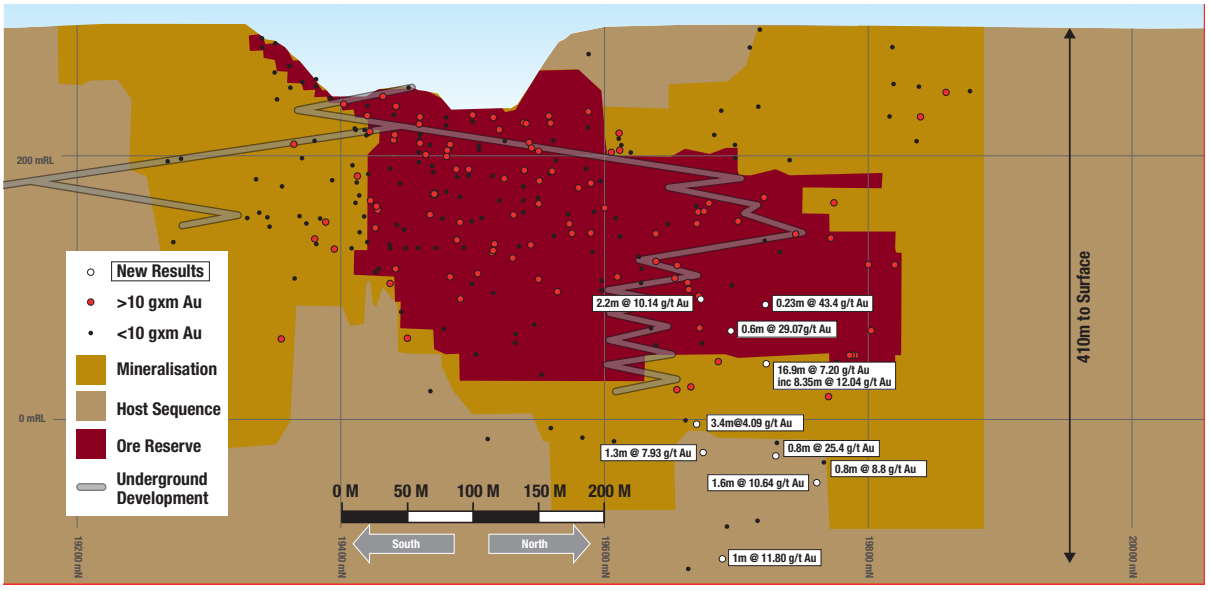
Exploration at Nicolsons has been primarily focussed on Mineral Resource and Ore Reserve growth to support the long term sustainability of the company's planned production growth to 80-100,000 ounces per annum. Drilling has been focussed beneath both the Hall and Anderson Lodes to the North and the Johnston Lode to the South. Drilling has returned high grade results at depth demonstrating the continuation of the structure and high-grade mineralisation below the Hall/Anderson lodes. A number of holes have intersected the mineralised structure at depth including NUD18003 (Plate 1), which is currently the deepest hole to intersect the mineralisation at Nicolsons, approximately 410 metres vertically below surface and 130 metres below the current Ore Reserve.

Phased drill programs, designed to test continued depth extensions to approximately 650m below surface are underway and will be ongoing throughout 2018.

Plate 1 - mineralised quartz sulphide vein in Hole NUD18003
drilled from the 2050 Hanging wall Exploration drive.

Results returned below the Hall/Anderson Lode include:

- 16.9 m @ 7.20 g/t Au (TW 4.56 m) including 8.35 m @ 12.04 g/t Au
- 1 m @ 11.80 g/t Au
- 1.6 m @ 10.64 g/t Au
- 2.2 m @10.14 g/t Au
- 1.3 m @ 7.93 g/t Au inc. 0.7m @ 13.90 g/t Au
- 0.8 m @ 25.40 g/t Au
- 0.6 m @ 29.07 g/t Au
- 0.7 m @ 14.10 g/t Au



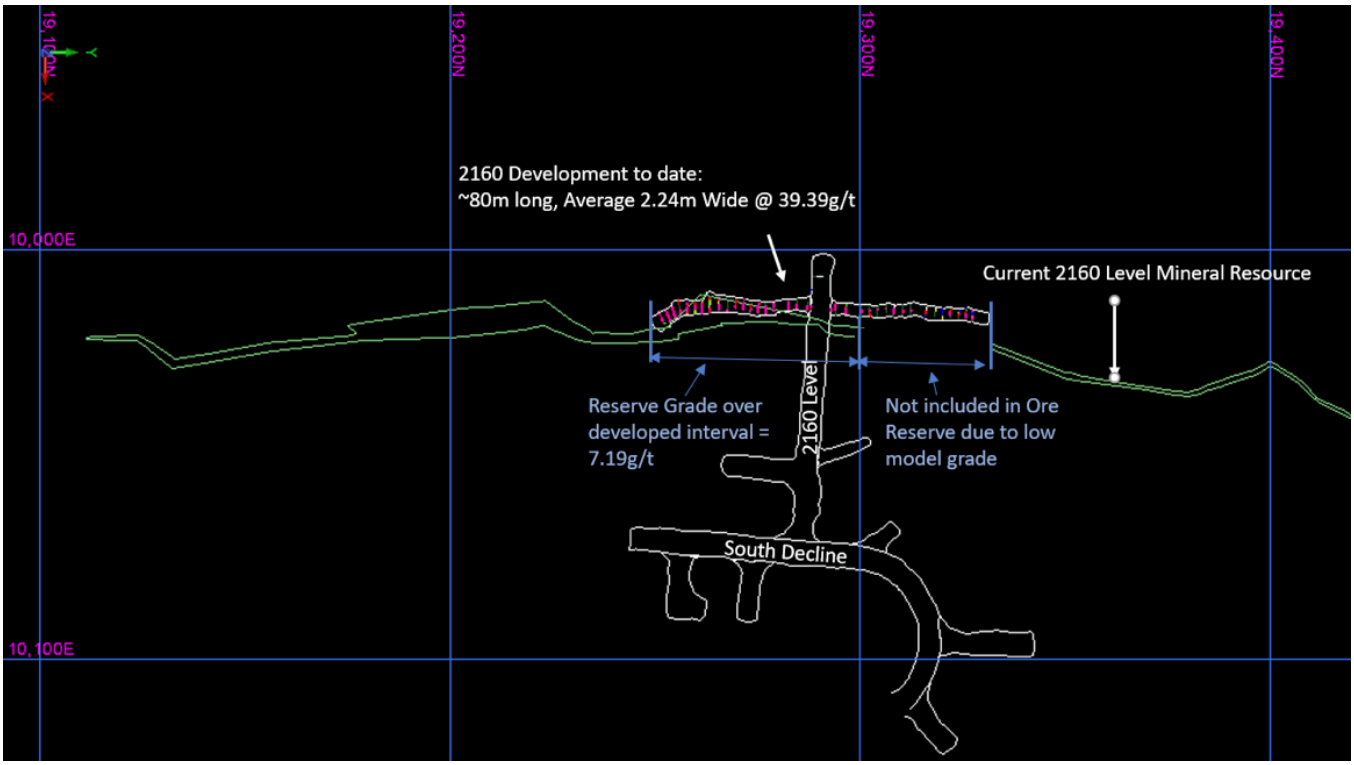
Hall/Anderson Lode Schematic Long Section

Johnston Lode Development

Development on the Johnston Lode has progressed significantly, with the 2215, 2200 and 2160 levels extensively developed. The ore has also been accessed on the 2180 level, with development due to commence.

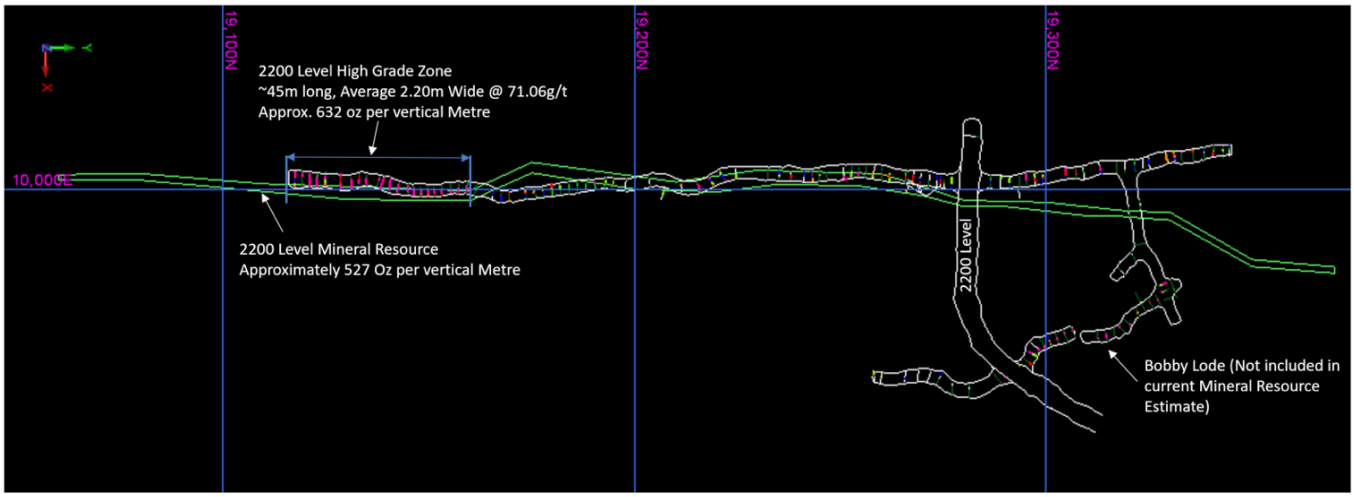
Development has continued to identify zones of very high-grade mineralisation which significantly out-perform the current Ore Reserve in a manner similar to the results in the Northern side of the mine.

Development on the 2160 level (the deepest level being developed from the Southern Decline) has displayed exceptional results well in excess of the current model. To date approximately 80 m along strike has been developed, returning an average ore width of 2.24 m at an uncut weighted average grade of 39.39 g/t Au. The zone equates to approximately 636 ounces per vertical metre, compared with the Johnston Lode Mineral Resource over the same strike length on the 2160 level of approximately 197 ounces per vertical metre. The current Johnston Lode Mineral Resource for the entire level is approximately 611 ounces per vertical metre.



Plan View of 2160mRL developed from the South Decline

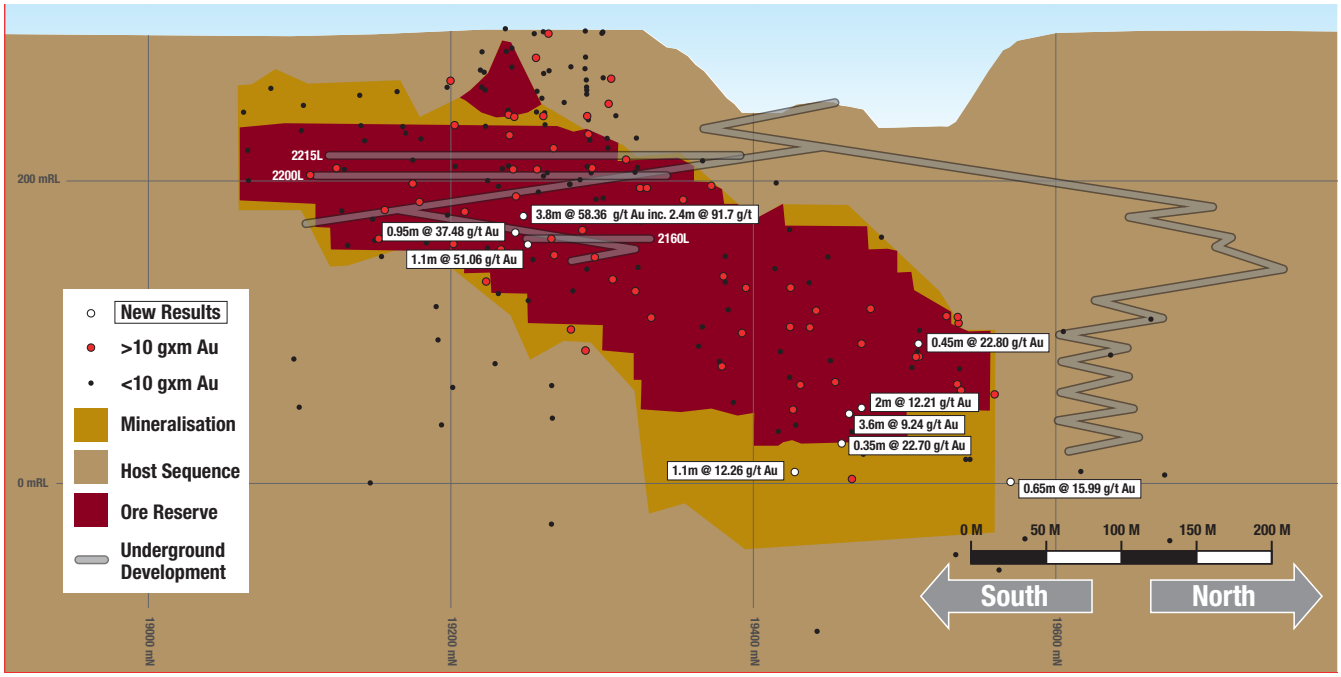
A similar very high grade zone is currently being developed over 45 m on the 2200 Level and remains in high grade ore. The 45 metre zone which has been developed to date has an average ore width of 2.20m at an uncut weighted average grade of 71.06 g/t Au. This high-grade zone equates to approximately 632 ounces per vertical metre compared with the total Johnston Lode Mineral Resource for the level of approximately 527 ounces per vertical metre.



Plan View of 2200mRL developed from the South Decline

In addition to the outstanding development results in the Johnston Lode, grade control and exploration drilling have confirmed high grades around this current development, and to the northerly plunge of the ore body in the depth extensions to the lode. Best new results include:

- 3.8 m @ 58.36 g/t Au Inc. 2.4 m @ 91.7 g/t Au
- 1.10 m @ 51.06 g/t Au
- 0.95 m @ 37.48 g/t Au
- 2 m @ 12.21 g/t Au
- 3.6 m @ 9.24 g/t Au
- 0.35 m @ 22.70 g/t Au
- 0.45 m @ 22.80 g/t Au
- 1.10 m @ 12.26 g/t Au
- 0.65 m @ 15.99 g/t Au



Johnston Lode Schematic Long Section

These results in the current development of the Johnston Lode demonstrate the clear upside potential above the current Ore Reserve calculation, and Pantoro will include these new results in the next Mineral Resource estimate and Ore Reserve update.

Appendix 1 – Tables of Exploration Results

Nicolsons Underground Face Sampling - 2160 Level

Hole ID	Northing	Easting	Elevation	Max Depth	Depth From	Depth To	Width	Au gpt
NFM001462	19287.75	10014.88	2160.71	1.2	0	0.6	0.6	6.65
NFM001462					0.6	1.2	0.6	15.66
NFM001463	19292.87	10014.1	2160.88	1.2	0.6	1.2	0.6	24.96
NFM001463					0	0.6	0.6	10.98
NFM001879	19293.99	10013	2161.4	3	0	0.4	0.4	5.31
NFM001879					0.4	1	0.6	23.15
NFM001879					1	2	1	18.33
NFM001885	19296.58	10013.34	2161.4	2.5	1.5	2	0.5	39
NFM001885					0.5	1	0.5	4.56
NFM001885					1	1.5	0.5	26.22
NFM001885					0	0.5	0.5	1.23
NFM001885					2	2.5	0.5	34.05
NFM001891	19282.47	10014.75	2161.24	2.5	1.5	2	0.5	22.28
NFM001891					0	0.5	0.5	29.42
NFM001891					0.5	1	0.5	279
NFM001891					1	1.5	0.5	66.83
NFM001904	19300.38	10013.78	2161.26	3.2	0.7	1.2	0.5	42.85
NFM001904					1.2	1.7	0.5	119.2
NFM001905	19278.98	10015.13	2161.19	2.1	0	0.6	0.6	92.55
NFM001905					0.9	1.5	0.6	43.88
NFM001905					1.5	2.1	0.6	142.65
NFM001908	19277.13	10015.91	2160.95	2.8	0.3	1.3	1	27.89
NFM001908					1.3	2.2	0.9	11.22
NFM001908					0	0.3	0.3	11.78
NFM001910	19302.39	10013.57	2161.19	2.8	0.9	1.8	0.9	63.7
NFM001910					2	2.8	0.8	3.48
NFM001924	19275.12	10016	2160.94	3	0.8	1.2	0.4	158.63
NFM001924					1.2	2.1	0.9	11.16
NFM001924					2.1	3	0.9	13.95

Hole ID	Northing	Easting	Elevation	Max Depth	Depth From	Depth To	Width	Au gpt
NFM001924					0.5	0.8	0.3	22.91
NFM001926	19304.33	10013.72	2161.17	2.7	0.7	1	0.3	20.37
NFM001926					1	1.3	0.3	104.8
NFM001939	19306.3	10013.44	2161.14	2.1	0.7	1	0.3	53.8
NFM001939					1	1.3	0.3	36
NFM001940	19273.18	10015.67	2160.88	2.8	0.5	1.4	0.9	10.46
NFM001940					1.4	2.3	0.9	6.39
NFM001946	19271.41	10014.76	2160.78	2.7	0	0.8	0.8	43.05
NFM001946					0.8	1.8	1	77.4
NFM001946					2.4	2.7	0.3	54.75
NFM001948	19308.24	10013.48	2161.1	3	0.8	1.5	0.7	15.47
NFM001948					0	0.8	0.8	0.09
NFM001948					1.5	2.5	1	29.66
NFM001951	19269.61	10014.43	2160.72	2.5	1.6	2.2	0.6	4.34
NFM001951					0	0.8	0.8	31.95
NFM001951					0.8	1.6	0.8	6.62
NFM001955	19310.39	10013.51	2159.99	2.5	1	1.5	0.5	3.01
NFM001955					1.5	2	0.5	34.8
NFM001956	19267.52	10015.28	2159.7	2.4	0	0.8	0.8	11.4
NFM002008	19265.51	10015.25	2159.74	3.5	1.9	2.6	0.7	2
NFM002008					0.7	1.9	1.2	55.2
NFM002008					0.3	0.7	0.4	24.62
NFM002008					2.6	3.5	0.9	15.8
NFM002020	19263.32	10015.51	2160.95	4.2	2	3.2	1.2	0.78
NFM002020					3.2	3.8	0.6	4.29
NFM002020					0	0.3	0.3	24.02
NFM002020					0.6	1.3	0.7	21.72
NFM002020					0.3	0.6	0.3	3.63
NFM002020					1.3	2	0.7	2.58
NFM002027	19261.49	10015.72	2160.97	4.5	0	0.6	0.6	122.8

Appendix 1 – Tables of Exploration Results (Continued)

Nicolsons Underground Face Sampling - 2160 Level (Continued)

Hole ID	Northing	Easting	Elevation	Max Depth	Depth From	Depth To	Width	Au gpt
NFM002027					2.8	3.4	0.6	2.57
NFM002027					0.6	1.8	1.2	111.9
NFM002027					1.8	2.8	1	60.6
NFM002030	19259.69	10015.85	2161.02	3	0	0.8	0.8	0.62
NFM002030					2.8	3	0.2	77.51
NFM002030					2.2	2.8	0.6	4.1
NFM002030					0.8	1.5	0.7	11.4
NFM002030					1.5	2.2	0.7	70.75
NFM002031	19316.39	10013.66	2161.42	3.2	1.3	2.4	1.1	4.22
NFM002031					0	0.8	0.8	0.15
NFM002031					0.8	1.3	0.5	0.03
NFM002031					2.4	3.2	0.8	0.21
NFM002038	19257.88	10015.97	2161.03	3	2.3	3	0.7	120.75
NFM002038					1.3	2.1	0.8	32.4
NFM002038					0	0.5	0.5	1.98
NFM002038					0.5	1.3	0.8	32.85
NFM002038					2.1	2.3	0.2	8.51
NFM002042	19318.44	10014.01	2160.2	2.5	0	0.5	0.5	0.08
NFM002042					0.5	1.1	0.6	2.03
NFM002059	19256.32	10016.45	2159.8	4.5	3	4.5	1.5	8.57
NFM002059					0.5	1.2	0.7	35.95
NFM002059					1.2	2	0.8	35.55
NFM002063	19320.17	10014.29	2160.22	3	0	0.6	0.6	0.29
NFM002063					0.6	2	1.4	0.36
NFM002063					2	3	1	2.01
NFM002067	19255.07	10017.22	2159.8	4.5	0.9	2	1.1	173.25
NFM002067					2	3.4	1.4	47.33
NFM002067					0	0.9	0.9	370.8
NFM002073	19322.05	10014.23	2160.26	2.5	1	1.9	0.9	22.52

Hole ID	Northing	Easting	Elevation	Max Depth	Depth From	Depth To	Width	Au gpt
NFM002073					0.5	1	0.5	4.64
NFM002079	19253.84	10018.01	2159.79	3.3	1.1	2.2	1.1	86.85
NFM002079					2.2	3.3	1.1	65.93
NFM002079					0	1.1	1.1	119.1
NFM002080	19324.16	10014.52	2160.32	2.5	0	0.8	0.8	0.26
NFM002080					0.8	1.1	0.3	2.37
NFM002080					1.1	1.4	0.3	27.92
NFM002080					1.4	2	0.6	8.37
NFM002085	19252.16	10018.14	2159.8	3.4	1.5	2.2	0.7	9.21
NFM002085					0	0.1	0.1	0.62
NFM002085					0.1	0.5	0.4	1.13
NFM002085					0.5	1	0.5	107.85
NFM002085					1	1.5	0.5	58.05
NFM002085					2.2	2.9	0.7	73.5
NFM002085					2.9	3.4	0.5	72
NFM002088	19325.81	10014.41	2160.38	2.5	2.05	2.5	0.45	26.79
NFM002088					0	0.2	0.2	0.45
NFM002088					0.2	0.6	0.4	1.26
NFM002088					0.6	1	0.4	5.3
NFM002088					1.1	2.05	0.95	32.85
NFM002088					1	1.1	0.1	5.45
NFM002098	19327.54	10014.81	2160.42	2.8	1.3	1.8	0.5	1.53
NFM002098					1.8	2.4	0.6	20.49
NFM002098					0.5	1.3	0.8	0.42
NFM002098					0	0.5	0.5	11.01

Appendix 1 – Tables of Exploration Results (Continued)

Nicolsons Underground Face Sampling - 2220 Level

Hole ID	Northing	Easting	Elevation	Max Depth	Depth From	Depth To	Width	Au gpt
NFM001902	19159.22	10000.83	2203.49	2.6	0.85	1.2	0.35	124.28
NFM001902					0.5	0.85	0.35	169.54
NFM001902					0	0.5	0.5	181.91
NFM001954	19158.99	10001.04	2203.47	3	0.2	1	0.8	29.46
NFM001954					1	1.5	0.5	77.03
NFM001954					1.5	2.1	0.6	41.03
NFM001966	19157	10001.14	2203.48	2.5	0	0.5	0.5	8.48
NFM001966					0.5	1	0.5	55.88
NFM001966					1	1.5	0.5	153.15
NFM001969	19155.25	10001.14	2203.49	2.5	0	0.5	0.5	330.15
NFM001969					0.5	1.1	0.6	43.28
NFM001977	19153.2	10001.63	2203.49	2.5	0.6	1.2	0.6	170.7
NFM001977					1.2	1.8	0.6	99.3
NFM001977					0	0.6	0.6	6.38
NFM001980	19151.34	10001.89	2203.5	2.5	0.3	0.8	0.5	7.83
NFM001980					0.8	1.3	0.5	61.65
NFM001980					1.3	2	0.7	34.5
NFM001983	19149.78	10001.91	2203.55	2.5	0.5	1	0.5	16.76
NFM001983					1	2	1	240
NFM001983					0	0.5	0.5	1.62
NFM001989	19147.99	10001.86	2203.59	2.5	1.6	2.1	0.5	122.85
NFM001989					0.4	0.9	0.5	1.85
NFM001989					0.9	1.6	0.7	311.55
NFM001995	19146.32	10001.6	2203.61	2.5	1.4	2.1	0.7	291
NFM001995					0.7	1.4	0.7	158
NFM001995					0	0.7	0.7	20.6
NFM002000	19145.02	10001.29	2203.63	2.9	0.6	1.5	0.9	128
NFM002000					1.5	2.4	0.9	97.6
NFM002006	19142.28	10001.1	2204	2.6	1.3	2.3	1	82.95

Hole ID	Northing	Easting	Elevation	Max Depth	Depth From	Depth To	Width	Au gpt
NFM002006					0.4	1.3	0.9	36.15
NFM002006					0	0.4	0.4	6.38
NFM002015	19140.25	10000.75	2204	3.8	0.2	0.6	0.4	7.88
NFM002015					2.6	3.6	1	106.2
NFM002015					1.1	2.6	1.5	82.5
NFM002015					0.6	1.1	0.5	14.18
NFM002021	19138.16	9999.91	2204	3.6	1.1	1.3	0.2	20.76
NFM002021					0	1.1	1.1	21.78
NFM002021					2.2	3.1	0.9	327.75
NFM002021					1.3	2.2	0.9	100.2
NFM002029	19137.31	9999.71	2204	3	1.8	2.15	0.35	50.95
NFM002029					2.15	2.5	0.35	40.95
NFM002044	19134.59	9998.87	2204	2.5	1	1.5	0.5	23.13
NFM002044					0.5	1	0.5	34.2
NFM002044					0	0.5	0.5	15.62
NFM002055	19132.88	9998.71	2204	2.5	0	0.6	0.6	22.53
NFM002055					0.6	1.2	0.6	59.1
NFM002055					1.2	1.8	0.6	9.35
NFM002058	19131.2	10000.16	2202.66	3	1.5	2.5	1	91.95
NFM002058					0	0.5	0.5	73
NFM002058					0.5	1	0.5	15.29
NFM002058					1	1.5	0.5	61.2
NFM002062	19128.56	10000.23	2202.69	4	0.3	1.1	0.8	72.6
NFM002062					1.1	1.9	0.8	119.5
NFM002062					1.9	3.1	1.2	8.4
NFM002062					3.1	4	0.9	83.05
NFM002066	19124.83	9999.55	2202.68	4	0	0.5	0.5	39.68
NFM002066					0.5	1	0.5	1.5
NFM002066					1	2	1	0.54
NFM002066					2	2.8	0.8	32.7

Appendix 1 – Tables of Exploration Results (Continued)

Nicolsons Underground Face Sampling - 2220 Level (Continued)

Hole ID	Northing	Easting	Elevation	Max Depth	Depth From	Depth To	Width	Au gpt
NFM002071	19122.75	9999.68	2202.68	3.5	0	0.6	0.6	194.4
NFM002071					0.6	2.7	2.1	21.24
NFM002071					2.7	3.2	0.5	1.1
NFM002078	19120.91	9999.54	2202.67	3.5	2.4	3.5	1.1	41.55
NFM002078					0	0.6	0.6	36.9
NFM002078					1.2	2.4	1.2	11.06
NFM002078					0.6	1.2	0.6	10.94
NFM002083	19119.14	9999.65	2202.66	4.2	0	0.2	0.2	35.18
NFM002083					2.7	3.5	0.8	56.03
NFM002089	19117.49	9999.75	2202.65	4.2	1.4	2.4	1	0.21
NFM002089					0.4	1.4	1	2.43
NFM002089					0	0.4	0.4	14.73
NFM002089					2.4	3.1	0.7	12.2
NFM002089					3.1	3.65	0.55	47.25
NFM002089					3.65	4.2	0.55	55.95
NFM002038					0.5	1.3	0.8	32.85
NFM002038					2.1	2.3	0.2	8.51
NFM002042	19318.44	10014.01	2160.2	2.5	0	0.5	0.5	0.08
NFM002042					0.5	1.1	0.6	2.03
NFM002059	19256.32	10016.45	2159.8	4.5	3	4.5	1.5	8.57
NFM002059					0.5	1.2	0.7	35.95
NFM002059					1.2	2	0.8	35.55
NFM002063	19320.17	10014.29	2160.22	3	0	0.6	0.6	0.29
NFM002063					0.6	2	1.4	0.36
NFM002063					2	3	1	2.01
NFM002067	19255.07	10017.22	2159.8	4.5	0.9	2	1.1	173.25
NFM002067					2	3.4	1.4	47.33
NFM002067					0	0.9	0.9	370.8
NFM002073	19322.05	10014.23	2160.26	2.5	1	1.9	0.9	22.52

Hole ID	Northing	Easting	Elevation	Max Depth	Depth From	Depth To	Width	Au gpt
NFM002073					0.5	1	0.5	4.64
NFM002079	19253.84	10018.01	2159.79	3.3	1.1	2.2	1.1	86.85
NFM002079					2.2	3.3	1.1	65.93
NFM002079					0	1.1	1.1	119.1
NFM002080	19324.16	10014.52	2160.32	2.5	0	0.8	0.8	0.26
NFM002080					0.8	1.1	0.3	2.37
NFM002080					1.1	1.4	0.3	27.92
NFM002080					1.4	2	0.6	8.37
NFM002085	19252.16	10018.14	2159.8	3.4	1.5	2.2	0.7	9.21
NFM002085					0	0.1	0.1	0.62
NFM002085					0.1	0.5	0.4	1.13
NFM002085					0.5	1	0.5	107.85
NFM002085					1	1.5	0.5	58.05
NFM002085					2.2	2.9	0.7	73.5
NFM002085					2.9	3.4	0.5	72
NFM002088	19325.81	10014.41	2160.38	2.5	2.05	2.5	0.45	26.79
NFM002088					0	0.2	0.2	0.45
NFM002088					0.2	0.6	0.4	1.26
NFM002088					0.6	1	0.4	5.3
NFM002088					1.1	2.05	0.95	32.85
NFM002088					1	1.1	0.1	5.45
NFM002098	19327.54	10014.81	2160.42	2.8	1.3	1.8	0.5	1.53
NFM002098					1.8	2.4	0.6	20.49
NFM002098					0.5	1.3	0.8	0.42
NFM002098					0	0.5	0.5	11.01

Appendix 1 – Tables of Exploration Results (Continued)

Nicolsons Underground Drilling

Hole ID	Northing	Easting	RL	Dip (degrees)	Azimuth (degrees)	End of Hole Depth(m)	From (m)	To (m)	Downhole intercept (m)	Au gpt (uncut)	True width
NGC17012	19438.2	10134.5	2130	0	94.33	17.7	4.5	6.9	2.4	1.03	2.26
NGC17012	19438.2	10134.5	2130	0	94.33	17.7	9.6	10.8	1.2	3.86	1.13
NGC17015	19431.01	10129.75	2130	0	327.03	25.5	21.27	21.85	0.58	7.90	0.23
NGC17021	19450.18	10134.46	2143.9	0	100.13	16.1	2.2	6.9	4.7	1.67	4.41
NGC17042A	19447.66	10141.39	2087.5	-0.1	246.62	92.5	76.3	76.95	0.65	4.12	0.61
NGC17046	19638.01	10117.92	2085.04	-56.3	242.12	122.8	78.7	79.18	0.48	4.42	0.39
NGC17046	19638.01	10117.92	2085.04	-56.3	242.12	122.8	93	93.65	0.65	6.29	0.52
NGC17051	19289.3	10038.96	2207.84	2.8	269.41	60.9	38.5	40.8	2.3	1.44	2.12
NGC17053	19290.36	10039.36	2207.93	1.5	308.21	92.66	48.37	49.15	0.78	1.21	0.52
NGC17053	19290.36	10039.36	2207.93	1.5	308.21	92.66	61	61.2	0.2	12.80	0.13
NGC17054	19277.17	10023.8	2205.22	4.1	234.11	59.1	33.9	36.3	2.4	5.06	2.16
NGC17055	19277.4	10025.81	2204.85	3.2	215.71	73.7	53	55.1	2.1	1.54	1.50
NGC17055	19277.4	10025.81	2204.85	3.2	215.71	73.7	11	12.2	1.2	1.67	0.86
NGC17089	19721.99	10182.04	2087.53	1.5	91.7	65.6	0	0.23	0.23	43.40	0.21
NGC18009	19233.44	10037.3	2168.26	-4.1	286.2	84.6	24.35	26	1.65	2.05	1.48
NGC18009	19233.44	10037.3	2168.26	-4.1	286.2	84.6	30.2	31.15	0.95	37.48	0.85
NGC18011	19235.09	10038.04	2167.68	-19.6	304.98	68.7	33	36	3	6.73	2.12
NGC18011	19235.09	10038.04	2167.68	-19.6	304.98	68.7	24.5	25.2	0.7	8.62	0.50
NGC18011	19235.09	10038.04	2167.68	-19.6	304.98	68.7	28.9	30	1.1	51.06	0.78
NGC18019	19785.35	10118.71	2048.28	6	275.68	8.3	2	4	2	12.11	1.80
NGC18020	19786.36	10118.62	2048.21	4.2	292.88	11	3.3	5.4	2.1	22.70	1.76
NGC18021	19786.95	10118.88	2048.39	2.6	305.78	12.4	4.7	6.2	1.5	28.13	1.05
NUD16050	19322.41	10124.04	2201.31	-57.9	315.5	173.8	139.8	144.6	4.8	1.69	2.72
NUD16063	19520.29	10038.02	2205.86	-55.3	74.98	279	189.8	191.1	1.3	1.84	1.06
NUD16066	19519.65	10031.99	2206.13	-47.3	90.98	260.8	152.7	153.75	1.05	3.37	0.93
NUD17003	19404.12	10157.83	2213.26	-76.2	168.87	236.1	64.9	66.3	1.4	8.24	0.84
NUD17007	19406.24	10155.1	2212.55	-61.4	285.26	206.2	166.9	168	1.1	5.06	0.83
NUD17017	19407.1	10155.38	2212.6	-56.9	306.76	236.6	175	176	1	5.60	0.69

Hole ID	Northing	Easting	RL	Dip (degrees)	Azimuth (degrees)	End of Hole Depth(m)	From (m)	To (m)	Downhole intercept (m)	Au gpt (uncut)	True width
NUD17017	19407.1	10155.38	2212.6	-56.9	306.76	236.6	193.3	195.3	2	12.21	1.37
NUD17018	19407.09	10155.49	2212.61	-61.3	309.06	231	187.7	191.3	3.6	9.24	2.36
NUD17018	19407.09	10155.49	2212.61	-61.3	309.06	231	220.05	220.4	0.35	22.70	0.23
NUD17019	19407.07	10155.55	2212.66	-64.2	309.46	258	198.4	199.8	1.4	2.03	0.91
NUD17019	19407.07	10155.55	2212.66	-64.2	309.46	258	162	162.7	0.7	7.92	0.45
NUD17020	19407.04	10155.77	2212.69	-67.8	312.86	252.4	226	227	1	5.08	0.60
NUD17021	19406.27	10155.57	2212.55	-74.1	290.76	249	65	68	3	1.29	1.76
NUD17021	19406.27	10155.57	2212.55	-74.1	290.76	249	101.8	103	1.2	4.98	0.70
NUD17021	19406.27	10155.57	2212.55	-74.1	290.76	249	212.4	213.5	1.1	12.26	0.65
NUD17022	19645.85	10166.59	2105.63	1.5	281.5	119.8	41.8	44	2.2	10.14	2.05
NUD17024	19522.61	10079.2	2201.06	-81.3	215.15	197.9	107.2	108	0.8	1.44	0.38
NUD17029	19525.42	10077.85	2200.97	-81.3	315.85	183.6	95.4	95.85	0.45	22.80	0.22
NUD17036	19762.37	10201.82	2139.09	-78	273.7	684.35	175.1	175.9	0.8	8.80	0.42
NUD17039	19760.87	10201.54	2139.04	-75.5	223.93	225.6	168.6	170.6	2	1.82	1.13
NUD17039	19760.87	10201.54	2139.04	-75.5	223.93	225.6	171.5	172.3	0.8	25.40	0.45
NUD17051	19670.81	10177.55	2107.86	-15.9	224.8	179.6	61.3	62	0.7	1.70	0.57
NUD17051	19670.81	10177.55	2107.86	-15.9	224.8	179.6	140.9	141.4	0.5	5.23	0.41
NUD17052	19673.4	10177.25	2107.97	-20.2	268.9	80.9	25.2	26.2	1	2.56	0.99
NUD17054	19671.03	10177.86	2107.19	-37	224.3	224	176.95	177.6	0.65	15.99	0.53
NUD17058	19674.82	10177.8	2107.38	-43.39	298.33	103.5	58.4	59	0.6	29.07	0.47
NUD17069	19131.6	10102.72	2174.49	-33	188.03	257.6	146.8	147.8	1	1.59	0.60
NUD17070	19761.05	10201.61	2139.1	-87.9	285.03	283.5	97.2	99.2	2	4.63	0.75
NUD17072	19133.76	10104.22	2174.67	-35.4	316.93	176.8	51.3	52.3	1	2.55	0.55
NUD17083	19133.07	10101.33	2173.93	-70	220	197.6	70.05	71.3	1.25	1.22	0.80
NUD17096	19281.12	10153.69	2195.42	-78	248.72	276.04	226.5	227.55	1.05	1.05	0.56
NUD17099	19281.24	10153.08	2195.43	-61.2	254.22	191.74	69.1	69.9	0.8	1.95	0.60
NUD17130	19654.32	10179.26	2066.82	-79.2	305.7	95.5	72.8	73	0.2	1.62	0.10
NUD17133	19654.32	10179.26	2066.82	-77.1	345.3	146.6	70.4	73.8	3.4	4.09	0.28
NUD17133	19654.32	10179.26	2066.82	-77.1	345.3	146.6	93.7	95	1.3	7.93	0.80
NUD17138	19654.32	10179.26	2066.82	-17.9	334.32	120.2	91.1	98	6.9	1.34	1.86
NUD17138	19654.32	10179.26	2066.82	-17.9	334.32	120.2	71.2	88.1	16.9	7.20	4.57

Appendix 1 – Tables of Exploration Results (Continued)

Nicolsons Underground Drilling

Hole ID	Northing	Easting	RL	Dip (degrees)	Azimuth (degrees)	End of Hole Depth(m)	From (m)	To (m)	Downhole intercept (m)	Au gpt (uncut)	True width
NUD17138	inc 8.35m @ 12.04 g/t Au from 79.2m										
NUD17145	19623.54	10294.24	2053.44	-28.3	261.4	245.1	120.5	121.4	0.9	3.38	0.89
NUD17146	19622.72	10294.73	2053.53	-27.1	254.3	307.8	152.2	152.9	0.7	3.96	0.69
NUD17146	19622.72	10294.73	2053.53	-27.1	254.3	307.8	147.2	148.4	1.2	5.48	1.19
NUD17146	19622.72	10294.73	2053.53	-27.1	254.3	307.8	274.4	274.8	0.4	7.02	0.40
NUD17148	19625.92	10295.78	2053.45	-37.4	294.19	278.7	170.6	174	3.4	2.24	2.81
NUD17155	19627.18	10296.04	2053.57	-30	314.9	311.1	207.7	209.3	1.6	10.64	0.92
NUD18002	19625.69	10296.29	2053.63	-45.3	296.08	302	190.6	192.1	1.5	1.22	1.21
NUD18003	19626.91	10295.73	2053.45	-51.2	296.98	319.3	204.6	205.6	1	11.80	0.80
NUD18004	19627.16	10296.03	2053.56	-41.9	305.18	260.5	195.3	196.15	0.85	2.36	0.60
NGC18010	19232.581	10042.14	2168.623	13.9	299.4	80.6	32	35.8	3.8	58.36	2.93
NGC18010	inc 2.4m @ 91.7g/t Au from 33.4m										

Appendix 2 – JORC Code 2012 Edition – Table 1

SECTION 1: SAMPLING TECHNIQUES AND DATA

Criteria	JORC Code explanation	Commentary
Sampling techniques	• Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. • Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. • Aspects of the determination of mineralisation that are Material to the Public Report. • In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	• This release relates to results from an ongoing underground extensional and grade control diamond drilling program at the Nicolsons underground deposit and underground face sampling related to the development of the Johnston Lode in the Nicolsons Underground mine. • The diamond drill core sampled is NQ2 • All core is logged and sampled according to geology, with only selected samples assayed. Core is halved, with one side assayed, and the other half retained in core trays on site for further analysis. Samples are a maximum of 1.2m, with shorter intervals utilised according to geology. • Core is aligned,measured and marked up in metre intervals referenced back to downhole core blocks . • Diamond drilling is completed to industry standard and various sample intervals based on geology (0.3m-1.2m) are selected based on geology. • Diamond core are dispatched to an external accredited laboratory where they are crushed and pulverized to a pulp (P90 75 micron) for fire assay (40g charge). Face samples 2-3kg samples are prepared at the onsite laboratory and 500g pulp (P90 75 micron) is delivered to an accredited laboratory in Perth for fire assay (40g charge) • For underground development face chip samples, Samples of approximately 2.0 kg are assayed at the onsite lab with a 500g pulverized pulp (P90 75 micron) assay by BLEG (bulk leach extractable gold) methodology following procedures established by an external accredited laboratory. This method determines cyanide recoverable gold only. Routinely any samples with assays returning greater than 1g/t have pulps dispatched to external accredited laboratory where sizing checks are completed to establish sample preparation is to standard and then fire assayed (40g charge). • Visible gold is encountered and where observed during logging, Screen Fire Assays are conducted • Face Sampling,, each development face / round is mapped geologically and chip sampled perpendicular to mineralisation. The sampling intervals are domained by geological constraints (e.g. rock type, veining and alteration / sulphidation etc.). The majority of exposures within the orebody are sampled.
Drilling techniques	• Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	• Underground diamond drilling is completed utilizing NQ2 (standard tube). • Core is oriented routinely utilizing a Ezi-Mark orientation device.

Criteria	JORC Code explanation	Commentary
Drill sample recovery	• Method of recording and assessing core and chip sample recoveries and results assessed. • Measures taken to maximise sample recovery and ensure representative nature of the samples. • Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	• All holes were logged at site by an experienced geologist. Recovery and sample quality were visually observed and recorded • Diamond drilling practices result in high recovery in competent ground as part of the current drill program • No significant core loss has been noted in fresh material. Good core recovery has generally been achieved in all sample types in the current drilling program.
Logging	• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. • Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. • The total length and percentage of the relevant intersections logged.	• Geological logging is completed by a qualified geologist and logging parameters include: depth from, depth to, condition, weathering, oxidation, lithology, texture, colour, alteration style, alteration intensity, alteration mineralogy, sulphide content and composition, quartz content, veining, and general comments. • All Development faces are mapped by a geologist and routinely photographed • Logging is quantitative and qualitative with all core photographed wet. • 100% of the relevant intersections are logged.
Sub-sampling techniques and sample preparation	• If core, whether cut or sawn and whether quarter, half or all core taken. • If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. • For all sample types, the nature, quality and appropriateness of the sample preparation technique. • Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. • Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. • Whether sample sizes are appropriate to the grain size of the material being sampled.	• Core samples were sawn in half utilising an Almonte core-saw, with one half used for assaying and the other half retained in core trays on site for future analysis. • Face Chips samples are nominally chipped perpendicular to mineralisation across the face from left to right, and sub-set via geological features as appropriate • For core samples, core was separated into sample intervals and separately bagged for analysis at the certified laboratory. • For face samples, the face was separated into sample intervals and separately bagged for analysis at site lab and the certified laboratory. • Core was cut under the supervision of an experienced geologist, was routinely cut on the orientation line. • All mineralised zones are sampled as well as material considered barren either side of the mineralised interval • Field duplicates i.e. other half of core or ¼ core has not been routinely sampled • Half core is considered appropriate for diamond drill samples.

Criteria	JORC Code explanation	Commentary
Quality of assay data and laboratory tests	• The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. • For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. • Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	• Diamond Core assays are completed in a certified laboratory in Perth WA. Gold assays are determined using fire assay with 40g charge. Where other elements are assayed using either AAS base metal suite or acid digest with ICP-MS finish. The methods used approach total mineral consumption and are typical of industry standard practice. • For underground development face chip samples, Samples of approximately 2.0 kg are assayed at the onsite lab with a 500g pulverized pulp (P90 75 micron) assay by BLEG (bulk leach extractable gold) methodology following procedures established by an external accredited laboratory. This method determines cyanide recoverable gold only. Routinely any samples with assays returning greater than 1g/t have pulps dispatched to external accredited laboratory where sizing checks are completed to establish sample preparation is to standard and then fire assayed (40g charge). The methods used approach total mineral consumption and are typical of industry standard practice. Results are compared for any variations outside of the limitations of the respective methods. • No geophysical logging of drilling was performed. • Lab standards, blanks and repeats are included as part of the QAQC system. In addition the laboratory has its own internal QAQC comprising standards, blanks and duplicates. Sample preparation checks of pulverising at the laboratory include tests to check that the standards of 90% passing 75 micron is being achieved. Follow-up re-assaying is performed by the laboratory upon company request following review of assay data. Acceptable bias and precision is noted in results given the nature of the deposit and the level of classification
Verification of sampling and assaying	• The verification of significant intersections by either independent or alternative company personnel. • The use of twinned holes. • Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. • Discuss any adjustment to assay data.	• Significant intersections are noted in logging and checked with assay results by company personnel both on site and in Perth. Diamond drilling confirms the width of the mineralised intersections. • There are no twinned holes drilled as part of these results • All primary data is logged on paper and later entered into the SQL database. Data is visually checked for errors before being sent to an external database manager for further validation and uploaded into an offsite database. Hard copies of original drill logs are kept in onsite office. • Visual checks of the data re completed in Surpac mining software • No adjustments have been made to assay data unless in instances where standard tolerances are not met and reassay is ordered.

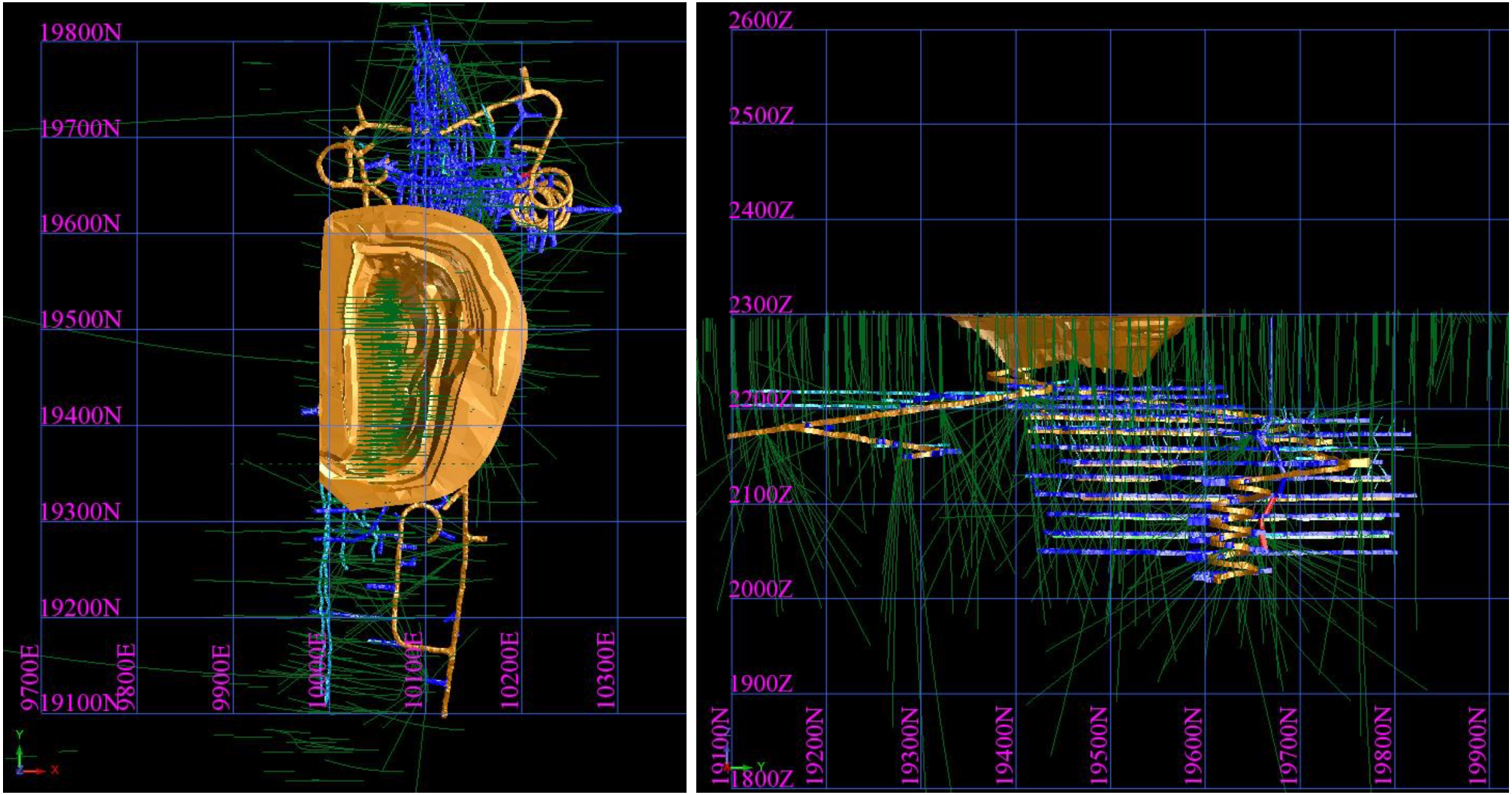
Criteria	JORC Code explanation	Commentary
Location of data points	• Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. • Specification of the grid system used. • Quality and adequacy of topographic control.	• Drilling is surveyed using conventional survey. Downhole surveys are conducted during drilling using a Reflex survey tool. All holes are surveyed down the hole at 15m, 30m and every 30m thereafter. When the hole is completed, multishots are taken every 6m from EOH when tripping rods. • All underground development is routinely picked up by conventional survey methods and faces referenced to this by measuring from underground survey stations prior to entry into the database • The project lies in MGA 94, zone 52. Local coordinates are derived by conversion: GDA94_EAST =NIC_EAST * 0.9983364 + NIC_NORTH * 0.05607807 + 315269.176 GDA94_NORTH = NIC_EAST * (-0.05607807) + NIC_NORTH * 0.9983364 + 7944798.421 GDA94_RL =NIC-RL + 101.799 • Topographic control uses DGPS collar pickups and external survey RTK data and is considered adequate for use.
Data spacing and distribution	• Data spacing for reporting of Exploration Results. • Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. • Whether sample compositing has been applied.	• Drill hole spacing at Nicolson's underground is variable due to the nature of drilling fans from suitable underground drilling platforms. Spacing of centres is generally targeted at between 40 m by 40 m with infill as required. • Face samples are taken on the basis of the length of the development rounds being approximately a 2m spacing along strike • The Competent Person is of the view that the drill/sample spacing, geological interpretation and grade continuity of the data supports the resource categories assigned. • No compositing is applied to diamond drilling or face sampling. • Core and face samples are both sampled to geology of between 0.2 and 1.2m intervals.
Orientation of data in relation to geological structure	• Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. • If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	• Drilling is generally perpendicular to the orebody other than the limitations introduced by the need to drill fans. All intervals are reviewed relative to the understanding of the geology and true widths calculated and reported in the tables attached in the body of the report. • No bias of sampling is believed to exist through the drilling orientation • Underground face and development sampling is nominally undertaken normal to the various orebodies.
Sample security	• The measures taken to ensure sample security.	• The chain of custody is managed by Pantoro employees and contractors. Samples are stored on site and delivered in sealed boxes and bags to the lab in Perth • Samples are tracked during shipping.
Audits or reviews	• The results of any audits or reviews of sampling techniques and data.	• No audit or reviews of sampling techniques have been undertaken however the data is managed by an offsite database contractor who has internal checks/ protocols in place.

SECTION 2: REPORTING OF EXPLORATION RESULTS

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. • The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	• Tenements containing Mineral Resources and Ore Reserves are 100% held by Pantoro subsidiary company Halls Creek Mining Pty Ltd. This is : M80/359. Tenement transfers to HCM are yet to occur as final stamp duty assessments have not been finalised by the office of state revenue. The tenements lie on a pastoral lease with access and mining agreements and predate native title claims. • The tenements are in good standing and no known impediments exist.
Exploration done by other parties	• Acknowledgment and appraisal of exploration by other parties.	• The deposits were discovered by prospectors in the early 1990s. After an 8,500 m RC program, Precious Metals Australia mined 23 koz at an estimated 7.7g/t Au from Nicolson's Pit in 1995/96 before ceasing the operation. Rewah mined the Wagtail and Rowdy pits (5 koz at 2.7g/t Au) in 2002/3 before Terra Gold Mines (TGM) acquired the project, carried out 12,000 m of RC drilling and produced a 100 koz resource estimate. GBS Gold acquired TGM and drilled 4,000 m before being placed in administration. Bulletin Resources Ltd acquired the project from administrators and conducted exploration work focused on Nicolsons and the Wagtail Deposits and completed regional exploration drilling and evaluation and completed a Mining Study in 2012 prior to entering into a JV with PNR in 2014.
Geology	• Deposit type, geological setting and style of mineralisation.	• Gold mineralisation in the Nicolson's Find area is structurally controlled within the 400 m wide NNE trending dextral strike slip Nicolson's Find Shear Zone (NFSZ) and is hosted within folded and metamorphosed turbiditic greywackes, felsic volcaniclastics, mafic volcanics and laminated siltstones and mudstones. This zone forms part of a regional NE-trending strike slip fault system developed across the Halls Creek Orogen (HCO). • The NFSZ comprises a NNE-trending anastomosing system of brittle-ductile shears, characterised by a predominantly dextral sense of movement. The principal shear structures trend NNE to N-S and are linked by NW, and to a lesser extent, by NE shears. Individual shears extend up to 500m along strike and overprint the earlier folding and penetrative cleavage of the HCO. • The overall geometry of the system is characterized by right step-overs and bends/jogs in the shear traces, reflecting refraction of the shears about the granite contact. Within this system, the NW-striking shears are interpreted as compressional structures and the NE-striking shears formed within extensional windows.

Criteria	JORC Code explanation	Commentary
		• Mineralisation is primarily focussed along NNE trending anastomosing systems of NNE-SSW, NW-SE and NE-SW oriented shears and splays. The NNE shears dip moderately to the east, while the NW set dips moderately to steeply to the NE. Both sets display variations in dip, with flattening and steepening which result in a complex pattern of shear intersections.. • Mineralisation is strongly correlated with discontinuous quartz veining and with Fe-Si-K alteration halos developed in the wall rocks to the veins. The NE shears are associated with broad zones of silicification and thicker quartz veining (typically white, massive quartz with less fracturing and brecciation); however, these are typically poorly mineralized. The NW-trending shears are mineralized, with the lodes most likely related to high fluid pressures with over-pressuring and failure leading to vein formation. Although the NE structures formed within the same shear system, the quartz veining is of a different generation to the mineralized veins. • Individual shears within the system display an increase in strain towards their centres and comprise an anastomosing shear fabric reminiscent of the pattern on a larger scale.
Drill hole Information	• A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: » easting and northing of the drill hole collar » elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar » dip and azimuth of the hole » down hole length and interception depth » hole length. • If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	• Tables containing the drill hole data and the development faces pertaining to this release is attached. • All material drill holes related to the context of this announcement with results available from the last public announcement are reported.
Data aggregation methods	• In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. • Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. • The assumptions used for any reporting of metal equivalent values should be clearly stated.	• Reported drill results are uncut • All relevant intervals to the reported mineralised intercept are length weighted to determine the average grade for the reported intercept. • No metal equivalents are reported.

Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	• These relationships are particularly important in the reporting of Exploration Results. • If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. • If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	• Drilling from the underground is drilled from locations which mean there are variable dips and azimuths due to access limitations • Downhole lengths are reported and true widths are calculated in both the section and plan view utilising a formulae in excel. • True widths are calculated and reported for drill intersections which intersect the lodes obliquely.
Diagrams	• Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	• Appropriate diagrams are included in the report.
Balanced reporting	• Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	• All holes available since the last report are included in the tables • Diagrams show the location and tenor of both high and low grade samples.
Other substantive exploration data	• Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	• No other meaningful data to report.
Further work	• The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). • Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	• These drilling results are part of an ongoing program to define and extend the known resource. • Further infill drilling will be planned on the basis of interpretation of the results as they become available



Competent Persons Statement

The information in this report that relates to Exploration Targets and Exploration Results is based on information compiled by Mr Scott Huffadine (B.Sc. (Hons)), a Competent Person who is a Member of the Australian Institute of Geoscientists. Mr Huffadine is a Director and full time employee of the company. Mr Huffadine is eligible to participate in short and long term incentive plans and holds shares, options and performance rights in the Company as has been previously disclosed. Mr Huffadine has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Huffadine consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.