NORTHERN STAR
RESOURCES LIMITED

ASX ANNOUNCEMENT
20 December 2018

Australian Securities Exchange Code: NST

Issued Capital
Shares 639.45 million
Performance Rights 10.38 million
Current Share Price A$9.00
Market Capitalisation
A$5.7 billion
Cash and Cash Equivalents
30 Sept 2018 - A$277 million

Level 1, 388 Hay St
Subiaco WA 6008

T +6 8 6188 2100
F +6 8 6188 2111
E infoatnsrltd.com
www.nsrltd.com

ABN: 43 092 832 892

AUSTRALIAN OPERATIONS: EXPLORATION UPDATE

OUTSTANDING RESULTS PAVE WAY FOR SUBSTANTIAL INCREASE IN INVENTORY AND MINE LIVES

KEY POINTS

- **Kalgoorlie Operations**

Kanowna Belle:

- **Resource extension drilling at Kanowna Belle has returned outstanding results which are expected to underpin substantial increases in Resource and Reserve inventory; These results include:**
  - **4.4m at 671g/t, including 0.3m at 12,860g/t, 3.6m at 115.3g/t, 12.4m at 4.9g/t and 4.5m at 14.5g/t (true widths)**
- **Recent drilling results support Northern Star's growing view that the Velvet lode at Kanowna Belle will link back to the Lowes deposit supported by the discovery of multiple mineralised structures down plunge from Velvet; Results from these structures include:**
  - **31.3m at 21.7g/t, 15.8m at 9.5g/t, 7.4m at 13.7 g/t, 5.5m at 17.8g/t, 6.5m at 12.4g/t and 9.7m at 6.6g/t (true widths)**
- **Several new structures have been identified in the hanging wall at Kanowna; These will provide new mining areas adjacent to existing infrastructure; Results include:**
  - **6.4m at 14.1g/t, 15.8m at 9.5g/t, 5.5m at 17.8g/t and 2.4m at 10.3g/t (true widths)**

Kundana (NST 100%):

- **Strong drilling results have extended the known mineralisation at the Millennium mine to the north; Results include:**
  - **1.8m at 80.4g/t, 1.6m at 73.2g/t and 2.2m at 29.4g/t (true widths)**
- **Recent surface diamond drilling has extended the known Xmas-Moonbeam mineralisation and greatly improved the understanding of all the geological settings**
- **Decline development from Millennium/Pope John to Xmas-Moonbeam has commenced and will provide an excellent platform to infill drill the significant Inferred Resource**

Kundana EJKV (NST 51%):

- **In-mine extensional drilling across the Rubicon-Hornet-Pegasus mining complex continues to extend the mineralised Pode system and the main K2 structure northwards and down-plunge from Pegasus; Results include:**
  - **2.6m at 35.3g/t, 1.5m at 26.9g/t and 7.5m at 4.5g/t (true widths)**
- **Extensional surface and underground drilling have continued to extend the Raleigh Main Vein mineralisation southwards from the existing resource model; Results include:**
  - **0.7m at 136.2g/t, 1.1m at 54.7g/t and 1.3m at 42.1g/t (true widths)**

- **Further south on the Raleigh structure towards the Golden Hind prospect, surface exploration drilling has confirmed the presence of high-grade intersections including;**
  - **0.6m at 171.6g/t, 1.1m at 89.9g/t and 4.2m at 21.5g/t (true widths)**

South Kalgoorlie Operation:

- **In-mine drilling at the HBJ underground mine has extended all mining surfaces significantly, with Resource and Reserve growth expected next year**
- **Regional exploration across the extensive tenement package has begun to achieve excellent results at several prospects. The six major geological trends are being systematically tested**

Jundee Operation

- **In-mine resource and extension drilling continue to expand the known extent of all the major mining areas with Reserve growth expected next year**
- **A surface drilling program is currently in progress to confirm the structural trends of the Zodiac system; The initial completed wedge hole successfully intersected mineralisation at all modelled target zones together with some additional unmodelled mineralisation**
- **Intersections returned from the first hole of this program include 7.4m at 3.4g/t and 9.8m at 3.6g/t (including 3.2m at 9.2g/t)**
- **The Zodiac system has now been traced over a strike length of approximately 2km and is open in all directions**
- **At the new Ramone deposit, Northern Star has committed to the development of an open-pit this financial year; Extensive infill grade control drilling has been completed with assays indicating an increase in the expected production grade**
- **Excellent surface diamond drilling results have indicated the underground potential of the Ramone system; Results include:**
  - **10.6m at 4.89g/t, 18.3m at 2.3g/t, 6.3m at 2.8g/t and 1.4m at 20.4g/t (true widths)**

Northern Star Resources (ASX: NST) is pleased to announce strong exploration results which lay the foundations for a further significant increase in inventory and mine lives across its Australian operations.

The results, which stem from Northern Star's record A$60 million FY2019 exploration budget, are expected to underpin both increases in Resources and conversion of existing Resources to Reserves when the Company publishes its annual inventory update in the middle of next year.

As at June 30, 2018, Resources at Northern Star's Australian operations stood at 15.9 million ounces, including Reserves of 4Moz.

Northern Star Executive Chairman Bill Beament said the latest results vindicated the Company's strategy to invest heavily in organic growth.

"We continue to find more and more gold around our tier-one operations," Mr Beament said.

"As we have demonstrated repeatedly, this highly successful organic growth strategy drives our industry-leading financial returns.

"Based on these results and the exploration activity planned for the next six months, we expect to generate substantial increases in our Resources and convert more of them into Reserves by the middle of next year.

"This will underpin further extensions in mine lives and provide us with options to continue growing production."

Northern Star intends to publish an operations update on its Pogo Gold Mine in Alaska early in the new year.

Details of Exploration Update

Kalgoorlie Gold Operations

Kanowna Belle

In-mine expansion and exploration drilling adjacent to the existing mining areas has continued with considerable success. These excellent results, together with new discoveries in the Velvet Lower and Porphyry Xenoliths corridors, are expected to underpin a significant increase in Resources and Reserves at Kanowna in mid-2019 (Figure 1)[1].

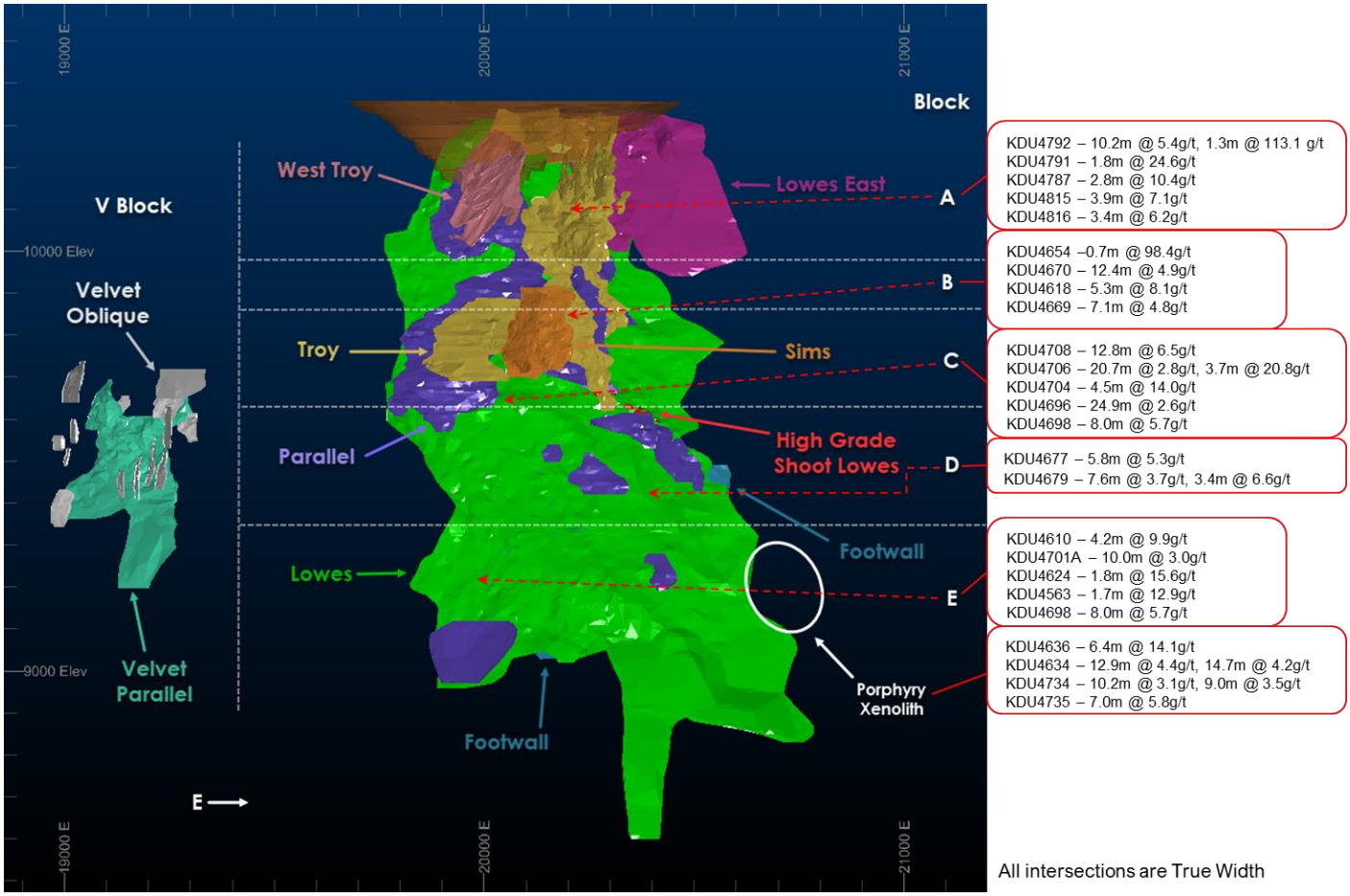

Figure 1 – Long section view Kanowna Belle Mine with significant resource areas

Deep drilling into the hanging wall of the main Lowes ore system across A, B and C blocks has outlined new, strongly mineralised structures up to 150 metres from the Fitzroy Fault which will provide additional mining areas adjacent to existing infrastructure.

In addition, new extensions to the high-grade Sims Lode have been intersected along the eastern margin of C and D blocks including a stunning intersection of 4.4m at 671g/t, including 0.3m at 12,860g/t gold in KDU4623 (Figure 2).

[1] *For all figures in this announcement, all intersection widths are estimated true widths unless stated.*

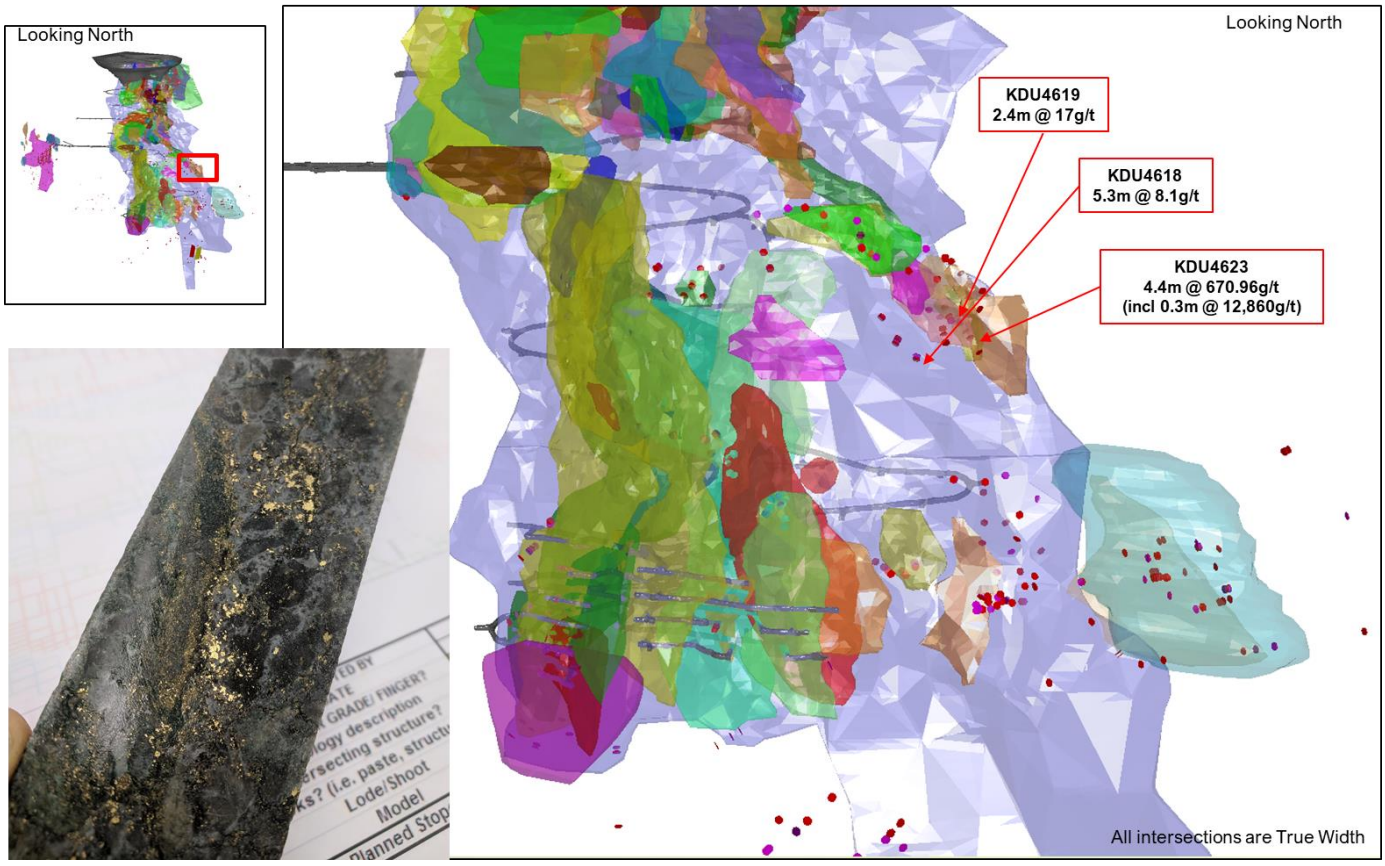

Figure 2 – Hanging wall intersection in D Block East with visible gold intersection in KDU4623

Further down, exploration drilling from the 9245-drill drive has outlined a new mineralised position at Porphyry Xenoliths (KDU4636 - 6.4m at 14.1g/t) extending 260 metres down plunge in a hanging wall position to the east of the controlling Fitzroy Fault (Figure 3). Infill drilling of this new position to the east of E Block continues with a maiden resource expected to be completed in the next quarter.

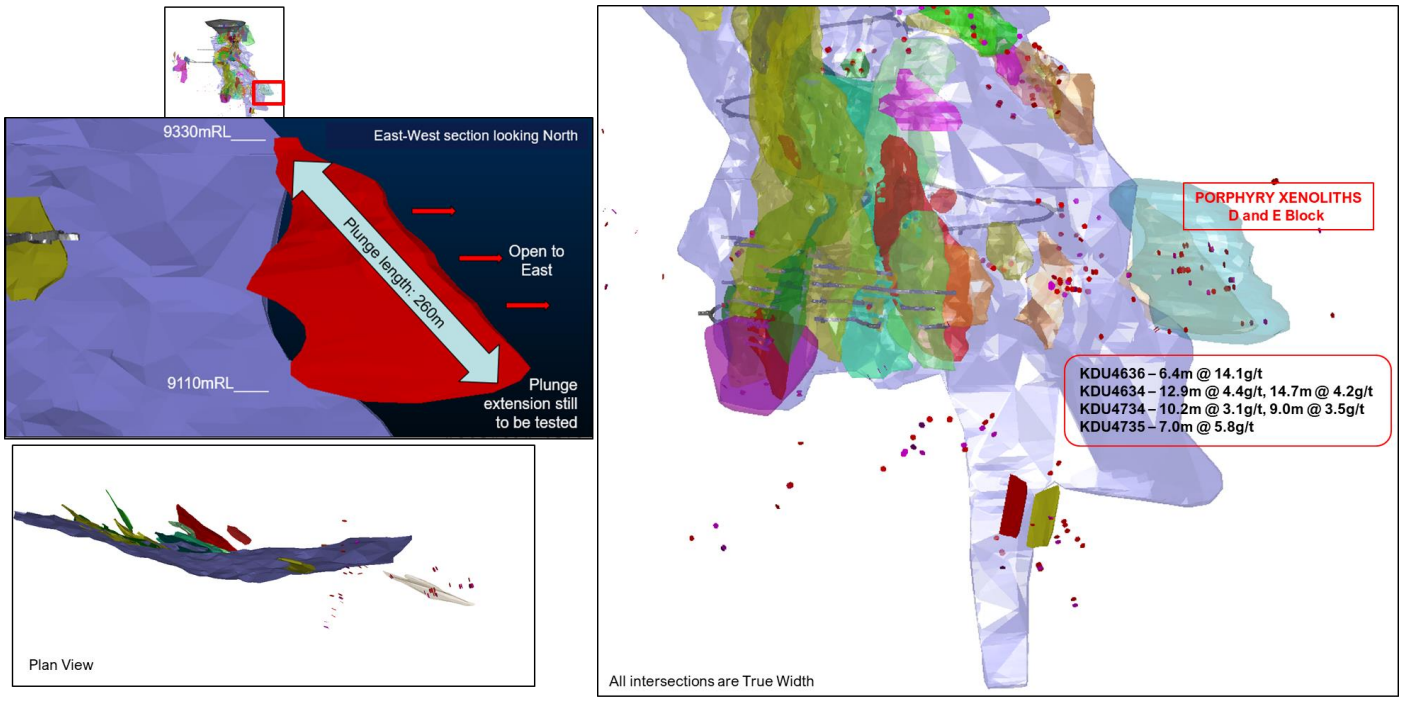

Figure 3 - Long section of Kanowna Belle Mine highlighting new Porphyry Xenoliths mineralisation

At Velvet, recent diamond drilling continues to expand the mineralisation footprint with both parallel zones adjacent to the main production area (Velvet NW, East and HW) and new down plunge extension (Velvet Lower) outlined.

In addition, drilling from the new 9410 DDR and 9112SP platforms has outlined a new mineralised position down plunge from Velvet (Figure 4). The discovery of multiple mineralised surfaces mid-way between Velvet and Lowes ore systems provides strong encouragement that the Velvet trend will ultimately link back into the main Lowes ore deposit.

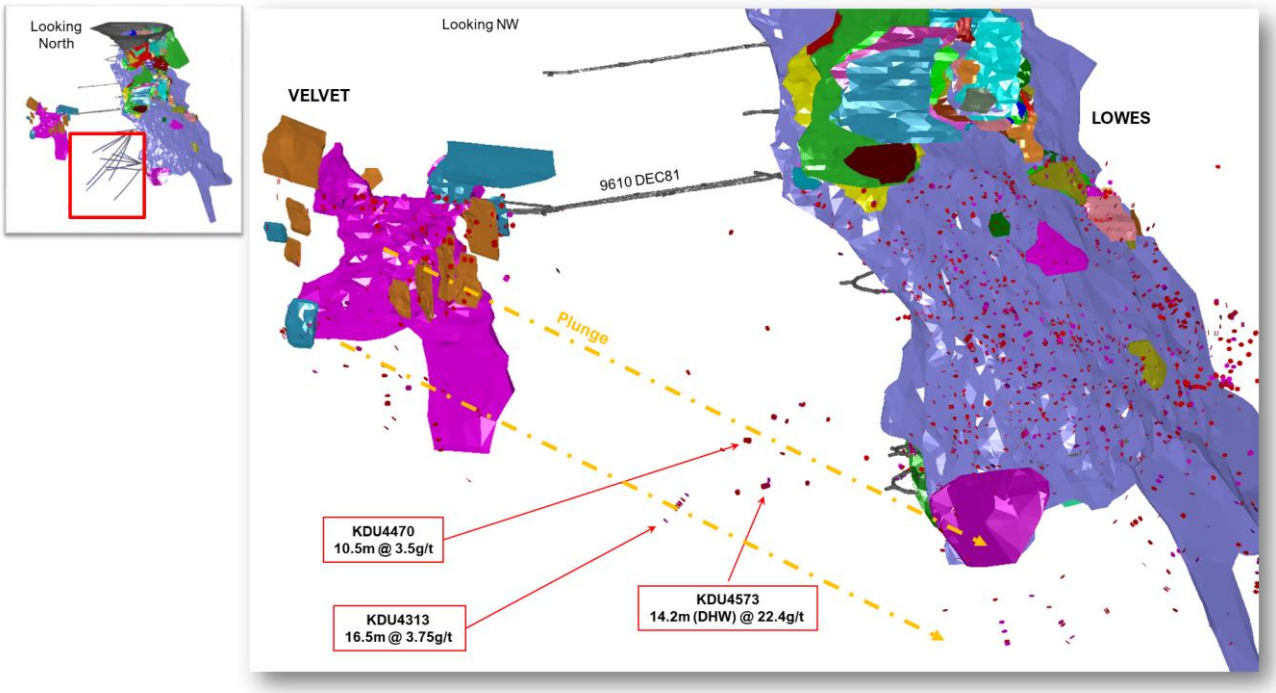

Figure 4 – Long section through Lowes and Velvet highlighting recent significant intersections at Velvet Lower and potential linkage to the main Lowes deposit

Kundana (NST 100%)

With the Millennium Mine in production and underground development progressing into the Pope John deposit, the focus of growth and development drilling has moved further southwards to the Xmas-Moonbeam deposits (Figure 5).

Moonbeam is the southern continuation of the Millennium-Centenary-Pope John K2 mineralisation across the major Lucifer Fault while the adjacent Xmas deposit is the extension of the Strzelecki mineralisation south of the Lucifer Fault. Although the two ore systems are different in character, spatially they straddle the Lucifer Fault and will combine into a single mining operation and enhance to ounces per vertical metre.

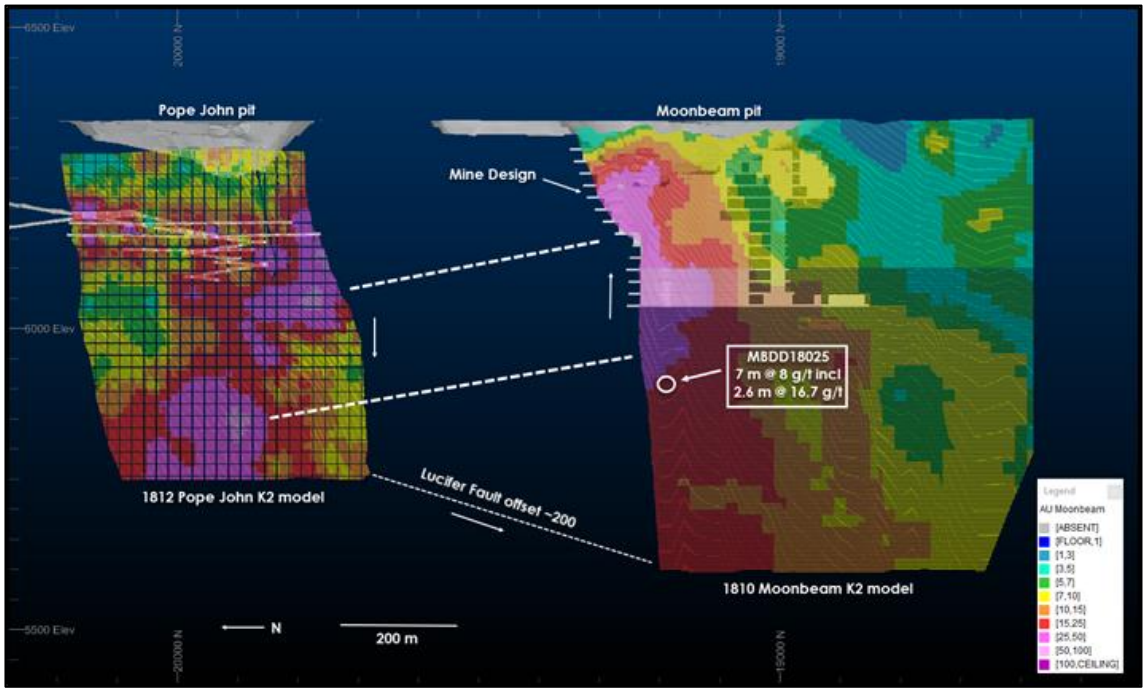

Figure 5 - Pope John-Moonbeam long section across Lucifer Fault

Modelling indicates that Moonbeam is the faulted offset of the Pope John deposit with recent surface diamond drilling extending the Moonbeam resource at depth adjacent to the Lucifer Fault contact (Figure 5) consistent with the north plunge direction evident at Pope John.

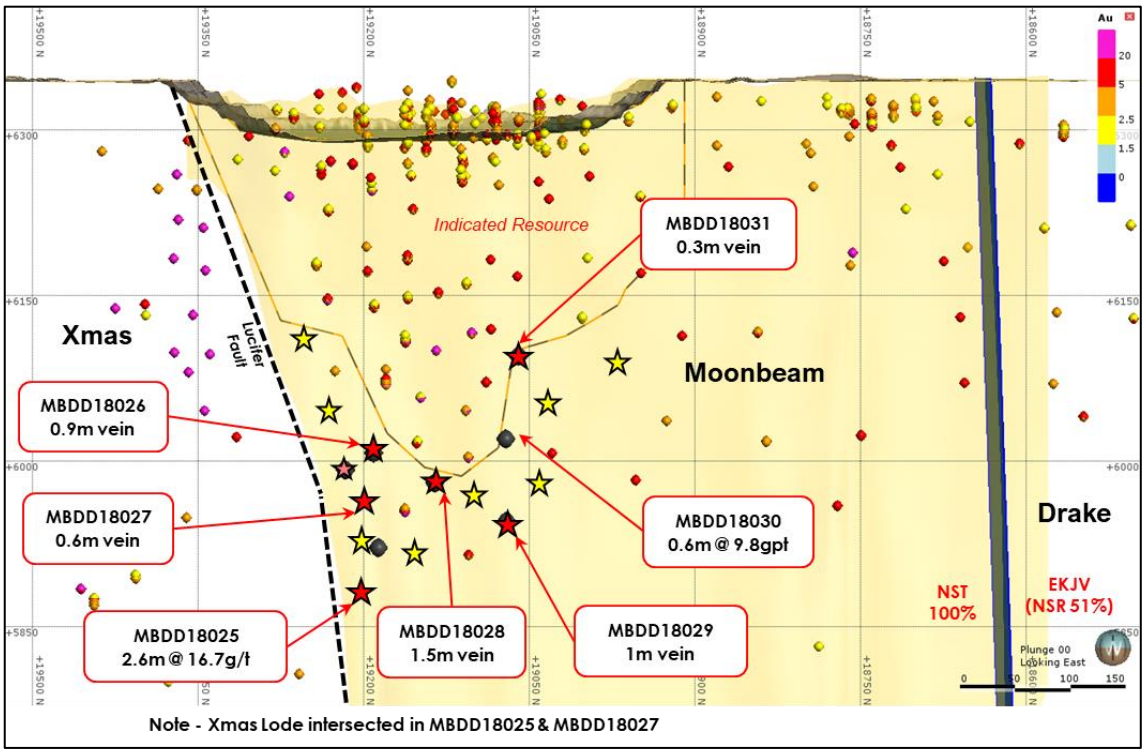

Figure 6 - Long section Xmas-Moonbeam showing current drilling activity

In addition, several Moonbeam drill holes intersected the Xmas structure in the upper portion of the drill holes indicating a flexure in the Lucifer Fault which provides for a potential overlap of the two structures with a southerly strike extension to the Xmas structure. Assay results for these holes are pending (Figure 6).

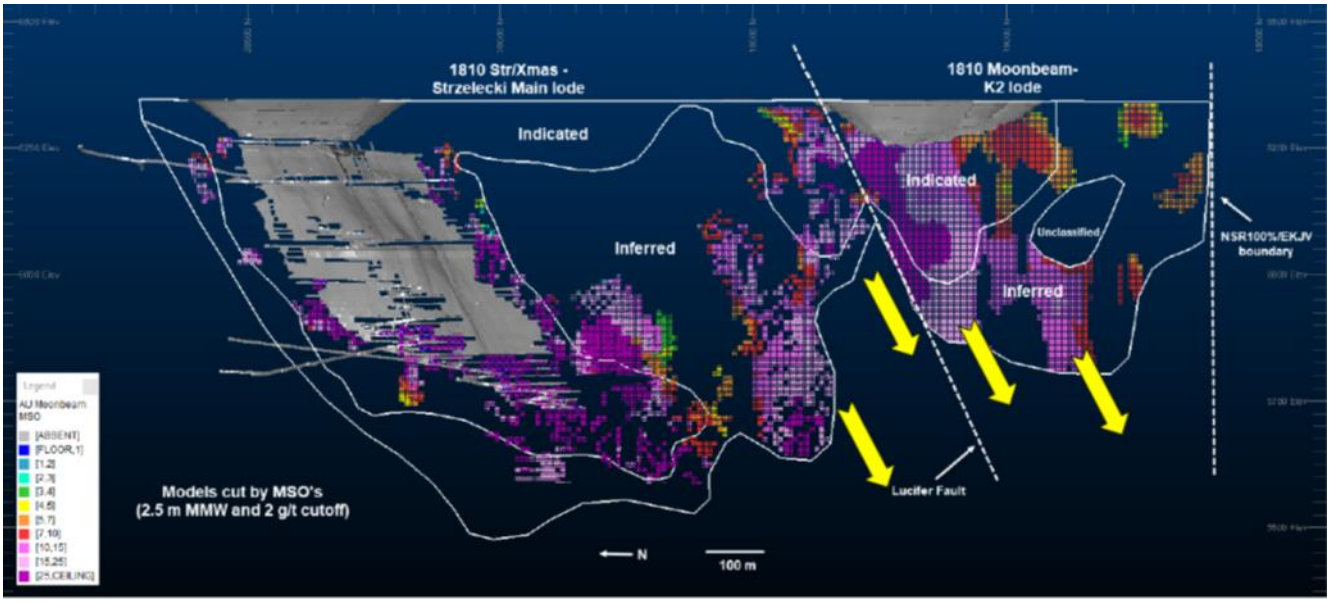

Figure 7 - Moonbeam and Xmas long sections with modelled resource outlines

Decline access development from Pope John to Xmas-Moonbeam has commenced which will provide an excellent underground diamond drill platform to infill drill the significant inferred Resource areas in the Xmas structure (Figure 7).

Kundana EKJV (NST 51%)

In-mine extensional underground diamond drilling across the Rubicon-Hornet-Pegasus mining complex continues to extend the mineralised Pode system and the main K2 structure northwards and down-plunge from Pegasus.

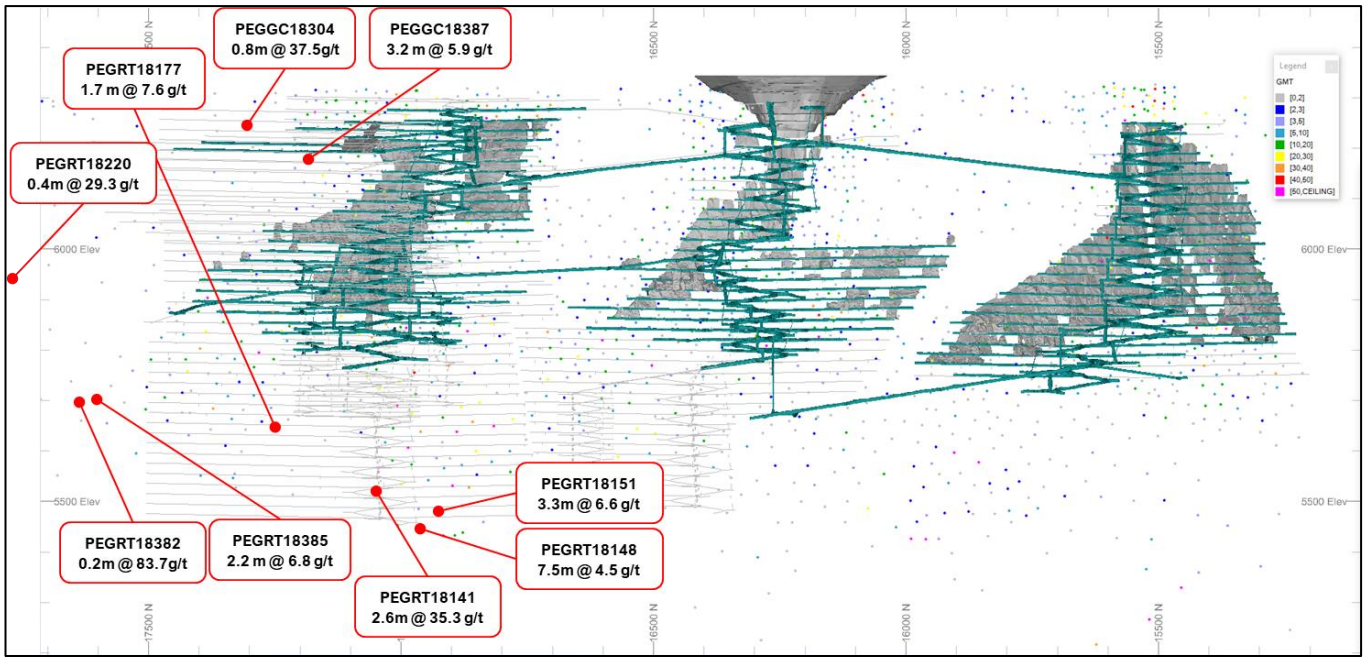

Figure 8 – Long section view of EKJV Rubicon-Hornet-Pegasus mining complex with significant drill hole intersections

With mining operations commencing, the Pode zone, associated with the K2B structure, continues to expand both down dip and northward from the current Pegasus infrastructure with recent high-grade intersections including PEGGC18319 – 1.9m at 34.6g/t, PEGGC18325 – 2.6m at 13.1g/t and PEGGC18304 – 0.8m at 37.5g/t (Figure 8). In addition, sub-parallel hanging wall zones to the Pode system at depth have provided further excellent results with the new Hebe zone returning PEGRSD18145 - 1.2m at 98.0g/t and PEGRSD18146 – 1.0m at 97.0g/t outside the existing resource inventory.

At Raleigh South, extensional surface and underground drilling have continued to extend the Raleigh Main Vein mineralisation southwards from the existing resource model towards the proposed internal Sadler decline development (Figure 9). While grades are variable, the overall economic intersection ratio is consistent with the historical average on the Raleigh structure with the better results including RALRSD18068 – 0.7m at 136.2g/t, RALRSD18185 – 1.1m at 54.7g/t and RALRSD18204 – 1.3m at 42.1g/t.

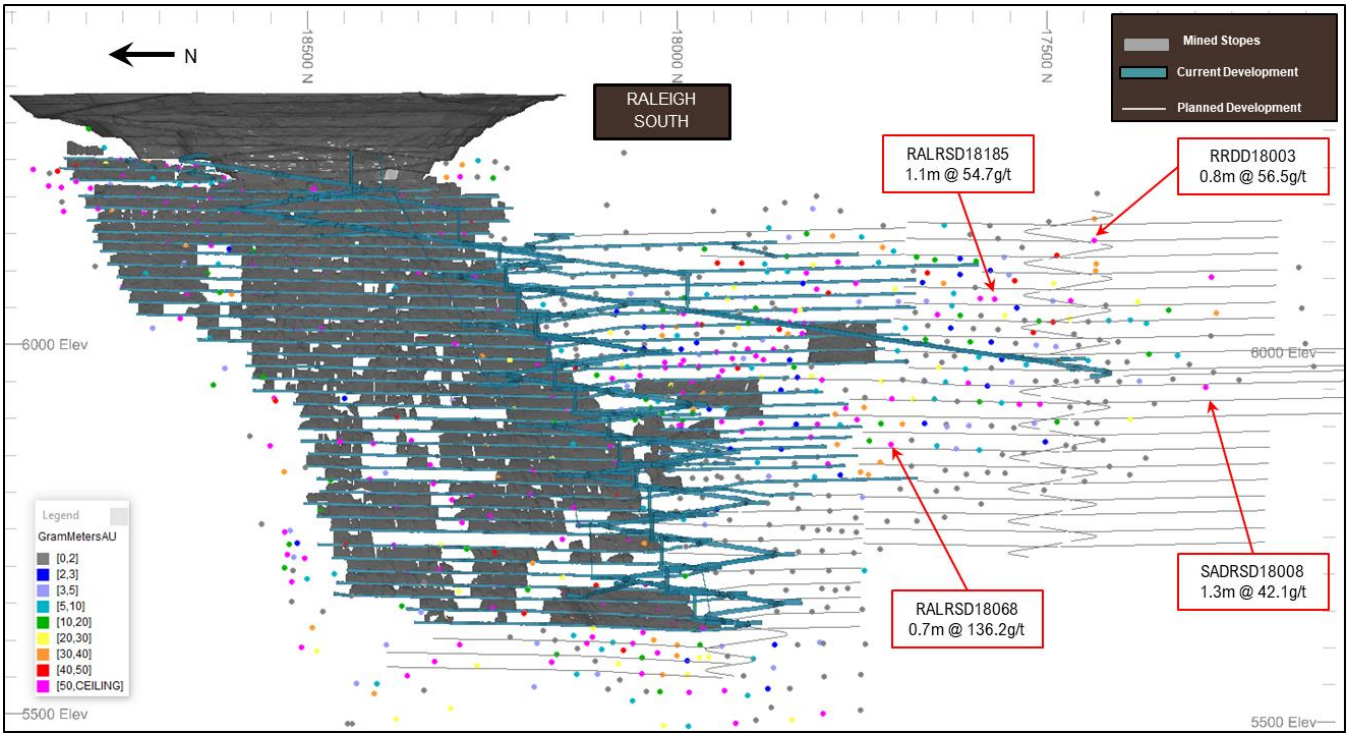

Figure 9 - Raleigh South long section with selected significant intersections

Further south on the Raleigh structure, surface exploration drilling at Sir Walter has confirmed the presence of high-grade intersections another 350 metres south of the proposed internal Sadler decline. The southernmost and last hole in the current program, SWCD18108, recorded the best result of 4.2m at 21.5g/t with the Raleigh structure remaining open in all directions.

South Kalgoorlie

HBJ Mine

In-mine drilling at the HBJ underground mine has advanced ahead of the current production areas with resource definition and extensional drilling programs at COZ, Jubilee and NOZ mine areas.

Down plunge drilling at COZ has extended the current mining block with intersections within, and on the contacts of, the central quartz-feldspar porphyry body including HBJUG0497 – 11.2m at 8.1g/t and HBJUG0486 – 3.7m at 7.1g/t.

Similarly, within the Jubilee area, initial extensional drilling has returned better than anticipated results from the eastern side of the ore zone including HBJUG0565B – 6.1m at 5.2g/t, HBJUG0553B – 2.7m at 9.7g/t and HBJU0552 – 3.5m at 7.7g/t.

Definition drilling at NOZ has achieved excellent widths and grades adjacent to, and beneath, the current mining front including HBJUG0525 -11.6m at 10.0g/t, HBJU0527 – 8.5m at 13.1g/t HBJU0511 – 10.5m at 6.1g/t and HBJU0530 – 7.3m at 7.5g/t. In addition, extensional drilling northwards from a new drill platform has commenced with first results including HBJUG0594 – 3.8m at 10.4g/t indicating potential higher resource grades from the NOZ area.

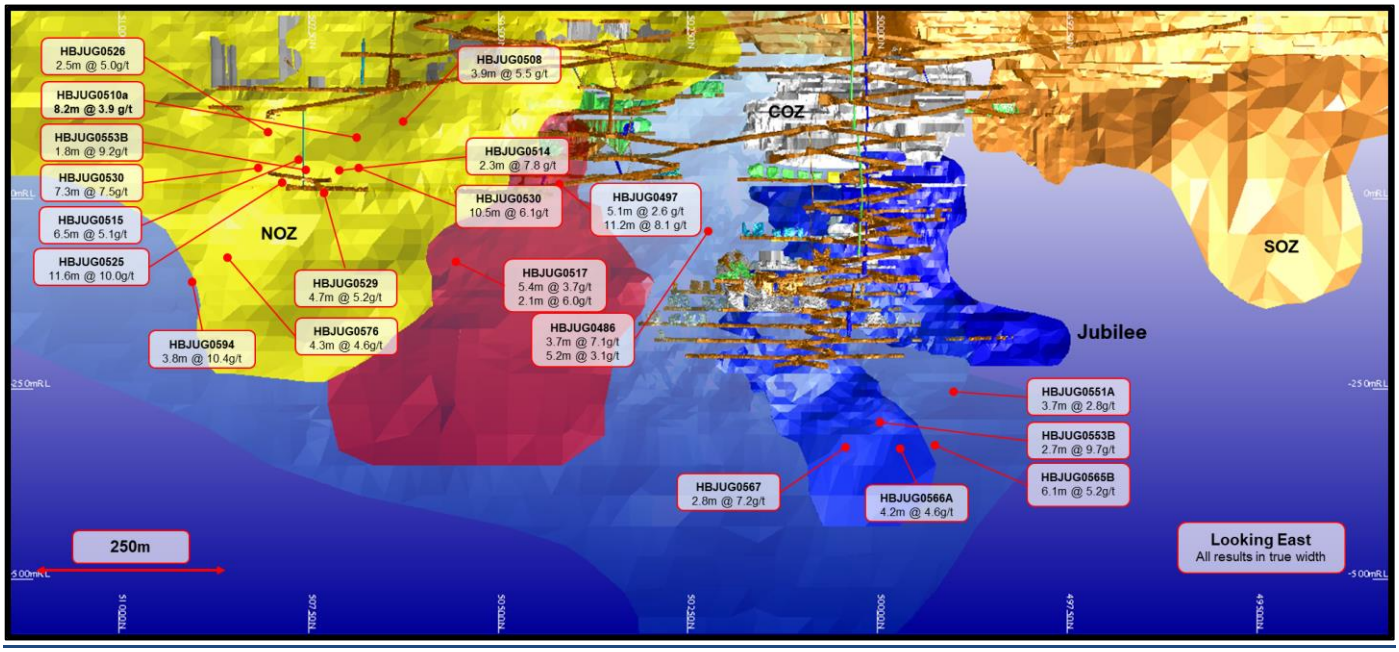

Figure 10 – South Kalgoorlie HBJ Mine – Significant drill hole intersections

Regional

Regional exploration across the extensive South Kalgoorlie tenements has begun to achieve success in several areas.

At the Tornado prospect within the Zuleika Shear corridor, diamond drilling beneath historical shallow oxide mineralisation returned encouraging multiple intersections from the first hole including TODD 18162 – 15.0m at 1.01g/t from 97m and 26.2m at 1.64g/t from 152.5m (Figures 12 and 13).

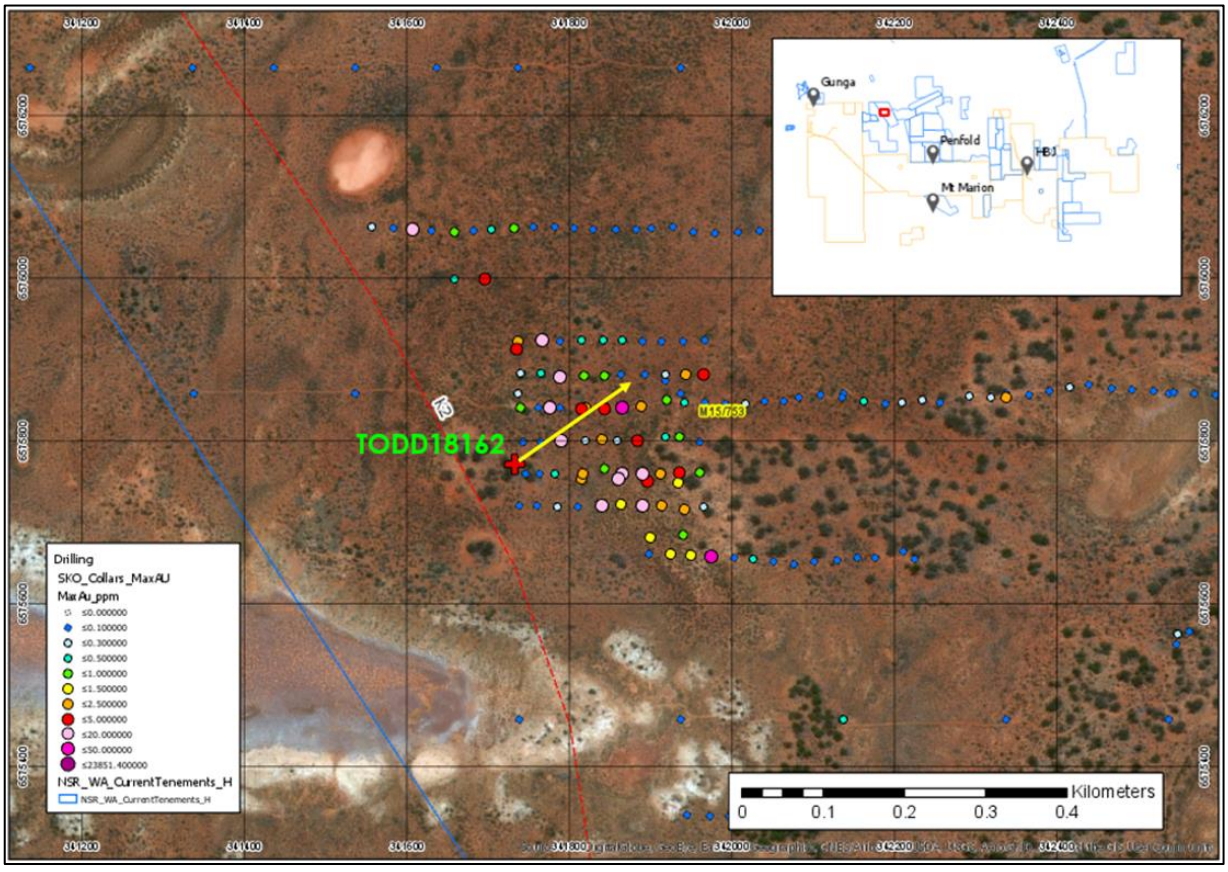

Figure 11 – South Kalgoorlie - Tornado Prospect Location Plan

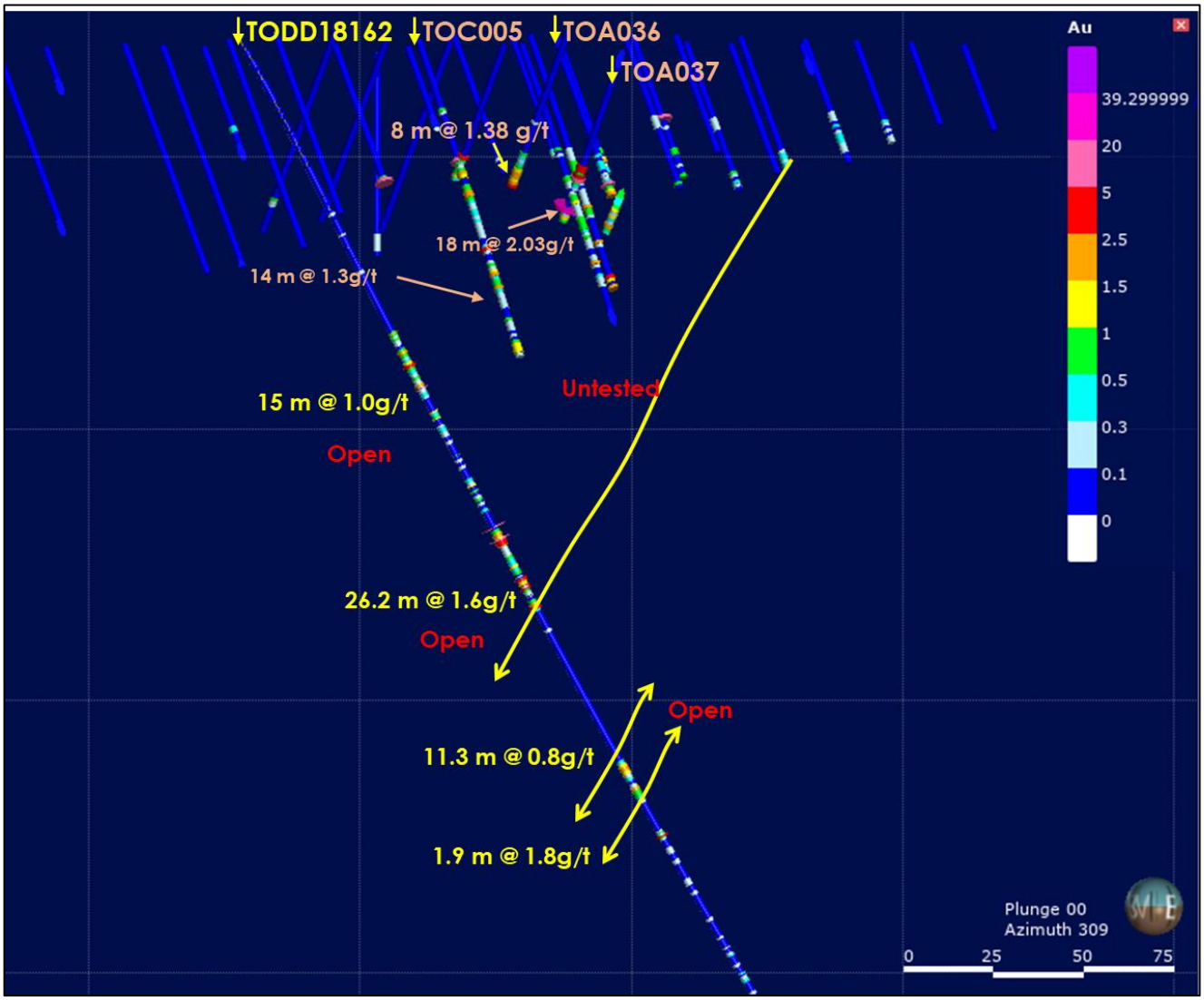

Figure 12 - Tornado Prospect – TODD18161 cross section looking north with significant assay results

Further east at the new Glasswing prospect, reconnaissance RC drilling of historic RAB anomalies has returned a strong initial result of XGRC18005 – 21.0m at 2.3g/t from 58m depth. Further step out drilling along strike is currently in progress.

Broad spaced reconnaissance diamond drilling below the historic Samphire open pit has outlined a series of stacked mineralised veins containing visible gold across a strike length of at least 400 metres. Results from the first two holes include SPDD 18001 - 1.4m at 8.9g/t from 222.9m, 2.0m at 43.8g/t from 233.6m, 3.3m at 4.5g/t from 305.6m and SPDD18002 – 1.9m at 5.2g/t from 151.3m, 0.35m at 17.6g/t indicate the potential for a significant mineralised system (Figure 13)

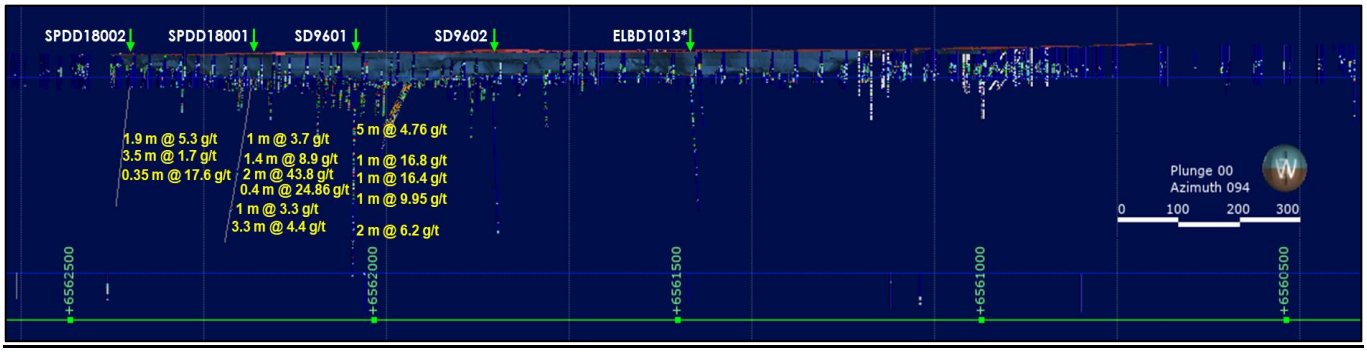

Figure 13 - Long Section through Samphire Prospect looking west highlighting recent diamond drill holes

Jundee

In-mine resource and extension drilling continue to expand the known extent of all the major mining areas at Jundee while scoping the potential of the new Zodiac discovery to the south of the main production areas.

Zodiac

The Zodiac system, represented by a broad zone with multiple mineralised intercepts, has been traced over a strike length of approximately 2km to date, remaining open in all directions (Figure 14).

A surface diamond drilling program of 4 wedge holes off the original JRD10447 diamond drill hole at Zodiac is currently in progress to confirm the structural trends of the Zodiac system. The initial wedge JRD10447W4 has been completed at 2,165m depth successfully intersecting mineralisation at all modelled target zones together with some additional unmodelled mineralisation. Combined intersections include 7.36m at 3.44g/t from 1,836.0m, 9.78m at 3.56g/t from 1,920.3m including 3.18m at 9.23g/t from 1,926.9m.

The second wedge hole, currently at 1,792m, has also successfully intersected multiple zones of extensive alteration and veining at the target depths and is drilling ahead to a total planned depth of 2,200m.

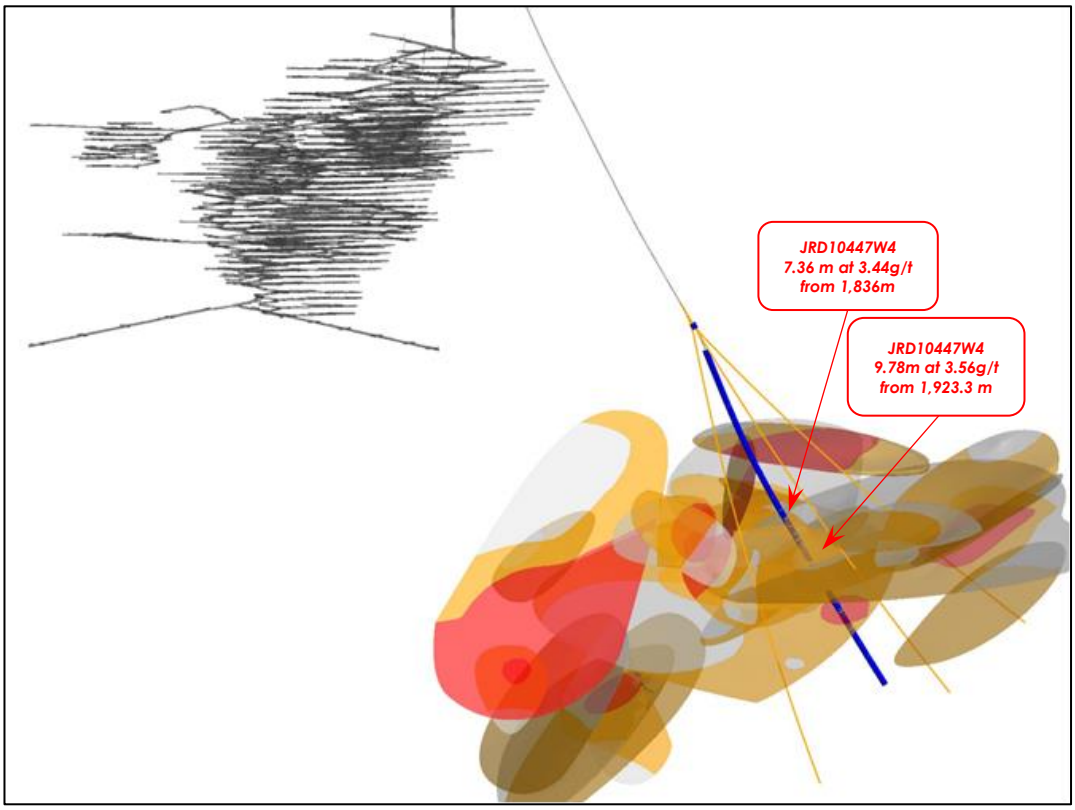

Figure 14 – Schematic up long section of Zodiac target area with JRD10447W4 drill hole intersections

Ramone

Northern Star has committed to the development of a new open-pit mining operation at the Ramone site during the current financial year. Permitting and a range of pre-development activities have commenced at the site together with the initial grade control drilling program for the upper levels of the planned open pit.

Infill grade control drilling has been completed over approximately 75% of the planned pit area to a vertical depth of approximately 60 metres. Initial assay results have significantly exceeded expectations from resource modelling indicating the potential for increased production from the upper portion of the open pit.

Selected better results include: NSRJRC11676 – 11.5m at 11.4g/t from 3m; NSRJRC11572 – 15.0m at 5.5g/t from 9m; NSRJRC11655 – 13.5m at 4.4g/t from surface; NSRJRC11555 - 5.0m at 10.6g/t from 12m; NSRJRC688 – 20.0m at 2.6g/t from16m and NSRJRC700 – 11.5m at 5.4g/t (all true widths).

In addition, surface diamond drilling has commenced to confirm the underground potential of the Ramone system beneath the planned open pit. To date, a total of 5 holes have been completed revealing several discrete high-grade cores within broader stockwork envelopes at depth with the deepest intersection in NSRJRD10489 returning the excellent result of 17.6m at 4.9g/t from 334m (Figure 15).

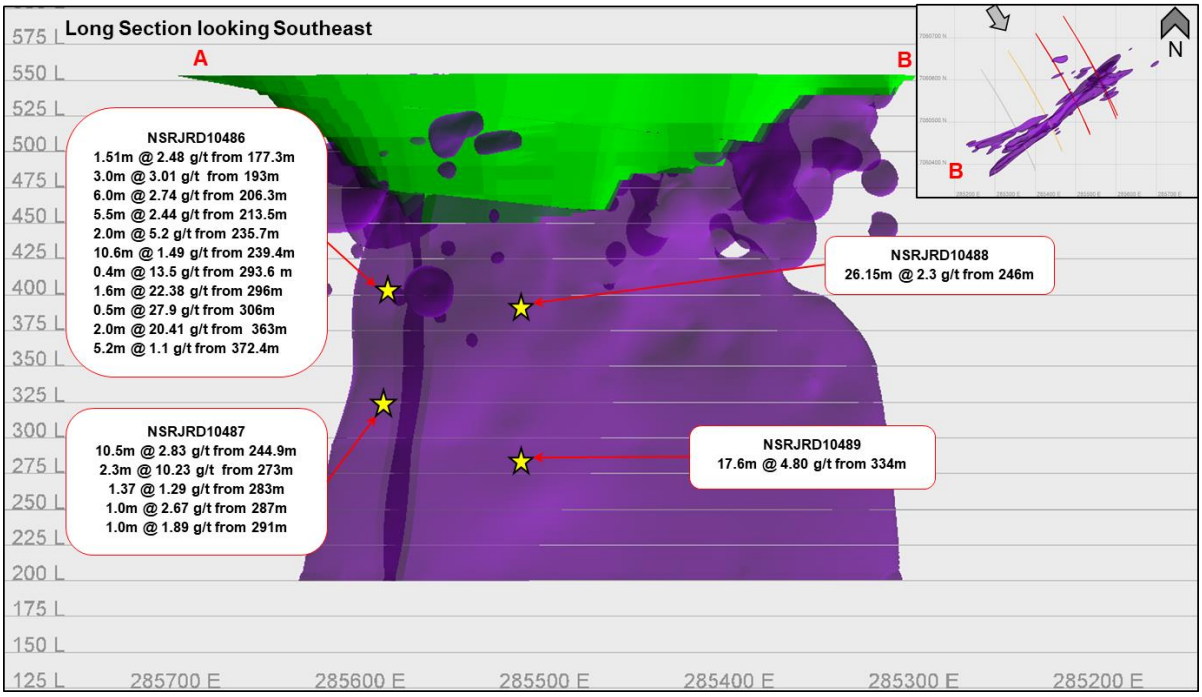

Figure 15 - Long section looking south west through Ramone deposit with diamond drilling results

Within the broader Ramone area, RC drilling has extended the Ramone mineralisation to the southwest including NSRJRC11383 – 5m at 14.24g/t from 65m. Along strike to the north-east, RC drilling at the Mosley prospect has identified extensions to the Ramone trend indicating the potential for additional small open pit development (Figure 16).

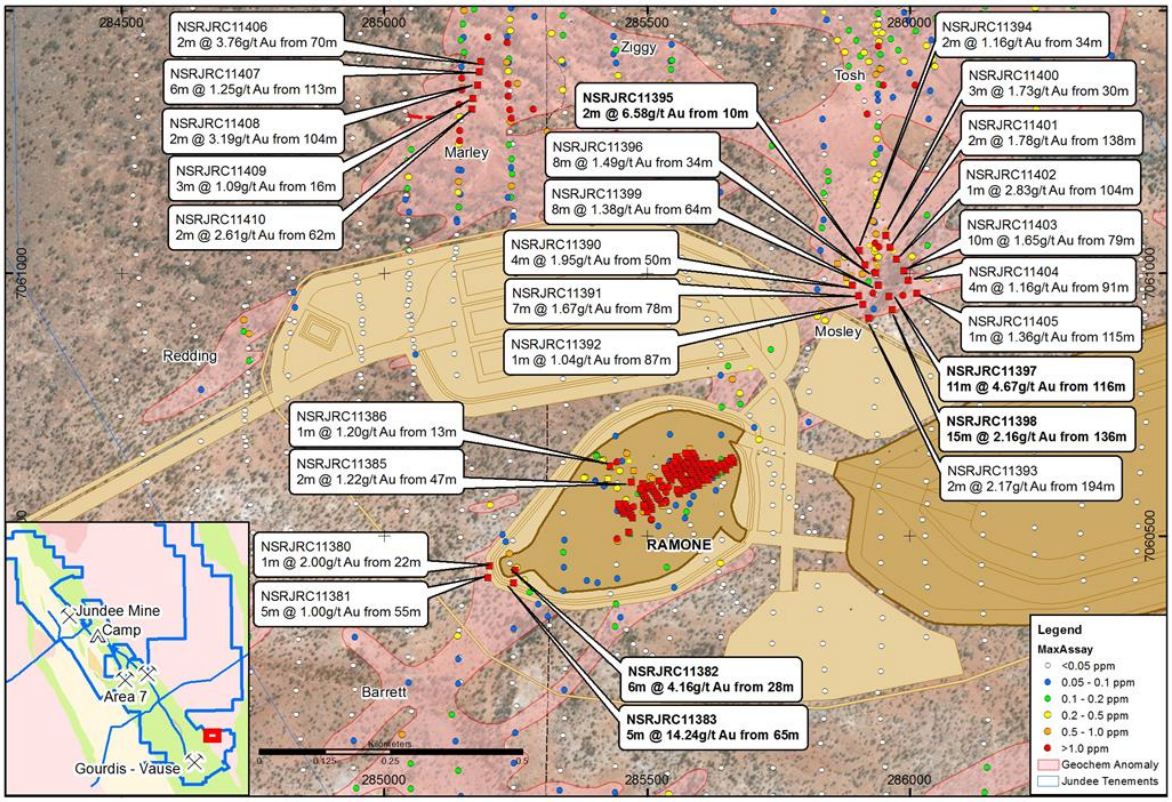

Figure 16 - Plan view of Ramone region showing extensional RC drilling results

Central Tanami Joint Venture (NST 40%)

As part of the ongoing evaluation of the Central Tanami Project, a program of RC and diamond drilling was completed beneath the existing treatment plant infrastructure testing for potential shallow extensions to the main Hurricane-Repulse mineralisation.

RC drilling intersected significant gold mineralisation at varying depths in all 23 drill holes completed beneath all major infrastructure at the CTP Plant (Figure 17).

Figure 17 – Central Tanami - Hurricane-Repulse Collar Plan

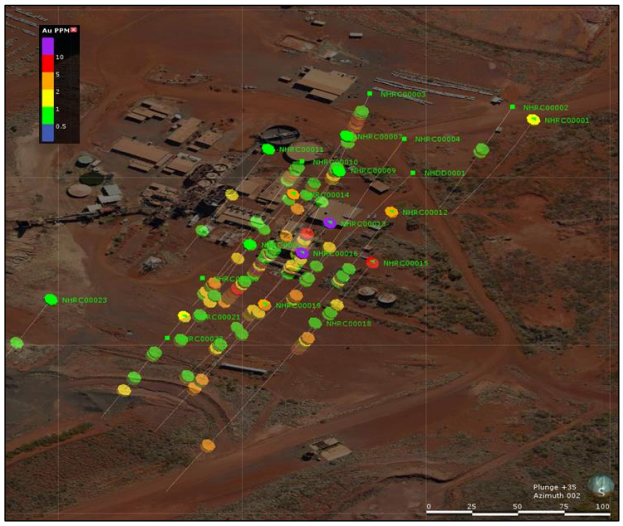

Figure 18 - Significant RC gold intercepts (Oblique view looking NW)

Significant intersections from the RC drilling program include:

NHRC00003 - 3m at 20.47g/t Au from 140m and 12m at 4.58g/t Au from 147m; NHRC00007 - 19m at 4.64g/t Au from 136m; NHRC00009 - 14m at 3.19g/t Au from 150m, and NHRC00015 - 15m at 2.89g/t Au from 92m.

In addition, single diamond drill hole testing the down plunge continuity of the new mineralised zones, intersected a wide zone of significant gold mineralisation located approximately 130 metres below the base of the existing Hurricane pit to the north. Significants assays included NHDD001 - 8.5m (dth) at 6.6 g/t gold from 177.9m depth confirming the potential for significant depth extensions to the Hurricane-Repulse mineralisation beneath the Central Tanami Processing Plant (Figure 18).

Further south at Jim's, diamond drilling beneath the existing Jim's open pit also returned significant gold intersections up to 170 metres beneath the base of the open pit. Significant results included: JDD001 - 7.2m at 2.31g/t Au from 184.5m and 26m at 3.88g/t Au from 224m; JDD002 – 10.0m at 5.70g/t gold from 401.0m; JDD003 – 8.0m at 3.94g/t gold from 219.1m; and JDD004 - 20.5m at 2.20g/t gold from 253.5m and 10.3m at 1.11g/t gold from 258.56m (Figure 19).

Further extensional RC and diamond drilling is planned at both locations commencing in late quarter three following cessation of the Wet season.

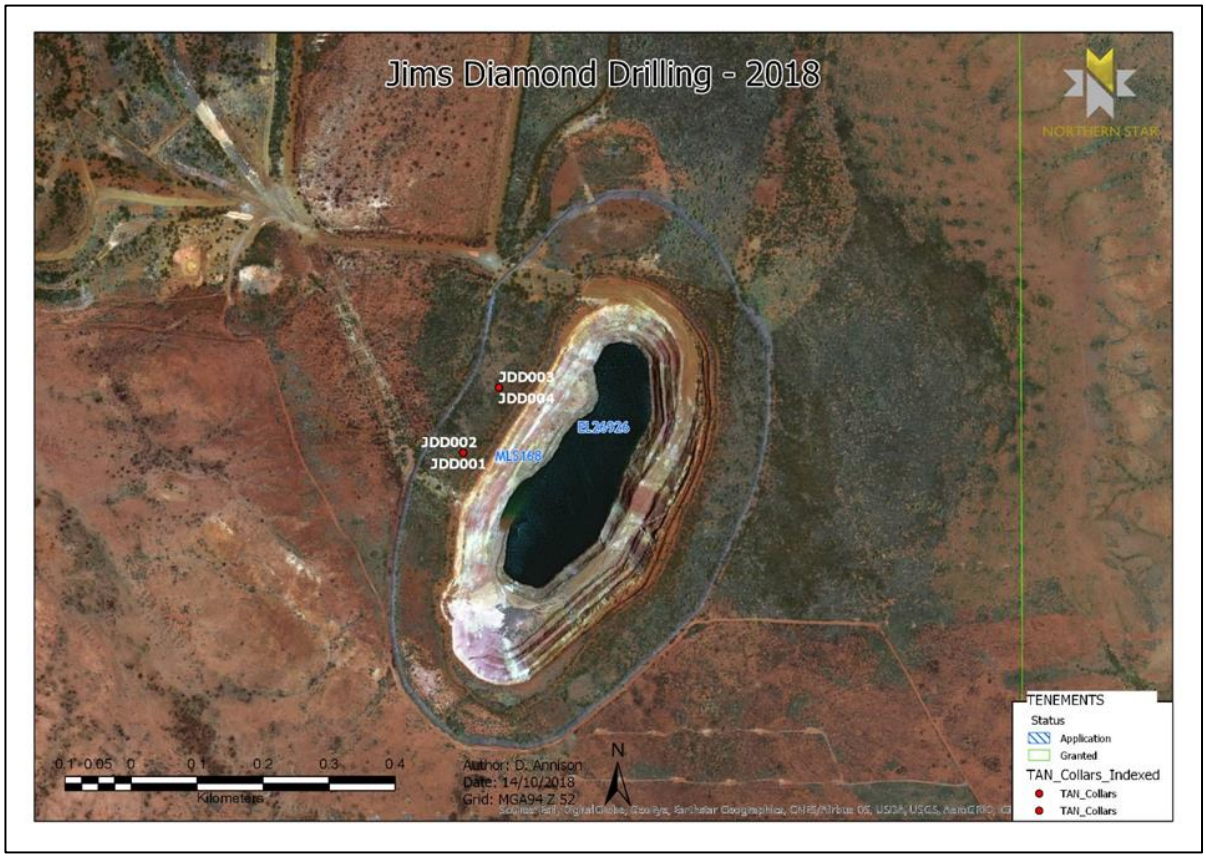

Figure 19 - Plan view of Jim's open pit and location of diamond drill holes

Yours faithfully

BILL BEAMENT
Executive Chairman
Northern Star Resources Limited

Investor Relations Enquiries:
Luke Gleeson
Northern Star Resources Limited
T: +61 8 6188 2103
E: lgleeson@nsrltd.com

Media Enquiries:
Paul Armstrong
Read Corporate
T: +61 8 9388 1474
E: paul@readcorporate.com.au

Competent Persons Statements

The information in this announcement that relates to exploration results, data quality, geological interpretations for the Company's Australian Project areas is based on information compiled by Michael Mulroney, a Competent Person who is a Member of the Australasian Institute of Mining and Metallurgy and a full-time employee of Northern Star Resources Limited. Mr Mulroney has sufficient experience that is relevant to the styles of mineralisation and type of deposits under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves" for the Company's Australian Project areas. Mr Mulroney consents to the inclusion in this announcement of the matters based on this information in the form and context in which it appears.

Forward Looking Statements

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APPENDIX A – DRILL RESULTS

Table 1 - Kanowna Significant Intersections

KANOWNA SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
A BLOCK											
KDU4815	20067	49949	10091	3	235	88	18.2	20.0	1.9	4.9	0.7
							27.0	**34.9**	**7.9**	**7.1**	**3.9**
KDU4816	20067	49949	10090	-12	227	82	**17.0**	**24.0**	**7.0**	**6.2**	**3.4**
							36.8	**37.1**	**0.3**	**31.7**	**0.2**
KDU4816	20067	49949	10090	-12	227	82	52.4	56.8	4.4	2.9	2.1
KDU4817	20067	49949	10090	-22	219	145	**19.0**	**22.0**	**3.0**	**15.0**	**1.3**
							39.4	44.0	4.6	2.3	2.0
							54.7	60.9	6.2	3.5	2.7
							120.7	**125.6**	**4.9**	**3.9**	**3.4**
KDU4818	20067	49949	10090	-17	212	129.2	**18.71**	**21.55**	**2.84**	**10.1**	**1.6**
							43.00	47.20	4.20	4.2	2.3
KDU4847	20068	49949	10093	34	213	43.8	16.00	17.38	1.38	2.9	1.2
KDU4784	20073	49949	10093	38	117	37	**4.0**	**12.2**	**8.2**	**2.4**	**5.0**
KDU4785	20071	49949	10093	40	172	32	22.7	28.6	5.9	1.0	5.0
KDU4786	20071	49949	10092	12	137	37	33.8	36.5	2.7	2.2	2.0
KDU4787	20069	49948	10091	3	177	36	10.2	12.1	1.9	3.1	1.7
							21.0	**24.1**	**3.1**	**10.4**	**2.8**
							27.7	30.6	3.0	2.9	2.6
KDU4788	20070	49949	10090	-20	146	61	25.8	30.2	4.4	2.8	2.2
							31.6	**33.9**	**2.3**	**10.0**	**1.1**
							36.5	38.9	2.4	2.4	1.2
							43.2	45.3	2.2	3.3	1.1
KDU4789	20070	49949	10090	-30	166	58	**18.8**	**26.2**	**7.4**	**5.9**	**2.3**
							31.1	33.3	2.2	3.0	1.1
							44.6	44.9	0.3	12.0	0.1
KDU4790	20069	49949	10090	-21	188	51	7.7	12.4	4.7	3.0	3.0
							19.8	**21.5**	**1.7**	**13.0**	**1.1**
							46.0	46.6	0.6	12.5	0.3
KDU4791	20067	49949	10090	-15	231	72	**20.0**	**24.4**	**4.4**	**6.7**	**2.8**
							56.4	**59.2**	**2.8**	**24.6**	**1.8**
KDU4792	20067	49949	10090	-5	237	71	**20.0**	**34.4**	**14.4**	**5.4**	**10.2**
							60.4	**62.2**	**1.8**	**113.1**	**1.3**
KDU4726	19895	49872	10055	23	71	95	52.8	57.0	4.2	3.4	2.1
KDU4727	19895	49872	10055	14	77	91	62.5	65.5	3.0	2.7	1.8
KDU4728	19895	49872	10055	18	80	103	**64.6**	**77.0**	**12.4**	**3.3**	**6.5**
							90.2	92.4	2.2	2.2	1.1
KDU4729	19895	49872	10055	12	85	195	**90.0**	**97.0**	**7.0**	**3.4**	**4.0**
							135.0	137.3	2.3	3.5	1.3
KDU4795	19895	49872	10055	23	62	92	**67.0**	**76.2**	**9.2**	**3.2**	**5.5**
KDU4822	19930	49877	10049	-34	116	80	35.0	35.8	0.8	0.0	0.0
KDU4823	19931	49877	10050	-3	91	75	47.6	48.9	1.3	4.8	0.6
							53.7	54.7	1.0	2.7	0.4
KDU4824	19932	49879	10050	3	67	48	**32.0**	**35.9**	**3.9**	**6.8**	**2.5**
KDU4825	19932	49878	10051	12	96	115	72.4	76.4	4.1	2.7	0.9
							79.0	84.0	5.0	3.3	1.1
KDU4826	19929	49880	10051	21	69	47	26.0	27.6	1.6	0.0	0.0
KDU4827	19915	49889	10054	35	43	53	15.7	18.9	3.2	7.5	1.3
B BLOCK											
KDU4618	**20461**	**49672**	**9511**	**-33**	**212**	**156**	**101.8**	**115.0**	**13.2**	**8.1**	**5.3**
KDU4622	20464	49672	9511	-33	173	128	**66.3**	**68.8**	**2.4**	**10.2**	**1.0**
							90.0	96.0	6.0	3.1	2.5
							103.1	109.0	5.9	3.5	2.5
KDU4653	20381	49915	9860	-30	131	441	215.6	217.0	1.4	3.5	Unknown
							231.0	237.0	6.0	2.7	Unknown
							279.0	279.5	0.5	10.1	Unknown
							308.0	310.0	2.0	2.4	Unknown
KDU4654	20381	49915	9861	-10	118	393	274.0	283.4	9.4	2.4	2.5
							306.1	312.0	5.9	2.1	1.5
							341.5	**342.2**	**0.8**	**98.4**	**0.7**
KDU4655	20381	49915	9861	7	130	342	290.0	291.0	1.0	4.5	0.1
							181.0	187.0	6.0	2.5	0.8
							221.5	230.7	9.1	2.7	1.1
KDU4657	20381	49915	9862	24	97	436	315.6	316.0	0.4	13.6	0.1
							315.6	316.0	0.4	13.6	0.1
							339.0	345.0	6.0	3.0	1.0
KDU4667	20085	49937	9967	19	186	30	27.1	29.7	2.6	1.7	Unknown
KDU4669	20091	49938	9968	25	171	66	32.3	40.8	8.5	4.8	7.1
							50.0	53.1	3.1	3.2	2.6
							58.0	58.9	0.9	10.0	0.8
KDU4670	**20091**	**49938**	**9967**	**17**	**171**	**67**	**32.1**	**45.0**	**12.9**	**4.9**	**12.4**
							47.6	48.0	0.4	11.4	0.4
							51.0	52.2	1.2	3.2	1.1
C BLOCK											
KDU4580	20146	49742	9809	-5	226	273	167.9	169.6	1.7	12.3	Unknown
							185.3	191.9	6.7	13.8	Unknown
KDU4581	20146	49742	9810	11	224	208	143.0	146.0	3.0	2.7	Unknown
							185.1	185.4	0.3	14.2	Unknown
KDU4532	19860	49810	9685	15	179	204	**18.0**	**26.0**	**8.0**	**5.3**	**7.6**
							31.0	**40.5**	**9.5**	**3.1**	**9.1**
							58.9	**63.0**	**4.1**	**6.9**	**4.0**
							91.6	94.4	2.8	3.7	2.7
KDU4534	19860	49810	9685	17	199	269	16.0	17.5	1.5	3.1	1.4
							34.7	**51.0**	**16.3**	**2.6**	**15.3**
							117.0	119.0	2.0	2.7	1.8
KDU4570	19819	49827	9687	30	213	210	18.3	19.8	1.5	2.7	1.4
							60.0	**63.4**	**3.4**	**5.0**	**2.9**
KDU4578	20146	49742	9810	-10	210	210	161.2	161.8	0.6	20.0	0.3
KDU4582	20146	49742	9810	5	230	234	**81.2**	**81.6**	**0.4**	**53.1**	**0.4**

KANOWNA SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
							226.6	227.2	0.6	6.0	0.5
							230.7	231.2	0.4	6.1	0.4
KDU4690	20142	49745	9809	1	234	184	**3.0**	**7.0**	**4.0**	**3.5**	**3.7**
							60.2	62.7	2.5	2.9	2.1
							93.0	95.0	2.0	2.3	1.9
KDU4691	20141	49745	9809	13	234	183	**4.0**	**8.0**	**4.0**	**4.1**	**3.6**
							47.7	50.6	2.9	2.1	2.6
							77.0	**80.0**	**3.0**	**5.6**	**2.8**
							106.0	**107.0**	**1.0**	**61.1**	**1.0**
							112.3	**113.0**	**0.7**	**18.8**	**0.7**
							121.0	**124.0**	**3.0**	**6.2**	**2.9**
KDU4692	20141	49745	9809	3	244	213	50.9	52.2	1.3	3.2	1.1
								60.4	4.4	2.4	4.0
								79.0	2.0	2.7	1.8
								103.0	1.2	3.8	1.1
								106.2	0.6	12.1	0.5
								117.0	1.8	3.4	1.6
								142.5	2.5	2.1	2.3
KDU4693	20141	49746	9811	26	236	195	**6.1**	**8.2**	**2.1**	**8.9**	**1.9**
							19.1	**24.6**	**5.5**	**2.3**	**5.0**
							175.0	175.7	0.7	12.4	0.4
							182.0	184.0	2.0	3.2	1.9
KDU4695	20141	49746	9809	9	254	401	**13.0**	**22.0**	**9.0**	**2.7**	**9.0**
							30.0	**33.6**	**3.6**	**3.2**	**3.4**
							41.0	43.5	2.5	4.2	1.8
							46.0	48.0	2.0	4.8	1.9
							66.0	66.3	0.3	10.6	0.3
							80.0	83.0	3.0	2.1	2.0
							93.4	96.7	3.3	2.6	3.2
							102.6	**105.0**	**2.4**	**4.4**	**2.4**
							136.2	137.9	1.7	4.0	1.7
							219.4	220.0	0.6	10.3	0.6
							225.3	226.6	1.3	3.3	1.3
KDU4696	**20140**	**49746**	**9809**	**18**	**257**	**222**	**19.0**	**46.8**	**27.8**	**2.6**	**24.9**
							62.0	62.3	0.3	11.1	0.3
							84.0	**86.0**	**2.0**	**5.7**	**1.8**
							130.0	**136.1**	**6.1**	**3.4**	**5.0**
KDU4697	20140	49746	9809	19	251	177	**16.0**	**21.3**	**5.3**	**3.4**	**5.2**
							41.0	**45.4**	**4.4**	**3.6**	**4.4**
							80.6	**82.8**	**2.2**	**5.0**	**2.1**
							126.8	128.2	1.4	2.3	1.4
KDU4698	**20141**	**49746**	**9810**	**31**	**251**	**192**	**10.0**	**18.0**	**8.1**	**5.7**	**8.0**
							26.0	29.0	3.0	3.2	3.0
							36.1	**40.0**	**3.9**	**3.0**	**3.9**
							49.0	**53.3**	**4.3**	**2.8**	**4.3**
							73.0	75.4	2.4	4.0	2.4
							107.1	108.0	0.9	10.1	0.9
							124.7	125.8	1.1	9.2	1.0
KDU4793	19782	49843	9689	30	222	300	15.2	15.8	0.6	0.8	0.5
KDU4794	19776	49846	9684	-31	263	348	251.3	252.0	0.7	23.2	0.2
KDU4804	19849	49812	9686	30	204	233.8	14.00	17.45	3.45	2.5	3.4
							25.00	28.00	3.00	3.0	2.8
							33.00	**39.00**	**6.00**	**4.4**	**5.6**
							54.00	55.85	1.85	3.5	1.7
KDU4805	19820	49826	9687	12	199	239	**15.6**	**20.0**	**4.4**	**8.9**	**4.0**
							60.0	61.4	1.4	5.2	1.4
KDU4806	19785	49842	9689	30	204	161	15.0	17.0	2.0	2.3	2.0
							46.0	**49.0**	**3.0**	**4.5**	**3.0**
KDU4807	19780	49844	9685	9	200	166	65.9	66.3	0.4	28.7	0.3
KDU4703	19818	49833	9617	29	213	114	44.7	46.3	1.6	3.6	1.4
							58.5	**60.8**	**2.3**	**10.7**	**2.2**
KDU4704	**19818**	**49833**	**9616**	**17**	**194**	**150**	**57.0**	**62.0**	**5.0**	**14.0**	**4.5**
							96.0	**99.4**	**3.4**	**5.5**	**3.3**
							132.7	134.0	1.3	3.9	1.2
KDU4705	19907	49780	9652	17	187	141	58.0	59.4	1.4	2.8	1.3
							64.7	66.1	1.4	3.5	1.3
							87.8	**92.0**	**4.2**	**2.7**	**3.9**
							107.5	107.8	0.3	6.8	0.1
KDU4706	**19907**	**49780**	**9652**	**6**	**187**	**147**	**56.4**	**79.0**	**22.6**	**2.8**	**20.7**
							88.0	**92.0**	**4.0**	**20.8**	**3.7**
							96.0	99.0	3.0	2.4	2.7
							111.0	115.0	4.0	1.9	3.7
KDU4707	19891	49784	9652	11	198	147	43.1	45.8	2.8	3.4	2.5
							75.5	**84.3**	**8.8**	**4.0**	**7.9**
							97.5	98.6	1.1	2.3	1.0
							112.6	**113.7**	**1.1**	**19.9**	**1.0**
KDU4708	**19856**	**49792**	**9652**	**-3**	**185**	**123**	**60.7**	**76.0**	**15.4**	**6.5**	**12.8**
KDU4709	19846	49796	9653	19	230	141	57.6	60.0	2.4	2.2	1.6
							65.2	**69.3**	**4.2**	**4.8**	**2.8**
D BLOCK											
KDU4620	20462	49672	9511	-26	198	159	66.9	71.9	5.0	1.6	0.0
KDU4621	20462	49672	9511	-18	185	110	46.6	48.5	1.9	2.2	1.8
							70.3	70.9	0.6	10.6	0.6
KDU4671	20452	49672	9511	-30	176	105	77.0	83.0	6.0	2.2	2.3
KDU4672	20452	49672	9511	-38	168	116	90.0	91.6	1.6	2.3	0.5
KDU4673	20462	49672	9511	-24	165	156	54.6	62.0	7.4	3.8	2.0
							83.4	88.0	4.6	6.0	1.2
KDU4674	20462	49672	9512	-16	138	174	61.4	66.0	4.6	4.0	1.3
							84.0	**93.0**	**9.0**	**2.9**	**3.7**
							141.0	143.0	2.0	4.0	0.8
KDU4702	20451	49672	9511	-21	222	115	**87.0**	**90.9**	**3.9**	**7.3**	**1.9**
KDU4619	**20462**	**49672**	**9511**	**-40**	**195**	**227**	**116.5**	**123.8**	**7.4**	**7.1**	**2.4**
KDU4619	20462	49672	9511	-40	195	227	185.8	186.7	0.9	3.9	0.3
KDU4623	20464	49672	9511	-30	154	186	72.7	73.9	1.2	14.9	0.5
							76.8	**87.7**	**10.9**	**671.0**	**4.4**
							87.7	**97.9**	**10.2**	**2.8**	**4.1**

KANOWNA SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
								Including	**0.5**	**12860.0**	**0.2**
KDU4675	20378	49706	9589	19	177	75	32.4	35.1	2.7	2.0	2.1
							50.0	53.3	3.3	2.5	2.6
KDU4676	20378	49706	9589	9	189	80	70.3	70.7	0.5	12.2	0.4
KDU4677	**20354**	**49708**	**9588**	**27**	**179**	**80**	**4.0**	**11.0**	**7.0**	**5.3**	**5.8**
							36.0	40.0	4.0	2.5	3.9
KDU4678	20354	49708	9588	15	189	83	35.1	36.0	1.0	4.3	0.8
							47.0	55.0	8.0	2.4	6.9
KDU4679	20318	49709	9587	15	171	82	34.6	37.0	2.4	3.0	1.7
							47.0	**58.0**	**11.0**	**3.7**	**7.6**
KDU4680	20318	49709	9587	-3	169	90	**47.6**	**52.0**	**4.4**	**6.6**	**3.4**
KDU4681	20318	49709	9586	-13	173	97	57.0	58.5	1.5	2.5	1.2
KDU4682	20318	49709	9587	-7	184	91	51.7	54.4	2.6	1.6	2.2
KDU4683	20307	49710	9588	32	180	87	47.0	50.6	3.6	1.3	3.3
KDU4684	20307	49710	9588	14	178	84	66.0	69.0	3.0	2.1	2.9
KDU4685	20307	49710	9588	24	184	87	**63.0**	**68.3**	**5.3**	**2.5**	**4.9**
KDU4686	20292	49711	9587	14	179	85	45.4	47.4	2.1	2.7	2.0
							60.0	64.2	4.2	1.7	4.0
KDU4687	**20292**	**49711**	**9588**	**24**	**191**	**95**	**60.1**	**61.4**	**1.4**	**9.1**	**1.3**
KDU4688	20262	49711	9588	22	184	94	**78.0**	**87.0**	**9.0**	**2.3**	**7.7**
KDU4689	20254	49711	9587	17	201	60	**34.8**	**38.0**	**3.2**	**5.1**	**3.0**
KDU4699	20318	49709	9587	5	178	85	47.0	52.0	5.0	2.2	4.4
KDU4700	20319	49709	9587	-26	181	83	62.0	62.6	0.6	0.0	0.0
KDU4701	20318	49709	9587	-24	161	84	45.0	49.0	4.0	3.0	1.9
					E BLOCK						
KDU4529	20474	49289	9242	24	37	363	17.6	20.0	2.4	7.9	0.0
							317.2	320.8	3.6	2.6	0.0
KDU4562	20000	49616	9097	3	220	148	**24.3**	**25.0**	**0.7**	**18.7**	**0.5**
							76.0	76.7	0.8	12.1	0.7
							96.8	97.2	0.4	11.8	0.2
KDU4588	20008	49554	9130	-23	201	95	78.0	80.0	2.0	6.7	1.3
							83.0	85.0	2.0	2.2	1.3
KDU4589	20008	49554	9130	-4	214	66	43.0	45.0	2.0	4.0	1.8
KDU4591	20008	49554	9130	2	246	183	61.9	64.0	2.1	3.8	1.8
							67.0	69.0	2.0	2.3	1.7
							82.3	**91.0**	**8.8**	**3.2**	**7.3**
KDU4592	19990	49558	9127	-13	207	63	40.1	43.3	3.2	2.1	2.5
KDU4593	19990	49558	9127	-4	221	64	**51.3**	**60.2**	**8.9**	**2.7**	**8.0**
KDU4599	20523	49561	9260	9	142	156	94.0	94.5	0.5	16.8	0.3
KDU4600	20523	49561	9260	20	155	150	101.0	104.0	3.0	2.8	2.7
KDU4601	20523	49561	9260	10	168	140	**84.5**	**97.4**	**12.9**	**2.3**	**11.7**
KDU4602	20523	49561	9260	-11	167	159	**78.9**	**93.0**	**14.2**	**2.8**	**10.3**
KDU4603	20523	49561	9260	-19	169	198	104.3	108.7	4.4	2.6	2.6
							115.0	**120.0**	**5.0**	**4.4**	**3.0**
KDU4604	20523	49561	9260	11	182	144	71.6	73.3	1.7	2.1	1.4
							136.0	138.0	2.0	2.1	1.7
KDU4605	20523	49561	9260	6	189	147	**83.0**	**89.0**	**6.0**	**2.9**	**4.9**
KDU4606	20523	49561	9260	-5	187	180	**18.4**	**22.2**	**3.9**	**4.1**	**3.2**
							83.5	**90.0**	**6.5**	**2.1**	**5.4**
							93.2	95.0	1.8	2.7	1.5
KDU4607	20523	49561	9260	-15	187	144	**104.0**	**110.0**	**6.0**	**3.1**	**3.8**
KDU4608	20523	49561	9260	29	186	189	**68.2**	**75.0**	**6.8**	**2.7**	**6.7**
							121.0	123.0	2.0	2.2	2.0
KDU4609	20523	49561	9260	28	207	167	**119.1**	**123.3**	**4.2**	**3.7**	**3.4**
KDU4610	**20523**	**49561**	**9260**	**34**	**160**	**152**	**69.0**	**73.3**	**4.3**	**9.9**	**4.2**
KDU4611	20474	49289	9240	-16	15	183	26.4	27.3	0.9	7.2	0.0
							162.8	167.1	4.3	2.2	3.7
							175.8	**177.5**	**1.8**	**8.2**	**1.5**
KDU4612	20474	49289	9240	-14	25	201	56.2	59.0	2.8	4.7	0.0
							167.5	170.4	2.9	2.1	2.2
							172.0	**178.0**	**6.0**	**3.1**	**4.6**
KDU4614	20474	49289	9240	-31	14	222	87.8	89.0	1.3	3.9	0.0
							134.0	136.0	2.0	2.5	0.0
							150.0	**154.5**	**4.5**	**3.4**	**4.2**
							162.0	**167.5**	**5.5**	**2.3**	**5.1**
KDU4615	20474	49289	9240	-26	27	222	16.0	17.0	1.0	10.1	0.0
							109.1	112.6	3.5	2.1	0.0
							150.0	151.4	1.4	4.4	0.0
							192.0	**198.0**	**6.0**	**3.0**	**4.9**
KDU4616	20474	49289	9240	-19	28	237	86.1	89.0	2.9	12.6	0.0
							167.9	**171.0**	**3.2**	**3.9**	**3.0**
							175.6	179.0	3.4	2.9	3.2
KDU4617	20474	49289	9240	-14	32	246	15.0	15.3	0.3	22.1	Unknown
							44.0	45.0	1.0	6.2	Unknown
							73.0	74.4	1.4	2.5	Unknown
							88.0	89.6	1.6	3.1	Unknown
							188.6	189.7	1.2	2.6	1.0
							220.0	221.7	1.7	2.1	1.5
KDU4710A	20527	49561	9258	-36	138	441	**261.0**	**292.0**	**31.0**	**2.3**	**6.9**
							416.7	**437.0**	**20.3**	**3.0**	**10.0**
KDU4594	20523	49561	9260	-21	148	219	122.1	126.5	4.5	5.1	2.5
							210.0	212.0	2.0	3.0	Unknown
KDU4597	20523	49561	9260	-8	147	186	141.0	159.0	18.0	0.0	Unknown
KDU4598	20523	49561	9260	0	149	159	59.5	60.9	1.4	2.2	Unknown
KDU4624	19891	49784	9651	-1	203	454	66.5	68.4	1.9	4.5	1.5
							76.0	**78.2**	**2.2**	**15.6**	**1.8**
KDU4563	**20000**	**49616**	**9097**	**8**	**220**	**188**	**23.0**	**25.0**	**2.0**	**12.9**	**1.7**
							91.7	**93.0**	**1.3**	**12.1**	**1.2**
							96.4	**99.0**	**2.6**	**5.3**	**2.3**
KDU4563	20000	49616	9097	8	220	188	110.0	113.3	3.3	2.4	2.9
							145.0	148.0	3.0	3.4	2.4
KDU4571	19887	49608	9115	38	272	280	178.6	180.7	2.1	3.6	1.1
							244.7	249.7	4.9	3.0	2.5
KDU4572	19887	49609	9115	27	283	341	211.0	212.0	1.0	2.9	0.3
							235.6	237.1	1.5	5.1	0.5
							241.7	245.0	3.2	2.9	1.1

KANOWNA SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
							250.7	253.0	2.3	2.4	0.7
							258.0	263.8	5.8	4.9	1.9
							266.0	268.0	2.0	6.1	0.7
KDU4573	**19887**	**49608**	**9113**	**3**	**271**	**375**	**276.0**	**290.2**	**14.2**	**22.4**	**10.7**
							338.3	**343.4**	**5.1**	**4.2**	Unknown
KDU4574	**19890**	**49771**	**9413**	**-33**	**217**	**273**	**268.0**	**271.5**	**3.5**	**3.3**	Unknown
KDU4587	20008	49554	9130	-13	199	81	67.8	68.4	0.6	3.5	0.3
KDU4590	20008	49554	9130	-21	211	78	69.0	70.1	1.1	8.3	0.8
PORHYRY XENOLITHS											
KDU4632	20477	49286	9242	-12	50	377	115.7	118.7	3.0	2.7	Unknown
							191.7	**196.2**	**4.4**	**5.0**	Unknown
							228.2	230.0	1.8	2.6	Unknown
KDU4633	20477	49286	9242	-7	59	309	**209.0**	**218.0**	**9.0**	**2.2**	**6.9**
							273.8	**279.0**	**5.3**	**5.8**	**4.0**
							282.0	**289.0**	**7.0**	**3.5**	**5.3**
KDU4634	**20477**	**49286**	**9242**	**3**	**66**	**570**	**233.5**	**255.5**	**22.1**	**4.4**	**12.9**
							288.0	**315.0**	**27.0**	**4.2**	**14.7**
							512.1	513.0	0.9	14.1	0.0
KDU4635	20477	49287	9242	-6	66	411	236.0	239.0	3.0	3.6	1.8
							247.0	**259.0**	**12.0**	**5.8**	**7.0**
							267.8	271.0	3.2	2.4	1.8
							291.3	**302.0**	**10.8**	**2.7**	**6.0**
							313.0	319.0	6.0	2.3	3.3
KDU4636	20477	49286	9242	-11	71	433	261.8	263.0	1.2	12.9	0.7
							333.8	**345.0**	**11.2**	**14.1**	**6.4**
KDU4730	20477	49286	9242	7	68	422	277.1	279.8	2.7	3.1	1.3
KDU4731	20477	49286	9242	-2	73	426	243.5	246.3	2.8	1.3	0.5
KDU4732	20477	49286	9242	-10	77	495	67.8	68.5	0.7	34.6	0.2
KDU4734	20477	49286	9240	-18	73	471	79.0	79.3	0.3	10.4	0.0
							231.0	**250.0**	**19.0**	**3.1**	**10.2**
							300.9	304.0	3.1	2.7	3.0
							310.0	311.5	1.5	12.7	0.7
							317.0	**317.6**	**0.6**	**43.7**	**0.3**
							351.0	**369.4**	**18.4**	**3.5**	**9.0**
SIMS											
KDU4493	20159	49804	9861	21	221	144	3.9	5.2	1.3	NSI	0.0
KDU4496	20183	49803	9861	8	191	238	0.0	3.0	3.0	1.4	2.8
							6.3	9.2	2.9	1.7	2.3
							54.4	60.1	5.6	2.3	4.4
							64.0	66.3	2.3	2.8	1.7
							206.0	**207.2**	**1.2**	**82.4**	**1.0**
							221.0	**222.4**	**1.4**	**28.6**	**1.1**
KDU4577	20145	49742	9809	1	209	267	**96.0**	**99.0**	**3.0**	**5.4**	**1.9**
							217.0	**219.0**	**2.0**	**53.2**	**1.4**
KDU4871	20141	49745	9808	1	224	333.3	**127.00**	**130.70**	**3.70**	**4.4**	**3.3**
							220.60	**224.50**	**3.90**	**115.1**	**3.6**
KDU4872	20141	49745	9808	-11	223	294.3	103.30	104.40	1.10	8.5	0.9
							112.00	**115.76**	**3.76**	**7.1**	**3.2**
							173.05	**175.47**	**2.42**	**7.6**	**2.1**
							226.48	226.78	0.30	24.3	0.3
							244.20	246.66	2.46	2.5	2.2
KDU4873	20141	49745	9808	-3	220	300.8	106.65	109.55	2.90	2.9	2.5
							134.90	139.00	4.10	2.5	3.7
							160.00	**161.00**	**1.00**	**35.6**	**0.9**
							184.82	**187.48**	**2.66**	**10.3**	**2.4**
							206.00	**210.65**	**4.65**	**2.5**	**4.2**
							237.40	**239.00**	**1.60**	**13.2**	**1.5**
KDU4875	20141	49745	9808	10	213	342.4	**85.28**	**91.00**	**5.72**	**2.7**	**4.7**
							97.81	101.00	3.19	2.7	2.7
							118.50	**121.05**	**2.55**	**6.8**	**2.2**
							127.90	**132.30**	**4.40**	**3.3**	**3.7**
							200.00	202.75	2.75	2.5	2.4
KDU4578	20146	49742	9810	-10	210	210	**35.0**	**36.0**	**1.0**	**18.5**	**0.6**
							48.5	**55.4**	**6.9**	**3.7**	**3.6**
							145.2	149.0	3.8	2.7	2.1
KDU4581	20146	49742	9810	11	224	208	85.0	86.3	1.3	15.4	0.4
VELVET											
KDU4628	**19285**	**50011**	**9633**	**-22**	**214**	**140**	**59.0**	**69.0**	**10.0**	**3.8**	**9.6**
							79.2	**91.0**	**11.8**	**2.0**	**11.3**
							100.0	102.0	2.0	3.9	1.9
KDU4631	19285	50014	9635	32	249	118	27.0	29.0	2.0	2.1	1.6
KDU4759	19265	49988	9440	0	220	10.0	1.40	1.97	0.57	0.0	0.0
KDU4760	19262	49997	9441	0	41	9.7	0.30	1.00	0.70	0.0	0.0
							3.00	5.00	2.00	0.0	0.0
KDU4761	19244	50005	9440	0	220	9.9	**0.00**	**1.42**	**1.42**	**10.7**	**1.3**
KDU4762	19232	50015	9440	0	217	9.0	0.00	1.00	1.00	8.3	0.9
KDU4763	19212	50039	9440	0	38	12.0	3.53	5.55	2.02	2.8	1.8
KDU4764	19186	50064	9440	0	41	10.0	**0.00**	**6.30**	**6.30**	**3.6**	**5.5**
KDU4765	19174	50074	9440	0	40	9.1	0.00	1.26	1.26	2.3	1.1
KDU4766	19160	50080	9440	-5	257	51.1	24.20	27.22	3.02	3.3	2.6
KDU4819	19257	50010	9478	-4	47	17	0.0	1.0	1.0	0.0	0.0
KDU4820	19250	50017	9478	0	42	15	4.0	5.0	1.0	0.0	0.0
KDU4821	19230	50032	9479	3	236	108	26.0	30.0	4.0	2.5	3.6
							34.0	37.6	3.6	2.4	3.3
KDU4821A	19251	50008	9479	2	237	96	34.0	37.8	3.8	2.2	3.4
KDU4849	19179	50063	9441	17	255	56.1	0.00	1.69	1.69	5.1	1.4
							6.00	**16.00**	**10.00**	**6.6**	**9.7**
							30.00	33.41	3.41	2.5	3.3
KDU4850	19189	50053	9440	-19	256	86.6	7.00	9.00	2.00	2.5	1.0
							15.00	**27.70**	**12.70**	**2.6**	**11.5**
KDU4851	19252	49998	9440	-21	254	102.0	0.00	4.10	4.10	4.0	2.0
							40.41	40.71	0.30	17.7	0.3
KDU4852	19262	49990	9443	42	248	100.0	**31.50**	**38.00**	**6.50**	**3.0**	**5.2**
							50.00	52.35	2.35	3.8	1.9
KDU4853	19110	50133	9403	-18	236	110.7	**22.77**	**28.49**	**5.72**	**4.6**	**4.0**

KANOWNA SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU4854	19110	50135	9403	-15	286	74.8	**47.00**	**51.00**	**4.00**	**13.0**	**0.8**
KDU4855	19327	50123	9570	34	217	98.0	**75.44**	**78.90**	**3.46**	**3.6**	**3.5**
							80.45	84.10	3.65	2.6	3.6
							90.00	**91.74**	**1.74**	**6.4**	**1.7**
KDU4856	19327	50123	9570	31	210	71.5	63.40	65.00	1.60	1.5	0.0
KDU4643	19226	50096	9629	-33	187	37.1	7.00	7.45	0.45	1.7	0.0
KDU4644	19226	50096	9629	-25	174	35.0	20.00	23.00	3.00	8.3	1.2
							25.61	**30.36**	**4.75**	**8.0**	**1.9**
KDU4645	**19224**	**50097**	**9633**	**55**	**234**	**23**	**5.0**	**11.6**	**6.6**	**4.3**	**5.6**
							13.5	19.0	5.5	2.5	3.5
KDU4646	**19226**	**50096**	**9633**	**53**	**182**	**29**	**15.0**	**20.9**	**5.9**	**7.9**	**5.0**
KDU4647	19225	50097	9631	24	166	33	29.6	32.0	2.4	3.4	1.4
KDU4767	19850	49771	9408	-31	185	281.4	248.25	255.20	6.95	1.6	2.2
KDU4768	19847	49773	9409	4	236	285.0	195.00	198.00	3.00	0.6	0.0
							248.00	249.38	1.38	1.3	0.0
KDU4769	19847	49773	9408	-27	238	407.5	190.17	190.54	0.37	11.2	0.2
							260.22	264.00	3.78	1.3	3.4
KDU4770A	19847	49773	9408	-29	249	521.6	262.00	264.12	2.12	2.2	0.8
KDU4774	19887	49607	9113	-9	231	234.2	133.00	134.00	1.00	0.8	0.0
KDU4775	19887	49607	9113	-9	251	297.3	192.71	194.14	1.43	0.9	0.0
KDU4776	19887	49607	9112	-26	241	371.9	281.00	283.34	2.34	1.2	0.0
KDU4777	19887	49607	9112	-23	252	413.7	**349.00**	**352.00**	**3.00**	**23.7**	**2.1**
							378.00	**387.20**	**9.20**	**12.4**	**6.5**
KDU4778	19887	49609	9113	5	272	438.2	**274.80**	**284.70**	**9.90**	**13.7**	**7.4**
							337.12	**340.70**	**3.58**	**4.4**	**2.8**
KDU4629	19285	50011	9633	-25	198	189	100.0	102.0	2.0	4.0	1.6
							105.0	106.6	1.6	2.8	1.3
							151.0	**156.8**	**5.8**	**3.1**	**4.8**
KDU4630	19285	50011	9636	33	218	126	76.3	79.0	2.6	2.4	2.3
KDU4658	19285	50014	9634	-1	265	279	33.0	35.0	2.0	2.2	1.4
KDU4659A	19285	50011	9633	-3	231	426	40.0	40.7	0.7	24.1	0.6
KDU4660	**19286**	**50010**	**9634**	**1**	**210**	**172**	**59.6**	**62.6**	**3.0**	**9.3**	**3.0**
							67.0	**70.8**	**3.8**	**8.4**	**3.5**
KDU4662	19351	50077	9463	-8	219	199	119.4	120.1	0.7	4.8	0.6
KDU4663	19351	50077	9463	6	208	227	**110.3**	**111.4**	**1.1**	**12.7**	**0.8**
							116.4	116.7	0.3	29.5	0.2
KDU4664	19352	50077	9463	14	220	213	170.0	172.4	2.4	0.9	2.4
KDU4665	19352	50076	9464	20	227	267	**190.4**	**194.0**	**3.7**	**3.3**	**3.6**
KDU4666	19352	50076	9464	27	222	227	**215.9**	**219.0**	**3.1**	**3.9**	**3.1**
KDU4746	19252	50007	9478	0	255	171	38.1	40.0	2.0	2.4	1.8
							46.9	47.2	0.3	36.1	0.2
KDU4747	19232	50038	9478	-12	50	15	**0.0**	**2.0**	**2.0**	**7.6**	**1.9**
KDU4748	19216	50049	9478	-8	228	31	21.5	22.6	1.1	2.5	0.9
KDU4749	19206	50062	9478	-8	230	21	3.4	4.3	0.9	1.4	0.8
KDU4750	19210	50065	9478	-9	29	16	**0.0**	**5.3**	**5.3**	**3.8**	**5.0**
KDU4751	19230	50032	9479	-5	255	107	25.0	28.0	3.0	2.6	2.6
KDU4752	19229	50033	9479	33	242	84	28.0	31.0	3.0	3.4	2.8
KDU4753	19206	50062	9478	-21	264	43	31.9	34.0	2.1	1.9	1.0
KDU4754	19196	50073	9477	-2	256	72	**14.4**	**25.0**	**10.6**	**3.9**	**7.7**
KDU4755	19194	50074	9479	28	252	70	**20.0**	**25.0**	**5.0**	**4.6**	**3.0**
KDU4756	19162	50094	9477	10	226	100	**0.0**	**0.8**	**0.8**	**30.4**	**0.7**
KDU4757	19162	50094	9476	-24	228	95	37.0	40.0	3.0	1.8	1.8
KDU4758	19240	50021	9481	42	254	66	**38.0**	**42.4**	**4.4**	**3.9**	**4.2**
KDU4781	19352	50076	9461	-39	228	411	**230.2**	**243.0**	**12.8**	**3.0**	**5.2**
							259.9	263.0	3.1	2.6	1.3
							381.0	**390.5**	**9.5**	**2.5**	**4.1**
KDU4782	19352	50075	9461	-43	194	255	251.4	252.1	0.7	0.0	0.0
KDU4783	19354	50073	9462	-44	185	390.2	374.00	376.00	2.00	4.9	0.4
KDU4828	19111	50132	9406	27	171	51	34.0	37.0	3.0	2.9	1.1
KDU4829	19110	50133	9405	24	258	44.0	16.00	20.00	4.00	0.0	0.0
KDU4830	19110	50132	9403	-15	217	86.4	21.45	25.00	3.55	3.2	2.7
							78.60	81.00	2.40	3.8	1.8
KDU4831	19111	50132	9402	-41	210	156.0	39.97	41.70	1.73	2.1	1.6
							120.00	**124.50**	**4.50**	**6.6**	**1.9**
KDU4832	19109	50133	9403	-13	260	52.1	24.68	31.00	6.32	2.2	3.7
KDU4833	19109	50133	9403	-23	274	68.5	**38.63**	**43.00**	**4.37**	**10.3**	**1.4**
							55.00	58.00	3.00	2.8	1.0
KDU4834	19110	50133	9403	-38	255	170.9	109.00	111.00	2.00	2.0	1.5
KDU4858	19262	49990	9442	25	215	128.9	34.00	39.00	5.00	2.0	3.9
							72.54	82.00	9.46	2.0	7.6
							87.00	89.00	2.00	3.5	1.6
KDU4627	19286	50011	9633	-43	209	195	94.0	95.0	1.0	2.0	0.4
							116.4	120.1	3.7	1.9	1.7
KDU4637	19269	50050	9632	0	219	20	0.0	1.3	1.3	2.4	1.2
KDU4638	19257	50061	9632	0	207	25	0.6	2.2	1.6	4.8	1.4
KDU4640	**19245**	**50068**	**9631**	**-21**	**200**	**16**	**1.2**	**7.8**	**6.7**	**2.9**	**4.9**
KDU4641	19236	50074	9632	10	206	20	0.0	6.3	6.3	2.0	3.8
KDU4860	19353	50073	9464	23	209	152.3	87.51	87.90	0.39	0.4	0.0
KDU4861	19353	50073	9462	-8	209	197.7	**118.00**	**125.24**	**7.24**	**8.3**	**5.6**
							181.02	182.77	1.75	1.8	1.4
KDU4862	19354	50073	9462	-17	200	194.9	133.00	138.00	5.00	0.7	0.7
KDU4863	19353	50073	9463	7	198	171.1	159.90	161.60	1.70	2.0	1.2
KDU4864	19354	50073	9462	-8	191	291.4	127.17	128.16	0.99	1.0	1.0
							127.17	128.16	0.99	1.0	1.0
KDU4446	**19843**	**49567**	**9072**	**17**	**278**	**366**	**172.2**	**175.7**	**3.5**	**11.9**	**3.5**
							253.4	**258.8**	**5.4**	**5.0**	**5.0**
							263.7	265.1	1.4	3.1	1.2
KDU4575	19890	49771	9413	7	267	193			NSI		
KDU4576	19890	49770	9416	21	260	276			NSI		
KDU4533	19895	49804	9684	16	188	84	33.4	48.0	14.6	2.9	2.2
							52.0	54.0	2.0	2.4	1.9
							57.0	58.5	1.4	2.8	1.4
							62.3	63.4	1.1	3.2	1.1
KDU4639	19251	50065	9634	37	213	17	**8.5**	**9.5**	**1.0**	**25.0**	**0.8**
KDU4876	19105	50226	9497	-10	260	180.1	**46.40**	**93.00**	**46.60**	**0.9**	**26.2**
KDU4877	19105	50226	9497	0	255	120.0	**39.00**	**91.00**	**52.00**	**0.7**	**36.4**

Table 2 - Moonbeam Significant Intersections

MOONBEAM SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
MBCD18015	9395	19098	6344	-71	60	470	460.1	461.8	1.7	4.3	1.3
MBCD18016	9397	19099	6344	-64	60	404	388.6	389.9	1.4	2.7	1.1
MBCD18016						404	389.9	390.7	0.8	18.8	0.6
MBCD18017	9396	19054	6344	-74	61	630	605.4	606.9	1.5	8.9	1.2
MBCD18018	9396	19054	6344	-67	66	514			NSI		
MBDD18019	9527	18943	6345	-77	51	395	372.3	373.2	0.8	10.8	0.7
MBDD18020	9538	18921	6345	-84	24	526	517.5	518.6	1.1	3.7	0.9
MBDD18021	9439	18696	6345	-63	15	599	559.6	560.6	1.0	2.8	0.8
MBDD18021							564.4	565.3	0.9	11.9	0.8
MBDD18022	9562	18729	6345	-73	7	481			NSI		
MBDD18025	9355	19286	6344	-65	83	483	455.4	458.7	3.3	16.7	2.7
MBDD18030	9466	19067	344	-67	55	501	348.4	349.0	0.6	9.8	0.5

Table 3 – EKJV Significant Intersections

EKJV SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
					PODE						
PEGGC18294	9792	17152	6206	-18.0	83	17.5	0.0	1.6	1.6	3.9	1.4
PEGGC18301	9792	17212	6208	22.4	291	26.9	**0.0**	**1.0**	**1.0**	**23.8**	**0.9**
PEGGC18302	9787	17229	6207	22.4	291	30.0	**1.5**	**3.4**	**1.9**	**7.8**	**1.4**
							4.3	4.6	0.3	2.0	0.2
							11.0	11.5	0.5	3.6	0.3
PEGGC18304	9785	17251	6208	-21.0	67	26.8	**0.0**	**1.0**	**1.0**	**37.5**	**0.8**
PEGGC18305	9793	17260	6206	-51.0	81	24.2	5.1	5.9	0.8	4.5	0.8
PEGGC18306	9788	17267	6209	32.6	287	24.1	0.0	1.0	1.0	2.9	0.9
							3.9	4.2	0.4	3.4	0.3
PEGGC18307	9792	17272	6208	-45.0	74	26.9	1.0	1.7	0.7	2.4	0.6
							3.6	3.9	0.3	4.3	0.2
							6.7	7.0	0.3	5.3	0.2
							8.7	**10.3**	**1.7**	**7.0**	**1.6**
							15.0	15.4	0.3	2.9	0.3
PEGGC18308	9788	17278	6207	-8.0	277	24.1	0.0	0.4	0.4	16.9	0.2
							2.9	3.6	0.7	4.4	0.4
							6.0	7.0	1.0	3.0	0.6
							15.6	16.7	1.1	10.9	0.6
PEGGC18309	9791	17286	6207	-20.6	67	30.1			NSI		
PEGGC18310	9783	17304	6209	-20.6	67	24.1	0.4	1.0	0.6	4.2	0.5
							2.0	2.3	0.3	4.2	0.2
							9.8	**11.1**	**1.3**	**21.2**	**1.0**
PEGGC18311	9786	17315	6208	-51.0	60	33.2			NSI		
PEGGC18313	9775	17151	6191	2.0	312	15.2	1.2	3.0	1.9	2.8	1.9
PEGGC18314	9781	17160	6191	-6.0	85	18.3	0.0	2.3	2.3	3.4	2.3
PEGGC18316	9783	17192	6193	13.0	267	17.9	0.5	2.4	1.9	2.2	1.9
PEGGC18318	9776	17203	6192	-2.0	264	18.3	0.0	0.5	0.5	5.4	0.3
							2.8	4.3	1.4	9.8	1.0
							6.4	6.7	0.3	7.8	0.2
							8.0	9.0	1.0	10.5	0.7
PEGGC18319	9771	17212	6192	3.0	286	21.2	0.0	1.0	1.0	2.2	0.7
							2.6	5.3	2.7	34.6	1.9
PEGGC18320	9770	17222	6192	3.0	300	21.2	4.6	4.9	0.3	2.2	0.3
PEGGC18320	9770	17222	6192	3.0	300	21.2	8.0	8.5	0.5	6.6	0.5
PEGGC18321	9775	17224	6191	-29.0	72	18.1	0.0	0.3	0.3	15.2	0.3
PEGGC18323	9777	17238	6191	-43.0	60	21.2	6.0	8.4	2.4	6.5	2.4
							10.4	10.7	0.3	14.5	0.3
PEGGC18325	9770	17256	6191	-52.0	55	20.9	0.0	2.6	2.6	13.1	2.6
PEGGC18328	9772	17276	6194	15.0	287	20.9	0.9	1.3	0.4	2.6	0.4
							4.8	5.1	0.3	4.3	0.3
							6.3	6.7	0.4	2.4	0.4
							8.7	10.2	1.5	5.8	1.5
PEGGC18329	9774	17293	6192	-35.0	63	23.5	0.8	1.5	0.7	2.1	0.7
							1.8	2.1	0.3	3.2	0.3
PEGGC18331	9770	17314	6194	17.0	320	21.0	0.3	0.7	0.4	2.7	0.3
							6.9	9.6	2.7	7.8	1.7
PEGGC18332	9774	17312	6193	-38.0	108	21.1	0.8	1.1	0.3	3.3	0.3
							5.1	5.6	0.4	6.2	0.4
PEGGC18345	9784	17335	6211	31.3	307	17.7	**1.2**	**2.3**	**1.1**	**15.3**	**0.9**
PEGGC18350	9792	17361	6208	-32.0	59	16.2	12.2	12.5	0.3	6.6	0.2
PEGGC18365	9784	17343	6194	-9.0	78	18.4	0.0	0.9	0.9	4.0	0.9
							8.0	**12.4**	**4.4**	**3.7**	**4.4**
PEGGC18367	9785	17362	6194	-38.0	98	15.2	1.0	3.0	2.0	2.3	2.0
PEGGC18369	9785	17376	6195	-28.0	77	12.1	2.8	3.1	0.3	3.8	0.3
							4.0	4.6	0.6	2.2	0.6
PEGGC18370	9781	17388	6196	21.0	311	11.5	0.8	1.2	0.4	8.5	0.4
PEGGC18373	9790	17405	6194	-45.0	97	15.0	5.5	6.0	0.5	2.9	0.5
PEGGC18375	9793	17415	6196	-11.0	71	17.7	0.3	1.0	0.7	6.9	0.6
						17.7	**5.3**	**7.5**	**2.2**	**8.4**	**1.7**
PEGRSD18096	9626	16971	5819	-12.0	278	267.3	149.8	150.4	0.6	4.6	0.4
							155.9	156.4	0.5	2.5	0.4
							242.0	243.0	1.0	5.0	0.9
PEGRSD18351	9801	17338	5938	20.0	287	282.0	1.0	1.5	0.5	6.5	0.4
							9.0	10.0	1.0	4.9	0.9
							20.8	21.1	0.3	41.5	0.2
							21.7	22.7	1.0	4.3	0.7
							257.9	**261.6**	**3.7**	**3.7**	**3.2**
							264.5	265.5	1.0	7.5	0.9
PEGRSD18352	9802	17338	5939	31.0	295	293.6	6.0	7.0	1.0	7.4	0.9
							15.4	**15.8**	**0.4**	**101.0**	**0.4**
							128.3	**131.0**	**2.8**	**4.7**	**2.3**

EKJV SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut		Est True Thickness (m)
							147.0	148.0	1.0	2.4		0.9
							253.6	254.6	1.0	3.5		0.9
							255.7	256.0	0.4	7.9		0.3
							258.5	259.0	0.5	4.0		0.5
PEGRSD18353	9802	17338	5940	41.0	285	245.4	0.0	0.6	0.6	15.4		0.6
							4.0	**4.7**	**0.7**	**84.8**		**0.6**
							216.0	217.0	1.0	6.0		1.0
PEGRSD18354	9796	17364	5939	20.0	298	299.5	22.5	23.1	0.6	15.8		0.5
							24.9	**25.4**	**0.4**	**38.2**		**0.4**
							26.9	**27.2**	**0.3**	**35.8**		**0.3**
							243.9	245.0	1.2	4.0		1.0
PEGRSD18355	9797	17363	5940	44.0	305	378.5	0.0	0.5	0.5	10.2		0.4
							18.7	**19.3**	**0.6**	**29.0**		**0.4**
							144.8	145.4	0.6	2.4		0.4
							252.0	253.4	1.4	7.0		1.3
PEGRSD18360	9797	17395	5939	16.0	301	293.8	18.6	19.0	0.4	9.9		0.3
PEGRT18094	9626	16969	5819	-14.0	241	318.4	138.7	139.2	0.5	5.6		0.4
RALEIGH SOUTH												
RRCD18014	9019	17381	6344	-70	94	240.0		223.5	224.1	0.6	9.1	0.5
RRCD18016	9056	17391	6344	-66	99	204.0		171.9	172.2	0.3	6.1	0.2
RRDD18001	**8819**	**17281**	**6342**	**-75**	**88**	**282.3**		**247.6**	**249.1**	**1.5**	**22.6**	**1.2**
RRDD18002	**9030**	**17437**	**6344**	**-72**	**88**	**267.0**		**240.4**	**242.1**	**1.7**	**20.5**	**1.3**
RRDD18003	**9051**	**17461**	**6344**	**-71**	**107**	**233.0**		**208.0**	**208.9**	**0.9**	**56.5**	**0.8**
RRDD18004	**8819**	**17281**	**6342**	**-66**	**106**	**220.0**		**183.0**	**184.0**	**1.0**	**26.4**	**0.8**
RRDD18005	**8959**	**17496**	**6344**	**-61**	**84**	**321.0**		**290.3**	**291.0**	**0.6**	**19.8**	**0.5**
								292.3	293.0	0.8	1.2	0.6
								296.2	297.0	0.8	2.0	0.7
RRDD18006	**8959**	**17498**	**6344**	**-56**	**87**	**287.0**		**266.3**	**267.0**	**0.7**	**44.3**	**0.5**
								283.6	284.0	0.4	2.4	0.3
RRDD18007	9010	17585	6345	-56	93	261.4		234.9	235.2	0.3	1.4	0.2
								238.3	238.8	0.5	2.0	0.4
								239.4	239.7	0.3	5.2	0.2
RRDD18008	8813	17161	6344	-65	80	215		194.0	194.7	0.7	1.2	0.6
RRDD18009	9102	17642	6345	-72	87	214		186.0	186.3	0.3	5.5	0.2
RRDD18013	9102	17730	6345	-70	90	210		189.4	189.8	0.3	1.2	0.3
								193.2	194.0	0.8	2.5	0.7
RRDD18023	8976	17521	6344	-66	83	309.2		**299.1**	**300.5**	**1.4**	**38.8**	**1.1**
RRDD18024	8976	17519	6344	-63	87	291.2		280.4	281.0	0.6	13.1	0.5
RRDD18026	8965	17493	6344	-64	101	306.0		298.1	298.7	0.6	9.8	0.5
RRDD18028	8997	17453	6344	-71	104	285.2		264.7	265.7	0.9	4.7	0.8
RALRSD18068	8984	17701	6005	-68.0	74	167.5		**146.1**	**147.3**	**1.2**	**136.2**	**0.7**
RALRSD18078	8983	17698	6005	-70.0	153	185.5		22.0	23.0	1.0	2.6	0.1
RALRSD18162	8948	17529	5980	-61.0	112	161.9		123.4	123.7	0.3	2.5	0.2
RALRSD18183	8948	17529	5980	22.0	117	155.8		133.6	133.9	0.4	5.6	0.3
RALRSD18185	8998	17693	6008	22.0	139	195.7		**165.4**	**167.2**	**1.9**	**54.7**	**1.1**
RALRSD18187	8998	17693	6008	11.0	88	131.5		108.5	109.6	1.1	5.1	1.0
RALRSD18188	8998	17694	6007	-7.0	81	116.9		95.1	95.4	0.3	15.3	0.3
RALRSD18190	8948	17529	5980	-21.0	119	110.9		91.9	92.1	0.2	21.4	0.2
RALRSD18191	8948	17529	5980	-18.0	138	131.0		108.6	108.9	0.3	11.4	0.2
RALRSD18193	8948	17529	5980	-9.0	159	188.7		171.0	171.8	0.8	5.2	0.5
RALRSD18194	8996	17692	6006	-60.0	143	146.9		129.6	130.9	1.3	4.6	0.8
RALRSD18202	8931	17844	5719	35.0	151	231.3		212.2	212.5	0.3	2.2	0.1
RALRSD18204	8931	17845	5720	35.0	92	125.8		9.8	10.1	0.3	3.5	0.0
RALRSD18204	8931	17845	5720	35.0	92	125.8		112.0	112.5	0.5	3.5	0.1
RALRSD18211	8928	17843	5718	4.0	152	146.4		7.5	7.8	0.3	26.6	0.2
RALRSD18308	8980	17536	5988	34.0	107	151.3		135.4	135.7	0.3	9.0	0.1
RALRSD18314	8979	17534	5984	-39.0	176	226.2		192.0	193.0	1.0	7.3	0.4
RALRSD18316	8979	17534	5984	-52.0	179	213.0		186.0	187.0	1.0	0.3	0.1
RALRSD18316	8979	17534	5984	-52.0	179	213.0		186.0	187.0	1.0	0.3	0.1
RALRSD18318	8977	17534	5985	-64.0	179	198.0		185.1	185.8	0.7		
RALRSD18319	8979	17534	5984	-59.0	164	155.1		139.4	139.7	0.3	0.1	0.1
RALRSD18320	8977	17534	5985	-71.0	168	174.1		162.8	163.3	0.5	3.0	0.1
RALRT18070	8983	17696	6005	-66.0	134	170.8		151.3	151.7	0.3	11.2	0.2
RALRT18086	8983	17698	6005	-69.0	166	230.3		205.8	206.5	0.7	6.7	0.3
RALRT18301	8979	17534	5988	24.0	151	235.0		**189.4**	**190.9**	**1.6**	**20.4**	**0.7**
RALRT18302	8979	17534	5987	18.0	158	263.8		207.3	207.7	0.4	4.7	0.1
RALRT18303	8978	17534	5986	2.0	163	228.1		**174.0**	**176.0**	**2.0**	**13.6**	**0.8**
RALRT18304	8979	17534	5984	-19.0	172	227.7		186.6	187.0	0.5	2.2	0.2
RALRT18305	8979	17534	5984	-29.0	172	194.5		**165.9**	**166.8**	**0.9**	**22.6**	**0.7**
SADRSD18001	8892	17450	5981	2.0	133	192.1		177.4	177.7	0.3	20.2	0.1
SADRSD18002	8891	17450	5982	-8.0	135	191.0		165.8	167.0	1.3	2.5	0.4
SADRSD18003	8891	17450	5982	-1.0	139	218.9		183.0	184.3	1.4	8.6	0.4
SADRSD18004	8891	17450	5982	-4.0	147	236.9		204.2	205.2	1.0	9.9	0.2
								208.0	209.0	1.0	3.5	0.2
								211.4	212.0	0.6	2.3	0.1
SADRSD18006	8891	17450	5982	-6.9	152	260.8		232.0	232.7	0.7	0.4	0.1
SADRSD18007	8891	17450	5982	-1.0	154	269.7		262.5	263.1	0.6	2.1	0.3
SADRSD18008	8891	17450	5982	-9.7	156	284.4		251.8	252.1	0.3	16.7	0.0
								11.0	12.0	1.0	7.7	0.6
								102.6	**104.8**	**2.2**	**42.1**	**1.3**
								139.4	139.7	0.3	0.1	0.1
								178.8	179.1	0.3	4.1	0.2
								192.0	193.0	1.0	7.3	0.4
								194.0	194.6	0.6	3.2	0.2
								211.5	214.1	2.6	4.5	0.9
								222.8	223.4	0.6	35.9	0.2
SIR WALTER												
SWCD18001	8819	17281	6342	-60	88	447.7		385.6	385.9	0.3	1.6	0.2
SWCD18002	8823	17161	6344	-60	89	411.3				NSI		
SWCD18003	8755	17041	6343	-60	86	465.3				NSI		
SWCD18004W1	8811	17042	6342	-60	88	413.0		392.4	392.7	0.3	0.9	0.2
SWCD18005	**8936**	**17305**	**6342**	**-62**	**99**	**306.4**		**279.3**	**280.1**	**0.8**	**171.9**	**0.6**
SWCD18006A	8959	17118	6341	-65	65	291.4		259.7	260.1	0.4	1.2	0.3
SWCD18007	**8813**	**17280**	**6342**	**-66**	**87**	**459.8**		**434.6**	**435.9**	**1.4**	**89.9**	**1.1**
SWCD18008	8813	17161	6344	-66	89	448.4		409.9	410.2	0.3	1.6	0.2

EKJV SIGNIFICANT INTERSECTIONS												
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut		Est True Thickness (m)
SWCD18009	8748	17041	6343	-66	87	537.4		507.6	508.3	0.6	2.8	0.5
SWCD18010	**8930**	**17304**	**6342**	**-68**	**101**	**335.7**		**316.1**	**317.1**	**1.0**	**26.2**	**0.8**
SWCD18017	8900	16924	6341	-60	98	291.1				NSI		
SWCD18018	**8913**	**16853**	**6341**	**-60**	**97**	**276.1**		**248.0**	**253.3**	**5.3**	**21.5**	**4.2**

Table 4 – South Kalgoorlie Significant Intersections

HBJ SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (degrees, MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
HBJUG0483	20173	50300	28	-11	149	127.2	71.00	76.00	5.00	2.1	2.5
HBJUG0484	20173	50300	2023	-36	149	143.1	**98.00**	**105.64**	**7.64**	**1.6**	**6.3**
HBJUG0485	20173	50300	28	-48	144	164.0	151.00	154.00	3.00	3.7	0.9
HBJUG0486	20173	50300	28	-17	140	119.0	62.00	68.00	6.00	7.1	3.7
HBJUG0486	20173	50300	28	-17	140	119.0	110.66	119.03	8.37	3.1	5.2
HBJUG0497	20179	50446	2085	18	116	86.4	59.32	71.32	12.00	8.1	11.2
HBJUG0549	20123	5071	1780	-1	135	293.0	227.00	229.00	2.00	4.0	1.5
HBJUG0550	20123	50071	1780	-1	131	291.0	266.95	269.57	2.62	1.5	2.2
HBJUG0552	20123	50071	1780	-34	118	**251.0**	**185.43**	**189.00**	**3.57**	**4.5**	**2.3**
							194.00	**197.97**	**3.97**	**7.7**	**3.5**
HBJUG0553B	20123	50071	1780	-28	121	**206.6**	**179.25**	**182.37**	**3.12**	**9.7**	**2.7**
HBJUG0565B	20123	50071	1780	-40	115	**252.0**	**182.74**	**192.00**	**9.26**	**5.2**	**6.1**
HBJUG0566A	20123	50071	-220	-37	104	**216.8**	**192.09**	**198.09**	**6.00**	**4.6**	**4.2**
HBJUG0568	20123	50071	-220	-48	120	303.0	254.42	255.00	0.58	12.4	0.4
HBJUG0551	20123	50071	1780	-12	127	**272.6**	**217.00**	**221.60**	**4.60**	**2.8**	**3.7**
HBJUG0508	20137	50728	2023	37	112	**159.1**	**138.50**	**143.50**	**5.00**	**5.5**	**3.9**
HBJUG0510a	20137	50728	2023	33	104	**149.2**	**125.30**	**134.66**	**9.36**	**3.9**	**8.2**
HBJUG0511	20137	50728	2023	18	100	**158.6**	**97.20**	**108.76**	**11.56**	**6.1**	**10.5**
HBJUG0513	20137	50728	2023	18	89	131.7	100.64	103.81	3.17	2.6	3.1
HBJUG0514	20137	50728	2023	7	94	**128.6**	**95.00**	**97.36**	**2.36**	**7.8**	**2.3**
HBJUG0515	20137	50728	2023	9	81	**143.0**	**94.00**	**100.80**	**6.80**	**5.1**	**6.5**
HBJUG0516	20137	50728	2023	-31	150	225.3	206.84	211.41	4.57	2.2	2.0
HBJUG0517	20137	50728	2023	-38	137	**243.4**	**217.00**	**227.00**	**10.00**	**3.7**	**5.4**
						243.4	**233.00**	**237.00**	**4.00**	**6.0**	**2.1**
HBJUG0519	20138	50728	22	44	105	240.7	164.16	167.06	2.90	4.2	2.1
HBJUG0525	20146	50816	2035	-5	84	**104.9**	**72.44**	**84.44**	**12.00**	**10.0**	**11.6**
HBJUG0526	20146	50816	2035	30	112	**117.8**	**100.86**	**104.04**	**3.18**	**5.0**	**2.5**
HBJUG0527	20146	50816	2035	-6	88	**93.0**	**70.28**	**79.00**	**8.72**	**13.1**	**8.5**
HBJUG0528	20146	50816	2035	10	88	**132.0**	**71.27**	**80.15**	**8.88**	**2.5**	**8.7**
HBJUG0529	20146	50816	2035	25	81	**147.0**	**83.59**	**89.42**	**5.83**	**5.2**	**4.7**
HBJUG0530	20146	50816	2035	0	75	**136.0**	**72.16**	**80.00**	**7.84**	**7.5**	**7.3**
HBJUG0531	20146	50816	2035	31	70	**141.4**	**96.54**	**98.54**	**2.00**	**9.2**	**1.8**
HBJUG0533	20146	50816	2035	31	68	126.2	101.41	104.57	3.16	3.2	2.5
HBJUG0534	20146	50816	2035	11	64	**99.3**	**82.29**	**85.97**	**3.68**	**8.7**	**3.3**
HBJUG0538	20146	50816	2035	9	46	**113.1**	**95.56**	**104.74**	**9.18**	**7.1**	**6.9**
HBJUG0539	20146	50816	2035	-3	46	**110.9**	**88.59**	**96.59**	**8.00**	**7.6**	**5.7**
HBJUG0540	20146	50816	2035	31	44	**151.3**	**121.97**	**128.60**	**6.63**	**5.1**	**4.2**
HBJUG0541	20146	50816	2035	1	38	**123.3**	**98.06**	**109.22**	**11.16**	**3.8**	**7.7**
HBJUG0542	20146	50816	2035	23	37	142.0			NSI		
HBJUG0543	20146	50816	2035	1	31	**140.0**	**111.00**	**117.00**	**6.00**	**7.5**	**3.3**
HBJUG0544	20146	50816	2035	20	31	163.0	-	-	0.00	-	-
HBJUG0545	20146	50816	2035	13	31	148.6	136.67	139.16	2.49	6.1	1.2
HBJUG0546	20146	50816	2035	21	27	182.4	170.00	173.42	3.42	3.6	2.1
HBJUG0547	20146	50816	2035	12	25	121.0	164.51	167.24	2.73	4.1	1.4
HBJUG0548	20146	50816	2035	2	24	176.0	163.62	169.73	6.11	2.3	3.1
HBJUG0554A	20137	50728	2023	-60	111	195.0	109.00	111.80	2.80	6.2	1.5
							180.37	183.00	2.63	5.1	1.5
HBJUG0557	20146	50816	2035	-70	84	321.9	-	-	0.00	-	-
HBJUG0567	20123	50071	-220	-48	120	303.0	**195.23**	**198.00**	**2.77**	**7.2**	**2.8**
HBJUG0573	20153	50982	19	-42	39	176.1	88.68	90.00	1.32	1.6	4.4
HBJUG0576	20153	50982	19	-52	85	138.8	**74.00**	**81.00**	**7.00**	**4.6**	**4.3**
HBJUG0594	20151	50982	17	-54	23	219.4	**118.00**	**134.00**	**16.00**	**10.4**	**3.8**

Table 5 – South Kalgoorlie Exploration Significant Intersections

SOUTH KALGOORLIE EXPLORATION SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (degrees, MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
XGRC18005	363545	6569420	377	-61	270	84.0	58.0	79.0	21.0	2.3	21.0
	including						75.0	78.0	3.0	7.6	3.0
SPDD18001	360070	6562019	336	-55	280	369.1	144.0	145.0	1.0	3.7	1.0
							222.9	224.3	1.4	8.9	1.4
	including						223.3	223.6	0.3	35.1	0.3
							233.6	235.7	2.0	43.8	2.0
							242.8	243.2	0.4	24.9	0.4
							302.6	304.1	1.6	3.3	1.6
							305.3	308.7	3.3	4.5	3.3
SPDD18002	360075	6562218	336	-52	283	296.7	151.3	153.2	1.9	5.3	1.9
	including						152.9	153.2	0.3	30.7	0.3
							155.4	158.9	3.5	1.7	3.5
							163.2	163.6	0.4	17.6	0.4
TODD18162	341738	6575807	342	-60	40	383.8	91.8	95.2	3.4	0.7	3.4
							97.0	112.0	15.0	1.0	15.0
							152.5	178.7	26.2	1.6	26.2
	including						152.5	152.8	0.3	17.6	0.3
							226.9	238.2	11.3	0.8	11.3
							248.5	250.4	1.9	1.8	1.9

Table 6 - Jundee Significant Intersections

JUNDEE SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
BARTON											
BDXP0664	50833	97456	2420	5	294	458.9	309.0	310.4	1.4	1.7	1.4
							397.0	399.0	2.0	2.9	0.9
							432.4	**433.0**	**0.6**	**58.7**	**0.5**
BDXP0665	50833	97455	2421	11	298	319.9	130.2	130.6	0.4	3.0	0.3
							256.6	257.0	0.4	2.3	0.3
BDXP0666	50833	97456	2420	1	299	467.9	255.5	255.8	0.3	4.8	0.3
							284.3	285.5	1.2	17.5	1.0
							307.0	309.0	2.0	2.8	0.7
							456.1	456.4	0.3	54.7	0.3
BDXP0667	**50833**	**97456**	**2420**	**1**	**305**	**467.6**	**163.0**	**164.0**	**1.0**	**51.0**	**1.0**
BDXP0676	50431	97382	2191	18	47	145.0			NSI		
BDXP0679	50438	97377	2189	-12	166	89.8			NSI		
BDXP0680	50438	97377	2189	-19	170	79.1			NSI		
BDXP0681	50437	97377	2189	-26	183	80.1			NSI		
BDXP0682	50437	97377	2189	-10	185	250.0	215.6	217.4	1.8	8.1	1.5
BDXP0668	50413	97375	2191	8	223	229.0	164.1	164.5	0.4	9.6	0.4
BDXP0668	50413	97375	2191	8	223	229.0	173.0	174.0	1.0	2.6	0.2
BDXP0668	50413	97375	2191	8	223	229.0	214.5	217.5	3.0	4.6	2.6
BDXP0669	50412	97378	2191	21	264	299.1			NSI		
BDXP0670	50412	97377	2190	-1	264	299.7			NSI		
BDXP0671	50422	97383	2190	9	13	90.1			NSI		
BDXP0672	50423	97383	2189	-10	21	60.0			NSI		
BDXP0673	50422	97383	2189	-45	3	69.0			NSI		
BDXP0674	50423	97383	2189	-59	311	79.1	33.4	36.8	3.5	3.9	2.4
BDXP0675	50425	97381	2188	-80	220	48.0	27.6	28.0	0.3	2.0	0.3
BDXP0675	50425	97381	2188	-80	220	48.0	28.4	29.0	0.6	7.6	0.4
BDXP0675	50425	97381	2188	-80	220	48.0	29.7	30.0	0.3	14.0	0.3
BDXP0677	50432	97382	2191	19	33	135.0			NSI		
BDXP0678	50432	97382	2190	11	27	86.2			NSI		
INVICTA											
VDXP0137	50317	97770	2350	-5	254	399.6	373.0	377.2	4.2	2.0	2.8
VDXP0140	50317	97770	2350	-5	278	359.9	245.5	246.6	1.1	5.7	0.6
							340.0	340.9	0.9	6.3	0.7
VDXP0134	50318	97770	2352	0	266	360.0	317.7	319.0	1.3	2.5	0.6
VDXP0136	50317	97770	2350	-2	269	360.0	211.7	213.5	1.8	11.3	0.9
							214.1	214.4	0.3	2.8	0.3
							215.7	218.1	2.4	9.5	1.2
							231.0	232.4	1.4	1.2	0.3
							333.0	333.4	0.4	2.0	0.3
VDXP0139	50317	97770	2351	0	273	349.9	212.7	213.7	1.1	3.1	0.9
							319.3	320.4	1.1	4.2	0.9
VDXP0141	50326	97772	2352	16	90	190.0			NSI		
VDXP0142	50326	97773	2352	23	60	321.7	154.0	155.0	1.0	10.5	0.3
							180.0	184.0	4.0	1.9	4.0
							231.3	231.7	0.4	12.1	0.3
							245.0	247.0	2.0	39.9	0.4
CARDASSIAN											
CDXP0447A	**50203**	**98262**	**2441**	**-5**	**276**	**402.8**	**118.4**	**119.9**	**1.5**	**34.3**	**1.2**
							174.3	175.0	0.7	10.1	0.3
CDXP0448	50203	98262	2440	-14	276	396.5			NSI		
CDXP0449	50203	98262	2441	4	276	361.0	191.7	192.0	0.3	19.0	0.3
							252.3	252.6	0.3	15.2	0.3
CDXP0452	50203	98263	2441	-9	282	270.7			NSI		
CDXP0457	50203	98262	2441	2	294	154.0	147.0	148.0	1.0	35.0	0.3
CDXP0446	50203	98262	2441	-9	272	380.7	121.0	123.6	2.6	2.6	2.2
							217.0	217.9	0.9	6.6	0.3
							277.5	277.8	0.3	5.2	0.3
							330.9	331.2	0.3	7.1	0.3
CDXP0451	50203	98262	2441	3	282	273.0	117.0	118.1	1.1	4.8	0.8
							173.0	173.4	0.4	2.6	0.3
							178.1	178.4	0.3	2.9	0.3
							193.1	193.4	0.3	34.2	0.3
							270.0	270.3	0.3	33.7	0.3
CDXP0453	50203	98262	2440	-16	284	196.0	130.2	132.6	2.4	2.6	1.5
							158.2	158.5	0.3	2.5	0.3
							188.1	188.4	0.3	3.6	0.3
CDXP0456	50203	98262	2441	-9	291	269.9	186.0	188.0	2.0	1.2	0.4
							224.7	225.0	0.3	0.3	0.3
CDGC0683	50132	98261	2397	7	263	354.8	107.0	108.0	1.0	2.1	0.3
							148.0	149.3	1.3	4.7	0.8
							148.0	149.3	1.3	4.7	0.3
							151.0	152.0	1.0	19.0	0.3
							151.0	152.0	1.0	19.0	0.5
							260.0	260.5	0.4	2.4	0.3
CDGC0685	50132	98261	2397	9	267	336.9	161.0	162.0	1.0	2.1	0.3
							193.9	**194.8**	**0.9**	**177.8**	**0.8**
CDGC0686	50132	98261	2396	2	268	252.0	140.0	141.0	1.0	2.8	0.2
							227.4	227.8	0.4	48.1	0.3
CDGC0688	50132	98261	2396	4	272	225.0	92.0	93.0	1.0	3.0	0.8
CDGC0692	50132	98261	2397	14	248	223.0			NSI		
CDGC0693	50132	98261	2397	5	249	242.0	125.4	126.0	0.5	11.5	0.4
							177.0	178.0	1.0	7.0	0.3
							201.5	202.0	0.5	22.8	0.3
							215.0	215.5	0.5	35.5	0.3
CDGC0694	50132	98261	2396	3	252	243.1	171.0	172.0	1.0	3.4	0.4
							205.0	206.0	1.0	13.3	0.3
							226.0	227.3	1.3	3.6	1.0
CDGC0697	50132	98261	2396	-1	256	470.1	64.9	65.4	0.5	10.4	0.5
							66.1	66.4	0.3	2.7	0.2
							67.3	68.3	1.0	4.5	0.8
							112.0	113.0	1.0	3.2	0.3

JUNDEE SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
							168.5	168.9	0.4	13.7	0.4
CDGC0698	50132	98261	2396	3	258	408.1	63.5	65.1	1.6	2.4	1.2
							195.7	196.1	0.4	10.4	0.3
							212.0	213.0	1.0	2.2	0.3
CDGC0681	50132	98261	2397	19	261	218.1	58.3	60.1	1.8	6.3	1.6
						218.1	130.0	131.0	1.0	7.7	0.3
						218.1	136.9	137.6	0.8	16.3	0.3
						218.1	187.9	188.5	0.5	9.4	0.4
						218.1	206.1	206.6	0.5	32.0	0.4
CDGC0684	**50132**	**98261**	**2397**	**14**	**264**	**354.9**	**123.3**	**124.0**	**0.7**	**98.2**	**0.7**
							173.3	174.0	0.7	11.3	0.6
							205.2	**205.8**	**0.6**	**290.8**	**0.6**
CDGC0689	50132	98261	2397	9	272	230.0	57.5	58.0	0.5	2.7	0.5
							140.7	141.0	0.3	5.3	0.3
							206.0	206.3	0.3	20.7	0.3
							207.9	208.2	0.3	8.3	0.2
CDGC0691	50132	98261	2397	8	276	234.0	58.4	59.3	0.9	2.3	0.9
							140.7	141.5	0.8	12.9	0.7
							208.9	**209.3**	**0.4**	**95.9**	**0.3**
							210.8	212.0	1.2	3.0	0.8
							213.4	**215.7**	**2.3**	**45.7**	**2.0**
CDGC0696	50132	98261	2396	1	256	367.2	65.4	67.6	2.2	5.1	1.9
							169.5	170.0	0.5	30.4	0.3
CDGC0668	49853	98532	2299	-38	350	104.4	64.5	65.0	0.5	8.6	0.3
CDGC0669	**49853**	**98532**	**2299**	**-38**	**350**	**91.0**	**50.9**	**51.6**	**0.7**	**149.0**	**0.3**
							61.3	**67.9**	**6.6**	**11.3**	**2.3**
CDGC0670	49852	98532	2302	24	354	222.2	23.5	23.8	0.3	2.2	0.3
							23.5	23.8	0.3	2.2	0.3
							50.0	50.8	0.8	2.3	0.3
							50.0	50.8	0.8	2.3	0.4
							111.4	112.1	0.8	8.1	0.6
							111.8	112.1	0.3	16.0	0.3
CDGC0671	49853	98532	2301	10	358	189.0	14.5	15.3	0.8	28.5	0.5
							94.6	**101.7**	**7.1**	**16.9**	**5.0**
CDGC0672	49853	98532	2300	-33	5	92.0	25.0	27.0	2.0	7.4	0.3
							49.4	49.7	0.3	11.7	0.3
							61.8	65.6	3.8	0.6	0.8
CDGC0673	49853	98532	2300	-15	15	91.1	13.6	14.3	0.8	7.7	0.3
							61.5	63.5	2.0	4.8	2.0
CDGC0674	49853	98532	2300	-55	28	99.0	23.3	24.1	0.8	16.4	0.5
							26.5	27.0	0.5	3.5	0.3
							29.3	30.0	0.7	3.7	0.5
CDGC0675	49853	98532	2299	-29	36	92.0	8.9	9.2	0.3	6.7	0.3
							62.0	62.3	0.3	3.4	0.3
CDGC0676	49853	98532	2300	-14	40	100.9	7.0	7.3	0.3	9.4	0.3
							71.9	82.2	10.3	1.5	7.0
CDGC0677	49853	98532	2301	6	48	143.0	6.7	7.0	0.3	8.2	0.3
							76.8	77.1	0.3	2.9	0.3
CDGC0678	**49854**	**98532**	**2299**	**-48**	**51**	**99.0**	**12.5**	**14.5**	**2.0**	**50.9**	**0.9**
							30.2	30.5	0.3	2.3	0.3
CDGC0679	49854	98532	2300	-24	51	96.0	7.6	8.0	0.3	23.2	0.3
CDGC0680	49854	98532	2300	-12	54	126.0	6.0	6.8	0.8	14.6	0.3
CDGC0686	50132	98261	2396	2	268	252.0	140.0	141.0	1.0	2.8	0.3
							227.4	227.8	0.4	48.1	0.4
DEAKIN											
DKXP0011	**50035**	**97834**	**2389**	**-28**	**292**	**250.0**	**178.0**	**179.2**	**1.3**	**29.0**	**0.8**
							218.2	**218.7**	**0.5**	**102.0**	**0.4**
DKXP0012	50035	97834	2389	-23	293	244.0	145.4	146.1	0.6	2.4	0.3
							207.4	207.9	0.6	6.1	0.5
DKXP0013	50035	97834	2389	-30	296	250.0	178.2	179.5	1.3	22.9	0.6
DKXP0016	50036	97831	2390	-27	282	487.1	212.4	213.9	1.5	5.0	1.2
							397.0	397.3	0.3	7.8	0.3
							398.9	399.3	0.4	13.1	0.3
DKXP0017	50036	97831	2390	-35	277	252.0			NSI		
DKXP0018	50036	97831	2390	-34	273	250.0	34.0	34.6	0.6	5.6	0.6
DKXP0019	50036	97831	2390	-32	267	251.0			NSI		
DKXP0020	50036	97831	2390	-28	267	242.0	31.0	31.3	0.3	3.3	0.3
							221.7	223.2	1.6	1.4	6.7
DKXP0007	50036	97831	2390	-25	284	251.9	212.7	213.4	0.7	3.0	0.5
DKXP0008	50035	97834	2389	-28	286	257.8			NSI		
DKXP0009	50035	97834	2389	-24	288	238.0			NSI		
DKXP0010	50035	97834	2389	-32	290	250.0			NSI		
DKXP0014	50035	97834	2389	-26	297	244.0	214.0	215.0	1.0	34.8	0.3
NEXUS											
NXXP0160	49467	96285	2357	-3	87	135.0	32.2	32.6	0.4	4.5	0.4
NXXP0164	49468	96282	2358	1	112	175.0			NSI		
NXXP0159	49467	96285	2356	-19	83	400.1	227.0	227.3	0.3	11.2	0.3
NXXP0161	49468	96282	2358	6	97	110.1	67.5	68.0	0.5	7.3	0.3
NXXP0162	49468	96282	2357	-13	98	89.9	32.0	32.3	0.3	2.2	0.3
NXXP0163	49468	96282	2356	-22	108	210.0	26.0	27.0	1.0	12.5	0.3
							130.0	131.0	1.0	4.8	0.3
NXXP0165	49468	96282	2357	-8	120	155.0			NSI		
NXXP0166	49468	96282	2357	6	123	149.9			NSI		
NXXP0167	49468	96282	2356	-22	131	149.9	48.0	48.3	0.3	9.1	0.3
NXGC0162	49272	96368	2338	2	48	188.9			NSI		
NXGC0163	49272	96368	2338	-2	51	166.0			NSI		
NXGC0165	49272	96368	2338	-7	65	125.0			NSI		
NXGC0166	49272	96368	2338	-14	72	110.0			NSI		
NXGC0167	49272	96368	2338	-8	85	118.0			NSI		
NXGC0168	49272	96368	2337	-38	93	88.1	81.8	83.2	1.4	1.9	1.3
NXGC0169	49272	96368	2337	-15	95	120.0			NSI		
NXGC0170	49272	96368	2337	-50	100	113.8	89.0	90.5	1.5	3.4	1.5
NXGC0171	49272	96368	2337	-12	108	121.1			NSI		
NXGC0172	49272	96368	2337	-35	114	113.9			NSI		
NXGC0182	49267	96379	2337	-53	10	286.9	157.2	158.8	1.6	4.2	0.8

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Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
							178.1	178.9	0.8	2.5	0.5
							180.7	181.0	0.3	3.8	0.3
							192.2	192.6	0.4	4.2	0.3
							215.3	215.6	0.3	2.2	0.3
NXGC0183	49267	96379	2337	-57	11	280.0			NSI		
NXGC0184	49267	96379	2337	-51	12	242.0	150.4	153.0	2.6	3.0	0.5
							154.5	156.7	2.2	3.3	1.5
							174.3	174.6	0.3	7.1	0.3
							197.0	197.8	0.8	5.2	0.5
NXGC0185	49267	96379	2337	-48	17	241.0	137.0	137.5	0.5	2.6	0.5
NXGC0186	49267	96379	2337	-55	17	275.1	187.1	187.4	0.3	3.9	0.3
NXGC0187	49267	96379	2337	-51	18	231.0	136.3	136.8	0.6	5.0	0.5
NXGC0188	49267	96379	2338	-32	18	256.0	110.0	110.5	0.5	4.7	0.5
							144.0	145.4	1.4	2.2	0.5
NXGC0193	49267	96379	2337	-43	24	226.0	157.5	158.0	0.5	4.4	0.4
NXGC0195	49267	96378	2337	-46	27	215.0	139.5	141.0	1.5	3.9	1.0
NXGC0178	49267	96379	2337	-58	1	290.2	56.0	57.0	1.0	2.4	0.3
							228.8	**229.1**	**0.3**	**80.2**	**0.3**
							230.5	230.8	0.3	8.6	0.3
							244.0	245.0	1.0	2.7	0.5
							252.6	254.3	1.7	7.3	1.0
							264.3	265.0	0.7	4.5	0.5
NXGC0179	49267	96379	2337	-55	3	292.0	216.6	217.0	0.4	4.6	0.3
NXGC0180	49267	96379	2337	-62	3	295.0	290.7	291.0	0.3	3.4	0.2
NXGC0189	49267	96379	2337	-43	19	236.1	186.0	189.2	3.2	3.9	3.0
NXGC0190	49267	96379	2338	-25	20	266.0	18.0	24.0	6.0	4.1	4.5
							25.7	26.5	0.8	8.7	0.6
							235.3	235.6	0.3	2.8	0.3
NXGC0191	49267	96379	2338	-34	21	245.0	133.8	134.1	0.3	2.1	0.3
							186.2	189.1	2.9	2.9	0.6
NXGC0192	49267	96379	2338	-26	24	252.0	114.1	116.0	1.9	7.9	1.5
							173.0	174.0	1.0	3.9	0.4
							190.0	190.3	0.3	3.2	0.3
							225.0	226.0	1.0	5.1	1.0
NXGC0194	49267	96379	2338	-31	24	241.1	21.2	24.0	2.8	1.9	1.4
							108.0	108.6	0.6	5.5	0.3
NXGC0196	49268	96378	2337	-41	28	218.5	193.7	194.3	0.6	2.0	0.3
NXGC0197	49268	96378	2338	-37	33	207.0			NSI		
NXGC0198	49303	96284	2330	-45	87	183.0	63.5	66.7	3.2	2.1	3.0
							68.4	68.9	0.5	9.5	0.4
							108.0	110.2	2.2	3.4	1.2
							167.4	168.4	1.0	6.5	0.9
NXGC0207	49303	96284	2330	-26	73	195.1	53.8	54.4	0.6	4.0	0.5
							58.7	59.5	0.8	2.8	0.8
							63.0	63.5	0.5	2.0	0.4
							114.8	**115.1**	**0.3**	**72.1**	**0.3**
							115.4	116.0	0.6	2.4	0.6
							185.0	186.2	1.2	11.4	0.5
							189.0	190.3	1.3	2.4	1.2
NXGC0210	49303	96284	2330	-32	64	184.1	53.6	54.3	0.7	3.2	0.5
							163.4	164.0	0.6	22.9	0.5
NXGC0213	49303	96284	2330	-42	64	178.9	47.5	49.1	1.7	2.6	1.5
							51.1	51.4	0.3	5.0	0.3
							62.8	64.1	1.3	2.1	1.2
							163.8	165.0	1.2	4.1	1.1
NXGC0197	49268	96378	2338	-37	33	207.0	90.8	91.1	0.3	2.5	0.3
							129.2	130.4	1.2	4.5	0.8
							132.1	132.5	0.3	4.2	0.3
							135.2	136.2	1.0	4.8	1.0
							176.4	176.7	0.3	3.3	0.3
							194.3	194.6	0.3	2.8	0.3
NXGC0198	49303	96284	2330	-45	87	183.0	63.5	66.7	3.2	2.1	3.0
							68.4	68.9	0.5	9.5	0.4
							69.4	69.7	0.3	6.3	0.3
							109.0	110.2	1.2	5.3	1.0
							167.4	168.4	1.0	6.5	0.9
NXGC0199	49303	96284	2330	-49	94	191.0	172.0	177.4	5.4	2.0	2.5
NXGC0200	49303	96284	2330	-55	93	189.1	71.1	71.7	0.6	5.1	0.3
							72.1	72.4	0.3	7.1	0.3
							74.2	75.5	1.3	5.0	0.5
NXGC0200	49303	96284	2330	-55	93	189.1	79.5	80.7	1.2	8.2	0.5
							69.8	82.2	12.4	3.0	6.5
							170.2	172.3	2.0	2.0	1.2
NXGC0206	49303	96284	2330	-22	69	196.0	52.9	53.2	0.3	6.2	0.3
							55.0	55.5	0.5	3.2	0.4
							57.0	57.4	0.4	4.5	0.3
							59.7	60.4	0.7	2.2	0.7
							62.2	67.5	5.3	4.8	4.0
							118.6	118.9	0.3	27.7	0.3
							190.2	192.7	2.5	2.5	2.1
REVELATION											
RVGC0099	49367	95287	2223	-23	36	135.1			NSI		
RVGC0120	49367	95287	2224	-8	109	198.0			NSI		
RVGC0125	49367	95287	2224	-2	122	229.0			NSI		
RVGC0125	49367	95287	2224	-2	122	229.0			NSI		
RVGC0126	49367	95287	2224	-14	122	234.0	167.6	168.0	0.4	8.4	0.4
							177.6	183.6	6.0	2.2	1.0
							203.3	203.7	0.3	5.8	0.3
							205.7	207.3	1.5	4.1	1.5
RVGC0128	49354	95387	2238	-4	20	460.2	249.0	251.0	2.0	2.4	0.3
							316.0	319.7	3.7	3.2	2.5
RVGC0129	49355	95386	2239	11	34	347.0	227.0	228.0	1.0	16.4	0.7
							273.3	273.6	0.3	36.2	0.3
RVGC0138	49356	95385	2238	-14	70	262.0			NSI		
RVGC0139	49356	95385	2238	-2	71	264.1	42.7	46.5	3.8	1.4	3.0
RVGC0140	49356	95385	2239	5	72	269.1	220.0	221.0	1.0	2.3	0.3

JUNDEE SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
RVGC0142	49356	95385	2238	-4	77	264.3	57.8	58.1	0.3	2.2	0.3
							57.8	59.7	1.9	1.1	1.0
							249.4	249.9	0.6	4.4	0.3
RVGC0145	49356	95384	2238	-10	81	260.0	74.2	75.5	1.3	4.0	0.8
							240.3	247.2	6.9	1.8	6.0
RVGC0174	49356	95385	2239	19	80	299.8	53.0	53.5	0.5	3.3	0.3
							72.8	73.1	0.3	5.9	0.3
							128.7	129.0	0.3	2.7	0.3
							264.0	264.3	0.3	12.5	0.3
RVGC0183	49356	95385	2239	17	92	305.1	163.0	164.0	1.0	2.0	0.7
RVGC0185	49356	95384	2241	39	99	77.1			NSI		
RVGC0135	**49367**	**95287**	**2224**	**5**	**81**	**268.0**	**82.3**	**86.4**	**4.1**	**5.3**	**3.8**
							113.0	113.4	0.4	2.7	0.3
							217.0	217.4	0.4	5.7	0.3
RVGC0137	49367	95287	2223	-19	99	244.9	165.0	167.0	2.0	10.2	1.5
							177.6	177.9	0.3	10.1	0.3
RVGC0143	49356	95384	2239	-22	80	215.0	87.2	87.5	0.3	13.8	0.3
							158.7	159.1	0.3	3.8	0.3
RVGC0144	49356	95384	2237	-42	81	219.0	144.0	153.0	9.0	2.4	5.1
RVGC0147	49356	95383	2237	-55	96	150.0			NSI		
RVGC0168	49355	95385	2239	3	67	231.1	31.0	32.0	1.0	4.1	0.3
							42.3	42.7	0.4	2.0	0.3
							61.3	61.7	0.5	11.0	0.3
RVGC0169	49355	95385	2239	9	73	234.9	74.7	75.0	0.3	4.6	0.3
							119.8	120.1	0.3	2.9	0.2
RVGC0172	49355	95385	2239	8	75	274.0	42.4	44.0	1.6	3.7	1.4
							56.9	59.2	2.3	1.7	1.0
							260.7	261.0	0.3	7.4	0.3
RVGC0173	49355	95385	2239	15	79	288.9	62.8	63.1	0.3	6.4	0.3
						288.9	266.2	266.5	0.3	2.4	0.3
RVGC0177	49356	95385	2239	18	86	300.0			NSI		
RVGC0178	49355	95385	2239	8	87	273.0	59.6	60.0	0.4	4.8	0.3
							78.8	81.0	2.2	2.1	1.8
RVGC0179	49355	95385	2239	-2	88	261.0	48.5	51.8	3.3	2.1	3.0
							64.0	65.7	1.7	2.6	1.2
							226.1	226.4	0.3	4.7	0.3
							242.2	242.9	0.7	3.5	0.7
RVGC0180	49355	95385	2239	6	90	272.0	67.4	67.7	0.3	3.9	0.3
							116.0	118.0	2.0	6.4	1.6
							230.1	230.6	0.5	7.5	0.3
RVGC0170	49356	95385	2239	18	73	302.0			NSI		
RVGC0175	49355	95385	2239	10	81	275.9	68.7	69.0	0.3	4.2	0.3
						275.9	257.2	258.2	1.0	1.4	0.5
RVGC0181	49355	95385	2239	1	92	266.1	62.9	63.2	0.3	9.4	0.2
							107.9	109.0	1.1	2.9	1.0
							235.0	236.0	1.0	2.2	0.3
							256.9	257.5	0.6	4.5	0.5
RVGC0182	49355	95385	2239	13	92	288.0	58.5	58.8	0.3	2.8	0.3
							71.6	71.9	0.3	4.7	0.3
RVGC0186	49308	95510	2258	-9	14	169.0	25.0	25.8	0.8	2.3	0.3
RVGC0187	49308	95510	2258	-4	26	164.0			NSI		
RVGC0188	49308	95510	2257	-41	20	183.0	89.0	95.5	6.6	2.8	1.4
						183.0	153.0	154.0	1.0	2.5	0.3
RVGC0189	49308	95510	2258	-17	40	274.3	31.8	32.6	0.8	3.9	0.3
RVGC0190	49308	95510	2258	4	50	267.0	107.8	108.3	0.5	2.8	0.4
							173.9	174.5	0.6	7.1	0.5
							176.9	177.3	0.3	47.1	0.3
							196.0	197.0	1.0	19.0	1.0
							224.0	231.2	7.2	1.1	6.0
RVGC0191	49308	95510	2257	-24	48	241.0	28.0	30.0	2.0	3.3	0.5
							32.0	32.9	0.9	7.3	0.8
							85.8	86.1	0.3	2.5	0.3
RVGC0192	49308	95510	2258	-1	55	241.0	200.5	208.1	7.7	2.1	6.0
							215.0	216.9	1.8	3.3	1.7
							230.1	231.0	0.9	2.1	0.8
RVGC0193	49308	95510	2258	-7	47	248.0	184.6	185.0	0.4	2.3	0.3
							231.1	231.4	0.3	2.5	0.3
RVGC0194	49308	95510	2259	8	79	145.0	80.4	81.0	0.7	2.0	0.5
							80.4	81.0	0.7	2.0	0.5
							135.7	141.9	6.2	3.0	3.5
							135.7	141.9	6.2	3.0	5.0
RVGC0196	49308	95510	2258	-20	85	148.9	25.2	26.0	0.8	3.2	0.4
RVGC0197	49308	95510	2258	-24	76	139.4	33.4	33.7	0.3	2.0	0.3
RVGC0199	49308	95510	2258	-10	39	133.1			NSI		
RVGC0201	49308	95510	2257	-36	35	155.6	85.7	87.7	2.0	3.3	1.0
RVGC0202	49308	95510	2257	-45	32	172.0			NSI		
RVGC0203	49308	95510	2257	-45	53	158.9			NSI		
RVGC0207	49308	95510	2258	-1	45	271.0	202.8	203.3	0.5	24.2	0.3
							205.8	206.1	0.3	7.8	0.3
RVGC0208	49308	95510	2258	-1	51	248.9	18.2	18.6	0.4	2.6	0.3
							201.9	202.3	0.4	3.8	0.3
							220.4	221.0	0.6	3.3	0.5
							233.0	234.0	1.0	2.6	0.3
RVGC0209	49308	95510	2258	-3	47	259.0	17.6	18.0	0.4	2.8	0.3
							37.5	38.0	0.5	2.0	0.3
							196.0	**197.0**	**1.0**	**386.0**	**0.3**
							204.2	205.1	0.9	2.8	0.8
							221.8	226.7	4.9	4.6	4.0
							232.0	232.6	0.6	2.5	0.5
RVGC0210	49308	95510	2258	-7	43	269.0	68.0	69.0	1.0	4.3	0.3
							191.2	192.4	1.2	1.8	0.3
RVGC0211	**49308**	**95510**	**2258**	**-12**	**46**	**244.0**	**204.9**	**205.3**	**0.3**	**266.0**	**0.3**
							229.0	229.6	0.6	2.9	0.4
RVGC0212	49308	95510	2258	-16	44	263.0	43.7	44.0	0.4	4.7	0.3
							184.7	185.1	0.4	5.4	0.3
							236.2	236.5	0.3	17.9	0.3

JUNDEE SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
							236.2	236.5	0.3	17.9	0.3
							239.4	239.9	0.5	10.8	0.4
							239.4	239.9	0.5	10.8	0.5
							256.0	260.0	4.0	1.5	1.0
RVGC0214	49308	95510	2258	-20	44	247.0	241.2	241.9	0.8	4.5	0.5
RVGC0216	49199	95675	2283	-9	51	221.9			NSI		
RVGC0218	49199	95675	2283	-5	43	255.1			NSI		
RVGC0220	49198	95676	2283	-5	36	284.8			NSI		
RVGC0221	49198	95675	2282	-16	34	295.0	268.2	268.5	0.3	2.9	0.3
RVGC0142	49356	95385	2238	-4	77	264.3	248.6	249.9	1.3	2.3	1.0
RVGC0200	49308	95511	2256	-22	37	141.0	29.8	30.2	0.4	2.9	0.3
RVGC0213	49308	95511	2257	-17	48	238.0			NSI		
RVGC0215	49199	95675	2282	-17	57	210.0	160.7	161.1	0.4	2.1	0.3
RVGC0219	49199	95675	2283	-13	40	262.0	234.3	234.6	0.3	4.4	0.3
					GATEWAY						
GWXP0419	**48897**	**96400**	**2290**	**-9**	**268**	**242.2**	**165.0**	**174.4**	**9.3**	**4.4**	**7.0**
							178.2	180.1	1.9	2.9	1.8
GWXP0419	48897	96400	2290	-9	268	242.2	207.9	209.8	1.8	3.0	1.3
GWXP0420	48897	96400	2290	7	272	152.8	132.3	134.6	2.3	3.3	2.0
GWXP0421	48897	96400	2290	-1	274	169.9	129.6	131.4	1.8	2.9	0.9
							151.7	154.2	2.5	4.2	2.0
							159.2	160.0	0.8	4.8	0.5
GWXP0419	**48897**	**96399**	**2290**	**-9**	**268**	**242.2**	**165.0**	**174.4**	**9.3**	**4.4**	**8.0**
							178.2	180.1	1.9	2.9	1.9
							207.9	210.2	2.3	2.5	2.0
GWXP0422	48897	96400	2292	27	276	179.9	81.5	82.4	0.9	9.6	0.7
							88.9	92.4	3.5	3.3	2.8
							101.0	102.0	1.0	5.0	0.3
							159.0	159.5	0.5	3.1	0.3
							177.0	177.9	0.9	6.4	0.5
GWXP0423	48897	96400	2290	-5	280	235.0			NSI		
GWXP0426A	48906	96403	2292	29	322	197.0	60.5	61.0	0.5	2.3	0.3
							153.0	154.8	1.8	5.1	0.8
							175.2	176.9	1.7	4.6	1.5
							191.0	192.0	1.0	14.8	0.5
GWXP0427	48907	96404	2291	19	340	111.7	57.1	57.4	0.4	2.3	0.3
GWXP0427A	48906	96403	2291	19	340	212.0			NSI		
GWXP0430	48906	96404	2292	20	7	209.0			NSI		
GWXP0433	**48897**	**96398**	**2291**	**10**	**259**	**150.0**	**71.9**	**76.7**	**4.8**	**7.9**	**4.0**
GWXP0434	48897	96399	2290	15	266	250.0			NSI		
GWXP0435	48897	96399	2290	-17	258	219.6			NSI		
GWXP0436	48897	96399	2290	-25	256	289.8			NSI		
GWGC0980	48897	96399	2294	57	242	119.0	4.1	5.0	0.9	2.5	0.6
GWGC0980	48897	96399	2294	57	242	119.0			NSI		
GWGC0981	48897	96399	2292	43	248	117.0			NSI		
GWGC0982	48897	96397	2292	34	257	117.1			NSI		
GWGC0983	48897	96397	2293	50	257	120.0	109.0	110.0	1.0	3.8	0.4
GWGC0984	48897	96398	2294	61	267	115.7	0.0	3.0	3.0	2.2	2.5
GWGC0985	48897	96397	2293	41	266	114.1			NSI		
GWGC0986	48897	96398	2293	50	275	113.8			NSI		
GWGC0987	48898	96400	2294	59	288	118.0			NSI		
GWGC0988	48897	96398	2293	56	300	120.1	67.0	71.9	4.9	1.6	3.5
							90.0	90.7	0.7	5.0	0.3
GWGC0989	48897	96399	2293	47	291	118.0	23.7	25.0	1.3	1.9	1.5
							106.6	107.0	0.4	2.0	0.3
GWGC0990	48897	96399	2292	38	281	134.0	30.6	31.0	0.3	2.5	0.3
							87.0	88.0	1.0	8.1	0.6
							116.7	117.1	0.4	2.7	0.3
GWGC0991	**48897**	**96399**	**2293**	**29**	**285**	**120.0**	**96.3**	**99.4**	**3.1**	**14.5**	**2.5**
GWGC0992	48897	96399	2291	6	264	142.0	126.9	129.0	2.1	5.9	1.8
GWGC0993	48897	96399	2290	-4	262	171.1	150.8	151.3	0.5	2.1	0.3
							153.0	154.0	1.0	2.2	0.3
GWGC0994	48897	96399	2290	-9	263	186.0	164.0	170.9	6.9	2.8	3.4
							175.0	175.7	0.7	2.5	0.3
GWGC0995	48897	96399	2290	0	266	158.3	144.8	145.7	0.9	17.8	0.7
GWGC0996	48897	96399	2290	-12	266	198.1	180.2	192.5	12.3	1.4	7.0
GWGC0997	48897	96399	2290	-15	270	216.0			NSI		
GWGC0999	48897	96399	2290	-7	276	213.2	137.6	137.9	0.3	5.4	0.3
							179.6	180.0	0.4	2.5	0.3
							190.2	191.0	0.8	0.9	0.6
							194.3	195.0	0.7	3.2	0.4
GWGC1000	48897	96399	2290	-15	276	245.0			NSI		
GWGC1001	48897	96399	2291	1	286	191.0	154.3	155.7	1.3	12.0	1.1
GWGC1002	**48897**	**96399**	**2291**	**6**	**281**	**179.0**	**146.8**	**149.8**	**3.0**	**15.3**	**2.6**
							153.7	154.0	0.3	20.5	0.2
GWGC1003	48897	96399	2291	3	286	199.5	69.4	69.8	0.5	4.8	0.3
GWGC1003	**48897**	**96399**	**2291**	**3**	**286**	**199.5**	**154.3**	**156.0**	**1.7**	**28.5**	**1.5**
GWGC1013	48849	95789	1897	34	285	93.9	93.6	93.9	0.3	14.6	0.3
GWGC1014	48849	95789	1897	43	280	107.8	72.0	74.8	2.8	4.9	0.5
GWGC1015	48849	95789	1897	34	274	137.9	84.0	85.0	1.0	3.4	0.5
						137.9	109.7	110.8	1.1	14.4	0.5
GWGC1016	48849	95789	1897	45	265	128.0	66.9	69.0	2.1	22.1	0.3
						128.0	**104.0**	**106.1**	**2.1**	**27.0**	**1.0**
						128.0	107.3	107.7	0.4	16.3	0.4
GWGC1017	48849	95789	1897	32	261	92.9	57.0	59.0	2.0	4.2	1.5
GWGC1018	**48849**	**95789**	**1895**	**17**	**263**	**87.0**	**67.8**	**69.8**	**2.0**	**25.7**	**1.3**
GWGC1020	48849	95789	1895	4	260	78.0	66.6	67.4	0.8	26.0	0.4
GWGC1021	48849	95789	1895	3	275	144.0	97.2	97.6	0.4	13.9	0.3
						144.0	106.3	106.6	0.3	3.9	0.3
GWGC1022	48849	95789	1894	-7	273	145.0	88.3	90.0	1.7	7.3	1.4
							112.8	113.4	0.5	33.2	0.3
							135.4	136.1	0.7	3.2	0.6
GWGC1023	48849	95789	1894	-8	261	73.0			NSI		
GWXP0447	48849	95789	1895	-6	254	95.0			NSI		
GWXP0448A	48849	95789	1894	-10	254	172.0	92.7	93.0	0.3	2.5	0.3
							96.1	97.2	1.1	4.3	0.5

JUNDEE SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
GWXP0440	48849	95789	1894	-6	242	88.1	73.6	73.9	0.3	20.8	0.3
							84.0	84.3	0.4	13.4	0.3
GWXP0448	48849	95789	1894	-10	254	16.7			NSI		
GWXP0443	48849	95789	1894	-10	248	177.1	90.4	91.0	0.6	11.2	0.4
WESTSIDE											
WSGC4968	49732	96410	1952	-6	265	150.8	31.1	31.5	0.4	7.1	0.3
							38.5	38.9	0.4	3.0	0.3
							88.8	90.6	1.8	1.4	1.4
							143.0	**146.4**	**3.4**	**9.7**	**3.2**
WSGC4969	49732	96410	1952	-17	264	165.0	30.7	31.0	0.3	4.1	0.3
							51.0	53.7	2.7	3.0	0.9
WSGC4970	49732	96409	1952	-7	254	155.1	37.2	37.6	0.4	4.7	0.3
							78.4	79.2	0.8	6.6	0.6
							137.2	**141.1**	**3.9**	**8.0**	**3.4**
WSGC4971	49732	96409	1952	-19	253	170.0			NSI		
WSGC4972	**49733**	**96408**	**1952**	**5**	**236**	**155.0**	**33.9**	**34.3**	**0.4**	**37.3**	**0.3**
							144.0	**144.5**	**0.5**	**25.3**	**0.5**
WSGC4973	49732	96409	1952	-9	240	131.8	32.6	32.9	0.3	5.1	0.3
							35.8	36.6	0.8	15.2	0.5
							66.2	67.0	0.8	4.1	0.6
WSGC4974	49733	96409	1952	-19	241	139.0	45.3	47.3	2.0	2.6	0.5
WSGC4975	49733	96409	1952	-8	227	108.0	37.0	37.4	0.4	2.5	0.3
							40.7	41.3	0.6	4.2	0.4
							61.2	61.8	0.5	5.0	0.4
WSGC4976	49733	96409	1951	-19	229	150.0	37.8	38.1	0.3	4.7	0.3
							58.8	59.8	1.0	18.0	0.7
							128.3	129.0	0.7	3.8	0.5
WSGC4977	49733	96408	1952	3	211	110.0	33.3	34.4	1.1	6.5	0.8
							35.3	35.6	0.3	4.8	0.3
							59.5	60.3	0.8	3.6	0.5
							70.0	70.7	0.8	5.2	0.7
WSGC4978	49733	96409	1952	-8	214	110.0	39.7	40.7	1.0	15.7	0.8
ZODIAC											
NSRJRD10447W4	49282	95392	2571	-60	102.3	2165.00	1632.38	1632.76	0.38	2.3	0.3
							1706.80	1707.10	0.30	3.5	0.3
							1715.72	1716.35	0.63	3.5	0.5
							1763.47	1763.83	0.36	4.8	0.3
							1775.30	1775.60	0.30	2.9	0.3
							1808.00	1809.00	1.00	3.0	0.6
							1813.84	1814.36	0.52	4.8	0.4
							1836.00	1836.30	0.30	4.8	0.3
							1837.13	1839.76	2.63	4.5	2.1
							1840.86	1843.36	2.50	3.8	1.7
							1865.33	1865.63	0.30	4.5	0.3
							1869.44	1869.75	0.31	4.5	0.3

Table 7 - Ramone Significant Intersections

RAMONE INFILL SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
NSRJRC11488	285667	7060640	554	-60	40	23.0	8.00	11.00	3.0	1.2	1.5
							13.00	15.00	2.0	1.3	1.0
							18.00	19.00	1.0	1.4	0.5
							22.00	23.00	1.0	1.2	0.5
NSRJRC11489	285664	7060645	554	-60	150	40.0	28.00	30.00	2.0	1.7	1.0
NSRJRC11490	285662	7060649	554	-60	150	40.0	23.00	24.00	1.0	6.4	0.5
NSRJRC11491	285658	7060635	554	-60	150	30.0	21.00	23.00	2.0	1.2	1.0
NSRJRC11492	**285653**	**7060644**	**554**	**-60**	**150**	**40.0**	**34.00**	**36.00**	**2.0**	**10.9**	**1.0**
NSRJRC11493	285652	7060626	554	-60	150	10.0	7.00	8.00	1.0	1.2	0.5
NSRJRC11494	285649	7060630	554	-60	150	20.0	16.00	17.00	1.0	1.2	0.5
NSRJRC11495	285647	7060635	554	-60	150	30.0	16.00	17.00	1.0	2.5	0.5
							24.00	**30.00**	**6.0**	**3.6**	**3.0**
NSRJRC11496	285644	7060639	554	-60	150	35.0	19.00	22.00	3.0	2.4	1.5
							31.00	35.00	4.0	1.2	2.0
NSRJRC11497	285643	7060621	554	-60	150	10.0			NSI		
NSRJRC11498	285641	7060625	554	-60	150	20.0			NSI		
NSRJRC11499	**285638**	**7060630**	**554**	**-60**	**150**	**30.0**	**16.00**	**26.00**	**10.0**	**6.5**	**5.0**
NSRJRC11500	285636	7060634	554	-60	150	35.0	30.00	35.00	5.0	2.6	2.5
NSRJRC11501	285635	7060616	554	-60	150	10.0			NSI		
NSRJRC11502	285632	7060620	554	-60	150	20.0	0.00	5.00	5.0	1.9	2.5
NSRJRC11503	**285630**	**7060625**	**554**	**-60**	**150**	**30.0**	**3.00**	**17.00**	**14.0**	**2.3**	**7.0**
							26.00	30.00	4.0	1.1	2.0
NSRJRC11504	285627	7060629	554	-60	150	40.0	13.00	14.00	1.0	1.0	0.5
							18.00	26.00	8.0	1.6	4.0
							28.00	30.00	2.0	1.3	1.0
NSRJRC11505	285625	7060633	554	-60	150	50.0	23.00	26.00	3.0	1.6	1.5
							33.00	34.00	1.0	1.1	0.5
							36.00	40.00	4.0	2.5	2.0
							43.00	44.00	1.0	1.2	0.5
NSRJRC11506	285622	7060638	554	-60	150	64.0	41.00	42.00	1.0	1.8	0.5
							44.00	49.00	5.0	1.1	2.5
							55.00	57.00	2.0	1.5	1.0
NSRJRC11507	285626	7060611	554	-60	150	10.0			NSI		
NSRJRC11508	285623	7060615	554	-60	150	20.0			NSI		
NSRJRC11509	**285621**	**7060620**	**554**	**-60**	**150**	**30.0**	**1.00**	**8.00**	**7.0**	**3.5**	**3.5**
NSRJRC11510	285618	7060624	554	-60	150	40.0	8.00	21.00	13.0	1.2	6.5
							23.00	26.00	3.0	1.4	1.5
NSRJRC11511	285616	7060628	554	-60	150	50.0	22.00	23.00	1.0	1.7	0.5
							26.00	**50.00**	**24.0**	**2.0**	**12.0**
NSRJRC11512	285613	7060633	554	-60	150	60.0	27.00	30.00	3.0	1.9	1.5
							39.00	41.00	2.0	1.1	1.0

RAMONE INFILL SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
							46.00	47.00	1.0	2.2	0.5
							53.00	54.00	1.0	1.7	0.5
							59.00	60.00	1.0	1.7	0.5
NSRJRC11513	285611	7060637	554	-60	150	64.0	5.00	6.00	1.0	7.5	0.5
							62.00	64.00	2.0	1.8	1.0
NSRJRC11514	285617	7060606	554	-60	150	10.0	6.00	7.00	1.0	2.7	0.5
NSRJRC11515	285615	7060610	554	-60	150	20.0			NSI		
NSRJRC11516	**285612**	**7060615**	**554**	**-60**	**150**	**30.0**	**0.00**	**8.00**	**8.0**	**4.5**	**4.0**
NSRJRC11517	285607	7060623	554	-60	150	50.0	14.00	17.00	3.0	1.4	1.5
							19.00	24.00	5.0	1.6	2.5
							26.00	34.00	8.0	1.7	4.0
NSRJRC11518	285605	7060628	554	-60	150	60.0	14.00	17.00	3.0	1.0	1.5
							24.00	25.00	1.0	10.8	0.5
							28.00	41.00	13.0	1.3	6.5
							43.00	**56.00**	**13.0**	**1.6**	**6.5**
NSRJRC11519	285602	7060632	554	-60	150	64.0	35.00	37.00	2.0	2.3	1.0
NSRJRC11520	285600	7060636	554	-60	150	64.0	11.00	12.00	1.0	2.1	0.5
							20.00	21.00	1.0	1.3	0.5
NSRJRC11521	285595	7060645	554	-60	150	64.0			NSI		
NSRJRC11522	285592	7060649	554	-60	150	64.0	28.00	29.00	1.0	1.0	0.5
NSRJRC11523	285590	7060654	554	-60	150	64.0	51.00	52.00	1.0	1.1	0.5
							56.00	57.00	1.0	1.0	0.5
NSRJRC11524	285587	7060658	554	-60	150	64.0	58.00	59.00	1.0	1.5	0.5
							62.00	64.00	2.0	2.4	1.0
NSRJRC11525	285582	7060667	554	-60	150	64.0			NSI		
NSRJRC11526	285608	7060601	554	-60	150	10.0			NSI		
NSRJRC11527	285606	7060605	554	-60	150	20.0	2.00	4.00	2.0	4.4	1.0
							6.00	11.00	5.0	1.3	2.5
NSRJRC11528	285603	7060610	554	-60	150	30.0	7.00	9.00	2.0	1.3	1.0
							13.00	15.00	2.0	1.3	1.0
NSRJRC11529	**285601**	**7060614**	**554**	**-60**	**150**	**40.0**	**5.00**	**26.00**	**21.0**	**3.0**	**10.5**
							30.00	32.00	2.0	1.1	1.0
NSRJRC11530	**285598**	**7060618**	**554**	**-60**	**150**	**50.0**	2.00	5.00	3.0	2.0	1.5
							11.00	34.00	23.0	4.9	11.5
NSRJRC11531	**285596**	**7060623**	**554**	**-60**	**150**	**60.0**	16.00	22.00	6.0	3.6	3.0
							24.00	**41.00**	**17.0**	**5.5**	**8.5**
							48.00	53.00	5.0	1.4	2.5
NSRJRC11532	285593	7060627	554	-60	150	64.0	0.00	2.00	2.0	1.4	1.0
							33.00	35.00	2.0	2.4	1.0
							37.00	43.00	6.0	1.3	3.0
							45.00	59.00	14.0	1.3	7.0
							62.00	64.00	2.0	1.7	1.0
NSRJRC11533	285591	7060631	554	-60	150	64.0	28.00	29.00	1.0	1.4	0.5
							43.00	48.00	5.0	1.8	2.5
NSRJRC11534	285588	7060636	554	-60	150	64.0	51.00	53.00	2.0	6.7	1.0
NSRJRC11535	285586	7060640	554	-60	150	64.0	37.00	38.00	1.0	1.7	0.5
							43.00	44.00	1.0	1.4	0.5
NSRJRC11536	285583	7060644	554	-60	150	64.0	28.00	29.00	1.0	1.5	0.5
							46.00	47.00	1.0	6.2	0.5
NSRJRC11537	285581	7060649	554	-60	150	64.0	34.00	35.00	1.0	2.3	0.5
NSRJRC11538	285578	7060653	554	-60	150	64.0	63.00	64.00	1.0	1.7	0.5
NSRJRC11539	285576	7060657	554	-60	150	64.0	45.00	46.00	1.0	1.0	0.5
NSRJRC11540	285600	7060596	554	-60	150	15.0	3.00	4.00	1.0	2.6	0.5
NSRJRC11541	285597	7060600	554	-60	150	25.0	8.00	13.00	5.0	1.6	2.5
NSRJRC11542	**285595**	**7060605**	**554**	**-60**	**150**	**35.0**	**11.00**	**22.00**	**11.0**	**2.9**	**5.5**
NSRJRC11543	**285592**	**7060609**	**554**	**-60**	**150**	**45.0**	**10.00**	**31.00**	**21.0**	**4.5**	**10.5**
							42.00	43.00	1.0	2.1	0.5
NSRJRC11544	**285590**	**7060613**	**557**	**-60**	**150**	**55.0**	**13.00**	**41.00**	**28.0**	**1.6**	**14.0**
NSRJRC11545	**285587**	**7060618**	**554**	**-60**	**150**	**64.0**	18.00	24.00	6.0	3.4	3.0
							26.00	**49.00**	**23.0**	**2.3**	**11.5**
							54.00	58.00	4.0	1.1	2.0
NSRJRC11546	285585	7060622	554	-60	150	64.0	30.00	31.00	1.0	1.1	0.5
							33.00	42.00	9.0	2.2	4.5
							44.00	**61.00**	**17.0**	**3.1**	**8.5**
NSRJRC11547	285582	7060626	554	-60	150	64.0	15.00	18.00	3.0	3.4	1.5
							21.00	26.00	5.0	1.1	2.5
							50.00	51.00	1.0	1.4	0.5
							54.00	**56.00**	**2.0**	**10.2**	**1.0**
							59.00	**64.00**	**5.0**	**30.8**	**2.5**
NSRJRC11548	285580	7060631	554	-60	150	64.0	0.00	1.00	1.0	2.5	0.5
NSRJRC11548	285580	7060631	554	-60	150	64.0	23.00	24.00	1.0	2.0	0.5
						64.0	41.00	47.00	6.0	1.0	3.0
							51.00	55.00	4.0	2.8	2.0
NSRJRC11549	285577	7060635	554	-60	150	64.0	62.00	63.00	1.0	2.7	0.5
NSRJRC11550	285575	7060639	554	-60	150	64.0	60.00	61.00	1.0	1.2	0.5
NSRJRC11551	285572	7060644	554	-60	150	64.0			NSI		
NSRJRC11552	285570	7060648	554	-60	150	64.0			NSI		
NSRJRC11553	285567	7060652	554	-60	150	64.0			NSI		
NSRJRC11554	285589	7060595	554	-60	150	25.0	8.00	13.00	5.0	3.5	2.5
NSRJRC11555	**285586**	**7060600**	**554**	**-60**	**150**	**64.0**	**12.00**	**22.00**	**10.0**	**10.6**	**5.0**
NSRJRC11556	**285584**	**7060604**	**554**	**-60**	**150**	**45.0**	**1.00**	**19.00**	**18.0**	**4.6**	**9.0**
							24.00	33.00	9.0	3.4	4.5
NSRJRC11561	285571	7060626	554	-60	150	64.0	21.00	23.00	2.0	2.2	1.0
							25.00	27.00	2.0	1.2	1.0
							34.00	38.00	4.0	2.3	2.0
							46.00	50.00	4.0	1.3	2.0
							55.00	58.00	3.0	4.5	1.5
NSRJRC11562	285569	7060630	554	-60	150	64.0	11.00	12.00	1.0	1.2	0.5
							35.00	41.00	6.0	2.6	3.0
							55.00	59.00	4.0	2.4	2.0
NSRJRC11563	285566	7060634	554	-60	150	64.0	33.00	38.00	5.0	1.1	2.5
							50.00	51.00	1.0	10.4	0.5
							53.00	56.00	3.0	1.0	1.5
NSRJRC11564	285564	7060639	554	-60	150	64.0	42.00	51.00	9.0	1.6	4.5
							59.00	61.00	2.0	2.3	1.0
NSRJRC11565	285561	7060643	554	-60	150	64.0	47.00	48.00	1.0	1.4	0.5

RAMONE INFILL SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
							52.00	55.00	3.0	2.7	1.5
							60.00	61.00	1.0	1.1	0.5
NSRJRC11566	285559	7060647	554	-60	150	64.0	3.00	4.00	1.0	1.2	0.5
							11.00	12.00	1.0	1.7	0.5
							28.00	29.00	1.0	1.0	0.5
NSRJRC11567	285556	7060652	554	-60	150	64.0	36.00	37.00	1.0	1.2	0.5
							63.00	64.00	1.0	1.4	0.5
NSRJRC11568	285580	7060590	554	-60	150	35.0			NSI		
NSRJRC11569	**285577**	**7060595**	**554**	**-60**	**150**	**45.0**	**1.00**	**17.00**	**16.0**	**2.0**	**8.0**
							28.00	29.00	1.0	13.0	0.5
NSRJRC11570	285575	7060599	554	-60	150	55.0	11.00	21.00	10.0	1.3	5.0
							23.00	28.00	5.0	1.2	2.5
NSRJRC11571	**285572**	**7060603**	**554**	**-60**	**150**	**64.0**	8.00	12.00	4.0	1.6	2.0
							14.00	**36.00**	**22.0**	**2.0**	**11.0**
							47.00	50.00	3.0	1.3	1.5
							52.00	54.00	2.0	2.5	1.0
NSRJRC11572	**285570**	**7060608**	**554**	**-60**	**150**	**64.0**	**9.00**	**39.00**	**30.0**	**5.5**	**15.0**
							43.00	46.00	3.0	1.2	1.5
							57.00	60.00	3.0	1.4	1.5
							62.00	64.00	2.0	3.2	1.0
NSRJRC11573	**285567**	**7060612**	**554**	**-60**	**150**	**64.0**	**13.00**	**21.00**	**8.0**	**5.7**	**4.0**
							23.00	28.00	5.0	4.1	2.5
							31.00	**41.00**	**10.0**	**6.0**	**5.0**
							45.00	54.00	9.0	3.5	4.5
							62.00	64.00	2.0	9.2	1.0
NSRJRC11574	285565	7060616	554	-60	150	64.0	16.00	25.00	9.0	2.9	4.5
							44.00	46.00	2.0	1.2	1.0
							50.00	53.00	3.0	2.6	1.5
							56.00	59.00	3.0	3.6	1.5
							61.00	64.00	3.0	1.6	1.5
NSRJRC11575	285562	7060621	554	-60	150	64.0	18.00	27.00	9.0	3.3	4.5
							33.00	34.00	1.0	2.3	0.5
							44.00	45.00	1.0	1.4	0.5
							51.00	54.00	3.0	8.3	1.5
							59.00	64.00	5.0	3.3	2.5
NSRJRC11576	285560	7060625	554	-60	150	64.0	23.00	28.00	5.0	1.5	2.5
							35.00	36.00	1.0	1.0	0.5
							39.00	40.00	1.0	5.5	0.5
							48.00	49.00	1.0	9.5	0.5
NSRJRC11577	285557	7060629	554	-60	150	64.0	35.00	39.00	4.0	1.6	2.0
							51.00	**54.00**	**3.0**	**7.1**	**1.5**
NSRJRC11578	**285555**	**7060634**	**554**	**-60**	**150**	**64.0**	**45.00**	**53.00**	**8.0**	**3.8**	**4.0**
NSRJRC11582	285569	7060590	554	-60	150	50.0	5.00	10.00	5.0	2.8	2.5
							13.00	14.00	1.0	2.9	0.5
							29.00	30.00	1.0	1.4	0.5
NSRJRC11583	285567	7060594	554	-60	150	60.0	4.00	7.00	3.0	1.2	1.5
							9.00	13.00	4.0	6.0	2.0
							33.00	35.00	2.0	1.8	1.0
NSRJRC11583	285567	7060594	554	-60	150	60.0	42.00	44.00	2.0	4.6	1.0
NSRJRC11584	**285564**	**7060598**	**554**	**-60**	**150**	**64.0**	**1.00**	**17.00**	**16.0**	**1.5**	**8.0**
							31.00	**48.00**	**17.0**	**3.1**	**8.5**
NSRJRC11585	**285562**	**7060603**	**554**	**-60**	**150**	**64.0**	**9.00**	**32.00**	**23.0**	**2.6**	**11.5**
							46.00	**57.00**	**11.0**	**2.6**	**5.5**
NSRJRC11586	285559	7060606	554	-60	150	64.0	1.00	2.00	1.0	1.3	0.5
							12.00	19.00	7.0	4.3	3.5
							26.00	44.00	18.0	2.5	9.0
							54.00	63.00	9.0	5.8	4.5
NSRJRC11587	285557	7060610	554	-60	150	64.0	30.00	53.00	23.0	3.3	11.5
							59.00	64.00	5.0	2.0	2.5
NSRJRC11579	285554	7060637	554	-60	150	64.0	53.00	64.00	11.0	2.5	5.5
NSRJRC11580	285551	7060641	554	-60	150	64.0	62.00	64.00	2.0	7.4	1.0
NSRJRC11581	285571	7060586	554	-60	150	40.0	3.00	6.00	3.0	6.3	1.5
							10.00	11.00	1.0	1.1	0.5
							19.00	20.00	1.0	2.0	0.5
NSRJRC11588	285554	7060616	554	-60	150	54.0	19.00	23.00	4.0	4.2	2.0
							30.00	**54.00**	**24.0**	**1.1**	**12.0**
NSRJRC11592	**285544**	**7060633**	**554**	**-60**	**150**	**64.0**	**50.00**	**64.00**	**14.0**	**1.8**	**7.0**
NSRJRC11593	285563	7060580	554	-60	150	40.0	4.00	6.00	2.0	1.1	1.0
							18.00	21.00	3.0	2.4	1.5
NSRJRC11594	**285560**	**7060585**	**554**	**-60**	**150**	**50.0**	**7.00**	**16.00**	**9.0**	**3.2**	**4.5**
							19.00	**31.00**	**12.0**	**4.9**	**6.0**
NSRJRC11595	285558	7060589	554	-60	150	60.0	0.00	2.00	2.0	1.1	1.0
							4.00	7.00	3.0	2.3	1.5
							10.00	13.00	3.0	1.2	1.5
							19.00	**42.00**	**23.0**	**2.1**	**11.5**
NSRJRC11596	285556	7060592	554	-60	150	64.0	1.00	10.00	9.0	2.3	4.5
							12.00	18.00	6.0	2.5	3.0
							24.00	25.00	1.0	7.8	0.5
							36.00	**47.00**	**11.0**	**3.2**	**5.5**
NSRJRC11597	**285552**	**7060598**	**554**	**-60**	**150**	**64.0**	**6.00**	**20.00**	**14.0**	**2.7**	**7.0**
							29.00	**52.00**	**23.0**	**1.2**	**11.5**
							54.00	**63.00**	**9.0**	**3.1**	**4.5**
NSRJRC11598	285550	7060602	554	-60	150	64.0	**7.00**	**30.00**	**23.0**	**3.8**	**11.5**
							42.00	**64.00**	**22.0**	**2.3**	**11.0**
NSRJRC11599	285547	7060607	554	-64	150	64.0	8.00	9.00	1.0	1.7	0.5
							25.00	**40.00**	**15.0**	**2.1**	**7.5**
							43.00	45.00	2.0	1.0	1.0
							59.00	64.00	5.0	2.2	2.5
NSRJRC11600	285545	7060611	554	-60	150	64.0	31.00	45.00	14.0	1.1	7.0
							47.00	49.00	2.0	2.0	1.0
NSRJRC11601	285542	7060615	554	-64	150	64.0	20.00	24.00	4.0	1.8	2.0
							34.00	**38.00**	**4.0**	**5.5**	**2.0**
							49.00	50.00	1.0	1.2	0.5
NSRJRC11602	285540	7060620	554	-60	150	64.0	48.00	51.00	3.0	1.2	1.5
NSRJRC11603	285538	7060624	554	-60	150	64.0	11.00	12.00	1.0	2.9	0.5
							45.00	51.00	6.0	1.6	3.0

RAMONE INFILL SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
NSRJRC11604	285535	7060628	554	-60	150	64.0	45.00	47.00	2.0	1.5	1.0
							53.00	55.00	2.0	3.1	1.0
							61.00	63.00	2.0	1.7	1.0
NSRJRC11625	285524	7060605	554	-60	150	64.0	55.00	59.00	4.0	1.2	2.0
							61.00	64.00	3.0	2.2	1.5
NSRJRC11642	285529	7060561	554	-60	150	40.0	24.00	26.00	2.0	2.0	1.0
NSRJRC11643	285524	7060570	554	-60	150	60.0	3.00	7.00	4.0	1.0	2.0
							9.00	**31.00**	**22.0**	**1.9**	**11.0**
NSRJRC11644	285522	7060574	554	-60	150	64.0	0.00	4.00	4.0	2.7	2.0
							12.00	16.00	4.0	2.2	2.0
							18.00	**31.00**	**13.0**	**2.0**	**6.5**
							34.00	35.00	1.0	1.4	0.5
NSRJRC11645	285519	7060577	554	-60	150	64.0	8.00	12.00	4.0	2.3	2.0
							18.00	19.00	1.0	2.4	0.5
							21.00	**36.00**	**15.0**	**2.2**	**7.5**
NSRJRC11646	285517	7060582	554	-60	150	64.0	9.00	10.00	1.0	1.1	0.5
							12.00	**17.00**	**5.0**	**4.2**	**2.5**
							19.00	**43.00**	**24.0**	**2.7**	**12.0**
NSRJRC11646	285517	7060582	554	-60	150	64.0	52.00	56.00	4.0	1.3	2.0
NSRJRC11647	285514	7060586	554	-60	150	64.0	16.00	18.00	2.0	2.5	1.0
							24.00	**40.00**	**16.0**	**2.5**	**8.0**
							42.00	**59.00**	**17.0**	**2.0**	**8.5**
							63.00	64.00	1.0	1.7	0.5
NSRJRC11648	**285511**	**7060591**	**554**	**-60**	**150**	**64.0**	**30.00**	**43.00**	**13.0**	**2.4**	**6.5**
							49.00	59.00	10.0	1.4	5.0
							61.00	64.00	3.0	1.1	1.5
NSRJRC11649	285508	7060595	554	-60	150	64.0	35.00	47.00	12.0	1.6	6.0
							50.00	51.00	1.0	1.5	0.5
							53.00	**60.00**	**7.0**	**11.7**	**3.5**
							62.00	64.00	2.0	1.8	1.0
NSRJRC11650	285505	7060600	554	-60	150	64.0	40.00	50.00	10.0	1.3	5.0
							60.00	64.00	4.0	2.6	2.0
NSRJRC11651	285502	7060604	554	-60	150	64.0	50.00	51.00	1.0	1.7	0.5
							62.00	64.00	2.0	1.5	1.0
NSRJRC11652	285522	7060551	554	-60	150	30.0	18.00	19.00	1.0	1.1	0.5
							0.00	1.00	1.0	2.1	0.5
							4.00	**9.00**	**5.0**	**15.0**	**2.5**
NSRJRC11654	**285517**	**7060560**	**554**	**-60**	**150**	**50.0**	**0.00**	**18.00**	**18.0**	**1.6**	**9.0**
							21.00	24.00	3.0	1.1	1.5
							40.00	41.00	1.0	2.9	0.5
NSRJRC11655	**285514**	**7060564**	**554**	**-60**	**150**	**60.0**	**0.00**	**27.00**	**27.0**	**4.4**	**13.5**
							30.00	32.00	2.0	1.5	1.0
NSRJRC11656	285511	7060569	554	-60	150	64.0	1.00	2.00	1.0	2.0	0.5
							4.00	6.00	2.0	1.2	1.0
							8.00	**40.00**	**32.0**	**2.9**	**16.0**
							56.00	57.00	1.0	8.7	0.5
NSRJRC11657	**285509**	**7060573**	**554**	**-60**	**150**	**64.0**	**12.00**	**44.00**	**32.0**	**1.8**	**16.0**
							63.00	64.00	1.0	1.1	0.5
NSRJRC11658	**285506**	**7060577**	**554**	**-60**	**150**	**64.0**	**13.00**	**49.00**	**36.0**	**2.3**	**18.0**
							61.00	64.00	3.0	1.2	1.5
NSRJRC11659	285504	7060581	554	-60	150	64.0	13.00	15.00	2.0	1.3	1.0
							23.00	**55.00**	**32.0**	**2.6**	**16.0**
							59.00	64.00	5.0	2.2	2.5
NSRJRC11660	**285501**	**7060586**	**554**	**-60**	**150**	**64.0**	**35.00**	**64.00**	**29.0**	**3.3**	**14.5**
NSRJRC11661	285498	7060590	554	-60	150	64.0	11.00	13.00	2.0	1.3	1.0
							36.00	37.00	1.0	1.9	0.5
							43.00	44.00	1.0	2.9	0.5
							48.00	**64.00**	**16.0**	**2.4**	**8.0**
NSRJRC11662	285496	7060594	554	-60	150	64.0	15.00	18.00	3.0	1.1	1.5
							54.00	64.00	10.0	1.4	5.0
NSRJRC11664	285511	7060551	554	-60	150	40.0	34.00	36.00	2.0	1.2	1.0
NSRJRC11665	285508	7060555	554	-60	150	50.0	0.00	3.00	3.0	5.4	1.5
							17.00	20.00	3.0	3.1	1.5
NSRJRC11666	**285506**	**7060559**	**554**	**-60**	**150**	**60.0**	**0.00**	**7.00**	**7.0**	**12.5**	**3.5**
							9.00	**30.00**	**21.0**	**4.4**	**10.5**
NSRJRC11667	**285503**	**7060564**	**554**	**-60**	**150**	**64.0**	**2.00**	**36.00**	**34.0**	**2.0**	**17.0**
							39.00	47.00	8.0	2.4	4.0
							49.00	52.00	3.0	1.4	1.5
NSRJRC11668	**285501**	**7060568**	**554**	**-60**	**150**	**64.0**	**12.00**	**29.00**	**17.0**	**3.5**	**8.5**
							31.00	47.00	16.0	1.2	8.0
							49.00	50.00	1.0	1.1	0.5
							52.00	58.00	6.0	1.6	3.0
NSRJRC11669	**285498**	**7060572**	**554**	**-60**	**150**	**64.0**	**25.00**	**49.00**	**24.0**	**4.2**	**12.0**
							51.00	53.00	2.0	1.0	1.0
							57.00	62.00	5.0	2.1	2.5
NSRJRC11670	285496	7060576	554	-60	150	64.0	14.00	15.00	1.0	3.0	0.5
							23.00	**33.00**	**10.0**	**4.3**	**5.0**
							35.00	43.00	8.0	1.3	4.0
							45.00	**56.00**	**11.0**	**4.1**	**5.5**
							58.00	60.00	2.0	1.4	1.0
							62.00	64.00	2.0	1.1	1.0
NSRJRC11671	285493	7060581	554	-60	150	64.0	30.00	36.00	6.0	1.6	3.0
							38.00	46.00	8.0	1.5	4.0
							48.00	**64.00**	**16.0**	**2.1**	**8.0**
NSRJRC11672	285491	7060585	554	-60	150	64.0	42.00	43.00	1.0	1.4	0.5
							45.00	**63.00**	**18.0**	**2.2**	**9.0**
NSRJRC11673	285488	7060589	554	-60	150	64.0	41.00	42.00	1.0	6.1	0.5
							49.00	51.00	2.0	2.0	1.0
							55.00	58.00	3.0	1.1	1.5
							60.00	61.00	1.0	1.2	0.5
NSRJRC11674	285502	7060546	554	-60	150	40.0	7.00	8.00	1.0	1.5	0.5
							25.00	26.00	1.0	1.0	0.5
NSRJRC11675	**285497**	**7060554**	**554**	**-60**	**150**	**60.0**	**4.00**	**28.00**	**24.0**	**3.1**	**12.0**
							35.00	36.00	1.0	1.6	0.5
NSRJRC11676	**285494**	**7060559**	**554**	**-60**	**150**	**64.0**	**3.00**	**26.00**	**23.0**	**11.4**	**11.5**
							28.00	34.00	6.0	1.4	3.0

RAMONE INFILL SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
							41.00	42.00	1.0	4.3	0.5
NSRJRC11684	285491	7060545	554	-60	150	55.0	0.00	1.00	1.0	3.1	0.5
							3.00	6.00	3.0	2.3	1.5
							12.00	22.00	10.0	1.5	5.0
NSRJRC11685	285488	7060549	554	-60	150	64.0	0.00	5.00	5.0	3.1	2.5
							7.00	**16.00**	**9.0**	**2.6**	**4.5**
							20.00	27.00	7.0	2.1	3.5
							34.00	36.00	2.0	3.6	1.0
NSRJRC11686	**285486**	**7060554**	**554**	**-60**	**150**	**64.0**	**4.00**	**25.00**	**21.0**	**2.9**	**10.5**
							27.00	**37.00**	**10.0**	**2.2**	**5.0**
NSRJRC11687	**285483**	**7060558**	**554**	**-60**	**150**	**64.0**	**10.00**	**40.00**	**30.0**	**3.4**	**15.0**
NSRJRC11688	285481	7060562	554	-60	150	64.0	2.00	5.00	3.0	1.4	1.5
							7.00	10.00	3.0	1.2	1.5
							16.00	**56.00**	**40.0**	**2.6**	**20.0**
NSRJRC11689	285478	7060567	554	-60	150	64.0	15.00	17.00	2.0	1.1	1.0
							20.00	26.00	6.0	1.3	3.0
							29.00	35.00	6.0	1.0	3.0
							38.00	47.00	9.0	1.5	4.5
							49.00	**64.00**	**15.0**	**3.2**	**7.5**
NSRJRC11690	285476	7060571	554	-60	150	64.0	26.00	28.00	2.0	5.8	1.0
							30.00	33.00	3.0	1.6	1.5
							35.00	38.00	3.0	1.1	1.5
							40.00	41.00	1.0	1.6	0.5
							43.00	**64.00**	**21.0**	**3.7**	**10.5**
NSRJRC11691	287433	286525	554	-60	150	64.0	8.00	9.00	1.0	1.7	0.5
							59.00	64.00	5.0	1.0	2.5
NSRJRC11692	285471	7060580	554	-60	150	64.0	29.00	30.00	1.0	1.0	0.5
							47.00	51.00	4.0	1.1	2.0
							54.00	58.00	4.0	1.9	2.0
							63.00	64.00	1.0	4.5	0.5
NSRJRC11693	285487	7060531	554	-60	150	35.0	2.00	4.00	2.0	1.3	1.0
NSRJRC11694	285485	7060536	554	-60	150	45.0	15.00	16.00	1.0	12.1	0.5
NSRJRC11699	285472	7060557	554	60	150	64.0	12.00	24.00	12.0	1.0	6.0
							32.00	**53.00**	**21.0**	**2.7**	**10.5**
							56.00	58.00	2.0	6.1	1.0
NSRJRC11700	285470	7060562	554	-60	150	64.0	4.00	7.00	3.0	1.5	1.5
							18.00	30.00	12.0	1.3	6.0
							41.00	**64.00**	**23.0**	**5.4**	**11.5**
NSRJRC11701	285467	7060566	554	-60	150	64.0	7.00	9.00	2.0	1.3	1.0
							12.00	14.00	2.0	5.3	1.0
							27.00	31.00	4.0	1.6	2.0
							36.00	37.00	1.0	1.7	0.5
							40.00	42.00	2.0	1.1	1.0
							47.00	**64.00**	**17.0**	**2.1**	**8.5**
NSRJRC11702	285465	7060570	554	-60	150	64.0	1.00	2.00	1.0	1.3	0.5
							34.00	37.00	3.0	1.4	1.5
							51.00	52.00	1.0	7.1	0.5
							54.00	56.00	2.0	1.7	1.0
NSRJRC11703	285462	7060575	554	-60	150	64.0			NSI		
NSRJRC11704	285481	7060522	554	-60	150	25.0	6.00	10.00	4.0	1.2	2.0
NSRJRC11705	285478	7060526	554	-60	150	35.0	5.00	6.00	1.0	1.4	0.5
							11.00	18.00	7.0	1.2	3.5
NSRJRC11706	285476	7060531	554	-60	150	45.0	0.00	3.00	3.0	1.5	1.5
							5.00	**9.00**	**4.0**	**6.1**	**2.0**
							19.00	20.00	1.0	3.2	0.5
							26.00	27.00	1.0	1.8	0.5
NSRJRC11707	285473	7060535	554	-60	150	55.0	1.00	11.00	10.0	1.2	5.0
							20.00	**27.00**	**7.0**	**4.6**	**3.5**
							41.00	43.00	2.0	1.1	1.0
NSRJRC11708	**285471**	**7060539**	**554**	**-60**	**150**	**64.0**	**0.00**	**16.00**	**16.0**	**1.6**	**8.0**
							18.00	30.00	12.0	1.1	6.0
							33.00	34.00	1.0	1.2	0.5
							44.00	47.00	3.0	1.9	1.5
NSRJRC11709	**285468**	**7060544**	**554**	**-60**	**150**	**64.0**	**7.00**	**36.00**	**29.0**	**1.9**	**14.5**
							41.00	42.00	1.0	2.8	0.5
							46.00	47.00	1.0	1.7	0.5
							53.00	54.00	1.0	1.3	0.5
NSRJRC11710	285466	7060548	554	-60	150	64.0	7.00	15.00	8.0	2.5	4.0
							18.00	**41.00**	**23.0**	**4.4**	**11.5**
							43.00	51.00	8.0	1.6	4.0
							59.00	60.00	1.0	1.9	0.5
							62.00	63.00	1.0	1.4	0.5
NSRJRC11711	285463	7060552	554	-60	150	64.0	15.00	17.00	2.0	1.8	1.0
							21.00	23.00	2.0	4.3	1.0
							27.00	**56.00**	**29.0**	**4.0**	**14.5**
							60.00	61.00	1.0	2.0	0.5
							63.00	64.00	1.0	1.4	0.5
NSRJRC11712	285461	7060557	554	-60	150	64.0	13.00	16.00	3.0	1.6	1.5
							20.00	26.00	6.0	1.0	3.0
							41.00	**64.00**	**23.0**	**4.5**	**11.5**
NSRJRC11713	285458	7060561	554	-60	150	64.0	24.00	25.00	1.0	2.1	0.5
							34.00	35.00	1.0	9.7	0.5
							38.00	44.00	6.0	1.2	3.0
							54.00	56.00	2.0	1.0	1.0
NSRJRC11713	285458	7060561	554	-60	150	64.0	58.00	64.00	6.0	1.2	3.0
NSRJRC11714	285456	7060565	554	-60	150	64.0	18.00	20.00	2.0	1.9	1.0
NSRJRC11715	285477	7060508	554	-60	150	10.0			NSI		
NSRJRC11716	285475	7060513	554	-60	150	15.0	10.00	14.00	4.0	1.0	2.0
NSRJRC11717	285472	7060517	554	-60	150	25.0	6.00	9.00	3.0	1.5	1.5
NSRJRC11718	**285470**	**7060521**	**554**	**-60**	**150**	**35.0**	**8.00**	**19.00**	**11.0**	**2.2**	**5.5**
NSRJRC11719	285467	7060526	554	-60	150	55.0	2.00	5.00	3.0	1.7	1.5
							11.00	25.00	14.0	1.1	7.0
NSRJRC11719	285467	7060526	554	-60	150	55.0	45.00	47.00	2.0	1.1	1.0
NSRJRC11720	285465	7060530	554	-60	150	64.0	1.00	12.00	11.0	1.2	5.5
							14.00	18.00	4.0	1.6	2.0
							20.00	28.00	8.0	2.1	4.0

RAMONE INFILL SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
							34.00	35.00	1.0	1.1	0.5
NSRJRC11721	285462	7060534	554	-60	150	64.0	14.00	23.00	9.0	1.4	4.5
							25.00	**34.00**	**9.0**	**2.3**	**4.5**
NSRJRC11722	285460	7060539	554	-60	150	64.0	0.00	7.00	7.0	1.8	3.5
							20.00	**36.00**	**16.0**	**2.5**	**8.0**
							61.00	64.00	3.0	4.1	1.5
NSRJRC11723	**285457**	**7060543**	**554**	**-60**	**150**	**64.0**	**7.00**	**13.00**	**6.0**	**3.6**	**3.0**
							16.00	17.00	1.0	1.0	0.5
							20.00	**48.00**	**28.0**	**1.8**	**14.0**
							56.00	57.00	1.0	1.9	0.5
NSRJRC11724	285455	7060547	554	-60	150	64.0	11.00	13.00	2.0	1.4	1.0
							22.00	24.00	2.0	1.5	1.0
							27.00	33.00	6.0	2.4	3.0
							35.00	**60.00**	**25.0**	**2.2**	**12.5**
							62.00	64.00	2.0	1.7	1.0
NSRJRC11725	285452	7060552	554	-60	150	64.0	32.00	33.00	1.0	1.3	0.5
							35.00	36.00	1.0	1.4	0.5
							38.00	48.00	10.0	1.3	5.0
							51.00	**56.00**	**5.0**	**4.6**	**2.5**
							59.00	62.00	3.0	1.8	1.5
NSRJRC11726	285450	7060556	554	-60	150	64.0	22.00	24.00	2.0	1.4	1.0
							31.00	32.00	1.0	1.1	0.5
							55.00	64.00	9.0	2.1	4.5
NSRJRC11727	**285447**	**7060560**	**554**	**-60**	**150**	**64.0**	**28.00**	**35.00**	**7.0**	**3.1**	**3.5**
							48.00	53.00	5.0	1.2	2.5
							61.00	64.00	3.0	1.4	1.5
NSRJRC11729	285466	7060508	554	-60	150	15.0	6.00	9.00	3.0	1.8	1.5
NSRJRC11730	285464	7060512	554	-60	150	25.0	10.00	12.00	2.0	1.6	1.0
NSRJRC11731	**285461**	**7060516**	**554**	**-60**	**150**	**35.0**	**2.00**	**17.00**	**15.0**	**2.7**	**7.5**
NSRJRC11731	285461	7060516	554	-60	150	35.0	25.00	26.00	1.0	4.6	0.5
NSRJRC11732	**285459**	**7060521**	**554**	**-60**	**150**	**60.0**	**9.00**	**26.00**	**17.0**	**2.7**	**8.5**
NSRJRC11733	**285451**	**7060534**	**554**	**-60**	**150**	**64.0**	**20.00**	**45.00**	**25.0**	**2.4**	**12.5**
							49.00	52.00	3.0	1.4	1.5
							63.00	64.00	1.0	1.0	0.5
NSRJRC11734	285449	7060538	554	-60	150	64.0	23.00	24.00	1.0	2.5	0.5
							29.00	**61.00**	**32.0**	**2.1**	**16.0**
							63.00	64.00	1.0	1.6	0.5
NSRJRC11735	285446	7060542	554	-60	150	64.0	34.00	36.00	2.0	1.8	1.0
							41.00	**64.00**	**23.0**	**2.5**	**11.5**
NSRJRC11736	285441	7060551	554	-60	150	64.0	21.00	24.00	3.0	2.5	1.5
							38.00	39.00	1.0	4.9	0.5
							45.00	47.00	2.0	2.9	1.0
							50.00	55.00	5.0	1.1	2.5
NSRJRC11736	285441	7060551	554	-60	150	64.0	61.00	64.00	3.0	1.2	1.5
NSRJRC11737	285462	7060494	554	-60	150	10.0			NSI		
NSRJRC11738	285460	7060498	554	-60	150	20.0	4.00	5.00	1.0	1.1	0.5
NSRJRC11739	285457	7060503	554	-60	150	30.0	14.00	15.00	1.0	1.3	0.5
NSRJRC11740	285455	7060507	554	-60	150	40.0	0.00	2.00	2.0	1.7	1.0
							5.00	9.00	4.0	1.9	2.0
							21.00	22.00	1.0	1.0	0.5
NSRJRC11741	**285452**	**7060511**	**554**	**-60**	**150**	**50.0**	**2.00**	**15.00**	**13.0**	**7.1**	**6.5**
NSRJRC11742	285450	7060516	554	-60	150	60.0	8.00	10.00	2.0	4.0	1.0
							12.00	**25.00**	**13.0**	**2.4**	**6.5**
							30.00	31.00	1.0	1.2	0.5
NSRJRC11743	285447	7060520	554	-60	150	64.0	6.00	8.00	2.0	2.0	1.0
							11.00	**27.00**	**16.0**	**1.7**	**8.0**
							36.00	39.00	3.0	2.5	1.5
							42.00	45.00	3.0	1.1	1.5
							59.00	64.00	5.0	1.9	2.5

Table 8 – Ramone Exploration Significant Intersections

RAMONE EXPLORATION SIGNIFICANT INTERSECTIONS											
Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (degrees, MGA	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
REGIONAL EXPLORATION											
NSRJRC11380	285201	7060443	551	-60	10	80.0	22.00	23.00	1.0	2.0	unknown
NSRJRC11381	285198	7060420	551	-60	10	110.0	55.00	60.00	5.0	1.0	unknown
NSRJRC11382	**285250**	**7060434**	**551**	**-60**	**10**	**80.0**	**28.00**	**34.00**	**6.0**	**4.2**	unknown
					(incl.)		29.00	30.00	1.0	9.7	unknown
							73.00	74.00	1.0	1.2	unknown
NSRJRC11383	**285246**	**7060410**	**551**	**-60**	**10**	**110.0**	**65.00**	**70.00**	**5.0**	**14.2**	unknown
					(incl.)		67.00	68.00	1.0	65.6	unknown
NSRJRC11385	285471	7060602	551	-60	10	120.0	47.00	49.00	2.0	1.2	unknown
NSRJRC11386	285430	7060632	551	-60	10	90.0	13.00	14.00	1.0	1.2	unknown
NSRJRC11390	285891	7060977	551	-60	330	200.0	43.00	45.00	2.0	1.2	unknown
							50.00	54.00	4.0	2.0	unknown
NSRJRC11391	285904	7060956	551	-60	330	132.0	78.00	85.00	7.0	1.7	unknown
NSRJRC11392	285912	7060940	551	-60	330	150.0	87.00	88.00	1.0	1.0	unknown
NSRJRC11393	285923	7060914	551	-60	330	200.0	159.00	160.00	1.0	1.4	unknown
							194.00	196.00	2.0	2.2	unknown
NSRJRC11394	285905	7061043	551	-60	330	120.0	25.00	26.00	1.0	1.3	unknown
							34.00	36.00	2.0	1.2	unknown
							60.00	61.00	1.0	1.0	unknown
NSRJRC11395	285916	7061015	151	-60	330	150.0	10.00	12.00	2.0	6.6	unknown
							45.00	47.00	2.0	1.4	unknown
							49.00	50.00	1.0	1.4	unknown
							65.00	67.00	2.0	1.3	unknown
							100.00	101.00	1.0	2.2	unknown
NSRJRC11396	285936	7061000	551	-60	330	200.0	34.00	42.00	8.0	1.5	unknown
NSRJRC11397	**285961**	**7060955**	**551**	**-60**	**330**	**150.0**	**116.00**	**127.00**	**11.0**	**4.7**	unknown
					(incl.)		117.00	118.00	1.0	13.8	unknown
NSRJRC11398	285968	7060930	551	-60	330	192.0	97.00	101.00	4.0	1.0	unknown

							131.00	132.00	1.0	1.3	unknown
							136.00	**151.00**	**15.0**	**2.2**	unknown
							155.00	156.00	1.0	1.2	unknown
							162.00	163.00	1.0	1.5	unknown
							180.00	182.00	2.0	1.0	unknown
NSRJRC11399	285941	7060977	551	-60	330	120.0	64.00	72.00	8.0	1.4	unknown
							82.00	83.00	1.0	1.6	unknown
							97.00	99.00	2.0	1.3	unknown
NSRJRC11400	285955	7061071	551	-60	330	135.0	30.00	33.00	3.0	1.7	unknown
							45.00	46.00	1.0	1.0	unknown
							78.00	79.00	1.0	2.4	unknown
NSRJRC11401	285963	7061049	151	-60	330	150.0	138.00	140.00	2.0	1.8	unknown
NSRJRC11402	285976	7061026	551	-60	330	200.0	104.00	105.00	1.0	2.8	unknown
NSRJRC11403	286990	7061004	551	-60	330	120.0	79.00	89.00	10.0	1.7	unknown
NSRJRC11404	285998	7060986	551	-60	330	150.0	91.00	95.00	4.0	1.2	unknown
NSRJRC11405	286014	7060961	551	-60	330	200.0	115.00	116.00	1.0	1.4	unknown
NSRJRC11406	285185	7061402	551	-60	10	120.0	70.00	72.00	2.0	3.8	unknown
							77.00	78.00	1.0	1.4	unknown
							80.00	81.00	1.0	1.1	unknown
							83.00	84.00	1.0	1.1	unknown
NSRJRC11407	285182	7061383	551	-60	10	150.0	38.00	39.00	1.0	2.0	unknown
							69.00	72.00	3.0	2.2	unknown
							93.00	94.00	1.0	1.4	unknown
							113.00	119.00	6.0	1.3	unknown
NSRJRC11408	285178	7061358	551	-60	10	200.0	53.00	54.00	1.0	3.3	unknown
							101.00	102.00	1.0	1.7	unknown
							104.00	106.00	2.0	3.2	unknown
							144.00	145.00	1.0	1.0	unknown
NSRJRC11409	285169	7061332	551	-60	10	150.0	16.00	19.00	3.0	1.1	unknown
							26.00	27.00	1.0	1.6	unknown
							128.00	130.00	2.0	1.6	unknown
NSRJRC11410	285167	7061312	551	-60	10	150.0	44.00	47.00	3.0	1.4	unknown
							62.00	64.00	2.0	2.6	unknown
							84.00	85.00	1.0	2.4	unknown
RAMONE DEPTH EXTENSIONS											
NSRJRD10486	285469	7060752	554	-45	148	396.2	177.34	178.85	1.5	2.5	1.1
							193.00	196.00	3.0	3.0	2.1
							206.30	212.25	6.0	2.7	4.2
							213.50	219.00	5.5	2.4	3.9
							235.70	237.70	2.0	5.2	1.4
							239.40	250.00	10.6	1.5	7.4
							293.60	294.00	0.4	13.5	0.3
							295.40	**297.00**	**1.6**	**22.4**	**1.1**
							306.00	306.50	0.5	27.9	0.4
							363.00	**365.00**	**2.0**	**20.4**	**1.4**
							372.41	377.60	5.2	1.1	3.6
NSRJRD10487	**285469**	**7060752**	**554**	**-56**	**148**	**500.3**	**244.90**	**255.40**	**10.5**	**2.8**	**6.3**
							273.00	275.30	2.3	10.2	1.4
							283.00	284.37	1.4	1.3	0.8
							287.00	288.00	1.0	2.7	0.6
							291.00	292.00	1.0	1.9	0.6
NSRJRD10488	**285400**	**7060712**	**554**	**-45**	**149**	**308.7**	**246.00**	**272.15**	**26.2**	**2.3**	**18.3**
NSRJRD10489	**285400**	**7060712**	**554**	**-56**	**147**	**490.0**	**334.00**	**351.60**	**17.6**	**4.8**	**10.6**

Table 9 -Tanami Significant Intersections

TANAMI SIGNIFICANT INTERSECTIONS											
Drill Hole #	**Easting (MGA grid)**	**Northing (MGA grid)**	**Collar RL (MGA)**	**Dip (degrees)**	**Azimuth (degrees, MGA grid)**	**Hole Depth (m)**	**Downhole From (m)**	**Downhole To (m)**	**Downhole Intersection (m)**	**Au (gpt) uncut**	**Est True Thickness (m)**
HURRICANE											
NHRC00001	574868	7792186	438	-60	320	120.0	0.0	1.0	1.0	1.3	0.7
NHRC00002	574857	7792198	439	-60	320	120.0	49.0	54.0	5.0	0.7	3.3
NHRC00003	**574780**	**7792216**	**438**	**-60**	**320**	**168.0**	**17.0**	**34.0**	**17.0**	**6.0**	11.1
							73.0	79.0	6.0	1.2	3.9
							82.0	86.0	4.0	2.1	2.6
							140.0	**143.0**	**3.0**	**20.5**	2.0
							147.0	**159.0**	**12.0**	**4.6**	7.8
							162.0	163.0	1.0	1.3	0.7
NHRC00004	574797	7792168	438	-60	317	200.0	121.0	123.0	2.0	1.0	1.3
							175.0	182.0	7.0	2.0	4.6
NHRC00005	574752	7792209	439	-60	310	130.0	0.0	1.0	1.0	0.6	0.7
							7.0	8.0	1.0	0.6	0.7
							76.0	77.0	1.0	0.7	0.7
							86.0	87.0	1.0	0.9	0.7
							0.0	1.0	1.0	0.6	0.7
NHRC00006	574733	7792230	438	-60	312	90.0	0.0	1.0	1.0	1.0	0.7
NHRC00007	**574766**	**7792172**	**438**	**-60**	**312**	**156.0**	0.0	1.0	1.0	0.7	0.7
							53.0	58.0	5.0	1.0	3.3
							81.0	82.0	1.0	2.6	0.7
							136.0	**155.0**	**19.0**	**4.6**	12.4
NHRC00008	574745	7792188	439	-60	320	132.0	92.0	94.0	2.0	2.1	1.3
NHRC00009	**574761**	**7792136**	**438**	**-60**	**320**	**174.0**	1.0	2.0	1.0	0.9	0.7
							81.0	90.0	9.0	2.6	5.9
							98.0	99.0	1.0	1.0	0.7
							102.0	106.0	4.0	1.3	2.6
							140.0	146.0	6.0	1.2	3.9
							150.0	**164.0**	**14.0**	**3.2**	9.1
							168.0	169.0	1.0	2.8	0.7
NHRC00010	574741	7792146	438	-60	315	132.0	10.0	23.0	13.0	1.6	8.5
							68.0	71.0	3.0	2.1	2.0
NHRC00011	574723	7792158	439	-60	310	120.0	0.0	1.0	1.0	0.9	0.7
							53.0	54.0	1.0	1.0	0.7
							96.0	97.0	1.0	0.8	0.7
NHRC00012	574788	7792094	436	-60	317	120.0	0.0	1.0	1.0	2.8	0.7
							75.0	83.0	8.0	0.8	5.2
NHRC00013	574754	7792082	437	-60	317	160.0	0.0	2.0	2.0	8.5	1.3
							43.0	47.0	4.0	0.7	2.6
							52.0	57.0	5.0	1.8	3.3

TANAMI SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (MGA grid)	Northing (MGA grid)	Collar RL (MGA)	Dip (degrees)	Azimuth (degrees, MGA grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
HURRICANE											
							151.0	154.0	3.0	0.4	2.0
							157.0	159.0	2.0	1.6	1.3
NHRC00014	574735	7792113	437	-60	310	132.0	0.0	1.0	1.0	3.5	0.7
							6.0	7.0	1.0	0.7	0.7
							39.0	40.0	1.0	1.0	0.7
							73.0	75.0	2.0	4.2	1.3
							103.0	109.0	6.0	1.7	3.9
							114.0	118.0	4.0	0.6	2.6
							0.0	1.0	1.0	3.5	0.7
							39.0	40.0	1.0	1.0	0.7
							73.0	75.0	2.0	4.2	1.3
							103.0	109.0	6.0	1.7	3.9
							114.0	118.0	4.0	0.6	2.6
NHRC00015	**574776**	**7792044**	**434**	**-60**	**312**	**120.0**	0.0	1.0	1.0	8.2	0.7
							51.0	52.0	1.0	1.3	0.7
							60.0	64.0	4.0	0.5	2.6
							92.0	**107.0**	**15.0**	**2.9**	9.8
NHRC00016	**574738**	**7792051**	**437**	**-60**	**317**	**162.0**	**0.0**	**1.0**	**1.0**	**42.1**	0.7
							15.0	20.0	5.0	1.3	3.3
							69.0	76.0	7.0	2.3	4.6
							155.0	158.0	3.0	2.2	2.0
NHRC00017	574710	7792062	436	-60	315	126.0	0.0	1.0	1.0	0.5	0.7
							69.0	70.0	1.0	1.0	0.7
							85.0	88.0	3.0	0.6	2.0
							116.0	119.0	3.0	1.4	2.0
NHRC00018	574743	7791983	4433	-60	315	210.0	0.0	1.0	1.0	0.6	0.7
							149.0	152.0	3.0	2.1	2.0
NHRC00019	574716	7792000	435	-60	310	156.0	0.0	1.0	1.0	3.4	0.7
			435	-60	310	156.0	9.0	11.0	2.0	1.2	1.3
			435	-60	310	156.0	34.0	36.0	2.0	0.7	1.3
			435	-60	310	156.0	90.0	93.0	3.0	1.4	2.0
			435	-60	310	156.0	100.0	103.0	3.0	3.6	2.0
			435	-60	310	156.0	0.0	1.0	1.0	3.4	0.7
			435	-60	310	156.0	9.0	11.0	2.0	1.2	1.3
			435	-60	310	156.0	34.0	36.0	2.0	0.7	1.3
			435	-60	310	156.0	90.0	93.0	3.0	1.4	2.0
			435	-60	310	156.0	100.0	103.0	3.0	3.6	2.0
NHRC00020	574683	7792026	437	-60	310	120.0	0.0	1.0	1.0	1.0	0.7
			437	-60	310	120.0	50.0	58.0	8.0	2.4	5.2
			437	-60	310	120.0	91.0	92.0	1.0	0.8	0.7
			437	-60	310	120.0	115.0	116.0	1.0	1.2	0.7
NHRC00021	574672	7791989	435	-60	315	120.0	0.0	1.0	1.0	1.3	0.7
							42.0	47.0	5.0	0.6	3.3
							72.0	75.0	3.0	1.8	2.0
							87.0	89.0	2.0	1.4	1.3
NHRC00022	574662	7791965	436	-60	317	132.0	0.0	2.0	2.0	1.3	1.3
							87.0	88.0	1.0	1.6	0.7
							125.0	126.0	1.0	1.5	0.7
NHRC00023	574600	7792005	438	-60	310	96.0	0.0	1.0	1.0	0.8	0.7
						96.0	52.0	53.0	1.0	0.5	0.7
NHDD001	**574801**	**7792135**	**436**	**-55**	**315**	**304.0**	19.2	20.2	1.0	0.5	0.6
							35.0	36.0	1.0	0.6	0.7
							68.0	69.0	1.0	0.6	0.7
							124.0	125.0	1.0	1.1	0.7
							130.5	131.3	0.8	0.8	0.5
							132.0	132.7	0.7	0.6	0.5
							133.8	134.1	0.4	0.8	0.2
							140.3	141.6	1.3	2.3	0.8
							162.2	163.0	0.8	1.5	0.5
							166.0	173.0	7.0	0.8	4.6
							177.9	**186.4**	**8.5**	**6.6**	5.5
							191.0	192.0	1.0	1.4	0.7
							210.7	211.0	0.3	1.1	0.2
							214.4	215.1	0.7	2.5	0.5
							218.8	219.9	1.2	1.0	0.8
							222.0	223.0	1.0	0.8	0.7
							225.5	226.4	0.9	0.6	0.6
							283.1	283.7	0.6	0.8	0.4
							295.6	295.6	1.0	4.6	0.7
JIM'S											
JDD001	**564672**	**7770984**	**416**	**-60**	**124**	**356.1**	58.0	59.0	1.0	1.1	0.7
							121.0	122.0	1.0	0.7	0.7
							133.0	134.6	1.6	1.4	1.0
							154.0	155.0	1.0	0.6	0.7
							158.0	159.0	1.0	4.2	0.7
							162.5	163.0	0.5	1.1	0.3
							170.0	171.5	1.5	0.7	1.0
							184.5	191.7	7.2	2.3	4.7
							201.0	203.0	2.0	0.8	1.3
							213.0	215.0	2.0	0.7	1.3
							218.0	219.0	1.0	1.1	0.7
							224.0	**250.0**	**26.0**	**3.9**	16.9
							285.7	289.1	3.4	0.4	2.2
							291.9	293.0	1.1	0.6	0.7
							298.0	304.0	6.0	1.7	3.9
							307.0	308.0	1.0	0.6	0.7
JDD002	**564672**	**7770984**	**416**	**-73**	**128**	**437.9**	212.0	213.0	1.0	0.8	0.7
							217.7	221.0	3.3	0.6	2.1
							231.0	237.0	6.0	1.9	3.9
							256.0	258.0	2.0	0.8	1.3
							291.0	293.0	2.0	0.8	1.3
							313.0	313.9	0.9	0.7	0.6
							343.0	344.1	1.1	0.7	0.7
							401.0	**411.0**	**10.0**	**5.7**	6.5

TANAMI SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (MGA grid)	Northing (MGA grid)	Collar RL (MGA)	Dip (degrees)	Azimuth (degrees, MGA grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
HURRICANE											
							413.2	419.0	5.8	0.8	3.8
							423.0	424.0	1.0	1.1	0.7
							431.0	432.0	1.0	5.2	0.7
JDD003	**564726**	**7771083**	**417**	**-59**	**131**	**363.3**	50.0	51.0	1.0	0.6	0.7
							126.0	127.0	1.0	1.4	0.7
							183.0	185.0	2.0	0.8	1.3
							192.0	193.0	1.0	0.6	0.7
							204.0	206.0	2.0	1.1	1.3
							219.1	**227.0**	**7.9**	**3.9**	5.1
							234.0	235.0	1.0	1.8	0.7
							265.7	267.0	1.3	0.8	0.9
JDD004	**564725**	**7771083**	**417**	**-71**	**131**	**438.1**	80.0	81.0	1.0	0.6	0.7
							113.9	115.0	1.1	0.6	0.7
							121.6	122.0	0.4	0.7	0.2
							205.0	208.0	3.0	2.0	2.0
							221.8	226.0	4.2	1.2	2.7
							229.0	230.0	1.0	1.4	0.7
							233.0	**253.5**	**20.5**	**2.2**	13.3
							253.7	254.1	0.4	0.6	0.2
							258.6	268.8	10.3	1.1	6.7
							272.0	276.0	4.0	1.7	2.6
							280.0	283.1	3.1	0.4	2.0
							285.3	286.8	1.5	1.2	1.0
							386.0	389.0	3.0	1.3	2.0
							429.4	429.8	0.4	1.0	0.3

APPENDIX B – JORC CODE 2012 – TABLE 1 REPORTS

Kanowna Belle (including Velvet) - Exploration Drill Results - December 2018
JORC Code, 2012 Edition – Table 1
Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	The sampling database for the Kanowna Belle and Velvet area has been compiled from information collected by several different companies since initial discovery in 1989. All information collected prior to involvement by Northern Star Resources in 2014 is hereafter referred to as historical data. Only historical data that is deemed as having acceptable and traceable location and assay information has been included in the Mineral Resource estimation datasets for both Kanowna Belle and Velvet.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	For DD samples metre delineation is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geologist during core mark-up prior to logging to prevent incorrect logging and sampling errors. Sample intervals are then marked on the core by a geologist, to honour geological boundaries. Sample interval lengths vary from 0.3m and 1.3m (NQ). DD core was orientated, measured and then sampled by cutting the core in half longitudinally using an "Almonte" diamond saw. Cutting was along orientation lines. The same half of the core is always selected for each sample interval, placed in numbered calico bags and submitted to the laboratory for analysis. The other half of the core is left in the core tray which was stamped for identification, stored and catalogued. Routine 'field duplicates' to assess sample representivity are not performed on diamond core as these are not considered to be true field duplicates.
	Aspects of the determination of mineralization that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralization types (e.g. submarine nodules) may warrant disclosure of detailed information.	Current sample preparation and assay procedures employed by Northern Star Resources are considered as following industry standard practice. All assay determinations are conducted by internationally recognised laboratories. The primary laboratory, Bureau Veritas, meets ISO 9001:2000. For preparation samples are oven dried until a constant mass is achieved. All samples are then processed through an Essa Jaw Crusher or a Boyd Crusher to 90% < 3 mm. The crushed sample is then pulverised for 4 minutes in an LM5 pulveriser for a product of 90% passing < 75 µm. Approximately 250 - 300g of the pulp is retained and a 40g catch weight for fire assay is extracted from the pulp packet. Samples are tested for sulphides and flux adjusted, flux is added at a ratio of 1:4. Samples are fired, hammered and cupelled. Prills placed in tubes, dissolved on hotplates and analysed using AA finish with over range dilutions. Sample preparation for Sulphur determination follows the same process as for Gold, with assaying taking place using the LECO method.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	DD core is mostly NQ diameter diameter core. Where possible diamond core was orientated using a spear, Ballmark™, Ezimark™, or ACE multi electronic tool.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	For DD, all recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geologist. Any issues are communicated back to the drilling contractor. Recovery is generally very high, in excess of 95%, and there have been no significant sample recovery problems. Historic DD core stored on site shows excellent recovery.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	For DD, drilling contractors adjust the rate of drilling and method if recovery issues arise. Minor loss occurs when drilling through fault zones such as the Fitzroy Fault. Areas of potential lower recovery are generally known before hand and controlled drilling techniques employed to maximise recovery.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	No specific study has been carried out on recovery and grade. As recoveries are generally very high (95%+) it is assumed that the potential for bias due to variable sample recovery is low.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	All DD core was logged by geologists with lithology, mineralisation, structure, alteration, veining and specific gravity were recorded. Quantitative measures such as structural measurements, intensity of alteration, percentage of mineralisation, thickness of veins and veins per metre were also recorded. Geotechnical measurements on DD

Criteria	JORC Code explanation	Commentary
		core include RQD, Recovery, and Fracture Frequency. For selected holes joint sets, infill, infill thickness and roughness were also geotechnically measured. All mineralised intersections are logged and sampled.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Geology logging is qualitative in nature with visual estimates made of mineralization percentages for core. Structural and geotechnical logging is quantitative in nature. All core is photographed wet as standard practice. Historically some core may have also been photographed dry.
	The total length and percentage of the relevant intersections logged.	100% of the drill core is logged.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	DD core is sampled by sawn half-core on intervals controlled by geological domaining represented by mineralisation, alteration and lithology. A selected number of grade control holes were full cored. Mineralised intersections are sampled with a maximum and minimum length of 1.3m and 0.3m, respecting lithological or alteration contacts. The down hole depth of all sample interval extents are recorded.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	No non-core results reported.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	Sample preparation follows industry standard practice. Samples are oven dried until a constant mass is achieved. All samples are then processed through an Essa Jaw Crusher or a Boyd Crusher to 90% < 3 mm. The crushed sample is then pulverised for 4 minutes in an LM5 pulveriser for a product of 90% passing < 75 µm. Approximately 250 - 300 g of the pulp is retained and a 40g charge prepared.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Coarse grind checks at the crushing stage (3mm) are carried out at a ratio of 1:25 samples with 90% passing required. Pulp grind checks at the pulverising stage (75 µm) are carried out at a ratio of 1:25 samples with 90% passing required. Laboratory duplicate samples are taken for coarse crush (3mm) and pulverising (75 µm) stages at a ratio of 1:25 samples. Repeat assays are carried out at a ratio of 1:10 on prepared pulp samples.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Quarter core sampling of diamond core is occasionally undertaken for check assays, however routine field duplicates are not performed on diamond core as these are not considered to be true field duplicates.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Grind checks are performed at both the crushing stage (3mm) and pulverising stage (75µm) requiring 90% of material to pass through the relevant size. No specific study has been carried out to determine optimum sub-sample size fractions. These material sizes are assumed to be acceptable for the mineralization style and material grain size present.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	Fire assay analysis is undertaken and this is considered to be a total assay method. Monthly QAQC reports are prepared to check for any bias or trends with conclusions discussed with the laboratory management. Holes that do not pass QAQC are not used for Mineral Resource estimation.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical tools were used to determine any element concentrations.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Sampling and assaying QAQC procedures include: - Periodical resubmission of samples to primary and secondary laboratories - Submittal of independent certified reference material - Sieve testing to check grind size - Sample recovery checks. - Unannounced laboratory inspections Standard control samples and blanks purchased from certified commercial suppliers are inserted at a ratio of 1:20. The standard control samples are changed on a 3-month rotation. The results are reviewed on a per batch basis and batches of samples are re-analysed if the result is greater than three standard deviations from the expected result. Any result outside of two standard deviations is flagged for investigation by a geologist and may also be re-assayed.

Criteria	JORC Code explanation	Commentary
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	All significant and anomalous intersections are verified by a Senior Geologist during the drill hole validation process.
	The use of twinned holes.	No twinned holes were drilled for this data set.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	All data are stored and validated within the site Acquire database. Data import into the database is controlled by documented standard operating procedures, and by a set of validation tools included in Acquire import routines. Hard copies and electronic copies of all primary location, logging and sample results data are filed for each hole.
	Discuss any adjustment to assay data.	Assay results are received in csv format and loaded directly into the database by the supervising geologist who then checks that the results have inserted correctly. Holes that cannot be accurately validated or do not meet the requirements of Kanowna QAQC are excluded prior to Mineral Resource estimation.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	All drill hole collar positions were surveyed. All recent DD holes were surveyed down hole by various methods including single shot down hole camera, EMS (Electronic Multi Shot) method or in-rod gyroscopic survey tools. Holes are typically surveyed at 15m and 30m intervals down hole thereafter. Since the 1st of June 2015, a true north seeking gyroscopic tool has been used to line up the rig and record a zero-meter survey. Any poor surveys are re-surveyed, and, in some cases, holes have been gyroscope surveyed by ABIMS for non-magnetic affected survey. If survey data was missing or quality was suspect and not replaced by more recent drilling, affected data was not used in estimation.
	Specification of the grid system used.	A local grid system (KBMINE grid) is used. It is rotated anticlockwise 28.43 degrees to the MGA94 grid.
	Quality and adequacy of topographic control.	Drill hole collars are located by the underground mine surveyors using a Laser system respective to the local mine grid and to the overall property in UTM or Australian grid coordinates. Topographic control is not relevant to the underground mine.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Drill hole spacing is nominally 60m x 60m down to 20m x 20m in the main zones of mineralization at the Kanowna Belle and Velvet deposits. Secondary mineralised structures in the hanging wall and footwall of Kanowna Belle are typically narrower and less consistent so have a nominal drill spacing of 15m x 15m.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The data spacings in the Mineralised domains at Kanowna Belle and Velvet are considered sufficient to support the definition of Mineral Resources and Reserves.
	Whether sample compositing has been applied.	The datasets were composited to 1 m intervals prior to grade estimation. This aligns with the most common sample length taken.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	Most data is drilled perpendicular to the interpreted strike of the Kanowna Belle and Velvet Mineralised zones. Due to the complex overlapping nature of the mineralised zones actual intersections may be slightly oblique to the intended right-angle intersections intended.
	If the relationship between the drilling orientation and the orientation of key mineralized structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	Holes with orientations that are considered likely to introduce sampling bias are flagged during drill hole validation and are excluded from the Mineral Resource estimation datasets.
Sample security	The measures taken to ensure sample security.	All core is kept within the site perimeter fence on the Mining Lease M27/103. Samples are dispatched and/or collected by an offsite delivery service on a regular basis. Each sample batch is accompanied with a: ▪ Job number ▪ Number of Samples ▪ Sample Numbers (including standards and duplicates) ▪ Required analytical methods ▪ A job priority rating A Chain of Custody is demonstrated by both Company and Bureau Veritas in the delivery and receipt of sample materials. Any damage to or loss of samples within each batch (e.g. total loss, spillage or obvious contamination), is reported to the Company in the form of a list of samples affected and detailing the nature of the problem(s).

Criteria	JORC Code explanation	Commentary
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	The last external audit was conducted in 2009 with the conclusion that industry best practice was being followed. Standards and procedures have remained largely unchanged since this time. A review of sampling techniques, assay results and data usage was conducted internally by the Companies' Principal Resource Geologist during 2015 with no material issues found.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Kanowna Belle mine and associated infrastructure is located on Mining Leases M27/92 and M27/103. Mining lease M27/92 (972.65 ha) was granted on March 14, 1988 and M27/103 (944.25 ha) was granted on January 12, 1989. Both leases were granted for periods of 21 years after which they can be renewed for a further 21 years. The Mining Leases and most of the surrounding tenement holdings are 100% owned by Northern Star (Kanowna) Pty Limited, a wholly owned subsidiary of Northern Star Resources Limited. The mining tenements are either located on vacant crown land or on pastoral leases. The leases containing the deposit are pre-1994 leases so are not subject to Native Title claims.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	No known impediments exist and the tenements are in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	Kanowna was discovered in 1989 by Delta Gold, open pit mining commenced between 1993 and 1998 resulting in a 220m deep pit. Underground operation began in 1998. In 2002, Delta Gold Limited and Goldfields Limited merged to form Aurion Gold Limited. Placer Dome Inc. (Placer Dome) subsequently acquired Aurion Gold Limited. In 2006 Barrick Gold Corporation acquired Placer Dome and in 2014 Northern Star acquired the operation from Barrick. Exploration drilling is ongoing from underground to extend the known mineral resources.
Geology	Deposit type, geological setting and style of mineralisation.	Kanowna Belle is located within the Kalgoorlie Terrane, one of several elongate, broadly NNW-SSE striking structural-stratigraphic late Archaean greenstone terranes of the Eastern Goldfields of Western Australia. The Kanowna Belle gold mine is located close to the centre of the NNW-SSE trending, greenstone-dominated Boorara Domain, the eastern most subdivision of the Kalgoorlie Terrane. The Kanowna Belle deposit can be categorised as a refractory, Archean lode-gold type deposit. The orebody is comprised of several ore shoots, including the large Lowes Shoot, and several smaller lodes including Troy, Hilder, Hangingwall and Footwall shoots controlled by sets of structures of various orientations oblique to Lowes. Lowes contains some 80% of known gold mineralization and strikes ENE, dips steeply SSW and plunges steeply SW. Lowes shoot has a strike length of 500m, width of 5m to 50m and down-plunge extent greater than 1,250m. The overall steep SE plunge is interpreted to reflect the intersection of D1 (ENE) and D2 (NW) structures. Kanowna Belle is one of the only known refractory pyritic orebodies in the Yilgarn Craton. Gold in the Kanowna Belle deposit occurs mostly as fine-grained (<10 µm) inclusions in pyrite or as very fine-grained gold located in arsenic-rich growth zones in pyrite. Typical ore assemblages contain 0.5% S to 1.5% S and 40 ppm As. The Kanowna Belle deposit is hosted by sedimentary volcanoclastic and conglomeratic rocks which are separated into hangingwall and footwall sequences by a major, steeply SSE dipping zone of structural disruption. This structure represents the product of at least three distinct stages of deformation, comprising the Fitzroy Mylonite, the Fitzroy Shear Zone and the Fitzroy Fault, which have produced clear structural overprinting relations. Importantly, this structure has localised emplacement of the Kanowna Belle porphyry which hosts at least 70% of known mineralisation. Localisation of high grade mineralization and most intense alteration around the composite structure emphasises its importance for acting as the major plumbing system for fluids. Formation of the Fitzroy Mylonite and Fitzroy Shear Zone are interpreted to have occurred during regional south-to-north D1 thrusting. A switch in far-field stress axes to the approximately ENE-WSW D2 orientation caused reactivation of the Fitzroy Shear Zone, resulting in sigmoidal folding of pre-existing structures and formation of a shallow lineation associated with sinistral transcurrent shearing. The Kanowna Belle porphyry cross-cuts fabrics associated with the D1 Fitzroy Mylonite and Fitzroy Shear Zone and is in turn overprinted by S2.

Criteria	JORC Code explanation	Commentary
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: ▪ easting and northing of the drill hole collar ▪ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar ▪ dip and azimuth of the hole ▪ down hole length and interception depth ▪ hole length.	Summary information is presented in the accompanying table.
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	All results for the period/area are reported.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	All reported assay results have been length weighted to provide an intersection width. A maximum of 2m of barren material between mineralised samples has been permitted in the calculation of these widths.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	No assay results have been top-cut for the purpose of this report. A lower cut-off of 1gpt has been used to identify significant results, although lower results are included where a known ore zone has been intercepted and the entire intercept is low grade.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalent values have been used for the reporting of these exploration results.
Relationship between mineralization widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results.	True widths have been calculated for intersections of the known ore zones, based on existing knowledge of the nature of these structures.
	If the geometry of the mineralization with respect to the drill hole angle is known, its nature should be reported.	Both the downhole width and true width have been clearly specified when used.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	Where mineralization orientations are unknown, downhole lengths are reported.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Appropriate plans and section have been included in this report.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and 'From' and 'To' depths.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	Nil.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	The down dip and hanging wall extensions of the Kanowna Belle and Velvet will be drill tested from various underground drilling platforms.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Included in the release.

K2 Drake – Moonbeam Deposit - December 2018
JORC Code, 2012 Edition – Table 1 Report
Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Sampling was completed using Diamond Drilling (DD). RC drilling was used to drill pre-collars for many of the holes with diamond tails.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Diamond core was transferred to core trays for logging and sampling. Half core samples were nominated by the geologist from both NQ2 and HQ diamond core with a minimum sample width of either 20cm (HQ) or 30cm (NQ2).
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	Samples were taken to Genalysis Kalgoorlie for preparation by drying, crushing to <3mm, and pulverising the entire sample to <75µm. 300g Pulps splits were then dispatched to Genalysis Perth for 50g fire assay charge and AAS analysis.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Diamond Drilling techniques were used at the K2 deposits. DD holes completed pre-2011 were predominantly NQ2 (50.5mm). All Resource definition holes completed post-2011 were drilled using HQ (63.5mm) diameter core. Core was orientated using the Reflex ACT Core orientation system.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	Core recovery is recorded but is generally very good.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	For diamond drilling, the contractors adjust their rate of drilling and method if recovery issues arise. All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Recovery is excellent for diamond core and no relationship between grade and recovery was observed.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	All diamond core is logged to industry best standards for regolith, lithology, veining, alteration, mineralisation and structure. Structural measurements of specific features are also taken through oriented zones.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	All logging is quantitative where possible and qualitative elsewhere. A photograph is taken of every core tray.
	The total length and percentage of the relevant intersections logged.	100% of the core is logged.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	Drill core is cut, and half the core is taken for sampling. The remaining half is stored for later use.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	No non-core results reported
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The sample preparation is considered appropriate.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Field duplicates were taken to industry standards at time of drilling.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Exploration sample preparation is conducted at Genalysis Kalgoorlie. This facility processed the samples which included sorting, checking and drying at less than 110°C to prevent sulphide breakdown. Samples were jaw crushed to a nominal -6mm particle size. If the sample is greater than 3kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3kg (typically 1.5kg) at a nominal <3mm particle size. The entire crushed

Criteria	JORC Code explanation	Commentary
		sample (if less than 3kg) or sub-sample is then pulverised to 90% passing 75µm, using a Labtechnics LM5 bowl pulveriser. 300g pulp subsamples are then taken with an aluminium scoop and stored in labelled pulp packets.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Grind checks are performed at both the crushing stage(3mm) and pulverising stage (75µm), requiring 90% of material to pass through the relevant size.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	A 50g fire assay charge is used with a lead flux in the furnace. The prill is totally digested by HCl and HNO_3 acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical tools were used to determine any element concentrations.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	CRMs are inserted into the sample sequence randomly at a rate of 1 per 20 samples to test the analysis process. Any values outside of 3 standard deviations are re-assayed with a new CRM. Blanks are inserted into the sample sequence at a rate of 1 per 20 samples. This is random, except where high grade mineralisation is expected. Here, a Blank is inserted after the high-grade sample to test for contamination. Failures above 0.2gpt are followed up, and re-assayed. New pulps are prepared if failures remain. No field duplicates are submitted for diamond core. Regular audits of laboratory facilities are undertaken by Northern Star personnel.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	All significant intersections are verified by another Northern Star geologist during the drill hole validation process, and later by a Competent Person to be signed off.
	The use of twinned holes.	No twinned holes were drilled for this data set.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Geological logging was captured using excel templates. Both a hardcopy and electronic copy of these are stored, as well as being loaded in to the database using automatic acquire loaders. Assay files are received in csv format and loaded directly into the database by the Database administrator (DBA). A geologist then checks that the results have inserted correctly. Hardcopy and electronic copies of these are stored.
	Discuss any adjustment to assay data.	No adjustments are made to this assay data.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Holes were pegged using a differential GPS system. During drilling, single-shot surveys are every 30m to ensure the hole remains close to design (using different downhole surveying techniques). Upon hole completion, all Northern Star commissioned holes were Gyroscopic surveyed, taking survey readings every 5m for improved spatial accuracy in a true north grid. Before this, final downhole surveys were conducted to industry standards.
	Specification of the grid system used.	The final collar position for surface holes is measured after hole completion by Differential GPS in the MGA 94_51 grid.
	Quality and adequacy of topographic control.	Quality topographic control has been achieved through Avista data and survey pickups of holes over the last 15 years.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Drill hole spacing across the area varies and ranges from 40m x 40m in the upper zones to +100m x 100m.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The data spacing is considered appropriate to establish a degree of geological and/or statistical confidences for the application of Resource and Reserve classification.
	Whether sample compositing has been applied.	No compositing has been applied to these exploration results, although composite intersections are reported.
	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	Most of the structures in the Kundana camp (including K2 and K2E) dip steeply (80°) to WSW. To target these orientations, the drill hole dips of 60-70° towards ~060° achieve high angle intersections on all structures.

Criteria	JORC Code explanation	Commentary
Orientation of data in relation to geological structure	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No sampling bias is considered to have been introduced by the drilling orientation.
Sample security	The measures taken to ensure sample security.	Prior to laboratory submission samples are stored by Northern Star Resources in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound, and tracked through their chain of custody and via audit trails.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	No audits or reviews have recently been conducted on sampling techniques.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Moonbeam Project is located on tenement M16/157 which is owned 100% by Northern Star Resources.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	No known impediments exist and the tenements are in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	The first reference to the mineralisation encountered at the Kundana project was a Mines Department report produced by Dr. I. Martin (1987). He reviewed work completed in 1983 – 1984 by a company called Southern Resources who identified two geochemical anomalies, creatively named Kundana #1 and Kundana #2. The Kundana #2 prospect was subdivided into a further two prospects, dubbed K2 and K2A. Between 1987 and 1997, limited work was completed. Between 1997 and 2006 Tern Resources (subsequently Rand Mining and Tribune Resources) and Gilt-Edged mining focused on shallow open pit potential which was not considered viable.
Geology	Deposit type, geological setting and style of mineralisation.	The Kundana camp is situated within the Norseman-Wiluna Greenstone Belt in an area dominated by the Zuleika Shear Zone, which separates the Coolgardie Domain from the Ora Banda Domain. K2-style mineralisation consists of narrow vein deposits hosted by shear zones located along steeply-dipping overturned lithological contacts. The K2 structure is present along the contact between a black shale unit (Centenary shale) and intermediate volcanoclastics (Spargoville Formation). The K2E structure is present along the contact between the Victorious Basalt and Centenary shale.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: ▪ easting and northing of the drill hole collar ▪ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar ▪ dip and azimuth of the hole ▪ down hole length and interception depth ▪ hole length.	All summary data is presented in the accompanying table.
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	All results for the recent Moonbeam drilling is presented. The results are not high graded.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	Exploration results are length weighted and uncut.

Criteria	JORC Code explanation	Commentary
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Exploration results are length weighted and uncut, nominally above 1g/t but practically the whole structure is reported which may include low grade.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents are reported.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results:	
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	Estimated true thickness is reported.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	K2 structure is well known, and an estimated true thickness is reported.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Part of the release.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	All results for this drill campaign are reported.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	No other exploration results reported.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Infill definition and extensional depth drilling is planned.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Representative plans and sections accompany this report.

EKJV, Raleigh South, Pegasus Pode, Sir Walter – December 2018
JORC Code, 2012 Edition – Table 1 Report
Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Sampling was completed using underground diamond drilling. Diamond core was transferred to core trays for logging and sampling. Whole core samples were nominated by the geologist and based upon geological and ore-zone boundaries, with the remaining sampled on metre intervals.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Diamond core was transferred to core trays for logging and sampling. Half core samples were nominated by the geologist from NQ2 diamond core with a minimum sample width of 30cm. Occasionally whole core sampling is employed where core recovered is overly fractured or for grade control purposes.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	DD drill core was cut in half using an automated core saw the mass of material collected will depend on the hole size and sampling interval. Core samples were nominated by the geologist from the diamond core, generally being around one metre in length, but with sample widths ranging between approximately 20cm and 100cm as dictated by the geology. Sample lengths varied because drill core samples were allocated so as not to cross significant geological boundaries.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Underground drilling utilised NQ2 (50.5mm) diameter core.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	For diamond drilling the contractors adjust their rate of drilling and method if recovery issues arise.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Recovery was excellent for diamond core and no relationship between grade and recovery was observed.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	All diamond core is logged for regolith, lithology, veining, alteration, mineralisation and structure. Structural measurements of specific features are also taken through oriented zones.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	All logging is quantitative where possible and qualitative elsewhere. A photograph is taken of every core tray.
	The total length and percentage of the relevant intersections logged.	
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	Diamond core is cut using an automated core saw. In most cases, half the core is taken for sampling with the remaining half being stored for later reference. Whole core sampling was only utilised in areas where the Geology is well understood and there is less requirement to retain core for future reference.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	Not relevant, drill core results only being released
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The sampling types used are considered appropriate for the deposits.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Grind checks are performed at both the crushing stage(3mm) and pulverising stage (75µm), requiring 90% of material to pass through the relevant size. Duplicates, pulp duplicates and crush duplicates are also performed.

Criteria	JORC Code explanation	Commentary
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Sample preparation was conducted at Bureau Veritas Kalgoorlie. The sample preparation process commencing with sorting, checking and drying at less than 110°C to prevent sulphide breakdown. Samples are jaw crushed to a nominal -6mm particle size. If the sample is greater than 3kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3kg (typically 1.5kg) at a nominal <3mm particle size. The entire crushed sample (if less than 3kg) or sub-sample is then pulverised to 90% passing 75µm, using a Labtechnics LM5 bowl pulveriser. 300g pulp subsamples are then taken with an aluminium or plastic scoop and stored in labelled pulp packets.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Grind checks are performed at both the crushing stage(3mm) and pulverising stage (75µm), requiring 90% of material to pass through the relevant size.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	A 40g Fire assay charge is used with a lead flux, dissolved in the furnace. The prill is totally digested by HCl and HNO3 acids before Atomic absorption spectroscopy (AAS) determination for gold analysis.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical tools were used to determine any element concentrations.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Certified reference materials (CRMs) are inserted into the sample sequence randomly at a rate of 1 per 20 samples to ensure correct calibration. Any values outside of 3 standard deviations are re-assayed with a new CRM. blanks are inserted into the sample sequence at a rate of 1 per 20 samples. The insertion points are selected at random, except where high grade mineralisation is expected. In these cases, a blank is inserted after the high-grade sample to test for contamination. Results greater than 0.2gpt is received are investigated, and re-assayed if appropriate. New pulps are prepared if anomalous results cannot be resolved. Field Duplicates are taken for all RC samples (1 in 20 sample). No Field duplicates are submitted for diamond core. Umpire sampling programs are undertaken on an ad-hoc basis.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	All significant intersections are verified by another Northern Star geologist during the drill hole validation process, and later by a Competent person to be signed off.
	The use of twinned holes.	No Twinned holes were drilled for this data set.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Geological logging is directly entered into an Acquire database. Assay files are received in csv format and loaded directly into the database by the project's responsible geologist with an Acquire importer object. Hardcopy and electronic copies of these are stored.
	Discuss any adjustment to assay data.	No adjustments are made to this assay data.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Underground diamond hole positions are marked before drilling by mine survey staff and the actual hole collar position located by mine survey staff once drilling is completed. During drilling, single-shot surveys are every 30m to ensure the hole remains close to design. This is performed using the Reflex Ez-Trac system. Upon hole completion, a Gyroscopic survey is conducted by a third-party surveying contractor, taking readings every 5m for improved accuracy. Direction measurements are collected relative to true north. For UG holes multi-shot surveys are taken every 9m when retreating out of the hole.
	Specification of the grid system used.	Data is collected using both local mine grid (Kundana 10) and MGA 94 Zone 51 as appropriate.
	Quality and adequacy of topographic control.	Quality topographic control has been achieved through Lidar data and survey pickups of holes over the last 15 years.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Drill hole spacing varies. Grade control drilling spacing is typically 20m x 20m to provide definition of economic ore shoots. Resource definition drilling spacing is typically 40m x 40m. This allows the Resource to be upgraded to indicated. Inferred Resources typically have a spacing of 80m x 80m. Some exploration holes are spaced up to 200m apart.

Criteria	JORC Code explanation	Commentary
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The data spacing and distribution is considered sufficient to support the Resource and Reserve estimates.
	Whether sample compositing has been applied.	Sample data is composited before grade estimation is undertaken. Average intersection grades are reported in ASX and corporate announcements.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	Most of the structures in the Kundana camp dip steeply (80°) to WSW. The Pode structure has a much shallower dip in a similar direction, approximately 60°. To target these orientations the drill hole dips of 60-70° towards ~060° achieve high angle intersections on all structures. Drill holes with low intersection angles will be excluded from Resource estimation where more suitable data is available.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No sampling bias is considered to have been introduced by the drilling orientation.
Sample security	The measures taken to ensure sample security.	Prior to laboratory submission samples are stored by Northern Star Resources in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound and tracked through their chain of custody and via audit trails.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	No audits or reviews have recently been conducted on sampling techniques.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	All holes mentioned in this report are located within the M16/309 and M16/326 Mining leases and are held by The East Kundana Joint Venture (EKJV). The EKJV is majority owned and managed by Northern Star Resources Limited (51%). The minority holding in the EKJV is held by Tribune Resources Ltd (36.75%) and Rand Mining Ltd (12.25%). The tenement on which the Rubicon, Hornet and Pegasus deposits are hosted (M16/309) is subject to three royalty agreements. The agreements that are on M16/309 are the Kundana- Hornet Central Royalty, the Lake Grace Royalty and the Kundana Pope John Agreement No. 2602-13. The southern portion of Raleigh is located on M15/993, which is held by the East Kundana joint venture entities. The northern extent of Raleigh is located on M16/157 which is 100% owned by Northern Star Resources.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	No known impediments exist, and the tenements are in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	The first reference to the mineralisation style encountered at the Kundana project was the mines department report on the area produced by Dr. I. Martin (1987). He reviewed work completed in 1983 – 1984 by a company called Southern Resources, who identified two geochemical anomalies, creatively named Kundana #1 and Kundana #2. The Kundana #2 prospect was subdivided into a further two prospects, dubbed K2 and K2A. Between 1987 and 1997, limited work was completed. Between 1997 and 2006 Tern Resources (subsequently Rand Mining and Tribune Resources), and Gilt-edged mining focused on shallow open pit potential which was not considered viable for Pegasus, however the Rubicon open Pit was considered economic and production commenced in 2002. In 2011, Pegasus was highlighted by an operational review team and follow-up drilling was planned through 2012. This report is concerned solely with 2014 drilling that led on from this period.
Geology	Deposit type, geological setting and style of mineralisation.	The Kundana camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain.

Criteria	JORC Code explanation	Commentary
		K2-style mineralisation (Pegasus, Rubicon, Hornet) consists of narrow vein deposits hosted by shear zones located along steeply-dipping overturned lithological contacts. The K2 structure is present along the contact between a black shale unit (Centenary shale) and intermediate volcaniclastics (Spargoville formation). Minor mineralisation, termed K2B, also occurs further west, on the contact between the Victorious basalt and Bent Tree Basalt (both part of the regional upper Basalt Sequence). As well as additional mineralisation including the K2E and K2A veins, Polaris/Rubicon Breccia (Silicified and mineralised Shale) and several other HW lodes adjacent to the main K2 structure. A 60° W dipping fault, offsets this contact and exists as a zone of vein-filled brecciated material hosting the Pode-style mineralisation at Pegasus and the Nugget lode at Rubicon. Ambition is interpreted similar in style to the north of Pegasus
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: o easting and northing of the drill hole collar o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar o dip and azimuth of the hole o down hole length and interception depth o hole length.	All drill holes are listed in the appendix
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Exclusion of the drill information will not detract from the understanding of the report
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	All reported assay results have been length weighted to provide an intersection width. A maximum of 2m of barren material between mineralised samples has been permitted in the calculation of these widths. Typically grades over 1.0gpt are considered significant, however, where low grades are intersected in areas of known mineralisation these will be reported. No top-cutting is applied when reporting intersection results.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.##gpt including ##.#m @ ##.##gpt.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalent values have been used for the reporting of these exploration results.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results:	True widths have been estimated for intersections of the known ore zones, based on existing knowledge of the nature of these structures.
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	The target structure is very planar and its orientation well constrained, allowing very reliable calculations of true widths. True widths have been calculated for all reported intersections.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	Both the downhole width and true width have been clearly specified when used.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Appropriate plans and section have been included in the body of this report.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and 'From' and 'To' depths.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk	No other recent material data has been collected.

Criteria	JORC Code explanation	Commentary
	density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Additional drilling is planned with the intention of extending known mineralisation laterally and at depth. Drilling will also be undertaken to improve confidence in previously identified mineralisation and to assist in the location of high grade shoots.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Appropriate diagrams accompany this release.

South Kalgoorlie Operations: Resources and Reserves – December 2018
JORC Code, 2012 Edition – Table 1 Report
Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Samples have been collected from RC drilling face-sampling hammer, and surface/underground diamond drilling.
	Include reference to measures taken to ensure sample retrospectivity and the appropriate calibration of any measurement tools or systems used.	Diamond drill-core is geologically logged and then sampled according to geology (minimum sample length of 0.4 m to maximum sample length of 1.5 m) – where consistent geology is sampled, a 1m length is used for sampling the core. The core is sawn half-core with one half sent off for analysis.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	RC Drilling: Sampling from a standard 5½" RC, three tier riffle splitter (approximately 5kg sample), split to a 12.5% fraction (approximately 3kg) or to a 12% fraction via a rig-mounted cone splitter. All residual material is retained on the ground in rows of 10 or 20 samples. Four-meter composites are obtained via representative scoop / spear sampling of the one-meter residual piles, until required for re-split analysis (samples returning Au >0.2ppm) or eventual disposal. Historical RC drilling is assumed to employ similar practices. An assumed 90% chip recovery (losses to fines) from RC drilling.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Diamond drilling is used for either testing / targeting deeper mineralised systems or to define the orientation of the host geology. Most of these holes have been drilled at NQ2 size with minor HQ sized core. All diamond holes were surveyed during drilling with downhole cameras, and then at end of hole using a Gyro Inclinometer at 5 or 10 m intervals. Drill hole collars were surveyed by onsite mine surveyors. RC drilling is used predominantly for defining and testing for near-surface mineralisation and utilises a face sampling hammer with the sample being collected on the inside of the drill-tube. RC drill holes utilise downhole single or multi shot cameras. Drill hole collars were surveyed by onsite mine surveyors.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	RC drilling contractors adjust their drilling approach to specific conditions to maximize sample recovery. Moisture content and sample recovery is recorded for each RC sample. No recovery issues were identified during RC drilling programs. Recovery was poor at the very beginning of each hole, as is normal for this type of drilling in overburden.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	Representation is assured through qualified geologists identifying intervals for sampling which are related directly to observed geology.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	No defined relationship exists between sample recovery and grade. Nor has sample bias due to preferential loss or gain of fine or coarse material been noted.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	Northern Star surface diamond drill-holes are all orientated and have been logged in detail for geology, veining, alteration, mineralisation and orientated structure. Northern Star underground drill-holes are logged in detail for

Criteria	JORC Code explanation	Commentary
		geology, veining, alteration, mineralisation and structure. Core has been logged in enough detail to allow for the relevant mineral resource estimation techniques to be employed. Surface core is photographed both wet and dry and underground core is photographed wet. All photos are stored on the companies' servers, with the photographs from each hole contained within separate folders. RC chips are geologically logged. All holes are logged completely.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	All logging is quantitative where possible and qualitative elsewhere. A photograph is taken of every core tray.
	The total length and percentage of the relevant intersections logged.	Chip samples have been logged by qualified geologists to a level of detail to support a Mineral Resource estimate.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	NQ2 and HQ diameter core is sawn half core using a diamond-blade saw, with one half of the core consistently taken for analysis. Smaller sized core (LTK48 and BQ) are whole core sampled. The un-sampled half of diamond core is retained for check sampling if required. SKO staff collect the sample in pre-numbered calico sample bags which are then submitted to the laboratory for analysis. Delivery of the sample is by a SKO staff member.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	RC samples are collected at 1m intervals with the samples being riffle split through a three-tier splitter. The samples are collected by the RC drill crews in pre-numbered calico sample bags which are then collected by SKO staff for submission. Delivery of the sample to the laboratory is by a SKO staff member.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	Upon delivery to the laboratory, the sample numbers are checked against the sample submission sheet. Sample numbers are recorded and tracked by the laboratory using electronic coding. Sample preparation techniques are considered appropriate for the style of mineralisation being tested for – this technique is industry standard across the Eastern Goldfields.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Procedures are available to guide the selection of sample material in the field. Standard procedures are used for all process within the laboratory.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Field duplicates are taken for diamond drill core samples at a rate of 1 in 30.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	The sample sizes are considered appropriate for the material being sampled.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	Only nationally accredited laboratories are used for the analysis of the samples collected at SKO. The laboratory oven dries, and if necessary (if the sample is >3kg) riffle split the sample, which is then jaw crushed and pulverised (the entire 3kg sample) in a ring mill to a nominal 90% passing 75 microns. All recent RC and Diamond core samples are analysed via Fire Assay, which involves a 30g charge (sub-sampled after the pulverisation) of the analytical pulp being fused at 1050°C for 45 minutes with litharge. The resultant metal prill is digested in Aqua regia and the gold content determined by atomic adsorption spectrometry – detection limit is 0.01 ppm Au.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical tools were used to determine any element concentrations.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Quality Assurance and Quality Control (QA/QC) samples are routinely submitted by SKO staff and comprise standards, blanks, assay pills, field duplicates, lab duplicates and repeat analyses. The results for these QA/QC samples are routinely analysed by Senior Geologists with any discrepancies dealt with in conjunction with the laboratory prior to the analytical data being imported into the database. There is limited information available on historic QA/QC procedures. SKO has generally accepted the available data at face value and carry out data validation procedures as each deposit is re-evaluated. The analytical techniques used are considered appropriate for the style of mineralisation being tested for – this technique is industry standard across the Eastern Goldfields.

Criteria	JORC Code explanation	Commentary
		Ongoing production data generally confirms the validity of prior sampling and assaying of the mined deposits to within acceptable limits of accuracy.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	Significant intersections are validated by senior geologists.
	The use of twinned holes.	Virtual twinned holes have been drilled in several instances across all sites with no significant issues highlighted. Drill hole data is also routinely confirmed by development assay data in the operating environment.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Primary data is collected utilising LogChief. The information is imported into a SQL database server and verified.
	Discuss any adjustment to assay data.	All data is compiled in databases (underground and open pit) which are overseen and validated by senior geologists. No adjustments have been made to any assay data.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Collar coordinates for surface RC and diamond drill-holes were generally determined by either RTK-GPS or a total station survey instrument. Underground drill-hole locations (Mount Marion and HBJ) were all surveyed using a Leica reflectorless total station. Recent surface diamond holes were surveyed during drilling with down-hole single shot cameras and then at the end of the hole by Gyro-Inclinometer at 5 or 10mm intervals. Holes not gyro-surveyed were surveyed using Eastman single shot cameras at 20m intervals. RC drill-holes utilised down-hole single shot camera surveys spaced every 15 to 30m down- hole. Down-hole surveys for underground diamond drill-holes were taken at 15 – 30m intervals by Reflex single-shot cameras.
	Specification of the grid system used.	MGA grid is used for HBJ and the regional exploration results.
	Quality and adequacy of topographic control.	Topographic control is generated from RTK GPS.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Drill spacing ranges from 10m x 5m grade control drilling to 100m x 100m at deeper levels of the resource.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	No resources or reserves are reported in the release.
	Whether sample compositing has been applied.	Composting is not applied to these results.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	Drilling intersections are nominally designed to be as perpendicular to the orebody as far as underground infrastructure constraints / topography allows.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	It is not considered that drilling orientation has introduced an appreciable sampling bias.
Sample security	The measures taken to ensure sample security.	For samples assayed at the on-site laboratory facilities, samples are delivered to the facility by Company staff. Upon delivery the responsibility for sample security and storage falls to the independent third-party operators of these facilities. For samples assayed off-site, samples are delivered to a third-party transport service, who in turn relay them to the independent laboratory contractor. Samples are stored securely until they leave site.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	Site generated exploration results are routinely reviewed by the Northern Star Corporate technical team.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	State Royalty of 2.5% of revenue applies to all tenements, although does not apply to the 16 freehold titles (which host the majority of SKO's Resource inventory). There are several minor agreements attached to a select number of tenements and locations with many of these royalty agreements associated with tenements with no current Resources and/or Reserves. Private royalty agreements are in place that relate to production from HBJ open-pit at $10/ oz. In addition, a royalty is payable in the form of 1.75% of the total gold ounces produced from the following resources: Shirl Underground, Golden Hope, Bellevue, HBJ Open-pit, Mount Martin open-pit, Mount Martin Stockpiles and any reclaimed tailings. The South Kalgoorlie Operations consists of 35 Mining Leases and 19 Exploration and Prospecting Licences. The Project also includes 9 Miscellaneous Licences, 2 groundwater Licences and 16 Freehold Lots known as the Hampton "Exempted East Locations". The Area of the leases covers approximately 35,638 Hectares with a further 71,861 Hectares of Freehold Land.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	All leases and licences to operate are granted and in the order of 2 and 21 years. There are no known impediments to continued operation.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	The HBJ 'line of lode' is a 6 km zone of mineralisation that extends from Golden Hope in the south to Celebration in the north. The existing HBJ pit was mined for over 25 years producing approximately 1.6 Moz Au and was owned by separate companies across the Location 48 and Location 50 tenement boundary. Gold was first discovered in the New Celebration area in 1919 and a short-lived gold rush ensued. Intermittent exploration for gold and nickel was undertaken by a variety of companies in the 1960s and 1970s. The rising gold price further rekindled interest in the area in the 1980s, and open-pit mining at New Celebration started in 1986 by a joint venture comprising Newmont Holdings Limited (subsequently Newcrest; 60%), Hampton Areas Australia Ltd., (25%) and Mt Martin Gold Mines (15%), which merged with Titan Resources in 1993. The New Celebration project includes the Hampton Boulder deposit. In June 2001 Hill 50 Gold agreed to purchase the New Celebration project from Newcrest Mining. In December 2001 Harmony Gold Mining acquired Hill 50 Gold, the transaction giving Harmony Gold Mining a 100% interest in the New Celebration project. The Jubilee deposit located south of the Hampton Boulder deposit was evaluated and mined by Hampton Areas Australia Ltd from 1984 to 1996 with open pit mining starting in 1987. New Hampton Goldfields (New Hampton) acquired the Jubilee deposit in 1996. In May 2001, Harmony Gold Mining acquired New Hampton, and combined the operations of New Hampton's Jubilee operations and associated small open pits with the New Celebration project into the South Kalgoorlie Operations (SKO). In 2007, Dioro Exploration NL (Dioro) acquired the SKO from Harmony Gold (Australia) Pty Ltd (Harmony) via its wholly-owned subsidiaries, South Kal Mines Pty Ltd, New Hampton Goldfields Ltd and Aurora Gold (WA) Pty Ltd. The tenement package at SKO was then purchased by Avoca Resources in April 2010, which was subsequently acquired by Alacer Gold Corp. Pty Ltd in early 2011. Westgold Resources Limited acquired the SKO tenement holdings in October 2013 via the acquisition of Alacer Gold's Australian assets. In April 2018 Northern Star Resources acquired the SKO tenement holdings with the purchase of HBJ Minerals Pty Ltd from Westgold.
Geology	Deposit type, geological setting and style of mineralisation.	Stratigraphy for the Ora Banda and Kalgoorlie Domains is relatively well-known and comprise (from stratigraphically lowest) a lower basalt unit, komatiitic to high-magnesian basaltic rocks, an upper basalt unit and overlying felsic volcanic-sedimentary units. Conglomeratic and sandstone units unconformably overlie the upper felsic units adjacent to major shear zones. Layered mafic sills occur within various stratigraphic units and cross-cutting Proterozoic dykes also occur throughout the region. Metamorphic grade ranges from upper greenschist to upper amphibolite facies. The deformation history of the area is generally divided into four main phases, comprising north-directed thrusting with recumbent folding and stratigraphic repetition in D1. The second deformation (D2) resulted in north-northwest trending folds which are reflected in the dominant north-northwest trending fabric of the greenstone belts. Shortening continued during D3 with strike slip movement along northwest to north northwest trending shear zones and D4 brittle faulting.

Criteria	JORC Code explanation	Commentary
		The HBJ orebodies form part of a gold mineralised system along the Boulder-Lefroy shear zone that is over 4 km long and includes the Celebration, Mutooroo, HBJ and Golden Hope open pit and underground mines. The HBJ orebodies are hosted within a steeply-dipping, north-northwest-striking package of mafic, ultramafic and sedimentary rocks and schists that have been intruded by felsic to intermediate porphyries. The area is extensively deformed with numerous north-striking shear zones and dilation of the porphyry intrusions. The main host rock for the Jubilee deposit is the Jubilee Dolerite.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: o easting and northing of the drill hole collar o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar o dip and azimuth of the hole o down hole length and interception depth o hole length.	All data is presented in the accompanying tables.
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	No data is excluded.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	Reported exploration results are uncut.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Short intervals are length weighted to create the final intersections.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents are reported.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results:	
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	Due to complex mineralisation geometry and varying intercept angles the true thickness is manually estimated on a hole by hole basis.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	Downhole length in addition to estimated true width is shown in the report tables if intersection structure is known. The drill hole intercept true thickness is notes as "Unknown" otherwise.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Selected diagrams form part of this release.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	All holes for selected periods or areas are presented, including NSI (no significant intersection) Results are not high graded.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	There is no other substantive exploration data associated with this release.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Ongoing surface and underground exploration activities will be undertaken to support continuing mining activities at Northern Star Gold Operations.

Criteria	JORC Code explanation	Commentary
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Diagrams in the release.

Jundee - December 2018
JORC Code, 2012 Edition – Table 1
Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	This deposit is sampled by diamond drilling (DD) DD - Sampled sections are generally NQ2 or BQ. Core sample intervals are defined by the geologist to honour geological boundaries ranging from 0.3 to 1.2m in length.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Core is aligned and measured by tape, comparing back to downhole core blocks consistent with industry practice.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	Diamond drilling completed to industry standard using varying sample lengths (0.3 to 1.2m) based on geological intervals, which are then crushed and pulverised to produce a ~200g pulp sub sample to use in the assay process. Diamond core samples are fire assayed (30g charge). Visible gold is occasionally encountered in core.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Surface diamond drilling carried out by using both HQ2 or HQ3 or PQ2 (triple tube) and NQ2 (standard tube) techniques. Sampled sections are generally NQ2. Core is routinely orientated using the ORI-shot device.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	DD – Recoveries are recorded as a percentage calculated from measured core verses drilled intervals.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	Diamond drilling practice results in high core recovery due to the competent nature of the ground.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	There is no known relationship between sample recovery and grade, diamond drill sample recovery is very high.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	Core samples have been logged by qualified Geologist to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Logging is Qualitative and Quantitative, and all core is photographed wet (some older core is pre-digital, photos not all reviewed). Visual estimates of sulphide, quartz and alteration as percentages.
	The total length and percentage of the relevant intersections logged.	100% of the drill core is logged.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	Core is half cut with an Almonté diamond core saw. Sample intervals are defined by a qualified geologist to honour geological boundaries. The left half is archived Core is sampled on the width of the geological/mineralized structure in recognized ore zones. The minimum sample length is 0.3m while the maximum is 1.2m. Total weight of each sample generally does not exceed 5kg.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	No no-core results are being reported

Criteria	JORC Code explanation	Commentary
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	Following drying at 100°C to constant mass, all samples below approximately 4kg are totally pulverised in LM5's to nominally 90% passing a 75µm screen. The very few samples generated above 4kg are crushed to <6mm and riffle split first prior to pulverisation. In 2012, Francois-Bongarcon (Agoratek International) conducted a heterogeneity studies, audit of site laboratory, and audit of plant samplers. Confirmed that the sampling protocol currently in use are appropriate to the mineralisation encountered and should provide representative results.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Repeat analysis of pulp samples (for all sample types – diamond, RC, rock and soil) occurs at an incidence of 1 in 20 samples.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Field duplicates, i.e. other half of cut core, have not been routinely assayed.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Sample sizes are considered appropriate.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	For all drill core samples, gold concentration is determined by fire assay using the lead collection technique with a 30-gram sample charge weight. An AAS finish is used to be considered as total gold.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	Not applicable to this report.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	The QAQC protocols used include the following for all drill samples: ▪ The field QAQC protocols used include the following for all drill samples: -Commercially prepared certified reference materials (CRM) are inserted at an incidence of 1 in 30 samples. The CRM used is not identifiable to the laboratory, -QAQC data is assessed on import to the database and reported monthly, quarterly and yearly. ▪ The laboratory QAQC protocols used include the following for all drill samples: -Repeat analysis of pulp samples occurs at an incidence of 1 in 20 samples, -Screen tests (percentage of pulverised sample passing a 75µm mesh) are undertaken on 1 in 50 samples, -The laboratories' own standards are loaded into the database, -The laboratory reports its own QAQC data on a monthly basis. -In addition to the above, ~ 3% of samples are sent to a check laboratory. Samples for check -assay are selected automatically from holes, based on the following criteria: grade above 1gpt or logged as a mineralized zone or is followed by feldspar flush or blank. ▪ Failed standards are generally followed up by re-assaying a second 30g pulp sample of samples between the failed standard and the next sequenced standard by the same method at the primary laboratory. Re-assays are dependent on grade above 0.1ppm Both the accuracy component (CRM's and third-party checks) and the precision component (duplicates and repeats) of the QAQC protocols are thought to demonstrate acceptable levels of accuracy and precision.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	Significant intersections verified by senior site geological staff
	The use of twinned holes.	There is no purpose drilled twinned holes.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Primary Data imported into SQL database using semi-automated or automated data entry. Hard copies of NSR and previous operators, core assays and surveys are stored at site. Visual checks are part of daily use of the data in Vulcan. Data from previous operators thoroughly vetted and imported to SQL database.
	Discuss any adjustment to assay data.	The first gold assay is almost always used. Exceptions occur when evidence from re-assaying and/or check-assaying dictates. A systematic procedure utilizing several re-assays and/or check assays is in place to determine

Criteria	JORC Code explanation	Commentary
		when the final assay is changed from the first gold assay. Some minor adjustments have been made to overlapping data.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Collar positions are recorded using conventional survey methods based on Leica TS15 3" total stations and Trimble R10 GNSS instruments. The location of each station is referenced to state-wide network of Standard Survey Marks (SSM) established and coordinated by the Department of Land Administration (WA Government). Where regional drill hole positions are distant from the SSM network the world wide Global Navigational Satellite System (GNSS) network is used. Positional checks are carried out using a combination of existing known positions (usually based on prominent landmarks) and grid referenced information such as ortholinear rectified photogrammetry based on the Australian Map Grid 1994 (MGA94_51). Collar coordinates are recorded in MGA94 or Local Jundee Grid (JUNL2) dependant on the location and orientation of ore-bodies. Cross checks were made on the survey control points and data in June 2005. Collar information is stored in both local coordinates and MGA94 coordinate in the drilling database. In-mine drill-hole collars are normally accurate to 10 cm. Multi shot cameras and gyro units were used for down-hole survey. Previous drilling has been set-out and picked up in both national and local grids using a combination of GPS and Survey instruments and are assumed to be to industry standards.
	Specification of the grid system used.	Collar coordinates are recorded in MGA94 Zone 51 and Local Jundee Grid (JUNL2) dependant on the location and orientation of ore-bodies. The difference between Jundee mine grid (GN) and magnetic north (MN) as at 30 July 2018 is 39° 00' 07" and the difference between magnetic north (MN) and true north (TN) is 1° 02' 00". The difference between true north (TN) and MGA94 Zone 51 is 1° 06' 26". The difference between true north and GDA is zero.
	Quality and adequacy of topographic control.	Topographic control is from Digital Elevation Contours (DEM) 2010, 1m contour data and site surveyed pit pickups.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Drill spacing of the released holes is quite variable, from a nominal 20 by 20 in grade control areas to greater than 100 by 100 in Zodiac exploration
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	No resource or reserve is being released.
	Whether sample compositing has been applied.	Core is sampled to geology; sample compositing is not applied until the estimation stage.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	The orientation of sampling is generally perpendicular to the main mineralisation trends. The orientation achieves unbiased sampling of all possible mineralisation and the extent to which this is known.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	The drill orientation to mineralised structures biases the number of samples per drill hole. It is not thought to make a material difference. As the opportunity arises, better angled holes are infill drilled.
Sample security	The measures taken to ensure sample security.	All samples are selected, cut and bagged in tied numbered calico bags, grouped in larger tied plastic bags, and placed in large sample cages with a sample submission sheet. The cages are either sent to the site laboratory or are transported via freight truck to Perth, with consignment note and receipted by external and independent laboratory. All sample submissions are documented and all assays are returned via email. Sample pulp splits from the site lab are stored at the Jundee mine site and those from the Newburn Lab in Perth are stored at the Newburn Lab. Pre NSR operator sample security assumed to be similar and adequate.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	In 2006, Maxwell conducted an audit of all Jundee data. In 2012, Francois-Bongarcon (Agoratek International) conducted a heterogeneity studies, audit of site laboratory, and audit of plant samplers. Both audits found the sampling techniques and data to be adequate. All recent NSR sample data has been extensively QAQC reviewed both internally and externally.

Criteria	JORC Code explanation	Commentary
		Pre-NSR data audits found to be minimal regarding QAQC though in line with industry standards of the time.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Jundee project consists of tenements comprising 62 mining leases and 1 general purpose lease, covering a total area of approximately 57,422.2 Ha. All are registered in the name of Northern Star Resources Limited. The project also includes 23 miscellaneous licences, 3 groundwater licenses, a pipeline license, and the Jundee Pastoral Lease. These cover the bore fields, roads, airstrip, and gas pipeline. There are numerous access agreements in place including access rights over part of Mark Creasy's mining lease 53/193 which lies contiguous to and beneath the general purpose lease on which the Jundee gold mine processing plant is located. There are no heritage issues with the current operation. The majority of the Jundee leases are granted Mining Leases prior to 1994 (pre-Mabo) and as such Native Title negotiations are not required. During 2004, two agreements where struck between Ngaanyatjarra Council (now Central Desert native Title Services (CDNTS)) and NYO, these agreements being the Wiluna Land Access Agreement 2004 and the Wiluna Claim Heritage Agreement 2004.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	All leases and licences to operate are granted and in the order for between 3 and 20 years.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	Data relevant to this Resource was predominantly NSR (Northern Star Resources), who have operated the mine since July 1, 2014. The Jundee/Nimary Deposits were discovered in the late 1980's/early 1990's after LAG and soil sampling by Mark Creasy (Jundee) and Hunter Resources (Nimary) identified large surface gold anomalies. The deposits were drilled out over the following years by Eagle Mining (which took over Hunter Resources), and Great Central Mines (which formed a joint venture with Creasy and later purchased his share). Open pit operations commenced in mid-1995, with the first gold poured in December 1995. Great Central Mines assumed full control of the field with its successful takeover of Eagle Mining in mid-1997. Great Central Mines was later taken over by Normandy in mid-2000, which in turn was taken over by Newmont in early-2002. All previous work is accepted and assumed to industry standard at that time.
Geology	Deposit type, geological setting and style of mineralisation.	Jundee is an Archean lode-gold mineralized deposit that is part of the Northern Yandal Greenstone belt. Gold mineralisation is controlled by a brittle fracture-system, is commonly fracture-centred, and is predominantly hosted in dolerite and basalt. Mineralisation can be disseminated or vein style host.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: o easting and northing of the drill hole collar o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar o dip and azimuth of the hole o down hole length and interception depth o hole length.	Too many holes to practically summarise all drill information used. (See diagram).
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Exclusion of the drill information will not detract from the understanding of the report. Holes are close spaced and tightly constrained to an active mine area.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	Reported exploration results are uncut.

Criteria	JORC Code explanation	Commentary
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Short intervals are length weighted to create the final intersections.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents are reported.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results:	
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	Due to complex mineralisation geometry and varying intercept angles the true thickness is manually estimated on a hole by hole basis.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	Downhole length in addition to estimated true width is shown in the report tables if intersection structure is known. The drill hole intercept true thickness is notes as "Unknown" otherwise.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Plan view and long section view of Jundee showing drill traces is attached.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	All intercepts for a period and area are included in this release, including NSI (no significant intersection).
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	No other meaningful data to report.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Further extensional and definition drilling is planned for FY2019 from both underground and surface positions.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Representative diagrams form part of the release.

Jundee (Ramone) – December 2018
JORC Code, 2012 Edition – Table 1 Report
Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Sampling is by both diamond drilling (DD) and Reverse Circulation (RC) drilling completed by NSR. DD samples are HQ and NQ core with sample intervals defined by the geologist to honour geological boundaries ranging from 0.3 to 1.2m in length. RC samples are collected via rig-mounted static cone splitter with sample falling though inverted cone splitter, splitting the sample in 88%/9%/3% ratio. 9% split retained for 1m composites and 3% split retained for 4m composites. 1m samples are sent for further analysis if any 4m composites return a gold value > 0.1ppm or intervals containing alteration/mineralisation failed to return a significant composite assay result. NSR Resource definition drilling routinely collects 1m composites.
	Include reference to measures taken to ensure sample representativity and the appropriate calibration of any measurement tools or systems used.	DD core is aligned and measured by tape, comparing back to down hole core blocks consistent with industry practice. RC metre intervals are delineated with spray paint to determine metres drilled. Sample rejects are left on the sample pad to indicate metres drilled for the hole.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	Diamond drilling is completed to industry standard using varying sample lengths (0.3 to 1.2m) based on geological intervals, which are then crushed and pulverised to produce a ~200g pulp sub sample to use in the assay process. Diamond core samples are fire assayed (50g charge) and screen fire assayed for visible gold. Visible gold is occasionally encountered in core. RC sampling to industry standard at the time of drilling where ~3-4kg samples are pulverised to produce a ~200g pulp sample to utilise in the assay process. RC samples are fire assayed (50g charge).
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	RC drilling is carried out using a face sampling hammer and a 130mm diameter bit. Diamond drilling carried used HQ3 (triple tube) and NQ2 techniques. Core is routinely orientated using the ORI-shot device.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	RC – Approximate recoveries are sometimes recorded as percentage ranges based on a visual and weight estimate of the sample. DD – Recoveries are recorded as a percentage calculated from measured core versus drilled intervals.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	Diamond drilling practice results in high core recovery due to the competent nature of the ground. RC drilling recovery is supervised on the rig and any recovery issues are recorded and rectified.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	There is no known relationship between sample recovery and grade, diamond drill sample recovery is very high.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	DD core and RC chip samples have been logged by qualified geologists to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies *Percussion holes logging were carried out on a metre by metre basis and at the time of drilling.*
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Logging is Qualitative and Quantitative; all core is photographed wet. Visual estimates are made of sulphide, quartz and alteration as percentages.
	The total length and percentage of the relevant intersections logged.	100% of all DD and RC drilling is logged.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	DD core is halved with an Almonté diamond core saw. The core is quarter cut when metallurgical samples are required. Sample intervals are defined by a qualified geologist to honour geological boundaries. The left half is archived.

Criteria	JORC Code explanation	Commentary
		All mineralised zones are sampled plus associated visibly barren material in contact with mineralised zones. Core is sampled on the width of the geological/mineralized structure with a minimum sample length of 0.3m and a maximum sample length of 1.2m. Total weight of each sample generally does not exceed 5kg.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	RC drilling uses a cyclone mounted inverted cone splitter.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	DD core is dried at 100°C to constant mass, all samples below approximately 4kg are totally pulverised in LM5's to nominally 90% passing a 75µm screen. The few samples generated above 4kg are crushed to <6mm and riffle split first prior to pulverisation. RC samples are dried at 100°C to constant mass, all samples below approximately 3kg are totally pulverised in LM5's to nominally 85% passing a 75µm screen. Samples generated above 4kg are crushed to <6mm and cone split to nominal mass prior to pulverisation. *For RC samples, no formal heterogeneity study has been carried out or monographed. An informal analysis suggests that the sampling protocol currently in use are appropriate to the mineralisation encountered and should provide representative results.*
	Quality control procedures adopted for all sub-sampling stages to maximise representativity of samples.	Repeat analysis of pulp samples (all sample types) occurs at an incidence of 1 in 20 samples. *Analysis of 2mm coarse crush and split has been completed for three RC bulk cone splitter rejects each of them divided into 32 equal splits.*
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Field duplicates, (i.e. other half of cut core) are routinely assayed. NSR routinely collects field duplicates during RC drilling.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Sample sizes are considered appropriate. No formal nomograph study has been conducted on the RC primary sub sample split. Industry standard practice supports splitting of primary sub samples at particle sizes of <6mm and P_{80} 75µm.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	For all drill samples, gold concentration was determined by fire assay using the lead collection technique with a 50-gram sample charge weight. MP-AES instrument finish was used to be considered as total gold. Various multi-element suites are analysed using a four-acid digest with an AT/OES finish.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	Not applicable to this report.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	The QAQC protocols used include the following for all drill samples: - Field QAQC protocols used for all drill samples include commercially prepared certified reference materials (CRM) inserted at an incidence of 1 in 30 samples. The CRM used is not identifiable to the laboratory with QAQC data is assessed on import to the database and reported monthly, quarterly and yearly. - NSR RC Resource definition drilling routinely inserts field blanks and monitor their performance. - Laboratory QAQC protocols used for all drill samples include repeat analysis of pulp samples occurs at an incidence of 1 in 20 samples and screen tests (percentage of pulverised sample passing a 75µm mesh) are undertaken on 1 in 40 samples. - The laboratories' own standards are loaded into the database and the laboratory reports its own QAQC data monthly. - In addition to the above, about 3% of diamond drill samples are sent to a check laboratory. Samples for check -assay are selected automatically from holes based on the following criteria: grade above 1gpt or logged as a mineralized zone or is followed by feldspar flush or blank. - Failed standards are generally followed up by re-assaying a second 50g pulp sample of all samples in the fire above 0.1ppm by the same method at the primary laboratory. *Both the accuracy component (CRM's and third-party checks) and the precision component (duplicates and repeats) of the QAQC protocols are thought to demonstrate acceptable levels of accuracy and precision.*

Criteria	JORC Code explanation	Commentary
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	Significant intersections not verified.
	The use of twinned holes.	There are no purpose drilled twin holes.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Sampling and logging data is digitally entered into a tablet using Logchief software imported into SQL database using semi-automated or automated data entry. Digital assay files are loaded directly into the database. Visual checks are part of daily use of the data in Vulcan.
	Discuss any adjustment to assay data.	The first gold assay is almost always utilised for any Resource estimation except where evidence from re-assaying and/or check-assaying dictates. A systematic procedure utilizing several re-assays and/or check assays is in place to determine when the final assay is changed from the first gold assay.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Collar positions are recorded using conventional survey methods based on Leica TS15 3" total stations and Trimble R10 GNSS instruments. The location of each station is referenced to state-wide network of Standard Survey Marks (SSM) established and coordinated by the Department of Land Administration (WA Government). Where regional drill hole positions are distant from the SSM network, the world wide Global Navigational Satellite System (GNSS) network is used. Positional checks are carried out using a combination of existing known positions (usually based on prominent landmarks) and grid referenced information such as ortho-linear rectified photogrammetry based on the Map Gird of Australia MGA94. Collar coordinates are recorded in MGA94. Surface collar RL's have been validated utilizing an airborne elevation survey by Arvista in October 2017. Multi shot cameras and gyro units were used for down-hole survey.
	Specification of the grid system used.	Collar coordinates are recorded in MGA94 Zone 51. The difference between magnetic north (MN) and true north (TN) is 1° 34' 30". The difference between true north (TN) and AMG84 Zone 51 (AMG GN) is 1° 02' 47". The difference between true north and GDA is zero.
	Quality and adequacy of topographic control.	Topographic control is from Digital Elevation Contours (DEM) 2017, 1m contour data and site surveyed pickups.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Tight spacing infill 5m by 10m.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Resources and Reserves are not being reported in this release.
	Whether sample compositing has been applied.	Core is sampled to geology; sample compositing is not applied until the estimation stage. RC samples are taken as 1 m samples and 4 m composites during first pass exploration,1m samples are sent for further analysis if any 4m composites return a gold value > 0.1ppm or intervals containing alteration/mineralisation failed to return a significant composite assay result. For RC Resource definition drilling 1 m samples are routinely collected. No RC samples greater than 1m were used in estimation.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	*The orientation of sampling is generally on a high angle to the main mineralisation trends as these are vertical to sub-vertical. Drill holes are drilled on a 60 degrees angle perpendicular to the strike of the mineralisation.*
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	The drill orientation to mineralised structures biases the number of samples per drill hole. It is not thought to make a material difference in the Resource estimation.
Sample security	The measures taken to ensure sample security.	All samples are selected, cut and bagged in tied numbered calico bags, grouped in larger tied plastic bags, and placed in large sample cages with a sample submission sheet. The cages are either sent to the site laboratory or are transported via freight truck to Perth, with consignment note and receipted by external and independent laboratory All sample submissions are documented and all assays are returned via email and hard copy.

Criteria	JORC Code explanation	Commentary
		Sample pulp splits from the site lab are stored at the Jundee mine site and those from the Newburn Lab in Perth are stored at the Newburn Lab. RC samples processed at SGS have had the bulk residue discarded and pulp packets sent to Jundee mine site for long term storage.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	Historical audits of all Jundee data were carried out by previous operators. In 2012, Francois-Bongarcon (Agoratek International) conducted a heterogeneity studies, audit of site laboratory, and audit of plant samplers. Both audits found the sampling techniques and data to be adequate. All recent NSR sample data has been extensively QAQC reviewed both internally and externally.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Jundee Project consists of 7 Exploration Licences, 62 Mining Leases and 1 General Purpose Lease covering a total area of approximately 86,341 Ha. All are currently registered in the name of Newmont Yandal Operations Pty Ltd but Northern Star Resources Limited are the beneficial owners and transfers will be registered once the Office of State Revenue have completed their assessment to duty. The Project also includes 23 Miscellaneous Licenses, 3 Groundwater Licenses, a Pipeline License and the Jundee Pastoral Lease covering the bore fields, roads, airstrip, and gas pipeline. There are numerous access agreements in place including access rights over part of M53/193 which lies contiguous to, and beneath, the General Purpose Lease on which the Jundee processing plant is located. There are no heritage issues with the current operation. The majority of the Jundee leases are granted Mining Leases prior to 1994 (pre-Mabo) and as such Native Title negotiations are not required. During 2004, two agreements where struck between Ngaanyatjarra Council (now Central Desert Native Title Services (CDNTS)) and Newmont Yandal Operations, these agreements being the Wiluna Land Access Agreement 2004 and the Wiluna Claim Heritage Agreement 2004, both agreements were transferred to Northern Star on purchase of the Jundee Operations in 2014.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	All leases and licences to operate are granted and in the order for between 3 and 21 years.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	Not Applicable, all the exploration work has been completed by NSR.
Geology	Deposit type, geological setting and style of mineralisation.	Ramone is Archean gold mineralized deposit that is part of the Northern Yandal Greenstone belt. Gold mineralisation is hosted by a granite and controlled by a brittle stockwork fracture-system within a north-easterly trending shear zone. The mineralisation formed by a stockwork of veins with smoky quartz, sulphides minor carbonate, chlorite and sericite hosted by a monzonitic granite. The mineralisation is intruded by an East-West striking (about 96 degrees) vertical dolerite dyke that cross cuts the mineralisation and is part of a suite of magnetic dolerite dykes that intrudes the Yandal belt in an East-West direction.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: o easting and northing of the drill hole collar o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar o dip and azimuth of the hole o down hole length and interception depth o hole length.	Summary drill data for all Ramone holes related to this release are presented.
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	No results excluded, both high and low grade intercepts are presented.

Criteria	JORC Code explanation	Commentary
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	Reported intercepts are length weighted and uncut, generally > 1g/t and no more than 1m of internal waste included.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Reported intercepts are length weighted.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents are reported.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results.	
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	Estimated true thickness is reported along with the downhole length.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	Estimated true thickness is reported along with the downhole length.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	A plan view of collar locations from part of this release.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	All results are reported.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	No other meaningful data to report.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Further extensional and resource definition drilling is continuing in FY2019.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Plans and sections of the Ramone deposit are included in this report.

Tanami (Hurricane-Repulse and Regional Exploration) – December 2018
JORC Code, 2012 Edition – Table 1 Report
Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Sampling is by Reverse Circulation (RC), Diamond (DD drilling, completed by NSR. RC samples are collected via rig-mounted static cone splitter, splitting the sample in 88%/12% ratio. 12% split retained for 1m composites and 88% split retained as a bulk reject. All 1m samples are sent for analysis. NSR Resource definition drilling routinely collects 1m composites. DD samples are HQ core with sample intervals defined by the geologist to honour geological boundaries ranging from 0.3m to 1.2m in length.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	RC metre intervals are delineated with spray paint to determine metres drilled. Sample rejects are left on the sample pad to indicate metres drilled for the hole. DD core is aligned and measured by tape, comparing back to down hole core blocks consistent with industry practice.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	RC sampling to industry standard at the time of drilling where ~4kg samples are pulverised to produce a ~200g pulp sample to utilise in the assay process. RC samples were fire assayed (30g charge). Diamond drilling is completed to industry standard using varying sample lengths (0.3m to 1.2m) based on geological intervals, which are then crushed and pulverised to produce a ~200g pulp sub sample to use in the assay process. Diamond core samples are fire assayed (50g charge).
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	RC drilling is carried out using a face sampling hammer with a 130mm diameter bit respectively. Diamond drilling used HQ3 (triple tube) techniques in their entirety to delivery good quality-oriented core for metallurgical/geotechnical/geology work. Sampled sections were HQ3.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	RC – Approximate recoveries are sometimes recorded as percentage ranges based on a visual and weight estimate of the sample. DD recoveries are recorded as a percentage calculated from measured core verses drilled intervals.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	RC drilling recovery is supervised on the rig and any recovery issues are recorded and rectified. Diamond drilling practice results in high core recovery due to the competent nature of the ground.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	There is no known relationship between sample recovery and grade. Diamond drill sample recovery is very high.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	RC chip samples and DD core have been logged by qualified geologists to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. RC hole logging was carried out on a metre by metre basis and at the time of drilling.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Logging is Qualitative and Quantitative. Visual estimates are made of sulphide, quartz and alteration as percentages.
	The total length and percentage of the relevant intersections logged.	100% of all DD and RC drilling is logged.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	DD core is halved with an Almonte core saw. Sample intervals are defined by a qualified geologist to honour geological boundaries. All mineralised zones are samples plus associated visibly barren material in contact with mineralised zones. DD core is sampled on the width of the geological/mineralised structure with a minimum sample length of 0.3m and maximum sample length of 1.2m. Total weight of each sample generally does not exceed 5kg.

Criteria	JORC Code explanation	Commentary
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	RC drilling uses a cyclone mounted inverted cone splitter.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	RC samples are dried at 100°C to constant mass, all samples below approximately 3kg are totally pulverised in LM5's to nominally 85% passing a 75µm screen. Samples generated above 4kg are crushed to <6mm and cone split to nominal mass prior to pulverisation. For RC samples, no formal heterogeneity study has been carried out or monographed. An informal analysis suggests that the sampling protocol currently in use are appropriate to the mineralisation encountered and should provide representative results. DD core is dried at 100°C to constant mass, all samples below approximately 4kg are totally pulverised in LM5's to nominally 85% passing a 75µm screen. The few samples generated above 4kg are crushed to <6mm and riffle split first prior to pulverisation.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Repeat analysis of pulp samples (all sample types) occurs at an incidence of 1 in 20 samples.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Field duplicates, (i.e. other half of cut core) are routinely assayed. NSR routinely collects field duplicates during RC drilling.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Sample sizes are considered appropriate. No formal monograph study has been conducted on the RC primary sub sample split. Industry standard practice supports splitting of primary sub samples at particle sizes of <6mm and P_{80} 75µm.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	For all drill samples, gold concentration was determined by fire assay using the lead collection technique with a 30-gram sample charge weight. MP-AES instrument finish was used to be considered as total gold. Various multi-element suites are analysed using a four-acid digest with an AT/OES finish.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	Not applicable to this report.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	The QAQC protocols used include the following for all drill samples: Field QAQC protocols used for all drill samples include commercially prepared certified reference materials (CRM) inserted at an incidence of 1 in 20 samples. The CRM used is not identifiable to the laboratory with QAQC data is assessed on import to the database and reported monthly, quarterly and yearly. NSR RC Resource definition drilling routinely inserts field blanks and monitor their performance. Laboratory QAQC protocols used for all drill samples include repeat analysis of pulp samples occurs at an incidence of 1 in 20 samples and screen tests (percentage of pulverised sample passing a 75µm mesh) are undertaken on 1 in 40 samples. The laboratories' own standards are loaded into the database and the laboratory reports its own QAQC data monthly. In addition to the above, approximately 2% of RC drill samples are sent to a check laboratory. Samples for check -assay are selected automatically from holes based on the following criteria: grade above 1gpt or logged as a mineralized zone or is followed by feldspar flush or blank. Failed standards are generally followed up by re-assaying a second 30g pulp sample of all samples in the fire above 0.1ppm by the same method at the primary laboratory. Both the accuracy component (CRM's and third-party checks) and the precision component (duplicates and repeats) of the QAQC protocols are thought to demonstrate acceptable levels of accuracy and precision.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	Significant intersections verified by corporate NSR personnel.
	The use of twinned holes.	There were purpose-drilled RC twinned holes to check selected legacy RC holes, with strong correlation of geological and assay results.

Criteria	JORC Code explanation	Commentary
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Primary data is imported into an SQL database using semi-automated or automated data entry with hard copies of core assays and surveys are stored at site. Visual checks are part of daily use of the data in geological modelling software including Vulcan, Leapfrog and MICROMINE.
	Discuss any adjustment to assay data.	The first gold assay is almost always utilised for any Resource estimation except where evidence from re-assaying and/or check-assaying dictates. A systematic procedure utilizing several re-assays and/or check assays is in place to determine when the final assay is changed from the first gold assay.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	RC collar positions are recorded using conventional survey methods based on Trimble R10 GNSS instruments. The location of each station is referenced to state-wide network of Standard Survey Marks (SSM) established and coordinated by the Department of Land Administration (WA Government). Where regional drill hole positions are distant from the SSM network, the world wide Global Navigational Satellite System (GNSS) network is used, this includes Air Core collars. Positional checks are carried out using a combination of existing known positions (usually based on prominent landmarks) and grid referenced information such as ortho-linear rectified photogrammetry based on the Map Gird of Australia MGA94. Surface collar RL's have been validated utilizing airborne elevation survey by Arvista in 2016. Multi shot cameras and gyro units were used for down-hole survey.
	Specification of the grid system used.	Collar coordinates are recorded in MGA94 Zone 52. The difference between magnetic north (MN) and true north (TN) is 0° 14' 38". The difference between true north and GDA is zero.
	Quality and adequacy of topographic control.	Topographic control is from Digital Elevation Contours (DEM) 2017, 1m contour data.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Exploration results in this report range from 25m x 25m drill hole spacing to 50m x 50m.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The data spacing and distribution is sufficient to establish geological and/or grade continuity appropriate for the Mineral Resource and classifications to be applied.
	Whether sample compositing has been applied.	RC samples are taken as 1 m samples. For RC Resource definition drilling 1 m samples are routinely collected. DD core is sampled to geology; sample compositing is not applied until the estimation stage.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	The orientation of sampling is generally on a high angle to the main mineralisation trends as these are vertical to sub-vertical. RC Drill holes are drilled on a 60-degree angle.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	The drill orientation to mineralised structures biases the number of samples per drill hole. It is not thought to make a material difference in the Resource estimation.
Sample security	The measures taken to ensure sample security.	All samples are selected and bagged in tied numbered calico bags, grouped in larger tied plastic bags, and placed in large bulka bags with a sample submission sheet. The bulka bags are sent via freight truck to Perth, with consignment note and receipted by external and independent laboratory. All sample submissions are documented and all assays are returned via email and secure FTP. Sample pulp splits from Perth are stored at the Malaga lab. RC samples processed at ALS have had the bulk residue retained and pulp packets sent to Central Tanami Mine for storage.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	All recent NSR sample data has been extensively QAQC reviewed both internally and externally.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Central Tanami Project consists of 20 Mining Leases, 1 Access Agreement Lease and 12 Exploration Leases covering a total area of approximately 149,942 Ha. All are registered jointly in the name of Northern Star (Tanami) Proprietary Limited and Tanami Gold NL. The Project also includes 1Bore Field License. There are no heritage issues with the current operation.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	All leases and licences to operate are granted and in the order for between 2 and 20 years.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	Not Applicable, all the exploration work has been completed by NSR.
Geology	Deposit type, geological setting and style of mineralisation.	Hurricane-Repulse is a Palaeo-Proterozoic, sediment hosted vein-mineralized deposit that is part of the Granites-Tanami Inlier. Gold mineralisation is controlled by a brittle fracture-system associated with larger regional scale structures both parallel and discordant to bedding orientations and is predominantly hosted in sediment and basalt. Mineralisation can be disseminated or vein style host.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: ▪ easting and northing of the drill hole collar ▪ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar ▪ dip and azimuth of the hole ▪ down hole length and interception depth ▪ hole length.	All relevant information is part of this release.
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Not applicable to this report.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	Results are reported using a nominal 0.5 g/t Au cut-off and up to 2-meter internal waste.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	All the RC samples are 1m in length.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents are reported.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results.	All RC drill holes have been drilled on 60-degree angle.
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	Mineralisation structures are vertical to sub-vertical.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	It is interpreted that true width is approximately 50-70% of down hole intersections.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Diagrams from part of the main release.

Criteria	JORC Code explanation	Commentary
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	All results for this period are listed, including those labelled NSI (no significant intersection.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	No other meaningful data available.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Review of drilling completed is required before further work is planned.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Plans and sections of the Hurricane deposit drill hole locations are included in this report.