ASX RELEASE

REWARD MINERALS LTD

QUARTERLY REPORT FOR THE PERIOD ENDING 31 MARCH 2019

30 April 2019

ASX CODE
RWD
RWDOA

SHARE PRICE
$0.11

ISSUED CAPITAL
162,596,057 RWD
13,167,866 RWDOA

MARKET CAPITALISATION
$18M (undiluted)

DIRECTORS

Colin McCavana
Chairman

Michael Ruane
Director

Rod Della Vedova
Non-Executive Director

MANAGEMENT

Greg Cochran
Chief Executive Officer

Bianca Taveira
Company Secretary

KEY PROJECT

Lake Disappointment Project

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Highlights

- **Infill Drilling Program – Excellent Grade Profile of Shallow Lakebed Aquifer Confirmed**
- **Crystallisation Trial Update – Final Assays Received and Under Final Review**
- **Environmental Permitting – WA EPA Public Consultation Process Closed and Public Comments Summary Received**
- **Applications lodged for large acreage of new tenements in the Officer Basin considered highly prospective for Sulphate of Potash**

Corporate

Expenditure by Reward during the March 2019 quarter was $1.1 Million, with net cash at the end of the period being approximately $2.07 Million.

During the quarter the Company bade farewell to its longstanding Project Director, Mr Dan Tenardi.

Dan was with Reward for approximately 7 years and was instrumental in opening up access to the LD Project site with the development of the Willjabu Track (see picture below), as well as overseeing LD's Scoping and Pre-Feasibility Studies. At the time of its release the LD Project PFS was seen as class leading due its detail and level of accuracy (as per ASX release dated 1 May 2018 entitled "PFS Confirms LD Project as a Globally significant SOP Project").

Reward's part-time CFO, Mr Ron Chamberlain, also departed during the quarter after accepting a fulltime appointment as CFO at Alliance Mineral Assets Limited. Despite his brief period with the Company Ron made a positive impact by strengthening Reward's finance and administration functions.

LD Project Infill Drilling Program

As part of ongoing resource development work at LD, infill auger drilling was undertaken between 30 October and 13 December 2018, as reported in previous quarterly reports. A total of 61 large diameter shallow auger holes were completed over the main Lake Disappointment playa. Drilling targeted the shallow lakebed aquifer over the area of the proposed brine extraction trenches as modelled in the PFS (see ASX announcement dated 1 May 2018 – “PFS Confirms LD Project as a Globally significant SOP Project”).

The main objectives of the auger drilling program were as follows:

- Infill previously completed 2006 Geoprobe and 2015 diamond core resource drilling to provide additional geological, hydrogeological and brine chemistry data to improve the confidence in the geological and hydrogeological model;
- Install properly constructed bores to facilitate pump testing to obtain additional hydraulic data and allow ongoing monitoring in support of numerical ground water modelling and a preliminary mine schedule; and
- Provide an additional network of suitable environmental monitoring sites for the ongoing collection of baseline information.

Reward’s AM315 amphibious excavator equipped with a 200mm diameter auger drill assembly was employed to complete drilling and assist with bore construction. Helicopter support was used to transport personnel and equipment between drilling sites.

Drilling was completed on a nominal 4 x 4km grid that infilled the 5 x 5km 2006 shallow Geoprobe drilling to bring the average spacing to within 3km in the shallow lakebed aquifer (see Figure 1 overleaf for original drilling plan).

At each drill site both a shallow vertical (4-5m depth) and deeper vertical (6-7m depth) auger hole was drilled and these were used to construct bores in accordance with Australian Guidelines (i.e. National Uniform Drillers Licensing Committee 2001, Minimum Requirements for Water Bores in Australia, Third Edition, February 2012). Screened sections of the bores were completed as follows:

- Shallow bores – between the standing water table (SWL) and nominally 3.0 metres below ground level (mbgl)
- Deeper bores – nominally between 3.0 and 6.0 metres below ground level (mbgl)

A total of 30 shallow holes and 31 deeper holes were completed with bores successfully constructed for all holes. Drilling and bore completion details are summarised in Table 1 below and details are provided in Appendix 1.

Table 1. Auger Drilling and Bore Hole Completion Summary Details

	Shallow Bores				Deeper Bores			
	Drilled Depth (mbgl)	Screened Interval			Drilled Depth (mbgl)	Screened Interval		
		From (mbgl)	To (mbgl)	Length (m)		From (mbgl)	To (mbgl)	Length (m)
Min	2.5	0.1	2.3	2.0	6.2	2.8	5.8	2.7
Max	5.0	0.3	3.3	3.0	7.2	3.4	6.4	3.1
Av.	4.1	0.2	3.1	2.9	6.7	3.1	6.0	3.0

All geological logging (completed on a nominal 1-metre interval with reference samples collected in sealed plastic bags), bore construction, bore development, lithological sampling and brine sampling was either completed by or supervised by an experienced hydrogeologist who was on-site for the entire duration of the program.

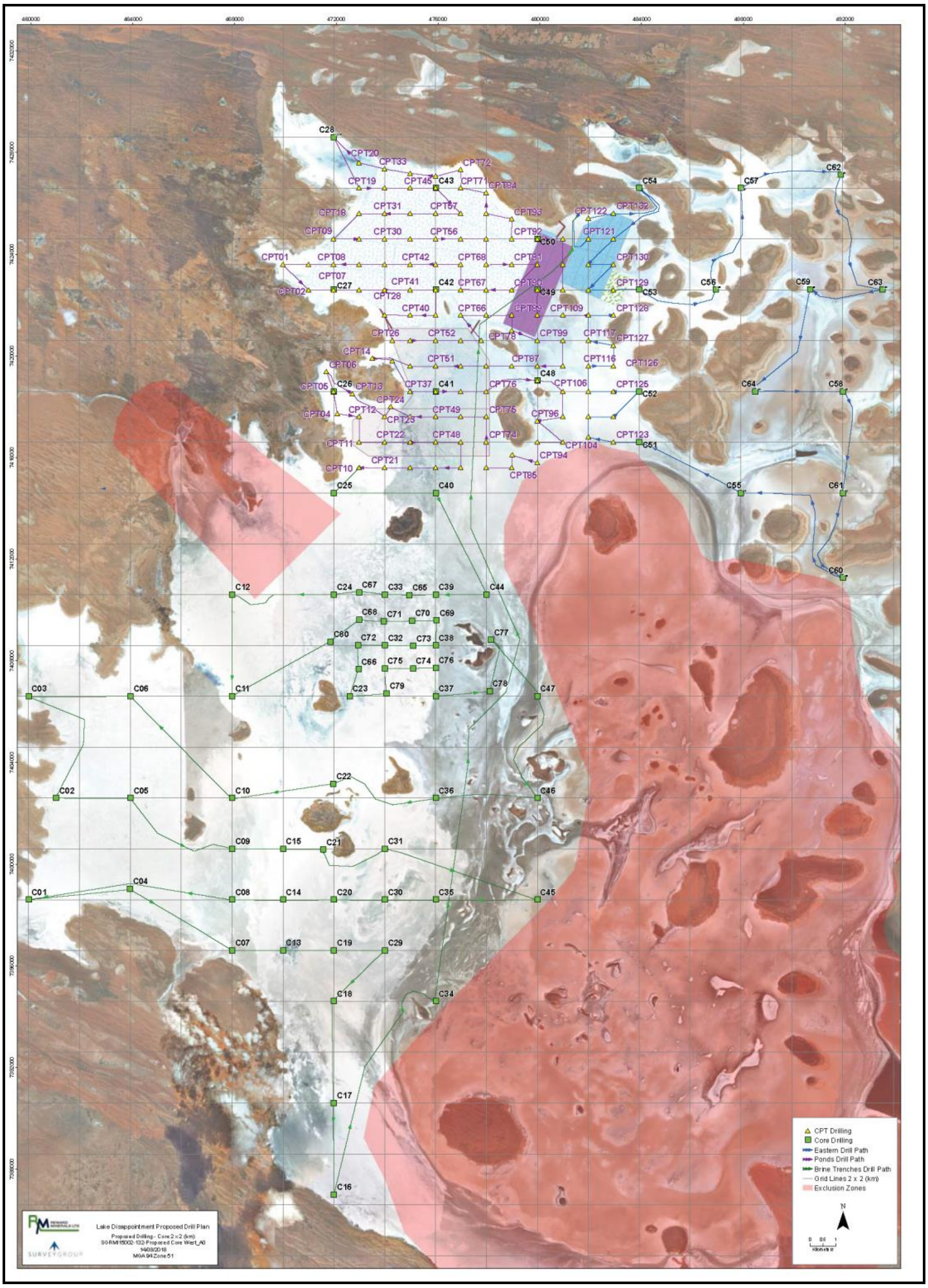

Figure 1. LD Project Original In-Fill Drilling (and CPT) Program

Following completion of the auger drilling and bore construction phase of the program, development of bores was undertaken. Development for the majority of bores was performed using a petrol powered 25mm centrifugal pump. Bores that exhibited higher flows upon initial pumping were developed using a diesel powered 50mm centrifugal pump. Bores were initially pumped an equivalent of 1-3 times their volume in order to promote brine flow through the aquifer into the gravel pack and screened section of the PVC casing. The pump's discharge was then adjusted until a stable flow rate had been achieved.

Figure 2. Auger Drilling with Surface Casing

Figure 3. A completed bore

During bore development pump flow rates were recorded using either a V-notch weir or digital flow meter (Figure 4). Development was deemed to be complete when a maximum flow rate was achieved and brine was visibly clear with no or little sediment evident in the bucket collecting the pump discharge.

A total of 40 bores were successfully developed whilst eight bores were only partially developed due to low flow rates and slow recharge. Ten bores were not developed as a result of low flow and recovery rates and limitations of the pumps. In addition, due to cement blocking the slotted PVC casing and obstructing insertion of the pump suction hose, development of another three bores could not be achieved.

Figure 4. Bore development with pump flow rates recorded by a V-notch weir

Bore hole development details are summarised in Table 2, in which it can be seen that the relative flow rates recorded during bore development are somewhat variable reflecting changes in lithological unit extent and thickness. The highest recorded flow rates correspond to the presence of abundant large gypsum crystals over the screened section of the bore whereas in contrast lowest flow rates occur in clay dominant units, where below the upper surficial unit, gypsum crystals have a marked reduction in size or are completely absent. Bores whose screened sections are predominantly through abundant evaporite and/or quartz sand and where coarse-grained gypsum is present, tended to produce moderate flow rates during bore development.

Table 2. Bore Development Summary

	Shallow Bores			Deeper Bores		
	Fully Developed	Partially Developed	Not Developed	Fully Developed	Partially Developed	Not Developed
Number	27	1	3	13	7	10
Pumped (min)	5 - 200	60	0 - 8	8 - 140	5 - 58	0 - 22
Min Flow (l/min)[1]	3.0	1.5	0	5.1	2.0	0
Max Flow (l/min)[1]	115	1.5	8.0	125	15	15

Note 1. Flow rates are purely qualitative in nature. Pump tests are required to obtain reliable hydraulic parameters

Brine samples were collected in 250ml plastic bottles upon the completion of bore development. In the case of lower yielding bores that were only partially or not developed, a sample was collected from the bore hole subsequent to abandoning development.

In addition to brine sampling of bore holes a total of 46 shallow pits were excavated across the playa surface and brine samples were taken to allow the near surface variability in brine chemistry to be assessed and comparisons made with the 2005 and 2006 sampling programs. Pit sampling details and analytical results are provided in Appendix 2.

All bore hole and pit brine samples were dispatched to ALS Metallurgy in Perth for chemical analysis of K, Ca, Na, Mg and S by induced coupled plasma mass spectrometry (ICP-MS). Analysis of chloride and specific gravity was completed in-house by Reward's chemist using Mohr Titration and liquid pycnometry respectively. Samples were submitted as two separate submissions in late-December and early-January respectively with results reviewed and finalised during the quarter. The analytical results were internally checked then compiled into a single data set.

Bore sampling results confirm the exceptional grade profile of the shallow lakebed sequence with SOP grades averaging 14.45kg/m^3 and 14.62kg/m^3 from the shallow and deeper bores respectively. The brine chemistry of the upper portion (~0-3mbgl) and lower portion (~3-6mbgl) of the saturated sediments is very consistent as shown in Table 3. Full details of the auger drilling and analytical results are provided in Appendix 1.

Table 3. Bore Hole Brine Sampling Results

	K	Ca	Mg	Na	SO_4	Cl	SOP
	(kg/m^3)						(kg/m^3)
Shallow Bore Hole Brine Sampling Results							
Min	4.65	0.15	3.76	85.30	24.45	126.30	10.36
Max	9.75	0.63	11.80	109.85	47.10	179.48	21.72
Mean	6.48	0.38	6.84	102.24	31.42	165.40	14.45
Deeper Bore Hole Brine Sampling Results							
Min	5.10	0.15	3.74	92.20	21.00	146.24	11.36
Max	9.85	0.55	12.00	109.10	43.95	181.70	21.95
Mean	6.56	0.38	6.79	102.30	30.78	166.43	14.62

A JORC Table 1 has been included in Appendix 3 which provides the full details of the sampling techniques and procedures adopted in the auger drilling program and for the shallow pits.

Geological and hydrogeological interpretation integrating results of the 2018 auger, Geoprobe and CPT drilling with historical drilling and trenching data will commence shortly to produce an updated hydrostratigraphic model for the shallow Lake Disappointment brine resource.

It is worth noting that the average SOP grade used in the LD PFS was 10kg/m^3 which was acknowledged as conservative at the time. The existing Indicated Mineral Resource has an average grade of 13.4kg/m^3 and trench pumping trials also consistently produced grades close to that average, see ASX Announcement dated 7 February 2017, "Lake Disappointment (LD) Project Confirmed as a Globally Significant Tier 1 Sulphate of Potash Deposit" and Reward's Quarterly reports dated 31 March and 30 June 2018.

The assay results of the infill drilling program provide cause to be optimistic for grade upside for the LD Project which could result in increased annual production and revenue (at the same brine abstraction rate and similar cost) or the same, PFS-level output, at a lower brine abstraction rate and therefore reduced cost.

LD Project Crystallisation Trials

The crystallisation trial that was conducted and reported upon throughout 2018 has effectively been completed. As highlighted in the previous quarterly report the high-grade brine from the two swimming pools SP1 and SP2 was drained and transferred to a third swimming pool, SP3, in December 2018 for Stage 2 potassium crystallisation (See Table 4).

On return to the LD site after the year-end break the solids in SP1 and SP2 were harvested, blended and piled to drain the entrained liquid. The drained liquid was collected and then also transferred to SP3. Subsamples weighing between 15 – 20kg each were collected from the drained piles and separately bagged for assay purposes. The subsamples were relatively coarse and were thus hammer milled to improve assay accuracy. The results of the assays conducted on the subsamples from the harvested solids from SP1 and SP2 are provided in Table 5.

The remaining solids, weighing 15.5 tonnes in total, were harvested into bulker bags and stored on site.

Table 4. SP3 Feed Brine Assays

Pool	Ca (kg/m^3)	K (kg/m^3)	Mg (kg/m^3)	Na (kg/m^3)	SO_4 (kg/m^3)	Cl (kg/m^3)
SP1	0.075	41.9	61.6	40.1	97.8	207.4
SP2	0.075	36.6	76.4	26.8	107.9	217.8
Estimated SP3 Grade	0.075	39.0	70.0	33.0	103.6	214.2

Table 5. SP1 and SP2 Drained Harvested Solids Assay Results

Date	Pool	Mass (t)	Ca (%w/w)	K (%w/w)	Mg (%w/w)	Na (%w/w)	SO_4 (%w/w)	Cl (%w/w)
8/02/19	SP1	7.78	0.014	6.4	4.1	20.2	28.8	27.7
8/02/19	SP2	7.75	0.015	7.4	4.6	19.0	28.9	28.2

The trial continued during the quarter by allowing the brine in SP3 to evaporate further until it reached approximately 130kg/m^3 magnesium to enable the crystallisation of a high potassium grade material suitable for harvesting. When that point was reached the crystallised solids (primarily kainite) were harvested, yielding 2.34 tonnes. This material has been sampled and sent to ALS Metallurgy for assay. Results have been received and are currently under final review. Once the review has been completed the detailed results of the trial will be published in a standalone release, which is anticipated within the next two weeks.

The End Brine drained from the high potassium grade harvested solids from SP3, which is high in magnesium chloride, was transferred temporarily to a fourth holding pool (SP4). This End Brine will be used in an additional evaporation trial to confirm the efficacy of the Back-Mix concept (aimed at producing high-grade potassium harvestable solids low in sodium chloride) to replicate results obtained in laboratory trials previously conducted by Reward. Analysis of the End Brine is shown in Table 6 below.

Table 6. SP3 End Brine Assay

Date	Ca (kg/m^3)	K (kg/m^3)	Mg (kg/m^3)	Na (kg/m^3)	SO_4 (kg/m^3)	Cl (kg/m^3)
8/02/19	0.075	3.2	129.3	3.0	56.0	343.5

Pond PP2 was topped up with fresh brine to get the grade back to approximately 40kg/m^3 potassium so that it can be used in the Back-Mix evaporation trial. In that trial a fifth swimming pool (SP5) will be used and brine from PP2 will be mixed with the high magnesium chloride End Brine. Success for this phase of the trial would see the crystallisation of low sodium chloride harvestable potassium solids suitable for (direct) processing to recover pure Leonite (or Schoenite depending on the ambient temperature) thence SOP without a flotation step.

LD Project Environmental Permitting Update

During the quarter Reward advised that it had received notification from the Department of Water and Environmental Regulation of Western Australia (EPA Services Division) that the LD Project's Environmental Review Document ("ERD") had been approved for release for public review.

The public review period ran for six weeks and closed on Monday, 18th March 2019. The EPA Services Division has provided Reward with a summary of the submissions made and the Company is working on responses to address these submissions. It aims to submit these responses as soon as possible during the current quarter.

In parallel with this process Reward is also preparing an additional report to address questions raised by the (Federal) Department of the Environment and Energy, with the objective of also completing this within the current quarter.

Applications lodged for prospective Officer Basin tenements

Reward applied for 5,521km^2 of Exploration Licences in the Officer Basin (Figures 5 and 6) to the east of its Lake Disappointment Project. The Company also obtained exclusive rights to an additional 3,075km^2 of Exploration Licences which are contiguous to these applications. Combined, the tenements make up a substantial land package in an area previously unexplored for buried Potash deposits.

The Officer Basin is one of a number of evaporite basins found in Western Australia that have historically been explored for oil and gas. Other basins in Western Australia, such as the Canning Basin, have also previously been explored for potash however there has been no concerted effort to explore for potash in the Officer Basin.

Based on its research and interpretation, Reward has concluded that the western part of the Officer Basin is highly prospective for hosting Sulphate of Potash (SOP) deposits at relatively shallow depths, which is the Company's prime target.

This conclusion was based on the rationale that the brine hosted SOP deposits (such as Lake Disappointment, Lake Dora, Lake Auld, etc located in central Western Australia, which are all relatively high in Potassium and Sulphate and hence amenable to SOP production) may be derived from the erosion of near surface Browne Formation evaporites. These evaporites are found in the Gibson Area (formerly Sub-basin) of the western Officer Basin.

The Licence applications are currently being processed through Department of Mines, Industry Regulation and Safety whilst Native Title discussions for access are also underway. The grant of these Tenements is expected by mid-year with field activities planned to commence thereafter.

Depending on funding a program of core holes to depths of 400 to 500 metres has been designed for completion during the 2019 field season to test the Gibson Area for shallow buried SOP mineralisation.

For further information please contact:

Greg Cochran
Chief Executive Officer
on behalf of the Board

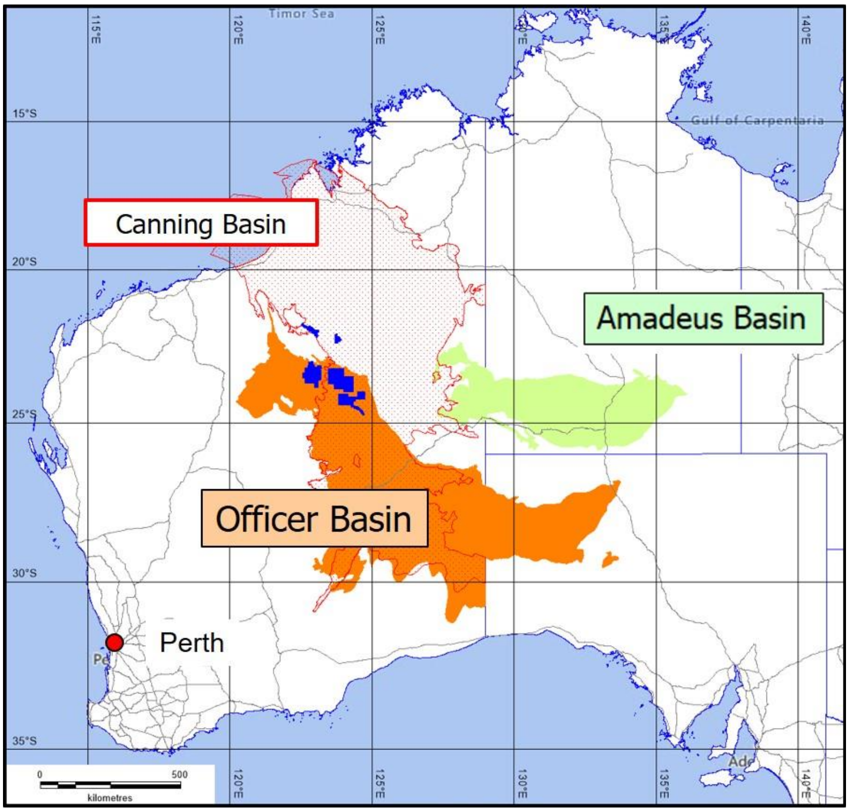

Figure 5. Location of WA's major evaporite basins Reward's tenements are in blue

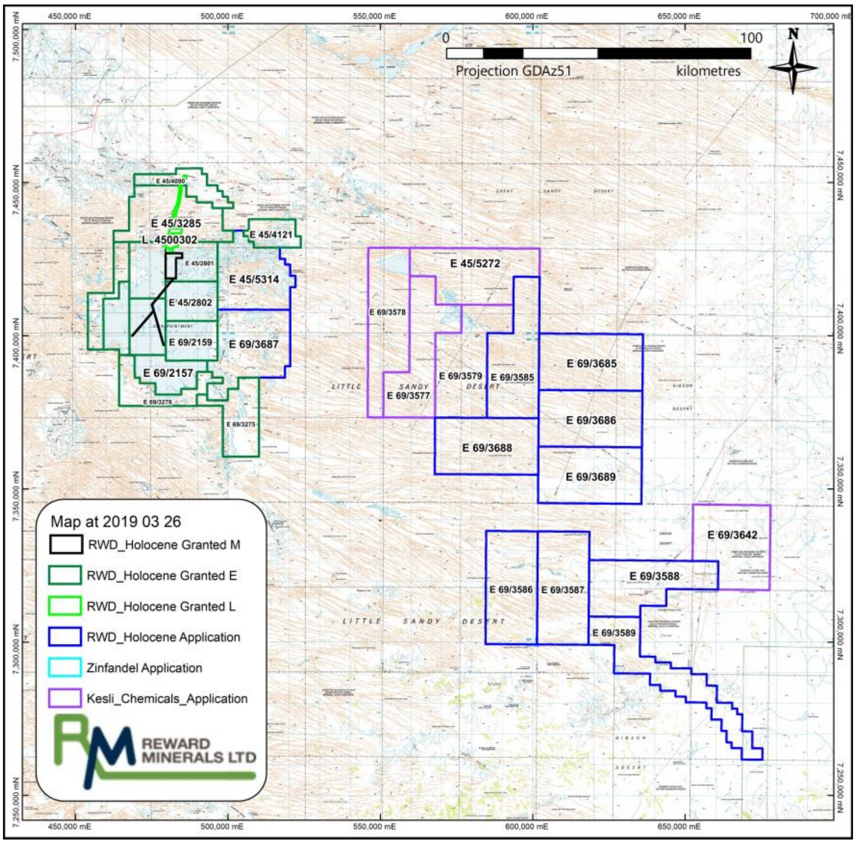

Figure 6. Officer Basin Tenements (Purple) Lake Disappointment Tenements (Green)

About Reward

Reward Minerals Ltd (Reward) is a potash-focussed exploration and development company listed on the Australian Securities Exchange (ASX Code: RWD) with a portfolio of advanced exploration projects in Australia hosting significant sulphate of potassium (SOP) resources. The Company's tenements cover approximately 10,000km^2 containing a series of highly prospective playa-style lakes and palaeovalleys known to host substantial volumes of high-density potassium rich brines.

Reward's flagship project is its 100% owned LD SOP Project, located 340 km east of Newman in the Little Sandy Desert of north-western Western Australia. The LD Project consists of a tenement package that covers over 3,000km^2 which hosts an Indicated and Inferred extractable Mineral Resource of 153Mt of SOP grading approximately 11.3kg/m^3 of SOP brine in sediments from surface to a depth of approximately 90m. The Project has a registered Indigenous Land Use Agreement with the Martu people, the traditional owners of the land, as well as a granted Mining Lease and associated Miscellaneous Licence. A Pre-Feasibility Study for the LD Project was completed at the end April 2018. Permitting is well advanced with state and federal regulators currently assessing the Project's Environmental Impact Assessment.

Competent Persons Statement

The information in this report that relates to Exploration Results is based on information compiled by Matthew Wheeler, a Competent Person who is a Member of the Australian Institute of Geoscientists. Mr Wheeler is contracted to Reward Minerals Ltd. Mr Wheeler has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Wheeler consents to the inclusion in the report of the matters based on the information in the form and context in which it appears.

The information in this report that relates to Brine Assays and Analyses is based on information compiled by Dr Michael Ruane, a Competent Person who is a Member of The Royal Australian Chemical Institute. Dr Ruane is an Executive Director of Reward Minerals. Dr Ruane has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Dr Ruane consents to the inclusion in the report of the matters based on the information in the form and context in which it appears.

Forward-Looking Statements

This document may contain certain "forward-looking statements". When used in this document, the words such as "could", "plan", "estimate", "expect", "intend", "may", "potential", "should", and similar expressions are forward-looking statements. Although Reward believes that the expectations reflected in these forward-looking statements are reasonable, such statements involve risks and uncertainties, and no assurance can be given that actual results will be consistent with these forward-looking statements.

For a more detailed discussion of such risks and uncertainties, see Reward's other ASX Releases, Presentations and Annual Reports. Readers should not place undue reliance on forward-looking statements. Reward does not undertake any obligation to release publicly any revisions to any forward-looking statement to reflect events or circumstances after the date of this ASX Release, or to reflect the occurrence of unanticipated events, except as may be required under applicable securities laws.

Appendix 1

Auger Drill Hole Completion Details

Hole ID	East MGA (Zone 51)	North MGA (Zone 51)	Inc. (Deg)	Nominal Diameter (mm)	Final Depth (mbgl)	SWL (mbgl)	Screened Interval From (mbgl)	Screened Interval To (mbgl)
LDA180001	479890	7424607	-90	200	4	0.343	0.3	3.0
LDA180002	479892	7424610	-90	200	6.8	0.343	3.0	6.0
LDA180003	479907	7422597	-90	200	4	0.258	0.3	3.3
LDA180004	479901	7422600	-90	200	6.4	0.258	3.3	6.0
LDA180005	475907	7418615	-90	200	6.6	0.153	3.0	6.0
LDA180006	475901	7418609	-90	200	3.8	0.153	0.3	3.3
LDA180007	475899	7414605	-90	200	3.7	0.103	0.3	3.3
LDA180008	475894	7414600	-90	200	6.8	0.103	3.3	6.3
LDA180009	477898	7410602	-90	200	2.5	0.282	0.3	2.3
LDA180010	477913	7410607	-90	200	7.2	0.282	3.0	6.0
LDA180011	479896	7406604	-90	200	4	0.298	0.3	3.3
LDA180012	479909	7402599	-90	200	6.8	0.282	3.0	6.0
LDA180013	479904	7402604	-90	200	4	0.282	0.3	3.3
LDA180014	475901	7402603	-90	200	4	0.341	0.3	3.0
LDA180015	475906	7402603	-90	200	6.7	0.341	3.0	6.0
LDA180016	471870	7403152	-90	200	4	0.421	0.2	3.2
LDA180017	471873	7403151	-90	200	6.7	0.421	3.1	6.1
LDA180018	467900	7402600	-90	200	4.5	0.105	0.3	3.0
LDA180019	467902	7402596	-90	200	6.8	0.105	3.0	6.0
LDA180020	463888	7402624	-90	200	6.8	0.232	3.0	6.0
LDA180021	463893	7402619	-90	200	4	0.232	0.2	3.1
LDA180022	467911	7398597	-90	200	4.5	0.310	0.3	3.3
LDA180023	467908	7398598	-90	200	6.8	0.310	2.9	6.0
LDA180024	471896	7398597	-90	200	6.8	0.360	3.0	6.0
LDA180025	471900	7398594	-90	200	4.2	0.360	0.3	3.2
LDA180026	475895	7398606	-90	200	6.8	0.220	3.0	6.0
LDA180027	475891	7398600	-90	200	4.3	0.220	0.1	3.1
LDA180028	479899	7398604	-90	200	6.8	0.410	3.0	6.0
LDA180029	479893	7398601	-90	200	4	0.410	0.2	3.2
LDA180030	475904	7394604	-90	200	6.8	0.300	3.0	6.0
LDA180031	475907	7394609	-90	200	4.1	0.300	0.1	3.1
LDA180032	471900	7394596	-90	200	6.2	0.430	3.1	6.1
LDA180033	471906	7394597	-90	200	4	0.430	0.2	3.1
LDA180034	471900	7390599	-90	200	6.8	0.340	3.3	6.3
LDA180035	471900	7390603	-90	200	4	0.340	0.1	3.1
LDA180036	471894	7386995	-90	200	4	0.630	0.1	3.1
LDA180037	471895	7387000	-90	200	6.8	0.630	3.4	6.4

Appendix 1 (continued)

Auger Drill Hole Completion Details

Hole ID	East MGA (Zone 51)	North MGA (Zone 51)	Inc. (Deg)	Nominal Diameter (mm)	Final Depth (mbgl)	SWL (mbgl)	Screened Interval	
							From (mbgl)	To (mbgl)
LDA180038	468910	7395812	-90	200	5	0.270	0.2	3.2
LDA180039	468913	7395807	-90	200	7	0.270	2.9	5.9
LDA180040	463891	7399011	-90	200	7	0.180	3.0	6.1
LDA180041	463888	7399011	-90	200	5	0.180	0.1	3.0
LDA180042	459903	7398593	-90	200	7	0.280	3.0	6.0
LDA180043	459907	7398592	-90	200	5	0.280	0.1	2.5
LDA180044	460988	7402608	-90	200	4	0.250	0.1	3.1
LDA180045	460988	7402605	-90	200	6.5	0.250	3.0	6.0
LDA180046	459892	7406600	-90	200	6.5	0.430	3.1	6.1
LDA180047	459896	7406597	-90	200	4	0.430	0.1	3.1
LDA180048	463899	7406601	-90	200	6.5	0.200	3.1	6.1
LDA180049	463895	7406602	-90	200	4	0.200	0.2	3.0
LDA180050	467901	7406600	-90	200	6.5	0.260	3.1	6.1
LDA180051	467897	7406599	-90	200	4	0.260	0.2	3.0
LDA180052	467893	7410603	-90	200	6.5	0.330	3.1	6.1
LDA180053	467893	7410598	-90	200	4	0.330	0.1	3.1
LDA180054	471914	7410599	-90	200	6.5	0.100	2.8	5.8
LDA180055	471910	7410598	-90	200	4.3	0.100	0.1	3.0
LDA180056	472516	7406595	-90	200	6.5	0.144	3.0	6.0
LDA180057	472513	7406608	-90	200	4.5	0.144	0.1	3.0
LDA180058	475895	7406600	-90	200	6.4	0.240	3.0	6.0
LDA180059	475896	7406604	-90	200	4	0.240	0.1	3.1
LDA180060	475903	7410584	-90	200	6.5	0.180	3.0	6.0
LDA180061	475904	7410579	-90	200	4.2	0.180	0.1	3.0

Auger Drill Hole Brine Sampling Chemical Analysis

Hole ID	From (mbgl)	To (mbgl)	Status[1]	Ca (mg/l)	K (mg/l)	Mg (mg/l)	Na (mg/l)	SO_4[2] (mg/l)	Cl (mg/l)	SOP[3] (kg/m^3)	SG	TDI[4] (mg/l)	Ionic Balance[5] (%)
LDA180002	3.00	6.00	FDEV	400	6,050	6,350	108,400	25,500	170,618	13.48	1.202	317,318	3.10
LDA180003	0.26	3.30	FDEV	425	5,800	6,350	108,750	25,950	170,618	12.92	1.200	317,893	-1.13
LDA180004	3.00	6.00	FDEV	425	6,100	6,650	108,350	28,650	166,186	13.59	1.199	316,361	1.65
LDA180005	3.00	6.00	UDEV	350	7,950	12,000	108,950	33,600	181,697	17.71	1.214	344,547	0.25
LDA180006	0.15	3.10	UDEV	300	8,200	11,800	107,550	34,500	179,481	18.27	1.215	341,831	0.76
LDA180007	0.10	3.10	FDEV	375	6,800	6,800	109,400	25,650	172,833	15.15	1.207	321,858	-9.08
LDA180008	3.00	6.00	FDEV	375	6,800	7,000	109,100	25,500	172,833	15.15	1.205	321,608	2.06
LDA180009	0.28	2.40	NDEV	450	5,300	5,550	106,450	26,700	163,970	11.81	1.195	308,420	-0.85
LDA180010	Not Assayed												
LDA180011	0.30	3.30	FDEV	625	4,650	3,760	85,300	24,450	126,301	10.36	1.154	245,086	9.57
LDA180012	3.00	6.00	FDEV	450	5,250	4,990	97,950	26,850	155,107	11.70	1.184	290,597	-5.62
LDA180013	0.30	3.30	FDEV	450	5,300	5,000	96,900	27,450	155,107	11.81	1.184	290,207	-8.23
LDA180014	0.34	3.20	FDEV	475	4,850	4,770	93,000	27,000	152,891	10.81	1.183	282,986	1.59
LDA180015	3.00	6.00	FDEV	450	4,950	5,100	93,150	28,650	152,891	11.03	1.186	285,191	1.84
LDA180016	0.30	3.00	FDEV	425	5,700	5,300	103,250	28,350	166,186	12.70	1.193	309,211	-0.44
LDA180017	3.00	6.10	PDEV	375	6,300	5,650	104,600	31,350	166,186	14.04	1.200	314,461	-4.09
LDA180018	0.11	3.00	FDEV	350	6,750	7,450	103,250	33,300	175,049	15.04	1.206	326,149	-7.02
LDA180020	3.00	6.00	NDEV	350	8,200	9,950	104,650	29,850	181,697	18.27	1.209	334,697	-2.09
LDA180021	0.23	3.00	FDEV	350	8,250	10,500	102,650	32,850	177,265	18.38	1.210	331,865	-1.19
LDA180022	0.31	3.00	FDEV	375	6,100	6,700	106,300	34,800	170,618	13.59	1.200	324,893	-7.27
LDA180023	3.00	6.00	FDEV	375	6,150	6,900	101,950	32,250	170,618	13.70	1.200	318,243	-5.40
LDA180024	3.00	6.00	NDEV	450	5,100	5,600	100,500	25,800	161,754	11.36	1.189	299,204	0.64
LDA180025	0.36	3.00	FDEV	400	5,350	6,350	99,850	28,500	163,970	11.92	1.194	304,420	-0.17
LDA180026	3.00	6.00	NDEV	375	5,650	6,500	102,850	29,700	168,402	12.59	1.198	313,477	-1.71
LDA180027	0.22	2.80	FDEV	375	5,900	6,650	103,600	28,050	166,186	13.15	1.200	310,761	-1.53
LDA180028	3.00	6.00	PDEV	500	5,350	3,880	92,200	28,800	146,244	11.92	1.173	276,974	2.71
LDA180029	0.41	3.00	FDEV	500	5,300	3,920	93,350	28,050	146,244	11.81	1.173	277,364	2.57
LDA180030	3.00	6.00	FDEV	550	5,150	3,740	98,100	21,000	157,323	11.47	1.180	285,863	0.51
LDA180031	0.30	3.10	FDEV	475	5,250	4,800	97,700	27,000	150,675	11.70	1.180	285,900	2.99
LDA180032	3.10	6.10	PDEV	450	5,400	4,710	98,800	27,900	157,323	12.03	1.185	294,583	-4.21
LDA180033	0.43	3.10	FDEV	375	5,700	6,550	102,150	32,400	163,970	12.70	1.197	311,145	-5.49
LDA180034	3.30	6.30	NDEV	425	6,100	5,250	104,500	28,800	166,186	13.59	1.194	311,261	0.89
LDA180035	0.34	3.10	FDEV	375	6,100	6,600	101,400	31,650	163,970	13.59	1.197	310,095	-2.84
LDA180036	0.63	3.00	NDEV	300	6,600	6,350	104,100	36,750	166,186	14.70	1.204	320,286	-1.83

Auger Drill Hole Brine Sampling Chemical Analysis (continued)

Hole ID	From (mbgl)	To (mbgl)	Status[1]	Ca (mg/l)	K (mg/l)	Mg (mg/l)	Na (mg/l)	SO_4[2] (mg/l)	Cl (mg/l)	SOP[3] (kg/m^3)	SG	TDI[4] (mg/l)	Ionic Balance[5] (%)
LDA180037	3.40	6.40	FDEV	325	6,550	6,700	102,700	36,900	166,186	14.59	1.203	319,361	-1.69
LDA180038	0.27	3.20	FDEV	350	6,800	6,800	103,950	31,650	170,618	15.15	1.204	320,168	-1.68
LDA180039	3.00	6.00	PDEV	375	6,650	6,450	104,400	29,250	172,833	14.82	1.202	319,958	-4.97
LDA180040	3.10	6.10	FDEV	350	6,700	7,650	102,500	33,150	175,049	14.93	1.204	325,399	-6.96
LDA180041	0.18	3.00	FDEV	350	6,700	7,450	104,350	33,600	170,618	14.93	1.205	323,068	-4.69
LDA180042	3.00	6.00	FDEV	400	5,900	5,700	100,350	31,950	159,539	13.15	1.193	303,839	-1.11
LDA180043	0.28	2.50	FDEV	375	5,950	5,700	99,450	32,400	161,754	13.26	1.195	305,629	-0.64
LDA180044	0.25	3.10	FDEV	150	9,750	9,500	106,000	42,300	175,049	21.72	1.221	342,749	-2.23
LDA180045	3.00	6.00	FDEV	150	9,800	10,600	103,500	42,900	175,049	21.83	1.221	341,999	-0.82
LDA180046	3.10	6.10	FDEV	375	7,150	6,550	97,850	35,700	150,675	15.93	1.190	298,300	1.86
LDA180047	0.43	3.10	FDEV	275	7,950	6,750	101,250	47,100	155,107	17.71	1.202	318,432	-5.23
LDA180048	3.10	6.10	FDEV	175	9,850	9,900	105,150	43,950	175,049	21.95	1.220	344,074	-2.94
LDA180049	0.20	3.00	FDEV	200	9,250	9,750	103,000	41,850	170,618	20.61	1.218	334,668	-1.34
LDA180050	3.10	6.10	NDEV	375	7,350	6,350	104,150	31,350	168,402	16.38	1.201	317,977	0.14
LDA180051	0.26	3.00	FDEV	325	7,650	7,600	103,400	29,250	172,833	17.04	1.206	321,058	-2.41
LDA180052	3.20	6.20	FDEV	350	6,850	6,100	100,050	32,850	161,754	15.26	1.198	307,954	-1.76
LDA180053	0.33	3.20	FDEV	375	6,950	6,100	101,100	35,100	161,754	15.48	1.197	311,379	-2.40
LDA180054	3.10	5.90	FDEV	350	6,900	7,100	103,950	30,300	170,618	15.37	1.206	319,218	-2.47
LDA180055	0.10	3.00	FDEV	350	7,050	7,250	106,000	30,300	172,833	15.71	1.207	323,783	-3.32
LDA180056	3.00	6.00	NDEV	400	6,350	7,850	102,150	29,700	172,833	14.15	1.202	319,283	-1.59
LDA180057	0.14	3.00	FDEV	375	6,250	7,650	103,150	30,000	170,618	13.93	1.201	318,043	-0.05
LDA180058	Not Sampled												
LDA180059	0.24	3.00	NDEV	400	6,000	7,950	101,000	32,100	168,402	13.37	1.199	315,852	-5.08
LDA180060	3.00	6.00	PDEV	375	6,650	8,050	101,250	28,950	170,618	14.82	1.203	315,893	-2.49
LDA180061	0.18	3.00	FDEV	375	6,700	7,900	101,900	30,150	175,049	14.93	1.203	322,074	-5.07

Notes:

1) Borehole development status at time of sampling: FDEV – fully developed, PDEV – partially developed, NDEV – not undeveloped
2) SO_4 values are obtained by multiplying the sulphur concentrations by a factor of 3.00
3) Calculated from potassium concentrations (SOP = K x 2.228)
4) Total Dissolved Ions (TDI) = Σ Ca, K, Mg, Na, SO_4, Cl and approximates Total Dissolved Solids (TDS) as determined by evaporation
5) Ionic Balance is calculated on % difference based on milliequivalents per litre (meq/l) as follows: [(Σ cations – Σ anions)/(Σ cations + Σ anions)]*100

Abbreviations: mbgl – metres below ground level, SWL – standing water table

Appendix 2

Pit Location and Depth Details

Pit ID	East MGA (Zone 51)	North MGA (Zone 51)	SWL (mbgl)	Depth (mbgl)
C01	459896	7398584	0.28	0.50
C02	460985	7402611	0.25	0.45
C03	459885	7406595	0.43	0.70
C04	463883	7406595	0.18	0.55
C06	463899	7406595	0.20	0.50
C07	468899	7406595	0.27	0.50
C08	467902	7406595	0.31	0.46
C10	463889	7406595	0.28	0.45
C11	467890	7406595	0.26	0.55
C12	467903	7406595	0.33	0.60
C16	471902	7406595	0.63	0.73
C17	471890	7406595	0.60	1.20
C18	471899	7406595	0.43	0.70
C20	471905	7406595	0.36	0.49
C23	472520	7406595	0.14	0.48
C24	471921	7406595	0.10	0.40
C25	471861	7406595	0.12	0.42
C26	471890	7406595	1.10	1.40
C27	471966	7406595	0.48	0.71
C28	471893	7406595	0.52	0.79
C34	475914	7406595	0.30	0.40
C35	475896	7406595	0.22	0.54
C37	475903	7406595	0.24	0.41
C39	476906	7406595	0.18	0.62
C40	475893	7406595	0.10	0.48
C41	475905	7406595	0.31	0.64
C42	475907	7406595	0.21	0.56
C43	475901	7406595	0.46	0.71
C45	479899	7406595	0.41	0.65
C48	479907	7406595	0.11	0.50
C49	479891	7406595	0.26	0.45
C50	479891	7406595	0.23	0.65
C51	483900	7406595	0.12	0.40
C52	483900	7406595	0.40	0.75
C53	483895	7406595	0.25	1.30
C54	483900	7406595	0.20	0.80
C55	487900	7406595	0.30	0.57
C56	486900	7406595	0.35	1.50
C57	487900	7406595	0.29	1.10
C58	491900	7406595	0.56	0.70
C59	490614	7406595	0.30	0.65
C60	491913	7406595	0.70	1.30
C61	491930	7406595	0.60	0.83
C62	491821	7406595	0.35	0.90
C63	493455	7406595	0.38	0.70
C64	488471	7406595	0.43	0.85

Pit Brine Sampling Chemical Analysis

Pit ID	From (mbgl)	To (mbgl)	Ca (mg/l)	K (mg/l)	Mg (mg/l)	Na (mg/l)	SO4[1] (mg/l)	Cl (mg/l)	SOP[2] (kg/m^3)	SG	TDI[3] (mg/l)
C01	0.28	0.50	400	5,600	5,800	99,400	28,050	166,186	12.48	1.199	305,436
C02	0.25	0.45	175	9,450	9,250	114,350	42,750	183,912	21.05	1.233	359,887
C03	0.43	0.70	200	8,250	7,000	104,350	47,850	159,538	18.38	1.209	327,188
C04	0.18	0.55	400	6,450	6,750	109,050	28,650	172,833	14.37	1.209	324,133
C06	0.20	0.50	325	7,450	7,100	110,900	33,450	181,697	16.60	1.213	340,922
C07	0.27	0.50	375	6,350	6,400	107,450	30,900	166,186	14.15	1.204	317,661
C08	0.31	0.46	425	5,550	6,550	106,800	28,050	163,970	12.37	1.199	311,345
C10	0.28	0.45	275	8,050	9,900	116,250	35,550	188,344	17.94	1.228	358,369
C11	0.26	0.55	375	6,650	6,950	105,100	29,250	175,049	14.82	1.204	323,374
C12	0.33	0.60	400	6,850	6,200	103,050	32,550	161,754	15.26	1.200	310,804
C16	0.63	0.73	325	6,100	5,850	107,700	33,150	161,754	13.59	1.204	314,879
C17	0.60	1.20	325	6,050	9,450	110,700	31,200	181,697	13.48	1.219	339,422
C18	0.43	0.70	375	5,550	6,150	99,250	31,950	161,754	12.37	1.200	305,029
C20	0.36	0.49	450	5,150	6,450	105,350	26,100	161,754	11.47	1.196	305,254
C23	0.14	0.48	400	6,450	7,650	102,550	28,350	172,833	14.37	1.203	318,233
C24	0.10	0.40	375	7,350	7,550	108,950	30,450	181,697	16.38	1.212	336,372
C25	0.12	0.42	325	8,250	8,700	108,700	33,600	179,481	18.38	1.216	339,056
C26	1.10	1.40	400	6,450	4,360	99,800	30,600	157,323	14.37	1.191	298,933
C27	0.48	0.71	350	7,850	8,250	104,050	34,500	172,833	17.49	1.205	327,833
C28	0.52	0.79	800	3,750	1,710	84,300	16,350	126,301	8.36	1.145	233,211
C34	0.30	0.40	650	4,500	3,800	84,800	22,200	135,165	10.03	1.163	251,115
C35	0.22	0.54	375	5,600	6,450	111,600	30,000	170,618	12.48	1.207	324,643
C37	0.24	0.41	400	6,000	8,050	100,350	30,150	166,186	13.37	1.199	311,136
C39	0.18	0.62	375	6,650	8,300	103,050	30,900	175,049	14.82	1.205	324,324
C40	0.10	0.48	350	7,850	8,000	115,250	34,500	181,697	17.49	1.218	347,647
C41	0.31	0.64	400	6,800	7,900	104,150	28,800	175,049	15.15	1.203	323,099
C42	0.21	0.56	425	6,550	5,900	105,050	27,300	172,833	14.59	1.195	318,058
C43	0.46	0.71	300	9,600	12,150	101,350	36,000	177,265	21.39	1.216	336,665
C45	0.41	0.65	550	5,000	3,540	86,600	24,900	135,165	11.14	1.168	255,755
C48	0.11	0.50	375	6,650	7,100	105,050	26,700	177,265	14.82	1.205	323,140
C49	0.26	0.45	425	6,200	6,700	109,000	27,750	172,833	13.81	1.201	322,908
C50	0.23	0.65	400	6,450	6,350	104,100	27,150	170,618	14.37	1.198	315,068
C51	0.12	0.40	425	5,400	6,150	103,350	28,050	168,402	12.03	1.196	311,777
C52	0.40	0.75	450	4,500	7,200	94,950	27,450	157,323	10.03	1.185	291,873
C53	0.25	1.30	525	4,550	6,200	96,450	23,400	155,107	10.14	1.180	286,232
C54	0.20	0.80	550	4,850	4,300	98,300	23,400	155,107	10.81	1.176	286,507
C55	0.30	0.57	625	4,700	3,790	83,500	23,400	126,301	10.47	1.153	242,316

Pit Brine Sampling Chemical Analysis (continued)

Pit ID	From (mbgl)	To (mbgl)	Ca (mg/l)	K (mg/l)	Mg (mg/l)	Na (mg/l)	SO4[1] (mg/l)	Cl (mg/l)	SOP[2] (kg/m^3)	SG	TDI[3] (mg/l)
C56	0.35	1.50	500	3,950	6,700	92,250	24,450	155,107	8.80	1.179	282,957
C57	0.29	1.10	475	4,750	5,150	102,650	22,050	168,402	10.58	1.191	303,477
C58	0.56	0.70	650	4,800	3,250	86,650	20,550	132,949	10.69	1.156	248,849
C59	0.30	0.65	700	4,100	3,990	88,950	18,900	139,596	9.13	1.159	256,236
C60	0.70	1.30	625	5,250	3,600	82,000	24,600	128,517	11.70	1.153	244,592
C61	0.60	0.83	600	5,350	3,580	87,400	25,950	132,949	11.92	1.159	255,829
C62	0.35	0.90	850	3,750	2,030	87,550	14,400	132,949	8.36	1.154	241,529
C63	0.38	0.70	525	5,650	3,750	97,150	23,850	148,459	12.59	1.175	279,384
C64	0.43	0.85	625	5,200	3,250	95,600	20,550	148,459	11.59	1.169	273,684

Notes:

1) SO_4 values are obtained by multiplying the sulphur concentrations by a factor of 3.00

2) Calculated from potassium concentrations (SOP = K x 2.228)

3) Total Dissolved Ions (TDI) = Σ Ca, K, Mg, Na, SO_4, Cl and approximate Total Dissolved Solids (TDS) determined by evaporation

Abbreviations: mbgl – metres below ground level, SWL – standing water table

Appendix 3

JORC Table 1 for Infill Drilling Program

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	*Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.* *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* *Aspects of the determination of mineralisation that are Material to the Public Report.* *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	The sampling program involved the collection of brine samples and lithological samples. Brine sampling completed subsequent to development of constructed bores. Brine samples from the shallow surficial sediments were also collected from hand-dug pits – these were single grab samples. 61 vertical large diameter auger holes and 46 shallow pits were completed. A total of 58 brine samples collected from constructed bores and 46 brine samples collected from pits were submitted for chemical analysis. Lithological samples at nominal 1-metre intervals were obtained by auger drilling methods. Test pits were not logged.
Drilling techniques	*Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	Auger drilling conducted using Reward's AM315 amphibious excavator equipped with a 200mm diameter auger drill assembly attached to the boom. All holes drilled vertically and depths referenced to metres below ground level (mbgl). Lithological samples were collected on a nominal 1-metre downhole intervals.
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.* *Measures taken to maximise sample recovery and ensure representative nature of the samples.* *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	Brine samples were collected from bores constructed within the completed large diameter auger holes. Bores were constructed so that only the slotted casing section contained gravel pack in the annulus between the wall of the auger hole and the PVC casing. The remainder of the hole was cased with plain PVC and the corresponding annulus of the hole plugged with cement. The bores were sufficiently pumped during development to ensure that the brine samples collected immediately after pumping was completed are representative of the target zone. Brine recovery from the test pits was good and is representative of the upper-most surficial aquifer. Lithological logging was completed on a nominal 1-metre downhole basis. Material obtained from each drill run (lithological sample) was removed manually from the auger flights and laid out in piles on the ground at each drill site. Lithological sample recovery was high in all completed auger holes.
Geologic Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.* *The total length and percentage of the relevant intersections logged.*	Geological logging of sediment samples was completed by qualified geologist/hydrogeologist. All lithological samples collected during auger drilling were qualitatively logged at a nominal 1-metre interval to gain an understanding of the lithological variability. Reference lithological samples stored in zip lock plastic bags. No logging was conducted for the shallow, hand-dug test pits.

Criteria	JORC Code explanation	Commentary
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.* *If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.* *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* *Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.* *Whether sample sizes are appropriate to the grain size of the material being sampled.*	Bore hole brine samples were obtained by collecting the pump discharge into a 20 litre bucket. Two separate brine samples (primary and field duplicate) from the bucket were collected in 250ml plastic bottles. Bottles were completely filled to ensure they contained little or no air. All sampled bottles were sealed by securely taping the lids to the bottle. The bores were appropriately constructed and sufficiently pumped during bore development to ensure that the brine samples collected immediately upon completion of pumping are representative of the target zone chemistry and not influenced by the effects of evaporation. Test pits were allowed to fill with brine after excavation, and the sample was collected directly from the pit immediately thereafter. Two separate brine samples (primary and field duplicate) were collected in 250ml plastic bottles. Bottles were completely filled to ensure they contained little or no air. All sampled bottles were sealed by securely taping the lids to the bottle. All samples were kept cool until delivery to Reward's Perth office. Upon receipt samples were sorted and reconciled against the Master Dispatch record generated on-site. Sub-sampling for assay: a portion of the primary brine sample was diluted with deionized water using a dilution factor of 50 (49:1 / diluent:brine). A separate aliquot of the resultant diluted solution was taken and submitted to ALS Metallurgy in Perth for chemical analysis. All other samples remained at Reward's premises in Perth.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	Brine samples were analysed for K, Na, Mg, Ca, S using ICP-MS, with chloride determined by Mohr titration and specific gravity by liquid pycnometry. No preparation was performed by the laboratory other than removal of a separate aliquot from the "as received" diluted solution. Laboratory equipment is calibrated with standard solutions. The average error in the ionic balance for analysed bore hole samples was 1.7% with a maximum recorded error of 9.6%. Ionic balances of 80% of analyses were within +/-5.0% and 90% were within +/-5.6% – indicating that there is a high degree of confidence in the accuracy of the analyses.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.* *The use of twinned holes.* *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* *Discuss any adjustment to assay data.*	Independent verification of significant brine grade intercepts was obtained by collecting brine samples prior to, during and at completion of development pumping of some of the bore holes. Twinning of 2018 CPT and Geoprobe Holes Were Completed as follows: (i) auger holes were completed at 3 CPT hole locations that were also twinned by a Geoprobe hole (ii) additionally auger holes were completed at 7 Geoprobe drill hole locations. Data entry is performed in the field to minimize transposition errors. Brine assay results are received from the laboratory in digital format to prevent transposition errors. Geological and assay results are stored in a project database. All chemical analyses were multiplied by the dilution factor of 50 to convert them from the diluted concentration to original concentration. Adjustment to assay also includes calculation of sulphate from the ICP-MS sulphur analysis (SO_4 = S x 3.00) and calculation of sulphate of potash from ICP-MS potassium analysis (SOP = K x 2.228).

Criteria	JORC Code explanation	Commentary
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* *Specification of the grid system used.* *Quality and adequacy of topographic control.*	The location of bore holes and test pits was determined with a handheld GPS. The accuracy achieved with a handheld GPS is appropriate for the reporting of Exploration Results. All co-ordinates are referenced to the Geodetic Datum of Australia (GDA94) and quoted in Universal Transverse Mercator (UTM) Eastings and Northings projected in Zone 51 Map Grid of Australia (MGA94). Bore hole and pit elevations were not recorded as hand-held GPS elevations generally have inaccuracies 3-4 times that of the x/y co-ordinates. Previous DGPS-RTK spot elevations completed on a 1km x 1km grid vary between 326.8 – 328.5 m AHD over the area of the auger drilling.
Data spacing and distribution	*Data spacing for reporting of Exploration Results.* *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* *Whether sample compositing has been applied.*	In addition to the 2018 auger, Geoprobe and CPT drilling, geological control is available from drilling completed by Reward in 2006, 2014 and 2015. Drill spacing varies between approximately 1km and 17km; spacing has been designed to provide brine samples over the extents of the Lake Disappointment main playa. Integrating effects of groundwater flow and the availability of historical drilling to support geological interpretation, the spacing is adequate to establish the geological and brine grade continuity appropriate for Indicated and Inferred Mineral Resources. No sample compositing has been applied other than for purposes of presenting brine grades in Table 3.
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	All drill holes are vertical which is appropriate given the flat-lying nature of the lake and underlying sedimentary sequence and the integrating effects of groundwater flow and the presence of mineralised brine in all intersected units.
Sample security	*The measures taken to ensure sample security.*	Laboratory chain-of-custody procedures have been used for all brine and lithological samples.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	No third-party audits or reviews have been undertaken.

Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	The Lake Disappointment Potash Project is 100% owned by Reward Minerals Ltd via its wholly-owned subsidiary Holocene Pty Ltd, with Project tenure via the following tenements granted under the Mining Act of Western Australia. E45/2801-2803, E45/3285-3286, E45/4090, E45/4121, E69/2156-2159, E69/3275-3276, L45/302, M45/1227 and L46/128 (Application). RWD has an Indigenous Land Use Agreement (ILUA) with the Western Desert Lands Aboriginal Corporation on behalf of the Martu Traditional Owners of the lands held under Native Title Determination WA (2002) FCA 2002 in respect of the Lake Disappointment Project.
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	No previous exploration had been undertaken on the Lake Disappointment Potash Project prior to that of RWD.
Geology	*Deposit type, geological setting and style of mineralisation.*	The deposit comprises potassium and sulphate rich brines that can be extracted to recover sulphate of potassium (SOP) salts. The brine is contained within saturated sediments below the lake surface and in sediments adjacent to the lake. The lake sits within a broader palaeovalley system.
Drill hole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* • *easting and northing of the drill hole collar* • *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* • *dip and azimuth of the hole* • *down hole length and interception depth* • *hole length.* *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	Information is provided in tabular format in Appendix 1 and 2 of this announcement. Bore hole and pit elevations were not recorded as hand-held GPS elevations generally have inaccuracies 3-4 times that of the x/y co-ordinates. Previous DGPS-RTK spot elevations completed on a 1km x 1km grid vary between 326.8 – 328.5 m AHD over the area of the auger drilling.
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	No minimum or maximum grade cut-offs have been applied. No data aggregation has been used to report bore hole and pit sample assay results presented in Table 3. No metal equivalents have been reported.
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.* *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	All drill holes are vertical and approximately orthogonal to the intersected flat-lying sedimentary sequence. Vertical drill hole intercepts are interpreted to represent the true thickness of the deposit. Brine samples have been collected from single intervals within the constructed bores and show brine concentrated in potassium, magnesium and sulphate occur within shallow saturated sediments across over the extents of the playa lake.
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Refer to Figure 1 in this announcement.

Criteria	JORC Code explanation	Commentary
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	All pertinent results have been reported.
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	All material exploration data reported.
Further work	*The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).* *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	Geological and hydrogeological interpretation integrating results of the 2018 auger, Geoprobe and CPT drilling with historical shallow pit sampling, drilling and trenching data to produce an updated hydrostratigraphic model.

Appendix 4

JORC Table 1 for Crystallisation Trials

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	*Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.*	Feed brine for the reported pond evaporation trial was pumped from a 1000m long x 1.5m wide x 2m deep trench dug into Lake Disappointment surface sediments. Feed brine samples were collected at approximately weekly intervals into clean 250 ml plastic sample bottles for analysis. The evaporation ponds comprised two membrane (HDPE) lined ponds placed on the lake surface plus three above ground swimming pools. Brine samples were taken manually at regular intervals from respective evaporation ponds for analysis. These samples were transported to Perth for analysis. When received, samples were placed in a 40°C water bath to dissolve any crystallised salts. Aliquats of brine were diluted x50 with distilled water (typically 10mls diluted to 500mls in volumetric flask) prior to dispatch to ALS Metallurgical Laboratories in Balcatta. Samples were assayed for Ca, K, Mg, Na and total S. Generally, Cl and SG analyses were undertaken in-house by RWD. Pond brine for a particular evaporation stage was evaporated to pre-determined K/Mg concentration to evaluate the composition of salts crystallised from evaporation of brine analysing within a certain composition range. When brines reached the trigger stage composition, the pond was drained and salts harvested manually (in this trial), stockpiled to drain further and then bagged for transport to Perth. Samples of harvest salt material were hammer milled to -6mm for sampling prior to analysis. Selected samples from each harvest solids collection were thoroughly mixed by hand in a large tub and then subsampled for dilution. Dilution of solid samples involved dissolving 20gms in 1 litre of distilled water using a volumetric flask.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Pond brine samples were collected below surface. Harvested solids were homogenised, piled to allow further drainage and then sampled along the surface of the piled material. Multiple samples were collected. Selected samples were hammer milled for more accurate subsampling then diluted for submission for assay. Variability of subsample analyses were within acceptable ranges.
	Aspects of the determination of mineralisation that are Material to the Public Report.	Not applicable.
	In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay').	Not applicable.

Criteria	JORC Code explanation	Commentary
	In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	
Drilling techniques	*Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	Not applicable.
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.* *Measures taken to maximise sample recovery and ensure representative nature of the samples.* *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	Not applicable.
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	No logging was carried out/required during the evaporation trial. Samples collected were noted on log sheets. Bagged solid samples were numbered and weighed.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Not applicable.
	The total length and percentage of the relevant intersections logged.	Not applicable.
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.*	Not applicable.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	Brine samples sent to Perth were heated in a water bath at 40°C to dissolve any crystallised salts, thoroughly mixed by inversion and then sampled for dilution via auto-pipette. Dilutions involved diluting 10ml aliquots to 250mls using distilled water. Diluted brine samples were sent to ALS Metallurgy for ICP analyses. Selected bags of hammer milled harvest solids were homogenised by hand in a large tub and subsampled for dilution. The 20gm subsamples were diluted with 1 litre of distilled water using a volumetric flask. Diluted solid based samples were also sent to ALS Metallurgy for ICP analyses. A small selection of hammer milled solid samples were also provided to the ALS Metallurgy - Mineralogy Dept for XRD analyses in order to identify the crystalline species present. These submitted solid samples were minus 6mm material collected exactly as described above. ALS Mineralogy dried the samples submitted for XRD analyses very carefully at 38°C over a number of days (to retain 'waters of crystallisation'). These 'dried' samples were then hand ground in a mortar and pestle prior to mounting for the XRD measurements.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The brine collection and dilution techniques used are appropriate for ICP analyses. The homogenising and subsampling of harvest solids are regarded as practical under the prevailing conditions on site. The solids dissolution ratios are also appropriate for ICP analyses. For XRD analyses directly on submitted (hammer milled) harvest solids, the careful 38°C drying and hand grinding of

Criteria	JORC Code explanation	Commentary
		these solids by ALS Metallurgy prior to XRD analyses are regarded as practical and best practice for the type of material being analysed.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	See above. Analyses of multiple subsamples indicated low level variability in the harvest samples.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.	See above. Multiple solids samples collected and assayed.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	See above.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	Procedures utilised are regarded as satisfactory for the work being undertaken – see subsampling and sample preparation above. ICP analyses were conducted by ALS Metallurgy on both diluted brine and harvest solids samples to determine Ca, Mg, K, Na and total Sulphur. SO_4 values were calculated by RWD assuming all S was present as SO_4. Chloride assays on both diluted brine and harvest solids samples were carried out in-house (by RWD) via $AgNO_3$ titration using a K_2CrO_4 indicator endpoint. XRD analyses were also conducted on a small selection of harvest solids samples. These analyses must be considered semi-quantitative especially with brine derived 'crystalline' solids. There are analytical limitations resultant from the sample type, sample crystallinity and the gentle preparation steps required prior to analysis (waters of hydration).
	For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	See above.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	ALS Metallurgy use procedures compliant with the ISO 9001 Quality Management System. As such, the use of internal checks via blanks and duplicates etc are a part of their standard protocols. ALS Metallurgy is used to conduct check analyses on in-house chloride assays on a regular basis.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.*	See sampling techniques above.
	The use of twinned holes.	Not applicable.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. *Discuss any adjustment to assay data.*	Initial data recorded onto log sheets. This data subsequently transferred to digital form in either Word or Excel. Paperwork stored either onsite or in Perth, digital files stored on Company PCs in Perth.
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* *Specification of the grid system used.* *Quality and adequacy of topographic control.*	Not applicable.

Criteria	JORC Code explanation	Commentary
Data spacing and distribution	*Data spacing for reporting of Exploration Results.* *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* *Whether sample compositing has been applied.*	Not applicable.
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	Data provided does not relate to geological structure.
Sample security	*The measures taken to ensure sample security.*	All samples were clearly marked and secured onsite before being transported by company vehicle to Perth. Samples were prepared in Perth lab prior to submitting to ALS for assay. All submitted samples were clearly labelled with Company identifiers. Assay samples were hand delivered to ALS by RWD staff.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	The Company and independent Consultants undertake detailed and regular data quality assurance, reviews and cross checks to verify the accuracy of all data and results.

Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	The Lake Disappointment Potash Project is 100% owned by Reward Minerals Ltd via its wholly-owned subsidiary Holocene Pty Ltd with Project tenure via the following tenements granted under the Mining Act of Western Australia. E45/2801-2803, E45/3285-3286, E45/4090, E45/4121, E69/2156-2159, E69/3275-3276, L45/302, M45/1227 and L46/128 (Application). RWD has an Indigenous Land Use Agreement (ILUA) with the Western Desert Lands Aboriginal Corporation on behalf of the Martu Traditional Owners of the lands held under Native Title Determination WA (2002) FCA 2002 in respect of the Lake Disappointment Project.
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	No previous exploration had been undertaken on the Lake Disappointment Potash Project prior to that of RWD.
Geology	*Deposit type, geological setting and style of mineralisation.*	Not applicable.
Drill hole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* • *easting and northing of the drill hole collar* • *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* • *dip and azimuth of the hole* • *down hole length and interception depth* • *hole length.* *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	Not applicable.
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	Not applicable due to exploration results being applicable to a brine and not a solid. No low- or high-grade cut-off grade has been implemented due to the consistent grade of the brine recovered.
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.* *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	Not applicable due to results relating to brine only being extracted.
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Not applicable.

Criteria	JORC Code explanation	Commentary
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	Reporting is balanced and more detailed results will be shortly released on completion of final internal reviews.
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Not applicable.
Further work	*The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).* *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	Next phase of the program involves the testing of the Back-Mix concept as explained in the report.

Tenement Holdings as at 31 March 2019

Tenement	Status	RWD Ownership at Quarter End	% Interest Acquired During the Quarter	% Interest Disposed During the Quarter
Lake Disappointment, Western Australia				
E45/2801	Granted	100%	-	-
E45/2802	Granted	100%	-	-
E45/2803	Granted	100%	-	-
E45/3285	Granted	100%	-	-
E45/3286	Granted	100%	-	-
E45/4090	Granted	100%	-	-
E45/4121	Granted	100%	-	-
E69/2156	Granted	100%	-	-
E69/2157	Granted	100%	-	-
E69/2158	Granted	100%	-	-
E69/2159	Granted	100%	-	-
E69/3275	Granted	100%	-	-
E69/3276	Granted	100%	-	-
L45/302	Granted	100%	-	-
M45/1227	Granted	100%	-	-
Runton, Western Australia				
ELA45/5314	Application	100%	-	-
Gibson, Western Australia				
ELA69/3585	Application	100%	-	-
ELA69/3586	Application	100%	-	-
ELA69/3587	Application	100%	-	-
ELA69/3588	Application	100%	-	-
ELA69/3589	Application	100%	-	-
ELA69/3685	Application	100%	100%	-
ELA69/3686	Application	100%	100%	-
ELA69/3687	Application	100%	100%	-
ELA69/3688	Application	100%	100%	-
ELA69/3689	Application	100%	100%	-
Balfour, Western Australia				
LA46/128	Application	100%	-	-
Dora, Western Australia				
E45/4292	Granted	100%	-	-
ELA45/4321	Application	100%	-	-
ELA45/4488	Application	100%	-	-