



ASX ANNOUNCEMENT 10 OCTOBER 2019

DRILLING STARTS AT AUSTRALIAN VANADIUM PROJECT

Australian Vanadium targeting significant mine life extensions with new programs of Resource drilling.

KEY POINTS

- Drilling to start at Australian Vanadium Project to further define the high-grade zone
- New infill drilling programs planned over southern portion of Inferred Resource base
- A Mineral Resource update will be completed at the end of each drill program
- Targeting conversion of current Inferred Resources to Indicated Resources
- Low cost of conversion of Resources, focusing on shallow infill drilling
- Increase in Indicated Resources will provide opportunity and flexibility for DFS scheduling
- Potential to significantly increase the current 17 year planned mine life or scale of the Project
- Drilling will not affect existing Feasibility Study and approval activities

Australian Vanadium Limited (ASX: AVL, "the Company" or "AVL") is pleased to announce that it has commenced drilling within the current Pre-feasibility Study (PFS) pit design to further refine the structural model and provide additional input to the resource and geotechnical data supporting the pit design. The Company also intends to conduct a series of resource development drilling programs along its southern strike extensions at The Australian Vanadium Project ("the Project") over the next 12 to 18 months. Existing drilling has confirmed the continuation of the Project's high-grade vanadium magnetite deposits in fault blocks to the south of the close-spaced drilling which are the subject of the Company's ongoing feasibility studies. A Mineral Resource update will be completed at the end of each program.

The new drilling complements the Feasibility Study work currently underway. The recently completed \$6.6 million capital raising by the Company ensures that funds are available for the completion of works required, with some of the funds being used for drilling.

Currently the southern resource blocks within AVL's leases contain Inferred Resources of 55.3 Mt at 0.97% V_2O_5 . Infill drilling is planned to further define and where possible, re-categorise vanadium bearing mineralisation to the Indicated Resource category.

The resource development drilling of these southern blocks will provide important flexibility to the Project. The options present the opportunity to increase the mine life or scale of the Project; and to define more transitional and fresh ore close to the surface, increasing scheduling flexibility during mining.

The objective of the drilling is to significantly increase the potential mine life or scale of the Project to beyond the current 17 years as defined in the PFS (see ASX announcement dated 19 December 2018 'Gabanintha Pre-Feasibility Study and Maiden Ore Reserve') and enable better informed decisions on the optimal scale and mine life of the Project.





Figure 1 The Australian Vanadium Project

The identification of additional surface transitional ore along the strike allows more options for satellite pits to be included in the mine schedule, increasing the flexibility in mining. The option to blend-in greater percentages of transitional and fresh material earlier in the mine schedule could also be beneficial. The PFS contemplates the mining and processing of 1.4 million tonnes of ore per annum.

Managing Director, Vincent Algar commented, "The Australian Vanadium Project has unique geology and metallurgy. AVL holds a significant strike position and we have the opportunity to use that to define new Reserves and increase the mine life substantially. Our targeted project investors will appreciate a de-risked, large resource base, with built-in flexibility for shallow open pit mining."

RESOURCES

The PFS defined an Ore Reserve of 18.24 Mt at $1.04 \text{W} \ \text{V}_2 \text{O}_5$ which is comprised of a Proved Reserve of 9.82 Mt at $1.07 \text{W} \ \text{V}_2 \text{O}_5$ and a Probable Reserve of 8.42 Mt at $1.01 \text{W} \ \text{V}_2 \text{O}_5$. The Reserve is derived (see APPENDIX 1) from 10.2 Mt at $1.11 \text{W} \ \text{V}_2 \text{O}_5$ Measured Resources and 12.1 Mt at $1.05 \text{W} \ \text{V}_2 \text{O}_5$ Indicated Resources. In addition to the Resources that form the current Reserve, there are 3.3 Mt of Indicated Resources at $1.04 \text{W} \ \text{V}_2 \text{O}_5$ and $8.9 \ \text{Mt}$ of Inferred Resources at $0.98 \text{W} \ \text{V}_2 \text{O}_5$ beneath the current pit optimisation. The total Resource (Measured, Indicated and Inferred) in the fault blocks where the pit is designed is $36.3 \ \text{Mt}$ at $1.04 \text{W} \ \text{V}_2 \text{O}_5$.

APPENDIX 2 summarises the current Mineral Resource estimate by High-Grade (HG), Low Grade domains (LG2-5) and Transported domains (Trans 6-8) by each fault block.



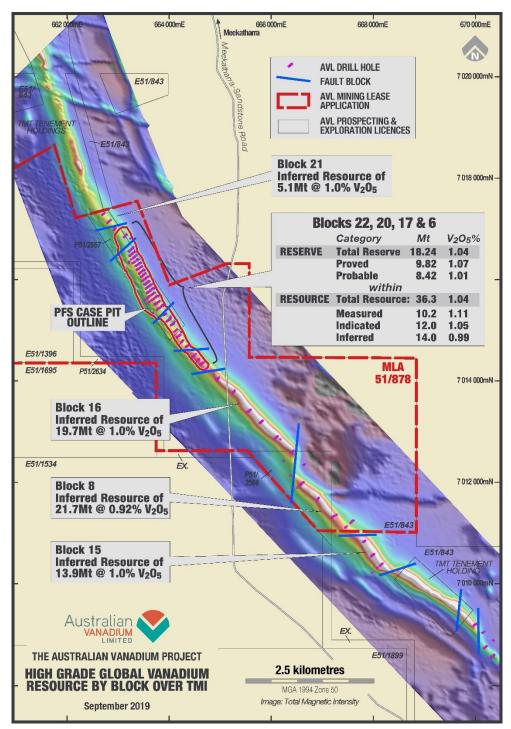


Figure 2 Total Magnetic Intensity Showing Mineral Resources by Major Fault Block

As shown in Figure 2, AVL's 100% controlled Mineral Resource extends over an 11.5km strike of the known magnetite bearing rocks. Mineralisation in the Indicated and Measured Resource category are all located in the northern portions of AVL's tenements. Drill spacing in this area ranges from 80m x 30m on average through the larger fault block 20, increasing to 130m x 30m on average in fault blocks 17 and 6. The southern area of the tenements were drilled at a spacing of over 400m x 25m on average in 2008 and resulted in defined mineralisation in the Inferred Resources category.

The target economic mineralisation at The Australian Vanadium Project is a massive vanadiferous titanomagnetite horizon located at the base of a thick gabbro sequence. The high-grade zone ranges in thickness



from 15 to 20m and dips between 45 and 60 degrees to the southwest. The high-grade zone 'HG 10' is separated occasionally by faulting and interpreted into kilometre-scale blocks. The planned infill drilling programs will focus on the higher grade and thicker portions of HG zone. The current PFS takes in Fault blocks 22, 20,17 and 6. Drilling to commence during October will infill the area where Fault blocks 20 and 17 intersect to an average spacing of 40m by 30m, to refine the structural model and evaluate any geotechnical impacts on the current PFS pit design. The southern blocks, 16, 15 and 8 will be the focus of the planned drilling programs. Table 1 below is a Resource table by Fault block.

The total Resources in these blocks are as follows:

Block	Area	Category	Current Resource Tonnage	Current Resource Grades					
Block #			Mt	V2O5 %	Fe %	TiO ₂ %	SiO ₂ %	Al ₂ O ₃ %	LOI %
22	la alt	Measured	1.0	1.10	41.7	12.5	10.4	9.3	4.9
22	In pit	Indicated	0.7	1.09	40.8	12.6	11.4	9.6	5.2
22	extents	Inferred	2.6	1.02	40.0	12.9	12.1	10.4	5.7
20	In pit	Measured	9.2	1.11	42.9	12.7	10.2	7.9	3.8
20	extents	Indicated	5.9	1.09	44.4	12.1	9.7	7.2	3.1
20	exterits	Inferred	4.7	1.08	43.4	12.0	10.6	7.7	3.4
17	In pit	Indicated	5.5	1.01	43.6	11.5	11.4	7.8	3.7
17	extents	Inferred	1.5	0.95	42.7	10.9	12.7	7.9	3.8
6	In pit extents	Inferred	5.2	0.91	40.1	10.4	14.7	8.4	3.3
Subtotal	Within PFS		36.3	1.04	42.6	11.9	11.3	8.1	3.7
Pit	pit extents								
21	North of pit	Inferred	5.1	1.00	41.7	11.4	12.3	7.8	3.9
16	South of pit	Inferred	19.7	1.00	42.5	11.0	11.3	7.2	2.3
8	South of pit	Inferred	21.7	0.92	40.5	11.0	12.7	8.4	3.8
15	South of pit	Inferred	13.9	1.00	45.1	11.3	9.1	6.3	3.7
Subtotal	Outside pit extents		60.4	0.97	42.29	11.11	11.37	7.45	3.29
Sum			96.7	1.00	42.4	11.4	11.3	7.7	3.5

Table 1 Resources by Fault Block

Block	Strike Extent (m)	Current Inferred Resource Tonnage to 140m Below Surface	Current Resource Inferred Grade to 140m Below Surface						
		Mt	V ₂ O ₅ %	Fe %	TiO ₂ %	SiO ₂ %	Al ₂ O ₃ %	LOI %	
8	1,590	16.8	0.94	41.3	11.3	11.7	8.1	3.8	
15	850	9.4	0.99	45.0	11.3	9.0	6.3	3.9	
16	2,220	12.5	1.01	42.9	11.2	10.9	7.1	2.3	
Sum		38.6	0.98	42.7	11.2	10.8	7.3	3.3	

Table 2 Target Blocks for Resource Definition Drilling to 140m Below Surface



RESOURCE DEFINITION DRILLING

As can be seen in Figure 2 and shown in Table 2, expansion of the Reserve base at the Project is achievable with low cost infill drilling through the southern Fault blocks. The outcome of conversion of any Resources to mining Reserves will add additional feedstocks to the Project life. The Project's processing plant is being designed to treat a blend of material types that are representative of the near surface mineralisation, which will include vanadiferous-titano-magnetites with a range of magnetic yields and concentrate grades. Opportunities to develop satellite pits can result in wider choices in scheduling which improves plant performance.

Mining costs increase significantly with increased mining depth, primarily due in this case to higher stripping ratio and the need to stockpile low-grade ore, which will not be processed in the early part of the mine's life or possibly ever (depending on economics). The planned Resource definition drilling programs are specifically targeting areas in the south which are interpreted as having greater thickness and shallower dip, to maximise the conversion to Indicated Resources. Only the top 140 metres will be targeted initially (surface ~450 m RL). The deposits are open at depth.

The PFS assumed an annual mining rate of ore to the plant at 1.4Mt per annum and the total mine life was constrained by the quantum of Indicated and Measured Resources.

EXPLORATION STRATEGY

The strategy for improving the quality of the southern Resources will be to initially drill the top 140m of the current Inferred Resources and where possible convert the Resources to the Indicated category.

Further follow up drilling may be required to extend the highest value areas which are a combination of width, dip, grade and magnetic susceptibility, hence having the highest contained vanadium per metre vertically and likely the most recoverable.

Significant previous drilling results in the southern blocks are outlined in Table 3, with intercepts defined as greater than 8 metres over $1.0\%~V_2O_5$. The location of the drillholes within the southern blocks are shown in Figure 3.

A series of drill programs, Program of Works (POW) applications and heritage clearances, where required, are being planned or underway. The first program at one of the southern blocks will commence in Q4 of this year or early Q1 in 2020. A Mineral Resource update will be completed at the end of each program.

Hole ID	Metre	Metre	Interval	Fault	V2O5%	Fe%	TiO₂%	SiO₂%	Al₂O₃%	LOI%
	From	То		Block						
GDH904	28	48	20	8	1.11	42.8	12.4	11.5	8.4	3.4
GDH905	102	128	26	8	1.00	43.9	11.4	11.3	7.9	3.7
GRC0062	42	65	23	8	1.05	43.0	12.3	9.0	7.5	3.7
GRC0064	23	45	22	8	1.06	42.3	12.8	10.0	8.1	3.5
GRC0068	17	34	17	8	1.11	46.7	13.1	7.0	5.9	2.3
GDH907	36	52	16	15	1.12	47.6	12.6	7.7	6.0	2.5
GRC0043	15	29	14	15	1.02	43.7	11.7	12.1	7.0	-
GRC0044	46	55	9	15	1.20	50.2	13.0	3.8	4.4	-
GRC0045	46	79	33	15	1.08	46.9	12.0	7.1	5.3	-
GRC0047	62	77	15	15	1.06	46.9	11.7	7.4	6.8	-



Hole ID	Metre	Metre	Interval	Fault	V2O5%	Fe%	TiO₂%	SiO₂%	Al₂O₃%	LOI%
	From	То		Block						
GRC0052	64	78	14	15	1.01	47.7	11.7	7.0	4.9	3.2
GRC0033	30	46	16	16	1.22	46.8	13.9	5.9	5.6	-
GRC0038	54	69	15	16	1.12	45.6	12.8	6.8	6.4	-
GRC0039	38	49	11	16	1.13	50.1	12.5	4.7	5.2	-
GRC0040	57	67	10	16	1.18	51.5	13.2	3.7	4.6	-
GRC0078	82	99	17	16	1.20	51.7	12.9	2.9	3.9	0.4
GRC0119	36	50	14	16	1.09	44.7	12.0	8.8	6.4	3.0
GRC0157	11	23	12	16	1.21	42.6	13.1	11.3	6.3	3.3
GRC0158	113	133	20	16	1.01	45.3	11.1	10.8	5.5	2.5

Table 3 Intercepts from Southern Blocks at greater than 8 m over 1.0% V_2O_5

Subsequent programs will be spaced out over 2020 and 2021. Work will be conducted in tandem with the ongoing DFS and subsequent engineering and construction work, subject to financing.



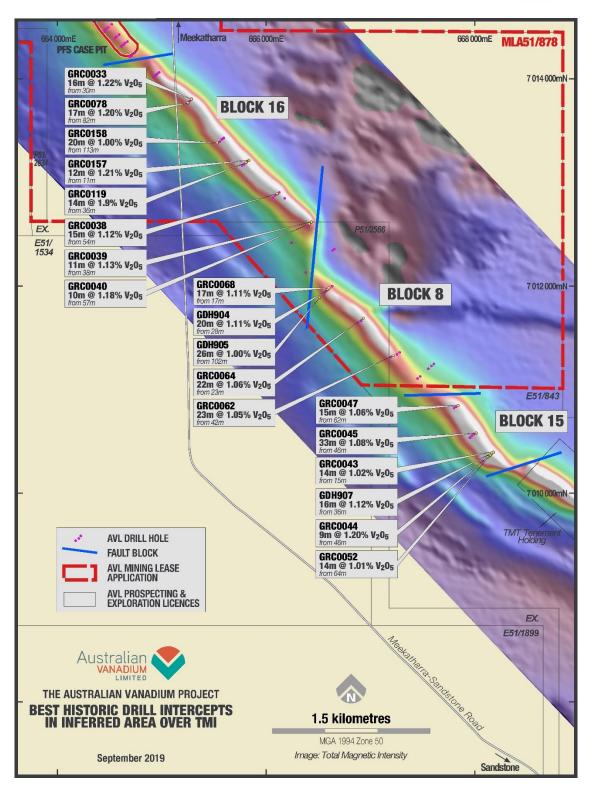
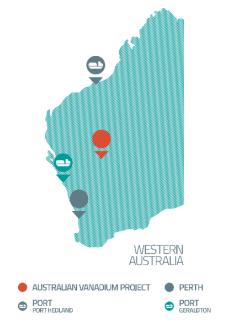


Figure 3 Historic Intercepts greater than 8 m over 1.0% V₂O₅ in Southern Blocks



For further information, please contact:

Vincent Algar, Managing Director +61 8 9321 5594



COMPETENT PERSON STATEMENT – EXPLORATION RESULTS AND EXPLORATION TARGETS

The information in this report that relates to Exploration Results and Exploration Targets is based on and fairly represents information and supporting documentation prepared by Mr Brian Davis (Consultant with Geologica Pty Ltd). Mr Davis is a shareholder of Australian Vanadium Limited. Mr Davis is a member of the Australasian Institute of Mining and Metallurgy and has sufficient experience of relevance to the styles of mineralisation and types of deposits under consideration, and to the activities undertaken to qualify as Competent Persons as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Specifically, Mr Davis consents to the inclusion in this report of the matters based on his information in the form and context in which they appear.

COMPETENT PERSON STATEMENT — MINERAL RESOURCE ESTIMATION

The information in this announcement that relates to Mineral Resources is based on and fairly represents information compiled by Mr Lauritz Barnes, (Consultant with Trepanier Pty Ltd) and Mr Brian Davis (Consultant with Geologica Pty Ltd). Mr Davis is a shareholder of Australian Vanadium Limited. Mr Barnes and Mr Davis are members of the Australasian Institute of Mining and Metallurgy (AusIMM) and Mr Davis is a member of the Australian Institute of Geoscientists, both have sufficient experience of relevance to the styles of mineralisation and types of deposits under consideration, and to the activities undertaken to qualify as Competent Persons as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Specifically, Mr Barnes is the Competent Person for the estimation and Mr Davis is the Competent Person for the database, geological model and site visits. Mr Barnes and Mr Davis consent to the inclusion in this announcement of the matters based on their information in the form and context in which they appear.

COMPETENT PERSON STATEMENT — ORE RESERVES

The scientific and technical information in this announcement that relates to ore reserves estimates for the Project is based on information compiled by Mr Roselt Croeser, an independent consultant to AVL. Mr Croeser is a member of the Australasian Institute of Mining and Metallurgy. Mr Croeser has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a competent person as defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Mr Croeser consents to the inclusion in the announcement of the matters related to the ore reserve estimate in the form and context in which it appears.



APPENDIX 1

The Australian Vanadium Project – Mineral Resource estimate by domain and resource classification using a nominal $0.4\%~V_2O_5$ wireframed cut-off for low-grade and nominal $0.7\%~V_2O_5$ wireframed cut-off for high-grade (total numbers may not add up due to rounding).

Zone	Classification	Mt	V₂O₅ %	Fe %	TiO₂ %	SiO₂ %	Al ₂ O ₃ %	LOI %
HG 10	Measured	10.2	1.11	42.7	12.6	10.2	8.0	3.9
	Indicated	12.1	1.05	43.8	11.9	10.6	7.6	3.5
	Inferred	74.5	0.97	42.1	11.2	11.6	7.6	3.4
	Sub-total	96.7	1.00	42.4	11.4	11.3	7.7	3.5
LG 2-5	Measured	-	-	-	-	-	-	-
	Indicated	28.6	0.50	24.6	6.9	27.5	17.9	8.6
	Inferred	53.9	0.49	25.3	6.7	27.5	16.4	7.3
	Sub-total	82.5	0.49	25.1	6.8	27.5	16.9	7.7
Transported	Measured	-	-	-	-	-	-	-
6-8	Indicated	-	-	-	-	-	-	-
	Inferred	4.4	0.65	28.2	7.2	24.7	16.7	8.5
	Sub-total	4.4	0.65	28.2	7.2	24.7	16.7	8.5
Total	Measured	10.2	1.11	42.7	12.6	10.2	8.0	3.9
	Indicated	40.7	0.66	30.3	8.3	22.5	14.8	7.1
	Inferred	132.7	0.77	34.8	9.2	18.5	11.5	5.1
	Sub-total	183.6	0.76	34.3	9.2	18.9	12.1	5.5



APPENDIX 2

The Australian Vanadium Project – Mineral Resource estimate by domain and resource classification using a nominal $0.4\%~V_2O_5$ wireframed cut-off for low-grade and nominal $0.7\%~V_2O_5$ wireframed cut-off for high-grade (total numbers may not add up due to rounding by fault block).

	Block #	Cat	Mt	V ₂ O ₅ %	Fe %	TiO ₂ %	SiO ₂ %	Al ₂ O ₃ %	LOI %
	20	Measured	9.2	1.11	42.9	12.7	10.2	7.9	3.8
	22		1.0	1.1	41.7	12.5	10.4	9.3	4.9
		Subtotal	10.2	11.1	42.7	12.6	10.2	8.0	3.9
	17	Indicated	5.5	1.01	43.6	11.5	11.4	7.8	3.7
	20		5.9	1.09	44.4	12.1	9.7	7.2	3.1
	22		0.7	1.09	40.8	12.6	11.4	9.6	5.2
		Subtotal	12.1	1.05	43.8	11.9	10.6	7.6	3.5
	6	Inferred	5.2	0.91	40.1	10.4	14.7	8.4	3.3
HG 10	8		21.7	0.92	40.5	11.0	12.7	8.4	3.8
¥	15		13.9	1.00	45.1	11.3	9.1	6.3	3.7
	16		19.7	1.00	42.5	11.0	11.3	7.2	2.3
	17		1.5	0.95	42.7	10.9	12.7	7.9	3.8
	20		4.7	1.08	43.4	12.0	10.6	7.7	3.4
	21		5.1	1.00	41.7	11.4	12.3	7.8	3.9
	22		2.6	1.02	40.0	12.9	12.1	10.4	5.7
		Subtotal	74.5	0.97	42.1	11.2	11.6	7.6	3.4
	Sum	HG Total	96.7	1.0	42.4	11.4	11.3	7.7	3.5
	17	Indicated	7.7	0.49	26.1	6.7	26.9	18.0	8.6
	20		18.1	0.51	24.1	7.0	27.8	17.8	8.4
	22		2.9	0.50	23.6	6.8	27.0	17.8	9.9
		Subtotal	28.6	0.5	24.6	6.9	27.5	17.9	8.6
	6	Inferred	4.0	0.46	25.2	6.3	28.1	16.4	7.9
	8		6.4	0.50	23.6	6.6	28.1	18.9	7.9
ru.	15		4.7	0.49	23.5	6.4	29.1	17.1	3.5
LG 2-5	16		18.6	0.52	26.8	6.9	26.5	14.3	5.9
_	17		3.0	0.48	25.7	6.7	27.5	17.7	8.5
	20		5.4	0.51	24.7	6.9	27.9	17.4	8.2
	21		5.6	0.45	25.4	6.6	26.7	17.6	9.9
	22		6.2	0.43	24.4	6.5	29.0	17.5	9.5
		Subtotal	53.9	0.49	25.3	6.7	27.5	16.4	7.3
	Sum	LG Total	82.5	0.49	25.1	6.8	27.5	16.9	7.7
	8	Inferred	0.9	0.73	33.5	8.4	19.4	12.3	8.2
	15		0.3	0.73	42.9	8.6	13.0	10.1	5.3
	17		0.0	0.53	21.5	7.5	31.7	19.7	8.2
00	20		1.1	0.55	16.4	7.4	31.6	24.1	10.9
-9 pa	21		0.3	0.50	28.3	5.7	24.9	16.6	10.2
orte	17		0.0	0.59	33.6	6.0	26.6	11.9	5.7
Transported 6-8	20		1.6	0.66	29.9	6.6	25.3	15.9	7.4
Tr	22		0.1	0.47	22.6	5.1	27.2	16.6	12.0
	20		0.1	0.50	30.9	5.1	26.3	15.1	7.5
	Sum	Transported Total	4.4	0.65	28.2	7.2	24.7	16.7	8.5
		Measured	10.2	1.1	42.7	12.6	10.2	8.0	3.9
-		Indicated	40.7	0.66	30.3	8.3	22.5	14.8	7.1
Total		Inferred	132.7	0.77	34.8	9.2	18.5	11.5	5.1
		Grand Total	183.6	0.76	34.3	9.2	18.9	12.1	5.5

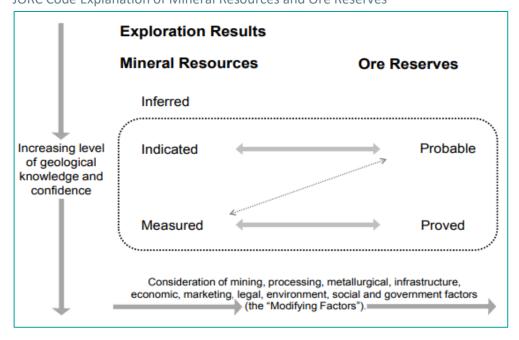


APPENDIX 3Collar Details for Southern Block Historic Intercepts

Hole ID	MGA 94 East	MGA 94 North	RL	Hole Depth (metres)	Hole Type	Dip	Azimuth
GDH904	666,566	7,011,966	465	90.5	Diamond	-59	50
GDH905	666,487	7,011,893	465	161.3	Diamond	-59	46
GRC0062	667,193	7,011,333	465	72	RC	-60	50
GRC0064	666,906	7,011,694	465	54	RC	-60	50
GRC0068	666,577	7,011,982	465	42	RC	-60	50
GDH907	668,132	7,010,371	464	99.5	Diamond	-61	52
GRC0043	668,146	7,010,382	464	61	RC	-60	50
GRC0044	668,119	7,010,369	464	67	RC	-60	50
GRC0045	667,986	7,010,571	464	79	RC	-60	50
GRC0047	667,810	7,010,838	464	79	RC	-60	50
GRC0052	668,102	7,010,345	463	111	RC	-60	50
GRC0033	665,261	7,013,799	464	55	RC	-60	50
GRC0038	666,079	7,012,897	465	73	RC	-60	50
GRC0039	666,412	7,012,610	466	55	RC	-60	50
GRC0040	666,391	7,012,594	466	69	RC	-60	50
GRC0078	665,225	7,013,769	464	102	RC	-60	50
GRC0119	665,783	7,013,193	465	60	RC	-60	50
GRC0157	665,802	7,013,211	465	30	RC	-60	50
GRC0158	665,505	7,013,375	465	138	RC	-60	50



APPENDIX 4JORC Code Explanation of Mineral Resources and Ore Reserves



APPENDIX 5

Reserve Statement

Reserve Classification	Tonnes	V ₂ O ₅ %	V₂O₅ Produced t
Proved	9,820,000	1.07	65,000
Probably	8,420,000	1.01	56,000
Total	18,240,000	1.04	121,000

The key inputs or modifying factors include:

- Ore mining recovery of 95%.
- Mining dilution of 5%.
- A nominal plant throughput of 1.45 Mt/a based on a blend of ore types.
- An overall Life of Mine (LOM) V_2O_5 process recovery of 64%. This was based on metallurgical testwork and refinery flowsheet benchmarks
- Geotechnical parameters based on an independent consultant report by Dempers & Seymour.
- CMB costs averaging A\$17.09/t were used for pit optimisation and is based on preliminary plant
 design and cost estimates by Wood, including expected power and consumable usage and an
 overhead cost (general and admin) of A\$2.24/t
- Total mining costs averaging \$3.50/t ore and waste mined (LOM).
- Pit designs based on optimal discounted cash flow pit shell using V₂O₅ revenue price of US\$8/lb.
- Gross royalty of 5.0% which includes 2.5% WA Government Royalty and additional royalties.



APPENDIX 6

2019 Drilling Progress Update with latest Mineral Resource Estimate dated November 2018 (2012 JORC Code – Table 1)

Section 1: Sampling Techniques and Data

Criteria	JORC Code Explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.	The Australian Vanadium Project deposit was sampled using diamond core and reverse circulation (RC) percussion drilling from surface. During 2019 a further 30 PQ diamond drill holes have been completed to collect metallurgy sample for a plant pilot study. 12 are drilled down-dip into the high-grade zone. These were complimented by an additional 18 PQ diamond drill tails on RC precollars, drilling vertically. The down dip holes are measured by hand-held XRF at 50 cm intervals to inform metallurgy characterisation but will not form part of any resource estimation update unless certified laboratory analysis is completed on a cut portion of the drill core. The 18 diamond tails were cut and a ¼ of the PQ sized core was sent for analysis. At the time of the latest Mineral Resource estimation (November 2018), a total of 250 RC holes and 20 diamond holes (6 of which are diamond tails) were drilled into the deposit. 59 of the 251 holes were either too far north or east of the main mineralisation trend or excised due to being on another tenancy. One section in the southern part of the deposit (holes GRC0156, GRC0074, GRC0037 and GRC0038) was blocked out and excluded from the resource due to what appeared to be an intrusion which affected the mineralised zones in this area. Of the remaining 191 drillholes, one had geological logging, but no assays and one was excluded due to poor sample return causing poor representation of the mineralised zones. Two diamond holes drilled during 2018 were not part of the resource estimate, as they were drilled into the western wall for geotechnical purposes. The total metres of drilling available for use in the interpretation and grade estimation was 17,530m at the date of the most recent resource estimate. The initial 17 RC drillholes were drilled by Intermin Resources NL (IRC) in 1998. These holes were not used in the 2015 and 2017 estimates due to very long unequal sample lengths and a different grade profile from subsequent drilling. 31 RC drillholes were drilled by Greater Pacific
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	PQ core from diamond tails was ¼ cored and sent for assay. The remaining core went to make up the pilot plant metallurgical sample. The Down Dip 2019 PQ core has not been sampled. Handheld XRF machines being used to take ½ metre measurements on the core have been calibrated using pulps from previous drilling by the Company, for which there are known head assays. 2018 HQ diamond core was half-core sampled at regular intervals (usually one metre) with smaller sample intervals at geological boundaries. 2015 diamond core was quarter-core sampled at regular intervals (usually one metre) and constrained to geological boundaries where appropriate. 2009 HQ diamond core was half-core sampled at regular intervals (one metre) or to geological boundaries. Most of the RC drilling was sampled at one metre intervals, apart from the very earliest programme in 1998. RC samples have been split from the rig for all programs with a cone splitter to obtain 2.5 – 3.5 kg of sample from each metre. Field duplicates were collected for every 40th drill metre to check sample representativity from the drill rig splitter.



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	Aspects of the determination of mineralisation that are Material to the Public Report.	RC drilling samples were collected at one metre intervals and passed through a cone splitter to obtain a nominal 2-5kg sample at an approximate 10% split ratio. These split samples were collected in pre-numbered calico sample bags. The sample was dried, crushed and pulverised to produce a sub sample (~200g) for laboratory analysis using XRF and total LOI by thermogravimetric analysis. Diamond core was drilled predominantly at HQ size for the earlier drilling (2009) and entirely HQ for the 2018 program, with the
		2015 and 2019 drilling at PQ3 size. Field duplicates, standards and blanks have been inserted into the sampling stream at a rate of nominally 1:20 for blanks, 1:20 for standards (including internal laboratory), 1:40 for field duplicates, 1:20 for laboratory checks and 1:74 for umpire assays.
Drilling techniques	Drill type (e.g. core, reverse circulation, openhole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-	Diamond drillholes account for 14% of the drill metres used in the Resource Estimate and comprises HQ and PQ3 sized core. RC drilling (generally 135 mm to 140 mm face-sampling hammer) accounts for the remaining 86% of the drilled metres. Six of the diamond holes have RC pre-collars (GDH911, GDH913 & GDH916, 18GEDH001, 002 and 003), otherwise all holes are drilled from surface.
	sampling bit or other type, whether core is oriented and if so, by what method, etc.).	No core orientation data has been recorded in the database. 17 RC holes were drilled during the 2018 program and three HQ diamond tails were drilled on RC pre-collars for resource and geotechnical purposes. The core was not orientated but all diamond holes were logged by OTV and ATV televiewer. Six RC holes from the 2018 campaign are not used in the resource estimate due to results pending at the time of the latest update, and two diamond holes drilled during 2018 were not used as they are for geotechnical purposes and do not intersect the mineralised zones.
		During 2019 a further 12 PQ diamond holes have been drilled down-dip on the high-grade zone for metallurgical sample but have not been sampled for assay analysis as they have been sampled for a metallurgy pilot study program. As such they do not form part of any resource estimation. An addition 18 PQ diamond tails on RC pre-collars have been drilled vertically, of which 16 are expected to contribute to the resource and two were used for the metallurgy pilot study program.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	Diamond core recovery is measured when the core is recovered from the drill string. The length of core in the tray is compared with the expected drilled length and is recorded in the database.
		For the 2019, 2018 and 2015 drilling, RC chip sample recovery was judged by how much of the sample was returned from the cone splitter. This was recorded as good, fair, poor or no sample. The older drilling programmes used a different splitter, but still compared and recorded how much sample was returned for the drilled intervals. All of the RC sample bags (non-split portion) from the 2018 programme were weighed as an additional check on recovery.
		An experienced AVL geologist was present during drilling and any issues noticed were immediately rectified.
		No significant sample recovery issues were encountered in the RC or PQ drilling in 2015.
		No significant sample recovery issues were encountered in the RC or PQ drilling in 2019 except where core loss occurred in three holes intersecting high grade ore. This involved holes 19MTDT012 between 142.9m and 143.3m; 19MTDT013 from 149m to 149.6m, 151m to 151.4m and 159.5m to 160m; as well as 19MTDT016 between 29.5m and 30.7m down hole. In each case the interval lost was included as zero grade for all elements for the estimation of the total mineralised intercept.



Criteria	JORC Code Explanation	Commentary
	Measures taken to maximize sample recovery and ensure representative nature of the samples.	Core depths are checked against the depth given on the core blocks and rod counts are routinely carried out by the drillers. Recovered core was measured and compared against driller's blocks. RC chip samples were actively monitored by the geologist whilst drilling. All drillholes are collared with PVC pipe for the first metres, to ensure the hole stays open and clean from debris.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	No relationship between sample recovery and grade has been demonstrated. Two shallow diamond drillholes drilled to twin RC holes have been completed to assess sample bias due to preferential loss/gain of fine/coarse material. Geologica Pty Ltd is satisfied that the RC holes have taken a sufficiently representative sample of the mineralisation and minimal loss of fines has occurred in the RC drilling resulting in minimal sample bias.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	All diamond core and RC chips from holes included in the latest resource estimate were geologically logged. Diamond core was geologically logged using predefined lithological, mineralogical and physical characteristics (such as colour, weathering, fabric, texture) logging codes and the logged intervals were based on lithological intervals. RQD and recoveries were also recorded. Minimal structural measurements were recorded (bedding to core angle measurements) but have not yet been saved to the database. The logging was completed on site by the responsible geologist. All of the drilling was logged onto paper and was transferred to a SQL Server drillhole database using DataShedTM database management software. The database is managed by Mitchell River Group (MRG). The data was checked for accuracy when transferred to ensure that correct information was recorded. Any discrepancies were referred back to field personnel for checking and editing. All core trays were photographed wet and dry. RC chips were logged generally on metre intervals, with the abundance/proportions of specific minerals, material types, lithologies, weathering and colour recorded. Physical hardness for RC holes is estimated by chip recovery and properties (friability, angularity) and in diamond holes by scratch testing. From 2015, drilling also had magnetic susceptibility recorded, with the first nine diamond holes (GDH901-GDH909) having readings taken on the core every 30 cm or so downhole. Holes GDH910 to GDH917 had readings every 50 cm and RC holes GRC0159 to GRC0221 had readings for each one metre green sample bag. 2018 RC drill holes also have magnetic susceptibility data for each one metre of drilling. Pulps from historic drillhole are in the process of being measured for magnetic susceptibility, with calibration on results applied from control sample measurement of pulps from drill programs from 2015 onwards where measurements of the RC bags already exist. All resource (vs geotechnical) diamond core and RC samples have been logged t
		PQ diamond drill holes completed during 2019 were geologically and geotechnically logged in detail by the site geologists.



Criteria	JORC Code Explanation	Commentary					
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Logging was both qualitative and quantitative in nature, with general lithology information recorded as qualitative and most mineralisation records and geotechnical records being quantitative. Core photos were collected for all diamond drilling.					
	The total length and percentage of the relevant intersections logged.	All recovered intervals were geologically logged.					
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	The 2018 and 2009 HQ diamond core was cut in half and the half core samples were sent to the laboratories for assaying. Sample intervals were marked on the core by the responsible geologist considering lithological and structural features. No core was selected for duplicate analysis. The 2015 PQ diamond core was cut in half and then the right-hand side of the core (facing downhole) was halved again using powered core saw. Quarter core samples were sent to the laboratories for assaying. Sample intervals were marked on the composition by the responsible geologist considering lithological and structural features. No core was selected for duplicate analysis. 16 of the 18 total vertical diamond PQ diamond drill holes from 2019 have been quarter core sampled and assayed. Sample					
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	intervals were marked on the core by the responsible geologist considering lithological and structural features. RC drilling was sampled by use of an automatic cone splitter for the 2019, 2018 and 2015 drilling programmes; drilling was generally dry with a few damp samples. Older drilling programmes employed riffle splitters to produce the required sample splits for assaying. One in 40 to 50 RC samples was resampled as field duplicates for QAQC assaying.					
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The sample preparation techniques employed for the diamond core samples follow standard industry best practice. All samples were crushed by jaw and Boyd crushers and split if required to produce a standardised ~3kg sample for pulverising. The 2015 programme RC chips were split to produce the same sized sample. All samples were pulverised to a nominal 90% passing 75 micron sizing and sub sampled for assaying and LOI determination tests. The remaining pulps are stored at an AVL facility. The sample preparation techniques are of industry standard and are appropriate for the sample types and proposed assaying methods.					
	Quality control procedures adopted for all sub- sampling stages to maximize representivity of samples.	Field duplicates, standards and blanks have been inserted into the sampling stream at a rate of nominally 1:20 for blanks, 1:20 for standards (including internal laboratory), 1:40 for field duplicates, 1:20 for laboratory checks and 1:74 for umpire assays. Also, for the recent sampling at BV, 1 in 20 samples were tested to check for pulp grind size. For 2019 diamond core samples, duplicates were created from the coarse crush at a frequency of 1 in 20 samples at the laboratory and assayed.					
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.	To ensure the samples collected are representative of the in-situ material, a 140mm diameter RC hammer was used to collect one metre samples and either HQ or PQ3 sized core was taken from the diamond holes. Given that the mineralisation at the Australian Vanadium Project is either massive or disseminated magnetite/martite hosted vanadium, which shows good consistency in interpretation between sections and occurs as percentage values in the samples, Geologica Pty Ltd considers the sample sizes to be representative. Core is not split for duplicates, but RC samples are split at the collection stage to get representative (2-3kg) duplicate samples. The entire core sample and all the RC chips are crushed and /or mixed before splitting to smaller sub-samples for assaying.					



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	Whether sample sizes are appropriate to the grain size of the material being sampled.	As all of the variables being tested occur as moderate to high percentage values and generally have very low variances (apart from Cr_2O_3), the chosen sample sizes are deemed appropriate.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	All samples for the Australian Vanadium Project were assayed for the full iron ore suite by XRF (24 elements) and for total LOI by thermo-gravimetric technique. The method used is designed to measure the total amount of each element in the sample. Some 2015 and 2018 RC samples in the oxide profile were also selected for SATMAGAN analysis that is a measure of the amount of total iron that is present as magnetite (or other magnetic iron spinel phases, such as maghemite or kenomagnetite). SATMAGAN analysis was conducted at Bureau Veritas (BV) Laboratory during 2018.
		Although the laboratories changed over time for different drilling programmes, the laboratory procedures all appear to be in line with industry standards and appropriate for iron ore deposits, and the commercial laboratories have been industry recognized and certified
		Samples are dried at 105°C in gas fired ovens for 18-24 hours before RC samples being split 50:50. One portion is retained for future testing, while the other is then crushed and pulverised. Sub-samples are collected to produce a 66g sample that is used to produce a fused bead for XRF based analysing and reporting.
		Certified and non-certified Reference Material standards, field duplicates and umpire laboratory analysis are used for quality control. The standards inserted by AVL during the 2015 drill campaign were designed to test the V_2O_5 grades around 1.94%, 0.95% and 0.47%. The internal laboratory standards used have varied grade ranges but do cover these three grades as well. During 2018 and 2019, three Certified Reference Materials (CRMs) were used by AVL as field standards. These covered the V_2O_5 grade ranges around 0.327%, 0.790% and 1.233%. These CRMs are also certified for other relevant major element and oxide values, including Fe, TiO ₂ , Al ₂ O ₃ , SiO ₂ , Co, Ni and Cu (amongst others).
		Most of the laboratory standards used show an apparent underestimation of V_2O_5 , with the results plotting below the expected value lines, however the results generally fall within \pm 5-10% ranges of the expected values. The other elements show no obvious material bias.
		Standards used by AVL during 2015 generally showed good precision, falling within 3-5% of the mean value in any batch. The standards were not certified but compared with the internal laboratory standards (certified) they appear to show good accuracy as well.
		Field duplicate results from the 2015 drilling all fall within 10% of their original values.
		The BV laboratory XRF machine calibrations are checked once per shift using calibration beads made using exact weights and they performed repeat analyses of sample pulps at a rate of 1:20 (5% of all samples). The lab repeats compare very closely with the original analysis for all elements.
		2019 PQ diamond core has been assayed, and studies on all results for QAQC sample performance is in progress.
		Geologica considers that the nature, quality and appropriateness of the assaying and laboratory procedures is at acceptable industry standards.



Criteria	JORC Code Explanation	Commentary
	For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	The geophysical readings taken for the Australian Vanadium Project core and RC samples and recorded in the database were magnetic susceptibility. For the 2009 diamond and 2015 RC and diamond drill campaigns this was undertaken using an RT1 hand magnetic susceptibility meter (CorMaGeo/Fugro) with a sensitivity of 1 x 10 ⁻⁵ (dimensionless units). The first nine diamond holes (GDH901 – GDH909) were sampled at approximately 0.3m intervals, the last eight (GDH910 – GDH917) at 0.5m intervals and the RC chip bags for every green bagged sample (one metre). During 2018 and 2019 RC and diamond core has been measured using a KT-10 magnetic susceptibility metre, at 1 x 10 ⁻³ ssi unit. In addition to the handhold magnetic susceptibility described above the 2019 drilling included downhole magnetic susceptibility. This was taken using a Century Geophysical 9622 Magnetic Susceptibility tool. The 9622 downhole tool sensitivity is 20 x 10 ⁻⁵ with a resolution of 10cm 2019 diamond core is being analysed using an Olympus Vanta pXRF with a 20 second read time. The unit has been calibrated using pulp samples with known head assays from previous drill campaigns by the Company. Standard deviations for each element analysed are being recorded and retained. Elements being analysed are: Mg, Al, Si, P, S, K, Ca, Ti, V, Cr, Mn, Fe, Co, Ni, Cu, Zn, As, Se, Rb, Sr, Y, Zr, Nb, Mo, Ag, Cd, Sn, Sb, W, Hg, Pb, Bi, Th, and U. Four completed diamond drillholes were down hole surveyed by acoustic televiewer (GDH911, 912, 914 and 915) as a prequel to geotechnical logging during the 2015 drill campaign. A further six holes from the 2018 campaign have been down hole surveyed using acoustic televiewer and optical televiewer (18GEDH001, 002 and 003 and partial surveys of 18GERC005, 008 and 011) for 627 metres of data. Televiewer data was also collected during 2018 on some of the holes drilled in 2015 and prior. The holes surveyed were GRC0019, 0024, 0168, 0169, 0173, 0178, 0180, 0183, 0200 and Na253, Na258 and Na376 for a further 286.75 m of data.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	QAQC results from both the primary and secondary assay laboratories show no material issues with the main variables of interest for the recent assaying programmes.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	Diamond drill core photographs have been reviewed for the recorded sample intervals. Geologica Pty Ltd Consultant, Brian Davis, visited the Australian Vanadium Project site on multiple occasions and the BV core shed and assay laboratories in 2015 and 2018. Whilst on site, the drillhole collars and remaining RC chip samples were inspected. All of the core was inspected in the BV facilities in Perth and selected sections of drillholes were examined in detail in conjunction with the geological logging and assaying. Resource consultants from Trepanier have visited the company core storage facility in Bayswater and reviewed the core trays for select diamond holes.
	The use of twinned holes.	Two diamond drillholes (GDH915 and GDH917) were drilled to twin the RC drillholes GRC0105 and GRC0162 respectively. The results show excellent reproducibility in both geology and assayed grade for each pair.



Criteria	JORC Code Explanation	Commentary
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	All primary geological data has been collected using paper logs and transferred into Excel spreadsheets and ultimately a SQL Server Database. The data were checked on import. Assay results were returned from the laboratories as electronic data which were imported directly into the SQL Server database. Survey and collar location data were received as electronic data and imported directly to the SQL database. All of the primary data have been collated and imported into a Microsoft SQL Server relational database, keyed on borehole identifiers and assay sample numbers. The database is managed using DataShed™ database management software. The data was verified as it was entered and checked by the database administrator (MRG) and AVL personnel
	Discuss any adjustment to assay data.	No adjustments or calibrations were made to any assay data, apart from resetting below detection limit values to half positive detection values.
Location of data points	Accuracy and quality of surveys used to locate drillholes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	The 2019 drill holes have been set out using a real-time Kinematic (RTK) GPS system. At completion of drilling the collar positions were picked up by a professional surveyor with an RTK system. For the 2018 drilling, all collars were set out using a handheld GPS. After drilling they were surveyed using a Trimble RTK GPS system. The base station accuracy on site was improved during the 2015 survey campaign and a global accuracy improvement was applied to all drillholes in the Company database. For the 2015 drilling, all of the collars were set out using a Trimble RTK GPS system. After completion of drilling all new collars were re-surveyed using the same tool. Historical drill holes were surveyed with RTK GPS and DGPS from 2008 to 2015, using the remaining visible collar location positions where necessary. Only five of the early drillholes, drilled prior to 2000 by Intermin, had no obvious collar position when surveyed and a best estimate of their position was used based on planned position data. Downhole surveys were completed for all diamond holes, using gyro surveying equipment, as well as the RC holes drilled in 2015 (from GRC0159). Some RC drillholes from the 2018 campaign do not have gyro survey as the hole closed before the survey could be done. These holes have single shot camera surveys, from which the dip readings were used with an interpreted azimuth (nominal hole setup azimuth). The holes with interpreted azimuth are all less than 120m depth. All other RC holes were given a nominal -60° dip measurement. These older RC holes were almost all 120m or less in depth.
	Specification of the grid system used.	The grid projection used for the Australian Vanadium Project is MGA_GDA94, Zone 50. All reported coordinates are referenced to this grid.



Criteria	JORC Code Explanation	Commentary
	Quality and adequacy of topographic control.	High resolution Digital Elevation Data was captured by Arvista for the Company in June 2018 over the MLA51/878 tenement area using fixed wing aircraft, with survey captured at 12 cm GSD using an UltraCam camera system operated by Aerometrex. The data has been used to create a high-resolution Digital Elevation Model on a grid spacing of 5m x 5m, which is within 20 cm of all surveyed drill collar heights, once the database collar positions were corrected for the improved ground control survey, that was also used in this topography survey. The vertical accuracy that could be achieved with the 12 cm GSD is +/- 0.10 m and the horizontal accuracy is +/- 0.24m. 0.5m contour data has also been generated over the mining lease application. High quality orthophotography was also acquired during the survey at 12cm per pixel for the full lease area, and visual examination of the imagery shows excellent alignment with the drill collar positions. The November 2018 Mineral Resource used this surface for topographic control within the Mining Lease Application area (MLA51/878).
		For the entire 2017 and July 2018 Mineral Resource estimates, and the November 2018 Mineral Resource estimate outside the MLA area, high resolution Digital Elevation Data was supplied by Landgate. The northern two thirds of the elevation data is derived from ADS80 imagery flown September 2014. The data has a spacing of 5M and is the most accurate available. The southern third is film camera derived 2005 10M grid, resampled to match it with the 2014 DEM. Filtering was applied and height changes are generally within 0.5M. Some height errors in the 2005 data may be +/- 1.5M when measured against AHD but within the whole area of interest any relative errors will mostly be no more than +/- 1M. In 2015 a DGPS survey of hole collars and additional points was taken at conclusion of the drill program. Trepanier compared the elevations the drillholes with the supplied DEM surface and found them to be within 1m accuracy.
		An improved ground control point has been established at the Australian Vanadium Project by professional surveyors. This accurate ground control point was used during the acquisition of high quality elevation data. As such, a correction to align previous surveys with the improved ground control was applied to all drill collars from pre-2018 in the Company drill database. Collars that were picked up during 2018 were already calibrated against the new ground control. 2019 drill collar locations have been verified with a DGPS in the field (accuracy about 20 cm on the horizontal) with final RTK pick up complete.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	The 2018 RC drilling in Fault Block 17 has infilled areas of 260 m spaced drill lines to about 130m spaced drill lines, with holes on 30 m centres on each line. The closer spaced drilled areas of the deposit now have approximately 80m to 100m spacing by northing and 25m to 30m spacing by easting. Occasionally these spacings are closer for some pairs of drillholes. Outside of the main area of relatively close spaced drilling (approximately 7015400mN to 7016600mN), the drillhole spacing increases to several hundred metres in the northing direction but maintains roughly the same easting separation as the closer spaced drilled area.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The degree of geological and grade continuity demonstrated by the data density is sufficient to support the definition of Mineral Resources and the associated classifications applied to the Mineral Resource estimate as defined under the 2012 JORC Code. Variography studies have shown very little variance in the data for most of the estimated variables and primary ranges in the order of several hundred metres.
	Whether sample compositing has been applied.	All assay results have been composited to one metre lengths before being used in the Mineral Resource estimate. This was by far the most common sample interval for the diamond drillhole and RC drillhole data.



Criteria	JORC Code Explanation	Commentary
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	The grid rotation is approximately 45° to 50° magnetic to the west, with the holes dipping approximately 60° to the east. The drill fences are arranged along the average strike of the high-grade mineralised horizon, which strikes approximately 310° to 315° magnetic south of a line at 7015000mN and approximately 330° magnetic north of that line. The mineralisation is interpreted to be moderate to steeply dipping, approximately tabular, with stratiform bedding striking approximately north-south and dipping to the west. The drilling is exclusively conducted perpendicular to the strike of the main mineralisation trend and dipping approximately 60° to the east, producing approximate true thickness sample intervals through the mineralisation.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	The orientation of drilling with respect to mineralisation is not expected to introduce any sampling bias. Drillholes intersect the mineralisation at an angle of approximately 90 degrees. The 2019 PQ diamond holes are deliberately drilled down dip to maximise the amount of metallurgy sample collected for the pilot study, with all material used for metallurgy purposes (hence not being available for assay). They are not intended to add material to the resource estimation, or to define geological boundaries, though where further control on geological contacts is intercepted, this will be used to add more resolution to the geological model.
Sample security	The measures taken to ensure sample security.	Samples were collected onsite under supervision of a responsible geologist. The samples were then stored in lidded core trays and closed with straps before being transported by road to the BV core shed in Perth (or other laboratories for the historical data). RC chip samples were transported in bulk bags to the assay laboratory and the remaining green bags are either still at site or stored in Perth. RC and core samples were transported using only registered public transport companies. Sample dispatch sheets were compared against received samples and any discrepancies reported and corrected.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	A review of the sampling techniques and data was completed by Mining Assets Pty Ltd (MASS) and Schwann Consulting Pty Ltd (Schwann) in 2008 and by CSA in 2011. Neither found any material error. AMC also reviewed the data in the course of preparing a Mineral Resource estimate in 2015. The database has been audited and rebuilt by AVL and MRG in 2015. In 2017 geological data was revised after missing lithological data was sourced. Geologica Pty Ltd concludes that the data integrity and consistency of the drillhole database shows sufficient quality to support resource estimation.



Section 2: Reporting of Exploration Results

Criteria	JORC Code Explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	Exploration Prospects are located wholly within Lease P51/2567 and E 51/843. The tenements are 100% owned by Australian Vanadium Ltd. The tenements lie within the Yugunga Nya Native Title Claim (WC1999/046). A Heritage survey was undertaken prior to commencing drilling which only located isolated artefacts but no archaeological sites <i>per se</i> . Mining Lease Application MLA51/878 covering most of E 51/1843 and the vanadium project is currently under consideration by the Department of Mines and Petroleum. AVL has no joint venture, environmental, national park or other ownership agreements on the lease area. A Mineral Rights Agreement has been signed with Bryah Resources Ltd for copper and gold exploration on the AVL Australian Vanadium Project tenements.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	At the time of reporting, there are no known impediments to obtaining a licence to operate in the area and the tenement is in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	The Australian Vanadium Project deposit was identified in the 1960's by Mangore P/L and investigated with shallow drilling, surface sampling and mapping. In 1998, Drilling by Intermin Resources confirmed the down dip extent and strike continuation under cover between outcrops of the vanadium bearing horizons. Additional RC and initial diamond drilling was conducted by Greater Pacific NL and then AVL up until 2018. Previous Mineral Resource estimates have been completed for the deposit in 2001 (Mineral Engineering Technical Services Pty Ltd (METS) and Bryan Smith Geosciences Pty Ltd. (BSG)), 2007 (Schwann), 2008 (MASS & Schwann), 2011 (CSA), 2015 (AMC), 2017 (Trepanier) and 2018 (Trepanier).
Geology	Deposit type, geological setting and style of mineralisation.	The Australian Vanadium Project is located approximately 40kms south of Meekatharra in Western Australia and approximately 100kms along strike (north) of the Windimurra Vanadium Mine. The mineralisation is hosted in the same geological unit as Windimurra, which is part of the northern Murchison granite greenstone terrane in the north west Yilgarn Craton. The project lies within the Gabanintha and Porlell Archaean greenstone sequence oriented approximately NW-SE and is adjacent to the Meekatharra greenstone belt. Locally the mineralisation is massive or bands of disseminated vanadiferous titano-magnetite hosted within the gabbro. The mineralised package dips moderately to steeply to the west and is capped by Archaean acid volcanics and metasediments. The footwall is a talc carbonate altered ultramafic unit. The host sequence is disrupted by late stage dolerite and granite dykes and occasional east and northeast - southwest trending faults with apparent minor offsets. The mineralisation ranges in thickness from several metres to up to 30m in thickness. The oxidized and partially oxidised weathering surface extends 50 to 80m below surface and the magnetite in



Criteria	JORC Code Explanation	Commentary
		the oxide zone is usually altered to Martite.
Drillhole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drillholes: easting and northing of the drillhole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drillhole collar dip and azimuth of the hole down hole length and interception depth hole length.	All drill results relevant to the mineral resource updates were disclosed at the time of the resource publication. All relevant historic drillhole collar information relating to this report are shown in <i>APPENDIX 3</i> .
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	Length weighed averages used for exploration results are reported in spatial context when exploration results are reported. Cutting of high grades was not applied in the reporting of intercepts.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	There were negligible residual composite lengths, and where present these were excluded from the estimate.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalent values have been used.



Criteria	JORC Code Explanation	Commentary
Relationship between mineralisation widths and intercept lengths	If the geometry of the mineralisation with respect to the drillhole angle is known, its nature should be reported.	Drillholes intersect the mineralisation at an angle of approximately 90 degrees. From the 2019 program the diamond tail holes were drilled vertically (-90 degrees). This decreases the angle of intersection with the mineralisation.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drillhole collar locations and appropriate sectional views.	See Figures 2,4 and Tables 1,2,3 of this release.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	Comprehensive reporting of drilling details has been provided in the body of this announcement.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	All meaningful and material exploration data has been reported
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Extensional resource infill drilling is planned during the next two years for the additional 8 km of mineralisation that is currently drilled at broad spacing.



Criteria	JORC Code Explanation	Commentary
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	The decision as to the necessity for further exploration at the Australian Vanadium Project is pending completion of mining technical studies on the currently available resource. Figure 3 in this report show areas of possible resource extension.



Section 3: Estimation and Reporting of Mineral Resources

Criteria	JORC Code Explanation	Commentary
Database integrity	Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.	All the drilling was logged onto paper and has been transferred to a digital form and loaded into a Microsoft SQL Server relational drillhole database using DataShed TM management software. Logging information was reviewed by the responsible geologist and database administrator prior to final load into the database. All assay results were received as digital files, as well as the collar and survey data. These data were transferred directly from the received files into the database. All other data collected for Australian Vanadium Project were recorded as Excel spreadsheets prior to loading into SQL Server. The data have been periodically checked by AVL personnel, the database administrator as well as the personnel involved in all previous Mineral Resource estimates for the project.
	Data validation procedures used.	The data validation was initially completed by the responsible geologist logging the core and marking up the drillhole for assaying. The paper geological logs were transferred to Excel spreadsheets and compared with the originals for error. Assay dispatch sheets were compared with the record of samples received by the assay laboratories.
		Normal data validation checks were completed on import to the SQL database. Data has also been checked back against hard copy results and previous mines department reports to verify assays and logging intervals.
		Both internal (AVL) and external (Schwann, MASS, CSA and AMC) validations were/are completed when data was loaded into spatial software for geological interpretation and resource estimation. All data have been checked for overlapping intervals, missing samples, FROM values greater than TO values, missing stratigraphy or rock type codes, downhole survey deviations of ±10° in azimuth and ±5° in dip, assay values greater than or less than expected values and several other possible error types. Furthermore, each assay record was examined and mineral resource intervals were picked by the Competent Person. QAQC data and reports have been checked by the database administrator, MRG. MASS & Schwann and CSA both reported on the available QAQC data for the Australian Vanadium Project.
Site visits	Comment on any site visits undertaken by the Competent Person and the outcome of those visits.	The drill location was inspected by John Tyrrell of AMC in 2015 for the initial 2012 JORC resource estimation. Consulting Geologist Brian Davis of Geologica Pty Ltd has visited all the Australian Vanadium Project drilling sites since 2015 and has been familiar with the Australian Vanadium Project iron-titanium-vanadium orebody since 2006. The geology, sampling, sample preparation and transport, data collection and storage procedures were all discussed and reviewed with the responsible geologist for the 2015, 2017 and 2018 drilling. Visits to the BV laboratory and core shed in Perth were used to add knowledge to aid in the preparation of this Mineral Resource Estimate.
	If no site visits have been undertaken indicate why this is the case.	N/A



Criteria	JORC Code Explanation	Commentary
Geological interpretation	Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.	The Australian Vanadium Project mineralisation lies along strike from the Windimurra Vanadium Mine and the oxidised portion of the high-grade massive magnetite/martite mineralisation extends for about 11.5 km in the company held lease area. Detailed mapping and mineralogical studies have been completed by company personnel and contracted specialists between 2000 and 2019, as well as six separate drilling programmes to test the mineralisation and continuity of the structures. These data and the relatively closely- spaced drilling has led to a good understanding of the mineralisation controls. The mineralisation is hosted within altered gabbros and is easy to visually identify by the magnetite/martite content. The main high grade unit shows consistent thickness and grade along strike and down dip and has a clearly defined sharp boundary. The lower grade disseminated bands also show good continuity, but their boundaries are occasionally less easy to identify visually as they are more diffuse over a metre or so.
	Nature of the data used and of any assumptions made.	No assumptions are made regarding the input data.
	The effect, if any, of alternative interpretations on Mineral Resource estimation.	Alternative interpretations were considered in the current estimation and close comparison with the 2015 resource model was made to see the effect of the new density data and revised geology model. The continuity of the low grade units, more closely defined from lithology logs is now better understood and the resulting interpretation is more effective as a potential mining model. The near-surface alluvial and transported material has also been more closely modelled in this estimation. The impact of the current interpretation as compared to the previous interpretation would be a greater volume of low grade mineralisation and a higher overall V_2O_5 grade for that mineralisation in the current estimate.
	The use of geology in guiding and controlling Mineral Resource estimation.	Geological observation has underpinned the resource estimation and geological model. The high grade mineralisation domain has a clear and sharp boundary and has been tightly constrained by the interpreted wireframe shapes. The low grade mineralisation is also constrained within wireframes, which are defined and guided by visual (from core) and grade boundaries from assay results. The low grade mineralisation has been defined as four sub-domains, which strike sub-parallel to the high grade domain. In addition there is a sub parallel laterite zone and two transported zones above the top of bedrock surface. The resource estimate is constrained by these wireframes. Domains were also coded for oxide, transition and fresh, as well as above and below the alluvial and bedrock surfaces. The extents of the geological model were constrained by fault block boundaries. Geological boundaries were extrapolated to
		the edges of these fault blocks, as indicated by geological continuity in the logging and the magnetic geophysical data.



Criteria	JORC Code Explanation	Commentary
	The factors affecting continuity both of grade and geology.	 Key factors that are likely to affect the continuity of grade are: The thickness and presence of the high grade massive magnetite/martite unit, which to date has been very consistent in both structural continuityand grade continuity. The thickness and presence of the low grade banded and disseminated mineralisation along strike and down dip. The low grade sub-domains are less consistent in their thickness along strike and down dip with more pinching and swelling than for the high grade domain. SW-NE oriented faulting occurs at a deposit scale and offsets the main orientation of the mineralisation. These regional faults divide the deposit along strike into kilometer scale blocks. Internally the mineralised blocks show very few signs of structural disturbance at the level of drilling.
Dimensions	The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.	The massive magnetite/martite unit strikes approximately 14 km overall (within AVL tenements and outside), is stratiform and ranges in thickness from less than 10m to over 30m true thickness. The low grade mineralised units are sub-parallel to the high grade zone, and also vary in thickness from less than 10m to over 20m. All the units dip moderately to steeply towards the west, except for two predominantly alluvial units (domains 7 and 8) and a laterite unit (domain 6) which are flat lying. All units outcrop at surface in some locations, but the low grade units are difficult to locate as they are more weathered and have a less prominent surface expression than the high grade unit. The high and low grade units are currently interpreted to have a depth extent of approximately 200m below surface. Mineralisation is currently open along strike and at depth.
Estimation and modelling techniques	The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.	Grade estimation was completed using ordinary kriging (OK) for the Mineral Resource estimate. Surpac TM software was used to estimate grades for V ₂ O ₅ , TiO ₂ , Fe ₂ O ₃ , SiO ₂ , Al ₂ O ₃ , Cr ₂ O ₃ , Co, Cu, Ni, S and loss on ignition (LOI) using parameters derived from statistical and variography studies. The majority of the variables estimated have coefficients of variation of significantly less than 1.0, with Cr ₂ O ₃ being the exception. Drillhole spacing varies from approximately 80 m to 100 m along strike by 25 m to 30 m down dip, to 500 m along by 25 m to 30 m down dip. Drillhole sample data was flagged with numeric domain codes unique to each mineralisation domain. Sample data was composited to 1 m downhole length and composites were terminated by a change in domain or oxidation state coding. No grade top cuts were applied to any of the estimated variables as statistical studies showed that there were no extreme outliers present within any of the domain groupings. Grade was estimated into separate mineralisation domains including a high grade bedrock domain, four low grade bedrock domains and low grade alluvial and laterite domains. Each domain was further subdivided into a fault block, and each fault block was assigned its own orientation ellipse for grade interpolation. Downhole variography and directional variography were performed for all estimated variables for the high grade domain and the grouped low grade domains. Grade continuity varied from hundreds of metres in the along strike directions to sub-two hundred metres in the down-dip direction although the down-dip limitation is likely related to the extent of drilling to date.



Criteria	JORC Code Explanation	Commentary
	The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.	Prior to 2017, there had been five Mineral Resource estimates for the Australian Vanadium Project deposit. The first, in 2001 was a polygonal sectional estimate completed by METS & BSG. The subsequent models by Schwann (2007), MASS & Schwann (2008) and CSA (2011) are kriged estimates. AMC (2015) reviewed the geological interpretation of the most recent previous model (CSA 2011), but used a new interpretation based on additional new drilling for the 2015 estimate. In 2017 a complete review of the geological data, weathering profiles, magnetic intensity and topographic data as well as incorporation of additional density data and more accurate modelling techniques resulted in a re-interpreted mineral resource. No mining has occurred to date at the Australian Vanadium Project, so there are no production records. Addition infill drilling and a single extensional diamond core holes have resulted in minor adjustments to the interpretation.
	The assumptions made regarding recovery of by-products.	Test work conducted by the company in 2015 identified the presence of sulphide hosted cobalt, nickel and copper, specifically partitioned into the silicate phases of the massive titaniferous vanadiferous iron oxides which make up the vanadium mineralization at the Australian Vanadium Project. Subsequent test work has shown the ability to recover a sulphide flotation concentrate containing between 3.8 % and 6.3% of combined base metals treating the non-magnetic tailings produced as a result of the magnetic separation of a vanadium iron concentrate from fresh massive magnetite. Further work is underway to evaluate the economic value of the concentrate by-product. See ASX Announcements dated 22 May 2018 and 5 July 2018.
	Estimation of deleterious elements or other nongrade variables of economic significance (e.g. sulphur for acid mine drainage characterization).	Estimates were undertaken for Fe ₂ O ₃ , SiO ₂ , TiO ₂ , Al ₂ O ₃ , and LOI, which are non-commodity variables, but are useful for determining recoveries and metallurgical performance of the treated material. Estimated Fe ₂ O ₃ % grades were converted to Fe% grades in the final for reporting (Fe% = Fe ₂ O ₃ /1.4297). Estimates were also undertaken for Cr ₂ O ₃ which is a potential deleterious element. The estimated Cr ₂ O ₃ % grades were converted to Cr ppm grades (Cr ppm = (Cr ₂ O ₃ *10000)/1.4615).



Criteria	JORC Code Explanation	Commentary
	In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.	The Australian Vanadium Project block model uses a parent cell size of 40 m in northing, 10 m in easting and 5 m in RL. This corresponds to approximately half the distance between drillholes in the northing and easting directions and matches an assumed bench height in the RL direction. Accurate volume representation of the interpretation was achieved.
	Any assumptions behind modelling of selective mining units.	Grade was estimated into parent cells, with all sub-cells receiving the same grade as their relevant parent cell. Search ellipse dimensions and directions were adjusted for each fault block.
		Three search passes were used for each estimate in each domain. The first search was 120m and allowed a minimum of 8 composites and a maximum of 24 composites. For the second pass, the first pass search ranges were expanded by 2 times. The third pass search ellipse dimensions were extended to a large distance to allow remaining unfilled blocks to be estimated. A limit of 5 composites from a single drillhole was permitted on each pass. In domains of limited data, these parameters were adjusted appropriately.
		No selective mining units were considered in this estimate apart from an assumed five metre bench height for open pit mining. Model block sizes were determined primarily by drillhole spacing and statistical analysis of the effect of changing block sizes on the final estimates.
	Any assumptions about correlation between variables.	All elements within a domain used the same sample selection routine for block grade estimation. No co-kriging was performed at the Australian Vanadium Project, but correlation studies on the composite data showed very good correlation (0.8 or above) between most variables, apart from Cr which has a correlation coefficient of 0.65 with V_2O_5 .
	Description of how the geological interpretation was used to control the resource estimates.	The geological interpretation is used to define the mineralisation, oxidation/transition/fresh and alluvial domains. All of the domains are used as hard boundaries to select sample populations for variography and grade estimation.
	Discussion of basis for using or not using grade cutting or capping.	Analysis showed that none of the domains had statistical outlier values that required top-cut values to be applied.
	The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.	 Validation of the block model consisted of: Volumetric comparison of the mineralisation wireframes to the block model volumes. Visual comparison of estimated grades against composite grades. Comparison of block model grades to the input data using swathe plots. As no mining has taken place at the Australian Vanadium Project to date, there is no reconciliation data available.
Moisture	Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.	All mineralisation tonnages are estimated on a dry basis. The moisture content in mineralisation is considered very low.



Criteria	JORC Code Explanation	Commentary
Cut-off parameters	The basis of the adopted cut-off grade(s) or quality parameters applied.	A nominal $0.4\% \ V_2O_5$ wireframed cut off for low grade and a nominal $0.7\% \ V_2O_5$ wireframed cut off for high grade has been used to report the Mineral Resource at the Australian Vanadium Project. Consideration of previous estimates, as well as the current mining, metallurgical and pricing assumptions, while not rigorous, suggest that the currently interpreted mineralised material has a reasonable prospect for eventual economic extraction at these cut off grades.
Mining factors or assumptions	Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.	AVL completed a mining Scoping Study in October 2016 for the Australian Vanadium Project. The primary mining scenario being considered is conventional open pit mining. AVL has assumed, based on initial concept study work and the nearby presence of a similar project (Windimurra mine site), that the Australian Vanadium Project deposit is amenable to open-pit mining methods. In September 2018, AVL released a base case PFS which included key assumptions supporting a planned open pit vanadium mining operation at the Australian Vanadium Project. Currently (September 2019) AVL is undertaking a DFS to refine metallurgical recovery, processing and cost models for the Australian Vanadium Project.



Criteria	JORC Code Explanation			Comm	entary			
Metallurgical factors or assumptions	regarding metallurgical amenability. It is always	Metallurgical studies have focused on bench-scale comminution and magnetic separation test work on 24 contiguous drill core intervals from the high-grade vanadium domain. These samples included 10 off from the "fresh" rock zone, 9 off from the zone defined as "transitional" and 5 off from the near surface oxidised horizon, "oxide".						
		Metallurgical Sample	Drillhole origin	From (m)	To (m)	Interval (m)	Mass (kg)	
	metallurgical treatment processes and	1 Fr	GDH903	191	199	8	33	
	parameters made when reporting Mineral	2 Fr 3 Fr	GDH903 GDH903	199 209	209	6.2	25 25	
	Resources may not always be rigorous. Where	4 Fr	GDH903 GDH911	98.9	105.5	6.6	59	
		5 Fr	GDH911	108	113.2	5.2	54	
	this is the case, this should be reported with an	6 Fr	GDH912	124	129	5.2	52	
	explanation of the basis of the metallurgical	7 Fr	GDH912	129	134.2	5.2	54	
	assumptions made.	8 Fr	GDH912	134.3	141	6.7	69	
		9 Fr	GDH914	108	114	6	58	
		10 Fr	GDH914	114	121	7	75	
		11 Tr	GDH902	98	105.8	7.8	34	
		12 Tr	GDH902	105.8	111.1	5.3	31	
		13 Tr	GDH902	111.1	117.1	6	27	
		14 Tr	GDH911	105.5	108	2.5	27	
		15 Tr	GDH913	127.9	133.2	5.3	26	
		16 Tr	GDH913	133.2	140	6.8	47	
		17 Tr	GDH913	140	145.2	5.2	45	
		18 Tr	GDH916	132	139	7	32	
		19 Tr	GDH916	139	151.3	12.3	101	
		20 Ox	GDH901	38	45	7	29	
		21 Ox	GDH901	45	54	9	44	
		22 Ox	GDH915	12	18	6	44	
		23 Ox	GDH915	18	23	5	35	
		24 Ox	GDH917	14.1	21.1	/	44	
		Bench-scale m separation usin carried out on	agnetic separang a hand held the magnetic contained mi	ation test work I I rare earth mag and non-magne	has included Da gnetic rod (260) etic products ar	avis tube testing O gauss at surfac nd selected mag	(1500 gauss) ar ce). 21 element netic concentra	on index testing. nd a customised two stage It XRF and LOI analysis has been It stes underwent QXRD to the mineral associations, grains



Criteria	JORC Code Explanation	Commentary
		Some preliminary sulphide concentrate recovery testing has been undertaken on selected 25kg fresh samples and a 90kg fresh composite sample. These samples were ground to a P_{80} of 106 μ m and underwent wet magnetic separation using a low intensity (1500 Gauss) magnetic separation drum. The non-magnetic stream was dried, sub split and provided feed for sulphide flotation testwork. The flotation testing has been carried out at benchscale using a scheme of typical sulphide flotation reagents. Rougher, scavenger and cleaner flotation has been tested with one concentrate (test BC 4113/2) reground prior to cleaning.
		The preliminary metallurgical investigation has demonstrated: - The oxide, transitional and fresh materials are similar in comminution behaviour and exhibit a moderate rock competency and ball milling energy demand. - The abrasiveness is considered low to moderate. - A positive and predictable response to magnetic separation can be demonstrated from the fresh and transitional material within the high-grade domain. The majority of vanadium exists within magnetic minerals which when separated at a grind size P_{80} of approximately 106 μ m, generates a consistently high V_2O_5 grade, low silica and alumina grade concentrate. - Oxidised material responds to magnetic separation, albeit at lower vanadium recovery and concentrate quality.
		At this stage of metallurgical understanding a primary mill grinding to P_{80} 106 μ m and application of magnetic drum separation is considered a reasonable flowsheet concept to produce a vanadium rich concentrate (approximately 1.4% V_2O_5) from material classified as oxide, transitional and fresh within the high-grade domain.
		Preliminary benchscale roast leach testwork has been undertaken using magnetic concentrate from metallurgical sample Fr 2. Vanadium leach extractions of 79 to 86% have been determined in roasting for 110 minutes at approximately 1050°C testing a range of sodium carbonate addition rates (3 to 6%). Further benchscale roast leach optimization testwork is in progress in preparation for pilot scale testing that is in progress in 2019.
		Given the indicated quality of the concentrate and the preliminary benchscale roast leach testwork results, it is assumed that production of a saleable V_2O_5 product would be achieved via a traditional roast, leach and ammonium meta vanadate (AMV) flowsheet path. Similar flowsheets were applied in the treatment of magnetic concentrate in Xstrata's Windimurra refinery flowsheet in Western Australia and at Largo Resources Maracas vanadium project in Bahia, Brazil. A pilot scale testwork program is being done in 2019 aimed at validating the flowsheet and finalising engineering design criteria to support a definitive feasibility study.



Criteria	JORC Code Explanation	Commentary
Environmental factors or assumptions	Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfield project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	Environmental studies have been undertaken for Pre-Feasibility work. Fauna and Flora surveys, stygofauna and troglofaunal studies, and an Environmental Management Plan has been formulated. Final work in the DFS will include submission of results to the Environmental Protection Authorities for an Environmental Impact Assessment.
Bulk density	Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.	Bulk density determinations (using the Archimedes' method) were made on samples from 15 diamond drillholes. Bulk density data from 313 direct core measurements were used to determine average densities for each of the mineralisation and oxide/transition/fresh domains. Bulk Density was estimated for HG, LG, Alluvial and waste material in Core taken to represent the main lithological units.
	The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.	The water immersion method was used for direct core measurements; all 231 of the latest measurements have been done using sealed core, the previous 97 measurements were not wrapped. AMC's observation of the core indicates that observable porosity was not likely to be high for most of the core at the deposit.



Criteria	JORC Code Explanation		Commentary	
	Discuss assumptions for bulk density estimates	The average bulk density value	es for material at the Australi	an Vanadium Project are:
	used in the evaluation process of the different materials.	Domain	Oxidation State	Bulk Density
	materials.	10 (high grade)	Oxide	3.39
		10 (high grade)	Transition	3.71
		10 (high grade)	Fresh	3.67
		2-8 (lowgrade)	Oxide	2.13
		2-8 (lowgrade)	Transition	2.20
		2-8 (lowgrade)	Fresh	2.62
		Alluvial	Oxide	2.63
		(waste)	Oxide	2.02
		(waste)	Fresh	2.45
		All values are in t/m ³ .		
		• Fresh: BD = (0.0325 x	Fe_2O_3 %) + 0.9707 .72 x Fe_2O_3 %) + 0.3701 Fe_2O_3 %) + 1.4716 reporting of the Australian V	content are as follows: /anadium Project Mineral Resource is based on the regression
Resources into varying confidence categories. mineralisation and grade, consideration of drillh (number of samples used and estimation pass).		ideration of drillhole and de estimation pass).	Resource estimate is based upon continuity of geology, nsity data spacing and quality, variography and estimation statistics resource and applicable for the nominated grade cut-offs.	
	Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).	drillhole spacing from a nomin deposit have drillhole spacings In general, the estimate has be high-grade domain where the generally restricted to the oxid drilling. Inferred Mineral Resource wireframe volumes.	al 80 m to 100 m x 25 m to 3 ranging up to 500 m x 25 m to 3 renging up to 500 m x 25 m to 3 renging up to 500 m x 25 m to 3 renging as Measured M drillhole spacings are less that le high grade and oxide and furce has been restricted to a	the deposit is well drilled for a vanadium deposit, having a 80 m in northing and easting. The lower confidence areas of the to 30 m in northing and easting directions. Ilineral Resource in an area restricted to the fresh portion of the an 80 to 100m in northing. Indicated Mineral Resource material is fresh low grade in the same area of relatively closely spaced my other material within the interpreted mineralisation diffied, due to very low possibility of economic extraction and



Criteria	JORC Code Explanation	Commentary
	Whether the result appropriately reflects the Competent Person's view of the deposit.	Geologica Pty Ltd and Trepanier Pty Ltd believe that the classification appropriately reflects their confidence in the grade estimates and robustness of the interpretations.
Audits or reviews	The results of any audits or reviews of Mineral Resource estimates.	The current Mineral Resource estimate has not been audited.
Discussion of Relative accuracy/ confidence	Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.	The resource classification represents the relative confidence in the resource estimate as determined by the Competent Persons. Issues contributing to or detracting from that confidence are discussed above. No quantitative approach has been conducted to determine the relative accuracy of the resource estimate. The Ordinary Kriged estimate is considered to be a global estimate with no further adjustments for Selective Mining Unit (SMU) dimensions. Accurate mining scenarios are yet to be determined by mining studies. No production data is available for comparison to the estimate. The local accuracy of the resource is adequate for the expected use of the model in the mining studies. Further investigation into bulk density determination and infill drilling will be required to further raise the level of resource classification.
	The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.	These levels of confidence and accuracy relate to the global estimates of grade and tonnes for the deposit.
	These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	There has been no production from The Australian Vanadium Project deposit to date.



Section 4: Estimation and Reporting of Ore Reserves

Criteria	JORC Code Explanation	Commentary
Mineral Resource estimate for conversion to Ore	Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.	The most recent Mineral Resource estimate was declared on 28 November 2018 and has been used in the PFS. Refer to the ASX release of 28 November 2018 for material assumptions and further information.
Reserves	Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.	The Measured and Indicated Resources from Section 3 have been used as the basis for conversion to the Ore Reserve. The Mineral Resources are inclusive of the Ore Reserve.
Site visits	Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is the case.	No site visit was undertaken by the Competent Person. There are no current facilities at the project site.
Study status	The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves. The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.	A Pre-Feasibility Study has been prepared.
Cut-off parameters	The basis of the cut-off grade(s) or quality parameters applied.	The break-even cut-off grade has been calculated based on the pit optimisation inputs. The basis for calculation of cut-off is: $ Cut\ off\ grade = \frac{(process + overhead\ cost) \times (1 + Mining\ Dilution(\%))}{Payable\ Vanadium\ Price \times Process\ Recovery\ (\%)} $ Cut-off grades have been calculated as $0.40\%\ V_2O_5$ for oxide ore, $0.18\%\ V_2O_5$ for transitional and $0.18\%\ V_2O_5$ for fresh. The selected cut-off grade of $0.8\%\ V_2O_5$ is higher than the calculated values as metallurgical testing suggests unpredictable recoveries below this chosen value.



Criteria	JORC Code Explanation	Commentary
Mining factors or assumptions	The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design). The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc. The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling. The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).	The Mineral Resources have been optimised using Whittle software followed by detailed final pit design. The Ore Reserve is the Measured and Indicated Resources within the pit design, after allowing for ore loss and mining dilution. In selecting the optimised pit shell used for pit designs the conservative pit shell with a revenue factor of 0.675 was selected. The mining method selected is open pit, selective mining of ore and waste on nominal 2.5 m benches using a backhoe excavator. Pit ramps are designed at a 10% gradient and 23 m wide, except for lower pit levels where the ramp reduces to 18 m wide and then 15 m. A Pre-Feasibility Study level geotechnical study has been completed by Dempers and Seymour. The pit design parameters from this study have been used for the pit design and the overall pit slope angle was estimated for the preceding pit optimisations. Grade control will be based on additional RC drilling, pit mapping and sampling from production drilling where necessary. A RC drilling pattern of 12.5 m along strike and 6.25 m across strike pattern has been allowed for.
	The mining dilution factors used. The mining recovery factors used. Any minimum mining widths used. The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion. The infrastructure requirements of the selected mining methods.	Mining dilution was estimated to be 5%, at zero grade. This was based on consideration of the width, continuity and orientation of the orebody and the planned mining method. Ore recovery of 95% has been estimated to allow for losses from blasting and grade control. A minimum mining width was set at 20 m. Inferred Resources within the pit design make up 21% of the total Mineral Resources and have not been considered for Ore Reserve estimates. Infrastructure required for the open pit mining operation includes mining contractor workshop, heavy equipment washpad, mining offices, water storage dam, ROM pad, fuel and explosives storage.



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Metallurgical factors or assumptions		The metallurgical process proposed includes beneficiation and refining of the vanadium product and an additional sulphide flotation circuit for base metals recovery, as discussed in Section 3.
	The metallurgical process proposed and the appropriateness of that process to the style of mineralisation. Whether the metallurgical process is well-tested technology or novel in nature. The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied. Any assumptions or allowances made for deleterious elements. The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole. For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?	Metallurgical processes proposed are all well-tested technology and appropriate for the styles of mineralisation. Extensive benchscale metallurgical testwork has been undertaken under the direction of Wood Mining and Metals, as detailed in Section 3 and included: Comminution Magnetic separation Sulphide flotation Preliminary roast leaching of concentrate Metallurgical domaining has been categorised into weathering stages including oxide, transitional and primary mineralisation with and without recoverable base metals, as defined in the Mineral Resource models. Metallurgical recoveries for the concentrator have been determined from testwork and indicate vanadium recoveries of 44% for oxides, variable with depth up to 87.8% for transitional and variable with grade from 76.7% to an expected maximum of 96% for primary material (for a grade of 1.5% V ₂ O ₅). Base metals recovery to a sulphide concentrate has been based on benchscale testwork outcomes up to a primary flotation concentrate and an assumed 90% cleaner flotation recovery. Vanadium recovery in the refinery flowsheet ranges from 79.7% (oxide concentrate) to 80.6% (fresh concentrate) and is based on operating benchmarks and experience from other similar flowsheets and is supported by preliminary benchscale roast leach testwork. Recoveries for the Ore Reserves were applied according to the recovery equations. Deleterious elements are discussed in Section 3.



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Environmen-tal	The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.	Environmental studies have been completed by AQ2. This included studies into: Flora. Fauna. Surface Hydrology. Soil, Waste Rock and Groundwater analysis. All potential environmental and social impacts associated with the Project have been considered and no issue has been identified that cannot be mitigated or managed to an acceptable degree. Further work is required to quantify the potential impact for some aspects, particularly for subterranean fauna. The approvals process will include referral and assessment by the EPA but is not expected to be subject to a Public Environmental Review. Waste geochemistry investigations have been undertaken by interpretation of the geological database indicating that none of the waste rock samples tested were potentially acid generating. Management of surface runoff and seepage from the waste dumps and pit walls during operation will need to be managed and final waste dumps capped with suitable materials to minimise water infiltration.
Infrastructure	The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.	The Sandstone to Meekatharra Road passes close to the mine lease area, however an access road will be constructed from the Northern Highway to the west to the operational area. This road will give access to Meekatharra, which is approximately 55 km away. Power will be generated on site using a gas fired power station using gas from a new gas pipeline. Water will be sourced from onsite pit dewatering and water supply bores. The mining lease is sufficiently extensive to accommodate all the required infrastructure. A communications tower and related equipment will be installed on site for phone and data communications. Accommodation will be constructed on site adjacent to the Project.



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Costs	The derivation of, or assumptions made, regarding projected capital costs in the study.	Capital costs for the plant and most of the rest of the infrastructure were estimated by Wood Mining and Metals. Mining capital costs for heavy equipment workshop and washpad will be part of the mining contract and have been estimated from a contractor quotation.
	The methodology used to estimate operating costs.	Mining operating costs have been based on contractor rates for similar projects in Western Australia and a quotation from a mining contractor that broadly supported the benchmarked mining costs. The average mining costs are \$3.50/t mined. General and administration costs were estimated based on experience with similar projects and make up \$2.24 /t of ore feed. Processing costs have been estimated based on the plant design and detailed costings derived by Wood Mining and Metals.
	Allowances made for the content of	Trocessing costs have been estimated based on the plant design and detailed costings derived by vrood mining and metals.
	deleterious elements. The source of exchange rates used in the study.	Not applicable
		For mining optimisation and design, the exchange rate used was AUD:USD 0.74. The exchange rate used in financial modeling was AUD:USD 0.72. The exchange rate used for capex and opex derivation was set on 8th November 2018 at AUD:USD 0.728, AUD:EUR 0.637 and AUD:GBP 0.555. The exchange rates were sourced from publicly available data produced by banks.
	Derivation of transportation charges.	
	The basis for forecasting or source of	The transport cost related to haulage of the product to the port of Fremantle has been estimated by Wood Mining and Metals. This has been estimated based on a rate A50t$ of V_2O_5 product sold FOB Fremantle. Backhaul rates after delivery of consumables to site have been assumed.
	treatment and refining charges, penalties for failure to meet specification, etc. The allowances made for royalties payable, both Government and private.	Processing and refining costs have been derived by Wood Mining and Metals based on their design of the processing plant and refinery.
	·	The royalty paid to the West Australian government will be 2.5% of revenue.
Revenue factors	The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges,	Revenue for pit optimisation assumes a V_2O_5 sale price of US\$8/lb. This is based on a FOB price for the V_2O_5 flake product. The sales price used for base case financial analysis was US\$8.67/lb V_2O_5 . A table of alternative prices is calculated and presented as upside sensitivity, given the conservative long-term price selected. Revenues from Cobalt, Nickel and Copper are based on LME prices for 13 September 2018 of AUD 84.01/kg, A\$ 16.57/kg and A\$ 7.95/kg respectively. A 65% payability has been assumed for these base metals that make up approximately 1.3% of the total revenue.
	penalties, net smelter returns, etc. The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.	The cyclical nature of the vanadium market is illustrated in 6 of the report summary above. Imbalances in supply have driven prices up above US\$30/lb twice during this time, and there was a prolonged period where prices hovered around US\$5/lb from 2012 to 2017. However, the average price for the 15-year period was well above this, at US\$8.67/lb in 2018 adjusted numbers.



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Market assessment		The market for Vanadium Pentoxide is substantially based on its use in steel alloys and now also in batteries. In the last few years the vanadium price slumped to below US\$5/lb leading to cutbacks in production. The price has now recovered, reaching over US\$30/lb in November 2018. Reasons for the price rise are based on continued low supply from reduced capacity and recent increase in demand from China.
	The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future. A customer and competitor analysis along with the identification of likely market windows for	Demand for vanadium has outstripped supply since mid-2015, corresponding to Evraz Group's Highveld Steel and Vanadium's (South Africa) closure. In late 2015, Chinese stone coal producers began to shut down due to Chinese environmental regulations, further reducing supply. Since then, supply and demand have not been in balance. In 2017, there was approximately 8,000 MTV of demand that was not met by production, or the approximate yearly output of one and a half plants the size of AVL's proposed Gabanintha project.
	the product. Price and volume forecasts and the basis for these forecasts. For industrial minerals the customer	Vanadium Redox Flow Battery (VRFB) technology uptake could have a large impact on medium to long term vanadium demand. If VRFBs capture even a small piece of the renewable energy storage demand, it could require thousands of MTV that are not currently available.
	specification, testing and acceptance requirements prior to a supply contract.	A market assessment analysis has been completed internally with information supplied by Daniel Harris (Technical Director AVL).
		Vanadium products include various oxides of Vanadium, that are converted to Ferro Vanadium or Vanadium Carbo-Nitride products for use in steelmaking. Refined Vanadium pentoxide, V ₂ O ₅ produced as a powder is supplied as a chemical, and can be used in the production of vanadium electrolyte solutions for VRFB.
Economic	The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc. NPV ranges and sensitivity to variations in the significant assumptions and inputs.	The December 2018 Pre-Feasibility Study includes the revenue and cost inputs discussed above and cash flows were discounted by an 8% rate. The post-tax NPV 8% of the project using the long-term historical pricing was estimated to be US\$125M. The mine life is significant but the current benign outlook for inflation does not justify an allowance for inflation. Sensitivity analysis has been completed based on different product price, other revenue related items such as grade and metallurgical recovery and costs. The project is most sensitive to the product price, metallurgical recovery, the mining cost and the processing cost, in decreasing order.
Social		The proposed Project will be located within mining lease application M 51/878, which is currently pending, due to native title processes. The native title claimant is the Yugunga-Nya Native Title Claim Group. A draft mining agreement between AVL and the Yugunga-Nya Native Title Claim Group was prepared in November 2017.
	The status of agreements with key stakeholders and matters leading to social licence to operate.	A standard Heritage agreement is in place with the Yugunga-Nya Native Title Claim Group. No land use agreements are in place with other local landowners but good relations are maintained.
		and and ago agreements and an place with other local landowners but good relations are maintained.



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Other	To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves: Any identified material naturally occurring risks. The status of material legal agreements and marketing arrangements. The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.	No material naturally occurring risks have been identified. No material legal or marketing agreements have been entered into. The Mining Lease Application MLA51/878 over the tenement that contains the Ore Reserves has not yet been granted. Application for the mining approval has not started but there are no impediments expected to this process. The timeframes for assessment of an environmental assessment proposal vary depending on the level of assessment set by the Environmental Protection Authority (EPA), the amount of consultation undertaken prior to referral and how quickly the proponent can compile the information required by the EPA
Classification	The basis for the classification of the Ore Reserves into varying confidence categories. Whether the result appropriately reflects the Competent Person's view of the deposit. The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).	Measured Resources have been converted to Proved Reserves. Indicated Resources have been converted to Probable Reserves. The estimated Ore Reserves are, in the opinion of the Competent Person, appropriate for these deposits. Not applicable
Audits or reviews	The results of any audits or reviews of Ore Reserve estimates.	No audits have been undertaken.



Criteria	JORC Code Explanation	Commentary
Discussion of	Where appropriate a statement of the relative	The Ore Reserve estimate have been completed to Pre-Feasibility Study with ±25 confidence.
relative	accuracy and confidence level in the Ore	
accuracy/	Reserve estimate using an approach or	The Ore Reserve is a global estimate in line with the Mineral Resource Statement
confidence	procedure deemed appropriate by the	
	Competent Person. For example, the	The AVL management and board has extensive experience in managing VTM sources and vanadium operations allowing
	application of statistical or geostatistical	comparison of operation of other plants in South Africa, Australia, USA and Russia to be drawn upon during the study process.
	procedures to quantify the relative accuracy of	
	the reserve within stated confidence limits, or,	
	if such an approach is not deemed appropriate,	
	a qualitative discussion of the factors which	
	could affect the relative accuracy and	
	confidence of the estimate.	
	The statement should specify whether it	
	relates to global or local estimates, and, if local,	
	state the relevant tonnages, which should be	
	relevant to technical and economic evaluation.	
	Documentation should include assumptions	
	made and the procedures used.	
	Accuracy and confidence discussions should	
	extend to specific discussions of any applied	
	Modifying Factors that may have a material	
	impact on Ore Reserve viability, or for which	
	there are remaining areas of uncertainty at the	
	current study stage.	
	It is recognised that this may not be possible or	
	appropriate in all circumstances. These	
	statements of relative accuracy and confidence	
	of the estimate should be compared with	
	production data, where available.	