17 April 2020

KARLAWINDA GOLD PROJECT
ORE RESERVES
INCREASE 35% TO 1.20 MILLION OUNCES

HIGHLIGHTS

- **Karlawinda Gold Project (KGP) Ore Reserves increase by 35% to 1,201,000 ounces from 892,000 ounces.**

- **KGP Mineral Resources increase by 41% to 2,145,000 ounces from 1,525,000 ounces.**

Updated Ore Reserve Estimate

The Capricorn Board is pleased to announce that recent drilling at both Bibra and Tramore deposits has contributed to a significant increase in KGP Ore Reserves to 1,201,000 ounces. Inhouse open-pit optimisations helped to target the drilling areas that would likely result in increased Ore Reserves through conversion of Inferred resources to Indicated.

The KGP JORC compliant Ore Reserves estimate updated to **43.5 million tonnes at 0.9g/t gold for 1,201,000 ounces** compared with the May 2018 estimate of 27.6 million tonnes at 1.0g/t gold for 892,000 ounces. This is a 309,000 ounce (35%) increase.

The Board is also pleased that the updated estimate is a robust Ore Reserve that will maximise mining efficiency:

- Contained gold increases 35% from the 2018 estimate to 1,201,000 ounces.
- **Stripping ratio (waste:ore) reduces significantly from 4.8 to 3.6**.
- **Expected project life increases from 9 years to 12 years**.
- Estimate uses lower cut-off grades of 0.3g/t (laterite & oxide ore) and 0.4g/t (transition & fresh ore) which capture additional economic ore at the **gold price of A$1,600 per ounce** (circa A$1,100/oz lower than current spot price) that was used for the Ore Reserve pit shells.
    - **Mine scheduling will be designed to deliver the >0.5g/t mined ore to the mill and the 0.3 – 0.5g/t mine ore to a stockpile** for processing in later years of the project.
    - **The >0.5g/t ore within the Ore Reserve is 32.1 million tonnes at 1.0g/t for 1,047,000 ounces.** This inventory alone is 155,000 ounces (17%) higher than the 2018 Ore Reserve Estimate of 892,000 ounces at the same grade (1.0g/t) and similar strip ratio of 5.2* (2018: 4.8).
    - **At expected plant throughput rates of 3.5 – 4.0mtpa the >0.5g/t mine to mill schedule should deliver gold production of 105,000 – 120,000 ounces per annum.**
- The updated estimate has reduced the number and complexity of geological domains in the Ore Reserve and as a result is expected to deliver a block model more “fit for purpose” for the large scale equipment and mining processes to be used in the practical open pit mining environment.
- Maximum vertical depth of Ore Reserve open pit design is less than 250 metres.

* calculated treating Ore tonnes between 0.4 – 0.5g/t as waste

Updated Mineral Resource Estimate

The recent drilling has also contributed to **a significant increase in the KGP Mineral Resource Estimate to 2,145,000 ounces**. The KGP JORC compliant MRE updated to 86.7 million tonnes at 0.8g/t gold for 2,145,000 ounces compared to the May 2018 estimate of 51.0 million tonnes at 0.9g/t gold for 1,525,000 ounces. This is a 620,000 ounce (41%) increase.

The MRE was **estimated using a gold price of A$2,000 per ounce** (circa A$700/oz lower than current spot price). In the current very strong gold price environment and with the low stripping ratio of the current Ore Reserve it is very encouraging to note that **the 937,000 ounces of the MRE that are currently not included in the Ore Reserve Estimate are primarily located immediately down dip of the current pit design.**

The maximum vertical depth of the MRE pit shell is 312 metres.

It is expected that these resources will be assessed for addition to the Ore Reserve once the project is operational and a steady state operating cost structure has been established. Any decision to proceed with cut-backs to access additional economic material in the MRE would not need to be made until the middle years of the current 12 year mine life.

This presents significant growth potential to the current mine plan.

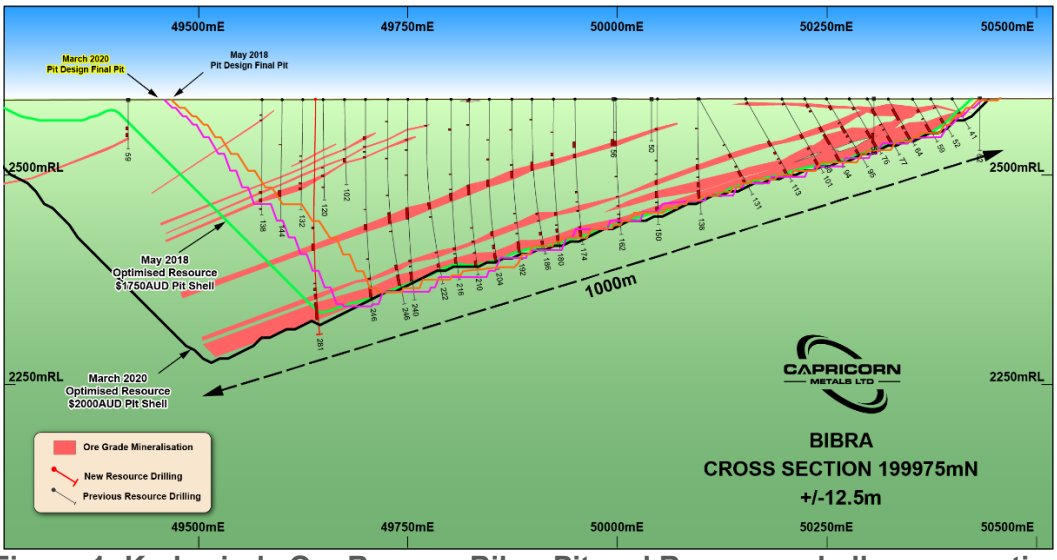


Figure 1: Karlawinda Ore Reserve Bibra Pit and Resource shell cross section

Comment

Capricorn Executive Chairman Mark Clark commented:

"The increase in the Karlawinda gold Ore Reserve to 1,201,000 ounces confirms the project as a standout new fully funded greenfield development project in the Western Australian gold industry. It is a robust, high margin, long life and low technical risk project in arguably the best mining jurisdiction in the world. With construction of the project already underway, the increase in the resource to 2,145,000 ounces and the large, under explored tenement package at Karlawinda offer significant mine life extension opportunity, particularly at the current strong A$ gold price."

ORE RESERVE

The Company is pleased to provide an updated JORC 2012 compliant Ore Reserve estimate of **43.5 million tonnes @ 0.9g/t Au for 1,201,000 ounces** for the Bibra Deposit (including the Southern Corridor pit) at the Karlawinda Gold Project, which is based on an updated Mineral Resource estimate of **86.7 million tonnes @ 0.8g/t Au for 2,145,000 ounces.**

The Ore Reserve is contained within a detailed open pit design (Figure 2) with a life of mine (LOM) stripping ratio of 3.6:1.

TABLE 1: KARLAWINDA OPEN PIT ORE RESERVE STATEMENT

			Proved			Probable			Total Ore Reserve		
Deposit	Type	Cut-Off	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
Bibra	Open Pit	0.3 <	-	-	-	39.0	0.9	1,090	39.0	0.9	1,090
Southern Corridor	Open Pit	0.3 <	-	-	-	4.6	0.8	111	4.6	0.8	111
Total	Total		-	-	-	43.5	0.9	1,201	43.5	0.9	1,201

Notes:
1. *Ore Reserves are a subset of Mineral Resources.*
2. *Ore Reserves are calculated using a gold price of A$1600/ounce.*
3. *Ore Reserves are calculated using a cut-off grade between 0.3g/t and 0.4g/t Au.*
4. *The above data has been rounded to the nearest 100,000 tonnes, 0.1 g/t gold grade and 1,000 ounces. Errors of summation may occur due to rounding.*

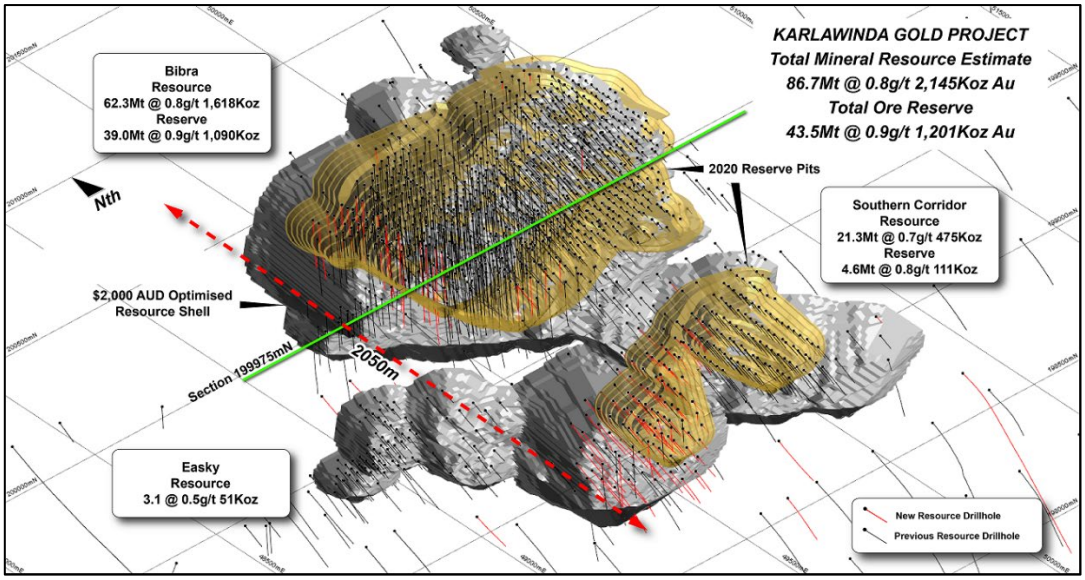


Figure 2: Karlawinda Ore Reserve pits (gold) and Mineral Resource pit shells (grey).

MINERAL RESOURCE

An updated Mineral Resource estimate for the Karlawinda Gold Project is provided below. The Ore Reserve statement (above) is a subset of these updated resources.

TABLE 2: KARLAWINDA OPEN PIT MINERAL RESOURCE

			Indicated			Inferred			Total Mineral Resources		
Deposit	Type	Cut-Off	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
Bibra	Open Pit	0.3 <	51.5	0.8	1,374	10.8	0.7	244	62.3	0.8	1,618
Southern Corridor	Open Pit	0.3 <	14.4	0.7	324	6.9	0.7	151	21.3	0.7	475
Easky	Open Pit	0.3 <	1.3	0.6	24	1.8	0.5	28	3.1	0.5	51
Total	Total		67.2	0.8	1,722	19.5	0.7	422	86.7	0.8	2,145

Notes:
1. *Mineral Resources are calculated using a gold price of A$2000/ounce.*
2. *Mineral Resources are calculated using a cut-off grade between 0.3g/t and 0.4g/t Au.*
3. *The above data has been rounded to the nearest 100,000 tonnes, 0.1 g/t gold grade and 1,000 ounces. Errors of summation may occur due to rounding.*

ORE RESERVE ESTIMATION

The Ore Reserve estimate has been completed on the basis of Modifying Factors used in the Company's November 2017 Feasibility Study (FS) and updated by subsequent studies including further optimisation and trade-off studies on the process plant and non-plant infrastructure. These studies were completed by a team consisting of Capricorn personnel and independent external consultants. Key points of this work include:

- Revised process plant design incorporates tertiary crushing, single Ball Mill comminution circuit followed by a conventional gravity and carbon in leach (CIL) process to treat the ore.
- Power will be generated on site utilising natural gas via a 56km pipeline connecting to the Goldfields Gas Pipeline (GGP).
- The gold price assumption for Ore Reserves has remained at A$1600/oz. This reflects the spot gold prices over the past 5 years and is well below current spot price.
- Ore Reserve pit design, staging and scheduling completed by Entech Pty Ltd in consultation with Capricorn personnel.
- Ore processing costs have reduced from the 2018 Ore Reserve as a result of improved plant throughput and efficiency to $9.78 / t for laterite ore, $9.57/t for oxide, $10.50/t for Transition and $11.73/t for fresh ore.
- A Mining Proposal (including a Closure Plan) has been approved and environmental approvals for the mining and water supply aspects of the project have been issued by the Department of Mines, Industry Regulation and Safety (DMIRS). A Native Vegetation Clearing Permit has been granted for the project site. The Mining Proposal will be updated for mining and processing of the increased Ore Reserve.
- Department of Water and Environmental Regulation (DWER) have granted a works approval under the Environmental Protection Act 1986 to construct a **3.5 – 4.0mtpa** gold processing plant and tailings storage facility, inert and putrescible landfill and sewage facility at the Karlawinda Gold Project. These approvals will be amended to allow for the processing of the increased Ore Reserve.

Financial modelling completed confirms that the project is economically viable under current assumptions. In the opinion of the Competent Person, cost assumptions and Modifying Factors applied in the process of estimating Ore Reserves are reasonable. The Ore Reserve is considered to provide the basis of a technically and economically viable project. The proposed mine plan is technically achievable. All proposals for the operational phase involve the application of conventional technology which is widely utilised in Western Australia.

All other material assumptions are largely unchanged since the 2018 Ore Reserve but have been considered as part of the Ore Reserve estimation process and are detailed below.

Karlawinda Gold Project Location and Tenure

The Karlawinda Gold Project is located in the Pilbara region of Western Australia, 70km by road south-east of the town of Newman.

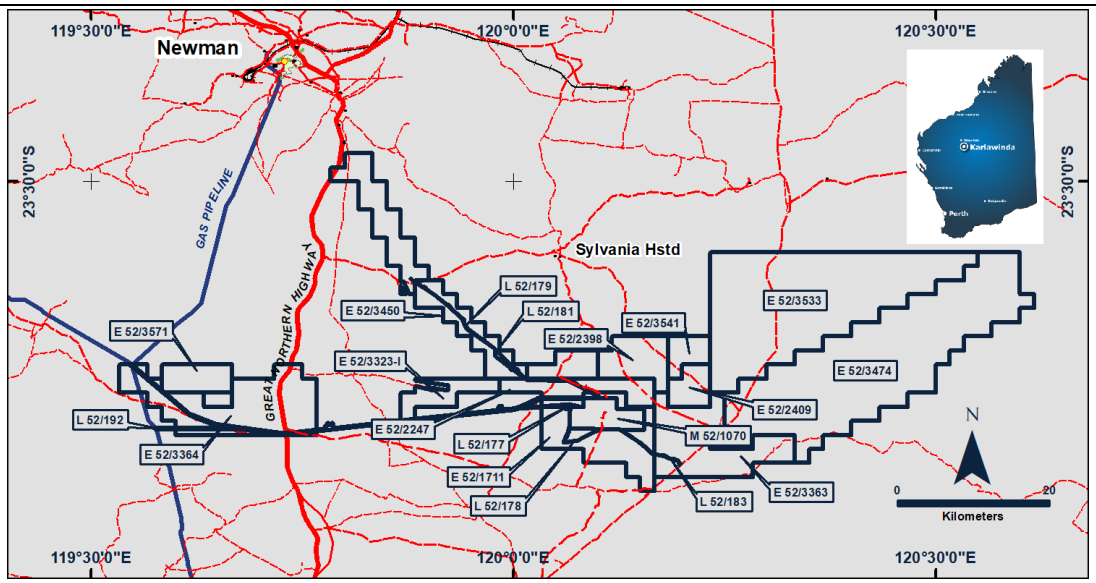


Figure 3: Location Map: Karlawinda Gold Project

Karlawinda is an advanced gold project which includes the Bibra deposit and numerous outstanding exploration targets including the Francopan prospect. The Project covers a total area of approximately 1,419km^2.

Capricorn completed a positive Scoping Study in July 2016, which was based on a single large open pit at Bibra feeding a 3Mtpa standalone CIP (carbon-in-pulp) processing facility on site. Annual gold production was forecast to average around 100,000oz/pa over an initial mine life of approximately 7 years.

In Nov 2017, Capricorn completed a Feasibility Study ('FS') on the development of the Karlawinda Gold Project. This study was underpinned by a major 75,000m in-fill RC and diamond drilling program completed in December 2016.

The Bibra deposit is covered by mining lease M52/1070 100% held by Greenmount Resources Pty Ltd, (Greenmount) a wholly owned subsidiary of Capricorn. M52/1070 is a granted mining lease of sufficient size to cover the Bibra resource area and with the granted ancillary miscellaneous licences the associated infrastructure for a future mining operation. M52/1070 was excised upon grant from exploration licence E52/1711. That exploration licence was acquired from BHP Billiton Ltd (BHPB) in 2008 by Independence Group NL. Greenmount subsequently acquired E52/1711 in 2015. South 32 Limited (via BHPB) retain a 2% NSR over E52/1711 and any successor tenements, including M52/1070.

Western Australia is recognised globally as a low risk mining jurisdiction.

The Nyiyaparli People hold Native Title over M52/1070 and the ancillary miscellaneous licences. There are no known heritage or environmental impediments over the mining lease. Capricorn has entered into a Land Access Agreement with the Nyiyaparli People over the mining lease and all other project tenure. No known social or environmental impediments exist with respect to the proposed mining operation.

Regional Infrastructure

The project site is within economic distances of existing infrastructure in the east Pilbara region. The town of Newman contains world class engineering, mining support services and key infrastructure including a major airport and power station and will act as a logistics base for the project. The project is planned to operate as a Fly In-Fly Out (FIFO) operation. However, there is the opportunity for Newman to be a residential base for project employees. Services and consumable supplies will be delivered by existing roads and a new 40km Access Road from the Great Northern Highway to the project.

Land availability is not considered an issue, with the mining and exploration tenure held by Capricorn covering all project requirements. The proposed mining area lies at the northern boundary of the Weelarrana pastoral lease and the Company has a co-operative working relationship with all pastoralists over the project area.

Bibra Deposit Geology

At Bibra, mineralisation is shoot-controlled along a series of dominant low-angle, north-east trending mineralised faults that combine to make up a very large-scale mineralised system. The system is hosted in a sequence of Archaean greenstones metamorphosed to amphibolite facies. The greenstones comprise a mafic volcanic sequence with interbedded sedimentary and volcanoclastic units.

The deposit has been defined by drilling over a 1.8km strike length and is drilled to 800m down-dip where it is still mineralised and open down-dip. The mineralised shoots are present in drilling as broad zones up to 50m wide and are continuous down plunge. It is thought the shoots are developed in dilation zones along the main structures. A large laterite and oxide weathering zone is developed over the primary geology and this is mineralised in the near surface, up-dip position of the main shoots of primary mineralisation. A thin veneer of transported sandy soil covers the deposit and is typically less than 3m thick, the transition/fresh rock boundary is about 60m below surface.

Geological logging suggests alteration consisting of biotite, carbonate and magnetite mineralisation forms a halo surrounding the intense silica, pyrite and gold mineralisation. The metamorphic overprint of the mineralisation may have altered some of the primary alteration and mineralisation to the present day mineral species.

Confidence in the geological interpretation is high. The stratigraphy is consistent and can be correlated between holes and along strike.

Geological logging and structural measurements from drillholes have been used to construct the geological resource model. Sections were interpreted, digitised and a three dimensional (3D) wireframe model constructed.

Mining Assumptions

The Bibra deposit will be mined by open pit mining methods using conventional mining equipment. The selected mining method, design and extraction sequence are tailored to suit orebody characteristics, minimise dilution and ore loss, defer waste movement, minimise rates of vertical mining advance, utilise planned process plant capacity and expedite free cash generation in a safe manner. The open pit has been scheduled based on realistic mining productivity with readily achievable mining rates along with consistent material movements.

The mining operating costs have been calculated from contractor quotes for drilling, blasting, loading and haulage which require the contractor to provide all equipment. Cost estimate studies for grade control have been completed by Capricorn with a suitable allowance made on a per ore tonne basis.

Mining dilution and mining recovery modifying factors are accounted for in the estimation of the Mineral Resource mainly from the low cut-off used for the estimation domains and the block size estimated at SMU dimensions.

Geotechnical Modelling

Geotechnical modelling has been completed by an external consultant based on field logging and laboratory testing of selected diamond drill core samples from 18 drilled for purpose geotechnical diamond drillholes. The open pit designs are based on the recommended geotechnical design parameters and assume dry slopes based on the assumption of adequate dewatering and/or depressurisation ahead of mining.

The low-angle dip of the deposit (28° to West) allows for a designed overall batter angle on the Footwall (Eastern side of pit) between ramps of 25°. The western wall (Hanging Wall) of the pit is designed to have an overall slope angle of 49.8°. Identical slope angles are used in the Southern Corridor pit, following analysis of two geotechnical diamond drillholes.

A separate hydrogeological report was prepared by independent consultants which considered the requirements to effectively dewater the open pit and pit slopes. This study was supported by the development of test bores and field test pumping analysis. The water quality of the defined aquifer at Karlawinda is low in total dissolved salts and only requires minor treatment to make potable.

Mining Infrastructure

The proposed mine plan includes waste rock dumps, a ROM pad, a surface water diversion channel, surface dewatering bores, light and heavy vehicle workshop facilities, explosives storage, supply facilities, technical services facilities, accommodation camp and administration facilities.

Metallurgical and Processing Assumptions

An optimised flowsheet, mass and water balances, equipment selection, and plant designs and layouts were all developed to FS standard based upon several phases of testwork.

The testwork was conducted on 35 composites (30 variability and 5 master) prepared from 779 meters of diamond drill core, totalling 90 intervals from 52 drill holes. These samples amount to 4,103kg and represent the four main weathering horizons in the Bibra deposit.

The test work demonstrated Bibra ore contains a gravity recoverable gold component and is free milling with high gold extractions achievable by conventional cyanidation.

Flowsheet

The proposed metallurgical flowsheet is commonly used in the Australian and international gold mining industry and is well-tested and proven technology.

It comprises of a comminution circuit which consists of a three stage crushing plant providing crushed ore to a crushed ore stockpile followed by a milling circuit which consists of a 7.5MW ball mill and cyclone classification. Gold recovery involves a conventional gravity circuit and Carbon-in-Leach (CIL) circuit. Gold is recovered by standard elution and electrowinning techniques prior to smelting. The tailings are placed in an Integrated Waste Landform (IWL) and water recovered and recycled. Reagent consumptions are all relatively low.

Comminution

Modelling of the comminution circuit for the Karlawinda Gold Project was undertaken by Orway Minerals Consultants (OMC) and others. Final circuit selection provides for a flexible flowsheet able to suitably treat the range of ores over the project life with the target throughput rates of 4MTPA for fresh ore and 5MTPA in oxide ore.

Metallurgical Recovery

Over 120 leach tests were performed on the various Bibra ores over the various testwork programs. The work showed that all ores were free milling, have a lower sensitivity to grind size, and with the gravity gold component removed is fast leaching with low reagent consumptions.

Estimated plant gold recovery ranges from 91% to 94% depending on grind size, head grade and ore type. An average of 25% of gold from oxide ore and 45% from fresh ore is estimated to be recovered by gravity methods. No deleterious elements of significance have been determined from metallurgical test work and mineralogy investigations.

Reagent Consumption

Reagent consumption estimates used in the Ore Reserve are based on various gold recovery and comminution test work and are considered to be relatively low when compared to similar Archaean greenstone deposits.

Tailings Disposal

Tailings disposal is intended to be within an Integrated Waste Landform (IWL) whereby tailings are encapsulated by mining waste, rather than having separate waste dumps and tailings facilities.

Infrastructure

The workforce will be Fly In-Fly Out (FIFO) and based at a dedicated camp on the mining lease during rostered days on. Either commercial flights to Newman airport, 55 km north of the Project or an onsite airstrip will be used.

Pump testing and modelling of the potential yield from the Karlawinda borefield indicate that there is sufficient groundwater to service the needs of the Project for the life-of-mine. This will require the development of numerous water production bores, of which 5 have already been developed. Miscellaneous licence applications to secure the tenure required for the all infrastructure not covered by Mining Lease have been approved.

Power will be generated on site utilising natural gas reticulated from the GGP. Cost assumptions used in the estimation of the Ore Reserve are based on quotes and consumption estimates for the revised processing plant configuration.

Cost and Economic Assumptions

The operating cost estimate is appropriate for the current market in Western Australia. Cost inputs have been estimated from quotations and/or by competent specialists.

Capital Costs for process plant and infrastructure are estimated in Australian dollars. In terms of determining whether the Ore Reserves can form the basis of a technically and economically viable project, the key capital cost estimates for the processing plant construction were based on prices from suppliers and contractors and on prices from recent processing plant builds. Pre-mining capital costs and sustaining capital costs are understood and estimated to a FS level of accuracy. Any modification to these costs in the FS are not considered to have a material negative impact on this Ore Reserve estimate.

Gold bullion transportation and refining charges are derived on the basis of a quote provided by a leading Australian gold refinery.

An allowance has been made for all royalties, including an allowance of 2.5% of revenue for royalties payable to the Western Australian State Government and a 2.0% allowance for the current commercial royalty to South 32. The terms of the royalty payable to the other private party is covered by confidentiality restrictions.

A Life-of-mine (LOM) gold price forecast of A$1,600/ounce is applied in the Ore Reserve estimation process. This price forecast was established by Capricorn based on historical A$ gold price trends over the last five years and by comparison against peer companies. Net present value (NPV) and free cashflow analysis of the Ore Reserve based on the key assumptions used in the estimate and sensitivity analysis of them indicates that the project retains a suitable profit margin against reasonable future commodity price assumptions.

Construction of the project has commenced and various contract negotiations have been finalised or are under negotiation. There are reasonable prospects to anticipate that contract terms assumed in the Ore Reserves estimate will be achieved.

Social and Environmental

Flooding risk has been analysed by an independent external expert and deemed to be minimal.

No significant flora or fauna species, including subterranean species have been identified that would be significantly impacted by the Project in a manner that could not be adequately managed.

Waste rock and tailings characterisation work has been completed and all waste types and tailings are non-acid forming and have limited metal leachate potential.

All mining tenure required for the Project has been obtained. Approvals required to enable the project to commence development and operation have been obtained. Some approvals will need to be amended to enable mining and processing of the increased Ore Reserve.

MINERAL RESOURCE

As part of the Ore Reserve process Capricorn Metals Limited has updated the Mineral Resource estimate at its 100%-owned Karlawinda Gold Project in WA. The new resource has been updated to include a further 23,102m of drilling mainly at Southern Corridor, which has converted the western half from Inferred to Indicated. The new March 2020 Mineral Resource is now reported using the Ore Reserve variable cut off grades of 0.3g/t for Laterite, 0.3g/t for Oxide, 0.4g/t for transitional and 0.4g/t for fresh material. The new cut off grades have been used to ensure the new Ore Reserve sits wholly inside the reported Mineral Resource. Key points from the resource update are listed below:

- 80% of the Mineral Resource is classified in the Indicated category.
- An Indicated Resource totalling 67.2 million tonnes @ 0.8g/t Au for 1.7 million ounces.
- A large portion of the Southern Corridor Mineral Resource has been elevated from Inferred to the Indicated classification.
- Ounces per vertical metre peak at over 12,000 between 80 and 140m from surface (Figure 4 below).

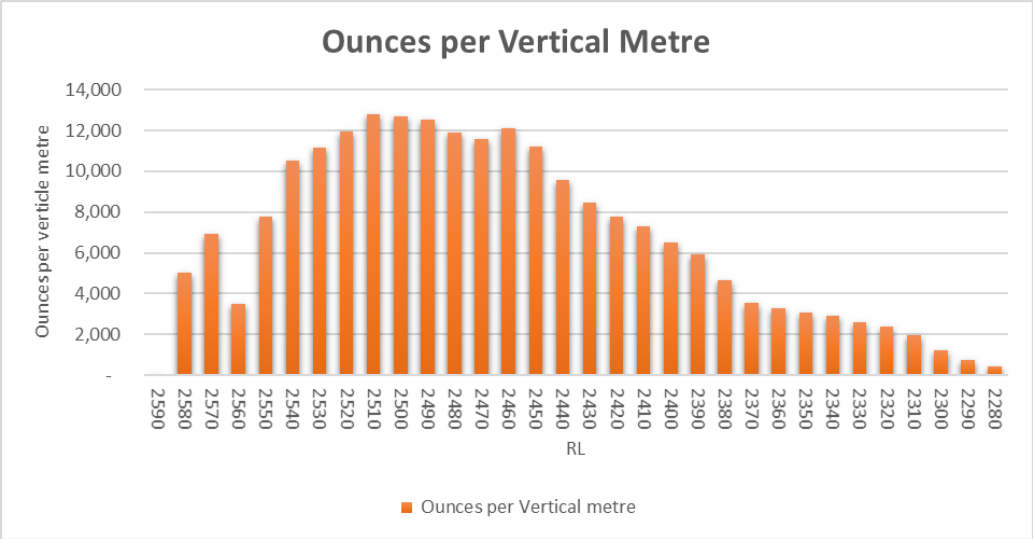


Figure 4: Bibra Mineral Resource ounces per vertical metre

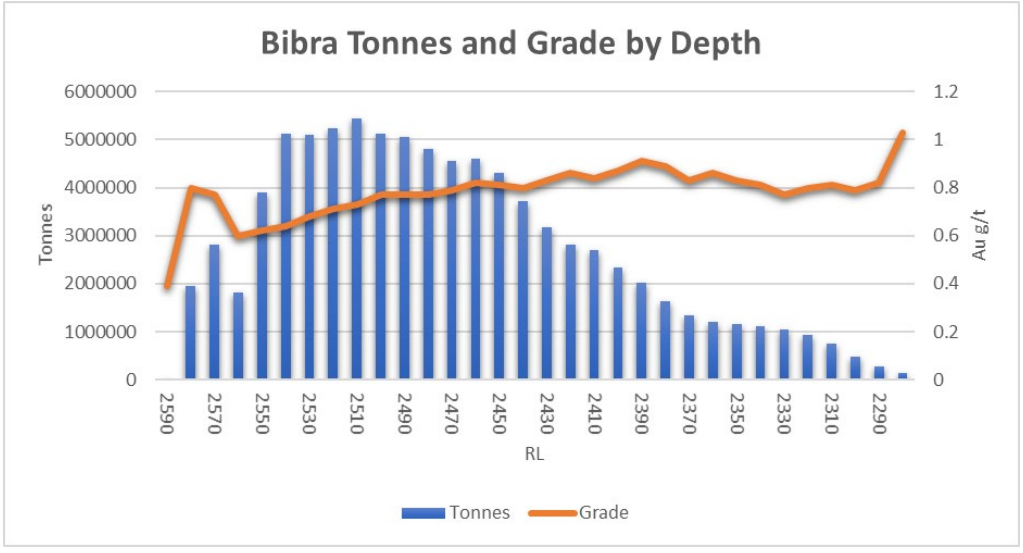


Figure 5: Bibra Tonnes and Grade by depth in metres (2590 RL is Surface)

Mineral Resource Estimation Methodology and Data

The following information is provided as an addendum to meet the requirements under listing rule 5.8.1. This information is provided in detail in the attached JORC Table 1 (Appendix 1).

Bibra is part of a large-scale Archaean aged gold mineralised system. The geology at Bibra predominantly comprises a sequence of alternating Archaean amphibolites and quartz-feldspar-chlorite-garnet schists with the majority of mineralisation hosted in silicified and magnetite altered, mylonitised “psmammites”. Gold mineralisation has developed on at least two parallel, 40m thick, shallow dipping sandstone units, which dip to the west-north-west at 22°. Laterite mineralisation has developed over the structures close to surface. Outside of the main mineralisation some smaller discrete lodes occur in the hanging wall. Mineralisation continues south of the main pit area into the Southern Corridor where mineralisation is hosted in volcanoclastic sandstones with broad lower grade mineralisation with zones of high grade mineralisation. The primary mineralisation is marked by 3-10% sulphides, subhedral magnetite grains, quartz veins/veinlets, and gold. Gold mineralisation is strata-form with lineations identified as controlling higher-grade shoots. The overall footprint of the mineralisation covers an area of 1800m (local grid N) by 1800m (local grid E). The deposit is oxidised to average depths of 50-70m.

Drilling Techniques

In total 182,863 metres of drilling has been completed within the constraints of the Bibra resource consisting of 92 diamond holes (13,983m/ 8%) and 1,283 Reverse Circulation drillholes (168,880/ 92%).

The drilling database consists of high quality RC and diamond drillholes with holes drilled at approximate spacings of 25m x 25m to 25m x 50m in the Indicated category area and 50m x 50m to 100m x 100m in the Inferred category area. Deeper holes and wider spaced drilling targeting along strike, down-dip and down-plunge extensions of the Bibra mineralisation have also been completed outside of the classified resource area and included in the model. However, currently this material remains unclassified/not reported and is a target for future resource development drilling.

Sampling and Sub-Sampling Techniques

Drilling at the Bibra deposit has been completed by two companies: Independence Group (IGO) and Capricorn Metals Group (CMM). The methods of collection have been very similar in terms of sampling procedures, drilling methods and sampling quality.

2kg - 3kg samples RC were split from dry 1m bulk samples. The sample was initially collected from the cyclone in an inline collection box with independent upper and lower shutters. Once the metre was completed, the drill bit was lifted off the bottom of the hole, to create a gap between sample, when the gap of air reached the collection box the top shutter was closed off. Once the top shutter was closed, the bottom shutter was opened, and the sample was dropped under gravity through a Metzke cone splitter. Once drilling reached fresh rock a fine spray of water was used to suppress dust and limit the loss of fines through the cyclone chimney. A second 2kg-3kg sample was collected at the same time the original sample as a field duplicate.

The diamond drillholes were saw cut, with one half being sent to the laboratory. Diamond core was sampled dominantly to 1 metre intervals, some smaller samples were collected where the core was sampled to geological/mineralisation contacts.

QAQC protocols have been executed to a high standard. QA/QC programs were implemented to test the quality of drilling, assaying and logging. In the drilling programs, samples were weighed to determine drillhole quality through the analysis of sample recovery and split ratio. It was shown through the gathering of this information, that the drilling was completed to a high standard with overall recovery greater than 80% and the split ratio through the splitter showing no material bias.

Sample Analysis Method

RC and diamond core samples were sent to Intertek, Genalysis or Aurum laboratories in Perth, where the samples were oven dried at 105°C. After drying, the core was crushed to a nominal 2mm and then both RC and diamond core were pulverised LM5 mills to 5 minutes to achieve 85% passing 75µm to provide a pulp sample for analysis. All samples submitted by CMM were analysed for Au using the FA50/MS technique, which is a 50g lead collection fire assay. The sample submitted by IGO were analysed by FA50/AAS which is a 50g lead collection fire assay.

Field duplicates were collected at a ratio of 1:20 through the mineralised zones (1:40 elsewhere) and collected at the same time as the original sample through the B chute of the cone splitter. OREAS certified reference material (CRM) and matrix matched CRMs were inserted at a ratio of 1:20 through the mineralised zone (1:40 elsewhere). The grade ranges of the CRMs were selected based on grade populations and economic grade ranges. The duplicate and CRMs were submitted to the lab using unique sample IDs.

Estimation Methodology

Three-dimensional wireframes were created to constrain the mineralisation and allocate geology to the block model. Surpac software was used for the wireframing of the ore and weathering profiles, Micromine software was used for the wireframing of geology. The Bibra mineralisation wireframe models were built using sectional interpretation and visualization of the mineralisation in three-dimensions. The sectional mineralisation strings were defined with a cut-off grade of 0.1g/t Au. There are four main domains and a Laterite domain. Located outside the Main Bibra Pit area, there are several other resource areas such as Easky, which were included in the estimate. The area previously referred to as Tramore has been included within the Southern Corridor area for this estimation update. The interpretation and wireframes of geology were built by on-site geologists to ensure the interpretation consistency. Geological logging and structural measurements from drillholes has been used to construct the geological model. Geological continuity has been assumed along strike and down-dip.

A block model was created to encompass the Bibra mineralisation and prospects in close proximity. 10 X by 10 Y by 5 Z is the parent block size, with sub-blocking only in the Z direction to reflect the flat lying geometry of the laterite portion of the deposit. Variography was undertaken on domains using Surpac software and that variography was used to undertake Kriging neighborhood analysis to optimise the block size, search distances and min/max sample numbers used. Search ellipses were also developed from the variography. The block model grades were estimated using ordinary kriging grade interpolation techniques constrained within the mineralisation wireframes. All work was completed in the local grid co-ordinate system. The estimation was completed in three passes with the following parameters;

Pass 1 non laterite: 16/64 min and max samples using an octant search, 40m search distance in the major direction, maximum of 4 samples used per hole, and a maximum of 4 adjacent octants failing to have the required composites. Block size estimated into is 10m/10m/5m XYZ.

Pass 1 laterite: 8/24 min and max samples using an ellipsoid search, 40m search distance in the major direction, maximum of 4 samples used per hole. Block size estimated into is 10m/10m/2.5m XYZ.

Pass 2 non laterite: 16/64 min and max samples using an octant search, 60m search distance in the major direction, maximum of 4 samples used per hole, and a maximum of 4 adjacent octants failing to have the required composites. Block size estimated into is 10m/10m/5m XYZ.

Pass 2 laterite: 8/24 min and max samples using an ellipsoid search, 60m search distance in the major direction, maximum of 4 samples used per hole. Block size estimated into is 10m/10m/2.5m XYZ.

Pass 3 non laterite: 8/64 min and max samples using an octant search, 100m search distance in the major direction, maximum of 4 samples used per hole, and a maximum of 8 adjacent octants failing to have the required composites. Block size estimated into is 20m/20m/10m XYZ.

Pass 3 laterite: 8/24 min and max samples using an ellipsoid search, 100m search distance in the major direction, maximum of 4 samples used per hole. Block size estimated into is 10m/10m/2.5m XYZ.

Top-cuts were applied to sample composites, with a high grade restriction utilised to limit the influence of higher grade data, particularly outside of the high grade zones. The high grade restriction is an indicator estimate completed at 1 g/t.

Density assumptions were based on 3,976 samples water immersion method density readings. Average densities for oxidation profiles were assigned to the block model.

The block model was validated using various techniques. These techniques consisted of visual checking, domain assay Vs block model grade and Swath plots. The new resource was also checked against an independently completed MIK estimate to make sure they were comparable.

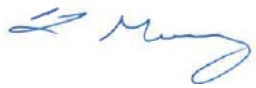
Resource Classification Criteria

The Indicated and Inferred classification reflects the relative confidence in the estimate, the confidence in the geological interpretation, the drilling spacing, input data, the assay repeatability and the continuity of the mineralisation.

Indicated classification was assigned from pass 1 and 2 of the estimation which roughly corresponds with 25m x 25m to 25m x 50m drill spacing. The Inferred classification was assigned from pass 3 of the estimation where the drill spacing was from 25m x 50m to 100m x 100m. This classification reflects the Competent Person's view of the deposit.

Mining and Metallurgical Methods and Parameters

Refer above to Ore Reserves section of this release.



For and on behalf of the Board
Kim Massey
Chief Executive Officer

For further information, please contact:

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Competent Persons Statement

The information in this report that relates to Mineral Resources is based on information compiled by Mr. Jarrad Price who is Resource Geologist and an employee of the Company. Mr. Jarrad Price is a current Member of the Australian Institute of Geoscientists and has sufficient experience, which is relevant to the style of mineralisation and types of deposit under consideration and to the activities undertaken, to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code of Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr. Price consents to the inclusion in the report of the matters based on the information in the form and context in which it appears.

The information in this report that relates to Ore Reserves is based on information compiled by Mr Daniel Donald. Mr Donald is an employee of Entech Pty Ltd and is a Member of the Australian Institute of Mining and Metallurgy (MAusIMM, #210032). Mr Donald has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity currently being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code of Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr. Donald consents to the inclusion in this report of the matters based on the information in the form and context in which it appears.

Appendix ONE
JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	Drilling at the Bibra deposit has been completed by two companies Independence Group (IGO) and Capricorn Metals Group LTD (CMM) using a combination of Reverse Circulation (RC) and diamond drilling (DD). The methods of collection have been very similar in terms of sampling procedures, drilling methods and sampling quality. For RC drilling from 2015 onwards the standard method of sample collection includes the following: 2kg - 3kg samples are split from dry 1m bulk samples. The sample was collected through a cyclone and cone splitter. Once drilling reached fresh rock a fine spray of water was used to suppress dust and limit the loss of fines thorough the cyclone chimney. A second 2kg - 3kg sample was collected at the same time as the original sample. This sample was stored on site and retained for follow up analysis and testwork. The bulk sample of the main ore zone was discharged from the cyclone directly into green bags. The bulk sample from the waste was dumped into piles on the ground. During the sample collection process, the cone split original and duplicate calico samples and the reject green bag samples were weighed to test for biases and sample recoveries. The majority of the check work was undertaken through the main ore zones. Upon determination that there were no sampling problems in 2019 drilling continued without these measures. RC Field duplicates were collected at a ratio of 1:20 through the mineralised zones (1:40 elsewhere) and collected at the same time as the original sample through the B chute of the cone splitter. For the diamond drilling, core was half cut in half using a corewise automatic core saw. Matrix matched CRMS and OREAS certified reference material (CRM) were inserted at a ratio of 1:20 through the mineralised zone (1:40 elsewhere). The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. In 2012, RC samples were collected for 1m intervals using a rig-mounted cone splitter. Wet samples were grab sampled and recorded as such in the database, few were within mineralised zones. NQ core was half-core sampled and HQ/HQ3 core was initially quarter-core sampled. Issues with quarter-coring in the regolith with complete disintegration of the sample and loss of material were identified, and reverted to half-core sampling with less water for better sample quality. Standards, blanks and field duplicates were inserted into each batch of samples submitted to the laboratory. Prior to 2011, RC samples were collected at the rig using a cone splitter. RC samples were originally composited to 2m by taking scoops from each of the 1m interval and submitted to Genalysis for sample preparation and analysis. Samples that returned values >0.5g/t Au

Criteria	JORC Code explanation	Commentary
		were submitted as 1m samples to Genalysis. In 2011, RC samples were not composited and 1m interval samples were sent directly to Genalysis. A rig mounted cone splitter was used to split the samples. NQ2 core was half-core sampled and PQ and PQ3 core was quarter-core sampled using a manual core-cutting diamond saw without water in the oxide zone. The dry cutting was to prevent loss of clays for the metallurgical samples. Sample quality is considered to be good and all RC drilling within the resource area was dry.
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	RC drilling rigs operated by Ranger, Profile and Blue Spec were used to collect chip samples over the numerous programmes. Some early drilling used face-sampling bits of 135mm diameter, with the majority of holes using 140mm diameter. Diamond drilling rigs operated by Westralian Diamond Drillers, Blue Spec, Boart and Foraco were used to collect diamond core samples over the numerous programmes. NQ2, PQ3, PQ, HQ3 and HQ are the core sizes collected. RC precollars were regularly used through barren zones and range from 20m to 200m. Core was orientated by Reflex ACE and Ezymark orientation tools.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	During the sample collection process, the cone split original and duplicate calico samples and the reject green bag samples were weighed to test for biases and sample recoveries. The majority of the check work was undertaken through the main ore zones. This process showed that the majority of ore grade samples had recoveries greater than 80%. Recovery measurement and weighing of bulk sample was discontinued after samples were determined to be of good quality. Once drilling reached fresh rock a fine spray of water was used to suppress dust and limit the loss of fines thorough the cyclone chimney. At the end of each metre the bit was lifted off the bottom to separate each metre drilled. The majority of samples were of good quality with ground water having minimal effect on sample quality or recovery. From the collection of recovery data, no identifiable bias exists. In 2012, RC sample recovery was variable, particularly in the regolith. Sample quality was recorded during logging and qualitative recovery codes were assigned to each sample. Sample weights were measured for each component of RC hole cuttings in mineralised zones, with results showing that regolith samples were generally poor quality (both under and over-weight samples) and quality was moderate in the other zones. Core was reassembled for mark-up and was measured, with metre marks and down-hole depths placed on the core. Depths were checked against driller's core blocks and discrepancies corrected after discussion with drillers. Core loss was recorded in the geological log. Core recovery was generally good. RC sample recovery prior to 2012 has been logged as good with samples kept dry during drilling. There is no obvious relationship between sample recovery and grade.

Criteria	JORC Code explanation	Commentary
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	Reverse circulation chips were washed and stored in chip trays in 1m intervals for the entire length of each hole. Chips were visually inspected and logged to record lithology, weathering, alteration, mineralisation, veining and structure. Data on rocktype, deformation, colour, structure, alteration, veining, mineralisation and oxidation state were recorded. RQD, magnetic susceptibility and core recoveries were recorded. RC chips sample quality and weights were also recorded, including whether wet or dry. Logging is both qualitative and quantitative or semi-quantitative in nature. Core was photographed both dry and wet.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	For RC holes drilled since March 2016 (since hole KBRC284) samples were split from dry, 1m bulk sample via a cone splitter directly from the cyclone. The quality control procedure adopted through the process includes: Weighing of both Calico samples and reject sample to determine sample recovery compared to theoretical sample recovery and to check sample bias through the splitter. This practice was discontinued during the 2019 programme once good sample quality and recovery was verified. Field duplicates were collected at a ratio of 1:20 through the mineralised zones (1:40 elsewhere) and collected at the same time as the original sample through the B chute of the cone splitter. OREAS certified reference material (CRM) was inserted at a ratio of 1:20 through the mineralised zone (1:40 elsewhere). The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. The duplicates and CRM's were submitted to the lab using unique sample ID's. 2kg – 3kg RC samples are submitted to the laboratory. Samples are oven dried at 105°C then jaw crushed to -10mm followed by a Boyd crush to a nominal -2mm. Samples were rotary split to 2.5kg. Samples were then pulverised in LM5 mills to 85% passing 75µm under sample preparation code EX03_05 which consists of a 5 minute extended preparation for RC/Soil/RAB. The extended time for the pulverisation is to improve the pulverisation of samples due to the presence of garnets in the samples. All the samples were analysed for Au using the FA50/MS technique which is a 50g lead collection fire assay. All core has been cut into half or quarter core for sampling. For early drillholes KBRC005-010, RC composite samples (2m) were submitted to Genalysis where they were sorted, dried and the total sample pulverised in a single stage mix and grind if the sample mass was <3kg. Samples >3kg mass were riffle split using a 50:50 splitter and one half pulverised. Samples were analysed for Au using an aqua regia digestion (AR10/OM) of a 10g pulp sample with ICP-MS determination. Samples that returned values

Criteria	JORC Code explanation	Commentary
		>0.5g/t Au were submitted to Genalysis as 1m resplit samples and prepared in a similar manner as the composites. For drillholes from KBRC011 to KBRC283 (2009-2012), no compositing took place, 1m split RC samples and core samples were submitted to Genalysis for fire assay. Samples were oven dried at 105°C then jaw crushed to -10mm followed by a Boyd crush to a nominal -2mm. Samples were rotary split to 2.5kg (2012 drilling). Samples were then pulverised in LM5 mills to 85% passing 75µm. All the samples were analysed for Au using the FA50/AAS technique which is a 50g lead collection fire assay with analysis by Flame Atomic Absorption Spectrometry. The fire assay method is considered a suitable assaying method for total Au determination. The aqua regia digestion results (used for samples that were <0.5g/t Au) may not allow for total Au determination in the transition and fresh rock zones. Aqua regia samples are only present for 5 holes and therefore represent only a very small percentage of the samples. For core and RC samples the sample preparation technique is appropriate and is standard industry practice for a gold deposit. Quality control for maximising representivity of samples included sample weights, insertion of field duplicates and laboratory duplicates.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	In the 2019 drilling samples were submitted to Intertek and Aurum laboratories in Perth and completed by a single 50g fire assay, which is a total assay. Assaying at Intertek also included Pt and Pd analysis. In the 2017 to 2018, drilling samples were submitted to Intertek laboratory in Perth and completed by a single fire assay. Analysis was also received for Pt and Pd. In the 2015 to 2016 drilling samples were submitted to the Intertek laboratory in Perth. In the main mineralised zone four fire assays from the sample pulp were completed, and only one in the waste zones. For samples prior to 2015, only single fire assay determination occurred on each sample. Analysis was also received for Pt and Pd. The samples from 2018 & 2015 drilling were determined for gold, pt, pd and additional elements/base metals, using ICP optical emission spectrometry and ICP mass spectrometry. Samples prior to 2015, were analysed using AAS. Field duplicates were collected at a ratio of 1:20 through the mineralised zones (1:40 elsewhere) and collected at the same time as the original sample through the B chute of the cone splitter. OREAS certified reference material (CRM) was inserted at a ratio of 1:20 through the mineralised zone (1:40 elsewhere). The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. Twin holes from the different drilling programs showed that over an intercept, the grades and lengths of mineralisation compared well, whereas at the individual assay level the results show some variability.

Criteria	JORC Code explanation	Commentary
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	Logging and sampling were recorded directly into a Micromine field marshal template, which utilises lookup tables and in file validation on a Toughbook by the geologist on the rig. Validated data was sent to the database administrator in Perth who then carried out independent verifications using Maxwell's Datashed. Assay results when received were plotted on section and were verified against neighbouring holes. Analysis of the RC/diamond hole twinning up, showed that mineralised intervals above a cut-off grade of 0.3g/t Au were similar in length and moderately well correlated in grade. From time to time assays will be repeated if they fail company QAQC protocols, however no adjustments are made to assay data once accepted into the database.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	Drillhole collar positions for 2019 drilling were surveyed after drilling using a Trimble RTK system, comprising an R10-2 Base and Receiver and a Trimble TSC3 Data Collector. The Base was set up on KB01 located on "Laterite Hill", which was adopted as control for the surveys. All surveys were checked against and closed off on KB01DRM to ensure accuracy. Down hole surveys were undertaken on 30m increments from end of hole, using a Reflex down hole gyroscopic tool. 2015 - 2018 drillhole collar positions were surveyed by Survey Group out of Port Hedland WA and Osbourne Park, WA. The survey was conducted using Trimble R8 RTK GPS base and rover, with an assumed positional accuracy of ±0.025m Horizontal and ±0.050m Vertical. Control used was installed by MHR Surveyors and issued to Survey Group by CMM. GPS base station was positioned over KB01 and checked against KB01DRM. Downhole surveys were collected by driller operated in-rod reflex north seeking gyro at the end of each hole. The measurements were taken every 10 to 30 metres. 2009 - 2012 drillhole collar positions were surveyed by licensed surveyors MHR Surveyors of Cottesloe, WA. The instrument used was a Trimble R8 GNSS RTK GPS (differential) system. Expected relative accuracies from the GPS base station were ±2cm in the horizontal and ±5cm in the vertical direction. Co-ordinates were surveyed in the MGA94 grid system. Downhole surveys were carried out by the drillers at about 50m intervals using a Reflex EZ shot digital downhole camera. Readings were taken in a non-magnetic stainless steel rod near the bottom of the drill string. The depth, dip, azimuth and magnetic field were recorded at each survey point. Drillhole location data was initially captured in the MGA94 grid system and have been converted to a local grid for resource estimation work. The natural surface topography was modelled using a DTM generated from the 2012 airborne LiDAR survey conducted in November 2012 by AAM Pty Limited. The DTM was rotated in-house to the local grid coordinate system. Horizontal point accuracy is expected to be <0.33m and vertical accuracy to 0.15m. Ground control was established using RTK GPS and ALTM3100 Static GPS. The reference datum was GDA94 and the projection was MGA Zone 51, with the data supplied as 50cm and 1m contours in MGA Zone 51. Topographic control is of good quality and is considered adequate for resource estimation.

Criteria	JORC Code explanation	Commentary
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	Drilling has been completed on a 50 x 50m and 25m x 25m and 25m x 50m grid. Drill spacing is sufficient for current resource classification. Samples were collected in 1 metre intervals and analysed for each metre down the hole. Whole hole is analysed at Bibra. At Tramore the upper portions of some holes were not sampled through the unmineralised Bangemall Basin. Prior to 2011 1m RC samples were collected at the rig using a cone splitter, with 2m composites taken from each of the 1m intervals and submitted to Genalysis for sample preparation and analysis. Samples that returned values >0.5g/t Au were submitted as 1m samples to Genalysis.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	Drill lines are oriented across strike on a local grid. Bibra orebody dips at 20 to 30 degrees to the North West. Holes in the drill programs have been drilled at inclination of -60 and -90 degrees. The orientation of the drilling is suitable for the mineralisation style and orientation of the Bibra mineralisation.
Sample security	• *The measures taken to ensure sample security.*	Calico sample bags are sealed into green bags/polyweave bags and cable tied. These bags were then sealed in bulka bags by company personnel, dispatched by third party contractor, in-company reconciliation with laboratory assay returns.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	All programmes are reviewed by company senior personnel. Prior to commencement of the 2016 drill program a meeting of industry specialists was held to discuss the sampling and analytical techniques to get consensus and or improvements on the drilling and sampling protocol. Prior to 2016, a review of practices documented in the IGO technical report supplied to Optiro Pty Ltd in 2012 as part of the resource estimate review did not highlight any significant issues. Optiro completed a resource audit of the 1606 and 1804 models which included auditing of the data. No fatal flaws were identified.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	The Bibra deposit is located in M52/1070 held by Greenmount Resources, a wholly owned subsidiary of Capricorn Metals. M52/1070 is within the area of granted E52/1711 exploration tenement in the Pilbara region of Western Australia. E52/1711 was acquired from BHPB in 2008. South32 (via the spin-out from BHPB) retain a 2% NSR whilst BHPB a claw-back provision whereby BHPB can elect to acquire a 70% equity in the project only if JORC compliant reported resources of 5,000,000 ounces of gold and/or 120,000 tonnes of contained nickel have been delineated. The Nyiyaparli People hold Native Title over the area including E52/1711 and M52/1070. There

Criteria	JORC Code explanation	Commentary
		is no known heritage or environmental impediments over the lease. No other known impediments exist to operate in the area.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	Prior to Capricorn Metals, E52/1711 was held by Independence group (IGO) who undertook exploration between 2008 & 2014. Prior to Independence group, WMC (BHPB) explored the area from 2004 to 2008.
Geology	• *Deposit type, geological setting and style of mineralisation.*	Bibra is part of a large-scale Archaean aged gold mineralized system. The resource is hosted within a package of deformed meta-sediments which has developed on at least two parallel, shallow dipping structures; Laterite oxide mineralization has developed over the structures close to surface. The primary mineralization is strata-bound with lineations identified as controlling higher-grade shoots. The deposit is oxidized to average depths of 50-70m.

Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*
	  ○ *easting and northing of the drill hole collar*
	  ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar*
	  ○ *dip and azimuth of the hole*
	  ○ *down hole length and interception depth*
	  ○ *hole length.*
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*
		All relevant RC and Diamond holes used in the estimation of the reported Mineral Resource estimation have been previously reported in ASX announcements.

Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	This release is in relation to a Mineral Resource estimate, with no exploration results being reported. No metal equivalent values are used.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	At Bibra, the geometry of the mineralisation has already been defined from previous drilling programs. The intersection angle between drill angle and the perpendicular angle to the ore zone is less than 10 degrees.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Refer to the diagrams in the body of this report and within previous ASX announcements.

Criteria	JORC Code explanation	Commentary
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	The accompanying document is considered to be a balanced report with a suitable cautionary note. Relevant drill assay results used in this Mineral Resource estimation have been released in previous ASX announcements.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Systematic metallurgical testwork programs over 2012 to 2019 on master and variability composites from diamond core identifies mineralisation as free milling and amenable to cyanidation. Geotechnical logging has been completed for determining ground conditions for open pit mining.
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	Resource Definition programs have been designed to further infill the Inferred material to the next level of classification. Drilling programmes have been designed to target unclassified areas of known mineralisation to move these areas into a higher classification.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	Since 2014 drilling has been collected in the field by geologists and field assistants using Micromine's Field Marshall program with in-built Validation. Once hole information was finalised on site the information was emailed to the CMM Database Administrator to load into Datashed SQL database. Prior to 2014, data has been collected by the geologists and field staff in either Excel spreadsheets or acQuire data entry objects on laptops for RC and diamond drilling and loaded into SQL acQuire software. The inherited validated data from IGO was imported into a Datashed SQL database by Maxwell Geoscience. Analytical data was received from the laboratories in electronic ASCII files of varying format and were merged with sampling data already present in the database. Assays received from laboratories were imported by the Database Administrator into the database. Any data files which did not validate were investigated and rectified by field staff or Database Administrator.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	The competent person has not made a site visit to Bibra as part of this study. All exploration and resource development drilling programmes are subject to review by experienced senior CMM technical staff. These reviews have been completed from the commencement of drilling and continue to the present. For the purpose of this update CMM were of the opinion that the mineralisation interpretations and estimations could be undertaken utilising the experience of the CMM project and

Criteria	JORC Code explanation	Commentary
		exploration geologists in combination with core photos of the diamond drilling within the MRE area. There is currently no open pit exposure to inspect/verify mineralisation controls.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	Confidence in the geological interpretation is good. Stratigraphy is consistent and can be correlated between holes and along strike. Geological logging and structural measurements from drillholes have been used to construct the geological model. Sections were interpreted, digitised and a 3D wireframe model constructed. Geological continuity has been assumed along strike and down-dip. The geological interpretation is robust. The geological model was built by on the ground geologists who logged and relogged and interpreted the geology to ensure the geological interpretation was consistent. With the current drill spacing it is unlikely that an alternative interpretation will develop. There is currently sufficient drilling to map the stratigraphic units and laterite zone. The geological model has been used to guide mineralisation envelopes and subsequent mineralisation wireframe modelling. Geological continuity has been assumed along strike and down-dip based on the drilling data. In general, continuity both geologically and grade-wise is good. Grades and thickness are more consistent down-dip than along strike.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	The Bibra mineralisation wireframes have been projected down-dip based on wider spaced drilling intercepts; however, this extrapolation has been removed from the resource estimate by limiting the reported tonnes and grade to within a conceptual optimal pit shell ($2000/oz Au). The main laterite zone extends 1250m along strike and 1150m across. It ranges from 2m to 15m in vertical thickness. The primary mineralisation extends below the laterite zone for a further vertical depth of 310m. The transition/fresh rock boundary is about 60m below surface. The primary mineralisation has 4 main sub-parallel zones and several smaller zones. Overall these zones extend for 1800m along strike (N-S) and 1800m across.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* • *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* • *The assumptions made regarding recovery of by-products.* • *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).* • *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*	The MRE has been estimated using Ordinary Kriging (OK) with no change of support. The OK estimation was constrained within Au mineralisation domains generated in Surpac. These were defined from the resource drilling and guided by a geological model created in Micromine. OK is considered an appropriate grade estimation method for the Bibra mineralisation given drilling density and mineralisation style, which has allowed the development of robust and high confidence estimation constraints and parameters. The grade estimate is based on 1m down-the-hole composites of the resource dataset created in Surpac each located by their mid-point co-ordinates and assigned a length weighted average gold grade. 1m composite length was chosen because it is a multiple of the most common sampling interval (1.0 metre). Statistical analysis identified a high-grade population which was flagged in the model using an indicator estimate at 1g/t Au. This enabled a high-grade restriction to be used involving those flagged blocks being estimated

Criteria	JORC Code explanation	Commentary
	• *Any assumptions behind modelling of selective mining units.* • *Any assumptions about correlation between variables.* • *Description of how the geological interpretation was used to control the resource estimates.* • *Discussion of basis for using or not using grade cutting or capping.* • *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	by a composite file within that flagged area cut to a higher upper-cut. The remaining portions of the domain are estimated with the total domain composite file cut to a lower uppercut. The high-grade restriction and high-grade cuts (as described below) have been applied to composites to limit the influence of higher-grade data. Statistical and geostatistical analysis was completed on the domain coded composite file (1m composites). This included exploration data analysis, boundary analysis and grade estimation trials. The variography applied to grade estimation has been generated using Surpac. These investigations have been completed on each ore domain separately. An independent multiple indicator kriging (MIK) check estimate was completed as part of the study which compares within acceptable levels to the Capricorn OK estimate. Metal is within 10% between the two models at multiple scales of reporting. No by-products are present or modelled. No deleterious elements have been estimated or are important to the project economics\planning at Bibra. Block dimensions are 10m (east) by 10m (north) by 5m (elevation) (with sub-blocking in the Z direction to 2.5m to better suit the flat lying laterite mineralisation) and was chosen as it approximates SMU for the deposit, and a quarter to half the drill hole spacing. The oxide/fresh interpolation utilised 3 estimation passes, with category 1 adopting a 40m octant search, 16 minimum/64 maximum composites used and a maximum of 4 composites per drill hole, with only 4 adjacent octants allowed to fail the search criteria. Category 2 uses a 60m search distance, 16 minimum/64 maximum composites, 4 maximum per hole and 4 adjacent octants allowed to fail the criteria. Category 3 uses a 100m search distance, 8 minimum/64 maximum composites, 4 maximum per hole and 8 adjacent octants allowed to fail the criteria, with category 3 being estimated into a doubled block size as well. The laterite portion of the deposit is estimated into the sub-blocked Z size of 2.5m. The search on each category is orientated to align to the orientation of the mineralisation of each specific domain. No selective mining units were assumed in this estimate. No correlated variables have been investigated or estimated. The grade estimate is based on mineralisation constraints which have been interpreted based on a lithological and weathering interpretation, and a nominal 0.1g/t Au lower cut-off grade. The mineralisation constraints have been used as hard boundaries for grade estimation wherein only composite samples within that domain are used to estimate blocks coded as within that domain. Statistical investigations have been completed to test the change in statistical and spatial characteristics of the domains grouped by weathering showing there to be little variation between profiles, hence they have been estimated inclusively. A review of the composite data captured within the mineralisation constraints was completed to assess the need for high grade cutting (capping). This assessment was completed both statistically and spatially to determine if the high-grade data clusters or were isolated. On the basis of the investigation it was decided to utilise a high-grade restriction, and appropriate

Criteria	JORC Code explanation	Commentary
		high-grade cuts were applied to all estimation domains. The grade estimate was checked against the input drilling/composite data both visually on section (cross and long section) and in plan, and statistically on swath plots.
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	Tonnages have been estimated on a dry basis.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	The MRE is reported at a cutoff grade of 0.3g/t for laterite, 0.3g/t for oxide, 0.4g/t for transitional and 0.4g/t for fresh. This is determined from standardised parameters used to generate the open pit MRE reporting shell, and also takes into account potential mining practices.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	Currently a contractor-operated open-pit mining option is the basis for the cut-off grade. Ore and waste would be paddock blasted on 5m benches and subsequently excavated as 2.5m flitches utilising a conventional excavator and truck mining fleet to facilitate moderate ore excavation selectivity.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	Test work was completed during 2017 using 32 composite samples from 779 metres of core. The Bibra ore is classified as free milling, with a high gravity recoverable gold component (up to 45%). Overall, gravity plus leach gold recoveries are in the range of 93% to 96%. The Bibra ore is relatively clean, with minimal to no cyanide or oxygen consuming gangue minerals present in the ore, leading to low residual WAD cyanide levels (<50ppm) in the leach circuit tailings solution. A gold recovery value of 95% was used in the generation of the open pit MRE reporting shell.
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	Waste rock from open pit operations would be placed in a waste rock landform adjacent to open pit operations, progressively contoured and revegetated throughout mine life. Process plant residue would be disposed of in a surface tailings storage facility (TSF). Adoption of an upstream, central decant design would utilise mine waste material for dam wall construction and facilitate water recovery to supplement process water requirements. It is expected that sufficient volumes of oxide material, able to be made sufficiently impermeable, will be available in the overburden stream to enable acceptable TSF construction.
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	Bulk density values have been calculated from 3,976 measurements collected on site and at laboratory using the water immersion method. Data has been separated into lithological and weathering datasets and mean density values derived.

Criteria	JORC Code explanation	Commentary
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	The Measured, Indicated and Inferred classification reflects the relative confidence in the estimate, the confidence in the geological interpretation, the drilling spacing, input data, the assay repeatability and the continuity of the mineralisation. The strategy adopted in the current study uses category 1 and 2 from the 3-pass octant search strategy as Indicated and category 3 as Inferred. This results in a geologically sensible classification whereby Category 1 and 2 are surrounded by data in close proximity. Category 3 blocks may occur on the peripheries of drilling but are still related to drilling data within reasonable distances. No measured has been applied in the classification method. This classification reflects the Competent Person's view of the deposit.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	The resource model has been reviewed for fatal flaws internally, although no audit has been completed on the MRE. An independent check estimate was completed using MIK as part of the study and compared within acceptable levels.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	The confidence level is reflected in the classification of the estimate. Mineralisation modelled but outside the $2000/oz Au reporting shell has been excluded from the estimate. The Mineral Resource estimate is an undiluted global estimate. There is no production data to compare the resource estimate with, as Bibra has not been mined.

Section 4 Estimation and Reporting of Ore Reserves

(Criteria listed in section 1, and where relevant in sections 2 and 3, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• *Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.* • *Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.*	The Mineral Resource estimate for the Bibra deposit which formed the basis of this Ore Reserve estimate was compiled by the Capricorn Competent Persons utilising relevant data. The estimate is based on 1,283 Reverse Circulation (RC) holes and 92 diamond holes of exploration drilling and assay data. The data set, geological interpretation and model was validated using Capricorn's internal and Quality Assurance and Quality Control (QAQC) processes and compared to an estimate completed by an independent external consultant. Ordinary Kriging was utilised to estimate the resource. The individual block size for estimation was 10 m x 10 m x 5 m, with sub-blocking at 2.5m in the Z direction for effective boundary definition for the laterite portion of the deposit. The Mineral Resources are reported inclusive of the Ore Reserve.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*	The Competent Person did not conduct a site visit. This is because:

Criteria	JORC Code explanation	Commentary
	• *If no site visits have been undertaken indicate why this is the case.*	• They are already familiar with the region • Due to the presence of transported cover, there are no outcrops, mine workings or infrastructure to inspect on the ground.
Study status	• *The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.* • *The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.*	The Ore Reserve estimate is based on findings of a 2017 Feasibility Study (FS) and further optimisation work completed by a team consisting of CMM personnel and independent external consultants. The proposed mine plan is technically achievable. All technical proposals made for the operational phase involve the application of conventional technology which is widely utilised in Western Australia. Material Modifying Factors (mining, processing, infrastructure, environmental, social and commercial) have been considered during the Ore Reserve estimation process. Financial modelling completed shows that the project is economically viable under current assumptions.
Cut-off parameters	• *The basis of the cut-off grade(s) or quality parameters applied.*	Variable economic cut-off grades have been applied in estimating the Ore Reserve. Cut-off grade is calculated in consideration of the following parameters: ▪ Gold price ▪ Operating costs including ore costs (eg grade control, ROM re-handle) ▪ Process recovery ▪ Transport and refining costs ▪ General and administrative cost ▪ Royalty costs. Cutoff grades are 0.3 g/t Au Laterite, 0.3 g/t Oxide, 0.4 g/t Transitional, 0.4 g/t Fresh.
Mining factors or assumptions	• *The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).* • *The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.* • *The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.* • *The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).* • *The mining dilution factors used.* • *The mining recovery factors used.* • *Any minimum mining widths used.* • *The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.* • *The infrastructure requirements of the selected mining methods.*	The Bibra deposit will be mined by open pit mining methods utilising conventional mining equipment. The final pit design is the basis of the Ore Reserve estimate. The selected mining method, design and extraction sequence are tailored to suit orebody characteristics, minimise dilution and ore loss, defer waste movement and capital expenditure, utilise proposed process plant capacity and expedite free cash generation in a safe manner. Geotechnical modelling has been completed by an external consultant on the basis of field logging and laboratory testing of selected dedicated diamond drill core samples from 16 geotechnical diamond drillholes. The recommended geotechnical design parameters assume dry slopes based on adequate dewatering and/or depressurisation ahead of mining. The low-angle dip of the deposit (28° to West) allows for a designed overall wall angle on the Footwall (Eastern side of pit) between ramps of 25°. The western wall (Hanging Wall) of the pit is designed to have an overall slope of 49.8°, however a decision on that final wall angle will not need to be made until at least 5 years into the mining operation and following expected learnings from interim wall performance.

Criteria	JORC Code explanation	Commentary
		A separate hydrogeological report was prepared by independent consultants which considered the infrastructure required to effectively dewater the open pit and pit slopes. This study was supported by the development of test bores and field test pumping analysis. Only open pit mining has been considered in the Mineral Resource and Ore Reserve studies. Mining dilution and recovery modifying factors have not been applied to the Ore Reserve. This has been accounted for in the MRE. The mining schedule is based on realistic mining productivity and equipment utilisation estimates and also considered the vertical rate of mining development. No Inferred Mineral Resources were used in Ore Reserve calculations. The proposed mine plan includes waste rock dumps, a ROM pad, a surface water diversion channel, surface dewatering bores, light and heavy vehicle workshop facilities, explosives storage and supply facilities and technical services and administration facilities.
Metallurgical factors or assumptions	• *The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.* • *Whether the metallurgical process is well-tested technology or novel in nature.* • *The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.* • *Any assumptions or allowances made for deleterious elements.* • *The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.* • *For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?*	A processing flowsheet, materials balance, water balance, equipment identification, mechanical and electrical layouts were all developed to FS standard. A tertiary crushing single Ball Mill comminution circuit followed by a conventional gravity and carbon in leach (CIL) process is proposed. This process is considered appropriate for the Bibra ore, which is classified as free-milling. The proposed metallurgical process is commonly used in the Australian and international gold mining industry and is considered to be well-tested and proven technology. Significant comminution, extraction, and physical properties testing has been carried out on approximately 2,000kg of half-HQ and NQ diamond drilling core samples from 24 drillholes, and 300kg of RC chip samples. This has been carried out on laterite, oxide, saprock, transitional, and fresh ore types which were obtained across the Bibra deposit and to a depth of approximately 200m. Estimated plant gold recovery ranges from 91.8% to 94.1% depending on grind size and ore type. No deleterious elements of significance have been determined from metallurgical test work and mineralogy investigations.
Environmental	• *The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.*	Baseline environmental studies and Level 1 and Level 2 studies of flora, vegetation, vertebrate fauna, short-range endemic invertebrates, and subterranean fauna are all completed. A Mining Proposal (including a Closure Plan) has been approved and environmental approvals for the mining and water supply aspects of the project have been issued by the Department of Mines, Industry Regulation and Safety (DMIRS). A Native Vegetation Clearing Permit has been granted for the project site. The Mining Proposal will be updated for mining and processing of the increased Ore Reserve. Waste rock and tailings characterisation work has been completed and all waste types and tailings are non-acid forming and have limited metal leachate potential. Waste rock and

Criteria	JORC Code explanation	Commentary
		tailings storage locations have been selected based on suitable geographical characteristics and proximity to the pit and plant. Department of Water and Environmental Regulation (DWER) have granted a works approval under the Environmental Protection Act 1986 to construct the gold processing plant and tailings storage facility, inert and putrescible landfill and sewage facility at the Karlawinda Gold Project. These approvals will be amended to allow for the processing of the increased Ore Reserve.
Infrastructure	• *The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.*	The project site is within economic distances of existing infrastructure in the east Pilbara region. Services and consumable supplies will be delivered by existing roads and a new 40 km Access Road from the Great Northern Highway to the Karlawinda Project. Land availability is unlikely to be an issue, with the mining and exploration tenure held by Capricorn more than covering all project needs. The project lies at the northern boundary of the Weelerrana cattle station. Tailings disposal is intended to be within an Integrated Waste Landform whereby tailings are encapsulated by mining waste, rather than having separate waste dumps and tailings facilities. The workforce will be Fly In-Fly Out (FIFO) and based at a camp on site during rostered days on. Either commercial flights to Newman airport, 55 km North of the Project or an onsite airstrip will be used. Pump testing and modelling of the potential yield from the Karlawinda borefield indicate that there is sufficient groundwater to service the needs of the Project for the life-of-mine. This will require the development of numerous water production bores, of which 5 have already been developed. Miscellaneous licence applications to secure the tenure required for the all infrastructure not covered by Mining Lease have been approved. Power will be generated on site utilising natural gas, requiring a 56 km pipeline construction.
Costs	• *The derivation of, or assumptions made, regarding projected capital costs in the study.* • *The methodology used to estimate operating costs.* • *Allowances made for the content of deleterious elements.* • *The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.* • *The source of exchange rates used in the study.* • *Derivation of transportation charges.* • *The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.* • *The allowances made for royalties payable, both Government and private.*	All capital estimates are based on current market rates. It is assumed that all mining equipment required for the project, including drill and blast equipment, will be supplied by contractors. Mine development costs were developed from a combination of inputs from Capricorn, Entech Pty Ltd (mining), Mintrex (processing), CMW Geosciences (tailings disposal), GRM (groundwater consultants) and Peter O'Brien (geotechnical). The basis of estimate is: • Contractor mining (with contractor drilling and blasting). • Mobilisation of mining equipment and personnel from Perth. • Earthworks quantities determined from detailed site investigations by a geotechnical engineer and geological modelling. • Mine dewatering requirements developed from airlift testing and hydrogeological modelling.

Criteria	JORC Code explanation	Commentary
		• A mining schedule developed on a quarterly basis. • A contingency allowance on capital cost items calculated to reflect the relevant level of confidence in the estimate. Processing and infrastructure development capital costs have been estimated by Mintrex and Capricorn engineers on the basis of: • Earthworks quantities determined from detailed site inspections by a geotechnical engineer. • Concrete and structural quantities developed from site layouts and similar designs from other projects. • A mechanical equipment list developed from the recommended process design criteria. • Budget and Tender pricing from local and international suppliers. • Contingency allowances calculated on a line by line basis relevant to the source and confidence in market rates. The operating cost estimate accuracy is -15% /+15%. Operating costs assume a FIFO scenario with various rosters on site. Mining operating costs have been estimated by Capricorn personnel/consultants based on scheduled material movement and estimated mining rates for a contractor mining scenario. Mine design and scheduling were prepared by Mining Engineers from Entech Pty Ltd. Process and infrastructure operating costs have been estimated by Mintrex and Capricorn on the assumption that: • A tertiary crushing single Ball Mill comminution circuit followed by a conventional gravity and carbon in leach (CIL) process will be utilised to treat the ore. • Comminution grind sizes will be in the range of 120µm (Fresh rock) to 150µm (Oxide rock). • Power will be generated on site utilising natural gas. • The process plant will be operated by CMM employees. The operating cost estimate is considered to be appropriate for the current market in Western Australia. No allowance is made for deleterious elements since testwork to date on ore from Bibra has not shown the presence of deleterious elements. Capital Costs for process plant and infrastructure are estimated in 2020 Australian dollars, and no exchange rates have been applied. Transport charges - Gold bullion transportation and refining charges are derived on the basis of a quote provided by a leading Australian Gold Refinery. An allowance has been made for all royalties, including an allowance of 2.5% of revenue for royalties payable to the Western Australian State Government and a 2% allowance for the

Criteria	JORC Code explanation	Commentary
		current commercial royalty to South 32. The terms of the royalty payable to the other private party is covered by confidentiality restrictions.
Revenue factors	• *The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.* • *The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.*	The mined ore head grades are estimated utilising industry accepted geostatistical techniques with the application of relevant mining Modifying Factors. Gold price and exchange rates have been determined by Capricorn on the basis of current market trends and by peer company comparison. A$1,600/oz is used for the Ore Reserve calculation process. The financial model is run at A$1,750/oz, and 200 koz are hedged at A$2,250/oz.
Market assessment	• *The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.* • *A customer and competitor analysis along with the identification of likely market windows for the product.* • *Price and volume forecasts and the basis for these forecasts.* • *For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.*	There is a transparent market for the sale of gold.
Economic	• *The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.* • *NPV ranges and sensitivity to variations in the significant assumptions and inputs.*	Inputs from the open pit mining, processing, sustaining capital and contingencies have been scheduled and costed to generate the cost estimate. Cost inputs have been estimated from quotations and/or by competent specialists. The Ore Reserve returns a positive NPV based on the assumed commodity price and the Competent Person is satisfied that the project economics that make up the Ore Reserve retains a suitable profit margin against reasonable future commodity price movements. Sensitivity analysis has indicated that the project drivers are gold prices, grade, metallurgical recoveries followed by operating costs; NPV remains favourable for the sensitivity tests within reasonable ranges.
Social	• *The status of agreements with key stakeholders and matters leading to social licence to operate.*	A Native Title Access Agreement has been signed for the Project (ASX Announcement 24 Nov 2016). After the Native Title Access Agreement, a Mining Lease was granted over the project area (ASX Announcement 24 Nov 2016) and several Miscellaneous Licences to cover the infrastructure corridors have been granted.
Other	• *To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:* • *Any identified material naturally occurring risks.* • *The status of material legal agreements and marketing arrangements.* • *The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.*	Flooding risk has been analysed by an independent external expert and deemed to be minimal, with the project located near the top of a small catchment system. No significant species have been identified that would be significantly impacted by the Project in a manner that could not be adequately managed. Construction of the project has commenced, and various contract negotiations have been finalised or under negotiation. There are reasonable prospects to anticipate that contract terms assumed in the Ore Reserves estimate will be achieved. Project commissioning is estimated for 2021.

Criteria	JORC Code explanation	Commentary
Classification	• *The basis for the classification of the Ore Reserves into varying confidence categories.* • *Whether the result appropriately reflects the Competent Person's view of the deposit.* • *The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).*	The main basis of classification of Ore Reserves is the underlying Mineral Resource classification. All Probable Ore Reserves derive from Indicated Mineral Resources in accordance with JORC Code (2012) guidelines. The results of the Ore Reserve estimate reflect the Competent Person's view of the deposit. No Probable Ore Reserves are derived from Measured Mineral Resources. No inferred Mineral Resource is included in the Ore Reserves.
Audits or reviews	• *The results of any audits or reviews of Ore Reserve estimates.*	The Feasibility Study and subsequent technical studies which form the basis of the Ore Reserve estimate was subjected to various reviews and audits: • Metallurgical testwork was reviewed by Capricorn's consulting metallurgists and process engineers and confirmed to be adequate for a FS. • Open pit designs, production schedules and mining cost models were reviewed through Entech's internal peer review system. • The pit designs were further reviewed by the independent geotechnical consultants to confirm the application of the prescribed design parameters The design for the process plant and infrastructure were reviewed by Capricorn personnel, consulting metallurgists and process engineers.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.* • *It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	The Karlawinda FS resulted in a technically robust and economically viable business case. Subsequent studies have been completed by a team consisting of Capricorn personnel and independent expert consultants. This is deemed to be an appropriate basis for a high level of confidence in the updated Ore Reserves estimate. In the opinion of the Competent Person, cost assumptions and modifying factors applied in the process of estimating Ore Reserves are reasonable. Gold price and exchange rate assumptions were set out by Capricorn and are subject to market forces and present an area of uncertainty.