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January 2015 Mineral Resource & Ore Reserve Update

HIGHLIGHTS

- **Mineral Resource increased 49% to over 10 million ounces of gold**
- **Ore Reserves maintained at above 1 million ounces of gold for 7th successive year**

Norton Gold Fields Ltd ("Norton" or the "Company") advises it has completed an update to its Mineral Resources and Ore Reserves for the period ending 31 December 2014.

Norton Managing Director and Chief Executive Officer, Dr Dianmin Chen stated "Norton aims to increase its Mineral Resources through a combination of exploration, innovation and acquisition. We are particularly pleased to have substantially increased our Mineral Resources, and to have maintained our Ore Reserves above 1 million ounces for the 7th successive year. This large resource base will provide an opportunity to grow our business and increase our gold production on the back of an already record year in 2014".

- **Total Measured, Indicated and Inferred Mineral Resources** for Norton Gold Fields as at 31 December 2014 now comprise:

247Mt @ 1.30g/t Au, containing 10.35Moz

  This figure represents a substantial increase of 3.41Moz (49%) on the mineral resource estimate at 31 December 2013 (6.94Moz reported in ASX announcement dated 24 January 2014).

- The resource increase includes acquisitions completed during 2014:

95Mt @ 1.05g/t Au (3.21Moz) from the Bullabulling Project
3.15Mt @ 1.32g/t Au (134koz) from the Mt Jewell Project

- **Total Proven and Probable Mining Reserves** comprise:

18.5Mt @ 1.87g/t Au, containing 1.11Moz

  Ore Reserve levels have been continually replenished and maintained above 1Moz since 2008, despite production and depletion of 1,126,000oz since the Norton acquisition of Paddington in 2007.

- Primary mining projects and ore reserves at the Paddington Operation include:

Enterprise Open Cut	4.84Mt @ 2.00g/t Au	312,000oz
Enterprise Underground	1.63Mt @ 3.10g/t Au	162,000oz
Federal Open Cut	1.86Mt @ 1.72g/t Au	103,000oz
Bullant Underground	0.43Mt @ 3.38g/t Au	46,000oz
Homestead Underground	0.22Mt @ 6.54g/t Au	47,000oz

- The Resources statement also includes projects requiring alternate processing streams, including :

Racetrack refractory mineralisation	current resource of 736,000oz
Binduli heap leach	current resource of 1.97Moz

- Mineral Resource and Ore Reserve status changes between the previous publicly released estimates (for 31 December 2013) and those reported herein are due to a combination of:

  - Addition from acquisition.
  - Mineral resource update and accompanying change or addition of ore reserve.
  - Re-definition of open-cut and underground reporting areas at Enterprise. An Enterprise underground reserve was introduced in favour of a Stage 4 open pit cutback.
  - Ore Reserve modification due to lower gold price at all projects.
  - Depletion from mining.
  - Change in reporting area allocation (for example some parts of the Racetrack, mineral resource were previously reported under the 'Mt Pleasant' umbrella).
  - Resource depletion due to consideration of economic factors.

Table 1: Norton Gold Fields Consolidated Resource Statement
Mineral Resource as at 31 December 2014

Project Area	Measured			Indicated			Inferred			Total		
	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces
Paddington	**2.32**	**1.8**	**135,000**	**69.64**	**1.43**	**3,191,000**	**76.39**	**1.5**	**3,678,000**	**148.35**	**1.47**	**7,004,000**
Mt Jewell	**0.00**	**0.00**	**0**	**3.11**	**1.32**	**132,000**	**0.04**	**1.37**	**2,000**	**3.15**	**1.32**	**134,000**
Bullabulling	**0.00**	**0.00**	**0**	**68.57**	**0.99**	**2,185,000**	**26.79**	**1.19**	**1,029,000**	**95.37**	**1.05**	**3,214,000**
Total Mineral Resource	**2.32**	**1.8**	**135,000**	**141.33**	**1.21**	**5,509,000**	**103.22**	**1.42**	**4,708,000**	**246.87**	**1.3**	**10,352,000**

Table 2: Paddington Resource Statement
Mineral Resource as at 31 December 2014

Project Area	Rounded	Measured			Indicated			Inferred			Total		
	DEPOSIT	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces
Golden Cities	Havana	0.00	0	0	3.82	1.62	199,000	0.15	1.63	8,000	3.97	1.62	207,000
	Federal OC	0.00	0	0	3.77	1.85	225,000	0.88	2.96	84,000	4.65	2.06	309,000
	Federal UG	0.00	0	0	0.00	0	0	0.20	5.36	35,000	0.20	5.36	35,000
	Jakarta	0.00	0	0	1.77	1.15	65,000	0.42	1.02	14,000	2.19	1.13	79,000
Mulgarrie	Mulgarrie	0.00	0	0	1.27	2.19	89,000	1.39	2.21	99,000	2.65	2.2	188,000
	Mulgarrie Well	0.00	0	0	0.16	1.68	9,000	0.31	1.36	14,000	0.47	1.47	22,000
Ora Banda	Enterprise OP	0.00	0	0	6.68	1.79	385,000	2.50	1.3	104,000	9.19	1.66	490,000
	Enterprise UG	0.00	0	0	3.16	2.94	298,000	1.10	2.57	91,000	4.25	2.84	389,000
	Enterprise West	0.00	0	0	0.07	0.87	2,000	1.11	1.15	41,000	1.18	1.13	43,000
	North Sandalwood	0.00	0	0	0.00	0	0	1.64	1.24	65,000	1.64	1.24	65,000
	Sleeping Beauty	0.00	0	0	0.00	0	0	0.62	1.36	27,000	0.62	1.36	27,000
	Tom Allen	0.00	0	0	0.00	0	0	0.91	1.70	50,000	0.91	1.7	50,000
Mt Pleasant	Mt Pleasant	0.00	0	0	0.67	2	43,000	1.45	2.11	98,000	2.12	2.08	141,000
	Racetrack OC	0.00	0	0	4.26	1.88	257,000	6.08	2.19	428,000	10.34	2.06	685,000
	Racetrack UG	0.00	0	0	0.00	0	0	0.26	6.21	51,000	0.26	6.21	51,000
	Royal Standard North	0.00	0	0	0.00	0	0	0.30	1.43	14,000	0.30	1.43	14,000
	Green Gum	0.00	0	0	0.11	2.43	9,000	0.19	1.8	11,000	0.30	2.03	20,000
	Blue Gum	0.00	0	0	0.12	1.77	7,000	0.24	1.42	11,000	0.36	1.53	18,000
	Homestead UG	0.11	19.1	66,000	0.09	14.1	42,000	0.14	13.1	60,000	0.34	15.3	169,000
	Golden Kilometre	0.00	0	0	0.00	0	0	0.76	4.17	102,000	0.76	4.17	102,000
	Quarters 040	0.00	0	0	0.11	2.31	8,000	0.05	1.3	2,000	0.16	2	10,000
	Tuart OC	0.00	0	0	3.44	1.66	184,000	1.11	2.04	73,000	4.55	1.75	256,000
	Tuart UG	0.00	0	0	0.12	7.19	28,000	0.79	6.27	159,000	0.91	6.39	187,000
	Marlock	0.00	0	0	0.08	1.65	4,000	1.04	2.07	69,000	1.12	2.04	74,000
	Natal	0.00	0	0	0.00	0	0	0.38	2.46	30,000	0.38	2.46	30,000
	Golden Flag	0.00	0	0	0.06	1.21	2,000	0.13	1.77	7,000	0.19	1.6	10,000
	Black Flag OC	0.00	0	0	0.05	1.4	2,000	0.11	2.6	9,000	0.17	2.21	12,000
	Black Flag UG	0.00	0	0	0.00	0	0	0.04	8.75	10,000	0.04	8.75	10,000
	Rose Dam South	0.00	0	0	0.00	0	0	0.54	1.22	21,000	0.54	1.22	21,000
	Rose	0.00	0	0	0.39	1.26	16,000	0.50	1.13	18,000	0.89	1.19	34,000
Lady Bountiful	Lady Bountiful	0.00	0	0	1.84	1.75	104,000	0.13	2.15	9,000	1.98	1.78	113,000
	Lady Bountiful Extended	0.00	0	0	0.00	0	0	4.25	1.72	235,000	4.25	1.72	235,000
	Liberty West	0.00	0	0	0.00	0	0	0.54	1.94	34,000	0.54	1.94	34,000
Binduli	Janet Ivy	0.00	0	0	8.36	0.87	234,000	5.25	0.92	155,000	13.61	0.89	389,000
	Navajo Chief	0.00	0	0	23.51	0.8	608,000	5.84	0.86	161,000	29.35	0.81	769,000
	Fort William	0.00	0	0	0.23	2.2	16,000	1.78	1.26	72,000	2.00	1.37	88,000
	Fort Scott	0.00	0	0	0.46	1.36	20,000	0.07	1.14	3,000	0.53	1.33	23,000
	Apache	0.00	0	0	0.00	0	0	0.63	1.67	34,000	0.63	1.67	34,000
	Ben Hur (1,2,3)	0.00	0	0	0.00	0	0	27.35	0.93	814,000	27.35	0.93	814,000
	Nefertiti	0.00	0	0	0.00	0	0	0.86	0.92	25,000	0.86	0.92	25,000
	Pitman South	0.00	0	0	0.00	0	0	0.10	2.2	7,000	0.10	2.2	7,000
	Walsh	0.00	0	0	0.00	0	0	0.22	1.69	12,000	0.22	1.69	12,000
	Walsh North	0.00	0	0	0.00	0	0	0.20	1.85	12,000	0.20	1.85	12,000
Carbine	Bullant UG	0.09	6.01	17,000	1.05	5.39	181,000	1.20	5.32	205,000	2.33	5.38	403,000
	Wattlebird	0.00	0	0	1.97	1.38	87,000	0.03	1.47	1,000	2.00	1.38	88,000
	Matt's Dam	0.00	0	0	0.00	0	0	0.34	1.54	17,000	0.34	1.54	17,000
	Matt's Dam South	0.00	0	0	0.00	0	0	0.66	1.3	28,000	0.66	1.3	28,000
	Porphyry	0.00	0	0	1.66	1.09	58,000	0.68	1.25	27,000	2.34	1.14	85,000
	Stockpiles (As at 31/12/2014)	2.12	0.75	51,000	0.37	0.67	8,000	0.93	0.66	20,000	3.43	0.72	79,000
	Total Mineral Resource	**2.32**	**1.8**	**135,000**	**69.64**	**1.43**	**3,191,000**	**76.39**	**1.5**	**3,678,000**	**148.35**	**1.47**	**7,004,000**

Note: Apparent arithmetic inconsistencies are due to rounding

Table 3: Mt Jewell Resource Statement

Mineral Resource as at 31 December 2014

DEPOSIT	Measured			Indicated			Inferred			Total		
	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces
Hughes	0.00	0.00	0	1.90	1.16	71,000	0.00	0.89	0	1.91	1.16	71,000
Tregurtha	0.00	0.00	0	1.21	1.58	62,000	0.03	1.43	1,000	1.24	1.58	63,000
Total Mineral Resource	**0.00**	**0.00**	**0**	**3.11**	**1.32**	**132,000**	**0.04**	**1.37**	**2,000**	**3.15**	**1.32**	**134,000**

Note: Apparent arithmetic inconsistencies are due to rounding

Table 4: Bullabulling Resource Statement
Mineral Resource as at 31 December 2014

DEPOSIT	Measured			Indicated			Inferred			Total		
	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces	Mt	Au g/t	Ounces
Bullabulling Trend	0.00	0.00	0	68.57	0.99	2,185,000	23.08	1.20	893,000	91.65	1.04	3,079,000
Gibraltar	0.00	0.00	0	0.00	0.00	0	3.72	1.13	136,000	3.72	1.13	136,000
Total Mineral Resource	**0.00**	**0.00**	**0**	**68.57**	**0.99**	**2,185,000**	**26.79**	**1.19**	**1,029,000**	**95.37**	**1.05**	**3,214,000**

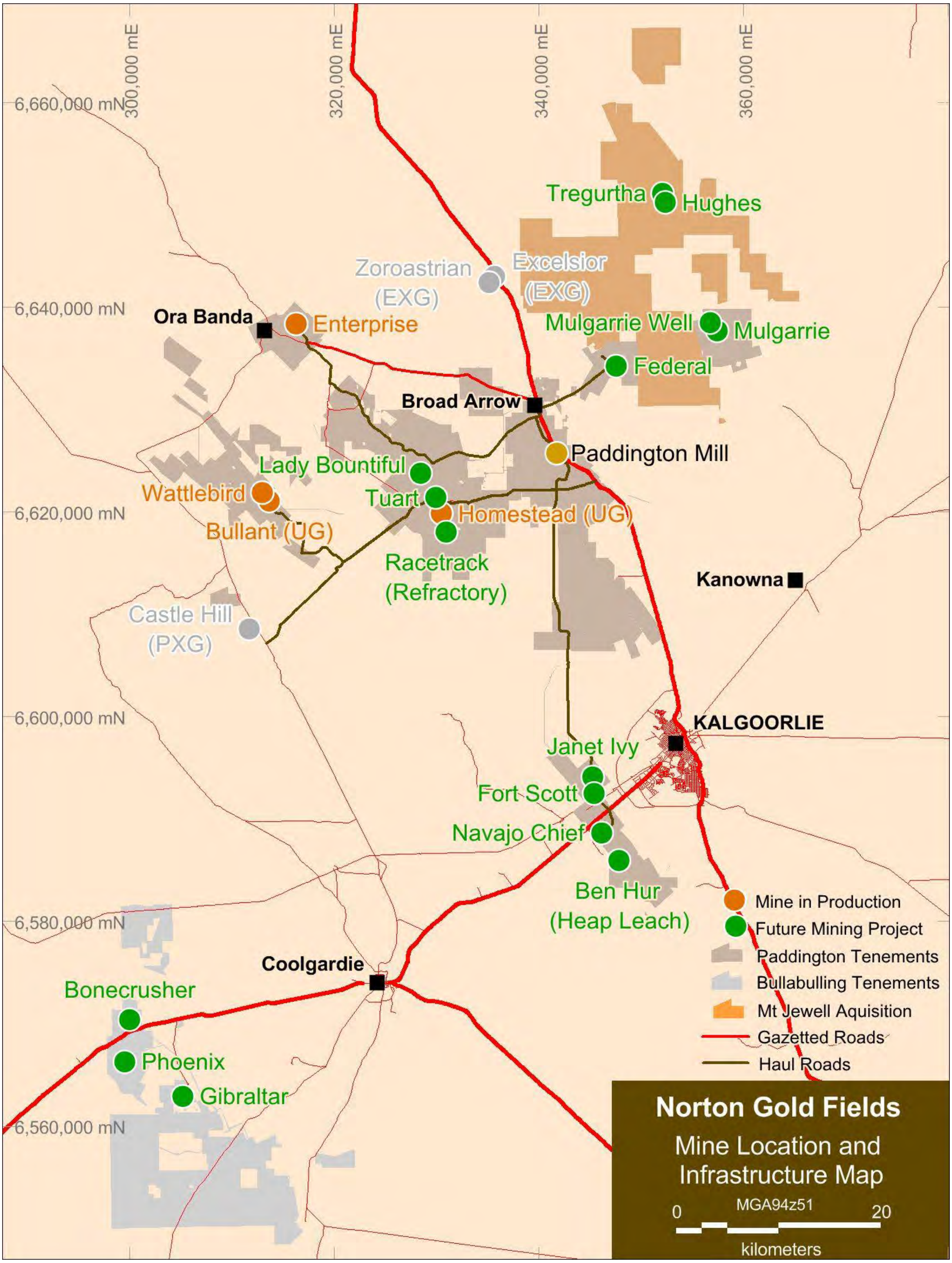
Note: Apparent arithmetic inconsistencies are due to rounding

Table 5: Norton Gold Fields – Paddington Ore Reserve as at 31 December 2014

	Proven			Probable			Total		
	Tonnes	Grade	Ounces	Tonnes	Grade	Ounces	Tonnes	Grade	Ounces
Open Pit									
Federal				1,858,968	1.72	102,686	1,858,968	1.72	102,686
Enterprise				4,839,083	2.00	311,841	4,839,083	2.00	311,841
Mulgarrie				815,857	2.23	58,599	815,857	2.23	58,599
Janet Ivy				2,394,257	1.11	85,291	2,394,257	1.11	85,291
Fort Scott				273,522	1.36	11,992	273,522	1.36	11,992
Wattle Bird	48,250	1.19	1,840	343,959	1.62	17,904	392,209	1.57	19,744
Lady Bountiful				818,646	1.73	45,462	818,646	1.73	45,462
Tuart				1,718,567	1.67	92,273	1,718,567	1.67	92,273
Mulgarrie Well				177,550	1.56	8,879	177,550	1.56	8,879
Hughes				674,679	1.19	25,833	674,679	1.19	25,833
Tregutha				504,241	1.68	27,265	504,241	1.68	27,265
Woolshed South Extended				304,238	1.61	15,745	304,238	1.61	15,745
Open Pit Total	**48,250**	**1.19**	**1,840**	**14,723,567**	**1.70**	**803,768**	**14,771,817**	**1.70**	**805,608**
Underground									
Homestead	157,054	6.35	32,061	64,387	7.02	14,531	221,441	6.54	46,591
Bullant	66,997	3.23	6,966	360,218	3.41	39,455	427,215	3.38	46,421
Enterprise				1,626,036	3.10	162,311	1,626,036	3.10	162,311
Underground Total	**224,051**	**5.42**	**39,027**	**2,050,641**	**3.28**	**216,297**	**2,274,692**	**3.49**	**255,324**
Stockpiles	**1,399,626**	**0.91**	**41,457**	**81,117**	**1.21**	**3,148**	**1,480,742**	**0.94**	**44,604**
INVENTORY - GIC									**3,339**
Total Reserves	**1,671,926**	**1.53**	**82,324**	**16,855,324**	**1.89**	**1,023,213**	**18,527,251**	**1.86**	**1,108,876**

Note: Apparent arithmetic inconsistencies are due to rounding

Figure 1: Norton Gold Fields – Project Location Map



Mineral Resource & Ore Reserve Update

Mineral Resources and Ore Reserves for the Paddington Project as at 31 December 2013 were announced on 24 January 2014. Total Measured, Indicated and Inferred Mineral Resources comprised 134Mt at 1.61g/t Au containing 6.94Moz. Proven and Probable Reserves totalled 19Mt at 1.75g/t Au containing 1.07 million ounces.

Mineral Resource and Ore Reserve updates as at 31 December 2014 now comprise total Measured, Indicated and Inferred Mineral Resources of 247Mt at 1.30g/t Au containing 10.35Moz, and total Proven and Probable Reserves of 18.5Mt at 1.87g/t Au containing 1.11Moz. These figures represent a net mineral resource increase of 3.41oz (49%), and a net ore reserve increase of 36,000oz (+3.3%). Production for CY2014 was 178,269oz.

Status changes between the current statement and that reported previously are summarized below. Variances in the Mineral Resource position include:

- Acquisition of the Bullabulling and Mt Jewell Projects
- Mineral Resource modelling updates at Homestead Underground, Bullant Underground, Racetrack, Tuart, Ben Hur, Fort Scott, Wattlebird and Mulgarrie Well
- Mining depletion at:
  - Enterprise
  - Homestead Underground (including Black Flag west)
  - Bullant Underground
  - Wattlebird
  - Green Gum
  - Golden Flag
- Re-definition of open-cut and underground reporting areas at Enterprise
- Resource depletion due to consideration of economic factors
- Some minor modification of reporting cut-off grade
- Change in reporting area allocation:
  - Parts of the current Racetrack area were previously included within the Mt Pleasant Mineral Resource group

Variances in the ore reserve statement include:

- Acquisition of the Mt Jewell – Hughes and Tregurtha Projects
- New mine plan and reserves at Bullant Underground and Enterprise Underground
- New mine plan and reserves at Woolshed South, Mulgarrie Well, Hughes and Tregurtha
- Reserve addition or modification based on Mineral Resource updates and operating cost reductions at:
  - Tuart
  - Lady Bountiful

- Ore Reserve modification due to lower gold price at all projects
- Mining depletion at:
  - Enterprise
  - Homestead Underground (including Black Flag west)
  - Bullant Underground
  - Wattlebird
  - Green Gum
  - Golden Flag

Detail on previously unreported Mineral Resource and Ore Reserve inventory is contained in the appended JORC 2012 Table 1 documentation.

Figure 2: Mineral Resource Status

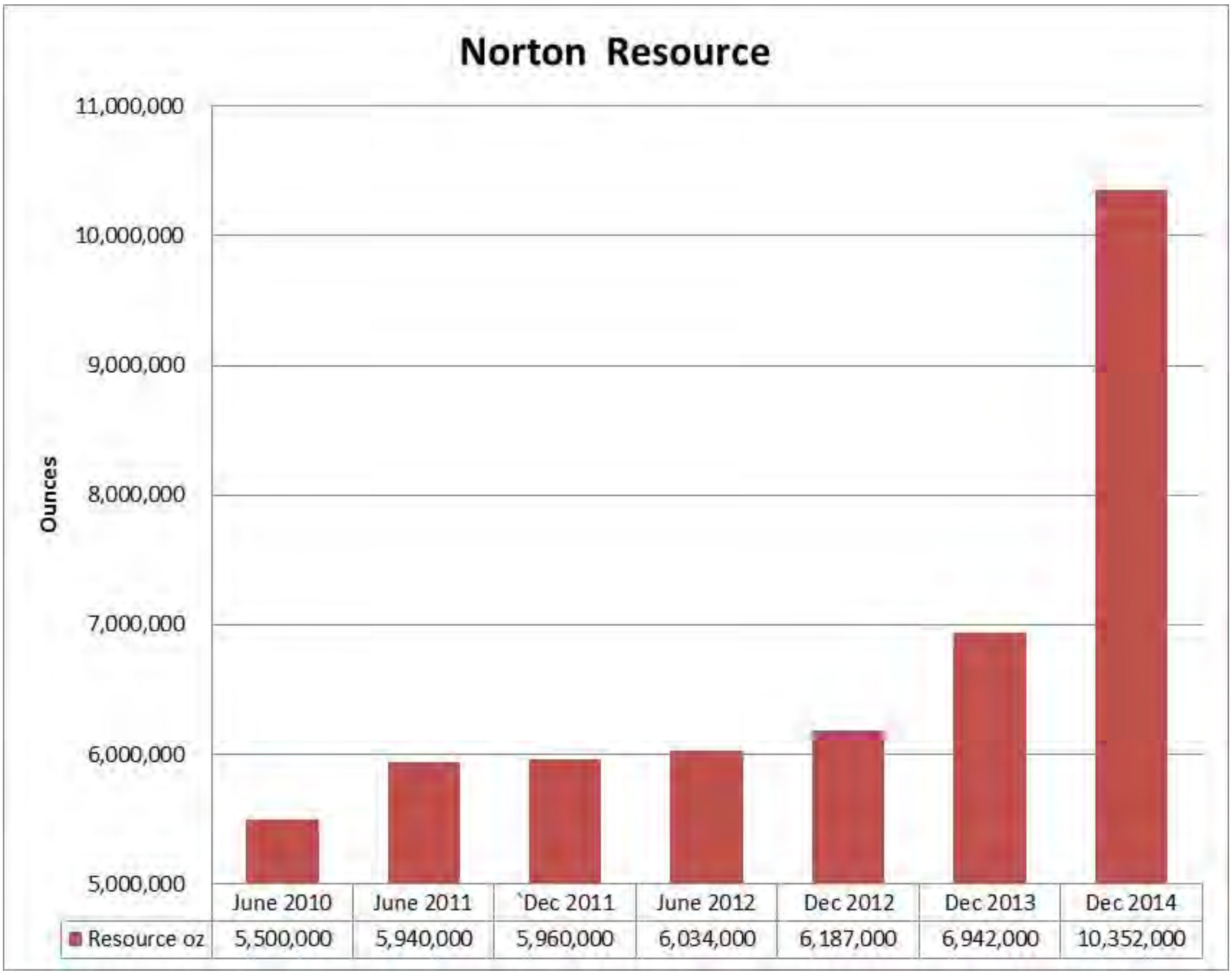


Figure 3: Mineral Resource Variance

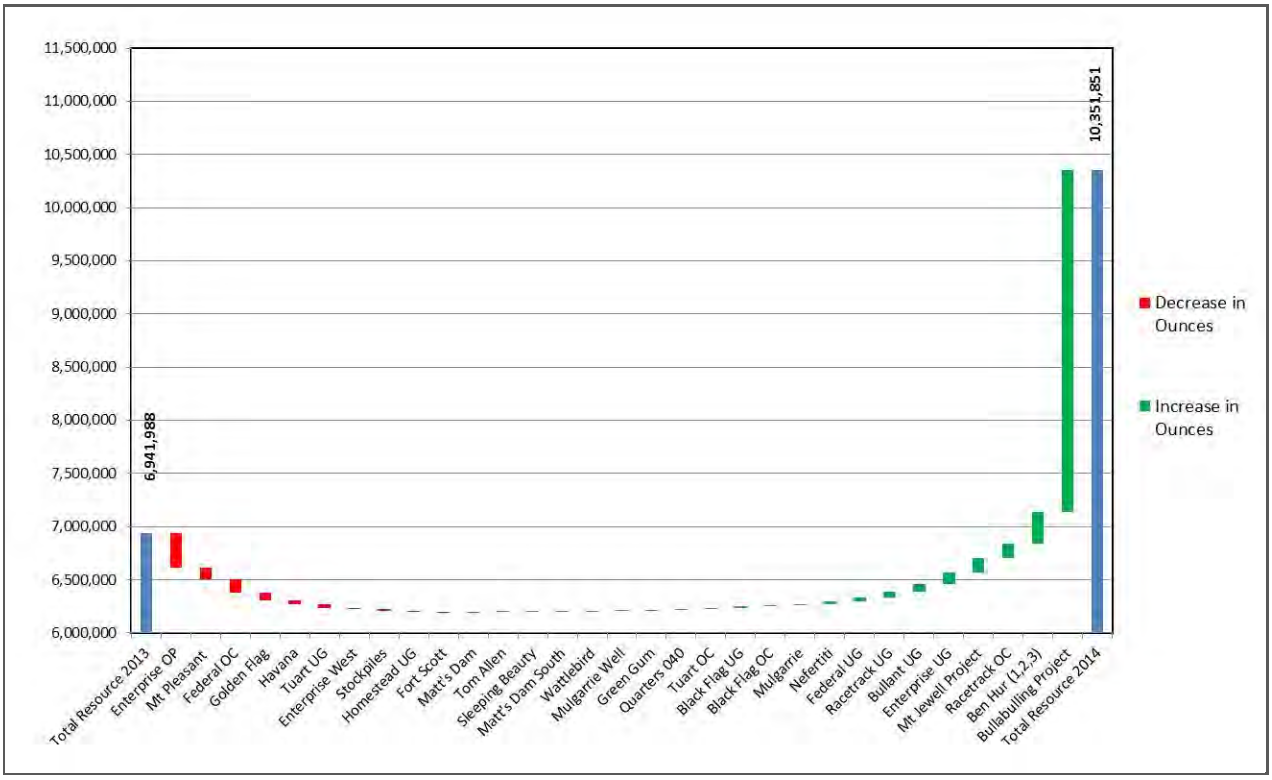
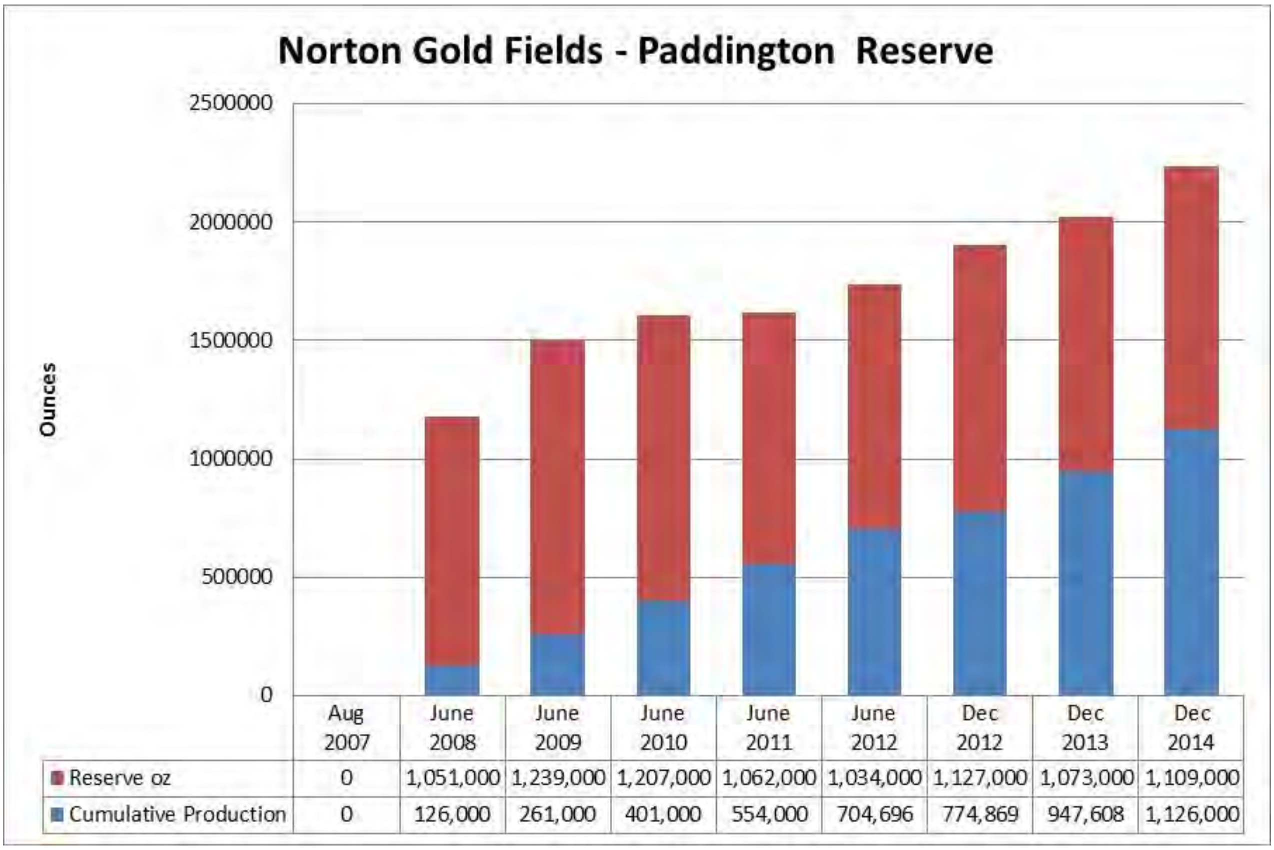
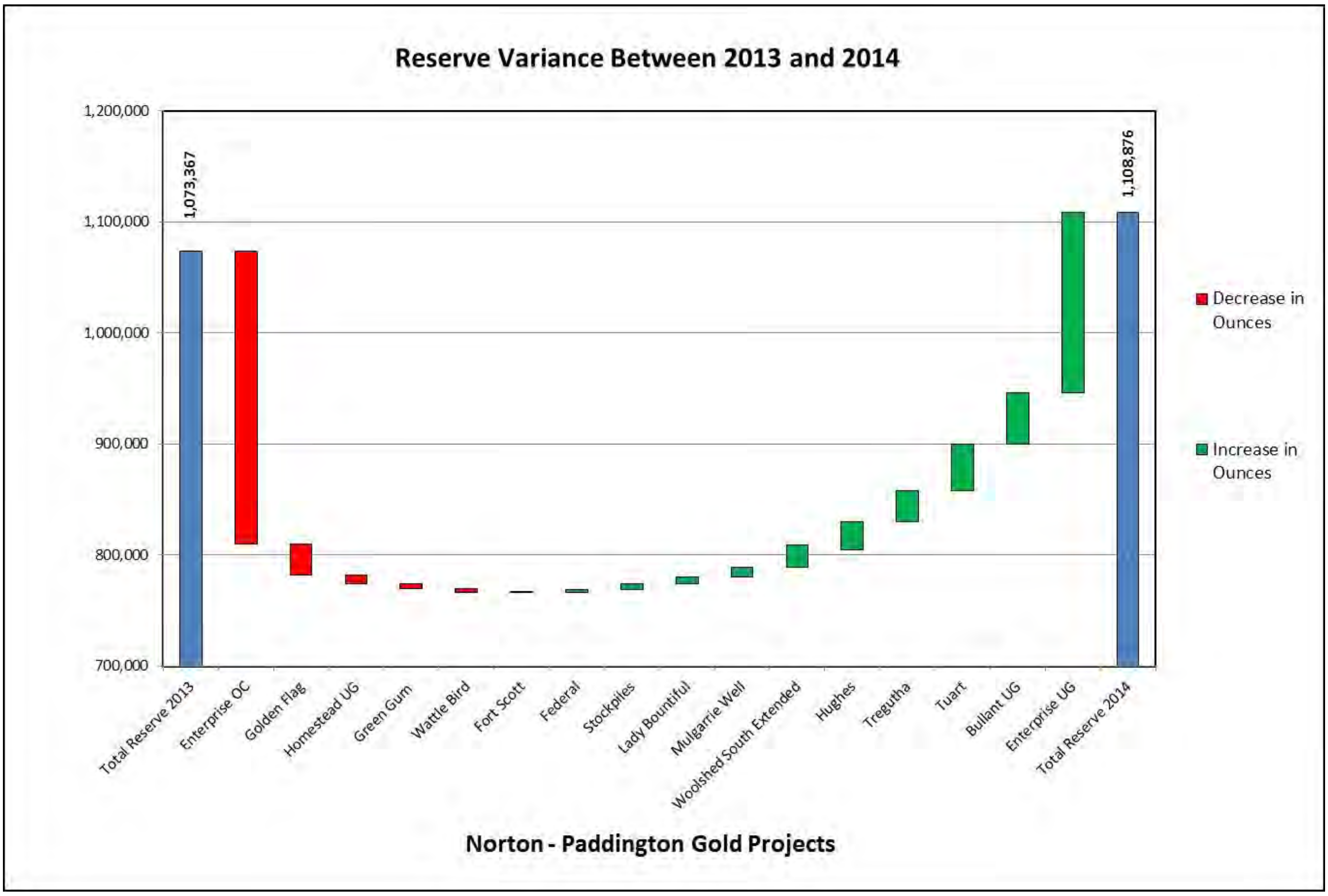


Figure 4: Production and Reserve Status



	Aug 2007	June 2008	June 2009	June 2010	June 2011	June 2012	Dec 2012	Dec 2013	Dec 2014
🟥 Reserve oz	0	1,051,000	1,239,000	1,207,000	1,062,000	1,034,000	1,127,000	1,073,000	1,109,000
🟦 Cumulative Production	0	126,000	261,000	401,000	554,000	704,696	774,869	947,608	1,126,000

Figure 5: Reserve Variance



Graphs illustrated in Figure 2 to Figure 5 demonstrate strong mineral resource growth, and a stable ore reserve inventory above 1Moz, despite mining production and depletion of 1,126,000oz since the Norton acquisition of Paddington in 2007.

A number of significant resource projects are being evaluated for future mineral resource to ore reserve conversion using alternate processing streams including:

- Racetrack refractory mineralisation (current resource of 730,000oz, including some oxide material)
- Binduli heap leach (current resource of 1.97Moz)

Evaluation of Racetrack refractory mineralisation is underway with substantial drilling programs completed during CY2014 and metallurgical testwork programs being planned. Historical metallurgical testwork indicates a high flotation recovery of sulphide hosted gold mineralisation, and effective recovery of gold through one of the oxidation processes, namely pressure oxidation, biological oxidation or ultra-fine grind oxidative leach.

Metallurgical testwork on potential Binduli heap leach ores to date has indicated favourable leach properties using high pressure grinding roll (HPGR) crushing technology. Testwork is continuing.

Mineral Resource Modelling Parameters

Mineral Resource models have been compiled using a number of modelling and estimation methodologies including Multiple Indicator Kriging (MIK), Ordinary Kriging (OK) and Inverse Distance Squared (ID2). Methodologies have been selected to best suit mineralisation styles which range from high grade narrow veins through to broad pervasive alteration or stockwork mineralised zones. In most cases validation models have been completed using alternate modelling techniques. Statistical analysis and variography of mineralised composites are utilised to control the estimation process. Estimation top-cut grades are based on statistical analysis of the relevant mineralisation domains. Lower reporting cut-off grades are based on break-even cut-off grades in similar deposits which have been mined by the Paddington Operation.

Drilling data utilised in mineral resource models includes a combination of reverse circulation (RC), surface diamond core, underground diamond core, and underground development face sampling. All sample analyses has been conducted at reputable analytical laboratories and data has been validated and subjected to internal quality control processes.

Drill spacing generally reflects the level of mineralisation continuity. As a guide, well defined mineralised areas with a nominal drill spacing of 20m x 20m qualify as Indicated classification status, with broader spaced drilling for Inferred classification status. Measured classification is applied to grade control drilled or underground developed mineralisation material.

Applied bulk densities are derived from measurements on diamond core or rock samples, and validated by comparison with similar lithological ore types from elsewhere within the project area (the Paddington Operation has been active since 1984 and has exploited a broad range of ore types in that period). Bulk density is coded by weathering type in each deposit to reflect oxide, transitional and primary ore characteristics.

Geological models are developed and continuously updated utilising feedback from mining and milling operations.

Details of all mineral resource models are documented in the appended JORC 2012 ‘Table 1’ documentation. A mineral resource parameter summary is shown below in Table 6.

Table 6: Mineral Resource Parameter Summary

Project Area	DEPOSIT	Modelling Methodology	Lower cut-off grade (g/t)	Top cut grade (g/t)
Golden Cities	Havana	OK	0.7	15
	Federal OC	OK	0.7	20 and 60
	Federal UG	OK	3	60
	Jakarta	MIK	0.6	NA
Mulgarrie	Mulgarrie	MIK	0.7	NA
	Mulgarrie Well	MIK	0.7	NA
Ora Banda	Enterprise OP	MIK	0.7	NA
	Enterprise UG	OK	1.5	nil
	Enterprise West	OK	0.7	10
	North Sandalwood	OK	0.7	nil - 12.5
	Sleeping Beauty	OK	0.7	6-15
	Tom Allen	OK	0.7	8 and 10
Greater Mt Pleasant	Mt Pleasant	OK	1.0	10-70
	Racetrack OC	OK	0.8	Various
	Racetrack UG	OK	3.0	Various
	Royal Standard North	ID2	0.8	8
	Green Gum	OK	0.7	20
	Blue Gum	OK	0.7	17
	Homestead UG	OK + ID2	3.5	nil & 50-200
	Golden Kilometre	OK	0	40
	Quarters 040	OK	0.7	17
	Tuart OC	OK	0.7	nil, 10, 30 and 37
	Tuart UG	OK	3.0	28, 30 and 40
	Marlock	OK	0.7	10 and 25
	Natal	OK	0.8	25 & 60
	Golden Flag	OK	0.7	10 & 20
	Black Flag OC	OK	0.7	5, 15 and 20
	Black Flag UG	ID2	3	nil and 30
	Rose Dam South	OK	0.7	nil
	Rose	OK	0.7	12
Lady Bountiful	Lady Bountiful	ID3	0.7	30
	Lady Bountiful Extended	OK	0.8	10-100, mostly 20-30
	Liberty West	OK	0.8	8.4-11.8
Binduli	Janet Ivy	MIK	0.5	NA
	Navajo Chief	MIK	0.5	NA
	Fort William	OK	0.6	10
	Fort Scott	OK	0.7	6-9
	Apache	Sectional polygonal	1.0	7
	Ben Hur (1,2,3)	MIK	0.5	NA
	Nefertiti	OK	0.5	NA
	Pitman South	Sectional polygonal	1.0	10
	Walsh	Sectional polygonal	1.0	7
	Walsh North	Sectional polygonal	1.0	7
Carbine	Bullant UG	OK	3.0	Various 20-50
	Wattlebird	MIK	0.7	NA
	Matt's Dam	ID2	0.7	6-8
	Matt's Dam South	ID2	0.7	15-22
	Porphyry	OK	0.8	5.5
Mt Jewell	Hughes	ID3	0.7	12
	Tregurtha	OK	0.7	5,15 and 20
Bullabulling	Bullabulling Trend	MIK (e-type) and OK	0.5	Various where applicable
	Gibraltar	MIK (e-type) and OK	0.5	Various where applicable

Ore Reserve Parameters

Open pit and underground ore reserves are generated from optimisation and design studies utilising appropriate mining methodology, geological/ geotechnical characteristics, equipment selection, and mining, haulage, processing and administration costing. Processing of ores is undertaken at the 3.5Mtpa Paddington mill. Metallurgical recovery of ores is documented from testwork or from previous treatment of similar geological ore types.

Open pit evaluation is generally based on Whittle Optimisation, mine design, scheduling and financial analysis. Underground evaluation is based on mine access, ore development, stope design, scheduling and financial analysis. Estimates of mining dilution and ore loss are guided by previous operating experience. Gold price is adjusted to reflect current spot price.

Open Cut:
Two different sized open cut mining fleets are utilised. The Bulk fleet comprises a Hitachi 3600 excavator and Caterpillar 789D dump-trucks. Selective fleets comprise two (2) Hitachi 1200 excavators and Caterpillar 777F dump-trucks.

Mining is conducted using conventional open cut drill and blast. Mining dilution in most deposits is estimated at 10%, and mining recovery is 95%.

Underground:
The underground load and haul fleet comprises Caterpillar R1700 loaders, Caterpillar R1300 loader and Caterpillar AD45B haul trucks.

Mining includes Jumbo development, Longhole Open Stoping and minor Airleg Stoping. Stoping is followed by Cemented Rock Backfill of the stoping void. Level interval is 15 – 25m. Ore drives are planned at 3.3m wide x 4.0m high or 4.0m wide by 4.5m high depending on area. Minimum mining width is 2m. Stoping dilution is estimated at 50 - 100% dependent on mining method. Ore loss is estimated at 5%.

Details of Ore Reserve estimation are documented in the appended JORC 2012 compliant 'Table 1' list. An Ore Reserve parameter summary is shown below in Table 7.

Table 7: Ore Reserve Parameter Summary

DEPOSIT	Mining Method	Status	Mining Study	Gold Price A$	Mining Dilution	Mining Ore Loss	Process Recovery	Ore cut-off grade (g/t Au)
Federal	Open Pit	Planned	Optimisation & Design	1,400	10%	5%	94%	0.75
Enterprise	Open Pit	Active	Optimisation & Design	1,400	0%	0%	83% - 94%	0.7 - 0.8
Mulgarrie	Open Pit	Planned	Optimisation & Design	1,400	0%	0%	94%	0.70
Janet Ivy	Open Pit	Planned	Optimisation	1,400	0%	0%	94%	0.70
Fort Scott	Open Pit	Planned	Optimisation & Design	1,400	10%	5%	94%	0.75
Wattle Bird	Open Pit	Active	Optimisation & Design	1,400	0%	0%	94%	0.70
Lady Bountiful	Open Pit	Planned	Optimisation & Design	1,400	10%	5%	94%	0.65
Tuart	Open Pit	Planned	Optimisation & Design	1,400	5%	5%	94%	0.70
Mulgarrie Well	Open Pit	Planned	Optimisation & Design	1,400	0%	0%	93%	0.6
Hughes	Open Pit	Planned	Optimisation & Design	1,400	10%	5%	94%	0.75
Tregurtha	Open Pit	Planned	Optimisation & Design	1,400	10%	5%	94%	0.75
Woolshed Sth Ext	Open Pit	Planned	Optimisation & Design	1,400	10%	5%	94%	0.70
Homestead U/G	Underground	Active	Mine Design	1,400	12%-53%	5%	94%	3.29
Bullant UG	Underground	Active	Mine Design	1,400	27%-40%	5%	94%	3.29
Enterprise	Underground	Planned	Mine Design	1,400	10%	5%	83%	2.12

Appendices:
JORC 2012 'Table 1' Documentation

JORC Code, 2012 Edition

Table 1 Report for the Greater Mt Pleasant area - Resource and Reserve Estimate Updates, December 2014

Section 1 Sampling Techniques & Data

Criteria	Commentary
Sampling techniques	• Sampling completed utilising a combination of Reverse Circulation (RC) & Diamond Core (DC) holes on 20m x 20m to 80m x 80m grid spacing. Drilling & sampling has been conducted by various companies over several campaigns since 1995 & includes exploration, resource development & grade control (GC) sampling (UG & open pit RC GC). Sampling techniques are summarised from drilling & sampling manuals/reports from Centaur Mining & Exploration, AurionGold, Placer Dome Asia Pacific, Barrick & Norton Gold Fields. • The drill hole locations were designed & oriented to allow for spatial spread of samples across mineralised zones & different rock types. • Field-based observations from geological supervision & geological records referring to sample quality, moisture content & recovery were used as a guide to sample representative. • All RC-recovered samples were passed through a splitting device (cone or riffle splitter) at 1m intervals to obtain a sample for assay, collected in an appropriately-sized calico bag. RC calico sample weights range from 2.5 to 4kg across all RC drilling campaigns (1995-2014). Bulk reject sample was also collected into a plastic bag for each metre. For legacy data, spear samples composited to 4m or less were collected from the bulk samples as a first-pass sampling technique. Single metre samples were collected & submitted for assay from areas of expected mineralisation or composite anomalism. • DC samples were placed into core trays at the rig & transferred to core processing facilities for logging, sawing/splitting & sampling. The DC samples are collected at nominated intervals by a Geologist from resultant half core with a minimum interval of 0.3m & a maximum of 1m.
Drilling techniques	• All assays referred to for resource estimation (1995-2014) were collected from either RC or DC drilling using various contractors. Early legacy RC drilling may have been performed by RC hammer with a cross-over sub, drag bit or skirted tricone bit; the details are generally not specified. The most recent drilling campaigns account for around 5% of the total drilling dataset. • Norton RC sampling is completed under contract by Drilling Australia using a Schramm T68SW equipped using Sullair combo-compressor (1150cfm/350psi or 900cfm/500psi) using a 5.25” or 5.5” diameter drill bit with a 5” Sandvik RE054 bottom face sampling hammer equipped with a rig mounted Metzke cone splitter. • DC sampling is a combination of HQ (63.5mm diameter) and/or NQ (47.6mm diameter) or NQ2 (50.5mm diameter) core sizes. DC is orientated by either a bottom of hole spear; EZI-Mark or ACE digital orientation systems.

Criteria	Commentary
Drill sample recovery	• RC Drillers are advised by geologists on the ground conditions expected for each hole & instructed to adopt an RC drilling strategy to maximize sample recovery, minimize contamination & maintain required spatial position. • All RC 1m sample rejects are collected into a UV resistant bag. Samples are visually logged for moisture content, qualitative estimated sample recovery & contamination. The DC samples are orientated, length measured & compared to core blocks denoting drilling depths by the drilling contractor. Any recovery issues are recorded. Sample loss or gain is reviewed at the time of drilling & feedback is provided to the drilling contractor to ensure the samples are representative. • DC contractors use a core barrel & wire line unit to recover the DC, adjusting drilling methods & rates to minimize core loss (e.g. changing rock type, broken ground conditions etc.). • A study of the weights of the 1m RC sample splits & gold grades (2012-2013 drilling) shows no correlation. The drilling contractors utilised drilling techniques to ensure minimal loss of any size fraction.
Logging	• All current RC samples are geologically logged at 1m interval which is an appropriate level of detail to support a Mineral Resource estimation. Some historic RC drilling intervals were selectively logged. Currently, each interval is inspected & the following parameters are recorded: weathering, regolith, rock type, alteration, mineralisation & structure. All DC is logged for core loss, photographed, marked into 1m intervals, orientated, structurally logged, geotechnically logged & geologically logged for the following parameters: weathering, regolith, rock type, alteration, & mineralisation. • Geological logging is qualitative & quantitative in nature. • All recent RC holes are logged in their entirety on a 1m interval basis. Where no sample is returned due to voids or lost sample, it is logged & recorded as such. DC is also logged over its entire length & any core loss or voids are recorded.
Sub-sampling techniques & sample preparation	• Assays from DC are all half core samples. The remaining DC resides in the core tray & is archived. • All RC samples were split by a cone or a riffle splitter & collected into a sequenced calico bag. For historical drilling, any wet samples that could not be riffle split initially were dried then riffle split. • The sample preparation conducted by commercial laboratories involves jaw crushing to nominal <10mm (DC), a riffle split to 3.5kg as required, & pulverizing in a one stage process to >85% passing 75um. The bulk pulverized sample is then collected & approximately 200g extracted by spatula to a numbered paper bag that is used for the 30g or 50g fire assay charge. Laboratory Quality Control (QC) includes duplicate samples collected after the jaw crushing stage, & repeat samples collected after the pulverising stage to provide data confirming the appropriateness of the sample preparation technique. All sub-sampling & lab preparations are consistent with other laboratories in Australia. • RC & DC samples submitted to the laboratory are sorted & reconciled against the submission documents. Routine CRM (standards & blanks) are inserted into the sampling sequence at a rate of 1:20 for standards or in specific zones at the Geologist's discretion. The commercial laboratories complete their own QC check. Both RC and diamond drilling campaigns utilised barren quartz flushes between

Criteria	Commentary
	expected mineralized sample interval(s) when pulverising. Selected barren quartz materials flushed within expected mineralised interval are assayed to identify potential smearing. • RC field duplicate data was collected routinely & for selected intervals suspected to contain mineralisation. Field duplicate samples were taken at the time of cone/riffle splitting the bulk sample at the drill rig to maintain sample support. The field duplicates are submitted for assay using the same process mentioned above, with the laboratory unaware of the duplicate nature. Some historic DC duplicates were taken by re-sampling ¼ of the remaining half core. • Sample sizes are considered appropriate to the grain size of the material being sampled on the basis of satisfactory duplicate correlations at all stages of the sample comminution process.
Quality of assay data & laboratory tests	• The assay method is designed to measure total gold in the sample. The laboratory procedures are considered appropriate for the testing of gold at this project given its mineralisation style. The technique involved using a 30g or 50g sample charge with a lead flux, which is decomposed in a furnace, with the prill being totally digested by 2 acids (HCl & HN03) before determination of gold by an AAS machine. • No geophysical tools or other remote sensing instruments were utilised for reporting or interpretation of gold mineralisation. • RC & DC samples submitted to the laboratory are sorted & reconciled against the submission documents. Certified Reference Material (CRM) (standards & blanks) are inserted into the sampling sequence at a rate of 1:25 for standards or in specific zones at the Geologist's discretion. The commercial laboratories undertake their own QC checks. Specific diamond drilling campaigns utilised barren quartz flushes between expected mineralised sample interval(s) when pulverizing. In the absence of Certified Blank Material, selected barren quartz materials flushed within expected mineralised interval are assayed to identify potential smearing. • Standard procedures are to examine any erroneous QC result (a result outside of expected statistically derived tolerance limits) & validate if required; establishing acceptable levels of accuracy & precision for all stages of the sampling & analytical process.
Verification of sampling & assaying	• Independent verification of significant intersections not considered material. • No holes were twinned. • Primary logging & sampling data is sent digitally every 2-3 days from the field to the company's Database Administrator (DBA). The DBA imports the data into a relational DataShed database, observing a number a validation checks. When assay results are received electronically from the laboratory, results & laboratory QAQC are also imported into the database after further validation checks. The responsible Geologist reviews the data in the database to ensure that it is correct & has merged properly & that all data has been received & entered. Any variations that are required are recorded permanently in the database. • No adjustments or calibrations were made to any assay data used in this report.
Location of data points	• After drilling, drill hole collar positions are surveyed by the site-based survey department (utilising either a theodolite or differential GPS) with a precision of less than 0.2m.

Criteria	Commentary
	• Down hole surveys consist of regular-spaced Eastman single shot, & electronic multi-shot surveys (generally <30m apart down hole). A minor amount of historic drill holes only have collar surveys. Ground magnetics can affect the result of the measured azimuth reading for these survey instruments. Most relatively recent survey data consists of surveys taken with north-seeking gyro instruments, representing more recent drilling. Gyro survey measurements are obtained every 5m down hole. • Recent data is collected in MGA 94 Zone 51 & AHD. Data pre-2012 was collected in AMG 84 Zone 51 & AHD. • Topographic control was generated from survey pick-ups of the area over the last 15 years, which have been used to generate an as-built and current Digital Terrain Model (DTM).
Data spacing & distribution	• The nominal drill spacing is 20m x 20m; with some areas at 40m x 40m & increasing to 80m x 80m past 0mRL. This description of data spacing refers to both the classified & unclassified portion of the deposits. Grade Control (GC) data (where applicable) is on 5m x 5m to 10m x 10m spacing. This spacing includes data that has been verified from previous exploration activities on the project. • Data spacing & distribution is considered acceptable for establishing geological continuity & grade variability appropriate for classifying a Mineral Resource. This inference is based on historical mining & reconciliation data. • Samples were composited to either 1m or 2m down hole prior to modelling.
Orientation of data in relation to geological structure	• Where practicable, drilling is orientated at a high angle to the dip or plunge of the mineralisation (depending on the direction of highest gold grade continuity). This technique enables sampling to be representative of true width of the mineralisation. • No drilling orientation & sampling bias has been recognized at this time.
Sample security	• Samples were under the custodial chain of the company until delivered to a commercial laboratory some 30km south of the operations; upon which they were secured in a fenced compound with restricted entry. Internally, the commercial laboratories operate an audit trail tracking the samples at all times whilst in their custody. • Historic samples are assumed to have been under the security of the respective tenement holders until delivered to the laboratory where they are assumed to have been under restricted access.
Audits or reviews	• Internal reviews are completed on sampling techniques & data as part of the Norton Gold Fields continuous improvement practice. No external or third party audits or reviews have been completed.

Section 2 Reporting of Exploration Results

Criteria	Commentary
Mineral tenement & land tenure status	• The Mt Pleasant resource is located within Mining Licenses M 24/16, 79, 82, 155, 166, 227, 234, 265-266, 302, 304, 393, 433 & 710. General Purpose lease G 24/11 & Miscellaneous leases L 24/54 & 205-206 are also located within the resource area. All tenements are 100% held by Paddington Gold P/L, a wholly owned subsidiary of Norton Gold Fields P/L. Several heritage sites exist within the tenure. All leases are granted pre-Native Title. Third party royalties are applicable to these tenements & are based on production ($/t) or proportion of net profit. All production is subject to a WA state government NSR royalty of 2.5%. • The tenements are in good standing & no known impediments exist.
Exploration done by other parties	• A significant proportion of exploration, resource development & mining was completed by companies which held tenure over Mt Pleasant since the mid 1990's. Companies included: Centaur Mining & Exploration PL (1995-2001), Auriongold (2001-2002), Placer Dome Asia Pacific (2002-2005) & Barrick Kanowna (2005-2007). Results of exploration & mining activities by the afore-mentioned companies has assisted in Norton Gold Field's more recent exploration, resource development & mining in the area. • **Reporting of results within this release only relates to results obtained since the September 2014 Quarterly Exploration Report.**
Geology	• The Mount Pleasant Resource comprises 13 individual deposits that are characterised in a geological setting. Deposits from north to south are: Golden Kilometre, Marlock, Salmon Gum, Blue Gum, Blue Gum South, Green Gum, Golden Flag, Rose, Rose Dam South, Golden Road, Woolshed, Woolshed South, Woolshed South Extended, Racetrack & Natal. • The deposit types are classified as narrow vein, orogenic gold deposits within the Norseman-Wiluna greenstone sequence. The accepted interpretation for gold mineralisation is related to (regional D2-D3) deformation of the stratigraphic sequence during an Archaean orogeny event. The mineralisation is hosted within the upper-mafic rock units of the Kalgoorlie stratigraphy. The metamorphic grade is defined as lower green-schist facies. The mineralisation is located in brittle-ductile shear zones typically associated with carbonate-sericite alteration +/- sulphides. • A second type of deposit is classified as supergene-enriched gold formed by geochemical processes, where mineralised structures intersect the regolith profile. • A third type of deposit is classified as Palaeo-channel related gold mineralisation associated with the mechanical transport & geochemical enrichment of gold within the Tertiary material.
Drill hole Information	• See Appendices 1-5.
Data aggregation methods	• All reported assay results have been length-weighted; no top cuts have been applied. Assay results are reported to a 0.8g/t Au lower cut over a minimum intersection of 1m for RC & 0.3m for DC. • A maximum of 2m of internal dilution (i.e. <2m @ <0.8g/t Au) is included for reporting RC intercepts targeting the supergene mineralisation & for DDH intercepts targeting the fresh rock mineralisation. • No metal equivalent values are used for reporting exploration results.

Criteria	Commentary
Relationship between mineralisation widths & intercept lengths	• Drill hole intersections are generally at a high angle to each mineralised zone. Reported down hole intersections are noted as approximately true width, or otherwise are denoted as 'true width not known'.
Diagrams	• See Appendices 3-5.
Balanced reporting	• All results have been reported relative to the intersection criteria.
Other substantive exploration data	• No other exploration data collected is considered material to this announcement. **Material known to be refractory is denoted as such in the respective resource.**
Further work	• Further work will include mining studies to determine if the project is economic to mine. Interpreted mineralised plunge directions require drill testing if mining studies indicate that the project is economic.

Section 3 Estimation & Reporting of Mineral Resources

Criteria	Commentary
Database integrity	• NGF employs SQL as the central data storage system using DataShed software as a front-end interface. User access to the database is regulated by specific user permissions, & validation checks & relational steps are part of the process to ensure data remains valid. • Existing protocols maximize data functionality & quality whilst minimizing the likelihood of introducing errors at primary data collection points & subsequent database upload, storage & retrieval points. Data templates with lookup tables & fixed formatting are used for collecting primary data on field laptops. The software has validation routines & data is subsequently imported into a secure central database. • The SQL server database is configured for validation through constraints, library tables, triggers & stored procedures. Data that fails these rules on import is rejected or quarantined until it is corrected. • The Database is centrally managed by a Database Manager who is responsible for all aspects of data entry, validation, development, quality control & specialist queries. There is a standard suite of vigorous validation checks for all data.
Site visits	• The Competent Person for this resource estimate is a full time employee of NGF & undertakes regular site visits ensuring industry standards of the Mineral Resource estimation process from sampling through to the final block model. • The deposit area is an active mining area for NGF & as such, regular site visits were undertaken during this update.
Geological interpretation	• The confidence of the geological interpretation is based on geological knowledge acquired from open pit production data, detailed geological DC & RC logging, assay data, underground development face mapping & pit mapping. No alternate interpretations are proposed as geological confidence in each model is high.

Criteria	Commentary
	• The dataset (geological mapping, RC & DC logging, assays etc.) is considered acceptable for determining a geological model. Key interpretation assumptions made for this estimation are: (1) where cross cutting relationships were not observed; & (2) the interpretation of the mineralisation past known drilling limits (extrapolated a reasonable distance considering geological & grade continuity – not more than the maximum drill spacing). • The geological interpretation is considered robust & alternative interpretations are considered not to have a material effect on the Mineral Resource. As additional geological data is collated the geological interpretation is continually being updated. • The geological interpretation is specifically based on identifying particular lithological boundaries, geological structures, associated alteration, veining & gold content. • Whilst the geological features are interpreted to be continuous, the gold distribution within them can be highly variable. This issue is mitigated by close-spaced sampling & ensuring sample & analytical quality is high. Historic mining data is also used to assist with understanding grade continuity. Geological structures post-dating the mineralisation can off-set & truncate the mineralisation affecting the geological continuity & are difficult to isolate.
Dimensions	• The Mount Pleasant resource area deposit is spatially located between 328,350mE & 335,700mE & 6,614,700mN to 6,622,600mN (MGA94 zone51). Mineralisation is observed to extend at least to 500m below the natural surface. • The resource is broken into several (smaller) resource models to accommodate local scale geological & resource parameter differences. • **In those cases where resource model has changed since the January 2014 Mineral & Ore Reserve Statement, the deposits are described below.** **Black Flag OC** • The Black Flag resource area deposit is spatially located between 329,800mE and 330,950mE and 6,619,100mN to 6,620,200 (MGA94 zone51). Mineralisation is observed to extend at least to 300m below the natural surface. • Gold mineralisation at Black Flag is located within the Black Flag Fault where the strike changes from 020° to 045° and has a vertical dip. Mineralisation has a strike extent of 700m and a dip extent of at least 290m. Mineralisation starts from surface. Supergene mineralisation (with a flat orientation) is also observed at the intersection of the Black Flag Fault and the regolith profile. • Black Flag forms part of the Henning area within the Mt Pleasant resource. Gold mineralisation within the Henning area is controlled by the Black Flag Fault structure and associated structural splays. The Henning area dimensions are between 329,500mE and 330,700mE and 6,618,850mN and 6,620250mN. **Black Flag UG** • The Black Flag resource area deposit is spatially located between 330,220mE and 330,860mE and 6,619,460mN to 6,620,140 (MGA94 zone51). Mineralisation is observed to extend at least to 250m below the natural surface. • Gold mineralisation modelled for the Black Flag underground resource associated in two vein breccia complexes. The mineralised system has a strike of 640m with a steep south-east dip of 85°. Dip extent for the south-east breccia complex is 300m with vein widths from 1m to 4m.

Criteria	Commentary
	Tuart: • The Tuart deposit is spatially located between 329,200mE and 330,100mE – running into the Quarters deposit and 6,620,400mN to 6,621,700mN (AMG84 zone51). Up to 5 gold lodes on varying orientations have been located. ○ T060 lode: -45° towards 330°, 1km strike and 150m known dip extent ○ T080 lode: sub-vertical dip and E-W strike, 600m strike 250m known dip extent ○ T115 lode: -55° towards 295°, 500m strike and 250m known dip extent ○ Q040 lode: convex dip striking ~070° then turning to 040° at Quarters, 350m dip extent ○ Golden Swan: moderate south dip and ENE strike, know strike 400m and known dip 100m. • Each lode is typically 0.5 to 2m wide true width. Bonanza intercepts are up to 4m wide (true width). Supergene mineralization is observed at the interface of the gold lodes with the regolith profile. Some gold is associated with the Tertiary material. Gold mineralization starts at 15m-25m below surface (supergene) & extends to 360m below surface (the extent of drilling). **Grand Racetrack OP (including Previous Racetrack and Woolshed South and Woolshed South Extended):** • Racetrack OP resource is gold deposit and hosted in the Victorious Basalt and the underlying Bent Tree Basalt and intrusion intermediate porphyry. Racetrack is located along splay structures Racetrack Shear/fault and Woolshed fault zone associated with the Black Flag Fault. Mineralisation is observed in multiply lodes orientate 20° to 70°. Lode widths are approximately 1~8m width. The lodes have a strike extent of 1200m & a dip extent of more than 600m. Supergene mineralisation (with a flat orientation) is also observed at the intersection of the lodes & the regolith profile. • The deposit dimensions are between 328,820mE & 330,980mE & 6,617,9660mN & 6,621,300mN. Mineralisation exists at 10m below the surface extends to at least 500m below. **Racetrack UG:** • Racetrack UG Resource dimensions are between 330,070mE & 330,870mE & 6,618,350mN & 6,620,050mN. Primary mineralisation exists at 40 m below the surface extends to at least 500m below. • Racetrack UG resource is hosted in the Victorious Basalt and the underlying Bent Tree Basalt and intrusion intermediate porphyry, same as OP Resource. High grade primary lodes are associated with Racetrack Shear/fualt system, orientate 55~75° moderate dip to northwest. Lodes have a strike extent of 300~700m and down dip of 200~400m. Lode widths are approximately 0.5~4m width.
Estimation & modelling techniques	**Grand Racetrack OP: (Racetrack, Woolshed South & Woolshed South Extended)** • Geological domains were based on the geological interpretation & mineralised trends. 3DM wireframes created by 20m spacing sectional interpretation of the drilling dataset. Where there was geological uncertainty, domain boundaries were modelled nominal at a 0.2g/t Au lower cut for supergene mineralisation and 0.5 g/t Au for primary mineralisation, a minimum interval of 4m is applied. Domain boundaries were treated as hard boundaries.

Criteria	Commentary
	• 2m composites were generated based on database coding from drilling hole intercepts inside domain 3DMs. • The statistics for each domain were viewed & key univariate statistical indicators used to describe the nature of each. Each domain showed a positively skewed data distribution with high-grade outlier composites. Top-cuts were applied based on mineralisation type and geo-statistics, ranging from 4g/t Au to 20g/t Au applied to domains whose coefficient of variation is above 1.75 until below 1.75. • Estimation was completed using GEOVIA Surpac software version 6.6.1, utilising the block modelling module. • Estimation was completed using a linear estimation technique. Both Ordinary Kriging (OK) and Inverse Distance Power 3 (ID3) was employed for grade interpretation, OK estimate results is suggested for reporting resource, ID3 is used for validation estimation purpose. • Sample search ellipses were set based on data spacing in similar orientation to the major mineralised orientation. Minimum & maximum samples were set for each sample search based on accepted levels of grade continuity. Search distances were based on sample spacing & spatial continuity. A total of 3 search passes were conducted with progressively relaxed search criteria to accommodate the data density. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered material to this style of mineralisation. • Block sizes were chosen to compromise between sample spacing & orientation of mineralisation i.e. 5m(X) by 5m(Y) by 2.5m (Z), block was rotated 55 degree to parallel orientation of major mineralisation. • The SMU is based on current open pit mining fleet configuration. The SMU is comparable to the block size of the resource model. • No correlation between variables was necessary. • The 3DM/DTM wireframes for the estimation domains, regolith & topographical files were used to constrain the resource estimate. Blocks from the block model were coded based on these volumes/surfaces by either block centroid in/out of 3DM or above/below a DTM surface. • Model validation has been completed using visual & numerical methods & formal peer review sessions by key geology staff.
	Racetrack UG:
	• Geological domains were based on the geological interpretation & mineralised trends. 3DM wireframes created by 20m spacing sectional interpretation of the drilling dataset. Where there was geological uncertainty, domain boundaries were modelled nominal at a 1.0 g/t Au for primary mineralisation. Domain boundaries were treated as hard boundaries. • 1m composites were generated based on database coding from drilling hole intercepts inside domain 3DMs.

Criteria	Commentary
	• The statistics for each domain were viewed & key univariate statistical indicators used to describe the nature of each. Each domain showed a positively skewed data distribution with high-grade outlier composites. Top-cuts ranging from 12g/t Au to 60g/t Au applied to domains whose coefficient of variation is above 1.25 until below 1.25. • Estimation was completed using GEOVIA Surpac software version 6.6.1, utilising the block modelling module. • Estimation was completed using a linear estimation technique. Ordinary Kriging (OK) was employed for gold grade interpretation. • Sample search ellipses were set based on data spacing in similar orientation to the major mineralised orientation. Minimum & maximum samples were set for each sample search based on accepted levels of grade continuity. Search distances were based on sample spacing & spatial continuity. A total of 3 search passes were conducted with progressively relaxed search criteria to accommodate the data density. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered material to this style of mineralisation. • Block sizes were chosen to compromise between sample spacing & orientation of mineralisation. Parent block size is 20m(Y) by 4m(X) by 1m (Z), sub block size is 5m(Y) by 0.5m(X) by 0.5m (Z). Block was rotated 60 degree to parallel orientation of major mineralisation. • The 3DM/DTM wireframes for the estimation domains, regolith & topographical files were used to constrain the resource estimate. Blocks from the block model were coded based on these volumes/surfaces by either block centroid in/out of 3DM or above/below a DTM surface. • Model validation has been completed using visual & numerical methods & formal peer review sessions by key geology staff.
	Tuart
	• Estimation was completed using a linear estimation technique - Ordinary Kriging (OK). OK is an estimation method where a single direction of continuity is modelled for each domain for a global estimate. An advantage of OK is the statistically unbiased weighting of composite samples to generate an estimate. A disadvantage is the use of this technique on variable, skewed datasets. • Geological domains were based on the geological interpretation & mineralised trends. RC/DC intercepts modelled to be a minimum down hole width of 4m. 3DM wireframes created by sectional interpretation of the drilling dataset. Domain boundaries were treated as hard boundaries. • 2m down hole composites for all drilling were created and subdivided into each domain using an inside/outside principle. • The statistics for each domain were viewed and key univariate statistical indicators used to describe the nature of each. Each domain showed a positively skewed data distribution with high-grade outlier composites. High-grade outliers were top-cut to 20g/t Au for all domains by viewing grade distribution histograms, where the continuity of the higher-grades diminished.

Criteria	Commentary
	• Spatial continuity modelling was completed on the top-cut composite datasets for each domain. Directions of continuity were similar to interpreted controls on mineralization with varying degrees of anisotropy. • Sample search ellipses were set based on data spacing in similar orientations to the spatial continuity directions for each lode. Minimum and maximum samples were set for each sample search based on accepted levels of grade continuity. Search distances were based on sample spacing and spatial continuity. A total of 5 search passes were conducted with progressively relaxed search criteria to accommodate the data density for GC drilling to the widest spaced drilling at 80m x 80m. • Estimation completed using Surpac V6.4.1 mining software block modelling module. • Mining production data is available to be compared with the estimation result. A Multiple Indicator Kriged (MIK) check estimate (utilizing the same data & geological domains) was also completed to compare with the estimation result. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered material to this style of mineralization. • Block model dimensions were set to 329,000mE to 300,900mE and 6,620,200mN to 6,621,950mN and between 400mRL and -100mRL. Block sizes were chosen to compromise between sample spacing and orientation of mineralization i.e. 10m(X) by 5m(Y) by 5m(Z). • No selective mining units were assumed in this estimate. • No correlation between variables was necessary. • The 3DM/DTM wireframes for the estimation domains, regolith and topographical files were used to constrain the resource estimate. Blocks from the block model were coded based on these volumes/surfaces by either block centroid in/out of 3DM or above/below a DTM surface. • Statistical analysis indicated that outlier management was crucial to prevent high grade smearing that could result in overestimation of gold content (an adverse effect of using OK on a skewed dataset). Top-cutting & restricted sample search or the combination of both has been used to reduce this effect. This was defined by examining histograms, probability curves and the spatial locations of the outliers. • Model validation has been completed using visual and numerical methods and formal peer review sessions by key geology staff. • Mineral Resource Model has been validated visually against the input composite/raw drill hole data with spot checks carried out on a number of block estimates on sections and plans. • Easting swath plots have been generated to check composite assay mean values for block estimates within swath windows. OK estimates have also been checked against the alternate MIK estimate & historic production data. • A comparison of block volume weighted mean versus the drill hole cell de-clustered mean grade of the composited data was undertaken.

Criteria	Commentary
	Black Flag OC • Estimation was completed using two linear estimation techniques - Ordinary Kriging (OK) and Inverse Distance Squared (IDS). OK is an estimation method where a single direction of continuity is modelled for each domain for a global grade estimate. IDS is an estimation technique that weights a composite based on the distance from an estimation point, irrespective of spatial location. An advantage of OK is the statistically unbiased weighting of composite samples to generate an estimate. A disadvantage is the use of this technique on variable, skewed datasets leading to conditional bias when reporting the resource at increasing cut-off grades. • Geological domains were based on the geological interpretation and mineralised trends. Three Dimensional Model (3DM) wireframes were created by sectional interpretation of the drilling dataset. Where there was geological uncertainty, domain boundaries were modelled to a 0.3 g/t Au lower cut. Domain boundaries were treated as hard boundaries. • 2m down-hole composites for all drill holes were generated and subdivided into each domain using an inside 3DM/outside 3DM principle. • The statistics for each domain were viewed and key univariate statistical indicators used to describe the nature of each. Each domain showed a positively skewed data distribution with high-grade outlier composites. Top-cuts ranging from 5g/t Au to 15g/t Au were applied to both domains by viewing grade distribution histograms, where the continuity of the higher-grades diminished. • Sample search ellipses were set based on data spacing in similar orientation to the major mineralised orientation. Minimum and maximum samples were set for each sample search based on accepted levels of grade continuity. Search distances were based on sample spacing and spatial continuity. A total of 4 search passes were conducted with progressively relaxed search criteria to accommodate the data density from the closest to the widest spaced drilling. • Estimation was completed using Surpac V6.4 mining software, utilising the block modelling module. • A comparison of previous resource estimates showed that the differences between the resource estimates was due to the inclusion of the recent drilling data. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered material to this style of mineralisation. • Block sizes were chosen to compromise between sample spacing and orientation of mineralisation i.e. 5m(X) by 5m(Y) by 2.5m(Z). • The Selective Mining Unit (SMU) is based on current open pit mining fleet configuration. The SMU is comparable to the block size of the resource model. • No correlation between variables was necessary.

Criteria	Commentary
	• The 3DM/DTM wireframes for the estimation domains, regolith and topographical files were used to constrain the resource estimate. Blocks from the block model were coded based on these volumes/surfaces by either block centroid in/out of 3DM or above/below a DTM surface. • Model validation has been completed using visual and numerical methods and formal peer review sessions by key geology staff. • Mineral Resource Model has been validated visually against the input composite/raw drill hole data with spot checks carried out on a number of block estimates on sections and plans. Swath plots have been generated on section eastings to check input composited assay means for block estimates within swath windows.
	Black Flag UG
	• Estimation was completed using the linear estimation technique Inverse Distance Squared (IDS). IDS was selected due to the low number of composite samples for each domain to conduct a valid spatial continuity analysis. • Geological domains were based on the geological interpretation and mineralised trends. Three Dimensional Model (3DM) wireframes were created by sectional interpretation of the drilling dataset. Domain boundaries were treated as hard boundaries. • 2m down-hole composites for all drill holes were generated and subdivided into each domain using an inside 3DM/outside 3DM principle. • The statistics for each domain were viewed and key univariate statistical indicators used to describe the nature of each. Each domain showed a positively skewed data distribution with high-grade outlier composites. Top-cuts of 30g/t Au were applied to two of the five domains. No top-cut was applied to the other three domains. • Sample search criteria for estimating block grades were based on the geological interpretation of a planar, steep dipping structure for the mineralisation associated with the Black Flag Fault. Search distances were based on sample spacing and spatial continuity. Three search passes were used to estimate into the block model for each domain. Each search was progressively relaxed and reflects a lower confidence for the block grade estimate. • Estimation was completed using Surpac V6.4 mining software, utilising the block modelling module. • Comparison with the current and previous resource statements for Black Flag UG mineralisation shows that the two estimates do not compare. The current estimate has less tonnes for more grade and less ounces overall. The 2014 Black Flag resource update is considered to be more accurate than the 2007 update due to the significant increase in drilling data, mining activity and subsequent geological understanding of the mineralisation. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered material to this style of mineralisation.

Criteria	Commentary
	• Block sizes were chosen to compromise between sample spacing and orientation of mineralisation i.e. 1m(X) by 10m(Y) by 10m(Z) with sub-cells of 0.5m x 5m x 5m. • No correlation between variables was necessary. • The 3DM/DTM wireframes for the estimation domains, regolith and topographical files were used to constrain the resource estimate. Blocks from the block model were coded based on these volumes/surfaces by either block centroid in/out of 3DM or above/below a DTM surface. • Model validation has been completed using visual and numerical methods and formal peer review sessions by key geology staff. • The Mineral Resource Model has been validated visually against the input composite/raw drill hole data with spot checks carried out on a number of block estimates on sections and plans. Composite statistics were also compared to block statistics for each domain.
Moisture	• Tonnages are estimated on a dry basis.
Cut-off parameters	• Cut-off reporting grades are 0.7g/t Au for open–cut resources and 3.0g/t Au for underground. The Cut-off parameters are based on current NGF mining & milling costs.
Mining factors or assumptions	• The resources are likely to be mined utilising open pit mining methods. • The fresh portion of the resource is likely to be mined utilising narrow-vein underground mining methods (jumbo cut & fill for development long-hole stoping for production). • Mining methods are based on current open pit & underground mining operations used by NGF. • The mineral resource is based on an optimisation shell using current mining, appropriate processing costs, local geotechnical parameters at a gold price of A$2,000/oz.
Metallurgical factors or assumptions	• No assumption or factors have been applied to the resource estimate regarding the metallurgical amenability. • Reasonable assumptions for metallurgical extraction are based on processing ore through the Paddington & the (historic) Mt Pleasant processing plants. The both processing plants utilise a CIP extraction process. • The fresh rock component of the gold deposits hosted within the Victorious Basalt, which include Racetrack, Woolshed South, and Woolshed South Extended, are considered refractory deposits. Ore from these deposits would be processed using alternative processing methods. • Target gold recoveries for oxide and non-refractory fresh ores are expected to range from 92% to 96% recovery. This range of recovery is based on processing data from previous open pits within the Mt Pleasant gold camp. • Target gold recoveries for the fresh rock component of the refractory deposits are based on historic metallurgical test work & are expected to be 88% recovery.

Criteria	Commentary
Environmental factors or assumptions	- No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining & processing history of existing open pit & underground operations with the project area. - Refractory ore types have a high arsenic content & require further environmental test work to determine any environmental impact from waste & process residue disposal.
Bulk density	- Insitu-bulk densities (ISBD) applied to the resource estimate were based on systematic test work completed on hand specimens & DC for selected material types. The ISBD determination method is based on a water-immersion technique. The ISBD test work reconciles against production tonnages from historic & current mining operations within the project area. - Samples that were porous were sealed & accounted for in the bulk density calculation.
Classification	- The models & associated calculations utilised all available data & are depleted for known workings as of July 1 2014. - NGF follows the JORC classification system with individual block classification being assigned by statistical methods & visually taking into account the following factors: o Drill spacing & orientation; o Classification of surrounding blocks; o Confidence of certain parts of the geological model; and o Portions of the deposit likely to be viably mined. - The classification result reflects the view of the Competent Person.
Audits or reviews	- The Mineral Resource has not been externally audited. An internal Norton Gold Fields peer review has been completed as part of the resource classification process.
Discussion of relative accuracy/ confidence	- The Mineral Resources have been reported in accordance with the guidelines of the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources & Ore Reserves & reflects the relative accuracy of the Mineral Resources estimate. The Competent Person deems the process to be in line with industry standards for resource estimation & therefore within acceptable statistical error limits. - The statement relates to global estimates of tonnes & grade for likely separate open pit & underground mining scenarios. - Historic production data was used to compare with the resource estimate (where appropriate) & assisted in defining geological confidence & resource classification categories.

Section 4 Estimation and Reporting of Woolshed South Extended Ore Reserve

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves		• A Whittle optimization and pit design was carried out for Woolshed South Extended by NGF personnel in Dec 2014. The pit design parameter complies with safety parameters based on existing NGF's open pit procedures. The pit design comprises Probable Reserves of 304.2Kt at 1.61g/t at a cutoff grade of 0.7g/t for oxide and 0.74g/t for transitional. Fresh ore have been discounted at this stage as NGF currently have no means of processing refractory ore. • The Mineral Resources are reported inclusive of the Ore Reserves.
Site visits		• Woolshed South Extended area has been visited by Peter Ruzicka (GM Geology "NGF" & CP for Resources) and Guy Simpson (GM Technical Services "NGF" & CP for Reserves) within the last 6 months. • Additional exploration work is currently being undertaken by NGF in this area.

Study status		• NGF Technical Services Department created a pit design for the Woolshed South Extended mineral deposit based on Whittle Shell Revenue Factor 1 which is inclusive of a minimum mining width of 30m. The pit design was based on Whittle optimization using a selling price of $AUD1, 400/Oz with 2.5% Royalty.
		  • The block model used for both Whittle optimization and Pit design is "rt_jan_2015_x.mdl".
		  • Modifying factors such as mining loss, mining dilution and recoveries have been applied
		• Operating cost used was based on "NGF's small digger fleet cost model" with average processing cost of \$26.34/t.

Cut-off parameters		• A cutoff grade of 0.7g/t for oxide and 0.74g/t for transitional. • The cutoff grade applied is shown by; $\text{Cut} - \text{off Grade} = \frac{\text{Mining Dilution x Processing Cost}}{\text{Processing Recovery x (Selling Price} - \text{Selling Cost)}}$ • Selling price = AUD$1,400/Oz. • State Royalty = 2.5%. • Metallurgical recovery = 94% for oxide and 89% for transitional • Processing cost = \$26.34/t.

Mining factors or assumptions	• The method used to convert Mineral resource to Ore Reserves is based upon a pit optimization identifying the economic shell within which a practical mining design can be applied to. • The mining method will be based on conventional open pit mining with diesel trucks and shovels. For Woolshed South Extended, "NGF's small digger fleet model" will be used to optimize the reserve. • As NGF is an owner operator Woolshed South Extended's operating model will be based on the pit being mined by NGF. • The Ore reserve estimate was created using DCF methodology within "Whittle" open pit optimization software in order to select the most appropriate and economically viable pit shell taking into account minimum mining width for the chosen equipment fleet. • Geotechnical slope design parameters were applied based on geotechnical domains/zones within the mining model. • An overall minimum mining width of 30m was applied. • An ore loss allowance of 5% and a mining dilution of 10% are anticipated with this type of operation based upon historical data in similar scale and type of operation • No inferred and or unclassified material has been included in the reserves. • Gold Price used = $AUD1, 400/Oz. • Processing cost = $26.34/t. • Infrastructure requirement for open pit mining includes; A workshop for all mobile equipment for maintenance requirements, offices, crib rooms and amenities, explosives storage, water dams and communication. Most of these infrastructures have to be erected on site before mining can commence.
Metallurgical factors or assumptions	• Metallurgical test work for fresh ore will be undertaken by NGF on Woolshed South Extended in 2015. • Ore from Woolshed South Extended will be delivered via road trains to NGF's Paddington mill for processing. • Paddington Mill is based on conventional carbon in pulp technology and has achieved an annual throughput of 3.72 million tonnes in 2014. The average feed grade and recovery is 1.67g/t and 88.88% respectively. • A recovery factor of 94% for oxide and 89% for transitional have been applied to Woolshed South Extended's oxide and transitional rock types as the ore will be blended with Paddington's other ore sources to be able to achieve this recovery factor.
Environmental	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. • All proposed operation and operational plans are within local historical practices and existing operational standards.
Infrastructure	• The site is considered a greenfield site thus before mining can commence infrastructure including electricity, water, offices, core facility, crib rooms, explosives storage, water dams and communications have to be in place.
Costs	• Woolshed South Extended's reserve estimate was based on a gold price of $AUD 1,400/Oz. • Allowance has been made for the 2.5% state government royalty. • Operating cost used was based on "NGF's small digger fleet cost model" with average processing cost of $26.34/t.

	• No penalties assumed and no deleterious elements in concentrate.
Revenue factors	• Financial analysis in this report is based on a gold price of $AUD 1,400/Oz. • The gold Dore is planned to be transported via recognized security service from gold room of Paddington processing plant to the gold refinery in Perth. • Contract payments and terms are expected to be typical of similar contracts for the refining and sale of Dore produced from other operations within Australia. • Allowance has been made for the 2.5% state government royalty.
Market assessment	• Historical gold price and forward looking estimates have been used for the gold price. Price flexing and sensitivity analysis have been carried out to determine the robustness of the project viability. • The cash flow was modelled in real terms and no price or cost escalations were applied.
Economic	• Inputs to economic analysis include factors described above including ore and metal quantities from mining/processing schedule (including described recovery/processing parameters), cost and price assumptions.
Social	• The majority of workforce will be sourced locally. • NGF will establish all relevant agreement with local stakeholders and government agencies.
Other	• Woolshed South Extended is an existing pit thus an updated Mine Management Plan will need to be submitted with the Western Australian Department of Mines pre-commencement of mining activity. There is no reason to suggest approvals and authorizations will not be granted.
Classification	• The Ore Reserve was classified as Probable in accordance with the JORC Code, corresponding to the resource classifications of Measured and Indicated. No Inferred Mineral Resources were included in the Ore Reserve estimate. • The estimated Ore Reserves and mining method are in the opinion of the Competent Person appropriate for this style of deposit.
Audits or reviews	• The resource and reserve was calculated by NGF personnel. The cost and mining parameters were reviewed internally against existing operations and consideration was made for current practice and cost structure. • It is not expected that practices assumed in the calculation of reserve will vary before the next annual reserve calculation.
Discussion of relative accuracy/ confidence	• All mining estimates are based on Australian costs, and relevant historical cost data. • The local estimate of Ore reserves available for technical and economic evaluation is 304.2Kt at 1.61g/t at a cutoff grade of 0.7g/t for oxide and 0.74g/t for transitional prior to processing. • There are no unforeseen modifying factors at the time of this statement that will have any material impact on the Ore Reserve estimate.

Appendix 1: Table of exploration results – RC & RC_DD Recent Drilling for Racetrack Deposit

Hole_ID	MGA_ East	MGA_ North	RL	Dip	Azi	Depth	From (m)	To (m)	DH Width(m)	Grade g/t Au
PMPD0085	330912.2	6618349.6	348.1	-55	146	254.5	52.9	53.3	0.4	2.88
							67.0	72.0	5.0	5.68
							75.5	75.9	0.4	1.38
							114.5	115.3	0.8	9.02
							188.0	194.2	6.2	6.15
							233.7	234.2	0.5	5.62
PMPD0087	330935.3	6618357.5	348.0	-55	146	240	50.0	52.0	2.0	4.95
							58.0	62.0	4.0	0.54
							68.0	70.0	2.0	1.57
							116.8	117.5	0.7	3.56
							159.0	160.0	1.0	6.22
							182.4	182.7	0.3	20.1
							185.0	196.0	11.0	6.12
PMPD0091	331202.8	6618414.4	347.1	-90	0	186.2	118.0	118.44	0.44	14.6
							138.47	140.0	1.53	2.97
							173.69	177.0	3.31	1.09
PMPD0092	331216.4	6618465.8	349.2	-70	146	168.1	81.1	82.0	0.9	1.17
							127.3	128.15	0.85	1.70
							131.57	138.33	6.76	7.84
PMPD0096	331005.4	6618431.5	349.2	-55	146	279.5				assays pending
PMPD0097	330986.1	6618421.1	349.4	-60	146	309.4				assays pending
PMPD0098	330914.1	6618455.0	349.7	-60	234.2	102	117.6	118.0	0.4	3.70
							167.5	167.8	0.3	3.23
							272.0	273.0	1.0	1.38
							285.0	285.7	0.7	2.24
PMPD0099	331400.4	6618626.4	367.6	-55	146	206.8				assays pending
PMPD0100	331386.1	6618608.8	367.1	-70	146	237.3	97.0	98.0	1.0	1.01
							114.0	115.0	1.0	0.83
							117.1	117.4	0.3	11.1
							154.7	155.3	0.6	3.81
							159.55	160.0	0.45	11.4
PMPD0101	331386.8	6618607.9	367.1	-55	146	229.5	82.85	84.0	1.15	2.25
							86.5	87.65	1.15	5.55
							104.0	104.5	0.5	6.68
							184.9	185.9	1.0	2.05
							214.0	215.0	1.0	0.91
PMPD0102	331364.0	6618605.2	367.1	-70	146	228.3	108.0	109.0	1.0	1.01
							116.0	119.85	3.85	2.56
							124.1	132.0	7.9	9.65
							147.0	148.0	1.0	1.24
							159.15	159.7	0.55	2.33
							161.75	162.05	0.3	5.16
							164.45	165.05	0.6	19.7
							223.9	224.2	0.3	7.80
PMPD0103	331364.7	6618604.3	367.1	-55	146	225.1	78.25	78.8	0.55	2.14
							96.65	97.3	0.65	3.57
							99.75	100.2	0.45	2.92
							109.45	113.0	3.55	8.45
							161.75	162.1	0.35	0.88
							194.75	195.2	0.45	1.60
							210.0	211.0	1.0	3.61

Hole_ID	MGA_ East	MGA_ North	RL	Dip	Azi	Depth	From (m)	To (m)	DH Width(m)	Grade g/t Au
PMPD0106	331347.8	6618581.7	359.1	-70	140	278.7	111.0	111.3	0.3	3.48
							133.6	133.9	0.3	3.77
							146.45	148.0	1.55	2.76
							151.0	153.35	2.35	9.87
							203.0	204.0	1.0	2.18
							240.0	241.0	1.0	2.01
PMPD0107	331348.4	6618580.8	359.1	-55	140	285.1	54.4	55.0	0.6	0.94
							90.6	91.2	0.6	3.04
							104.0	105.0	1.0	1.17
							127.1	127.4	0.3	5.33
							136.2	136.5	0.3	6.92
							149.1	151.45	2.35	14.2
							193.2	194.75	1.55	1.81
							208.2	208.6	0.4	1.73
PMPD0108	331333.9	6618576.4	358.5	-55	146	102.4	____	____	____	NSR
PMPD0109	331306.6	6618585.0	358.4	-60	146	192.3	158.3	161.0	2.7	6.17
							187.0	187.45	0.45	1.88
PMPD0110	331347.3	6618630.4	367.6	-74	146	237.3	95.0	96.0	1.0	1.35
							144.5	145.0	0.5	0.95
							163.0	168.0	5.0	9.97
							171.0	172.0	1.0	1.29
							184.0	188.0	4.0	7.53
PMPD0111	330783.2	6618284.6	347.6	220	155	-46	59.0	60.0	1.0	1.16
							73.0	74.0	1.0	1.03
							87.0	89.0	2.0	3.07
PMPD0111 A	330783.0	6618285.9	347.7	-55	146	353.4				assays pending
PMPD0112	330781.4	6618283.8	347.6	-54	156	318	85.3	88.6	3.3	1.10
							94.3	95.2	0.9	1.65
							134.0	135.0	1.0	1.31
							139.25	140.0	0.75	6.75
							162.0	163.0	1.0	2.09
							170.0	171.5	1.5	1.19
							174.0	174.8	0.8	0.88
							178.5	183.0	4.5	2.48
							187.0	188.0	1.0	1.13
							228.9	229.25	0.35	1.18
PMPD0113	331476.8	6618620.1	356.1	-60	146	225.3				assays pending
PMPD0114	331533.7	6618573.2	349.3	-90	146	189.3				assays pending
PMPD0115	331205.9	6618387.5	346.1	-63.5	183	146.8				assays pending
PMPD0116	331208.4	6618389.4	346.1	-46.5	170	175.7				assays pending
Analysis by 30g Fire Assay Results compiled by using a 0.8 g/t cut-off grade, no top-cut grade Maximum of 2m internal dilution , minimum interval of 0.3 m										

Appendix 2: Table of exploration results – Recent RC Drilling for Racetrack West Deposit

Hole_ID	MGA_East	MGA_North	RL	Dip	Azi	Depth	From (m)	To (m)	DH Width(m)	Grade g/t Au
PMPC1326	329952.1	6617964.7	347.9	-60	150	138	80	82	2	2.69
PMPC1327	330100.7	6617829.8	347.3	-70	150	90	37	39	2	1.57
PMPC1328	330056.3	6617866.6	347.5	-70	150	78	45	46	1	3.46
PMPC1331	330106.1	6618362.5	347.8	-60	90	90	20	22	2	4.34
							31	32	1	4.65
							51	52	1	1.35
							82	83	1	3.90
PMPC1332	330119.2	6618376.8	347.7	-60	90	96	24	25	1	1.53
							32	33	1	1.73
							40	43	3	1.01
							51	52	1	1.07
							58	61	3	3.05
							71	72	1	0.97
PMPC1333	330137.1	6618396.4	347.8	-60	90	96	20	21	1	2.64
							38	39	1	1.04
							66	67	1	0.80
PMPC1334	330097.5	6618397.5	347.6	-60	90	102	23	24	1	2.23
							81	83	2	2.27
PMPC1335	330113.4	6618416.8	347.9	-60	90	90	15	23	8	1.47
							51	52	1	1.33
							83	84	1	1.73
PMPC1336	330118.5	6618436.9	347.9	-60	90	90	20	21	1	1.65
PMPC1337	330165.8	6617996.1	347.4	-70	150	72	49	50	1	1.13
PMPC1338	330083.5	6617819.6	347.4	-70	150	60	44	45	1	5.03
							57	58	1	5.57
PMPC1339	330048.3	6617880.8	347.5	-70	150	60	42	47	5	2.44
PMPC1340	330027.5	6617916.3	347.6	-70	150	60	44	46	2	1.59
PMPC1341	330007.8	6617950.8	347.7	-70	150	72	59	60	1	2.09
PMPC1342	329975.2	6618003.7	347.8	-60	150	114	59	60	1	3.59
							63	67	4	6.00
							76	78	2	3.53
PMPC1343	330101.8	6617866.5	347.4	-70	150	54	38	39	1	5.00
PMPC1344	330054.8	6617949.3	347.7	-70	150	66	42	43	1	2.12
PMPC1345	330079.3	6617946.0	347.5	-70	150	84	42	50	8	2.19
PMPC1346	330176.9	6617898.5	347.2	-70	150	60	____	____	____	NSR
PMPC1347	330157.0	6617932.7	347.3	-70	150	60	46	47	1	1.77
PMPC1348	330215.2	6617910.1	347.2	-70	150	66	29	32	3	1.14
PMPC1349	330196.2	6617944.5	347.4	-70	150	60	____	____	____	NSR
PMPC1350	330213.5	6617954.6	347.3	-70	150	60	____	____	____	NSR
PMPC1351	330193.3	6617989.5	347.5	-70	150	66	53	55	2	2.96
PMPC1352	330027.2	6617833.8	347.6	-70	150	66	56	58	2	2.75
PMPC1353	329982.9	6617914.0	347.8	-70	150	96	66	67	1	2.48
PMPC1354	329918.4	6617944.8	348.1	-60	150	84	____	____	____	NSR
PMPC1355	330194.9	6618146.3	347.5	-60	150	120	106	107	1	0.86
PMPC1356	330172.6	6618105.2	347.6	-60	150	84	____	____	____	NSR
PMPC1357	330160.2	6618127.1	347.5	-60	150	120	73	74	1	1.26
							77	79	2	2.42
PMPC1358	330155.1	6618096.3	347.6	-60	150	90	43	44	1	1.87
							73	74	1	1.33
PMPC1359	330139.5	6618122.3	347.7	-60	150	138	80	83	3	2.31
							106	110	4	1.08
							120	121	1	0.80
PMPC1360	330056.6	6618031.3	347.7	-60	150	102	44	45	1	4.27
							76	77	1	5.52

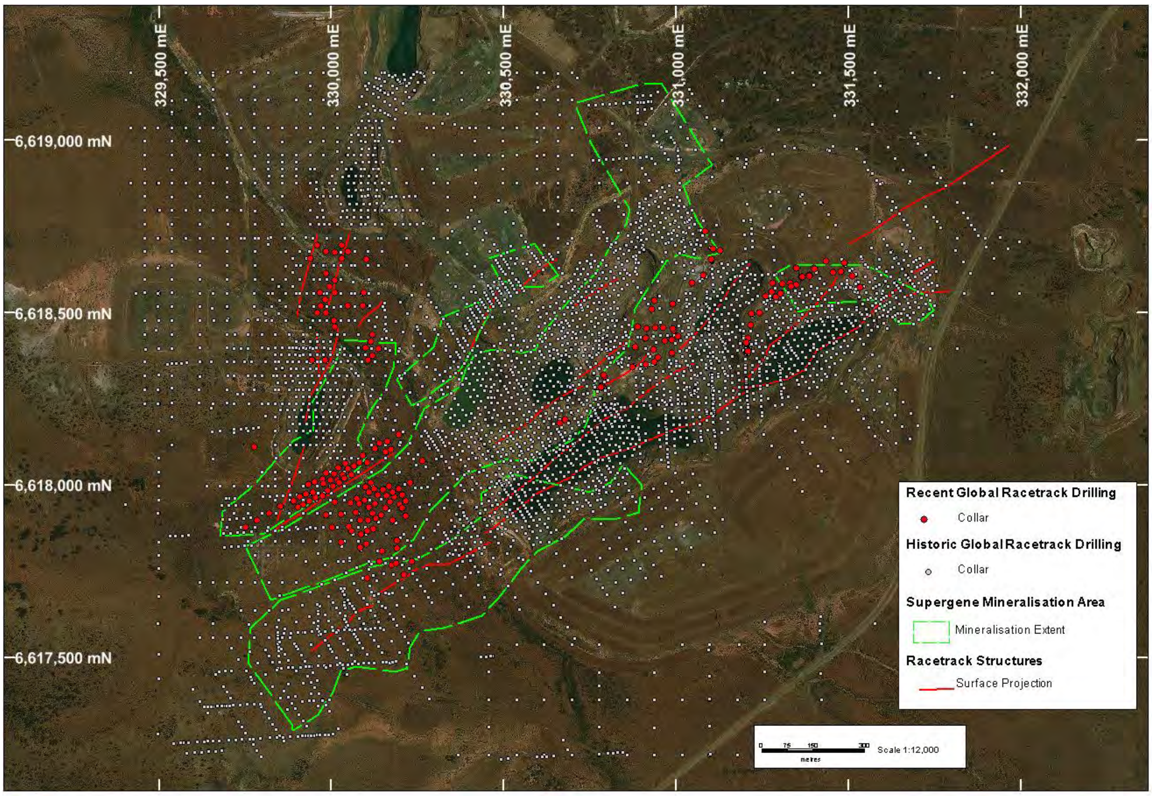
Hole_ID	MGA_East	MGA_North	RL	Dip	Azi	Depth	From (m)	To (m)	DH Width(m)	Grade g/t Au
PMPC1361	330047.5	6618047.5	347.6	-60	150	120	88	94	6	7.41
							110	120	10	1.35
PMPC1362	330038.7	6618062.8	347.7	-60	150	150	114	116	2	7.08
PMPC1363	330031.0	6618030.6	347.7	-60	150	120	41	42	1	1.05
							60	61	1	1.21
							75	76	1	1.20
							94	95	1	0.90
PMPC1364	330018.9	6618051.6	347.7	-60	150	156	115	119	4	2.39
PMPC1365	330017.0	6618014.2	347.8	-60	150	108	55	56	1	1.26
							65	66	1	1.53
							91	92	1	0.93
PMPC1366	330006.5	6618033.2	347.8	-60	150	150	75	76	1	4.48
PMPC1367	329945.1	6617980.4	348.1	-60	150	126.5	91	93	2	3.31
							109	112	3	2.01
							117	118	1	0.83
PMPC1368	329931.6	6618002.8	348.2	-60	150	162	98	103	5	4.57
							113	117	4	1.95
							151	159	8	5.59
PMPC1369	329924.0	6617975.6	348.2	-60	150	120	80	89	9	10.56
PMPC1370	330124.7	6618106.8	347.6	-60	150	120	65	80	15	6.91
							83	85	2	1.19
							94	95	1	0.86
							113	115	2	0.95
PMPC1371	330090.7	6618087.0	347.7	-60	150	120	36	39	3	1.26
PMPC1372	329982.4	6618034.8	347.9	-60	150	180	178	179	1	0.80
PMPC1373	330004.1	6617996.7	347.9	-60	150	102	75	79	4	2.60
							84	85	1	1.19
PMPC1374	329973.6	6617968.9	347.9	-60	150	90	71	75	4	3.54
PMPC1375	329901.3	6617935.3	348.4	-60	150	84	____	____	____	NSR
PMPC1376	329889.9	6617955.1	348.3	-60	150	120	62	68	6	2.53
							71	72	1	1.48
PMPC1377	329851.5	6617939.3	348.5	-60	150	136	____	____	____	NSR
PMPC1378	329817.2	6617919.4	348.8	-60	150	136	44	45	1	1.02
							63	67	4	2.48
							75	77	2	1.37
							80	81	1	0.85
PMPC1379	329783.6	6617898.8	349.0	-60	150	136	58	59	1	3.06
							121	122	1	0.86
PMPC1380	330007.3	6618477.2	348.0	-60	90	138	5	6	1	1.46
							67	68	1	6.59
							91	92	1	3.90
							104	105	1	3.16
PMPC1381	329959.0	6618501.2	348.3	-60	90	66	55	57	2	5.20
PMPC1382	329983.2	6618501.1	348.1	-60	90	60	33	34	1	0.91
PMPC1383	330007.8	6618458.7	347.8	-60	90	120	7	12	5	1.23
							25	26	1	2.27
							58	59	1	1.44
							62	64	2	3.29
							78	79	1	1.53
PMPC1384	329967.9	6618519.7	347.7	-60	90	60	42	43	1	6.45
PMPC1385	329980.2	6618362.5	348.1	-60	90	78	13	14	1	1.03
							39	42	3	1.02
							47	54	7	2.96
PMPC1386	329942.3	6618363.0	348.1	-60	90	150	65	85	20	2.86
							98	99	1	1.09
							106	138	32	3.83
PMPC1387	330089.1	6618520.2	347.7	-60	90	90	32	33	1	3.05
							52	53	1	1.53

Hole_ID	MGA_East	MGA_North	RL	Dip	Azi	Depth	From (m)	To (m)	DH Width(m)	Grade g/t Au
							58	59	1	1.25
							72	76	4	2.93
							86	87	1	27.60
PMPC1388	330047.2	6618519.9	347.7	-60	90	120	18	20	2	6.33
							83	84	1	1.67
							104	105	1	0.86
							108	111	3	2.00
PMPC1389	329980.4	6618538.7	348.2	-60	90	60	32	37	5	1.42
PMPC1390	330092.0	6618558.2	348.2	-60	90	120	29	30	1	3.43
							110	111	1	0.84
PMPC1391	330008.0	6618557.7	348.2	-60	90	66	39	41	2	1.44
							57	63	6	1.89
PMPC1392	329966.9	6618558.4	348.2	-60	90	78	19	20	1	0.90
							39	40	1	2.58
							46	55	9	6.64
PMPC1393	329994.2	6618576.2	348.2	-60	90	60	14	21	7	8.61
							24	25	1	0.80
							45	46	1	0.81
PMPC1394	330008.5	6618594.6	348.3	-60	90	60	39	40	1	2.64
PMPC1395	329982.5	6618613.9	348.4	-60	90	72	41	45	4	1.23
PMPC1396	329938.0	6618657.2	348.6	-60	90	145	101	102	1	2.86
							105	108	3	1.89
							131	132	1	2.13
PMPC1397	330101.2	6618656.7	348.3	-60	90	72	____	____	____	NSR
PMPC1398	330047.7	6618677.1	348.3	-60	90	78	54	55	1	3.58
PMPC1399	330029.3	6618656.9	348.5	-60	90	84	68	69	1	0.85
PMPC1400	330008.4	6618676.6	348.5	-60	90	84	16	27	11	1.47
							57	58	1	0.85
							69	71	2	2.21
PMPC1401	329983.3	6618677.2	348.5	-75	90	138	23	25	2	1.42
							108	109	1	2.02
PMPC1402	329957.8	6618696.7	348.5	-60	90	138	33	34	1	1.48
							49	51	2	1.24
							91	92	1	0.93
							108	111	3	2.17
							121	122	1	1.07
PMPC1403	330029.0	6618696.4	348.5	-60	90	78	36	40	4	0.81
							66	70	4	1.96
PMPC1404	330102.4	6618065.2	347.6	-60	150	96	66	70	4	10.98
PMPC1405	330080.1	6618065.8	347.5	-60	150	102	____	____	____	NSR
PMPC1406	330064.8	6618056.7	347.6	-60	150	114	____	____	____	NSR
PMPC1407	329995.5	6618016.3	347.8	-60	150	120	____	____	____	NSR
PMPC1408	329973.0	6618017.0	347.8	-60	150	150	51	53	2	2.20
PMPC1409	329951.2	6618008.8	348.0	-60	150	156	60	62	2	2.45
							69	71	2	6.02
							83	92	9	6.93
PMPC1410	329935.8	6617955.0	348.1	-60	150	102	89	92	3	1.96
PMPC1411	329906.9	6617965.5	348.1	-60	150	120	72	74	2	14.13
PMPC1412	329749.0	6617879.0	349.1	-60	150	138	66	67	1	1.05
PMPC1413	330228.5	6618008.3	347.5	-70	150	66	____	____	____	NSR
PMPC1414	330169.5	6617950.4	347.3	-70	150	72	35	36	1	4.11
PMPC1415	330159.3	6617968.6	347.3	-70	150	78	44	45	1	3.90
PMPC1416	330148.9	6617986.0	347.4	-70	150	72	26	27	1	1.35
							42	44	2	27.07
PMPC1417	330133.9	6617971.8	347.4	-70	150	72	39	41	2	4.02
PMPC1418	330114.2	6618006.7	347.5	-70	150	72	31	32	1	1.69
							45	46	1	0.82
PMPC1419	330144.5	6617912.5	347.2	-70	150	60	46	47	1	3.72

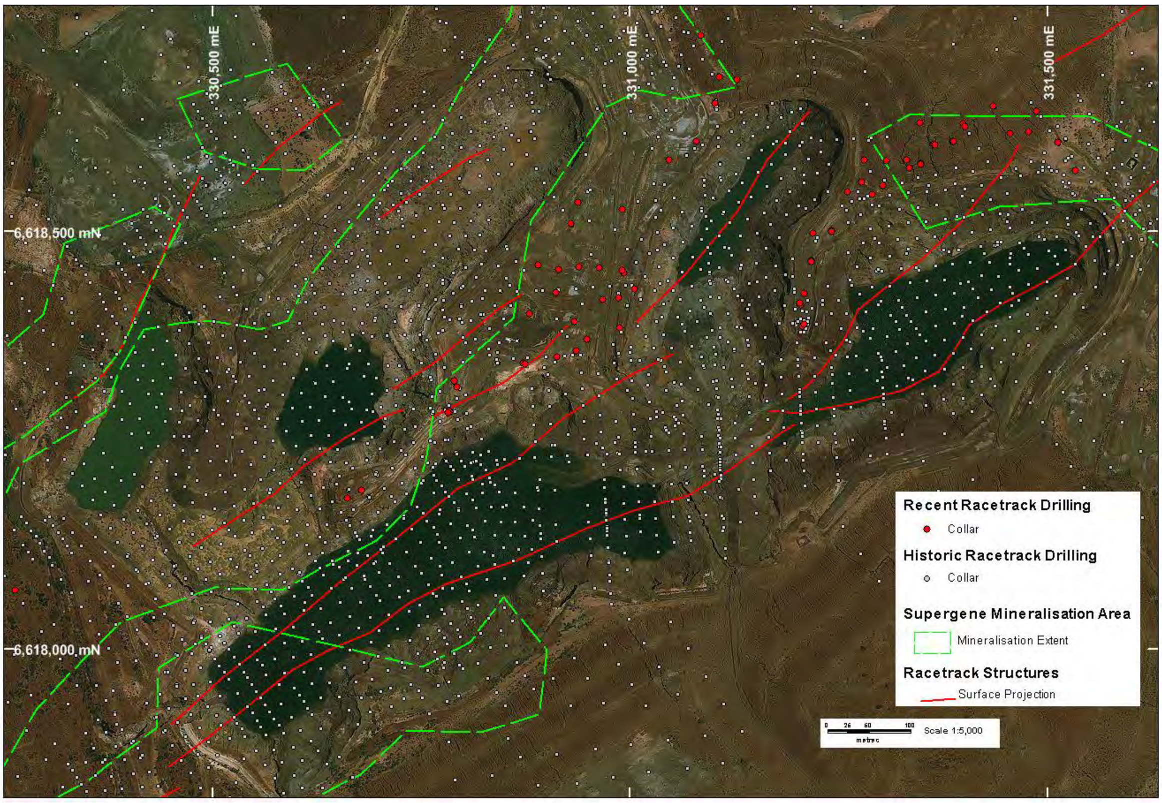
Hole_ID	MGA_East	MGA_North	RL	Dip	Azi	Depth	From (m)	To (m)	DH Width(m)	Grade g/t Au
							59	60	1	2.84
PMPC1420	330125.2	6617947.6	347.3	-70	150	66	41	42	1	10.50
PMPC1421	330106.9	6617979.2	347.4	-70	150	72	53	58	5	1.49
PMPC1422	330097.9	6617994.5	347.6	-70	150	84	37	38	1	1.30
PMPC1423	330127.3	6617902.5	347.3	-70	150	60	42	43	1	6.44
							52	53	1	5.77
PMPC1424	330118.1	6617918.3	347.3	-70	150	78	43	44	1	5.80
PMPC1425	330107.6	6617937.3	347.4	-70	150	78	42	44	2	6.08
PMPC1426	330071.3	6617960.6	347.4	-70	150	78	____	____	____	NSR
PMPC1427	330120.4	6617873.9	347.3	-70	150	60	34	37	3	2.36
PMPC1428	330106.5	6617898.3	347.4	-70	150	66	40	41	1	0.81
PMPC1429	330083.4	6617898.3	347.5	-70	150	54	40	41	1	0.84
PMPC1430	330084.4	6617858.0	347.4	-70	150	60	41	42	1	5.39

Analysis by 30g Fire Assay
Results compiled by using a 0.8 g/t cut-off grade, no top-cut grade
Maximum of 2m internal dilution , minimum interval of 1.0 m

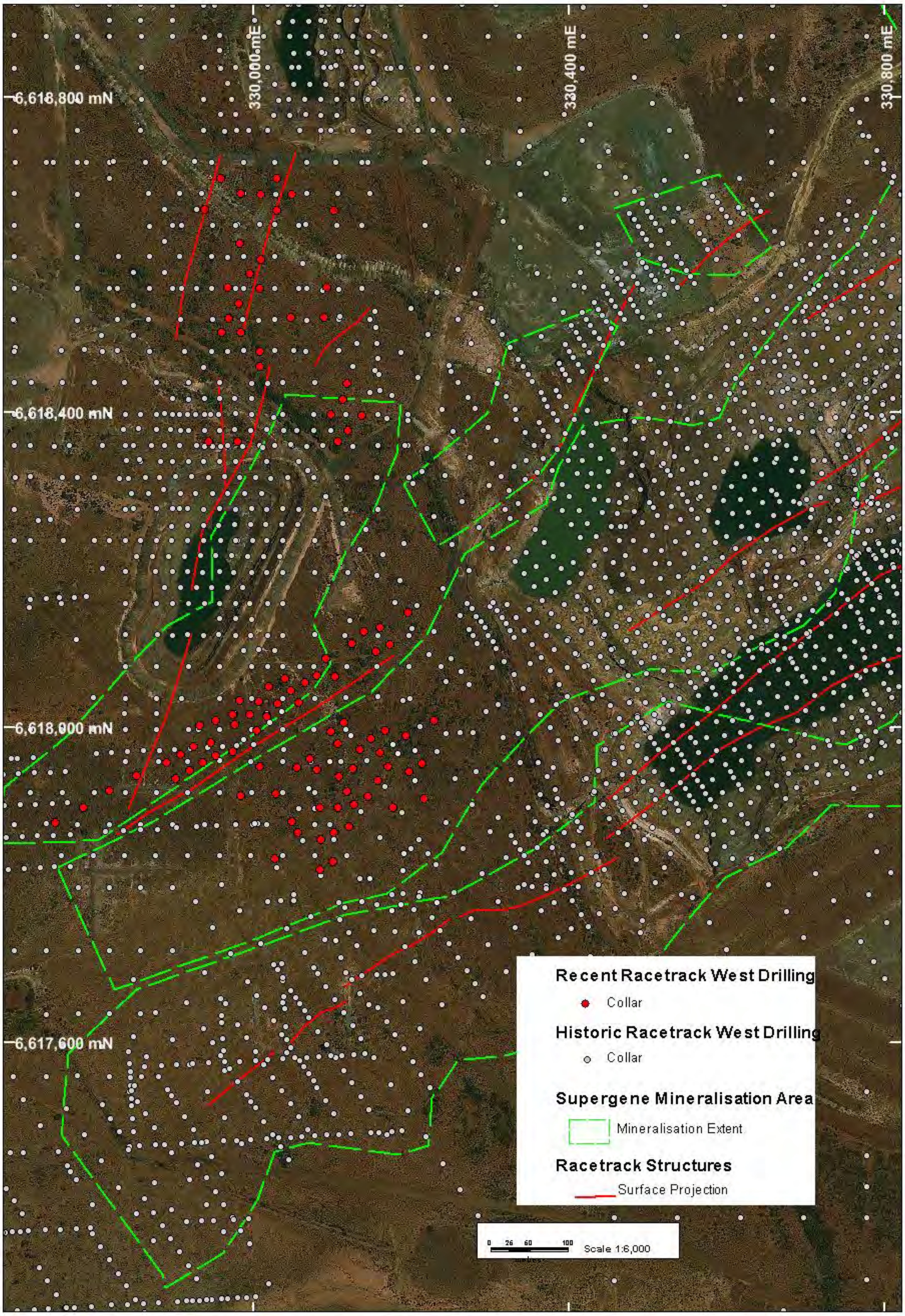
Appendix 3: A map showing the collar locations of the recent RC & RC_DD drilling at Global Racetrack



Appendix 4: A map showing the collar locations of the recent RC & RC_DD drilling at Racetrack



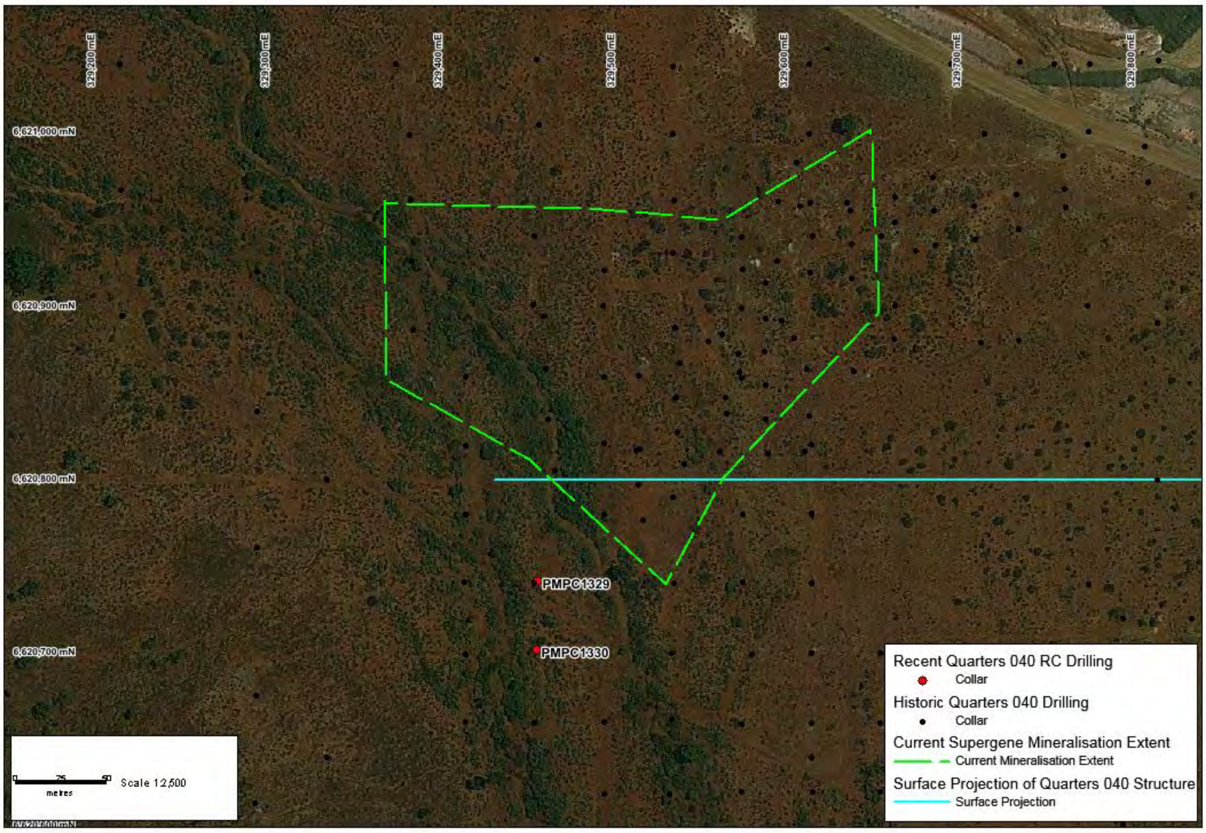
Appendix 5: A map showing the collar locations of the recent RC drilling at Racetrack West



Appendix 6: Table of exploration results – Recent Drilling (RC) for Quarters 040 Deposit

Hole_ID	MGA_East	MGA_North	RL	Dip	Azi	Depth	From (m)	To (m)	DH Width(m)	Grade g/t Au
PMPC1329	329,458.9	6,620,738.7	351.9	-55	000	234	186	187	1	1.80
PMPC1330	329,458.4	6,620,699.0	351.7	-55	000	240	____	____	____	NSR
Analysis by 30g Fire Assay Results compiled by using a 0.8 g/t cut-off grade, no top-cut grade Maximum of 2m internal dilution , minimum interval of 1.0 m										

Appendix 7: A map showing the collar locations of the recent RC drilling at Quarters 040



JORC Code, 2012 Edition – Table 1 Homestead Underground and Tuart Underground

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	Commentary
Sampling techniques –Homestead	• Sampling completed utilising a combination of Diamond Core holes (DC), Face Sampling (FS) and Reverse Circulation (RC) holes. The drill hole locations were designed and holes oriented to allow for spatial spread of samples across mineralised zones and different rock types. Face sampling was performed on each face from development drives that showed possibility of mineralisation. • Diamond core samples were placed into core trays at the rig and transferred to NGF's core processing facility for logging and sampling. Prior to drilling the drill hole locations were marked by survey department using a Leica Total Station, Model TS15. After drilling, drill hole collar positions were re-surveyed. All drill holes are down hole surveyed. Historic holes by Maxibor or by Down Hole Electronic Multishot (DEMS) camera, recent (post 2001) by combination of Electronic Single and Multi Shot cameras.
Sampling techniques –Tuart UG	• Sampling completed utilising a combination of Reverse Circulation and Diamond Core holes on 20m x 20m to 80m x 80m grid spacing. Drilling and sampling has been conducted by various companies since 1995 and includes exploration, resource development and grade control (GC) sampling (UG and open pit RC GC). Sampling techniques are a summary of drilling and sampling manuals/reports from Centaur Mining and Exploration, Aurion Gold, Placer Dome Asia Pacific, Barrick and Norton Gold Fields. • The drill hole locations were designed and oriented to allow for spatial spread of samples across mineralised zones and different rock types. • Field based observations from geological supervision and geological records referring to sample quality, moisture content and recovery were used as a guide to sample representivity. • All RC-recovered samples were passed through a splitting device (cone or riffle splitter) at 1m intervals to obtain a sample for assay, collected in an appropriately-sized calico bag. Target RC calico sample weights range from 2.5 to 4kg across all RC drilling campaigns (1995-2013). Bulk reject sample was also collected into a plastic bag for each metre. Spear samples, composited to 4m or less, were collected from the bulk samples as a first-pass sampling technique. Single metre samples were collected and submitted for assay from areas of expected mineralisation or composite anomalism. • DC samples were placed into core tray at the rigs and transferred to core processing facilities for logging and sampling. The DC samples are collected at nominated intervals by a Geologist from resultant half core with a min. interval of 0.2m and a max. of 1m.

Criteria	Commentary
	• Samples were submitted to a commercial laboratory for assay. Sample preparation, summarised for all drilling campaigns (1995-2013), included all or part of: oven dry between 85°C and 105°C, jaw-crushing (nominal 10mm) and splitting to 3.5kg as required, pulverize sample to >85% passing 75um, from which a 30g (current) or 50g (historic) fire assay charge was analysed by Atomic Absorption Spectrometry (AAS) finish.
Drilling techniques – Homestead	• The dataset used for the Homestead resource estimate is a combination of historic data dating back to the 1980's which includes RC and surface DC holes; and new data consisting mostly of underground collared DC holes and FC samples from the development levels. • Historic holes are being progressively excluded from a dataset used for resource estimation. As new data are acquired, some of the old intercepts which do not agree with the more accurately located samples from the shorter holes or with the face data are removed. Review of the database has also identified a number of drill holes which are of doubtful reliability due to their orientation (along strike or down dip of the ore zones) and these were also excluded from the dataset. • In the latest estimates 8 RC holes were used (less than 0.5%), 584 DC holes (23%) and 1,959 face sampling strings (77%). • In the DC dataset 33 holes (6% of all DC) are legacy data drilled by Centaur Mining and Exploration Ltd • The RC diameter used is un-known. The DC is in 98% NQ (47.6mm diameter core sizes) or LTK60 (44.0mm diameter core sizes) with some BQ (36.4mm diameter core sizes). • Selected DC were oriented using electronic orientation tool BQTK ACT 11.
Drilling techniques – Tuart UG	• All assays referred to for resource estimation (1995-2013) were collected from either RC or DC drilling using a drilling contractor. The most recent drilling campaign accounts for 5% of the total drilling dataset. • RC sampling completed using a 5.25" or 5.5" diameter drill bit with a 5" bottom face sampling hammer. RC drilling rigs were equipped with a booster compressor. DC sampling is a combination of HQ (63.5mm diameter) and/or NQ (50.5mm diameter) core sizes. DC is orientated utilising either a bottom of hole spear, EZI-Mark or ACE system.
Drill sample recovery – Homestead	• DC contractors use a core barrel and wire line unit to recover the DC core, adjusting drilling methods and rates to minimize core loss (e.g. changing rock type, broken ground conditions etc.) as advised by supervising geologist. . • Core recovery was recorded and was on average 99.4%.
Drill sample recovery – Tuart UG	• RC Drillers advised by geologists on the ground conditions expected for each hole and instructed to adopt an RC drilling strategy to maximize sample recovery, minimize contamination and maintain required spatial position. • All RC 1m samples are collected into a UV resistant bag. Samples are visually logged for moisture content, estimated sample recovery and contamination. The DC samples are orientated, length measured and compared to core blocks denoting drilling depths by the

Criteria	Commentary
	drilling contractor. Any recovery issues are recorded. Sample loss or gain is reviewed at the time of drilling and feedback is provided to the drilling contractor to ensure the samples are representative. All samples sent to the laboratory are weighed and monitored to ensure that they are representative. • DC contractors use a core barrel and wire line unit to recover the DC, adjusting drilling methods and rates to minimize core loss (e.g. changing rock type, broken ground conditions etc.). • A study of the weights of the 1m RC sample splits and gold grades (2012-2013 drilling) show no correlation between the two. The drilling contractors utilized drilling techniques to ensure minimal loss of any size fraction.
Logging – Homestead	• All DC data was geologically logged using codes set up for direct computer input. Hole ID, interval, rock type, stratigraphy, grainsize, weathering, colour, alteration style type and intensity, structure, mineralisation style type and percentage were recorded. • Geological logging was qualitative and quantitative in nature. • All DC was photographed after logging (and before cutting) using a digital camera. • Every attempt was made to ensure consistency of logging despite the number of geologists involved. Validation was applied at the database level to ensure only logging codes matching reference tables can be entered to database. • Geotechnical information was collected from underground DC over the whole length of the drill hole. From the underground grade control DC only RQD measurements were recorded. From the resource definition DC data relating to Modified Rock Tunnelling Quality Index, Q' was recorded. Q’ data (and its precursor, Q) is an important tool in the stability analysis of underground excavations. It is used to determine factors of safety in stope and pillar design. Information collected from these holes includes RQD, number of joints (Jn), number of fractures, joint roughness and infill type and thickness. • Dedicated DC undergo specific geotechnical investigation to aid in structural interpretation and to determine rock mass characterization.
Logging – Tuart UG	• All current RC samples are geologically logged at 1 metre intervals, which is an appropriate level of detail to support Mineral Resource estimation. In some of historic RC holes samples were selectively logged. Currently, each interval is inspected and the following parameters are recorded: weathering, regolith, rock type, alteration, mineralisation and structure. All drill core is logged for core loss, marked into 1m intervals, orientated, structurally logged, geotechnically logged and geologically logged for the following parameters: weathering, regolith, rock type, alteration, and mineralisation. • Geological logging is qualitative and quantitative in nature. • The entire length of RC holes are logged on a 1m interval basis (i.e. 100% of the drilling is logged). Where no sample is returned due to voids or lost sample, it is logged and recorded as such. DC is logged over its entire length and any core loss or voids are recorded.

Criteria	Commentary
Sub-sampling techniques and sample preparation – Homestead	• In both surface and underground DC, sampling intervals were determined by geological logging. All sampling was performed at nominal 1m intervals with a minimum sample length of 0.3 metres for diamond core and 0.1 metre for face sampling. Sample intervals always conform to the logged lithological boundaries. • Resource definition DC was halved for sampling using a diamond saw, half was sampled and assayed, the remaining half resides in the core tray and is archived. The underground grade control DC was sampled as a whole over the determined sampling interval. • All RC recovered samples were passed through a splitting device (cone or riffle splitter) at 1m intervals to obtain sample for assay, which was collected in an appropriately sized calico bag. Target RC calico sample weights range from 2.5 to 4kg across all RC drilling campaigns. Bulk reject sample was also collected into a plastic bag for each metre. Spear samples, composited to 4m or less, were collected from the bulk samples as a first-pass sampling technique. Single metre samples were collected and submitted for assay from areas of expected mineralisation or composite anomalism. • RC and DC samples submitted to the laboratory were sorted and reconciled against the submission documents. • The sample preparation was conducted by accredited commercial laboratories. The technique and practices are deemed appropriate for the type and style of mineralisation. Geochemical samples were dried at 85°C. Prior to mid-2012 dried samples were crushed in a Jaw Crusher then split in riffle splitter if they were above 4kg and pulverized to minimum 95% passing 75µm in LM5 pulveriser. A 200g sample was scooped out and reduced to a 50g sub sample, which was then subject to the Fire Assay process. Since mid-2012 the entire dried sample has been crushed to 2mm in Boyd Crusher and then rotary split to obtain 1kg sample which was pulverized in LM2 pulveriser to 85% passing 75µm. A 200g pulp sample was scooped from LM2 out of which the catch weight sample of 30g was scooped for the Fire Assay. • The sample sizes are considered to be appropriate for the type, style, thickness and consistency of mineralisation present in this deposit. The sample size is also appropriate for the sampling methodology employed and the gold grade ranges returned.
Sub-sampling techniques and sample preparation – Tuart UG	• Assays from DC are all half core samples, the remaining DC resides in the core tray and archived. • All RC samples were split by a cone or a riffle splitter and collected into a sequenced calico bag. For historical drilling any wet samples that could not be riffle split were initially dried then usually riffle split. • The sample preparation conducted by commercial laboratories involves all or part of: oven dried (between 85°C and 105°C), jaw crushed to nominal <10mm, riffle split to 3.5kg as required, pulverized in a one stage process to >85% passing 75um. The bulk pulverized sample is then collected and approximately 200g extracted by spatula to a numbered paper bag that is used for the 30g or 50g fire assay charge. Laboratory Quality Control (QC) includes duplicate samples collected after the jaw crushing stage, and repeat samples collected after the pulverising stage to provide data confirming the appropriateness of the sample preparation technique. All sub-sampling & lab preparations are consistent with other laboratories in Australia & are satisfactory for the intended purpose.

Criteria	Commentary
	• RC and DC samples submitted to the laboratory are sorted and reconciled against the submission documents. Routine CRM (standards and blanks) are inserted into the sampling sequence at a rate of 1:25 for standards and 1:75 for blanks or in specific zones at the Geologist's discretion. The commercial laboratories complete their own QC check. Specific diamond drilling campaigns utilized barren quartz flushes between expected mineralised sample interval(s) when pulverising. • RC field duplicate data was collected routinely and for selected intervals suspected to contain mineralisation. Field duplicate samples were taken at the time of cone/riffle splitting the bulk sample at the rig to maintain sample support. The field supplicates are submitted for assay using the same process mentioned above. The laboratory is unaware of duplicate nature. A selection of historic RC field duplicates was submitted to the laboratory and underwent a screen fire 50g analysis. Some historic DC duplicates were taken by re-sampling ¼ of the remaining half core. The sample and size (2.5kg to 4kg) relative to the grain size (>85% passing 75um) of the material sampled is a commonly utilised practice for gold deposits within the Eastern Goldfields of Western Australia for effective sample representivity.
Quality of assay data and laboratory tests – Homestead	• The assay method was designed to measure total gold in the sample. The laboratory procedures are appropriate for the testing of gold at this project given its mineralisation style. The Fire Assay charge of 30g (previously 50g) was fused with a lead flux then decomposed in a furnace with the prill being totally digested by 2 acids (HCl and HN03) before measurement of the gold content by an Atomic Absorption Spectrometer. Samples were submitted in 78 sample batches including QC samples. • Routine Certified Reference Material (CRM) - standards and blanks were inserted into the sampling sequence at a rate of 1:25 for standards and 1:75 for blanks and also submitted around expected zones of mineralisation. The commercial laboratories completed their own QC check. • Since 2012 barren flushes have been utilized between expected mineralised sample intervals when pulverizing DC samples. • Historic RC drilling Quality Control procedures are not well documented, but not considered material for the resource estimation of this deposit. However the existing Centaur Mining and Exploration Ltd report states that Assay QC was performed for Duplicate and Replicate pulp assays; Re-split and composite assays; Standard assay checks; Fire Screen assays and Umpire assays. • Any erroneous QC results were examined and validated if required; establishing acceptable levels of accuracy and precision for all stages of the sampling and analytical process. If there were any issues with any given CRM, the samples associated with the CRM were immediately re-assayed. Therefore all CRM data and their associated samples satisfy a gross tolerance before being accepted in the database.
Quality of assay data and laboratory tests – Tuart UG	• The assay method is designed to measure total gold in the sample. The laboratory procedures are considered appropriate for the testing of gold at this project given its mineralisation style. The technique involved using a 30g or 50g sample charge with a lead flux, which is decomposed in a furnace, with the prill being totally digested by 2 acids (HCl and HN03) before measurement of the gold content by an AAS machine. • No geophysical tools or other remote sensing instruments were utilised for reporting or interpretation of gold mineralisation.

Criteria	Commentary
	• QC samples were routinely inserted into the sampling sequence and also submitted around expected zones of mineralisation. Standard procedures are to examine any erroneous QC result (a result outside of expected statistically derived tolerance limits) and validate if required; establishing acceptable levels of accuracy and precision for all stages of the sampling and analytical process.
Verification of sampling and assaying – Homestead	• No holes were twinned. • Primary logging and sampling data was sent digitally every 2-3 days from the field to NGF's Database Administrator (DBA). The DBA imports the data into an industry accepted relational DataShed database. When assay results were received electronically from the laboratory they were imported into database. At the same time results of companies and laboratory QAQC testing were also imported into database after further validation checks. The responsible geologist reviewed the data in the database to ensure that it was correct and has merged properly and that all data has been received and entered. Any variations that were required are recorded permanently in the database. • No adjustments or calibrations were made to any assay data used in this report
Verification of sampling and assaying – Tuart UG	• Independent verification of significant intersections not considered material. • No holes were twinned. • Primary logging and sampling data is sent digitally every 2-3 days from the field to the company's Database Administrator (DBA). The DBA imports the data into an industry accepted relational DataShed database. When assay results were received electronically from the laboratory they were imported into database. At the same time results of companies and laboratory QAQC testing were also imported into database after further validation checks. The responsible Geologist reviews the data in the database to ensure that it is correct and has merged properly and that all data has been received and entered. Any variations that are required are recorded permanently in the database. • No adjustments or calibrations were made to any assay data used in this report
Location of data points Collars – Homestead	• Drill holes collars were surveyed by site-based surveyors using a Leica Total Station, Model TS15. This instrument measures distances to an accuracy of ± 0.005m. • The surface data was collected in Map Grid of Australia 1994, zone 51 (MGA 94) and AHD. Historic data pre 2012 and underground data was collected in the Australian Map Grid of 1984, zone 51 (AMG84) and AHD. All DC collar locations were checked against planned co-ordinates for gross errors. • Topographic control was generated from comprehensive survey pick-ups of the area over the last 15 years, which have been used to generate a Digital Terrain Model (DTM). • Historical data collar co-ordinates within the dataset are estimated to have been transformed between Map Grid of Australia 1994, zone 51 (MGA94) and AMG84 (possibly several times).

Criteria	Commentary
	- The current resource estimate was calculated using AMG84 grid coordinates. - The magnetic declination for Kalgoorlie has a five year moving average of +0.108 degrees.
Location of data points Collars – Tuart UG	- After drilling, drill hole collar positions are surveyed by the site-based survey department (utilising either a theodolite or differential GPS) with a precision of less than 0.2m. - Recent data is collected in MGA 94 Zone 51 and AHD. Data pre-2012 is collected in AMG 84 Zone 51 and AHD - Topographic control was generated from comprehensive survey pick-ups of the area over the last 15 years, which have been used to generate a Digital Terrain Model (DTM).
Location of data points Down Hole Surveys - Homestead	- Most historic drill holes used in the project were surveyed using a Down Hole Electronic Multishot (DEMS) camera. There also are 20 x long (300m) surface diamond holes which were surveyed using Maxibore instrument. The affected holes are in the CTRFIHCD series, which define the upper portion of the orebody. This could be an issue as the Maxibor methods proved to be unreliable. - For the 2007 surface drilling campaign (HED040 to HED052), a chrome barrel was used to minimise drill hole deviation. Eastman single shot surveys were also taken at an average of 30 metres down the drill hole to ensure that the drill holes continued on the design path. All these diamond drill holes were also surveyed with a north-seeking gyro instrument. - All underground collared DC holes in HUD series are surveyed by DEMS. Short underground holes (HUB) are not surveyed.
Location of data points Down Hole Surveys – Tuart UG	- Down hole surveys consist of regular spaced Eastman single shot, and electronic multishot surveys (generally <30m apart down hole). Ground magnetics can affect the result of the measured azimuth reading for these survey instruments. Twenty-nine per cent of RC of survey data consists of surveys taken with north seeking gyro instruments. Gyro survey measurements are obtained every 5m down hole.
Data spacing and distribution – Homestead	- The nominal drill spacing is 20m x 15m expanding to 40m x 30m and to 60m x 60m below -150mRL. - Data spacing and distribution is considered acceptable for establishing geological continuity and grade variability appropriate for classifying a Mineral Resource. - Samples were composited creating a single composite across each mineralised domain. This strategy has a benefit of reducing the support bias, reducing data variability, reducing effect of a nugget and therefore contributes to a better quality of the resulting estimate.
Data spacing and distribution – Tuart UG	- The nominal drill spacing is 20m x 20m with some areas of the deposit at 40m x 40m to around 230mRL, expanding to 80m x 80m down to around 0mRL. This description of data spacing refers to both the classified and unclassified portion of the deposit. Grade

Criteria	Commentary
	Control (GC) data is on 5m x 5m spacing. This spacing includes data that has been verified from previous exploration activities on the project. • Data spacing and distribution is considered acceptable for establishing geological continuity and grade variability appropriate for classifying a Mineral Resource. • Sample were composited to 2m to assist with the effects of volume variance and to decrease grade variability.
Orientation of data in relation to geological structure – Homestead	• Most of the surface DC was drilled from the hanging wall to the footwall to achieve the best possible angle of intersection. Some of the surface holes intersect the orebody at acute angles. After the underground drilling platforms became available in the late 2009 DC were also drilled from footwall to hanging wall. All FS sampling was performed across the mineralised veins. • No drilling orientation and sampling bias has been recognized at this time.
Orientation of data in relation to geological structure – Tuart UG	• The nominal drill spacing is 20m x 20m with some areas of the deposit at 40m x 40m to 230mRL, and expanding to 80m x 80m down to 0mRL. This description of data spacing refers to both the classified and unclassified portion of the deposit. Grade Control (GC) data is on 5m x 5m spacing. This spacing includes data that has been verified from previous exploration activities on the project. • Data spacing and distribution is considered acceptable for establishing geological continuity and grade variability appropriate for classifying a Mineral Resource. • Sample compositing applied was 2m to assist with the effects of volume variance and decrease grade variability.
Sample security	• Historical samples are assumed to have been under the security of the respective tenement holders until delivered to the laboratory where samples would be expected to have been under restricted access. • Recent samples were all under the security of Paddington until delivered to an analytical laboratory in Kalgoorlie where they were in a secured fenced compound security with restricted entry. Since 2012 all samples from Homestead DC are submitted for analysis to ALS laboratory in Kalgoorlie. Internally, ALS operates an audit trail that has access to the samples at all times whilst in their custody.
Audits or reviews	• Internal reviews are completed on sampling techniques and data as part of the Norton Gold Fields continuous improvement practice • No external or third party audits or reviews have been completed.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	Commentary
Mineral tenement and land tenure status – Homestead	• Homestead is located on tenement M24/155 and M24/79 which are 100% owned by Paddington Gold P/L a wholly owned subsidiary of Norton Gold Fields P/L. The M24/155 and M24/79 licences are part of the Mount Pleasant Project area that has a combined reporting group reference of C36/2009. Mining lease status was granted for all tenements in the early to mid-1990's and has an annual expenditure commitment of $36,600 • Tenements are in good standing and there are not known impediments.
Mineral tenement and land tenure status –Tuart UG	• The Tuart deposit is located within Mining Licenses M24/155, M24/234, M24/266, M24/265 and M24/302. All tenements are 100% held by Paddington Gold P/L, a wholly owned subsidiary of Norton Gold Fields P/L. Two Miscellaneous Licenses cross cut these tenements (L24/54 held by a Norton Gold Fields subsidiary company and L24/205 held by an unrelated party). Several heritage sites exist within the tenure including site IDs: 20,877, 22,885, 15,260, 15,261, 21,715, 21,716, 21,856, 21,857 and 21,858. All leases are granted pre-Native Title. Third party royalties are applicable to these tenements and are based on production ($/t) and proportion of net profit. • The tenements are in good standing and no known impediments exist.
Exploration done by other parties	• A significant proportion of exploration, resource development and open pit mining was completed by companies which held tenure over the Homestead and Tuart deposits since the mid 1990's. Companies included: Centaur Mining and Exploration PL (1995-2001), Aurion Gold (2001-2002), Placer Dome (2002-2005) Asia Pacific and Barrick Kanowna (2005-2007). Results of exploration and mining activities by the afore-mentioned companies aid in Norton Gold Field's more recent exploration, resource development and mining in the area. • In the current Homestead resource only less than 3% of all data is legacy data. • Reporting of results herein only relates to results obtained by Norton Gold Fields.
Geology – Homestead	• The Homestead deposits are located within the Norseman-Wiluna greenstone sequence, at or below the lithological contact between the Bent Tree (BTB) and Victorious Basalt (VB) units. The metamorphic grade is defined as lower green-schist facies. A significant deformation zone is observed at Homestead, the Homestead Shear Structure (HSS). The HSS is a splay off the Black Flag Fault. Homestead deposits are classified as a narrow vein, orogenic gold deposits. Gold mineralisation is hosted within the laminated quartz veins and typically associated with scheelite, sphalerite and galena mineralisation. One or two laminated quartz veins are observed in the underground development oriented parallel to the structural corridor (VN01). At the northern limit the veins are cut by a northeast trending fault, which offsets the HSS by 40 metres to the west. The offset northern extension is

Criteria	Commentary
	named VN03. Cross cutting veins (Black Flag West and Phantom) are generally brittle-ductile accommodation structures.
Geology - Tuart	• The deposit type is classified as a, narrow vein, orogenic gold deposit within the Norseman-Wiluna greenstone sequence. The accepted interpretation for gold mineralisation is related to (regional D2-D3) deformation of the stratigraphic sequence during an Archaean orogeny event. The mineralisation is hosted within the upper-mafic rock unit of the Kalgoorlie stratigraphy. The metamorphic grade is defined as lower green-schist facies. • The mineralisation is located in brittle-ductile shear zones typically associated with carbonate-sericite alteration +/- sulphides.
Drill hole Information	• See Appendix 1
Data aggregation methods	• All reported assay results have been length-weighted, no top cuts have been applied. Assay results are reported above a 3.5/t Au lower cut. • A maximum of 2m of internal dilution is included for reporting intercepts. Minimum reported interval is 1.0m for RC and 0.3m for DC intercepts. • No metal equivalent values are used for reporting exploration results
Relationship between mineralisation widths and intercept lengths – Homestead	• Most of the DC holes were drilled to achieve the best possible angle of intersection. Some of the surface holes intersect the orebody at acute angles.
Relationship between mineralisation widths and intercept lengths – Tuart UG	• Drill hole intersections are generally planned to intersect known targets at a high angle to each mineralised zone.
Diagrams	• See Appendix 2
Balanced reporting	• All results have been reported relative to the intersection criteria.
Other substantive exploration data	• No other exploration data collected is considered material to this announcement.
Further work – Homestead	• Further work at Homestead will include additional resource development drilling and updating geological models.
Further work - Tuart	• Further work will include mining studies to determine if the project is economically viable. Interpreted mineralised plunge directions require further drill further if the mining studies indicate that the project is economically viable.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	Commentary
Database integrity	• NGF geological data is stored in SQL server databases. The SQL databases are hosted on site at Paddington and managed by Paddington personnel. User access to the database is regulated by specific user permissions and validation checks to ensure data remains valid. DataShed software has been implemented as a front-end interface to manage the geological database. • Existing protocols maximize data functionality and quality whilst minimizing the likelihood of error introduction at primary data collection points and subsequent database upload, storage and retrieval points. Data templates with lookup tables and fixed formatting are used for collecting primary data on field laptops. The software has validation routines and data is subsequently imported into a secure central database. • The SQL server database is configured for validation through parent/child table relationships, required fields, logical constraints and referenced library tables. Data that fails these rules on import is rejected or quarantined until it is corrected. • Historic data has been merged into the main SQL database, PGMshed. This dataset had various validation issues including duplicate hole identification, missing and poor quality survey data, missing geology, and duplicate and missing assays. Most of these issues have been resolved by a series of data quality improvement projects targeting specific areas of concern. It is, however, an ongoing task to review and upgrade the validity of historic data. • All geological data in digital format is now contained in two SQL databases. PGMshed contains current and historic exploration and resource definition data. PitShed contains current and recent grade control data. • The current resource estimates used MS Access subsets of data created from SQL database. To validate this datasets hole traces were visually (on screen) examined to identify missing or incorrect survey and collar location information in the Homestead and Tuart areas.
Site visits	• The Competent Person for this update is a full time employee of NGF and undertakes regular site visits ensuring industry standards of the Mineral Resource estimation process from sampling through to final block model. • The deposit area is an active mining area for NGF and as such regular site visits were undertaken during this update. • An independent geological consultant has reviewed the project area in 2009 which included a site visit.

Criteria	Commentary
Geological interpretation – Homestead	• The high confidence of the geological interpretation is based on geological knowledge acquired from detailed geological DC and RC logging, assay data, underground development backs and face mapping and pit mapping. • The geological model of the main mineralised vein system at Homestead was created in Surpac V6.1.4 mining software. Solids representing mineralised veins were built from strings created on plan sections and from points snapped directly to drill hole intersections. The underground development mapping was also utilized to aid in understanding of veins structure. • The geological interpretation was based on identifying particular geological structures, associated alteration, veining and gold content. A gold grade cut off of 3g/t was used. In the absence of gold enrichment the lithological codes determining vein boundaries were occasionally used instead. • Between 2009 and 2012 Homestead deposits and other resource areas within the Mount Pleasant mining camp were subjected to structural studies by independent consultants. Observations collected from the pit walls and from underground openings helped to establish dimensions and orientation of continuity of mineralised veins and aided in targeting of extensions to existing resource. • The geological interpretation is considered robust. As geological data is collated the geological interpretation is continually being updated. • Whilst the geological features are deemed to be continuous, the gold distribution within them can be highly variable. The in situ distribution of precious metals is a factor affecting the grade continuity. This was overcome by defining sample spacing and ensuring sample and analytical quality was high. Geological structures post-dating the mineralisation can off-set and truncate the mineralisation affecting the geological continuity and are sometimes difficult to isolate. • The dataset (geological mapping, RC and DC logging, assays etc.) is considered acceptable for determining a geological model. A key interpretation assumption made for this estimation was the interpretation of the mineralisation past known drilling limits (extrapolated a reasonable distance considering geological and grade continuity).
Geological interpretation – Tuart UG	• The high confidence of the geological interpretation is based on geological knowledge acquired from the open pit production data, detailed geological DC and RC logging, assay data, underground development face mapping of the adjacent underground deposit and pit mapping. • The dataset (geological mapping, RC and DC logging, assays etc.) is considered acceptable for determining a geological model. Key interpretation assumptions made for this estimation are: (1) where cross cutting relationships were not observed; and (2) the interpretation of the mineralisation past known drilling limits (extrapolated a reasonable distance considering geological and grade continuity). • The geological interpretation is considered robust; therefore alternative interpretations are considered inferior and are not considered to have detrimental effect on the Mineral Resource. No alternate interpretation is proposed as geological confidence in

Criteria	Commentary
	the model is high. As geological data is collated the geological interpretation is continually being updated. • The geological interpretation is specifically based on identifying particular geological structures, associated alteration, veining and gold content. • Whilst the geological features are deemed to be continuous, the gold distribution within them can be highly variable. The insitu distribution of precious metals is a factor affecting the grade continuity. This is overcome by defining sample spacing and ensuring sample and analytical quality is high. Geological structures post-dating the mineralisation can off-set and truncate the mineralisation affecting the geological continuity and are difficult to isolate.
Dimensions – Homestead	• Several laminated veins are observed in Homestead area. The veins are usually mineralised hosting four known deposits: o VN01: striking 010°, dipping -80° towards W, 250m strike and 500m known dip extent o VN03: striking 020°, semi-vertical, 200m strike and 350m known dip extent o Phantom: striking 090°, dipping -60° towards N, 100m strike and 170m known dip extent o Black Flag West: striking 275° to 320°, dipping -70° towards NE, 150m strike and 250m known dip extent • Other veins of various orientations have also been identified, but at this stage do not form part of a reportable resource. • Each lode is typically 0.5 to 2m wide true width. VN01 and VN03 are located within Homestead Sheer Structure. • The Homestead deposit is spatially located between 329,950mE and 330,400mE and between 6,619,550mN to 6,620,150mN (AMG84 zone51).
Dimensions – Tuart UG	• The Tuart deposit is spatially located between 329,200mE and 330,100mE – running into the Quarters deposit and 6,620,400mN to 6,621,700mN (AMG84 zone51). Up to 5 gold lodes on varying orientations have been located. o T060 lode: -45° towards 330°, 1km strike and 150m known dip extent o T080 lode: sub-vertical dip and E-W strike, 600m strike 250m known dip extent o T115 lode: -55° towards 295°, 500m strike and 250m known dip extent o Q040 lode: convex dip striking ~070° then turning to 040° at Quarters, 350m dip extent o Golden Swan: moderate south dip and ENE strike, know strike 400m and known dip 100m • Each lode is typically 0.5 to 2m wide true width. Bonanza intercepts are up to 4m wide (true width) Supergene mineralisation is observed at the interface of the gold lodes with the regolith profile. Some gold is associated with the Tertiary material. Gold mineralisation starts at 15m-25m below the surface (supergene) and extends to below 0mRL – the extent of drilling

Criteria	Commentary
Estimation and modeling techniques – Homestead	• Estimation was completed using linear estimation techniques - Ordinary Kriging (OK) for VN01 and Inverse Distance Squared (ID2) for VN03, Phantom and Black Flag West. • Geological domains were based on the geological interpretation. Three dimensional wireframes were created by sectional interpretation of the drilling dataset with points snapped to drill hole and face sampling intercepts. Domain boundaries were treated as hard boundaries. • The choice of compositing technique took into account several criteria including: o The thickness of the ore zones (between 0.2 and 4.8 metres thick – 1 metre on average) o Samples were of unequal support (10 centimetres to a meter and up to 4 metres in RC holes) o Variable data spacing – from 3 metres by 15 metres to 80 metres by 80 metres for vein intercepts o Short-scale grade and geometry variability • Since it is not possible (or desirable) to mine any of the individual veins selectively across their width, a single composited sample was generated from each drill hole within each of the solid objects representing individual domains. This strategy also had the benefit of reducing the support bias, reducing data variability, reducing the nugget effect, and therefore contributes to a better quality of the resulting estimate. • The statistics for each domain were viewed and key univariate statistical indicators used to describe the nature of each. Each of the population of the composite data from the Homestead mineralised quartz veins was positively skewed and showed a number of high grade outliers, typical of most of gold mineral deposits. High-grade outliers were top-cut to o 200g/t; 150g/t and 50g/t Au in VN01 o 120g/t Au in VN03 o 20g/t; 80g/t and 120g/t Au in Phantom o 50g/t Au in Black Flag West in domain 3 • Top-cuts were determined by way of viewing grade distribution histograms. The following factors were taken into account o Coefficient of Variation (CV) of samples should be reduced to preferably no more than 1.4 o Preferably 95% of the mean should be maintained o Variance should be reduced as much as possible considering the above factors • Spatial continuity modeling was completed in Snowden Supervisor V7.10.18 software. Investigation was conducted on the top-cut composite datasets for the main vein in VN01 and applied to remaining, semi-parallel smaller veins. Directions of continuity were similar to interpreted controls on mineralisation with varying degrees of anisotropy. In VN03 the special analysis performed for the

Criteria	Commentary
	main vein were used to determine orientation of search ellipsoids. • Sample search ellipsoids were set based on data spacing in similar orientations to the spatial continuity directions for each domain: in VN01 and VN03 using variography analysis, and in Phantom and Black Flag West to mirror the orientation of mineralised envelopes. The search parameters were set to minimum and maximum samples for each sample search based on accepted levels of grade continuity. Search distances were based on sample spacing and spatial continuity. A total of 3 search passes were conducted with progressively relaxed search criteria to accommodate the data density from face sampling to the widest spaced drilling at 80m x 80m. • Block model dimensions, block sizes and sub-blocking was chosen after a careful examination of the extents of mineralisation, general shape of mineralised veins and distribution of data points ○ VN01 - 10m(Y) by 1m(X) by 10m(Z) ○ VN03 - 10m(Y) by 1m(X) by 5m(Z) ○ Phantom - 1m(Y) by 5m(X) by 10m(Z) ○ Black Flag West - 5m(Y) by 1m(X) by 5m(Z) • Blocks in the block models were coded based on the interpreted solids by block centroid in or out of solids. The validity of the size of sub-blocking was check by comparing volumes of interpreted solids with volumes of domains generated in block model. The volumes of solids and volumes of domains matched within 1 to 2%. Domain coding was used to control the grade estimation process. • No correlation between variables was necessary. • Estimation completed using Surpac V6.1.4 mining software. • Standard block model validation has been completed using visual and numerical methods and peer review by key geology staff. • Mineral Resource Model has been validated visually against the input composite/raw drill hole data with sufficient spot checks carried out on a number of block estimates on sections and plans. • A comparison of blocks' and the informing samples' (top-cut composites) statistics was undertaken. • Mining production data is available to be compared with the estimation result.
Estimation and modeling techniques – Tuart UG	• Estimation was completed using a linear estimation technique - Ordinary Kriging (OK). OK is an estimation method where a single direction of continuity is modelled for each domain. An advantage of OK is the inbuilt function for data de-clustering. A disadvantage is the use of this technique on variable, skewed datasets. • Geological domains were based on the geological interpretation. RC/DC intercepts modelled to be a minimum down-hole width of

Criteria	Commentary
	1m. 3DM wireframes created by sectional interpretation of the drilling dataset. Domain boundaries were treated as hard boundaries. • A single composites for each down hole intercept was generated and subdivided into each domain using an inside/outside principle • The statistics for each domain were viewed and key univariate statistical indicators used to describe the nature of each. Each domain showed a positively skewed data distribution with high-grade outlier composites. Top-cuts ranged from 28g/t to 40g/t Au for all domains by way of viewing grade distribution histograms, where the continuity of the higher-grades decreased to a nominal level. • Spatial continuity modelling was completed on the top-cut composite datasets for each domain. Directions of continuity were similar to interpreted controls on mineralisation with varying degrees of anisotropy. • Sample search ellipses were set based on data spacing in similar orientations to the spatial continuity directions for each lode. Minimum and maximum samples were set for each sample search based on accepted levels of grade continuity. Search distances were based on sample spacing and spatial continuity. A total of 4 search passes were conducted with progressively relaxed search criteria to accommodate the data density for GC drilling to the widest spaced drilling at 80m x 80m. • Estimation completed using Surpac V6.4.1 mining software block modeling module • No previous underground mining reconciliation data is available for cross checking this resource estimate. Historic resource estimate grades compare to this resource estimate. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered • Block model dimensions were set to 329,100mE to 300,450mE and 6,620,350mN to 6,621,950mN and between 370mRL and -100mRL. Block sizes were chosen to compromise between sample spacing and orientation of mineralisation i.e. 10m(X) by 2m(Y) by 5m(Z). • No selective mining units were assumed in this estimate. • No correlation between variables was necessary. • The 3DM/DTM wireframes for the estimation domains, regolith and topographical files were used to control the resource estimate. Blocks from the block model were coded based on these volumes/surfaces by either block centroid in/out of 3DM or above/below a DTM surface. • Statistical analysis indicated that outlier management was crucial to prevent high grade smearing that could result in overestimation of gold content (an adverse effect of using OK on a skewed dataset). Top-cutting and restricted sample search or the combination of both (top-cuts and restricted search were defined following thorough examinations of histograms, probability curves and the spatial locations of the outliers) has been used to reduce this effect.

Criteria	Commentary
	• Standard model validation has been completed using visual and numerical methods and formal peer review sessions by key geology staff. • Mineral Resource Model has been validated visually against the input composite/raw drill hole data with sufficient spot checks carried out on a number of block estimates on sections and plans. • Easting swath plots have been generated to check input composited assay means for block estimates within swath windows. OK estimates have also been checked against an alternate MIK estimates and historic production data. • A comparison of block volume weighted mean versus the drill hole cell de-clustered mean grade of the composited data was undertaken.
Moisture	• Tonnages were estimated on a dry basis
Cut-off parameters	• Cut-off of 3g/t Au was used for creating solids for mineralised veins. A low grade envelope based on 0.5g/t cut-off was also created around all veins (except for Phantom) to aid in accurate calculation of diluting grades for Ore Reserve estimations.
Mining factors or assumptions	• The models were depleted for known workings. • No selective mining units were assumed in this estimate. • Mining methods are based on current underground mining operations at Homestead. The resource is mined utilising narrow-vein underground mining methods (jumbo cut and fill for development long-hole stoping for production). • The fresh portion of the Tuart UG resource is likely to be mined utilising the same mining methods.
Metallurgical factors or assumptions	• No assumption or factors have been applied to the resource estimate regarding the metallurgical amenability. • Ore from Homestead is processed through the Paddington Mill (owned by NGF). The mill utilizes a CIP extraction process. • The gold recoveries from Paddington Mill which treats also low grade ore from different sources fluctuate around 93% – 94%. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered material to this style of mineralisation. • Assumptions for metallurgical extraction of gold from Tuart UG deposit are based on processing Tuart ore through the Paddington Mill in the past.
Environmental factors or assumptions	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on current and historic mining and milling of existing operations in the area.
Bulk density – Homestead	• The current Homestead models are fully within fresh rock. The data used to determine bulk density of the fresh rock was compiled during a 2007 drilling campaign. Diamond core samples were taken in fresh basalt every ten metres down the drill hole. To

Criteria	Commentary
	determine bulk density of each sample a gravimetric method (Archimedes Principal) has been used, where samples are first weighted in air, then in water and a bulk density is calculated. A total of 384 bulk density values were calculated with a statistical analysis shown below. ○ Mean: 2.64 ○ Standard deviation: 0.28 ○ Mode: 2.75 ○ Median; 2.71 The determined mean bulk density value was deemed to be too low and the value of 2.68 (average of mean and median value) was used instead for 2008 model and in all consecutive models. For consistency the same value was applied to the current model. During 2010 bulk density determination was carried out on 539 samples collected from HUD series underground diamond core. Data collected to date suggests that density higher than 2.68 is possible, however most of the measurements came from the basalt with only small proportion collected in quartz veins. It would be prudent to collect more samples from the quartz veins and alteration zones before changing bulk density value currently applied to block models. The implication of the change could be 2% addition to resource tonnes and therefore to ounces.
Bulk density – Tuart UG	• Bulk densities applied to the resource estimate were based on systematic test work completed on hand specimens and DC for selected material types. The bulk density determination method is based on the water immersion technique. The bulk density test work reconciles against production tonnages from historic and current mining operations within the project area. Samples that were porous were wax coated and accounted for in the bulk density calculation.
Classification	• NGF follows the JORC classification system with individual block classification based on statistical methods taking into account the following factors: ○ Confidence of certain parts of the geological model supported by ○ Drill spacing and orientation ○ Classification of surrounding blocks; ○ Portions of the deposit that is likely to be viably mined. • At Homestead Measured category was assigned to resource within 7.5 metres vertically from mine development. Indicated category to resource where distance between data points was not larger than 40 metres. Inferred category to resource estimated using a higher data points separation, estimated using a more relaxed estimation run.

Criteria	Commentary
	• The classification strategy reflects the view of the Competent Person.
Audits or reviews	• The Mineral Resource has not been externally audited. An internal Norton Gold Fields peer review has been completed as part of the resource classification process.
Discussion of relative accuracy/ confidence	• The Mineral Resources have been reported in accordance with the guidelines of the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves and reflects the relative accuracy of the Mineral Resources estimate. The Competent Person deems the process to be in line with industry standards for resource estimation and therefore within acceptable statistical error limits. • The statements relates to global estimates of tonnes and grade for existing underground mining extraction. • Production data was used to compare with the resource estimate (where appropriate) and assisted in defining geological confidence and resource classification categories • To assess an influence of face sampling data, a second estimate was performed in VN01 using only samples from drill holes. A comparison of two estimates revealed that there is negligible difference (1%) in ounces generated using these different sets of data.

Section 4 Estimation and Reporting of Homestead Ore Reserves

(Criteria listed in section 1, and where relevant in sections 2 and 3, also apply to this section.)

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• A financial evaluation, underground life of mine design and schedule were completed for Homestead by NGF personnel in December 2014. The development and stope design parameters are based on existing NGF underground procedures. The scheduled life of mine reserves consist of proven reserves of 157,054 @ 6.35g/t Au and probable reserves of 64,387t at 6.36g/t at a cut off grade of 3.3g/t. • The Mineral Resources are reported inclusive of the Ore Reserves.
Site visits	• Homestead Underground is currently an active mine site which has been in operation since August 2009. • Homestead Underground has been visited by Elizabeth Jones (UG Manager “NGF” & CP for Reserves) within the last 6 months. • Inspection of the existing stoping and development has been carried out and geotechnical constraints such as stope stability, ore types, hydrogeological setting has been undertaken and incorporated into the mineable reserve.

Criteria	Commentary
Study status	• NGF Technical Services Department undertook financial review and design of the Homestead mineral deposit. The Life of Mine plan was based on a selling price of $AUD 1,400/oz with a 2.5% royalty. • The block models used for the Underground design are “hs_bfw_rot_oct14.dm, hs_vn01_nov14.dm & hs_vn03_apr14.dm”. • Mining dilution, ore loss and mill recovery factors were applied (12-59%, 5% and 95% respectively). • Operating cost used was based on NGF’s current Underground fleet with average processing cost of $24.70/t (Including haulage from Homestead and G&A costs).
Cut-off parameters	• A break even cut off grade of 3.3 g/t was calculated using the 2015 budget and physicals • Selling price = AUD$1,400/Oz. • State Royalty = 2.5%. • Metallurgical recovery = 95%. • Processing cost = $24.70/t.
Mining factors or assumptions	• The method used to convert Mineral resource to Ore Reserves is based upon identifying which proposed mining panels and development areas are economic. • The mining method will be based on standard jumbo development and long hole open stoping with flat-back mining utilised in some areas. • NGF is an owner operator and Homestead is currently being mined by NGF using its operating model. • The Ore reserve estimate was created using mining shapes with an allocated level of confidence. All shapes were checked by a resource geologist to ensure correct assignment of resource category • Gold Price used = $AUD1,400/Oz. • Processing cost = $24.70/t (Including haulage from Homestead and G&A costs). • Infrastructure requirement for underground mining includes; A workshop for all mobile equipment for maintenance requirements, offices, crib rooms and amenities, explosives storage, water dams and communication. All of these infrastructures are already on site and actively used.
Metallurgical factors or assumptions	• Homestead ore has been milled continuously at NGF’s Paddington mill since 2009. • Ore from Homestead will be delivered via road trains to NGF’s Paddington mill for processing. • Paddington Mill is based on conventional carbon in pulp technology and has achieved an annual throughput of 3.72 million tonnes in 2014 with average feed grade of 1.68g/t with average recovery of 89%. • A recovery factor of 95% has been applied to all Homestead ore.
Environmental	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. • All proposed operation and operational plans are within local historical practices and existing operational standards.

Criteria	Commentary
Costs	• Homestead's reserve estimate was based on a gold price of $AUD 1,400/Oz. • Allowance has been made for the 2.5% state government royalty. • Operating cost used was $121.61/ore t. This is based on budgeted numbers for Homestead in 2015.
Infrastructure	• The site has existing infrastructure including electricity, water and road infrastructure. • The site has a fully operational office, core facility, crib rooms, explosives storage, water dams and communication.
Revenue factors	• Financial analysis in this report is based on a gold price of $AUD 1,400/Oz. • The gold Dore is planned to be transported via recognized security service from gold room of Paddington processing plant to the gold refinery in Perth. • Contract payments and terms are expected to be typical of similar contracts for the refining and sale of Dore produced from other operations within Australia. Allowance has been made for the 2.5% state government royalty.
Market assessment	• Historical gold price and forward looking estimates have been used for the gold price. Price flexing and sensitivity analysis have been carried out to determine the robustness of the project viability. The cash flow was modelled in real terms and no price or cost escalations were applied.
Economic	• Inputs to economic analysis include factors described above including ore and metal quantities from mining/processing schedule (including described recovery/processing parameters), cost and price assumptions.
Social	• The majority of workforce is from Kalgoorlie. • NGF has established all relevant agreement with local stakeholders and government agencies.
Classification	• The Ore Reserve was classified as Proven and Probable in accordance with the JORC Code, corresponding to the resource classifications of Measured and Indicated. No Inferred Mineral Resources were included in the Ore Reserve estimate. • The estimated Ore Reserves and mining method are in the opinion of the Competent Person appropriate for this style of deposit.
Audits or reviews	• The resource and reserve was calculated by NGF personnel. The cost and mining parameters were reviewed internally against existing operations and consideration was made for current practice and cost structure. • It is not expected that practices assumed in the calculation of reserve will vary before the next annual reserve calculation.
Discussion of relative accuracy/ confidence	• All mining estimates are based on Australian costs, and relevant historical cost data. • All Proven reserves have been developed with a vertical level interval of less than 25m. • There are no unforeseen modifying factors at the time of this statement that will have any material impact on the Ore Reserve estimate.

Appendix 1: Table of exploration results – Homestead Diamond Core

Hole ID	AMG East	AMG North	AMG RL	Dip	Azimuth	Depth (m)	From (m)	To (m)	DH Width (m)	Grade (g/t au)
HUD979	330287.7	6619756	108.1	-29.5	69	166				NSI
HUD980	330359.8	6619724	225.3	-25.3	173.4	86.7				NSI
HUD981	330359	6619725	225.0	-53	190.6	59.4	35.4	36.35	0.95	9.04
							45.7	47.75	2.05	9.92
HUD982	330359.2	6619725	226.4	-1.6	184.1	84				NSI
HUD983	330358.4	6619726	226.2	-9.6	209.4	50.35	46.85	48.3	1.45	8.76
HUD984	330291.9	6619768	227.0	25.4	136	80.1	65.5	67.1	1.6	17.47
							79	79.4	0.4	31.4
HUD985	330291.4	6619768	227.3	29.4	152.2	67.3	48.95	51.4	2.45	5.89
							62.3	63.15	0.85	29.3
HUD986	330290.6	6619768	227.5	33.8	170.1	50.8	42.5	43.13	0.63	126
HUD987	330289.8	6619768	228.2	42.8	190.6	58.25	29.7	32.17	2.47	39.57
HUD988	330217.6	6619790	225.3	22	97.4	32.5	17.95	18.4	0.45	9.39
HUD989	330216	6619792	224.9	15.8	41.4	32.85	10.2	10.7	0.5	4.04
HUD990	330248.9	6619877	20.1	-17.8	90.2	125.6	105.8	107.8	2	2.33
HUD991	330248.8	6619877	20.4	-11.3	90.2	104.7	86	87.1	1.1	13.74
HUD992	330248.5	6619877	20.4	-13.7	74.4	90.5	68.75	71.3	2.55	9.64
HUD993	330248.5	6619877	22.1	25.3	76.1	48.5	32	34.6	2.6	2.49
HUD994	330248.2	6619878	20.0	-24.4	54.1	102	42	42.65	0.65	12.67
							72.7	74.5	1.8	8.41
							77.65	78.9	1.25	5.43
HUD995	330248.1	6619878	20.4	-15.0	54.0	80.1	53.9	56.25	2.35	5.5
HUD996	330248.1	6619878	22.6	32.7	54.0	46.3	27.9	28.8	0.9	4.84
HUD997	330251.7	6619896	19.5	-26.6	48.4	90.3	45.1	49.1	4	9.22
							52.2	55.5	3.3	3.55
HUD998	330251.6	6619896	20.7	-0.9	48.4	47.6	22.35	23.9	1.55	5.45
HUD999	330251.2	6619895	23.1	40.4	48.4	32.8				NSI
HUD1000	330339.5	6619733	225.0	-65.6	244.0	36.4	10.05	11.85	1.8	28.18
							14.85	18.7	3.85	7.14
							20.8	21.1	0.3	4
HUD1001	330339	6619733	224.7	-47.9	244.0	33.7	4.8	8.25	3.45	8.4
							14.2	14.9	0.7	5.49
							27.45	28.45	1	7.13
HUD1002	330055.7	6619960	-92.1	-40.8	306	80.7				NSI
HUD1003	330056.1	6619961	-91.2	-11	326.4	69	50.7	51.4	0.7	8.99
							56	56.6	0.6	5.29
HUD1004	330056.1	6619961	-91.5	-22.6	326.4	75.1	51	52	1	15.6
							58	58.75	0.75	8.31
HUD1005	330056.1	6619961	-92.3	-43.5	326.4	100.3	88.4	89.3	0.9	9.25
HUD1006	330056.5	6619961	-91.2	-11.5	336.2	79.7	68.5	69.25	0.75	29.2
HUD1007	330056.4	6619961	-91.6	-23.3	336.2	95.6	64.7	68.7	4	4.38
							73	76.2	3.2	4.84
HUD1008	330056.4	6619961	-92.0	-36	336.2	110.8	74.5	75.5	1	4.71
HUD1009	330056.7	6619961	-91.4	-20	343.2	100.5				NSI
HUD1010	330401.9	6619794	63.7	-30.4	34.3	68.6	1.15	2.15	1	5.65
							27.4	31.4	4	56.67
							33.4	34.4	1	6.69
HUD1011	330402.4	6619794	63.4	-33.7	52.5	86.7	53	54	1	4.32
HUD1012	330062.7	6619961	-91.6	-23	53	43	19.75	20.75	1	3.76

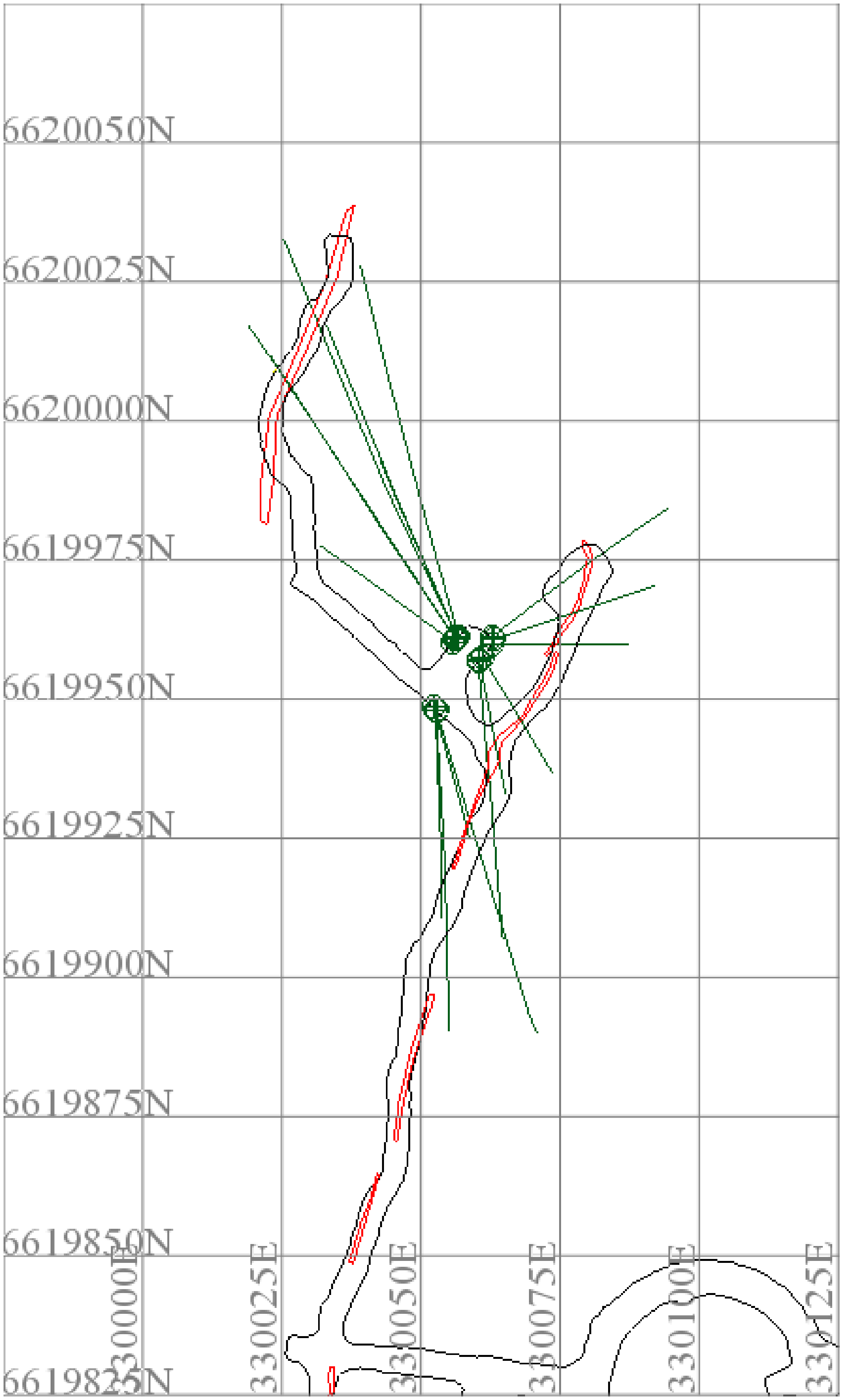
Hole ID	AMG East	AMG North	AMG RL	Dip	Azimuth	Depth (m)	From (m)	To (m)	DH Width (m)	Grade (g/t au)
HUD1013	330062.8	6619960	-92.0	-35.5	88	30				NSI
HUD1014	330061.1	6619958	92.0	-33.5	147	29.3	14.5	15.5	1	7.81
HUD1015	330060.3	6619957	-92.0	-23.5	172	54.5	20.9	21.2	0.3	4.56
							28.5	29.9	1.4	4.79
HUD1016	330060.4	6619957	-92.2	-46	168	46.95	26.45	27.8	1.35	48.03
HUD1017	330052.8	6619948	-92.1	-22.5	165	65.6	27.45	28	0.55	4.48
							45.9	47	1.1	6.5
HUD1018	330052.3	6619949	-92.6	-46.5	165	68.2	31.75	32.7	0.95	40.6
							57.75	60	2.25	3.47
HUD1019	330052.7	6619948	-91.8	-16.5	178.5	60.4				NSI
HUD1020	330052.6	6619948	-92.6	-34.5	178.5	65.2	36.5	38.5	2	29.2
HUD1021	330063.1	6619961	-88.9	27.5	65.5	34.4	18.95	19.7	0.75	140
HUD1022	330162.5	6619748	50.9	-12	76	410.9				NSI
HUD1023	330162.6	6619749	50.4	-17.5	68	379.4	280	280.4	0.4	8.67
HUD1024	330162.8	6619748	50.2	-23	73	497.7				NSI
HUD1025	330162.6	6619749	45.0	-26	62	420				NSI
HUD1026	330162.5	6619750	45.0	-28	49	401.7				NSI
HUD1027	N/D									
HUD1028	N/D									
HUD1029	330403.3	6619793	63.3	-28.8	69.0	95.4	52.05	54.4	2.35	27.97
							60.4	61.4	1	5.56
							69.4	70.4	1	4.85
HUD1030	N/D									
HUD1031	N/D									
HUD1032	330403.3	6619793	63.5	-24.2	79.5	110.1	68.75	69.75	1	3.71
							95.85	96.85	1	3.58
HUD1033	330403.5	6619793	64.0	-10.3	87	110	57.6	60.6	3	33.79
							72.6	73.6	1	7.24
							77.1	78.1	1	4.53
HUD1034	330216.7	6619750	194.0	-8.5	86.3	205.5	30	31.3	1.3	9.22
							171	174	3	17.42
HUD1035	330216.9	6619750	193.0	-23	106	197.4	28	28.4	0.4	4.09
HUD1036	330217.7	6619751	193.7	-2.9	82.3	63				NSI
HUD1037	330217.4	6619752	195.0	-32.9	82.3	71.4				NSI
HUD1038	330151	6619668	54.8	-15	91.3	218.9	71.4	73	1.6	23.83
HUD1039	330151.3	6619669	55.4	1	82	155.5	79.5	85.5	6	5.04
							88.5	89.5	1	10.7
							94.7	95.7	1	6.61
							101	102	1	5.34
							105	106	1	8.89
HUD1040	330151.3	6619670	55.5	0	69.7	128.4	41	42	1	18.8
HUD1041	330148.7	6619665	55.4	0	169	363.7				NSI
HUD1042	330216.7	6619750	194.0	4	115	179.4	140.2	140.8	0.6	6.58
							154	154.6	0.6	8.24
HUD1043	330145.4	6619818	228.7	-20	185.5	59.3	50.1	51.8	1.7	4.71
							54	54.6	0.6	27.7
HUD1044	330145.4	6619818	229.2	-0.5	185.5	64.2	30.1	33.6	3.5	3.02
HUD1045	330145.4	6619818	230.0	17.5	185.5	66	33.3	34.3	1	6.71
							26.9	27.6	0.7	4.95
HUD1046	330144.4	6619818	228.4	-22.2	208.4	47.4	36.3	41.5	5.2	40.94

Hole ID	AMG East	AMG North	AMG RL	Dip	Azimuth	Depth (m)	From (m)	To (m)	DH Width (m)	Grade (g/t au)
HUD1047	330144.5	6619818	229.1	-2	208.4	74.2	24.9	27.3	2.4	8.51
							37	39.45	2.45	4.08
							43.7	45.3	1.6	25.62
							48.5	49.1	0.6	3.59
HUD1048	330144.6	6619818	230.1	16	208.4	62.6	30.3	30.6	0.3	7.72
							34	35	1	4.61
							39.4	40	0.6	5.07
HUD1049	330143.3	6619818	228.3	-19.5	229.5	26.5				NSI
HUD1050	330143.3	6619818	229.3	1	229.5	74.1	9.8	10.2	0.4	3.89
							25	26.1	1.1	56.65
							28.3	31.55	3.25	164.33
							36.3	37	0.7	4.12
							45	47.2	2.2	3.21
HUD1051	330143.3	6619818	230.6	20	229.5	69	14.5	15.1	0.6	4.56
							19.25	22	2.75	36.05
							30.5	35.6	5.1	40.18
HUD1052	330150.9	6619669	56.4	-22.5	93.2	252				NSI
HUD1053	330150.9	6619669	56.4	-25.5	86.1	222	14	16	2	7.73
HUD1054	330150.9	6619669	56.4	22.8	91.3	147				NSI
HUD1055	330150.9	6619669	56.4	17.4	102.4	188.9				NSI
HUD1056	330150.9	6619669	56.4	-2.3	96.2	205	76.2	77	0.8	5.1
HUD1057	330150.9	6619669	56.4	12.6	109.5	228				NSI
HUD1058	330310.5	6619842	105.6	0	358.4	214.1				NSI
HUD1059	330310.5	6619842	105.6	0	60.5	183				NSI
HUD1060	329930.5	6619772	28.0	14.1	282.1	114.1				NSI
HUD1061	329930.5	6619772	28.0	23.9	317.1	80.2				NSI
HUD1062	329935.2	6619767	26.5	6.5	187.0	329.9	86	87	1	5.18
HUD1063	329933.6	6619808	27.5	-10	7.3	395.8	389	390	1	4.31

Analysis by 30g Fire Assay

Results compiled by using a 3.5g/t cut-off grade, no top-cut grade,
Maximum of 2m internal dilution, minimum interval of 0.3m

Appendix 2: Maps showing the collar locations of the 2014 DD at Homestead

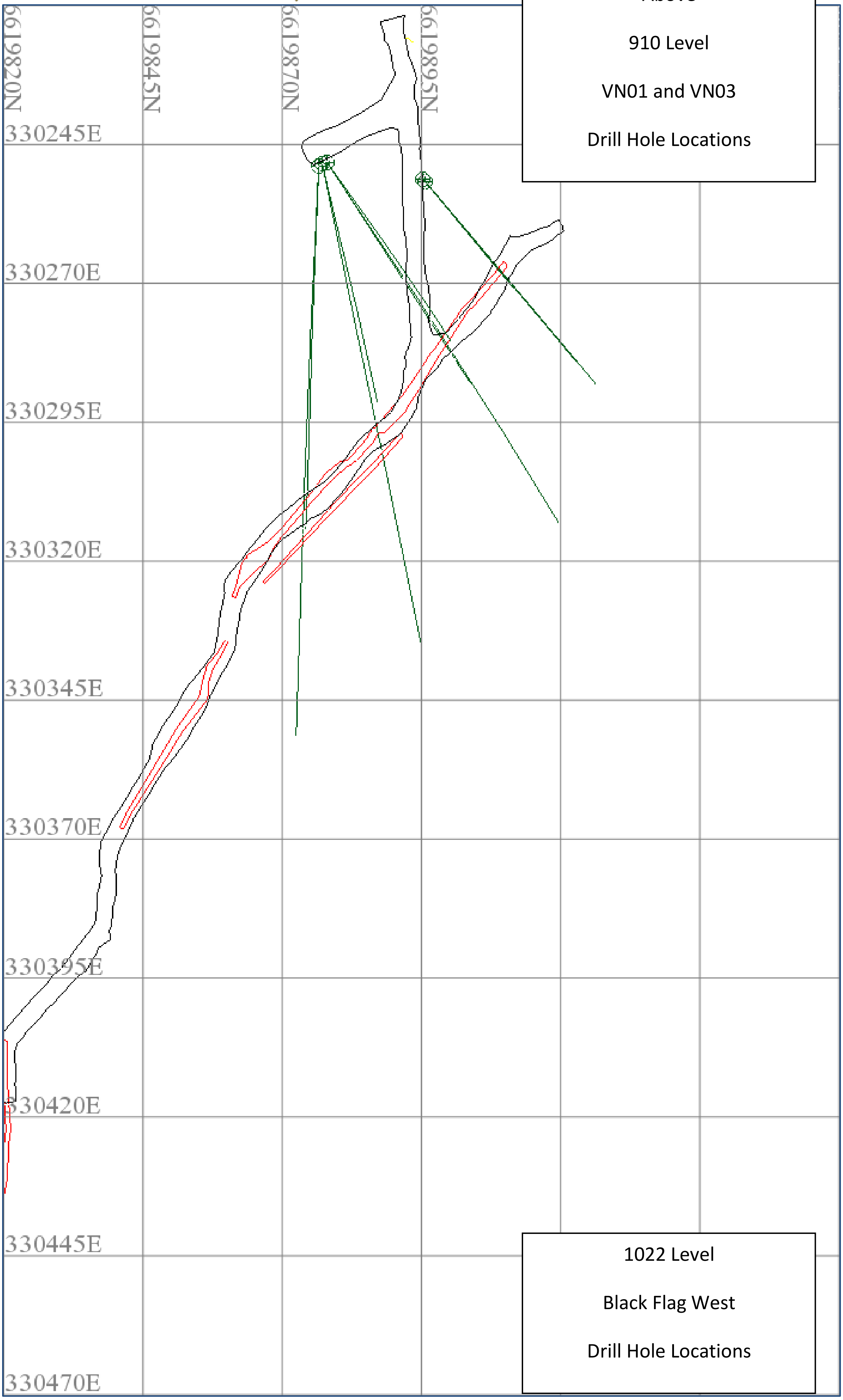


Above

910 Level

VN01 and VN03

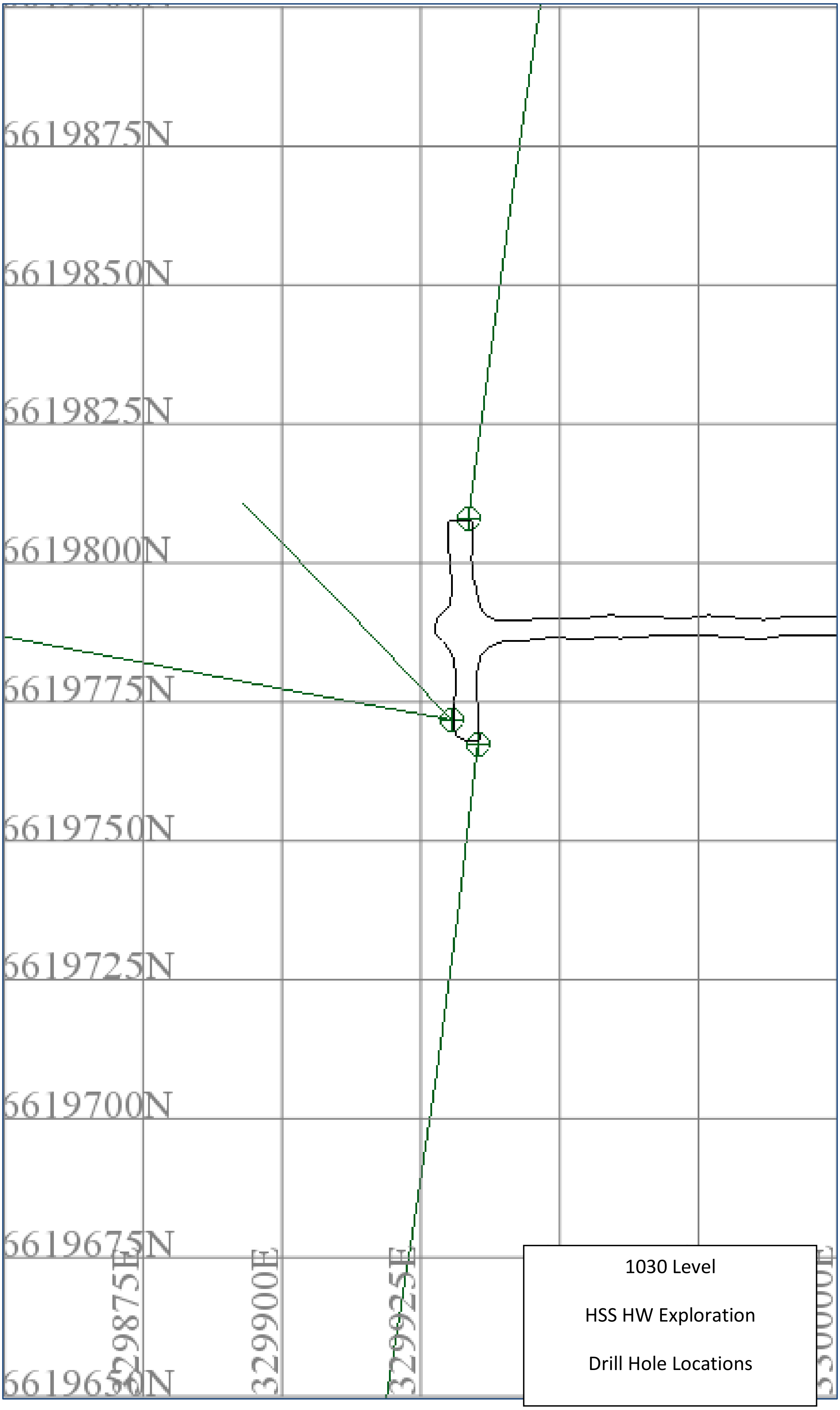
Drill Hole Locations



1022 Level

Black Flag West

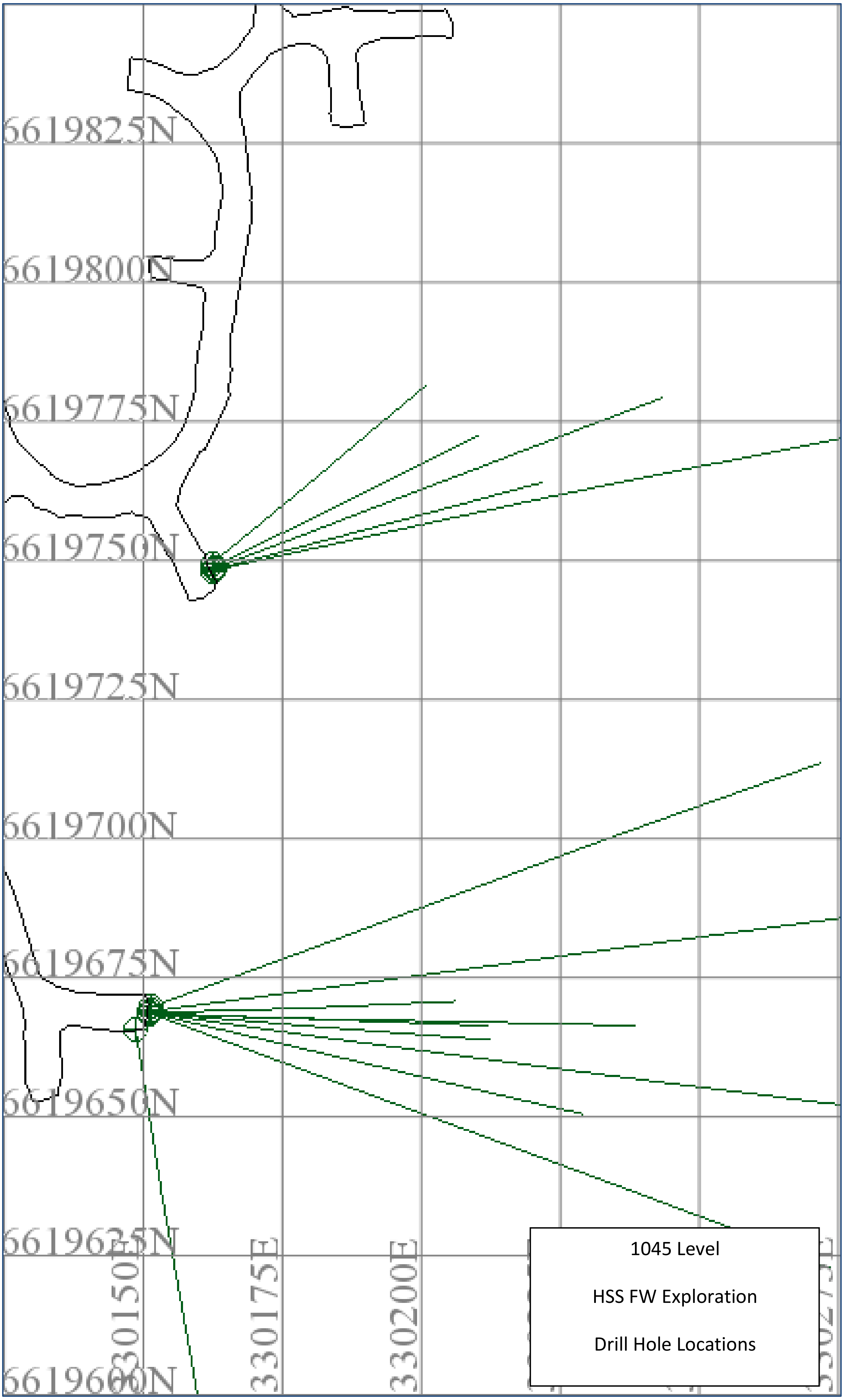
Drill Hole Locations



1030 Level

HSS HW Exploration

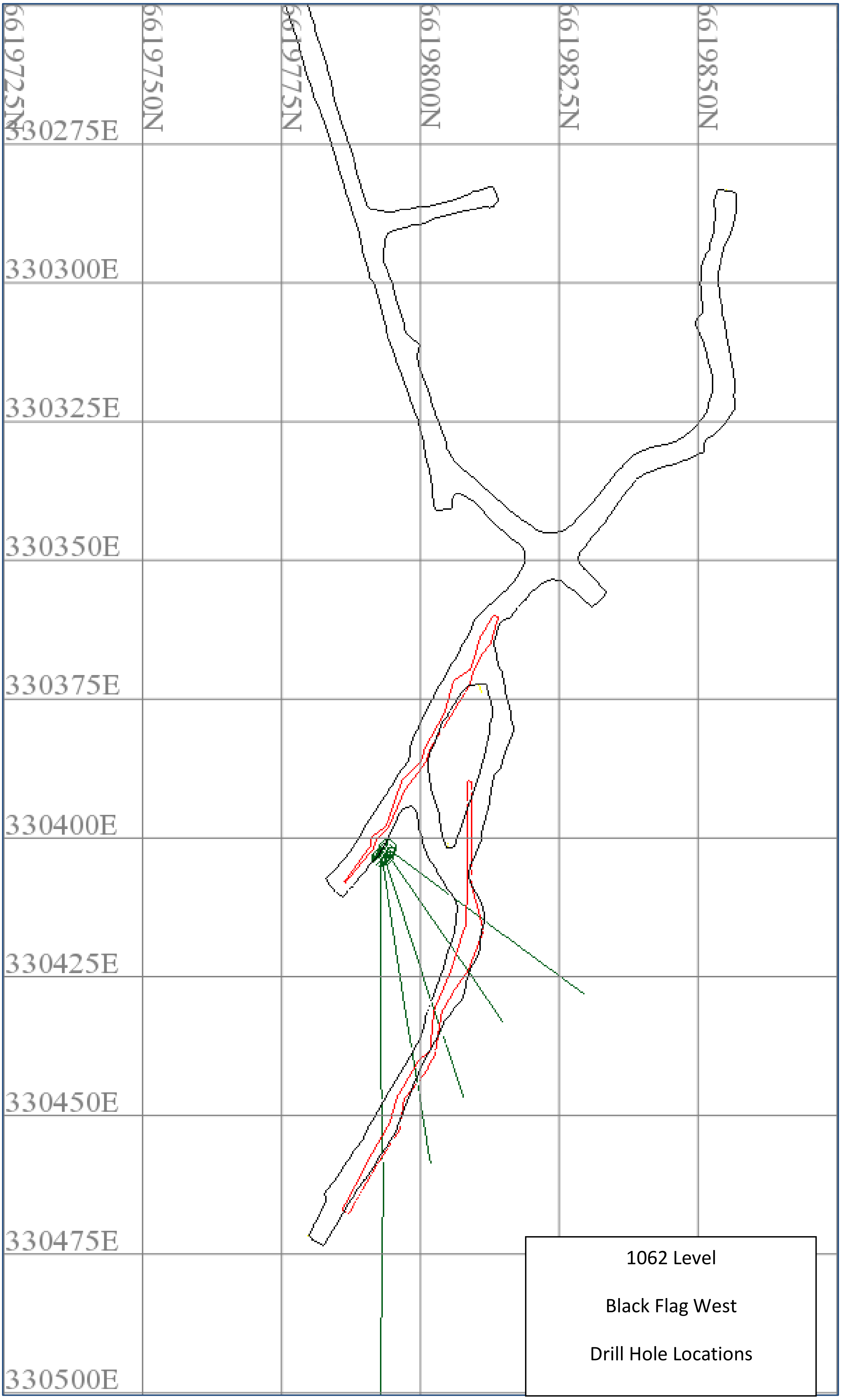
Drill Hole Locations



1045 Level

HSS FW Exploration

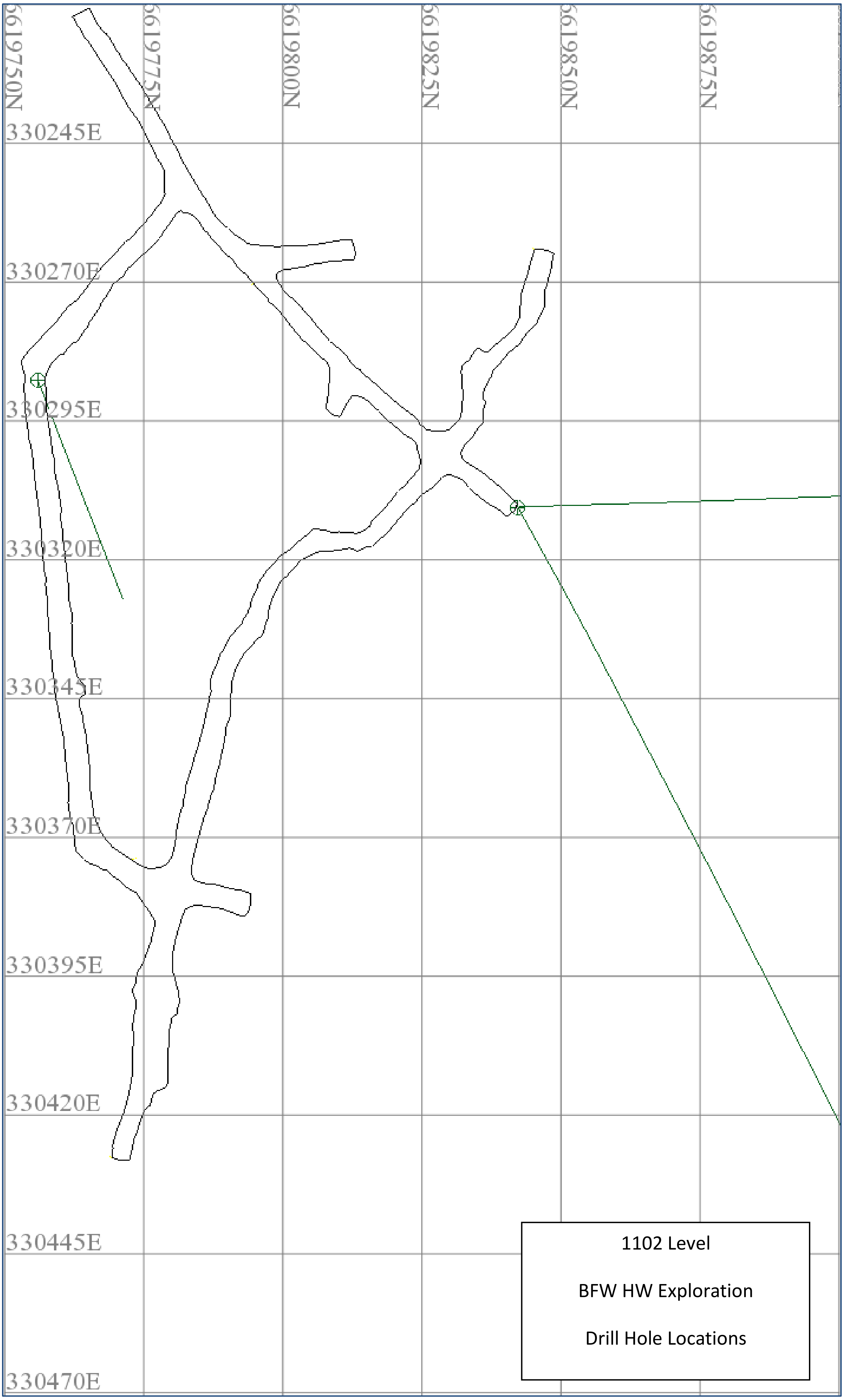
Drill Hole Locations



1062 Level

Black Flag West

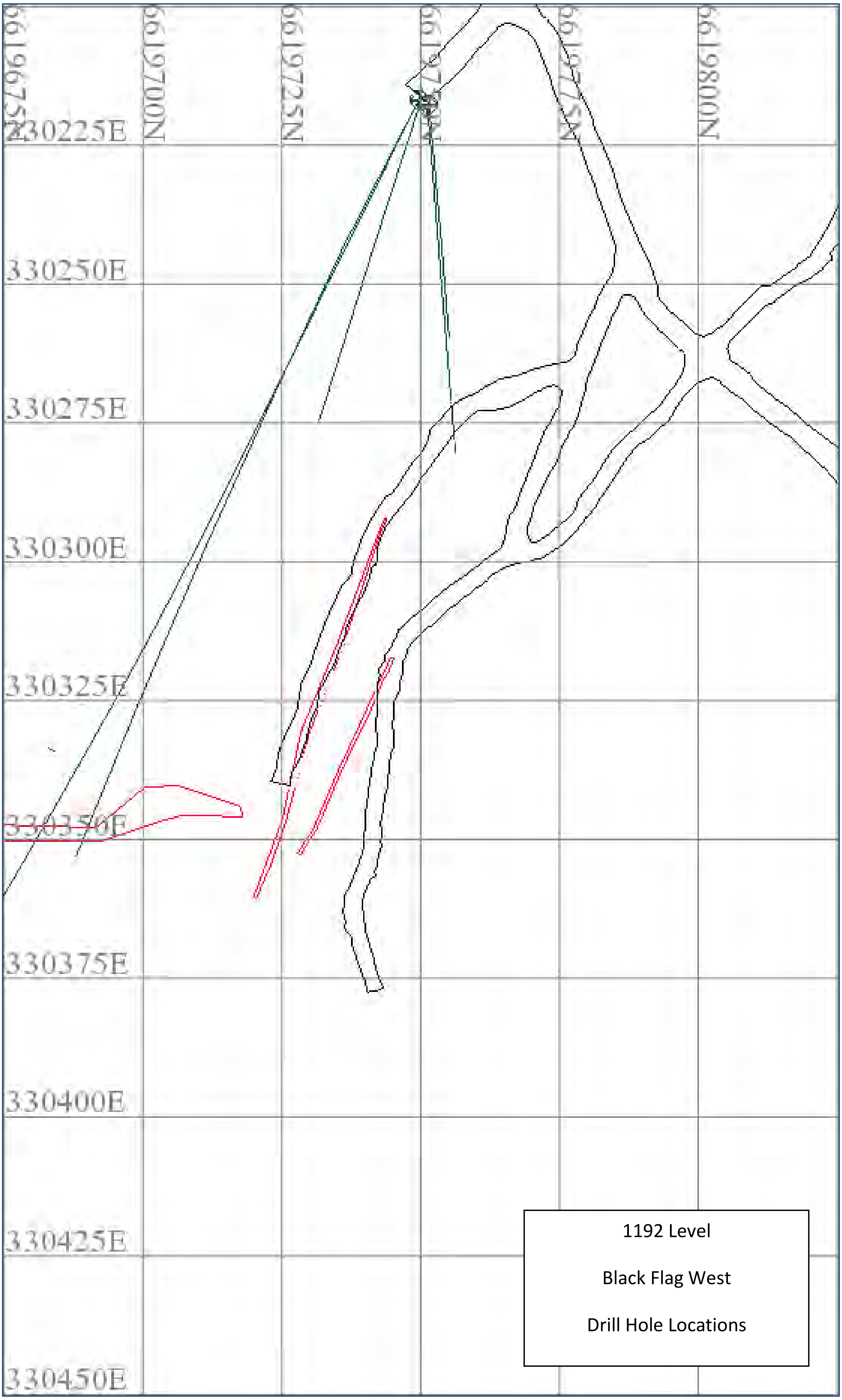
Drill Hole Locations



1102 Level

BFW HW Exploration

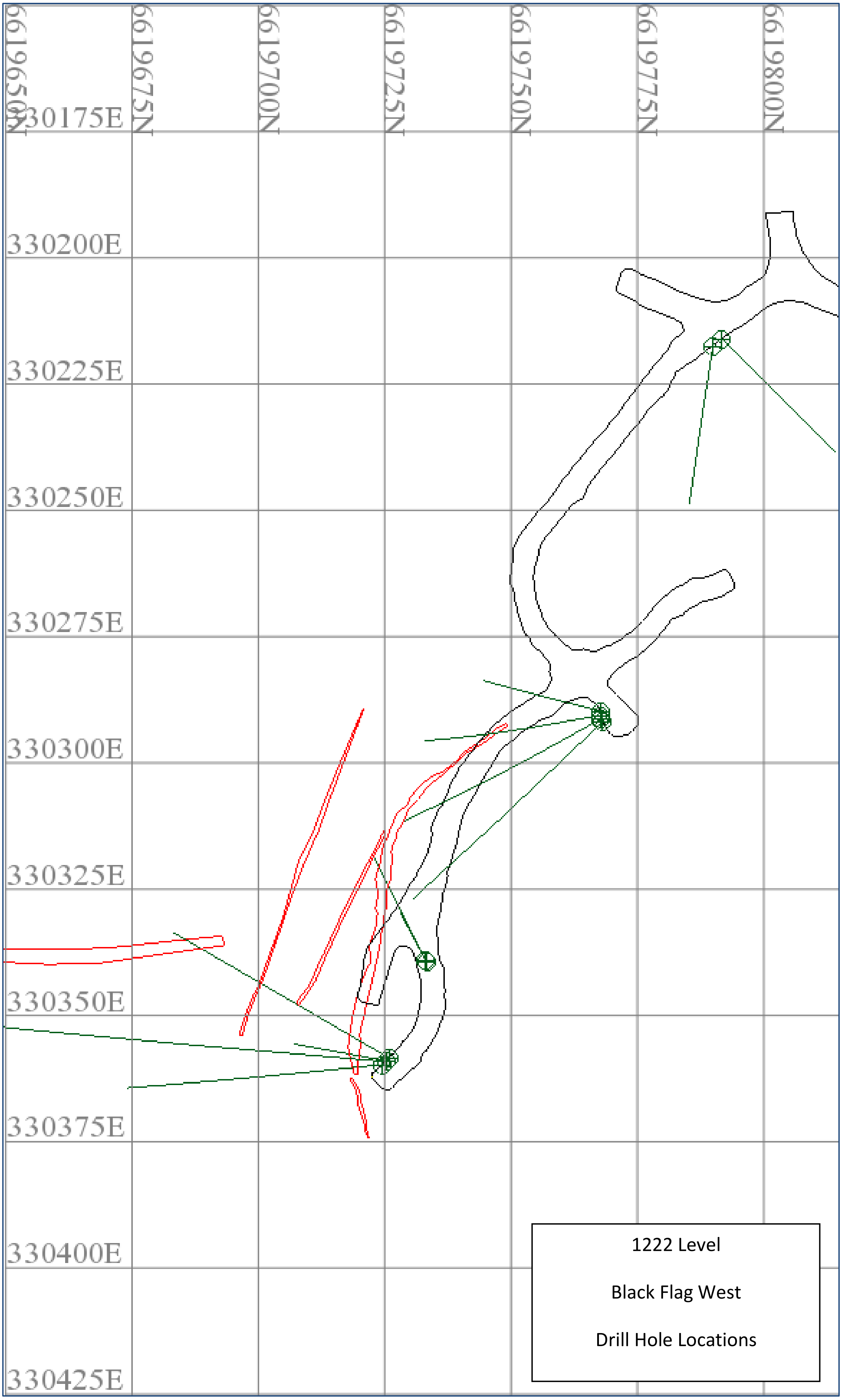
Drill Hole Locations



1192 Level

Black Flag West

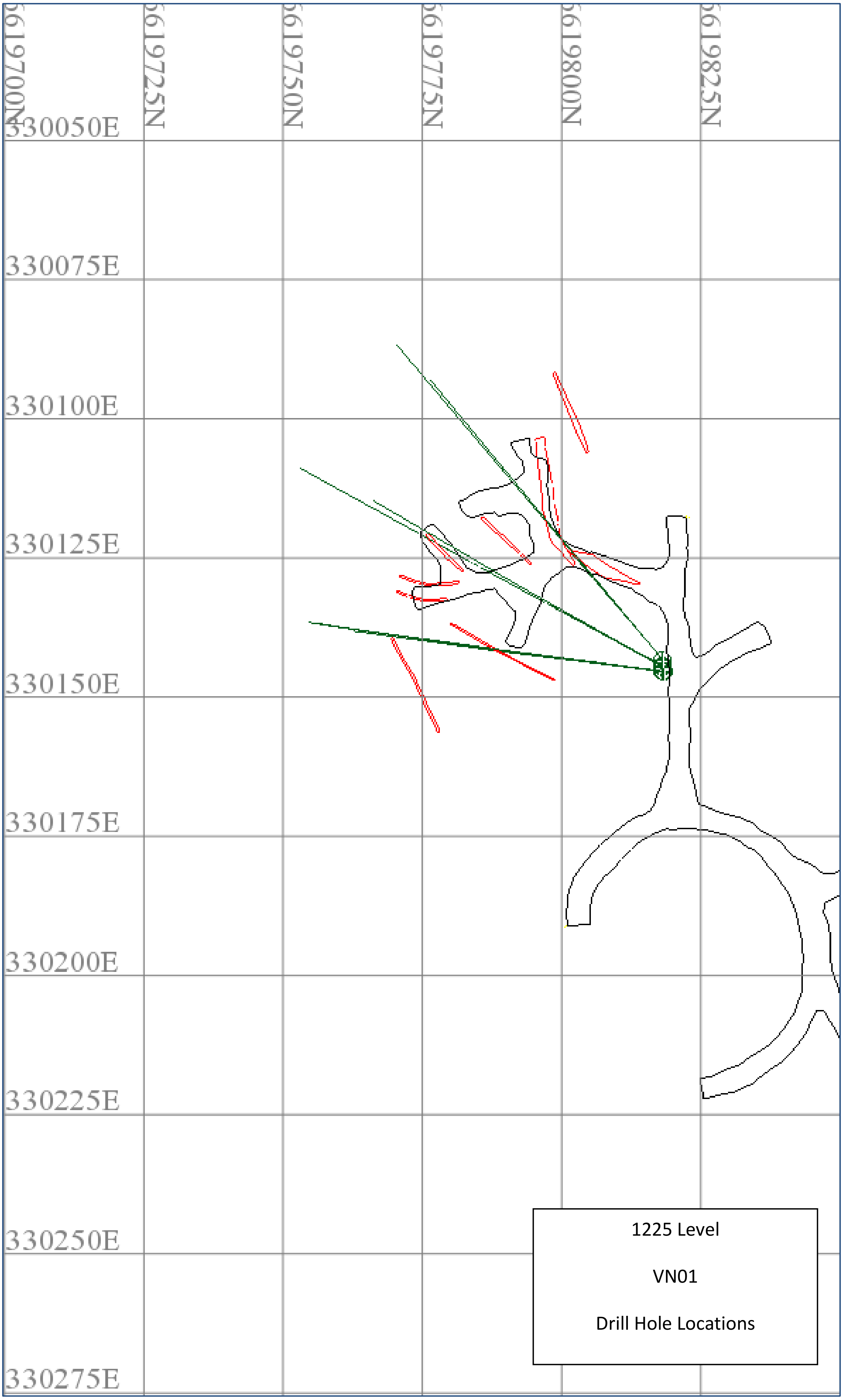
Drill Hole Locations



1222 Level

Black Flag West

Drill Hole Locations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6198250N
330050E
330075E
330100E
330125E
330150E
330175E
330200E
330225E
330250E
330275E
1225 Level
VN01
Drill Hole Locations

JORC Code, 2012 Edition – Table 1 Report for Enterprise Underground Resource and Reserve Estimate – December 2014

Section 1 Sampling Techniques & Data

Criteria	Commentary
Sampling techniques	• Sampling completed utilising a combination of Reverse Circulation (RC) & Diamond Core (DC) holes on 25m x 25m to 50m x 50m grid spacing. Drilling & sampling has been conducted by various companies since 1992 & includes exploration & resource development. Sampling techniques are summarised from drilling & sampling manuals/reports from Centaur Mining & Exploration, Goldfields Exploration, Placer Dome Asia Pacific, Barrick & Norton Gold Fields. Drilling & sampling conducted by Newcrest (1992-1997) is considered as legacy data due to the missing detail of the dataset. The Newcrest drilling accounts for 58% of the dataset. The legacy data was used to generate resource estimates forming the basis of reserve estimates & subsequent mining between 1994 & 1996. Reconciliation data from this mining period & further RC & DC twinning in 2012-2013 was used to assist with determining the integrity of the legacy data. • The drill hole locations were designed & oriented to allow for spatial spread of samples across mineralised zones & different rock types. • Field based observations from geological supervision & geological records referring to sample quality, moisture content & recovery were used as a guide to sample representivity. • All RC-recovered samples were passed through a splitting device (cone or riffle splitter) at 1m intervals to obtain a sample for assay, collected in an appropriately-sized calico bag. Target RC calico sample weights range from 2.5 to 4kg across all RC drilling campaigns (1992-2013). Bulk reject sample was also collected into a plastic bag for each metre. Spear samples, composited to 4m or less, were collected from the bulk samples as a first-pass sampling technique. Single metre samples were collected & submitted for assay from areas of expected mineralisation or composite anomalism. • DC samples were placed into core trays at the rig & transferred to core processing facilities for logging, sawing/splitting & sampling. The DC samples are collected at nominated intervals by a Geologist from resultant half core with a minimum interval of 0.2m & a maximum of 1m. • Samples were submitted to commercial laboratories for assay. Sample preparation, summarised for all drilling campaigns (1992-2013), included all or part of: oven dry between 85°C & 105°C; jaw-crushing for DC (nominal 10mm) & splitting to 3.5kg as required; pulverize sample to >85% passing 75um, from which a 30g (current) or 50g (historic) fire assay charge was analysed via Atomic Absorption Spectrometry (AAS) finish.
Drilling techniques	• All assays referred to for resource estimation (1992-32013) were collected from either RC (36% of the dataset) or DC (64% of the dataset) drilling using a drilling contractor. The most recent drilling campaign accounts for around 17% of the total drilling dataset.

Criteria	Commentary
	• RC sampling completed using a 4.5” to 5.5” diameter drill bit with a face sampling hammer (1992 to 2013). RC drilling rigs were equipped with a booster compressor. DC sampling is a combination of HQ (63.5mm diameter) and/or NQ2 (50.5mm diameter) or NQ3 (45mm) core sizes (1997 to 2013). DC is orientated by either a bottom of hole spear, EZI-Mark or ACE system. • In the case of utilising diamond tails, RC pre-collars are up to 180m deep. This technique was employed to effectively drill down to the mineralisation & collect DC through this zone.
Drill sample recovery	• RC Drillers are advised by geologists on the ground conditions expected for each hole and instructed to adopt an RC drilling strategy to maximize sample recovery, minimize contamination & maintain required spatial position. • All RC 1m samples are collected into a UV resistant bag. Samples are visually logged for moisture content, estimated sample recovery & contamination. The DC samples are orientated, length measured & compared to core blocks denoting drilling depths by the drilling contractor. Any recovery issues are recorded. Sample loss or gain is reviewed at the time of drilling & feedback is provided to the drilling contractor to ensure the samples are representative. All samples sent to the laboratory are weighed & monitored to ensure that they are representative. • DC contractors use a core barrel & wire line unit to recover the DC, adjusting drilling methods & rates to minimize core loss (e.g. changing rock type, broken ground conditions etc.). • A study of the weights of the 1m RC sample splits & gold grades (2012-2013 drilling) show no correlation between the two. The drilling contractors utilized drilling techniques to ensure minimal loss of any size fraction.
Logging	• All current RC samples are geologically logged at 1m intervals, which is an appropriate level of detail to support Mineral Resource estimation; in some historical RC drilling samples were selectively logged. Currently, each interval is inspected & the following parameters are recorded: weathering, regolith, rock type, alteration, mineralisation & structure. All drill core is logged for core loss, marked into 1m intervals, orientated, structurally logged, geotechnically logged & geologically logged for the following parameters: weathering, regolith, rock type, alteration, & mineralisation. • Geological logging is qualitative & quantitative in nature. • All RC holes are logged in their entirety on a 1m interval basis. Where no sample is returned due to voids or lost sample, it is logged & recorded as such. DC is also logged over its entire length & any core loss or voids are recorded.
Sub-sampling techniques & sample preparation	• Assays from DC are all half core samples, the remaining DC resides in the core tray & archived. • All RC samples were split by a cone or a riffle splitter & collected into a sequenced calico bag. For historical drilling, any wet samples that could not be riffle split initially were dried then usually riffle split. • The sample preparation conducted by commercial laboratories involves jaw crushing to nominal <10mm (DC), a riffle split to 3.5kg as required, & pulverising in a one stage process to >85% passing 75um. The bulk pulverized sample is then collected & approximately 200g

Criteria	Commentary
	extracted by spatula to a numbered paper bag that is used for the 30g or 50g fire assay charge. Laboratory Quality Control (QC) includes duplicate samples collected after the jaw crushing stage, & repeat samples collected after the pulverising stage to provide data confirming the appropriateness of the sample preparation technique. All sub-subsampling & lab preparations are consistent with other laboratories in Australia. • RC & DC samples submitted to the laboratory are sorted & reconciled against the submission documents. Routine CRM (standards & blanks) are inserted into the sampling sequence at a rate of 1:25 for standards & 1:75 for blanks or in specific zones at the Geologist's discretion. The commercial laboratories complete their own QC check. Specific diamond drilling campaigns utilized barren quartz flushes between expected mineralized sample interval(s) when pulverising. • RC field duplicate data was collected routinely & for selected intervals suspected to contain mineralisation. Field duplicate samples were taken at the time of cone/riffle splitting the bulk sample at the rig to maintain sample support. The field duplicates are submitted for assay using the same process mentioned above, with the laboratory unaware of the duplicate nature. Some historic DC duplicates were taken by re-sampling ¼ of the remaining half core. • Sample sizes are considered appropriate to the grain size of the material being sampled on the basis of satisfactory duplicate correlations at all stages of the sample comminution process.
Quality of assay data & laboratory tests	• The assay method is designed to measure total gold in the sample. The laboratory procedures are considered appropriate for the testing of gold at this project, given its mineralisation style. The technique involved using a 30g, 40g or 50g sample charge with a lead flux, which is decomposed in a furnace, with the prill being totally digested by 2 acids (HCl & HN03) before measurement of the gold content by an AAS machine. • No geophysical tools or other remote sensing instruments were utilised for reporting or interpretation of gold mineralisation. • Standard procedures are to examine any erroneous QC result (a result outside of expected statistically derived tolerance limits) & validate if required; establishing acceptable levels of accuracy & precision for all stages of the sampling & analytical process.
Verification of sampling & assaying	• Independent verification of significant intersections not considered material. • An analysis of 7 NGF drill holes within 15m of Centaur Mining & Exploration & Newcrest Mining drill holes was completed in 2012. Comparison of relatively close-spaced drill holes attempted to measure the reliability of the incumbent sampling & assaying data. • In 2013, a program of 5 RC holes for 814m was completed to specifically twin 2 RC & 3 DC holes, completed by Newcrest Mining (drilled between 1992 & 1995), to verify Newcrest sampling & assaying. The basis for selecting the Newcrest Mining drill holes for twinning was to compare results from different drill & material types. • Primary logging & sampling data is sent digitally every 2-3 days from the field to the company's Database Administrator (DBA). The DBA imports the data into a relational DataShed database. When assay results are received electronically from the laboratory, results &

Criteria	Commentary
	laboratory QAQC are also imported into the database after further validation checks. The responsible Geologist reviews the data in the database to ensure that it is correct & has merged properly & that all data has been received & entered. Any variations that are required are recorded permanently in the database. • No adjustments or calibrations were made to any assay data used in this report.
Location of data points	• All drill holes used in the resource estimation have been surveyed for easting, northing & reduced level. Recent data is collected in MGA 94 Zone 51 & AHD. Data pre-2012 is collected in AMG 84 Zone 51 & AHD. • Drill hole collar positions are surveyed by the site-based survey department (utilsing a differential GPS or conventional surveying techniques, with reference to a known base station) with a precision of less than 0.2m. • Down hole surveys consist of regular-spaced Eastman single or mutli-shot borehole camera, & digital electronic multi-shot surveys (generally <30m apart down hole). A minor amount of historic drill holes only have collar surveys. Ground magnetics can affect the result of the measured azimuth reading for these survey instruments at Enterprise. Thirteen per cent of survey data consists of surveys taken with north-seeking gyro instruments, representing more recent drilling. Gyro survey measurements are obtained every 5m down hole. • Topographic control was generated from survey pick-ups of the area over the last 19 years, which have been used to generate a Digital Terrain Model (DTM).
Data spacing & distribution	• The nominal drill spacing is 25m x 25m with some areas at 50m x 50m to around 0mRL & increasing to 50m x 100m down to -200mRL. This spacing includes data that has been verified from previous exploration activities on the project. • Data spacing & distribution is considered sufficient for establishing geological continuity & grade variability, appropriate for classifying a Mineral Resource. • Samples were composited to 2m down hole prior to modelling to assist with the effects of volume variance & decrease grade variability.
Orientation of data in relation to geological structure	• Mineralisation is considered to be encased by two sub-parallel EW striking faults, with an upper boundary consisting of the Cashman's Sedimentary Horizon. The ore envelope strikes broadly EW with a plunge of approximately 23°. This regime resulted in an ore shoot plunge that is approximately 150m wide, 130m high, with a strike extent of 1,000m, dipping at 23° to the west. Drilling is oriented either north or south, intersecting the envelope at a high angle, which enables sampling to be representative of true width of the mineralisation. • No drilling orientation & sampling bias has been recognized at this time.
Sample security	• Historic samples are assumed to have been under the security of the respective tenement holders/operators until delivered to the commercial laboratory where samples would be expected to have been under restricted access.

Criteria	Commentary
	• Samples collected between 2012 & 2013 were all under the security & custodial chain of NGF employees until delivered to ALS Kalgoorlie laboratory some 30km south, where they were received in a secured fenced compound security with restricted entry. Internally, ALS operates an audit trail, tracking the samples at all times whilst in their custody.
Audits or reviews	• Internal reviews are completed on sampling techniques & data as part of the Norton Gold Fields continuous improvement practice. No external or third party audits or reviews have been completed.

Section 2 Reporting of Exploration Results

Criteria	Commentary
Mineral tenement & land tenure status	• The Enterprise deposit is located within Mining License M24/170. M24/170 is 100% held by Paddington Gold P/L, a wholly owned subsidiary of Norton Gold Fields P/L. A Miscellaneous License cross cuts the tenement (L24/30 held by Norilsk Nickel Cawse PL). No heritage or historical sites exist within the tenure. M24/170 was granted pre-Native Title. Third party royalties are applicable to these tenements & are based on production ($/t) or proportion of net profit. All production is subject to a WA state government NSR royalty of 2.5%. • The tenement is in good standing & no known impediments exist.
Exploration done by other parties	• A significant proportion of exploration, resource development & mining was completed by companies which held tenure over the Enterprise deposit since the mid 1980's. Companies included: Broken Hill Proprietary Limited (pre 1992), Newcrest Mining PL (1992-1997), Centaur Mining & Exploration PL (1997-2001), Goldfields Exploration (2001-2002), Placer Dome Asia Pacific (2002-2005) & Barrick Kanowna (2005-2007). Results of exploration & mining activities by the afore-mentioned companies has assisted in Norton Gold Field's more recent exploration, resource development & mining in the area.
Geology	• The deposit type is classified as an orogenic gold deposit within the Norseman-Wiluna greenstone sequence. The accepted interpretation for gold mineralisation is related to (regional D2-D3) deformation of the stratigraphic sequence during an Archaean orogeny event. The mineralisation is hosted within the Enterprise Dolerite (a differentiated sill) of the Kalgoorlie stratigraphy. The metamorphic grade is defined as lower green-schist facies. • The mineralisation is located in brittle-ductile shear zones typically associated with sericite & muscovite alteration +/- sulphides.
Drill hole Information	• Not Applicable
Data aggregation methods	• All reported assay results have been length-weighted; no top cuts have been applied. Assay results are reported to a 0.8g/t Au lower cut over a minimum intersection of 1m for RC & 0.2m for DC

Criteria	Commentary
	• A maximum of 2m of internal dilution (i.e. <2m @ <0.8g/t Au) is included for reporting RC intercepts targeting oxide mineralisation & for DDH intercepts targeting the fresh rock mineralization. • No metal equivalent values are used for reporting exploration results.
Relationship between mineralisation widths & intercept lengths	• Drill hole intersections are generally at a high angle to each mineralised zone. Reported down hole intersections are noted as approximately true width, or otherwise are denoted as 'true width not known'.
Diagrams	• See Appendix 1
Balanced reporting	• All results have been reported relative to the intersection criteria.
Other substantive exploration data	• No other exploration data collected is considered material to this announcement. Such factors are well understood & derived from recent mining history of the deposit.
Further work	• The deposit is currently being mined. Further work will include mining studies to determine if the project economics can support underground mining of the deposit.

Section 3 Estimation & Reporting of Mineral Resources

Criteria	Commentary
Database integrity	• NGF employs SQL as the central data storage system using Data shed software as a front-end interface. User access to the database is regulated by specific user permissions, & validation checks & relational steps are part of the process to ensure data remains valid • Existing protocols maximize data functionality & quality whilst minimizing the likelihood of error introduction at primary data collection points & subsequent database upload, storage & retrieval points. Data templates with lookup tables & fixed formatting are used for collecting primary data on field laptops. The software has validation routines & data is subsequently imported into a secure central database. • The SQL server database is configured for validation through constraints, library tables, triggers & stored procedures. Data that fails these rules on import is rejected or quarantined until it is corrected. • The Database is centrally managed by a Database Manager who is responsible for all aspects of data entry, validation, development, quality control & specialist queries. There is a standard suite of vigorous validation checks for all data.

Criteria	Commentary
Site visits	• The Competent Person for this update is a full time employee of NGF & undertakes regular site visits ensuring industry standards of the Mineral Resource estimation process from sampling through to final block model. • The deposit area is an active mining area for NGF & as such regular site visits were undertaken during this update.
Geological interpretation	• The high confidence of the geological interpretation is based on geological knowledge acquired from the open pit production data, detailed geological DC & RC logging, assay data & pit mapping. • The dataset (geological mapping, RC & DC logging, assays etc.) is considered acceptable for determining a geological model. Key interpretation assumptions made for this estimation are: (1) where geological relationships were interpreted but not observed; & (2) the interpretation of the mineralisation past known drilling limits (extrapolated a reasonable distance considering geological & grade continuity – not more than the maximum drill spacing). • The geological interpretation is considered robust & alternative interpretations are considered not to have a material effect on the Mineral Resource. No alternate interpretations are proposed as geological confidence in the model is high. As additional geological data is collated, the geological interpretation is continually being updated. • The geological interpretation is specifically based on identifying, favourable stratigraphy within the Enterprise Dolerite, particular geological structures, associated alteration, veining & gold content. • Whilst the geological features are deemed to be continuous, the gold distribution within them can be highly variable. This issue is mitigated by close-spaced sampling & ensuring sample & analytical quality is high. Historic mining data is also used to assist with understanding grade continuity. Geological structures post-dating the mineralization can off-set & truncate the mineralisation affecting the geological continuity & are difficult to isolate.
Dimensions	• The Enterprise deposit is spatially located between 315,000mE & 316,540mE & 6,637,900mN to 6,638,800mN (AMG84 zone51). 8 domains were modeled (including a waste domain) & 3 subdomains (based on regolith profiles). • Mineralisation is controlled by structural & stratigraphic features that have a known plunge extent of 1,000m (starting from surface), -23° to the west. The plunge shoot is up to 150m wide & 130m high.
Estimation & modelling techniques	• The estimation was completed using a linear estimation technique - Ordinary Kriging (OK). OK is an estimation method where a single direction of continuity is modelled for each domain for a global grade estimate. An advantage of OK is the statistically unbiased weighting of composite samples to generate an estimate. A disadvantage is the use of this technique on variable, skewed datasets leading to conditional bias when reporting the resource at increasing cut-off grades. • Geological domains were based on the geological interpretation & mineralised trends. 3DM wireframes were generated by sectional interpretation of the drilling dataset orthogonal to the mineralisation. Where there was geological uncertainty, domain boundaries were modelled to a 0.3 g/t Au lower cut. Domain boundaries were treated as hard boundaries.

Criteria	Commentary
	• 2m down hole composites for all drilling were created & subdivided into each domain using an inside 3DM/outside 3DM principle. • The statistics for each domain were viewed & key univariate statistical indicators used to describe the nature of each. Each domain showed a positively skewed data distribution with high-grade outlier composites. A top-cut of 22.5g/t Au was applied to all domains by viewing grade distribution histograms, where the continuity of the higher-grades diminished. • Sample search ellipses were set based on data spacing in similar orientation to the major mineralized orientation. Minimum & maximum samples were set for each sample search based on accepted levels of grade continuity. Search distances were based on sample spacing & spatial continuity. A total of 3 search passes were conducted with progressively relaxed search criteria to accommodate the data density from the closest to the widest spaced drilling at 50m x 100m. • Estimation was completed using Surpac V6.3 mining software, utilizing the block modelling module. • The open pit (MIK) check estimate (utilising the same data) was used to compare against the estimation result. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered material to this style of mineralisation. • Block model dimensions were set to 315,000mE & 316,540mE & 6,637,900mN to 6,638,800mN & between 550mRL & -250mRL. Block sizes were chosen to compromise between sample spacing & representing the mineralised volume i.e. 5m(X) by 5m(Y) by 5m(Z). • This resource estimate is to be used for both open pit & underground mining studies & as such, no SMU were assumed. • No correlation between variables was necessary. • The 3DM/DTM wireframes for the estimation domains, regolith & topographical files were used to constrain the resource estimate. Blocks from the block model were coded based on these volumes/surfaces by either block centroid in/out of 3DM or above/below a DTM surface. • Model validation has been completed using visual & numerical methods & formal peer review sessions by key geology staff. • Mineral Resource Model has been validated visually against the input composite/raw drill hole data with sufficient spot checks carried out on a number of block estimates on sections & plans. • Swath plots have been generated on section eastings to check input composited assay means for block estimates within swath windows. OK estimates have also been checked against an alternate MIK estimates.
Moisture	• Tonnages are estimated on a dry basis.
Cut-off parameters	• Cut-off parameters are 1.5g/t Au for the resource estimate west of 315,750mE (likely UG). Cut-off parameters are based on current NGF mining (underground) & milling costs.
Mining factors or assumptions	• The western portion of the resource is likely to be mined utilizing bulk underground mining methods. • Mining methods are based on current open pit & underground mining operations for NGF.

Criteria	Commentary
Metallurgical factors or assumptions	• No assumption or factors have been applied to the resource estimate regarding the metallurgical amenability. • Reasonable assumptions for metallurgical extraction are based on metallurgical test work from DC. • Target gold recovery is expected to be 85% for fresh rock ore.
Environmental factors or assumptions	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining & milling history of existing open pit & underground operations with the project area.
Bulk density	• Insitu-bulk densities (ISBD) (dry basis) applied to the resource estimate were based on systematic test work completed on hand specimens & DC for selected material types. The ISBD determination method is based on a water immersion technique. The ISBD test work reconciles against production tonnages from historic & current mining operations within the project area. • Samples that were porous were sealed by various methods & accounted for in the bulk density calculation.
Classification	• The models & associated calculations utilised all available data & are depleted for known workings. • NGF follows the JORC classification system with individual block classification being assigned statistical methods & visually taking into account the following factors: ○ Drill spacing & orientation; ○ Classification of surrounding blocks; ○ Confidence of certain parts of the geological model; and ○ Portions of the deposit that are likely to be viably mined. • The classification result reflects the view of the Competent Person.
Audits or reviews	• The Mineral Resource has been not been externally audited. An internal Norton Gold Fields peer review has been completed as part of the resource classification process.
Discussion of relative accuracy/ confidence	• The Mineral Resources have been reported in accordance with the guidelines of the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources & Ore Reserves & reflects the relative accuracy of the Mineral Resources estimate. The Competent Person deems the process to be in line with industry standards for resource estimation & therefore within acceptable statistical error limits. • The statement relates to global estimates of tonnes & grade for likely separate open pit & underground mining scenarios. • Historic production data was used to compare with the resource estimate (where appropriate) & assisted in defining geological confidence & resource classification categories.

Section 4 Estimation and Reporting of Ore Reserves

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• A financial evaluation, underground life of mine design and schedule was completed for Enterprise UG by NGF personnel in December 2014.The development and stope design parameters are based on existing NGF underground procedures. The scheduled life of mine reserves consist of probable reserves of 1.63Mt @ 3.10g/t Au at a break even cutoff grade of 2.12g/t. • The Mineral Resources are reported inclusive of the Ore Reserves.
Site visits	• Enterprise Open Pit is currently an active mine site which has been in operation since May 2013. • Enterprise Open pit have been visited by Guy Simpson (GM Technical Services "NGF" & CP for Reserves) within the last 6 months and whilst he was seconded as Deputy GM Operations in Quarter Four 2013.
Study status	• NGF Technical Services Department undertook financial review and design of the Enterprise UG mineral deposit. The Life of Mine plan was based on a selling price of $AUD 1,400/oz with a 2.5% royalty. • The block model used for the underground design is "ent_bm_2014.bmf" • Modifying factors such as mining loss, mining dilution and recoveries have been applied • Operating cost used was based on NGF's current underground fleet with average processing cost of $20.57/t
Cut-off parameters	• A break even cutoff grade of 2.12g/t was calculated using cost from mechanized sub-level open stoping with paste and rough waste fill mining method at an annual production rate of 750Kt per annum. • The cutoff grade applied is shown by; $\text{Cut} - \text{off Grade} = \frac{\text{Mining Dilution x Processing Cost}}{\text{Processing Recovery x (Selling Price} - \text{Selling Cost)}}$ • Selling price = AUD$1,400/Oz. • State Royalty = 2.5%. • Metallurgical recovery = 83%. • Processing cost = $20.57/t.
Mining factors or assumptions	• The method used to convert Mineral resource to Ore Reserves is based upon identifying which proposed mining panels and development areas are economic.

Criteria	Commentary
	• The mining method will be mechanized sub-level open stoping with paste and rough waste fill. • NGF is an owner operator and Enterprise Open Pit is currently being mined by NGF using its operating model. • The ore reserve estimate was created using mining shapes with an allocated level of confidence. • Processing cost = $20.57/t (Including haulage from Enterprise). • Infrastructure requirement for underground mining includes; A workshop for all mobile equipment for maintenance requirements, offices, crib rooms and amenities, explosives storage, water dams and communication. All of these infrastructures are already on site and actively used
Metallurgical factors or assumptions	• Metallurgical test work was undertaken by NGF on Enterprise ore. • Ore from Enterprise is currently delivered via road trains to NGF's Paddington mill for processing. • Metallurgical extraction are based on processing Enterprise ore through the Paddington processing plant from August 2013 to present. • Ore from Enterprise UG will be delivered via road trains to NGF's Paddington mill for processing. • Paddington Mill is based on conventional carbon in pulp technology and has achieved an annual throughput of 3.72 million tonnes in 2014. The average feed grade and recovery is 1.67g/t and 88.88% respectively. • A recovery factor of 83% have been applied to Enterprise UG's ore which will be blended with Paddington's other ore sources to be able to achieve this recovery factor.
Environmental	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. • All proposed operation and operational plans are within local historical practices and existing operational standards.
Infrastructure	• The site is serviced by a haul road which is capable of handling 200t road trains. • The site has existing infrastructure including electricity, water and communications infrastructure. • The site has a fully operational office, core facility, crib rooms, explosives storage, water dams and communication.
Costs	• Enterprise UG's reserve estimate was based on a gold price of $AUD 1,400/Oz. • Allowance has been made for the 2.5% state government royalty. • Operating cost used is $52/t and $106/t without and with capital respectively. These cost are from budgeted figures used for NGF's Homestead UG mine as well as benchmarking against underground mines of similar mining method and production rates. • No penalties assumed and no deleterious elements in concentrate.

Criteria	Commentary
Revenue factors	• Financial analysis in this report is based on a gold price of $AUD 1,400/Oz. • The gold Dore is planned to be transported via recognized security service from gold room of Paddington processing plant to the gold refinery in Perth. • Contract payments and terms are expected to be typical of similar contracts for the refining and sale of Dore produced from other operations within Australia. • Allowance has been made for the 2.5% state government royalty.
Market assessment	• Historical gold price and forward looking estimates have been used for the gold price. Price flexing and sensitivity analysis have been carried out to determine the robustness of the project viability. • The cash flow was modelled in real terms and no price or cost escalations were applied.
Economic	• Inputs to economic analysis include factors described above including ore and metal quantities from mining/processing schedule (including described recovery/processing parameters), cost and price assumptions.
Social	• The majority of workforce is from Kalgoorlie. • NGF will establish all relevant agreement with local stakeholders and government agencies.
Classification	• The Ore Reserve was classified as Probable in accordance with the JORC Code, corresponding to the resource classifications of Measured and Indicated. No Inferred Mineral Resources were included in the Ore Reserve estimate. • The estimated Ore Reserves and mining method are in the opinion of the Competent Person appropriate for this style of deposit.
Audits or reviews	• The resource and reserve was calculated by NGF personnel. The cost and mining parameters were reviewed internally against existing operations and consideration was made for current practice and cost structure. • It is not expected that practices assumed in the calculation of reserve will vary before the next annual reserve calculation.
Discussion of relative accuracy/ confidence	• All mining estimates are based on Australian costs, and relevant historical cost data. • The local estimate of Ore reserves available for technical and economic evaluation is 1.63Mt @ 3.10g/t Au at a break even cutoff grade of 2.12g/t prior to processing. • There are no unforeseen modifying factors at the time of this statement that will have any material impact on the Ore Reserve estimate.

JORC Code, 2012 Edition – Table 1 Bullant Underground

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	Commentary
Sampling techniques	• Sampling completed utilising a combination of Diamond Core holes (DC), Face Sampling (FS) and Reverse Circulation (RC) holes. The drill hole locations were designed to allow for spatial spread of samples across mineralised zones and different rock types. Face sampling was performed on most of the faces from development drives. • Drilling and sampling has been conducted by various companies since 1980 including BHP Gold Mines; Newcrest Mining; Centaur; Goldfields Group; Aurion Gold; Placer Dome; Barrick; and Kalgoorlie Mining Company (KMC) and recently by Norton Gold Fields (Norton). • Drilling includes exploration, resource development and grade control sampling (DC for underground and RC for open pit). • All RC recovered samples were passed through a splitting device (cone or riffle splitter) at 1m intervals to obtain sample for assay, which was collected in an appropriately sized calico bag. Target RC calico sample weights range from 2.5 to 4kg across all RC drilling campaigns. Bulk reject sample was also collected into a plastic bag for each metre. Spear samples, composited to 4m or less, were collected from the bulk samples as a first-pass sampling technique. Single metre samples were collected and submitted for assay from areas of expected mineralisation or composite anomalism. • DC samples were placed into core trays at the rig before being bought to the core yard for processing.
Drilling techniques	• The dataset used for the Bullant resource estimate is a combination of historic data dating back to the 1980's which includes reverse circulation and surface diamond drill holes; and the new data consisting mostly of underground collared diamond drill holes and face samples from the development levels. • In the latest estimates 609 RC holes were used (20%), 613 DC holes (20%) and 1813 face sampling strings (60%). • The RC diameter used is un-known. The DC is in 11% NQ2 (47.6mm diameter core sizes), 89% of unknown diameter. • The RC drilling predominantly confined to the upper limits of the deposit including open pit grade control. • All the historic holes used in the estimation were assumed to have been processed and sampled in a similar fashion to the added KMC and Norton holes. • Recent DC holes were oriented. • The recent drilling campaigns accounts for 11% of the total DC drilling dataset.

Criteria	Commentary
	• The recent face sampling accounts for 20% of total face sampling dataset.
Drill sample recovery	• RC Drillers are advised by geologists on the ground conditions expected for each hole and instructed to adopt an RC drilling strategy to maximize sample recovery, minimize contamination and maintain required spatial position • All RC 1m samples are collected into a UV resistant bag. Samples are visually logged for moisture content, estimated sample recovery and contamination. • Sample loss or gain is reviewed at the time of drilling and feedback is provided to the drilling contractor to ensure the samples are representative. All samples sent to the laboratory are weighed and monitored to ensure that they are representative. • DC contractors use a core barrel and wire line unit to recover the DC, adjusting drilling methods and rates to minimize core loss. • The DC samples are orientated, length measured and compared to core blocks denoting drilling depths by the drilling contractor. Any recovery issues are recorded. • All recoveries are recorded in the geology Geotech Logging sheet. • Core recovery where recorded was on average 96%.
Logging	• All drill hole data was geologically logged using codes set up for direct computer input. Hole ID, interval, rock type, changes in shear intensity and changes in alteration type or the occurrence of quartz veining were recorded. • All development faces were logged before sampling. • Geological logging was qualitative and quantitative in nature. • All core was photographed after logging (and before cutting) using a digital camera. • Geotechnical information was collected from selected DC holes. Information collected includes RQD and fracture frequency. • Historical RC samples were also geologically logged. The following parameters were recorded: weathering, rock type, alteration, mineralization and structure.
Sub-sampling techniques and sample preparation	• Diamond core samples were collected at intervals nominated by a geologist from half core or whole core with a minimum interval of 0.1m and a maximum of 1.1m. Face samples were collected by channel sampling with minimum sampling interval of 0.1m and maximum of 1.3m. • Sample intervals always conform to the logged lithological boundaries. • Core which was halved for sampling was split using diamond saw, half was sampled and assayed, the remaining half resides in the core tray and archived. • Samples collected from DC are placed into pre-numbered bags and sent to the lab. The remainder of the core is stored in the core

Criteria	Commentary
	yard on Bullant mine site or in Panglo core storage facility. • Samples were taken to a commercial laboratory for assay. Historically Amdel, Analab and Genalysis laboratories were used. All recent samples (since 2010) were sent to SGS laboratory in Kalgoorlie. • All RC samples were split by a splitting device to collect sample. Recent RC samples undergone splitting in three-stage riffle splitter to achieve app. 3kg sample for each down-hole metre. Historically the first pass composite (<4m) sampling was used which utilised a spear sample collected from the bulk sample. Recently all 1m reduced samples were placed in pre-numbered calico bag and send for assay. • Samples submitted to the laboratory were sorted and reconciled against the submission documents. • The sample preparation technique for all samples followed industry best practice, by accredited commercial laboratories. The technique and practices are deemed appropriate for the type and style of mineralization. Between 2010 and 2012 the geochemical samples were dried at 100°C. Dried samples were crushed in Jaw Crusher then split in riffle splitter if they were above 4kg and pulverized to minimum 90% passing 75µm in LM5 pulveriser. 200g sample was scooped out and reduced to 50g sub sample, which entered the Fire Assay process. Since mid-2012 entire dried sample is crushed to 2mm in Boyd Crusher and then rotary split to obtain 1kg sample which was pulverized in LM2 pulveriser to 85% passing 75µm. A 200g pulp sample was scooped from LM2 out of which the catch weight sample of 30g was scooped for the Fire Assay. • Laboratory Quality Control (QC) includes duplicate samples collected after the jaw crushing stage, and repeat samples collected after the pulverising stage to provide data confirming the appropriateness of the sample preparation technique. All sub-subsampling & lab preparations are consistent with other laboratories in Australia & are satisfactory for the intended purpose.
Quality of assay data and laboratory tests	• The assay method was designed to measure total gold in the sample. The laboratory procedures are appropriate for the testing of gold at this project given its mineralization style. The Fire Assay charge of 30g was fused with a lead flux then decomposed in a furnace with the prill being totally digested by 2 acids (HCI and HN03) before measurement of the gold content by an Atomic Absorption Spectrometer. Samples were submitted in 78 sample batches including QC samples. • Routine Certified Reference Material (CRM) - standards and blanks were inserted into the sampling sequence at a rate of 1:25 for standards and 1:75 for blanks and also submitted around expected zones of mineralization. The commercial laboratories completed their own QC check. • Since 2012 barren flushes have been utilized between expected mineralised sample intervals when pulverizing DDH samples. • Historic RC drilling Quality Control procedures are not well documented. However the existing Centaur Mining and Exploration Ltd report states that Assay QC was performed for Duplicate and Replicate pulp assays; Re-split and composite assays; Standard assay checks; Fire Screen assays and Empire assays.

Criteria	Commentary
	• Any erroneous QC results were examined and validated if required; establishing acceptable levels of accuracy and precision for all stages of the sampling and analytical process. If there were any issues with any given CRM, the samples associated with the SRM were immediately re-assayed. Therefore all CRM data and their associated samples satisfy a gross tolerance before being accepted in the database.
Verification of sampling and assaying	• No holes were twinned. • Duplicate face sampling was performed on 10 faces during 2010-2012 data collection campaign. There was close correlation of two sample sets. • Primary data was sent digitally every 2-3 days from the field to NGF's Database Administrator (DBA). The DBA imports the data into the commercially available and industry accepted Data Shed database software. Assay results were merged when received electronically from the laboratory. The responsible geologist reviewed the data in the database to ensure that it was correct and has merged properly and that all data has been received and entered. Any variations that were required are recorded permanently in the database. • No adjustments or calibrations were made to any assay data used in this report
Location of data points Collars	• Drill holes collars were surveyed by surveyors using a Leica Total Station, Model TS15. This instrument measures distances to an accuracy of ± 0.005m. • Collar position was validated in Surpac software against planned co-ordinates and underground development pick-ups. • All recent surface and underground data was collected in mine grid based on local Zuleika grid. It is not specified in database what grid was used for collection of historic data (pre 2010). It seems like various grids were used over the wide spread of companies involved, therefore it is likely that data undergone some level of transformation between grids (possibly few times). • Topographic control was generated from comprehensive survey pick-ups of the area over the last 30 years. • The magnetic declination for Kalgoorlie has a five year moving average of +0.108 degrees.
Location of data points Down Hole Surveys	• Most of historic drill holes used in the project were surveyed using various magnetic based methods (Multi-shot or Single-shot cameras). 81 holes were surveyed with a north-seeking gyro instrument. There also are 4 short (40 metres) DC holes and 4 short (23 metres) RC holes which were surveyed using Maxibore instrument. Unfortunately for 4 DC holes and 2,238 RC holes the survey method was not recorded. All recent holes were surveyed by magnetic methods.
Data spacing and distribution	• The drill spacing for the Main Lode Indicated resource varies between 50 metres in the close to surface portion of underground deposit to between 16 metres and 40 metres at deeps, on average 25m in the northern deeps, 40 metres in the deeps south. • The drill spacing for the Indicated resource in East Lode varies between 20 metres to 40 metres. The average distance to the samples used is generally below 50 metres.

Criteria	Commentary
	• Data spacing and distribution is considered acceptable for establishing geological continuity and grade variability appropriate for classifying a Mineral Resource. • The length of samples used for resource estimation was generally 1m with some samples shorter due to sampling to geological boundaries. A few samples were 2 metres and greater due to original 4 metres compositing when collecting sample for assay. The samples were therefore composited to 1m down-hole interval. • For estimating marginal halo mineralisation, samples were composited to 0.5m down-hole length.
Orientation of data in relation to geological structure	• All care was taken to achieve the best possible angle of intersection. Availability of drill sites however and presence of pits course many of drill holes intercepting ore body at acute angles. • All FS sampling was performed across the mineralised veins. • No drilling orientation and sampling bias has been recognized at this time.
Sample security	• Historical samples are assumed to have been under the security if the respective tenement holders until delivered to the laboratory where samples to be expected to have been under restricted access. • Samples were all under the security of Norton until delivered to analytical laboratory in Kalgoorlie where they were in a secured fenced compound security with restricted entry.
Audits or reviews	• Internal reviews were completed on sampling techniques and data as part of the Norton continuous improvement practice • No external or third party audits or reviews have been completed.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	Commentary
Mineral tenement and land tenure status	• The Bullant mine is located on tenement M16/44 and M16/45 which are held by Kalgoorlie Mining Company (Bullant) Pty Ltd. • On the 7 August 2013, Norton Gold Fields Limited (Norton) completed a 90% off-market takeover offer for all fully paid ordinary shares in Kalgoorlie Mining Company Limited (KMC) and moved to compulsory acquisition of the remaining shares under the provisions of the Corporation Act. Norton acquired Paddington Gold Pty Limited (Paddington) from Barrick Australia Ltd in August 2007. Paddington is the Operating Manager of the KMC tenements. • The mine is located 20 kilometres south-west of Ora Banda and 65 kilometres north-west of Kalgoorlie. Access from Kalgoorlie is north via the sealed Menzies Highway, then west along the Broad Arrow to Ora Banda Road, then south via the unsealed Bullant access road. The tenements M16/44 and M16/45 are located in the Coolgardie Mineral Field within the Kunanalling District and

Criteria	Commentary
	are found on the Ora Banda 1:50,000 Map Sheet. • Tenements are in good standing and there are no known impediments.
Exploration done by other parties	• A significant proportion of exploration, resource development and mining was completed by companies which held tenure over the Bullant deposit since 1980. Companies included: BHP Gold Mines; Newcrest Mining; Centaur; Goldfields Group; Aurion Gold; Placer Dome; Barrick; and Kalgoorlie Mining Company (KMC). Results of exploration and mining activities by the fore mentioned companies' aid in current resource development. In the current Bullant resource over 80% of all data is legacy data.
Geology	• The Bullant project is located in the western margin of the regionally extensive Norseman-Wiluna Belt, lying within the Coolgardie Domain of the Kalgoorlie Terrane. The geology of the Bullant area is dominated by the Bolshevic syncline which comprises a sequence of folded mafic and ultramafic rocks and interflow sediments constrained by the Zulieka Shear Zone in the east and by the Kunanalling Shear Zone in the west. The gold mineralisation at the Bullant project is hosted in four main reefs which include Main Lode, East Lode, West Lode and Cross Lode. The Main and East lodes to date have hosted the majority of the gold mineralisation mined at the project, and are hosted in biotite altered Bent Tree basalt.
Drill hole Information	• See appendix 1
Data aggregation methods	• All reported assay results have been length-weighted, no top cuts have been applied. Assay results are reported above a 3.5g/t Au lower cut. • A maximum of 2m of internal dilution is included for reporting intercepts. Minimum reported interval is 1.0m for RC and 0.3m for DC intercepts. ○ No metal equivalent values are used for reporting exploration results
Relationship between mineralization widths and intercept lengths	• The DC holes were drilled to achieve the best possible angle of intersection. • Drill hole intersections vary due to infrastructure issues and drill rig access. Many of the drill holes intersect the ore body at acute angles. • All FS sampling was performed across the mineralised veins and are representing approximate true width.
Diagrams	• See appendix 2
Balanced reporting	• All results have been reported relative to the intersection criteria.
Other substantive exploration data	• No other exploration data collected is considered material to this announcement.
Further work	• Further work at Bullant deposit will include additional resource development drilling and updating geological models.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	Commentary
Database integrity	• Database used for the resource estimation of Bullant deposit is a combination of a number of historic databases inherited mainly from Barrick Australia and new drilling conducted by KMC between 2010 and 2012 and Norton in 2014. • An examination of historical drilling information, QAQC verification and database management was undertaken in 2012. • Face sampling data was merged into drill hole database. • The main database that was inherited from Barrick was combined with a number of grade control databases and exploration databases that covered both of KMC's tenements. • Norton geological data is stored in SQL server databases. The SQL databases are hosted on site at Paddington and managed by Paddington personnel. User access to the database is regulated by specific user permissions and validation checks to ensure data remains valid. DataShed software has been implemented as a front-end interface to manage the geological database. • Existing protocols maximize data functionality and quality whilst minimizing the likelihood of error introduction at primary data collection points and subsequent database upload, storage and retrieval points. Data templates with lookup tables and fixed formatting are used for collecting primary data on field laptops. The software has validation routines and data is subsequently imported into a secure central database. • The SQL server database is configured for validation through parent/child table relationships, required fields, logical constraints and referenced library tables. Data that fails these rules on import is rejected or quarantined until it is corrected. • Historic data has been merged into the main SQL database, PGMshed. • The current resource estimates used MS Access subsets of data created from SQL database. To validate this datasets hole traces were visually (on screen) examined to identify missing or incorrect survey and collar location information in the Bullant Mine area. • A visual validation was carried out on all data once it had been into the 3D visualisation software Surpac. Hole traces were visually (on screen) examined to identify missing or incorrect survey and collar location information in the area.
Site visits	• The Competent Person for this update is a full time employee of Norton and undertakes regular site visits ensuring industry standards of the Mineral Resource estimation process from sampling through to final block model. • The deposit area is an active mining area for Norton and as such regular site visits were undertaken during this update. • An independent geological consultant has reviewed the project area in 2012 which included a site visit.

Criteria	Commentary
Geological interpretation	• The high confidence of the geological interpretation is based on geological knowledge acquired from detailed geological DC and RC logging, assay data, underground development backs and face mapping and pit mapping. • The Bullant deposit has been interpreted by KMC to have six mineralised zones which have been wireframed in Vulcan software as closed solids. These zones were sometimes split by the west dipping fault and cross fault. Solids representing mineralised envelopes were built from points snapped directly to drill hole intersections. The underground development mapping was also utilized to aid in understanding of geometry of mineralised zones and faults. The six mineralised zones interpreted were. ○ Main Lode ○ East Lode ○ West North Lode ○ West South Lode ○ West Deep Lode ○ Cross Lode • A down-hole gold grade cut off of 1 g/t was used for creating wireframes. • The geological interpretation is considered robust. • Wireframed surfaces representing the current topography were also constructed, bottom of complete oxidation and top of fresh rock • All Vulcan wireframes were imported to Surpac software and updated using the recent sampling results before updating block model. • The dataset (geological mapping, RC and DC logging, assays etc.) is considered acceptable for determining a geological model.
Dimensions	• The Bullant Main and East lodes have a continuous strike over 1,000 metres with depth extensions reaching 800 metres below surface. • Each lode is typically 1.5 to 6 metres wide true width. • The Bullant deposit is spatially located between 22,850mE and 23,100mE and between 5,300mN to 6,750mN (Zuleika local grid).

Criteria	Commentary
Estimation and modeling techniques	• Geological domains were based on the geological interpretation. Three dimensional wireframes were created from points snapped to drill hole and face sampling intercepts. Domain boundaries were treated as hard boundaries. • The choice of compositing technique took into account several criteria including: ○ The thickness of the ore zones (between 1.5 and 6 metres thick – 2.5 metre on average) ○ Samples were of unequal support (10 centimetres to a meter and up to 4 metres in RC holes) ○ Variable data spacing – from 3 metres by 15 metres to 80 metres by 80 metres for vein intercepts ○ Short-scale grade and geometry variability • The length of samples used for resource estimation was generally 1m with some samples shorter due to sampling to geological boundaries. A few samples were 2 metres and greater due to original 4 metres compositing when collecting sample for assay. The samples were therefore composited to 1m down-hole interval. • The statistics for each domain were viewed and key univariate statistical indicators used to describe the nature of each. Each of the populations of the composite data from the Bullant mineralised domains was positively skewed and showed a number of high grade outliers, which is typical of most of gold mineral deposits. • Top-cuts were determined by way of viewing grade distribution histograms and probability plots to determine what grade separated the outliers from the population. The following factors were taken into account ○ Coefficient of Variation (CV) of samples should be reduced to preferably no more than 1.4 ○ Preferably 95% of the mean should be maintained ○ Variance should be reduced as much as possible considering the above factors • High-grade outliers were top-cut to ○ 20g/t and 50g/t Au in Main Lode ○ 22g/t and 35g/t Au in East Lode ○ 41g/t; 31g/t and 11g/t Au in West Lode ○ 26g/t Au in Cross Lode ○ 5g/t Au in waste envelope • Spatial continuity was examined for each domain. In general the experimental variograms were robust and well defined. The exception was the West Lode where relatively few composites were available due to limited extent. An investigation was conducted on the top-cut composite datasets. • Ordinary Kriging method of grade estimation was used utilising the variogram models. The variogram models were generally kept

Criteria	Commentary
	similar to those used for the Bullant modelling in late 2012. • A total of 3 search passes were conducted with progressively relaxed search criteria to accommodate the data density from face sampling to the widest spaced drilling at 80m x 80m. • Block model dimensions, block sizes and sub-blocking was chosen after a careful examination of the extents of mineralisation, general shape of mineralised veins and distribution of data points ○ Parent block size: 5m(X) by 10m(Y) by 10m(Z) ○ Sub-blocking: 1.25m(X) by 2.5m(Y) by 2.5m(Z) • Blocks in the block models were coded based on the interpreted solids by block centroid in or out of solids. Domain coding was used to control grade estimation process. • No correlation between variables was necessary. • Estimation completed using Surpac mining software. • Standard block model validation has been completed using visual methods by peer review by key geology staff and by comparing with previous estimate. • Mineral Resource Model has been validated visually against the input composite/raw drill hole data with sufficient spot checks carried out on a number of block estimates on sections and plans. • “Weathering” variable was created and assigned values to represent various stages of oxidation near surface.
Moisture	• Tonnages were estimated on a dry basis
Cut-off parameters	• Cut-off of 1g/t Au was used for creating solids for mineralised veins. Gold grade was also estimated into surrounding waste to aid in accurate calculation of diluting grades for Ore Reserve estimations.
Mining factors or assumptions	• The models were depleted for known workings. • Mining methods are based on previous underground mining operation at Bullant. The resource was mined utilizing narrow-vein underground mining methods (jumbo for development, sub-level long-hole open stoping with backfill for production).
Metallurgical factors or assumptions	• No assumption or factors have been applied to the resource estimate regarding the metallurgical amenability. • Ore from Bullant underground was processed through the Paddington mill. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered material to this style of mineralization.
Environmental factors or assumptions	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining and milling of the Bullant deposit.

Criteria	Commentary
Bulk density	• The density data for Bullant deposit has been compiled by Placer Dome, Barrick and KMC (2010-2012) using diamond drilling and stock pile sampling. • To determine bulk density of each sample a gravimetric method (Archimedes Principal) has been used, where samples are first weighted in air, then in water and a bulk density is calculated. The moisture contains was also determined from stock pile sampling. Each sample, approximately 10kg was after collection sealed in a plastic bag before being sent to the laboratory. Collected information was used to confirm the density of fresh rock at Bullant being 2.78t/m³. • Density values assigned to block model cells were as follows: ○ Oxide 1.85t/m³ ○ Transitional 2.3t/m³ ○ Fresh rock 2.8t/m³
Classification	• For this update Norton maintained KMC classification from the previous, late 2012 estimate. KMC followed the JORC classification system with individual block classification based on statistical methods taking into account the following factors: ○ Confidence of certain parts of the geological model supported by ○ Level of geological understanding ○ Drill spacing and orientation ○ Confidence in data quality • Measured category was assigned to resource around mine development. Indicated category to resource where distance between data points was not bigger than 40 metres. Inferred category to resource estimated using a higher data point's separation.
Audits or reviews	• The continuity analysis and kriging parameters used to estimate gold grade into resource model were reviewed by independent geology consultant – Haren Consulting in late 2012.
Discussion of relative accuracy/ confidence	• The Mineral Resources have been reported in accordance with the guidelines of the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves and reflects the relative accuracy of the Mineral Resources estimate. The Competent Person deems the process to be in line with industry standards for resource estimation and therefore within acceptable statistical error limits. • The statements relates to global estimates of tonnes and grade for underground mining extraction. • Production data was used to compare with the resource estimate (where appropriate) and assisted in defining geological confidence and resource classification categories

Section 4 Estimation and Reporting of Ore Reserves

(Criteria listed in section 1, and where relevant in sections 2 and 3, also apply to this section.)

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• A financial evaluation, underground life of mine design and schedule were completed for Bullant by NGF personnel in December 2015. The development and stope design parameters are based on existing NGF underground procedures. The scheduled life of mine reserves consist of proven reserves of 66,997t @ 3.23g/t Au and probable reserves of 360,218t at 3.41g/t at a cut off grade of 3.1g/t. • The Mineral Resources are reported inclusive of the Ore Reserves.
Site visits	• Bullant Underground is currently an active mine site which has been in operation since January 2014. • Bullant Underground has been visited by Elizabeth Jones (UG Manager "NGF" & CP for Reserves) within the last 6 months. • Inspection of the existing stoping and development has been carried out and geotechnical constraints such as stope stability, ore types, hydrogeological setting has been undertaken and incorporated into the mineable reserve.
Study status	• NGF Technical Services Department undertook financial review and design of the Bullant mineral deposit. The Life of Mine plan was based on a selling price of $AUD 1,400/oz with a 2.5% royalty. • The block models used for the Underground design are "Bullant_nov14.mdl". • Mining dilution, ore loss and mill recovery factors were applied (22-40%, 5% and 95% respectively). • Operating cost used was based on NGF's current Underground fleet with average processing cost of $25.57/t (Including haulage from Bullant and G&A costs).
Cut-off parameters	• A break even cut off grade of 3.1g/t was calculated using the 2015 budget & LOM physicals • Selling price = AUD$1,400/Oz. • State Royalty = 2.5%. • Metallurgical recovery = 95%. • Processing cost = $25.57/t.
Mining factors or assumptions	• The method used to convert Mineral resource to Ore Reserves is based upon identifying which proposed mining panels and development areas are economic. • The mining method will be based on standard jumbo development and long hole open stoping with flat-back mining utilised in some areas. • NGF is an owner operator and Bullant is currently being mined by NGF using its operating model.

Criteria	Commentary
	• The Ore reserve estimate was created using mining shapes with an allocated level of confidence. All shapes were checked by a resource geologist to ensure correct assignment of resource category • Gold Price used = $AUD1,400/Oz. • Processing cost = $25.57/t (Including haulage from Bullant and G&A costs). • Infrastructure requirement for underground mining includes; A workshop for all mobile equipment for maintenance requirements, offices, crib rooms and amenities, explosives storage, water dams and communication. All of these infrastructures are already on site and actively used.
Metallurgical factors or assumptions	• Bullant ore has been milled at NGF's Paddington mill in 2014 and historically prior to 2007. • Ore from Bullant will be delivered via road trains to NGF's Paddington mill for processing. • Paddington Mill is based on conventional carbon in pulp technology and has achieved an annual throughput of 3.72 million tonnes in 2014 with average feed grade of 1.68g/t with average recovery of 89%. • A recovery factor of 95% has been applied to all Bullant ore.
Environmental	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. • All proposed operation and operational plans are within local historical practices and existing operational standards.
Costs	• Bullant's reserve estimate was based on a gold price of $AUD 1,400/Oz. • Allowance has been made for the 2.5% state government royalty. • Operating cost used was $109.78/ore t. This is based on budgeted numbers for Bullant in 2015.
Infrastructure	• The site has existing infrastructure including electricity, water and road infrastructure. • The site has a fully operational office, core facility, crib rooms, explosives storage, water dams and communication.
Revenue factors	• Financial analysis in this report is based on a gold price of $AUD 1,400/Oz. • The gold Dore is planned to be transported via recognized security service from gold room of Paddington processing plant to the gold refinery in Perth. • Contract payments and terms are expected to be typical of similar contracts for the refining and sale of Dore produced from other operations within Australia. • Allowance has been made for the 2.5% state government royalty.

Criteria	Commentary
Market assessment	• Historical gold price and forward looking estimates have been used for the gold price. Price flexing and sensitivity analysis have been carried out to determine the robustness of the project viability. The cash flow was modelled in real terms and no price or cost escalations were applied.
Economic	• Inputs to economic analysis include factors described above including ore and metal quantities from mining/processing schedule (including described recovery/processing parameters), cost and price assumptions.
Social	• The majority of workforce is from Kalgoorlie. • NGF has established all relevant agreement with local stakeholders and government agencies.
Classification	• The Ore Reserve was classified as Proven and Probable in accordance with the JORC Code, corresponding to the resource classifications of Measured and Indicated. No Inferred Mineral Resources were included in the Ore Reserve estimate. • The estimated Ore Reserves and mining method are in the opinion of the Competent Person appropriate for this style of deposit.
Audits or reviews	• The resource and reserve was calculated by NGF personnel. The cost and mining parameters were reviewed internally against existing operations and consideration was made for current practice and cost structure. • Dilution calculations are expected to be reviewed in line with past practices at Bullant and current stoping performance. Dilution parameters were conservative during the reserve estimation process and are expected to be reduced upon a detailed review.
Discussion of relative accuracy/ confidence	• All mining estimates are based on Australian costs, and relevant historical cost data. • All Proven reserves have been developed with a vertical level interval of less than 25m. • There are no unforeseen modifying factors at the time of this statement that will have any material impact on the Ore Reserve estimate.

Appendix 1: Table of exploration results – Bullant Diamond Core

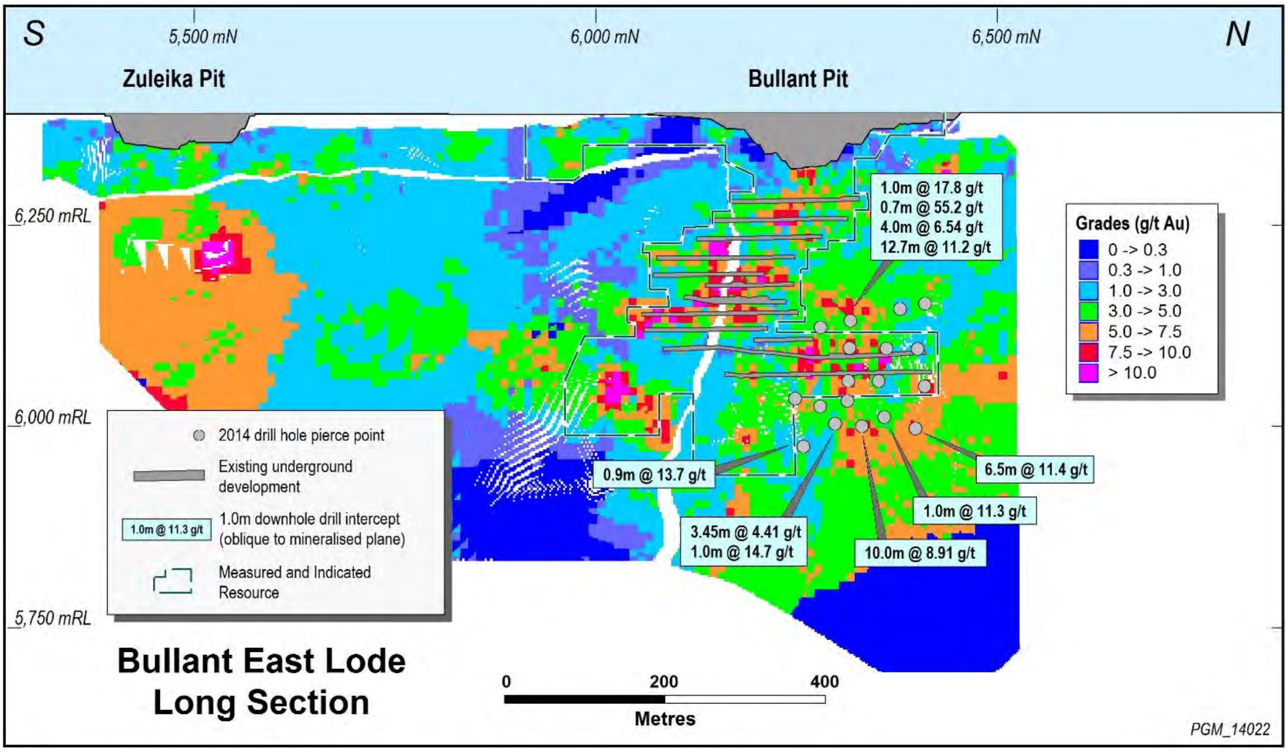
Hole ID	ZUL East	ZUL North	ZUL RL	Dip	Azimuth	Depth (m)	From (m)	To (m)	DH Width (m)	Grade (g/t au)
BUGD1047	22983.6	6380.2	5669.6	-64	286.1	215	125	133	8	5.95
							164	165	1	6.92
BUGD1048	22983.2	6379.3	5670.4	-55	309.5	386.8	124	126	2	7.52
							133	136	3	4.34
							303.6	304.3	0.7	8.65
BUGD1050	22979.0	6550.5	5645.2	-25.5	225.3	164.5	98.6	99.5	0.9	19.1
BUGD1051	22978.6	6551.3	5645.8	-3.5	245.3	125.5	78.8	83.1	4.3	3.67
BUGD1052	22977.8	6552.6	5647.3	21.8	276	134.4	8.5	8.85	0.35	11.9
BUGD1053	22978.4	6552.6	5644.9	-33.5	276	134.5	26	26.8	0.8	11.3
							85.87	86.4	0.53	13.3
BUGD1054	22978.2	6553.7	5648.4	35.5	300	158.3	144.4	145	0.6	5.1
BUGD1055	22978.3	6553.7	5645.7	-3.5	300	137.3				NSI
BUGD1056	22978.6	6554.8	5647.0	15	315	182.3	153	156	3	17.59
							174.45	175.2	0.75	6.82
BUGD1057	22978.7	6554.8	5644.9	-21.5	315	173.5				NSI
BUGD1058	22979.3	6555.0	5647.5	25	325	263.7	215.5	217.9	2.4	8.35
BUGD1059	22979.1	6555.2	5645.8	-2	325	216	17	18.65	1.65	4.18
BUGD1060	22978.8	6550.0	5645.7	-3.1	225.2	140.5	97.5	99.3	1.8	6.67
BUGD1061	22978.5	6551.1	5647.1	21.7	245.3	119.6	8.3	8.8	0.5	21.6
BUGD1061							94	95	1	4.77
BUGD1062	22978.8	6551.2	5645.0	-31.3	245.2	137.6	116.15	117.15	1	3.77
BUGD1063	22978.3	6552.3	5645.7	-4.1	276	107.3	79.45	80.7	1.25	4.93
BUGD1064	22978.4	6553.8	5647.0	19.1	300	141	117.1	118.3	1.2	6.01
BUGD1065	22979.5	6552.2	5645.6	-28.3	300	119.5				NSI
BUGD1066	22979.6	6552.9	5645.5	-28.3	315	198				NSI
BUGD1067	22979.6	6552.9	5645.5	-2.6	315	148.7				NSI
BUGD1068	22979.6	6552.9	5645.5	12.5	325	205.5	198.8	200.8	2	5.52

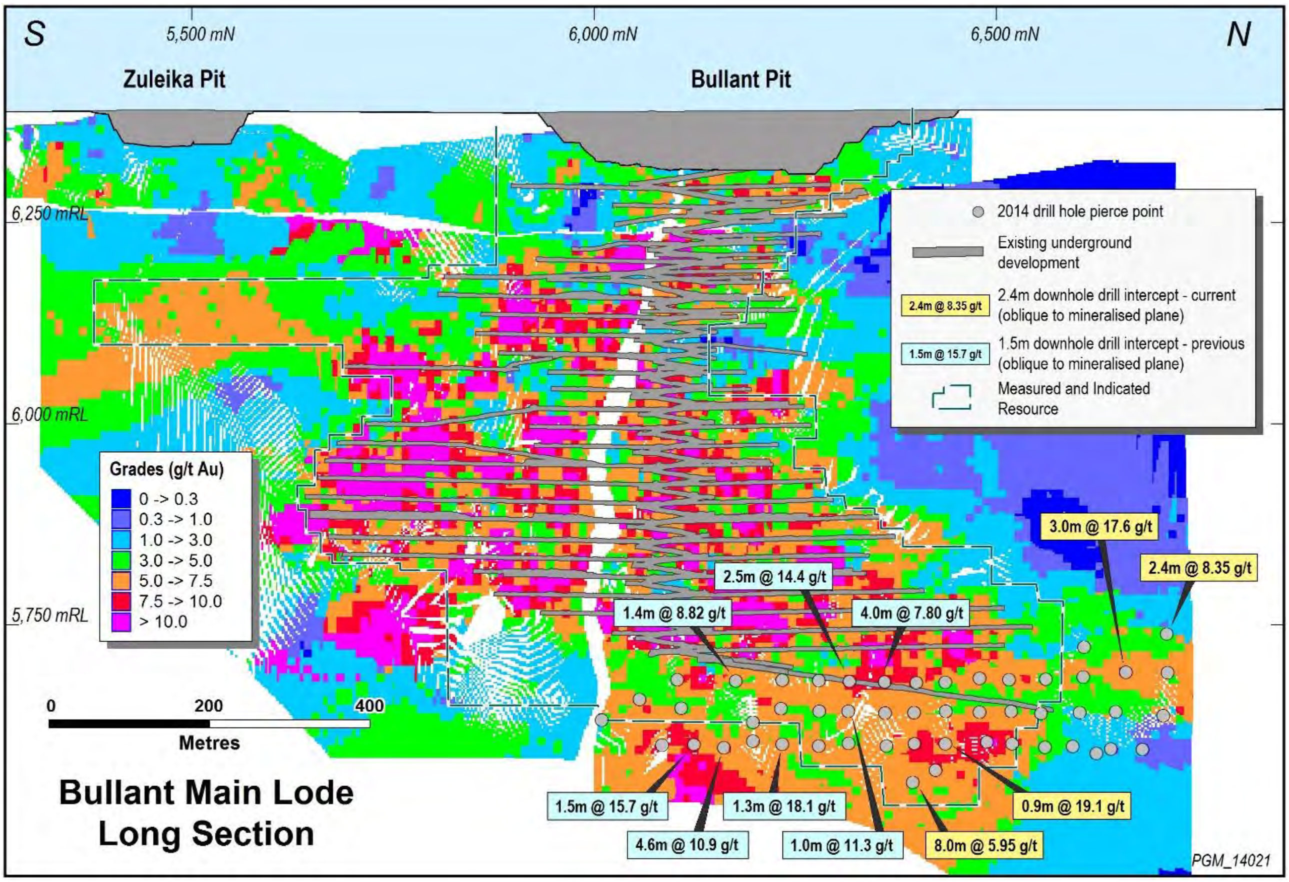
Analysis by 30g Fire Assay

Results compiled by using a 3.5/t cut-off grade, no top-cut grade,

Maximum of 2m internal dilution, minimum interval of 0.3m

Appendix 2: Figures showing the diamond drill hole pierce points of the 2014 drilling at Bullant





JORC Code, 2012 Edition – Table 1 Wattlebird Resource and Reserve 2014

Section 1 Sampling Techniques and Data

Criteria	Commentary
Sampling techniques	• Sampling defining Wattlebird mineralisation is a combination of Diamond Core holes (DC), Reverse Circulation (RC), Rotary Air Blast (RAB) and Air Core (AC) holes. Only DC and RC drilling was used for Estimation of Mineral Resource. • Drilling and sampling has been conducted in 1980's and 1990's by Newcrest Mining; Centaur Mining and Exploration ("Centaur") and by Aurion Gold in 2002. The most recent campaign was completed by Norton Gold Fields. • Drilling, sampling and QAQC information is extracted from Centaur 1998 resource report for Zuleika-Carbine project area, which includes Wattlebird deposit. Sampling techniques from the recent campaign is also summarized from Norton Gold Fields drilling report & sampling procedures. • All RC recovered samples were passed through a 3 stage splitting device (riffle splitter) at 1m intervals to obtain sample for assay. All samples from the first split were bagged in plastic bags and marked with hole and depth identification for each metre drilled. The samples from the final split were collected in an appropriately sized calico bag and labeled with sample number, hole number and down hole interval. Target RC calico sample weights ranged from 2 to 5kg. All RC holes were initially sampled using a 3 to 5 kilogram sample over a 4 metre sample interval. This composite sample was obtained by either using a 3rd or 4th stage riffle split that returned about 4% of the total one metre sample or by the use of a spear sample taken from the samples stored in plastic bags or from the ground. Single metre samples were then submitted for assay from areas of composite anomalism. • DC samples were placed into core trays at the rig before being bought to the core yard for processing.
Drilling techniques	• The dataset used for the Wattlebird resource estimate is all historic data dating back to the 1980's, 1990's and 2002, which include RC and surface DC holes; • In the latest estimates 429 RC holes were used (95%) and 22 DC holes (5%). • Norton RC sampling is completed under contract by Drilling Australia using a Schramm T68SW equipped using Sullair combo-compressor (1150cfm/350psi or 900cfm/500psi) using a 5.25" or 5.5" diameter drill bit with a 5" Sandvik RE054 bottom face sampling hammer equipped with a rig mounted Metzke cone splitter. • DC sampling is a combination of NQ (47.6mm dimater) or NQ2 (50.5mm diameter) core sizes (9 holes of WBRCD series).
Drill sample recovery	• RC Drillers are advised by geologists on the ground conditions expected for each hole and instructed to adopt an RC drilling strategy to maximize sample recovery, minimize contamination and maintain required spatial position. • All RC 1m samples from the first split were collected into a UV resistant bag. Samples were visually logged for moisture content, estimated sample recovery and contamination. The size of sample was recorded, but is no longer available.

Criteria	Commentary
	• Sample loss or gain is reviewed at the time of drilling and feedback is provided to the drilling contractor to ensure the samples are representative. All samples sent to the laboratory are weighed and monitored to ensure that they are representative. • DC contractors use a core barrel and wire line unit to recover the DC, adjusting drilling methods and rates to minimize core loss. • The DC samples are length measured and compared to core blocks denoting drilling depths by the drilling contractor. • Sample recovery statistics are only available for 9 DC holes of WBRCD series reporting an average recovery of 99.7% • Same 9 holes have Rock Quality Designation (RQD) data recorded, which is on average 96.7%. A conclusion can be made that the ground condition in fresh rock in the area of Wattlebird resource area were good therefore no significant core loss could be expected.
Logging	• All DC hole data was geologically logged. Hole ID, interval, rock type, changes in shear intensity and changes in alteration type or the occurrence of quartz veining were recorded. • Geological logging was qualitative in nature. • Geotechnical information was collected from selected DC holes. Information collected includes RQD, and fracture frequency. • RC samples were also geologically logged. The following parameters were recorded: weathering, rock type, alteration, mineralization, veining and structure. Where no sample is returned due to voids or lost samples, it is logged & recorded as such.
Sub-sampling techniques and sample preparation	• DC samples for assay were collected at intervals nominated by a geologist from half core with a minimum interval of 0.3m and a maximum of 1.0m. • Sample intervals always conform to the logged lithological boundaries. • Core was halved for sampling using diamond saw, half was sampled and assayed, the remaining half resides in the core tray and archived. • Samples collected from DC are placed into pre-numbered bags and sent to the lab. • Samples were taken to a commercial laboratory for assay. • All RC samples were split by a splitting device at the rig to collect sample for assay of app. 3kg for each down-hole metre. Those 1m samples or composite samples were placed in pre-numbered calico bag and send for assay. • RC & DC samples submitted to the laboratory are sorted & reconciled against the submission documents. Routine CRM (standards & blanks) are inserted into the sampling sequence at a rate of 1:20 for standards or in specific zones at the Geologist's discretion. The commercial laboratories complete their own QC check. Both RC and diamond drilling campaigns utilised barren quartz flushes between expected mineralized sample interval(s) when pulverising. Selected barren quartz materials flushed within expected mineralised interval are assayed to identify potential smearing.

Criteria	Commentary
	• RC field duplicate data was collected routinely & for selected intervals suspected to contain mineralisation. Field duplicate samples were taken at the time of cone/riffle splitting the bulk sample at the drill rig to maintain sample support. The field duplicates are submitted for assay using the same process mentioned above, with the laboratory unaware of the duplicate nature. • The sample preparation technique for all samples followed industry standard procedures by accredited commercial laboratories. All samples were died, crushed in Jaw Crusher then split in riffle splitter if they were above 4kg and pulverized. 200g sample was scooped out and reduced again to obtain a sub sample, which entered the Fire Assay process. • All sub-subsampling & lab preparations are consistent throughout Australia & are satisfactory for the intended purpose.
Quality of assay data and laboratory tests	• All samples were analysed for gold by Australian Assay Laboratories, MinLab, Amdel or Australian Laboratory Services all in Kalgoorlie. • Aqua Regia assays were done innately on 4 metre composite samples from 50g pulps followed by Fire Assay for samples above 0.2g/t Au. • The Fire Assay method was designed to measure total gold in the sample. The Fire Assay charge of 50g was fused with a lead flux then decomposed in a furnace with the prill being totally digested by 2 acids (HCl and HN03) before measurement of the gold content by an Atomic Absorption Spectrometer. • QAQC for Wattlebird drilling consists of: o Duplicate samples o RC pulp replicates o Internal Laboratory checks and standards o External or inter-laboratory checks • Duplicate samples were collected from 1 metre RC intervals at the rate of 1 in 15. Each sample was a separate re-split of the original sample supplied for assays with different sample number. All duplicates were compared to original assays by plotting on correlation graphs. Correlation of two sets of data was good showing correlation coefficient of 0.889 (in 1998 Centaur resource report) 0.83 (in 1997 QAQC report). • Some duplicate samples were also taken from DC holes by splitting half-core. • Pulp replicate assays - comparing original assays to second replicates showed greater variability with coefficient of correlation at 0.441 (in 1997 QAQC report). Population for this was small, only 124 samples. • All assay laboratory conducted internal checks by the use of certified reference material of known grade as well as testing of replicate samples. All laboratories report the results of their internal checks to the clients on regular bases. Some reports from

Criteria	Commentary
	Analabs are still available. • Samples were submitted to third party laboratories to check accuracy between laboratories. The samples were sent as pulps from which the original sub-sample was derived. Difference between laboratories ranged on average from +8% to –5% from original laboratory. • 1997 QAQC report for Ora Banda also states that Certified Reference Material (CRM) samples were inserted at the rate of 1 in 50 RC composite samples and 1 in 30 for 1 metre fire assayed samples. For DC testing CRM was inserted at the rate of 1 in 50 samples. CRM prepared by Gannet Holdings Pty Ltd range in expected values from 0.13g/t Au to 5.01g/t Au. Assays results for supplied 285 CRM samples were compared to expected values by plotting on correlation graphs. Reported coefficient of correlation for this work was 0.92 (1997). • Recent RC samples submitted to the laboratory are sorted & reconciled against the submission documents. Certified Reference Material (CRM) (standards & blanks) are inserted into the sampling sequence at a rate of 1:25 for standards or in specific zones at the Geologist’s discretion. The commercial laboratories undertake their own QC checks. Specific diamond drilling campaigns utilised barren quartz flushes between expected mineralised sample interval(s) when pulverizing. In the absence of Certified Blank Material, selected barren quartz materials flushed within expected mineralised interval are assayed to identify potential smearing. • Standard procedures are to examine any erroneous QC result (a result outside of expected statistically derived tolerance limits) & validate if required; establishing acceptable levels of accuracy & precision for all stages of the sampling & analytical process.
Verification of sampling and assaying	• All drill hole data files were constructed kept in Micromine software. Any errors such as missing, incorrect or mismatched assays were immediately flagged and corrected. Plots of acquired data were regularly developed to check for errors in collar or down-hole survey files. • Primary logging and sampling data was imported to Micromine database and checked against hardcopy logs, sample submission sheets and database records. Assay results were received by database administrator electronically from the laboratory and imported to database after validation checks. The responsible geologist reviewed the data in the database to ensure that it was correct and has merged properly and that all data has been received and entered. • No adjustments or calibrations were made to any assay data used in this report
Location of data points Collars	• Collar co-ordinates for all drill holes used for resource estimation were surveyed in local (Zuleika) grid or in AMG-84 Zone 51. • In 1996 an aerial survey of the area was undertaken by Fugro Surveys. Resulting digital data set was converted into topographic contours. • The magnetic declination for Kalgoorlie has a five year moving average of +0.108 degrees.
Location of data points	• Drill holes were surveyed using magnetic based methods (Multi-shot or Single-shot cameras). Changes in down-hole azimuth were

Criteria	Commentary
Down Hole Surveys	generally consistent demonstrating gradual increase in drift after about 100 metres depth. RC holes show higher than DC holes deviation.
Data spacing and distribution	• The drill hole locations were designed to allow for spatial spread of samples across mineralized zones and different rock types Data spacing and distribution is considered acceptable for establishing geological continuity and grade variability appropriate for classifying a Mineral Resource. • Drilling was completed on 20 metres by 20 metres spacing with shallow 10 metres by 10 metres infill in places, to maximum 40 metres by 40 metres for the majority of deposit. • The length of samples used for resource estimation was generally 1m with some samples shorter due to sampling to geological boundaries. A few samples were 2 metres and greater due to original 4 metres compositing when collecting sample for assay.
Orientation of data in relation to geological structure	• All care was taken to achieve the best possible angle of intersection. Majority of recent RC holes dip 60 degrees to the Northeast and Southwest providing good angle of intersection with semi vertical mineralised zone.
Sample security	• Historical samples are assumed to have been under the security if the respective tenement holders until delivered to the laboratory where samples to be expected to have been under restricted access. • Samples were under the custodial chain of the company until delivered to a commercial laboratory some 30km south of the operations; upon which they were secured in a fenced compound with restricted entry. Internally, the commercial laboratories operate an audit trail tracking the samples at all times whilst in their custody.
Audits or reviews	• Numerous reviews were completed during all stages of sale process, most recently by Norton Gold Fields Ltd in 2012. Identified issues are discussed in further paragraphs. For the recent campaign internal reviews are completed on sampling techniques & data as part of the Norton Gold Fields continuous improvement practice. No external or third party audits have been completed.

Section 2 Reporting of Exploration Results

Criteria	Commentary
Mineral tenement and land tenure status	• The Wattlebird deposit is located on tenement M16/44 which are held by Kalgoorlie Mining Company (Bullant) Pty Ltd. • On the 7 August 2013, Norton Gold Fields Limited (Norton) completed a 90% off-market takeover offer for all fully paid ordinary shares in Kalgoorlie Mining Company Limited (KMC) and moved to compulsory acquisition of the remaining shares under the provisions of the Corporation Act. Norton acquired Paddington Gold Pty Limited (Paddington) from Barrick Australia Ltd in August 2007. Paddington is the Operating Manager of the KMC tenements. • The mine is located 20 Kilometres south-west of Ora Banda and 65 Kilometres north-west of Kalgoorlie. Access from Kalgoorlie is

Criteria	Commentary
	north via the sealed Menzies Highway, then west along the Broad Arrow to Ora Banda Road, then south via the unsealed Bullant access road. The tenement M16/44 is located in the Coolgardie Mineral Field within the Kunanalling District and is found on the Ora Banda 1:50,000 Map Sheet. • Tenement is in good standing and there are not known impediments.
Exploration done by other parties	• A significant proportion of exploration, resource development and mining was completed by companies which held tenure over the Wattlebird deposit since 1980, namely Newcrest Mining; Centaur Mining and Exploration Ltd ("Centaur") and Aurion Gold. Results of exploration & mining activities by the afore-mentioned companies has assited in Norton Gold Field's more recent exploration, resource development & mining in the area.
Geology	• The Wattlebird deposit is located in the western margin of the regionally extensive Norseman-Wiluna Belt, lying within the Coolgardie Domain of the Kalgoorlie Terrane. The geology of the area is dominated by the Bolshevic syncline which comprises a sequence of folded mafic and ultramafic rocks and interflow sediments constrained by the Zulieka Shear Zone in the east and by the Kunanalling Shear Zone in the west. The gold mineralisation within and below weathered profile at Wattlebird occurs in steep dipping high-magnesium basalt.
Drill hole Information	• See Appendix 1
Data aggregation methods	• All reported assay results have been length-weighted; no top cuts have been applied. Assay results are reported to a 0.8 g/t Au lower cut over a minimum intersection of 1m for RC.
Relationship between mineralization widths and intercept lengths	• Drill hole intersections are generally at a high angle to each mineralized zone. Reported down hole intersections are noted as approximately true width, or otherwise are denoted as 'true width not known'
Diagrams	• See Appendix 2
Balanced reporting	• All results have been reported relative to the intersection criteria
Other substantive exploration data	• No other exploration data collected is considered material to this announcement.
Further work	• The deposit is currently being mined. Further work at Wattlebird deposit will include geotechnical studies around the southern sector of the pit to aid in pit design.

Section 3 Estimation and Reporting of Mineral Resources

Criteria	Commentary
Database integrity	• Database used for the resource estimation of Wattlebird deposit is a combination of a number of historic databases inherited from Barrick Australia during the sale of the Bullant project to KMC. Drilling and sampling has been conducted in 1980's and 1990's by Newcrest Mining; Centaur Mining and Exploration ("Centaur") and by Aurion Gold in 2002. • An examination of historical drilling information, QAQC verification and database management was undertaken in 2011 by KMC. • All data is transformed to local Zuleika grid. It is evident that collar co-ordinates and survey files within the dataset have been transformed between various grids (possibly several times). • Drill hole data was supplied to BM Geological Services (BMGS) who developed resource mode in 2011 as MS Access database. • A validation was carried out on drill hole data by BMGS during which some obvious errors were identified. The errors related to overlapping intervals, which was remediated by changing priority rating of relevant intervals. • Validation process filed to identify that 3 DC holes (WBRCD001 to WBRCD003) had erroneous down-hole survey data. For those 3 holes MGA94 azimuth values were used, which was in disagreement with all other data, which was in local Zuleika grid. These were the holes surveyed with gyro instrument. • Slight discrepancy was also noted between drill hole collar positions and topography.
Site visits	• Un-known
Geological interpretation	• Geological model for the Multiple Indicator Kriged (MIK) model was developed by creating the estimation domain based on geological logging of drill holes using mafic rock as primary domain. • Waste domain was also created, which represents all areas outside of the mafic rock. • Regolith profiles were used to create sub-domains, namely oxide, transitional and fresh rock sub-domains. • KMC have constructed wireframed surfaces representing the current topography, bottom of complete oxidation and top of fresh rock
Dimensions	• The data supplied extends from 7,000mN to 7,500mN and from 22,800mE to23,300mE in Zuleika grid • Block model was constructed between 6,810mN and 7,690mN and between 22,800mE to 23,300mE with vertical extend of 460 metres also in Zuleika grid. • Model covers areas previously mined as Wattlebird Pit and Old Zuleika Pit

Criteria	Commentary

Estimation and modeling techniques	- Geological domains were based on geological logging of drill holes using mafic rock as primary domain 1. Areas outside were treated as primary domain 2. Oxidation profile was used to create 6 sub-domains.
	- The length of samples used for resource estimation was generally 1m (99%) with some samples shorter due to sampling to geological boundaries. A few samples were 2 metres and greater due to original 4 metres compositing when collecting sample for assay. The samples were composited to 2m down-hole interval. Two metre composites were chosen to:
	  ○ Reduce the variability of the composite data
	  ○ Achieve sample support close to mining parameters
	- Samples below detection limit recorded as negative number were substituted for 0.01 grams. Missing values were omitted.
	- The statistics for each domain and sub-domain were viewed and key univariate statistical indicators used to describe the nature of each. Each of the population of the composite data from the Wattlebird mineralised domains was positively skewed and showed number of high grade outliers, resulting in high coefficient of variation (between 5.1 and 2.49) which is typical of the most of mineral deposits.
	- A non-linear – Multiple Indicator Kriging (MIK) method of estimation was chosen.
	- Fifteen indicator thresholds were established for each of 6 subdomains corresponding to 10th to 100th percentile plus 75th, 85th, 95th, 97th and 99th percentile.
	- Spatial continuity of gold mineralisation was examined for each primary domain. One set of indicator variograms was calculated and modelled for each of the primary domains.
	- Block model dimensions and block sizes was chosen taking into account size of Smallest Mining Unit (SMU) of 5 metres by 5 metres by 2.5 metres. The size of blocks was therefore established as 10 metres East by 20 metres North by 5 metres vertically.
	- A total of 3 search passes with progressively relaxed search criteria were conducted for each threshold to estimate a probability of each block in the model being above each of threshold grades.
	- Primary domain and subdomain and panel proportions were calculated directly from wireframes. If a block centroid fell within the wireframe volume or above below DTM surfaces, the centroid was coded by the attribute.
	- Estimation completed using Hellman and Schofiels GS3 software.
	- The GS3 MIK modelling software has a variance adjustment function to reflect sample support for likely open pit mining practices (the recoverable resource parameters). Panel histograms generated at sample support were adjusted to reflect open cut mining with a selectivity of around 5 metres by 5 metres by 1 metre. The GS3 lognormal-normal method was used with a total adjustment of 0.05 both primary domains. The correction factor was selected to give recoverable resources for likely mining practices. Dilution

Criteria	Commentary
	and ore loss should therefore be considered as being built into the model. • Block model validation has been completed using visual methods by comparing block grades to drill hole data. Latest estimation was also compared to previous estimate of 2003 (at the cut off of 0.9g/t Au). Slightly more tonnes (70,000) at similar grade were estimated in latest model. This small discrepancy could be contributed to hole WBRCD003 being erroneous as discussed in previous paragraphs and to higher specific gravity values used.
Moisture	• Tonnages were estimated on a dry basis
Cut-off parameters	• Cut-off of 0.7g/t Au was used to report Mineral Resource.
Mining factors or assumptions	• Mining methods are based on current NGF open pit mining practices.
Metallurgical factors or assumptions	• No assumption or factors have been applied to the resource estimate regarding the metallurgical amenability. • Historically reported recoveries for Wattlebird ore were 87% for oxide and 90% for transitional and fresh rock material.
Environmental factors or assumptions	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material.
Bulk density	• The density data for the Ora Banda area has been compiled over the years using two different methods. ○ DC sampling where 10cm to 25cm core samples were sent to analytical laboratories for specific gravity determination ○ RC neutron activation (gamma gamma) down-hole logging, calibrated against a standard of known core material. • Historically the density values used were: ○ Oxide 1.8t/m^3 ○ Transitional 2.1t/m^3 ○ Fresh rock 2.7t/m^3 • In previous model (2003) the density values used were: ○ Oxide 2.1t/m^3 ○ Transitional 2.1t/m^3 ○ Fresh rock 2.7t/m^3 • In current 2011 estimate the density values used were: ○ Oxide 2.0t/m^3

Criteria	Commentary
	○ Transitional 2.4t/m³ ○ Fresh rock 2.7t/m³
Classification	• Confidence level was assigned to block model by NGF personnel based on estimation pass. • Confidence of blocks adjacent to erroneous holes in WBRCD series was downgraded to un-classified. These blocks were removed from reportable resource.
Audits or reviews	• Block model and background data was reviewed by NGF personnel. Some of the findings are discussed above.
Discussion of relative accuracy/ confidence	• Reported Mineral Resources for Wattlebird deposit are subject to inherited risks in relation to: ○ Limited QAQC data available ○ Limited bulk density information available ○ Errors in down-hole surveys for 3 DC holes ○ Slight inconsistency in drill hole collar position compared to topography wireframe ○ Limited historic reconciliation data • Wattlebird deposit will require re-modelling.

Section 4 Estimation and Reporting of Ore Reserves

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• A Whittle optimization and pit design was carried out for Wattlebird by NGF personnel in October 2013. The pit design parameter complies with safety parameters based on existing NGF's open pit procedures. The pit design comprises Probable Reserves of 392.2Kt at 1.57g/t at a cutoff grade of 0.61g/t for oxide, transitional and fresh. • The Mineral Resources are reported inclusive of the Ore Reserves.
Site visits	• A site visit was conducted at KMC operations for Wattlebird Pit on the 1st May 2013 with Steve McKenzie (Mine Foreman "KMC"), Trevor Eddie (Senior Geologist "KMC"), Peter Ruzicka (GM Geology "NGF" & CP for Resources), Guy Simpson (GM Technical Services "NGF" & CP for Reserves) and Gary Goh (Mining Technical Services Manager "NGF").
Study status	• NGF Technical Services Department created a pit design for the Wattlebird mineral deposit based on Whittle Shell Revenue Factor 1 which is inclusive of a minimum mining width of 30m. The pit design was based on Whittle optimization using a selling price of $AUD1, 400/Oz with 2.5% Royalty.

Criteria	Commentary
	• The block model used for both Whittle optimization and Pit design is "wb_mik0511.mdl". As the block model is a "MIK" model, mining dilution and ore loss factors were not applied. • Operating cost used was based on "NGF's small digger fleet cost model" with average processing cost of $25.15/t.
Cut-off parameters	• A cutoff grade of 0.61g/t for oxide, transitional and fresh rock. • The cutoff grade applied is shown by; $\text{Cut}-\text{off Grade} = \frac{\text{Mining Dilution x Processing Cost}}{\text{Processing Recovery x (Selling Price}-\text{Selling Cost)}}$ • Selling price = AUD$1,400/Oz. • State Royalty = 2.5%. • Metallurgical recovery = 94%. • Processing cost = $25.15/t.
Mining factors or assumptions	• The method used to convert Mineral resource to Ore Reserves is based upon a pit optimization identifying the economic shell within which a practical mining design can be applied to. • The mining method will be based on conventional open pit mining with diesel trucks and shovels. For Wattlebird, "NGF's small digger fleet model" will be used to optimize the reserve. • As NGF is an owner operator Wattlebird's operating model will be based on the pit being mined by NGF. • The Ore reserve estimate was created using DCF methodology within "Whittle" open pit optimization software in order to select the most appropriate and economically viable pit shell taking into account minimum mining width for the chosen equipment fleet. • Geotechnical slope design parameters were applied based on geotechnical domains/zones within the mining model. • An overall minimum mining width of 30m was applied. • As the block model is a "MIK" model, mining dilution and ore loss factors were not applied. • No inferred and or unclassified material has been included in the reserves. • Gold Price used = $AUD1, 400/Oz. • Processing cost = $25.15/t. • Infrastructure requirement for open pit mining includes; A workshop for all mobile equipment for maintenance requirements, offices, crib rooms and amenities, explosives storage, water dams and communication. Most of these infrastructures are already on site.

Criteria	Commentary
Metallurgical factors or assumptions	• No metallurgical test work was undertaken by NGF on Wattlebird. • Ore from Wattlebird will be delivered via road trains to NGF's Paddington mill for processing. • Paddington Mill is based on conventional carbon in pulp technology and has achieved an annual throughput of 3.67 million tonnes in 2012 with average feed grade of 1.37g/t with average recovery of 94%. • A recovery factor of 94% have been applied to Wattlebird's oxide, transitional and fresh rock types as the ore will be blended with Paddington's other ore sources to be able to achieve this recovery factor.
Environmental	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. • All proposed operation and operational plans are within local historical practices and existing operational standards.
Infrastructure	• The site has existing infrastructure including electricity, gas, water and road infrastructure. • The site has a fully operational office, core facility, crib rooms, explosives storage, water dams and communication.
Costs	• Wattlebird's reserve estimate was based on a gold price of $AUD 1,400/Oz. • Allowance has been made for the 2.5% state government royalty. • Operating cost used was based on "NGF's small digger fleet cost model" with average processing cost of $25.15/t. • No penalties assumed and no deleterious elements in concentrate.
Revenue factors	• Financial analysis in this report is based on a gold price of $AUD 1,400/Oz. • The gold Dore is planned to be transported via recognized security service from gold room of Paddington processing plant to the gold refinery in Perth. • Contract payments and terms are expected to be typical of similar contracts for the refining and sale of Dore produced from other operations within Australia. • Allowance has been made for the 2.5% state government royalty.
Market assessment	• Historical gold price and forward looking estimates have been used for the gold price. Price flexing and sensitivity analysis have been carried out to determine the robustness of the project viability. • The cash flow was modelled in real terms and no price or cost escalations were applied.
Economic	• Inputs to economic analysis include factors described above including ore and metal quantities from mining/processing schedule (including described recovery/processing parameters), cost and price assumptions.
Social	• The majority of workforce will be sourced locally. • NGF will establish all relevant agreement with local stakeholders and government agencies.

Criteria	Commentary
Other	• Wattlebird is an existing pit thus an updated Mine Management Plan will need to be submitted with the Western Australian Department of Mines pre-commencement of mining activity. There is no reason to suggest approvals and authorizations will not be granted.
Classification	• The Ore Reserve was classified as Probable in accordance with the JORC Code, corresponding to the resource classifications of Measured and Indicated. No Inferred Mineral Resources were included in the Ore Reserve estimate. • The estimated Ore Reserves and mining method are in the opinion of the Competent Person appropriate for this style of deposit.
Audits or reviews	• The resource and reserve was calculated by NGF personnel. The cost and mining parameters were reviewed internally against existing operations and consideration was made for current practice and cost structure. • It is not expected that practices assumed in the calculation of reserve will vary before the next annual reserve calculation.
Discussion of relative accuracy/ confidence	• All mining estimates are based on Australian costs, and relevant historical cost data. • The local estimate of Ore reserves available for technical and economic evaluation is 392.2Kt at 1.57g/t at a cutoff grade of 0.61g/t for oxide, transitional and fresh prior to processing. • There are no unforeseen modifying factors at the time of this statement that will have any material impact on the Ore Reserve estimate.

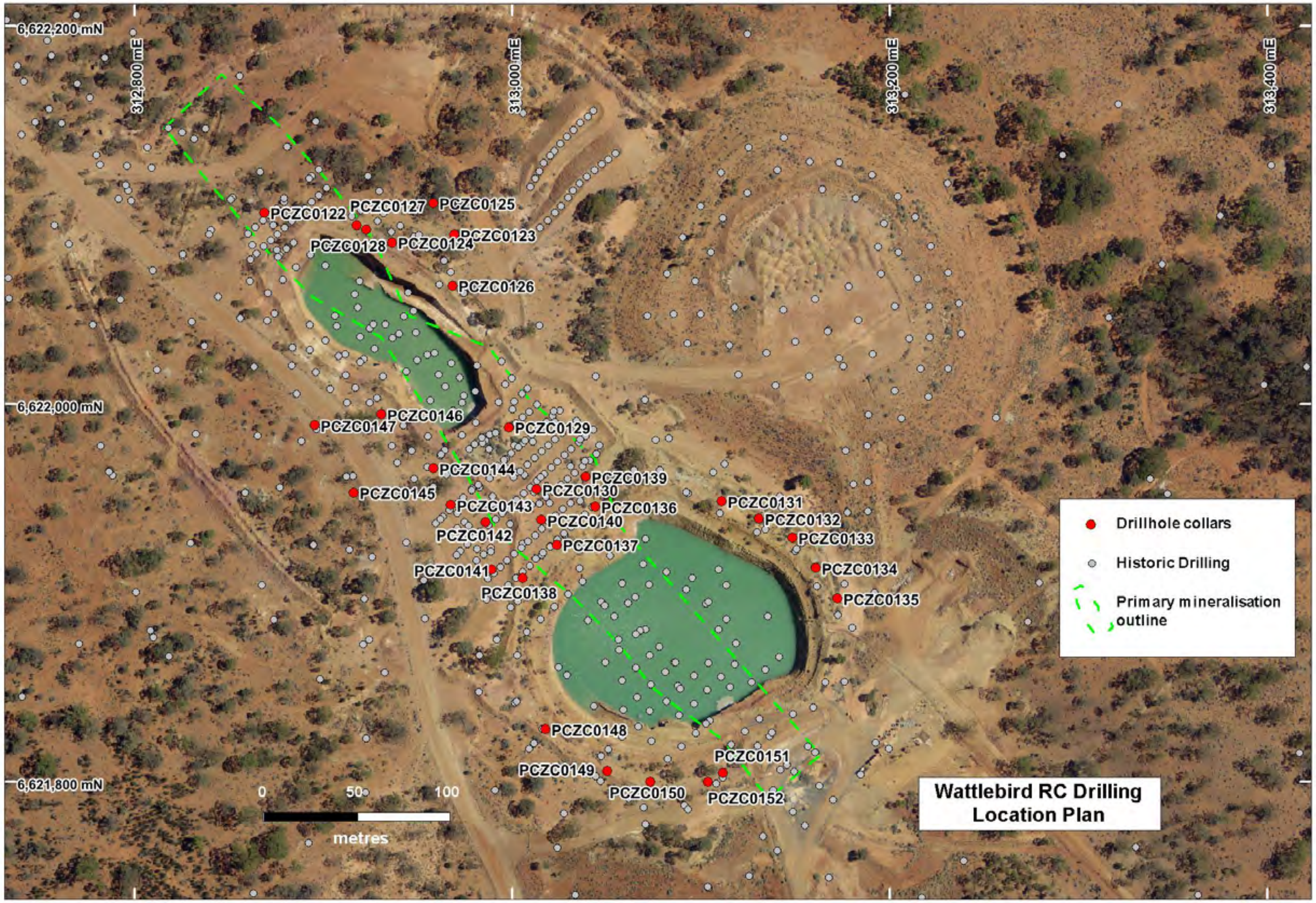
Appendix 1: Table of exploration results – RC Recent Drilling for Wattlebird Deposit

Hole ID	MGA East	MGA North	Dip	Azi	RL	Depth	From (m)	To (m)	DH Width (m)	Grade g/t Au
PCZC0122	312869	6622101	-60	45	401.0	66	20	21	1	2.74
							27	29	2	1.5
							40	41	1	1.12
PCZC0123	312969	6622090	-60	225	398.9	102	70	71	1	2.88
							82	85	3	1.18
							95	100	5	1.3
PCZC0124	312936	6622086	-58	225	399.4	138	11	13	2	2.16
							23	24	1	0.87
							27	28	1	1.34
							33	34	1	2.63
							56	72	16	4.38
							117	118	1	1.04
							121	122	1	0.83
							127	128	1	2.16
PCZC0125	312958	6622106	-60	225	399.0	78	52	53	1	0.95
PCZC0126	312968	6622063	-60	225	399.0	120	34	38	4	9.22
							42	47	5	0.67
							75	88	13	1.64
							99	101	2	2.16
							108	109	1	1.08
PCZC0127	312917	6622095	-53	225	399.8	78	14	16	2	1.18
							52	57	5	1.03
							65	66	1	2.32
PCZC0128	312923	6622093	-90	360	399.7	72	6	7	1	0.83
							22	24	2	2.85
							28	29	1	1.9
PCZC0129	312998	6621988	-58	45	396.3	36	0	2	2	4.45
							29	30	1	17.1
PCZC0130	313013	6621955	-60	45	398.1	54	49	52	3	0.96
PCZC0131	313111	6621948	-60	225	396.9	120	77	79	2	1.55
							83	84	1	2.33
							97	98	1	2.7
PCZC0132	313130	6621939	-53	225	396.9	120	86	120	34	3.52
PCZC0133	313148	6621929	-57	225	396.4	174	100	101	1	1.13
							122	131	9	1.51
							151	153	2	1.29
							161	163	2	1.46
							167	168	1	1.04
							171	173	2	1.39
PCZC0134	313161	6621913	-57	225	396.4	144	98	99	1	1.89
							115	116	1	0.88
PCZC0135	313172	6621897	-60	225	396.4	120	0	1	1	1.32
							87	90	3	1.43

Hole ID	MGA East	MGA North	Dip	Azi	RL	Depth	From (m)	To (m)	DH Width (m)	Grade g/t Au
PCZC0136	313044	6621946	-60	45	398.1	66	32	33	1	3.75
							41	42	1	0.91
PCZC0137	313023	6621925	-60	45	398.4	84	3	4	1	0.95
							30	33	3	1.63
PCZC0138	313005	6621908	-58	45	398.1	66	____	____	____	NSI
PCZC0139	313039	6621962	-58	45	398.4	65	15	16	1	2.11
							19	20	1	1.28
PCZC0140	313015	6621939	-57	45	398.2	84	24	26	2	1.38
							29	34	5	0.85
							63	64	1	8.32
							72	73	1	0.86
PCZC0141	312989	6621912	-60	45	398.1	78	15	16	1	1.09
							40	41	1	1.23
							49	50	1	2.63
							55	56	1	4.03
PCZC0142	312986	6621937	-58	45	398.6	110	9	10	1	4.28
							80	81	1	0.84
							94	95	1	4.88
PCZC0143	312967	6621947	-52	45	398.6	120	28	29	1	0.97
							44	54	10	2.04
							57	60	3	0.99
							64	73	9	1.65
							79	81	2	3.96
							90	92	2	4.26
							95	96	1	1.24
							103	105	2	1.27
PCZC0144	312958	6621966	-55	45	398.9	108	39	42	3	1.06
							45	49	4	1.87
							62	65	3	0.89
							68	69	1	0.97
							72	78	6	2.67
							93	95	2	0.98
PCZC0145	312916	6621953	-53	45	398.8	162	101	102	1	1.71
							105	106	1	2.75
							111	115	4	3.98
							127	129	2	1.16
							132	139	7	6.61
							150	151	1	1.77
PCZC0146	312930	6621995	-54	45	399.5	102	61	64	3	1.11
							70	74	4	0.94
							90	91	1	2.13
							98	99	1	1.05
PCZC0147	312895	6621989	-55	45	399.3	48	____	____	____	NSI
PCZC0148	313018	6621828	-55	45	397.5	114	75	86	11	1.77
							89	91	2	2.44
PCZC0149	313050	6621806	-53	45	397.4	144	51	57	6	1.3

Hole ID	MGA East	MGA North	Dip	Azi	RL	Depth	From (m)	To (m)	DH Width (m)	Grade g/t Au
							118	126	8	5.66
PCZC0150	313073	6621800	-58	45	397.3	144	121	122	1	1.93
							126	132	6	1.29
PCZC0151	313112	6621805	-58	45	396.7	102	64	65	1	0.94
PCZC0152	313103	6621800	-60	45	396.5	120	____	____	____	NSI
Analysis by 30g Fire Assay Results compiled by using a 0.8g/t cut-off grade, no top-cut grade Maximum of 2m internal dilution , minimum interval of 1.0 m										

Appendix 2: A map showing the collar locations of the recent RC drilling at Wattlebird



JORC Code, 2012 Edition – Table 1 Report for Binduli Project Resource Estimates and Reserves (Ben Hur, Nefertiti and Fort Scott Deposits)

Section 1 Sampling Techniques & Data

Criteria	Commentary
Sampling techniques	• Sampling for gold utilised a combination of Reverse Circulation (RC) and Diamond Core (DC) holes. Drilling and sampling for gold has been conducted by various companies since 1987. ***Sampling techniques*** is a summary of drilling and sampling methods as reported by Defiance Mining NL (Defiance), ACM Gold Ltd (ACMG), Croesus Mining NL (Croesus), Placer Dome Asia Pacific Ltd (Placer), Bellamel Mining Ltd (Bellamel) and Norton Gold Fields Ltd (NGF). • Drill hole locations and orientations were designed to allow for adequate coverage across and delineation of the mineralised zones, lithologies and regolith types. Drilling was located on variable 20m x 10m, 20m x 15m, 20m x 20m to 40m x 20m grid spacing’s, with most holes dipping -60^{0} towards local grid east. • Sample representivity is guided by field based observations from geological supervision, logging and other field records referring to sample quality, content and recovery. 1987 to 1991 • Sampling of Defiance Mining RC drilling from 1987 to 1988 was by collection of 2m interval samples beneath a cyclone. RC drilling by Defiance and ACMG from 1989 to 1991 was by collection of 1m interval samples beneath a cyclone. “Representative” 2m sub-samples and 2m or 5m composites of 2-3kg were submitted for fire assay. Where the first pass 2m or 5m composite samples returned values ≥0.5g/t Au or more or ≥0.4g/t Au respectively, the 1m samples were subsequently submitted for analysis. No documentation was located on how the “representative” 1m samples were collected (i.e. if riffle split or spear or scoop sampled). Drilling was by way of Aircore blade for softer material and RC hammer for harder material. • Diamond core was logged and quarter diamond core sampled at generally 1metre or geological intervals before submission to a commercial laboratory for analysis by fire assay for ppm Au. 1993 to 2000 • Sampling of Croesus RC drilling from 1993 to mid-2000 was by collection of 1m interval samples beneath a cyclone into plastic bags and laid in rows of 10 or 20. 5m 2-3kg or 3-4kg PVC spear composites of dry samples (scoop samples if wet) were submitted for fire assay as first pass samples. Where the composite samples returned anomalous values, 1m samples were riffle split on site (scoop sampled if wet), and the resultant 2-3kg or 3-4kg samples submitted for whole sample crush and fire assay for gold determination.

Criteria	Commentary
	• Diamond core was placed directly into core trays. After orientation, logging and photographing half diamond core was sampled on a 1m basis or at smaller intervals and submitted for whole sample grind and analysis using fire assay/ICP for gold determination. Core trays were aluminium tag labelled and placed in storage at the core yard facilities. 2001 Onward • Croesus RC drill samples were collected in large plastic retention bags below a free standing cyclone at 1m intervals, with analytical samples initially formed by composite sampling over 5m intervals. Where samples were dry, analytical composites were formed by spear sampling, where a 50mm diameter plastic pipe is pushed through the drill cuttings in the sample retention bag to the base of the bag and removed carefully with the contents of the pipe containing a representation of the retained metre. Wet RC drill samples where thoroughly mixed in the sample retention bag and 'scooped' sampled to form a composite sample. Five metre composite analytical samples, returning values greater than 0.1g/t gold, were riffle split at 1m intervals where samples were dry, and grab sampled where wet. • All RC composite and 1m split samples were analysed for gold (Fire assay/ICP Optical Spectrometry) • Placer samples were collected every metre from a riffle splitter mounted beneath the cyclone. A 2-3 kg sample for assaying was collected in a calico bag obtained from the riffle splitter (87.5/12.5) for every 1m interval. If bulk samples were too damp for splitting no sample shall be collect while drilling. These bulk samples were spread out and dried in the sun then ripple split. • Samples were sent to a commercial laboratory and analysed for gold (Fire assay) and multi-elements (AAS). • Bellamel RC samples were collected during drilling on 1 metre intervals using a rig-mounted 3-tier riffle splitter. These samples were farmed at the end of the drill hole. A composite spear sample was taken every 4 metres from the sample for analysis. Each composite sample returning an assay of > 0.1g/t Au was resampled on 1m intervals by collecting the corresponding 1m split samples and submitting them for analysis. • All samples were sent to a commercial laboratory and analysed for Au by fire assay (FA50). • NGF RC samples were collected during drilling on 1 metre intervals and passed through a riffle/cone splitter to generate two split samples. The remaining sample from each of the two, metre intervals was collected into a green bag. Holes were grouped into composite and metre subsamples, e.g. if it was determined that from 20 to 30m would compose the mineralized intercept, the individual metre bags would be sent directly to the lab and not composited. Composite samples and duplicates were collected for analysis by several methods. • Using a riffle splitter: Four of the consecutive individual metre subsamples were passed through the riffle again to generate a composite sample. For composite samples that returned anomalous grades (>0.1 g/t), the single metre samples were collected and submitted for analysis. • Composites were collected by scooping samples out of the green bags, if composite results better than 0.2g/t were returned then the single metre samples were collected and submitted for analysis.

Criteria	Commentary
	• All samples, both composite and individual metre samples, were collected into pre-numbered calico bags, which were then placed into green bags and sent to a commercial laboratory. RC sample weights for assay ranged from 2.5 to 4kg. • The analytical method used was 30g fire assay followed by atomic absorption spectroscopy, assaying for gold only, with detection limit of 0.01 ppm. • Croesus, Placer, Bellamel and NGF diamond core samples were collected into core trays and transferred to core processing facilities for logging and sampling. The DC samples were collected at nominated intervals by a Geologist from NQ and HQ half core with a minimum interval of 0.2m and maximum of 1m. Analysis was as for RC samples at a commercial laboratory.
Drilling techniques	• Assay data and geological logging data used for resource estimation were obtained from drill samples collected from either RC or DC drill holes. 1987 to 1991 • RC drilling was completed by various drilling contractors and drill rigs. Bit sizes ranged from 4.25” (105mm) upwards in diameter. Earlier holes were drilled by Aircore blade in relatively soft ground, then RC hammer with cross-over sub where harder ground was encountered. It is unknown if face sampling hammer methods were used for any of these drill programs. • DC drilling was generally HQ size. 1993 to 2000 • RC drilling was completed by various drilling contractors and drill rigs. Early holes were drilled by RC blade in relatively soft ground, and RC hammer where harder ground was encountered. Face hammer sampling using a 5.25” or 5.5” diameter drill bit with a 5” bottom face sampling hammer was introduced in 1996 with drilling rigs equipped with booster compressors. • DC drilling was HQ size (63.5mm diameter) and NQ (50.5mm diameter) core sizes. Drill core was orientated by a bottom of hole spear. 2001 Onward • RC sampling completed using a 5.25” or 5.5” diameter drill bit with a 5” bottom face sampling hammer. RC drilling rigs were equipped with a booster compressor. • DC sampling was a combination of HQ (63.5mm diameter) and/or NQ (50.5mm diameter) core sizes. Drilling was orientated utilizing either a bottom of hole spear, EZI-Mark or ACE system.
Drill sample recovery	• RC drillers are instructed to adopt an RC drilling strategy for the ground conditions advised by geologist expected for each hole to maximize sample recovery, minimize contamination and maintain specified spatial position. • RC drill sample recovery was not recorded quantitatively prior to 2000. Drill sample quality and moisture content was recorded in some

Criteria	Commentary
	instances, but in qualitative terms. Post 2000 RC drill samples were visually logged for moisture content, sample recovery and contamination. • DC contractors use a core barrel and wire line unit to recover the DC, adjusting drilling methods and rates to minimize core loss (e.g. changing rock type, broken ground conditions etc.). Core was orientated, length measured and compared to core blocks denoting drilling depths by the drilling contractor. Any recovery issues are recorded.
Logging	• RC samples are geologically logged. Specifically, each interval is inspected and the weathering, regolith, rock type, alteration, mineralisation and structure recorded. • The entire length of RC holes are logged on a 1m interval basis (i.e. 100% of the drilling is logged). Where no sample is returned due to voids or lost sample, it is logged and recorded as such. DC is logged over its entire length and any core loss or voids are recorded. • For DC, the oriented core was geologically and geotechnically logged, photographed and cut in half. Core loss is recorded in the logging process. • Geological logging is qualitative and quantitative in nature. Logged data is currently captured by a portable data logger utilising LogChief software.
Sub-sampling techniques & sample preparation	1987 to 1991 • Sub-sampling of both RC and DC drill samples prior to submission to the analytical laboratories is described in ***Sampling techniques***. • Sample preparation for both RC and DC was conducted by commercial laboratories and involved drying and pulverising the entire sample to -200 mesh in a chromium steel mill, then riffle splitting to obtain a 50gm sub-sample. Analysis was by fire assay which involved alkali fusion of the sub-sample at 1,100°C for 50 minutes using lead oxide (litharge) as a flux and precious metal collector. The resultant precious metal bearing lead button was then heated under oxidising conditions (cupellation), converting the lead back to lead oxide and leaving a precious metal bearing prill. The prill was then digested in aqua regia and analysed for gold using a flame atomic absorption spectrometer. This technique has a lower level of detection of 0.01ppm Au and an accuracy of ±10% at 10 times the level of detection. 1993 to 2000 • Sub-sampling of both RC and DC drill samples prior to submission to the analytical laboratories is described in ***Sampling techniques***. • The sample preparation has been conducted by commercial laboratories and involves all or part of: oven dried (between 85°C and 105°C), DC jaw crushed to nominal <10mm, riffle split to < 3.5kg as required, pulverized in a one stage process to >85% passing 75um. The bulk pulverized sample is then bagged and approximately 200g extracted by spatula to a numbered paper bag that is used for the 30g or 50g fire assay charge.

Criteria	Commentary
	<u>2001 Onward</u> • Sub-sampling of both RC and DC drill samples prior to submission to the analytical laboratories is described in ***Sampling techniques.*** • The sample preparation has been conducted by commercial laboratories & involves all or part of: oven dried (between 85°C & 105°C), jaw crushed to nominal <10mm, riffle split to 3.5kg as required, pulverized in a one stage process to >85% passing 75um. The bulk pulverized sample is then bagged & approximately 200g extracted by spatula to a numbered paper bag that is used for the 30g or 50g fire assay charge. • RC & DC samples submitted to the laboratory are sorted and reconciled against the submission documents. Routine CRMs & blanks are inserted into the sampling sequence at a rate of 1:25 for standards & 1:75 for blanks or in specific zones at the Geologist's discretion. The commercial laboratories complete their own QC check. Specific diamond drilling campaigns utilized barren quartz flushes between expected mineralized sample interval(s) when pulverizing. • RC field duplicate data was collected routinely and for selected intervals. Field duplicate samples were taken at the time of cone/riffle splitting the bulk sample to maintain sample support. The field supplicates are submitted for assay using the same process mentioned above. The laboratory is unaware of such submissions. A selection of historic RC field duplicates was submitted to the laboratory & underwent a screen fire 50g analysis. Some historic DC duplicates were taken by re-sampling ¼ of the remaining half core. • The sample size (2.5kg to 4kg) relative to the grain size (>85% passing 75um) of the material sampled is a commonly utilised practice for gold deposits within the Eastern Goldfields of Western Australia for effective sample representivity. • RC and DC samples submitted to the laboratories are sorted and reconciled against the submission documents. • Not all phases of drilling to 2000 have complete descriptions of CRM and blank insertion processes. Generally, routine CRMs were inserted into the sampling sequence at rates of 1:20 to 1:25 for standards and 1:75 for blanks or in specific zones at the Geologist's discretion. The commercial laboratories complete their own QC check. • RC field duplicate data is recorded as being collected from 1995. Field duplicate samples were taken consistently from 1996 onwards at the time of riffle splitting the bulk sample to maintain sample support. Field duplicates were submitted for assay using the same process as above. The laboratory is unaware of such submissions.
Quality of assay data & laboratory tests	• The assay methods are designed to measure total gold in the sample. The laboratory procedures are considered appropriate for the testing of gold values in the mineralisation style of this project. The technique involved using a 30g or 50g sample charge with a lead flux which is decomposed in a furnace, with the prill being totally digested by aqua regia before measurement of the gold content by an AAS. • No geophysical tools or other remote sensing instruments were utilised for reporting or interpretation of gold mineralisation. • QC samples were routinely inserted into the sampling sequence and also submitted around expected zones of mineralisation. Standard procedures are to examine any erroneous QC result (a result outside of expected statistically derived tolerance limits) and validate if required; establishing acceptable levels of accuracy and precision for all stages of the sampling and analytical process.

Criteria	Commentary
	• Of the NGF samples submitted, a small proportion were tested for a specified grind size of 90% passing at 75um. This is required from the laboratory. Generally, the samples tested met these criteria. The effect of poor sizing (non-homogeneous sample) can be a cause of bias. • Limited inter-laboratory analysis of selected or “comparability” samples has been carried out for the sampling.
Verification of sampling & assaying	• No holes were twinned. • Primary data was collated and validated by the responsible Geologists to ensure it was correct. Hardcopy data has been migrated to digital format. • No adjustments or calibrations were made to any assay data used in this report.
Location of data points	• On completion of drilling, drill hole collar positions were surveyed by either contract or site-based surveyors. Some earlier drilling was surveyed prior to drilling, but not resurveyed on completion. Survey was by theodolite or differential GPS, to varying precision and accuracy relative to the AHD. • Down hole surveys consist of regular spaced Eastman single shot, electronic multishot surveys (generally <30m apart down hole) and north seeking gyro instruments obtained every 5m down hole. Ground magnetics affect the result of the measured azimuth reading for these survey instruments. • Many of the earlier shallower drill holes (≤50m) were not down-hole surveyed and design azimuth and dip applied. • Data was collected on local grids, AMG84 and/or MGA94 co-ordinates. • Topographic control was generated from survey pick-ups of the area over the last 20 years.
Data spacing & distribution	• Drilling was located on variable 20m x 10m, 20m x 15m, 20m x 20m to 40m x 20m grid spacing, with most holes dipping -60° towards local grid east. • Data spacing and distribution is considered acceptable for establishing geological continuity and grade variability appropriate for classifying a Mineral Resource. • The numbers of drill holes used in the estimations are:

Deposit	RC		DC		Aircore		RAB	
	No Holes	Metres	No Holes	Metres	No Holes	Metres	No Holes	Metres
Ben Hur & Nefertiti	1,181	92,396	71	18,992	714	34,342	1,144	40,659
Fort Scott	121	14,415	0	0	0	0	23	1,128

Criteria	Commentary
	For Ben Hur, Nefertiti and Fort Scott some of the resources were estimated using RC and DC drilling, with Aircore (AC) drilling used for a portion of Ben Hur where AC drilling is predominant. Resource classification has taken into account the use of Aircore drilling. RAB drilling was used to aid interpretation but not for estimation. • Sample compositing intervals for the individual deposits are:

Deposit	Composite Length
Ben Hur	2m
Nefertiti	2m
Fort Scott	2m

Criteria	Commentary
Orientation of data in relation to geological structure	• The drilling directions were designed to intersect the interpreted mineralisation trend at relatively steep angles. • No drilling orientation and sampling bias has been recognised at this time.
Sample security	• Samples are assumed to have been under the security if the respective tenement holders or until delivered to the laboratory where they are assumed to have been under restricted access.
Audits or reviews	• Internal reviews were completed on sampling techniques and data as part of the various operating companies' quality assessment practices.

Section 2 Reporting of Exploration Results

Criteria	Commentary
Mineral tenement & land tenure status	• The Ben Hur, Nefertiti and Fort Scott deposits are located within Mining Licenses M26/420, M26/430, M26/445, M26/446, M26/447 and M26/629. All tenements are 100% held by Bellamel Mining Pty Ltd, a wholly owned subsidiary of Norton Gold Fields. All leases are granted pre-Native Title. The State Government royalty of 2.5% applies on gold produced. Janet Ivy has a royalty based on ore tonnes processed payable to a 3rd party. • The tenements are in good standing and no known impediments exist.
Exploration done by other parties	• All of the historic mining, exploration and resource development for the Binduli deposits was completed by companies which held tenure over the Binduli Project since before 1987 up to 2013. The companies include BHP, Dampier Mining, ACM Gold Ltd (ACMG), Croesus Mining NL (Croesus) Placer Dome Asia Pacific Ltd (Placer), Bellamel Mining Ltd (Bellamel) and Norton Gold Fields Ltd (NGF). Results of exploration and mining activities by these companies aids NGF's exploration, resource development and mining.
Geology	• The regional geology of the area consists of the Ora Banda Domain, constrained by 2 NNW trending shears, the Zulieka shear to the west and the Abbatoir shear to the east. Within this zone lies the Black Flag Group, dated around 2680 Ma, it is a sequence of sediments, felsic volcanics and pyroclastic rocks, which is unconformably overlain by the Kurrawang Formation, dated at 2655 Ma. Several felsic porphyry bodies intrude this area. • Generally the Ben Hur (including Nefertiti) line of deposits extends northwest-southeast in the immediate footwall of the Centurion Fault (CF). Gold mineralisation is hosted in porphyry breccias, folded porphyry's, fine and coarse epi-clastic sediments. The mineralisation is in the form of very shallow west dipping veins that have selectively developed in hematite-magnetite altered feldspar-quartz porphyry, in which the porphyry is decomposed to clays in the upper weathering profile. The supergene gold is typically covered by a leached zone that is 20m to 30m thick. This style of mineralisation is commonly situated directly above primary gold zones, forming a mushroom shaped geometry. There seems to be multiple supergene fronts with moderate dispersion of gold along the supergene blankets. The multiple fronts are likely to be related to fluctuating water tables. Primary gold mineralisation predominately forms in steeply dipping west orientated veins striking ~340˚. The water in the pits prevents observation of primary lodes; a mapping field trip at Binduli suggested that mineralisation at Ben Hur 1 is and in Ben Hur 2 is wedged between a splay of the CF and sheared carbonaceous shales. The drill hole data supports a steep dipping primary structure. The alteration assemblage associated with the gold mineralisation is typically silica-haematite-pyrite-carbonate-sericite. • Locally three dominant lithological features define the Fort Scott project area. These are alluvials and regolith, sediments (conglomerates, sandstones, siltstones and mudstones) and porphyry.

Criteria	Commentary
	Surficial alluvial quartz sands range from fine to medium grained and are found to a maximum depth of 4 meters. Regolith consists of a well-developed saprolite horizon, (both upper and lower saprolite), of variable thickness. Conglomerates in the sequence show a reasonably well constrained range of clast sizes. The majority of conglomerates are pebble through to cobble in clast size. The clast composition within the conglomerates is predominantly sediments ranging from mudstone through to sandstone, though porphyry clasts are also evident. Sandstones range from very fine grained through to very coarse grained. Siltstones and mudstones in diamond holes showed few structural anomalies, mainly in the form of slips and parasitic folds, though in general were little more than planar well bedded units. Porphyries are generally moderately packed, with sub-angular to angular feldspars, and a low quartz concentration. Shearing where present, was weak resulting in a weakly to moderately developed foliation. The porphyry is often strongly sericite altered and can also show weak to moderate haematite alteration, while magnetite may or may not be present. Supergene mineralisation is confined to the saprolitic horizon and coincides with elevated hematite levels and infrequently minor pyrite. Primary gold mineralisation is vein hosted in sediments and porphyries. Mineralisation is commonly associated with the combined presence of pyrite and sericite alteration, ± hematite alteration.
Drill hole Information	• See Sections 1 and 3.
Other substantive exploration data	• No unreported exploration data has been collected relevant to these deposits considered material to this announcement.
Further work	• Further work will include re-estimation of the Ben Hur, Fort Scott and Fort William deposit resources and mining studies appropriate to NGF’s current open-cut mining methods. Review of mineralisation for bulk mining/ heap leach technology is in progress.

Section 3 Estimation & Reporting of Mineral Resources

Criteria	Commentary
Database integrity	• Data is hosted on an SQL backend database with Geologists interfacing via the Maxwell Geoservice's DataShed front end. User access to the database is controlled via user permissions which are configured both at the group level by Systems Administration and the user level by the Database Administrator. Field and project Geologists are responsible for data entry. Existing protocols maximize data functionality and quality whilst minimizing the likelihood of error introduction at primary data collection points and subsequent database upload, storage and retrieval points. Data templates with lookup tables and fixed formatting are used for collecting primary data on field laptops. The software has validation routines and data is subsequently imported into a secure central database. • The SQL server database is configured for validation through constraints, library tables, triggers and stored procedures. Data that fails these rules on import is rejected or quarantined until it is corrected. • Database is centrally managed by a Database Manager who is responsible for all aspects of data entry, validation, development, quality control and specialist queries. There is a standard suite of rigorous validation checks for all data.
Site visits	• The Competent Person for this update is a full time employee of NGF and undertakes regular site visits ensuring company standards of the Mineral Resource estimation process from sampling through to final block model. • The deposit area is a recently active mining area for NGF and as such regular site visits have been undertaken.
Geological interpretation	• The high confidence of the geological interpretation is based on geological knowledge acquired from detailed geological DC and RC logging, assay data, and data obtained from mining of adjoining deposits. • The dataset (geological mapping, RC and DC logging, assays etc.) is considered acceptable for determining a geological model. Key interpretation assumptions made for this estimation are the existence of supergene zones at the oxide and transitional interfaces as distinct from the primary mineralisation. • The geological interpretation is considered robust overall, with no known alternative interpretations. • The geological interpretation is specifically based on identifying particular geological structures, weathering profiles, associated alteration and gold content. • Whilst the geological features are deemed to be continuous, the gold distribution within them can be highly variable.

Criteria	Commentary
Dimensions	• Mineral Resource dimensions for the deposits are:

Deposit	Mineralisation Length	Primary Mineralisation Dip	Primary Horizontal Mineralisation Width	Vertical Depth Extents
Ben Hur	3,550m striking 335̊	-50̊ to -85̊ towards 235̊	Multiple lodes, 2m up to 20m	From 10m to 300m below surface
Nefertiti	240m striking 325°	-15° towards 55°	Single lode 200m to 260m wide	From 30m to 100m below surface
Fort Scott	385m striking 325̊	-30̊ to -70̊ towards 235̊	Multiple lodes, 2m up to 20m	From 30m to 130m below surface

- Resource model extents are:

Deposit	Grid		Easting	Northing	Elevation
Ben Hur	GDA94	Minimum	348,350	6,584,193	-200
		Maximum	349,730	6,586,913	370
Nefertiti	GDA94	Minimum	349,015	6,584,125	190
		Maximum	349,695	6,584,665	370
Fort Scott	GDA94	Minimum	344,640	6,593,200	150
		Maximum	345,080	6,593,850	380

<table>
<tr><th>Criteria</th><th>Commentary</th></tr>
<tr><td>Estimation & modelling techniques</td><td>
Estimation techniques and top cuts applied are:
<table>
<tr><th>Deposit</th><th>Estimation Method</th><th>Minimum Block Size (Ym x Xm x Zm)</th><th>Top Cut (g/t Au)</th><th>Composite width</th></tr>
<tr><td>Ben Hur</td><td>Multiple Indicator</td><td>5 x 5 x 2.</td><td>None</td><td>2m</td></tr>
<tr><td>Nefertiti</td><td>Ordinary Kriging</td><td>5 x 5 x 2.</td><td>7</td><td>2m</td></tr>
<tr><td>Fort Scott</td><td>Ordinary Kriging</td><td>5 x 5 x 2.5</td><td>6 to 9</td><td>2m</td></tr>
</table>

Mining production data for Janet Ivy and Navajo Chief was utilised in the estimation process and compared with the estimation results.
No assumptions were made regarding recovery of by-products during the Mineral Resource estimate.
The estimation of deleterious elements was not considered material to this style of mineralisation.
Selective mining units (SMUs) of 5m x 5m x 2.5m were assumed for Ben Hur, Nefertiti and Fort Scott.
Interpreted wireframes for the estimation domains, and regolith and topographical files were used to define the resource estimate. Blocks within the models were coded based on these surfaces.
The Mineral Resource estimates were validated by:

<table>
<tr><th>Deposit</th><th>Validation Methods</th></tr>
<tr><td>Ben Hur</td><td rowspan="3">Visual against raw drill data and statistical analysis of average block grade against the average 2m composite grades.</td></tr>
<tr><td>Nefertiti</td></tr>
<tr><td>Fort Scott</td></tr>
</table>
</td></tr>
<tr><td>Moisture</td><td>
Tonnages are estimated on a dry basis.
</td></tr>
<tr><td>Cut-off parameters</td><td>
Reporting cut-off grades are:
<table>
<tr><th>Deposit</th><th>Reporting Cut-off Grade (g/t Au)</th></tr>
<tr><td>Ben Hur</td><td>0.5</td></tr>
<tr><td>Nefertiti</td><td>0.5</td></tr>
<tr><td>Fort Scott</td><td>0.7</td></tr>
</table>
</td></tr>
<tr><td>Mining factors or assumptions</td><td>
The resource is likely to be mined by open cut mining. Open cut mining scenario is likely to utilise an excavator to mine 2.5m or 5m flitches. Mining methods are based on current open pits for NGF.
</td></tr>
</table>

Metallurgical factors or assumptions	• No assumption or factors have been applied to the resource estimate regarding the metallurgical amenability. • Reasonable assumptions for metallurgical extraction are based on previous processing of the ore from the nearby deposits Janet Ivy and Navajo Chief through the Paddington Mill (owned by NGF). The mill utilises a CIP extraction process. • Target gold recoveries would range from 93% to 96% recovery.
Environmental factors or assumptions	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining and milling history of existing open pit operations with the project area.
Bulk density	• In-situ bulk densities applied to the resource estimates were based on those used in previous studies and estimates.
Classification	• The calculations utilised all available data and are depleted for known workings. • JORC resource classification was based on search parameters including search distance and number of informing samples, and on data quality, including the existence, availability and quality of QC. • Ben Hur and Nefertiti were classified as Inferred only. • The classification result reflects the view of the Competent Person.
Audits or reviews	• The Mineral Resources have not been externally audited.
Discussion of relative accuracy/ confidence	• The Mineral Resources has been reported in accordance with the guidelines of the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves and reflects the relative accuracy of the Mineral Resources estimate. The Competent Person deems the process to be in line with industry standards for resource estimation and therefore within acceptable statistical error limits. • The statements relates to global estimates of tonnes and grade for likely open pit mining and processing scenarios.

Section 4 Estimation and Reporting of Fort Scott Ore Reserves

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• A Whittle optimization and pit design was carried out for Fort Scott by NGF personnel in August 2014. The pit design parameter complies with safety parameters based on existing NGF's open pit procedures. The pit design comprises Probable Reserves of 273.5Kt at 1.36g/t at a cutoff grade of 0.75g/t for oxide, transitional and fresh. • The Mineral Resources are reported inclusive of the Ore Reserves.
Site visits	• Fort Scott has been visited by Guy Simpson (GM Technical Services "NGF" & CP for Reserves) within the last 6 months. • Fort Scott is a Greenfield site and is situated between Fort William and Janet Ivy.
Study status	• NGF Technical Services Department created a pit design for the Fort Scott mineral deposit. The optimization study was based on Whittle optimization using a selling price of $AUD1, 400/Oz with 2.5% Royalty. • The block model used for both Whittle optimization and Pit design is "fs_ok_mga_jun14.mdl". • Modifying factors such as mining loss, mining dilution and recoveries have been applied. • Operating cost used was based on "NGF's small digger fleet cost model" with average processing cost of $28.28/t.
Cut-off parameters	• A cutoff grade of 0.75g/t for oxide, transitional and fresh rock. • The cutoff grade applied is shown by; $\text{Cut} - \text{off Grade} = \frac{\text{Mining Dilution x Processing Cost}}{\text{Processing Recovery x (Selling Price} - \text{Selling Cost)}}$ • Selling price = AUD$1,400/Oz. • State Royalty = 2.5%. • Metallurgical recovery = 94%. • Processing cost = $28.28/t.
Mining factors or assumptions	• The method used to convert Mineral resource to Ore Reserves is based upon a pit optimization identifying the economic shell within which a practical mining design can be applied to. • The mining method will be based on conventional open pit mining with diesel trucks and shovels. For Fort Scott, "NGF's small digger fleet model" will be used to optimize the reserve. • As NGF is an owner operator Fort Scott's operating model will be based on the pit being mined by NGF.

Criteria	Commentary
	• The Ore reserve estimate was created using DCF methodology within “Whittle” open pit optimization software in order to select the most appropriate and economically viable pit shell taking into account minimum mining width for the chosen equipment fleet. • Geotechnical slope design parameters were applied based on geotechnical domains/zones within the mining model. • An ore loss allowance of 5% and a mining dilution of 10% are anticipated with this type of operation based upon historical data in similar scale and type of operation. • An overall minimum mining width of 30m was applied. • No inferred and or unclassified material has been included in the reserves. • Gold Price used = $AUD1, 400/Oz. • Processing cost = $28.28/t. • Infrastructure requirement for open pit mining includes; A workshop for all mobile equipment for maintenance requirements, offices, crib rooms and amenities, explosives storage, water dams and communication. Most of these infrastructures have to be erected on site before mining can commence.
Metallurgical factors or assumptions	• No metallurgical test work was undertaken by NGF on Fort Scott. • Ore from Fort Scott will be delivered via road trains to NGF’s Paddington processing facilities. • Paddington Mill is based on conventional carbon in pulp technology and has achieved an annual throughput of 3.72 million tonnes in 2014 with average feed grade of 1.67g/t with average recovery of 88.88%. • A recovery factor of 94% have been applied to Fort Scott’s oxide, transitional and fresh rock types as the ore will be blended with Paddington’s other ore sources to be able to achieve this recovery factor.
Environmental	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. • All proposed operation and operational plans are within local historical practices and existing operational standards.
Infrastructure	• The site is serviced by a haul road which is capable of handling 100t road trains. • The site is considered a greenfield site thus before mining can commence infrastructure including electricity, water, offices, core facility, crib rooms, explosives storage, water dams and communications have to be in place.
Costs	• Fort Scott’s reserve estimate was based on a gold price of $AUD 1,400/Oz. • Allowance has been made for the 2.5% state government royalty. • Operating cost used was based on “NGF’s small digger fleet cost model” with average processing cost of $28.28/t. • No penalties assumed and no deleterious elements in concentrate.

Criteria	Commentary
Revenue factors	• Financial analysis in this report is based on a gold price of $AUD 1,400/Oz. • The gold Dore is planned to be transported via recognized security service from gold room of Paddington processing plant to the gold refinery in Perth. • Contract payments and terms are expected to be typical of similar contracts for the refining and sale of Dore produced from other operations within Australia. • Allowance has been made for the 2.5% state government royalty.
Market assessment	• Historical gold price and forward looking estimates have been used for the gold price. Price flexing and sensitivity analysis have been carried out to determine the robustness of the project viability. • The cash flow was modelled in real terms and no price or cost escalations were applied.
Economic	• Inputs to economic analysis include factors described above including ore and metal quantities from mining/processing schedule (including described recovery/processing parameters), cost and price assumptions.
Social	• The majority of workforce will be sourced locally. • NGF will establish all relevant agreement with local stakeholders and government agencies.
Other	• Fort Scott is a Greenfield site thus a new Mine Management Plan will need to be submitted with the Western Australian Department of Mines pre-commencement of mining activity. There is no reason to suggest approvals and authorizations will not be granted.
Classification	• The Ore Reserve was classified as Probable in accordance with the JORC Code 2012, corresponding to the resource classifications of Measured and Indicated. No Inferred Mineral Resources were included in the Ore Reserve estimate. • The estimated Ore Reserves and mining method are in the opinion of the Competent Person appropriate for this style of deposit.
Audits or reviews	• The resource and reserve was calculated by NGF personnel. The cost and mining parameters were reviewed internally against existing operations and consideration was made for current practice and cost structure. • It is not expected that practices assumed in the calculation of reserve will vary before the next annual reserve calculation.
Discussion of relative accuracy/ confidence	• All mining estimates are based on Australian costs, and relevant historical cost data. • The local estimate of Ore reserves available for technical and economic evaluation is 273.5Kt at 1.36g/t at a cutoff grade of 0.75g/t for oxide, transitional and fresh prior to processing. • There are no unforeseen modifying factors at the time of this statement that will have any material impact on the Ore Reserve estimate.

JORC Code, 2012 Edition – Table 1 Report for Mulgarrie Well Resource and Reserve Estimates December 2014

Section 1 Sampling Techniques & Data

Criteria	Commentary
Sampling techniques	• Sampling completed utilising a combination of Reverse Circulation (RC) & Diamond Core (DC) holes on 25m x 25m to 50m x 50m grid spacing. Drilling & sampling has been conducted by various companies since late 1986 & includes exploration & resource development. Sampling techniques are summarised from drilling & sampling manuals/reports by BHP Minerals International (1986-1990), Newcrest Mining Limited (1990-1995), Delta Gold NL (1995-2002), Placer Dome Asia Pacific (2002-2005), Barrick (2005-2007) & Norton Gold Fields Ltd (2007 to present). Drilling & sampling conducted by BHP & Newcrest between 1986 &1995 is considered as legacy data due to the missing detail of the dataset. This drilling accounts for 7.5% of the dataset. The legacy data was used to generate resource estimates forming the basis of reserve estimates & subsequent mining between 1986 & 1990. Reconciliation data from this mining period & further drilling was used to assist with determining the integrity of the legacy data. • The drill hole locations were designed & oriented to allow for spatial spread of samples across mineralised zones & different rock types. • Field based observations from geological supervision & geological records referring to sample quality, moisture content & recovery were used as a guide to sample representivity. • All RC-recovered samples were passed through a splitting device (cone or riffle splitter) at 1m intervals to obtain a sample for assay. Target RC sample weights range from 2.5 to 4kg across all RC drilling campaigns (1986-2013). Bulk reject sample was also collected into a plastic bag for each metre. Spear samples, composited up to 5m, were collected from the bulk samples as a first-pass sampling technique. Single metre samples were collected & submitted for assay from areas of expected mineralisation or composite anomalism. • DC samples were placed into core trays at the rig & transferred to core processing facilities for logging, sawing/splitting & sampling. The DC samples are collected at nominated intervals by a Geologist from resultant half core with a minimum interval of 0.2m & a maximum of 1m. • Samples were submitted to commercial laboratories for assay. Sample preparation, summarised for all drilling campaigns (1986-2013), included all or part of: oven dry between 85°C & 105°C, jaw-crushing (nominal 10mm) & splitting to 3.5kg as required, pulverize sample to >85% passing 75um. Samples were either assayed by Aqua Regia digest or from a 30g or 50g fire assay charge. Analysis was completed via Atomic Absorption Spectrometry (AAS).
Drilling techniques	• All assays referred to for resource estimation (1986-2013) were collected from either: RC (39% of the dataset), RC grade control (55% of the dataset) or DC (6% of the dataset) drilling using a drilling contractor. The most recent drilling campaign accounts for around 2.4% of the total drilling dataset.

Criteria	Commentary
	• RC sampling completed using a 4.5” to 5.5” diameter drill bit with a face sampling hammer (1992 to 2013). RC drilling rigs were equipped with a booster compressor. DC sampling is a combination of HQ (63.5mm diameter) and/or NQ2 (50.5mm diameter) or NQ3 (45mm) core sizes. DC is orientated by either a bottom of hole spear, EZI-Mark or ACE system. • In the case of utilising diamond tails, RC pre-collars are up to 250m deep. This technique was employed to effectively drill down to the mineralisation & collect DC through this zone.
Drill sample recovery	• RC Drillers are advised by geologists on the ground conditions expected for each hole & instructed to adopt an RC drilling strategy to maximize sample recovery, minimize contamination & maintain required spatial position. • All RC 1m samples are collected into a UV resistant bag. Samples are visually logged for moisture content, estimated sample recovery & contamination. The DC samples are orientated, length measured & compared to core blocks denoting drilling depths by the drilling contractor. Any recovery issues are recorded. Sample loss or gain is reviewed at the time of drilling & feedback is provided to the drilling contractor to ensure the samples are representative. All samples sent to the laboratory are weighed & monitored to ensure that they are representative. • DC contractors use a core barrel & wire line unit to recover the DC, adjusting drilling methods & rates to minimize core loss (e.g. changing rock type, broken ground conditions etc.). • A study of the weights of the 1m RC sample splits & gold grades (2013 drilling) show no correlation between the two. The drilling contractors utilized drilling techniques to ensure minimal loss of any size fraction.
Logging	• All current RC samples are geologically logged at the detail of 1m intervals to support Mineral Resource estimation; in some historic RC drilling, samples were selectively logged. Geological features that are logged included: weathering, regolith, rock type, alteration, mineralisation & structure. All DC is logged for core loss, marked into 1m intervals, orientated, structurally logged, geotechnically logged & geologically logged for the following parameters: weathering, regolith, rock type, alteration, & mineralisation. • Geological logging is qualitative & quantitative in nature. • RC holes are logged on a 1m interval basis. Where no sample is returned due to voids or lost sample, it is logged & recorded as such. DC is also logged over its entire length & any core loss or voids are recorded.
Sub-sampling techniques & sample preparation	• Assays from DC are all half core samples, the remaining DC resides in the core tray & archived. • All RC samples were split by a cone or a riffle splitter & collected into a sequenced calico bag. For historical drilling, any wet samples that could not be riffle split initially were dried then usually riffle split. • The sample preparation conducted by commercial laboratories involves jaw crushing to nominal <10mm (where required), a riffle split to 3.5kg as required, & pulverising in a one stage process to >85% passing 75um. The bulk pulverized sample is then collected & approximately 200g extracted by spatula to a numbered paper bag that is used for the 30g or 50g fire assay charge or aqua regia digest.

Criteria	Commentary
	Laboratory Quality Control (QC) includes duplicate samples collected after the jaw crushing stage, & repeat samples collected after the pulverising stage to provide data confirming the accuracy & precision of the preparation technique. All sub-subsampling & lab preparations are consistent with other laboratories in Australia are certified by the laboratory. • RC & DC samples submitted to the laboratory are sorted & reconciled against the submission documents. The commercial laboratories complete their own QC check. • RC field duplicate data was collected routinely & for selected intervals suspected to contain mineralisation. Field duplicate samples were taken at the time of cone/riffle splitting the bulk sample at the drill rig to maintain sample support. The field duplicates are submitted for assay using the same process mentioned above, with the laboratory unaware of the duplicate nature. No DC duplicates have been collected. • Sample sizes are considered appropriate to the grain size of the material being sampled on the basis of satisfactory duplicate correlations at all stages of the sample comminution process.
Quality of assay data & laboratory tests	• The assaying & laboratory procedures are designed to measure total gold in the sample. The laboratory procedures are considered appropriate for the testing of gold at this deposit, given the reconciliation data. • The fire assay technique involved using a 30g, 40g or 50g sample charge with a lead flux, which is decomposed in a furnace, with the prill being totally digested by 2 acids (HCl & HN03) before measurement of the gold content by an AAS machine. Aqua regia is a process of dissolving pulverised mineral sample into solution by a series of acids (HCl & HNO3); heat is added as a catalyst. An organic solvent is added before analysis is completed by an AAS machine. This analysis was completed for samples within the regolith profile where the technique is considered as total gold analysis technique. • No geophysical tools or other remote sensing instruments were utilised for reporting or interpretation of gold mineralisation. • RC & DC samples submitted to the laboratory are sorted & reconciled against the submission documents. Certified Reference Material (CRM) (standards & blanks) are inserted into the sampling sequence at a rate of 1:115 for standards or in specific zones at the Geologist’s discretion. The commercial laboratories undertake their own QC checks. Both RC and diamond drilling campaigns utilised barren quartz flushes between expected mineralised sample interval(s) when pulverizing. • Standard procedures are to examine any erroneous QC result (a result outside of expected statistically derived tolerance limits) & validate if required; establishing acceptable levels of accuracy & precision for all stages of the sampling & analytical process.
Verification of sampling & assaying	• Independent verification of significant intersections not considered material. • No twinned holes were completed. An analysis of grade control drilling in close proximity to the resource drilling was completed, comparing assay grades. Overall, economic assay values in the resource drilling compare to the grade control sample values. The mean

Criteria	Commentary
	grade of assays from the grade control dataset, for within the current open pit, are 0.3 g/t Au higher than for the resource assays for the same volume. • Primary logging & sampling data is sent digitally every 2-3 days from the field to the company's Database Administrator (DBA). The DBA imports the data into a relational database. When assay results are received electronically from the laboratory, results & laboratory QAQC are also imported into the database after further validation checks. The responsible Geologist reviews the data in the database to ensure that it is correct & has merged properly & that all data has been received & entered. Any variations that are required are recorded permanently in the database. • No adjustments or calibrations were made to any assay data used in this report.
Location of data points	• All drill holes used in the resource estimation have been surveyed for easting, northing & reduced level. Recent data is collected in MGA 94 Zone 51 & AHD. Data pre-2012 is collected in local grid or AMG 84 Zone 51 & AHD. • Drill hole collar positions are surveyed by the site-based survey department (utilsing a differential GPS or conventional surveying techniques, with reference to a known base station) with a precision of less than 0.2m. • Down hole survey methodologies are missing from the dataset pre 2002. Historic reports document surveys were conducted utilising down hole tools but lack adequate description. Down hole surveys for drilling conducted post 2002 were completed utilising a north-seeking down hole gyro tool. • Topographic control was generated from survey pick-ups of the area over the last 20 years, which have been used to generate a Digital Terrain Model (DTM).
Data spacing & distribution	• The nominal drill spacing is 25m x 25m with some areas from 12m x 12m up to 50m x 50m for the distil parts of the resource (and past 150mRL). This spacing includes data that has been verified from previous exploration activities on the project. • Data spacing & distribution is considered sufficient for establishing geological continuity & grade variability, appropriate for classifying a Mineral Resource. • Samples were composited to 2m down hole prior to modelling to assist with the effects of volume variance & decrease grade variability.
Orientation of data in relation to geological structure	• The drilling is orientated at a high angle to the gross ore zone geometry (NW-strike, moderate NE dip). This orientation is sub-parallel to the known orientation of the smaller scale gold-bearing structures. The sampling, for the most part, is sub-parallel to the mineralisation. In this instance, assay results appear to be highly variable, but assist with delineating the gross ore-zone morphology (along with identifying other geological features of the ore zone).

Criteria	Commentary
	• A geostatistical study of the assay results for the grade control (drilled & sampled at a high angle to the mineralised structures) data & the resource assay results (drilled sub-parallel to the mineralised structures) shows that the resources assays report 20% lower than the grade control assays (for the same volume).
Sample security	• Historic samples are assumed to have been under the security of the respective tenement holders/operators until delivered to the commercial laboratory where samples would be expected to have been under restricted access. • Samples collected between 2012 & 2013 were all under the security & custodial chain of NGF employees until delivered to ALS Kalgoorlie laboratory some 30km south, where they were received in a secured fenced compound security with restricted entry. Internally, ALS operates an audit trail, tracking the samples at all times whilst in their custody.
Audits or reviews	• Internal reviews are completed on sampling techniques & data as part of the Norton Gold Fields continuous improvement practice. No external or third party audits or reviews have been completed.

Section 2 Reporting of Exploration Results

Criteria	Commentary
Mineral tenement & land tenure status	• The Mulgarrie Well deposit is located within Mining License M27/38. The ML is 100% held by Norton Gold Fields Ltd. No heritage or historical sites exist within the tenure. M27/38 was granted pre-Native Title. Third party royalties are applicable to these tenements & are based on production ($/t) or proportion of net profit. All production is subject to a WA state government NSR royalty of 2.5%. • The tenements are in good standing & no known impediments exist.
Exploration done by other parties	• A significant proportion of exploration, resource development & mining was completed by companies which held tenure over the Mulgarrie Well deposit since the mid 1980's. Companies included: Broken Hill Proprietary Limited (pre 1990), Newcrest Mining PL (1990-1995), Delta Gold (1996-2002), Placer Dome Asia Pacific (2002-2005) & Barrick Kanowna (2005-2007). Results of exploration & mining activities by the afore-mentioned companies has assisted in Norton Gold Field's more recent exploration, resource development & mining in the area. Reporting of results here within only relates to results previously not required to have been reported to the ASX by Placer Dome Asia Pacific and Barrick.
Geology	• The deposit type is classified as an orogenic gold deposit within the Norseman-Wiluna greenstone sequence. The accepted interpretation for gold mineralisation is related to (regional D2-D3) deformation of the stratigraphic sequence during an Archaean orogeny event. The mineralisation is hosted within a komatiite unit in fault contact with a high-magnesium basalt unit. The metamorphic grade is defined as lower green-schist facies.

Criteria	Commentary
	- The mineralisation is located in brittle deformation zones within carbonate alteration pods, associated with thrust-faulting along the komatiite/high-magnesium basalt contact.
Drill hole Information	- See Appendix 1.
Data aggregation methods	- All reported assay results have been length weighted; no top cuts have been applied. Assay results are reported to a 0.8g/t Au lower cut over a minimum intersection of 1m. A maximum of 2m of internal dilution (i.e. <2m @ <0.8g/t Au) is included for reporting RC intercepts. - No metal equivalent values are used for reporting exploration results.
Relationship between mineralisation widths & intercept lengths	- Drill hole intersections are generally at a high angle to each mineralised zone. Reported down hole intersections are noted as approximate true width, or otherwise are denoted as 'true width not known'.
Diagrams	- See Appendix 2
Balanced reporting	- All results have been reported relative to the intersection criteria.
Other substantive exploration data	- No other exploration data collected is considered material to this announcement.
Further work	- Further work will include mining studies to determine if the project economics can support larger scale open pit mining of the deposit.

Section 3 Estimation & Reporting of Mineral Resources

Criteria	Commentary
Database integrity	- NGF employs SQL as the central data storage system using DataShed software as a front-end interface. User access to the database is regulated by specific user permissions, & validation checks & relational steps are part of the process to ensure data remains valid - Existing protocols maximize data functionality & quality whilst minimizing the likelihood of error introduction at primary data collection points & subsequent database upload, storage & retrieval points. Data templates with lookup tables & fixed formatting are used for collecting primary data on field laptops. The software has validation routines & data is subsequently imported into a secure central database. - The SQL server database is configured for validation through constraints, library tables, triggers & stored procedures. Data that fails these rules on import is rejected or quarantined until it is corrected.

Criteria	Commentary
	• Database is centrally managed by a Database Manager who is responsible for all aspects of data entry, validation, development, quality control & specialist queries. There is a standard suite of vigorous validation checks for all data.
Site visits	• The Competent Person for this update is a full time employee of NGF & undertakes regular site visits ensuring all facets of the Mineral Resource estimation process from sampling through to resource estimation are of a satisfactory level. • The deposit area is an active mining area for NGF & as such regular site visits were undertaken during this update.
Geological interpretation	• The high confidence of the geological interpretation is based on geological knowledge acquired from the open pit production data, detailed geological DC & RC logging, assay data & pit mapping. • The dataset (geological mapping, RC & DC logging, assays etc.) is considered acceptable for determining a geological model. Key interpretation assumptions made for this estimation are: (1) where geological relationships were interpreted but not observed; & (2) the interpretation of the mineralisation past known drilling limits (extrapolated a reasonable distance considering geological & grade continuity – not more than the maximum drill spacing). • The geological interpretation is considered robust & alternative interpretations are considered not to have a material effect on the Mineral Resource. As additional geological data is collated, the geological interpretation is continually being updated. • The geological interpretation is specifically based on identifying carbonate alteration within the komatiite unit & quartz veining to define the mineralised envelope. The Tertiary boundary & regolith boundaries are also identified, assisting with interpreting secondary mineralisation processes. • Whilst the geological features are deemed to be continuous, the gold distribution within them can be highly variable. This issue is mitigated by close-spaced sampling & ensuring sample & analytical quality is high. Historic mining data is also used to assist with understanding grade continuity. Geological structures post-dating the mineralization can off-set & truncate the mineralisation affecting the geological continuity & are difficult to isolate.
Dimensions	• The Mulgarrie Well deposit is spatially located between 356,360mE & 357,200mE & 6,638,300mN to 6,639,000mN (MGA94 zone51). 2 domains were modeled (including a waste domain) & 3 subdomains (based on regolith profiles). • Mineralisation at the Mulgarrie Well deposit is controlled by structural & stratigraphic features that have a known dip extent of 150m (starting from 330mRL).
Estimation & modelling techniques	• The estimation was completed using a non-linear interpolation technique – Multiple Indicator Kriging (MIK). MIK is an interpolation method better suited to geological domains having a highly skewed composite dataset distribution. • Geological domains were based on the geological interpretation & mineralised trends. 3DM wireframes were created by sectional interpretation of the drilling dataset. Where there was geological uncertainty, domain boundaries were modelled to a 0.3 g/t Au lower cut. Domain boundaries were treated as soft boundaries.

Criteria	Commentary
	• 2m down hole composites for all drilling were created & subdivided into each domain using an inside/outside principle. • The composite dataset for each domain was divided into 14 indicator thresholds. The statistics for each indicator threshold were reviewed. Spatial continuity modelling was completed for each indicator threshold, within each domain. Directions of continuity were similar to interpreted controls on mineralization with varying degrees of anisotropy. • Sample search ellipses were set based on data spacing in similar orientation to the major mineralized orientation. Minimum & maximum samples were set for each sample search based on accepted levels of grade continuity. Search distances were based on sample spacing & spatial continuity. A total of 3 search passes were conducted with progressively relaxed search criteria to accommodate the data density from the closest to the widest spaced drilling at 50m x 50m. • Panel histograms generated at sample support & were adjusted to reflect open cut mining with a selectivity of around 5m(X) by 5m(Y) by 2.5m(Z). This correction factor was selected to give recoverable resources for likely mining practices. • Estimation was completed using GS3 resource modelling software & imported into Surpac V6.4 mining software, utilizing the block modelling module. • Historic Inverse Distance Squared (IDS) & MIK models were used as check estimates. An MIK model utilising the grade control data was also generated to compare with the estimation result. Several MIK check estimates, with different estimation parameters, were generated to compare with the estimation result. • Reconciliation data was used to compare to the estimation result. • No assumptions were made regarding recovery of by-products during the Mineral Resource estimate. • The estimation of deleterious elements was not considered material to this style of mineralization. • Block model dimensions were set to 356,360mE & 357,200mE & 6,638,280mN to 6,638,960mN & between 400mRL & -50mRL. Block sizes were chosen to compromise between sample spacing & orientation of mineralisation i.e. 20m(X) by 20m(Y) by 5m(Z). • A selective mining unit of 5m(X) by 5m(Y) by 2.5m(Z) was assumed. • No correlation between variables was necessary. • The three dimensional model & digital terrain models for the estimation domains, regolith & topographical files were used to constrain the resource estimate. Blocks from the block model were coded based on these volumes/surfaces by either block centroid in/out of 3DM or above/below a DTM surface. • Outlier grades within the top two indicator thresholds of each domain were managed by substituting the mean grade with the median grade. • Model validation has been completed using visual & numerical methods & formal peer review sessions by key geology staff.

Criteria	Commentary
	• Mineral Resource model has been validated visually against the input composite/raw drill hole data with spot checks carried out on a number of block estimates on sections & plans.
Moisture	• Tonnages are estimated on a dry basis.
Cut-off parameters	• Cut-off parameters are 0.7g/t Au. Cut-off parameters are based on current NGF mining (open cut) & milling costs.
Mining factors or assumptions	• The resource is likely to be mined by open cut mining. The currently planned Open cut mining scenario utilises an excavator to mine 2.5m flitches. • Mining methods are based on current open pit & underground mining operations for NGF.
Metallurgical factors or assumptions	• An assumption was made that metallurgical recoveries would support economic mining of the resource. Reasonable assumptions for metallurgical extraction are based on processing Mulgarrie ore through the Paddington processing plant between 1997 & 1998. The processing plant utilized a CIP extraction process. • Target gold recovery is expected to be 94% for oxide, transitional & fresh ore. The oxide & transitional range of recoveries is based on milling data from the adjoining Mulgarrie milling campaigns. Fresh rock recovery data is based on metallurgical test work of un-weathered diamond core.
Environmental factors or assumptions	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining & milling history of existing open pit & underground operations with the project area.
Bulk density	• Insitu-bulk densities (ISBD) (dry basis) applied to the resource estimate were based on systematic test work completed on hand specimens & DC for selected material types. The ISBD determination method is based on a water immersion technique. The ISBD test work reconciles against production tonnages from historic & current mining operations within the project area. • Samples that were porous were sealed by various methods & accounted for in the bulk density calculation.
Classification	• The models & associated calculations utilised all available data & are depleted for known workings. • NGF follows the JORC classification system with individual block classification being assigned statistical methods & visually taking into account the following factors: ○ Drill spacing & orientation; Classification of surrounding blocks; ○ Confidence of certain parts of the geological model; and ○ Portions of the deposit that are likely to be viably mined. • The classification result reflects the view of the Competent Person.
Audits or reviews	• An internal Norton Gold Fields peer review has been completed as part of the resource classification process.

Criteria	Commentary
Discussion of relative accuracy/ confidence	• The Mineral Resources have been reported in accordance with the guidelines of the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources & Ore Reserves & reflects the relative accuracy of the Mineral Resources estimate. The Competent Person deems the process to be in line with industry standards for resource estimation & therefore within acceptable statistical error limits. • The statement relates to global estimates of tonnes & grade for likely separate open pit & underground mining scenarios. • Historic production data was used to compare with the resource estimate (where appropriate) & assisted in defining geological confidence & resource classification categories.

Section 4 Estimation and Reporting of Ore Reserves

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• A Whittle optimization and pit design was carried out for Mulgarrie Well by NGF personnel in December 2014. The pit design parameter complies with safety parameters based on existing NGF's open pit procedures. The pit design comprises Probable Reserves of 177.6Kt at 1.56g/t at a cutoff grade of 0.6.g/t for oxide, transitional and fresh. • The Mineral Resources are reported inclusive of the Ore Reserves.
Site visits	• Mulgarrie Open pit have been visited by Guy Simpson (GM Technical Services "NGF" & CP for Reserves) within the last 6 months.
Study status	• NGF Technical Services Department created a pit design for the Mulgarrie Well mineral deposit based on Whittle Optimization which is inclusive of a minimum mining width of 30m. The pit design was based on a selling price of $AUD1, 400/Oz with 2.5% Royalty. • The block model used for both Whittle optimization and Pit design is "mu_mik_dec14 - Copy". As the block model is a "MIK" model, mining dilution and ore loss factors were not applied • Operating cost used was based on "NGF's large digger fleet cost model" with average processing cost of $24.24/t.
Cut-off parameters	• A cutoff grade of 0.6g/t for oxide, transitional and fresh rock. • The cutoff grade applied is shown by; $\text{Cut} - \text{off Grade} = \frac{\text{Mining Dilution x Processing Cost}}{\text{Processing Recovery x (Selling Price} - \text{Selling Cost)}}$ • Selling price = AUD$1,400/Oz. • State Royalty = 2.5%. • Metallurgical recovery = 94%. • Processing cost = $24.24/t.

Criteria	Commentary
Mining factors or assumptions	• The method used to convert Mineral resource to Ore Reserves is based upon a pit optimization identifying the economic shell within which a practical mining design can be applied to. • The mining method will be based on conventional open pit mining with diesel trucks and shovels. For Mulgarrie Well, "NGF's large digger fleet model" will be used to optimize the reserve. • As NGF is an owner operator Mulgarrie's operating model will be based on the pit being mined by NGF. • The Ore reserve estimate was created using DCF methodology within "Whittle" open pit optimization software in order to select the most appropriate and economically viable pit shell taking into account minimum mining width for the chosen equipment fleet. • Geotechnical slope design parameters were applied based on geotechnical domains/zones within the mining model. • An overall minimum mining width of 30m was applied. • As the block model is a "MIK" model, mining dilution and ore loss factors were not applied. • No inferred and or unclassified material has been included in the reserves. • Gold Price used = $AUD1, 400/Oz. • Processing cost = $24.24/t. • Infrastructure requirement for open pit mining includes; A workshop for all mobile equipment for maintenance requirements, offices, crib rooms and amenities, explosives storage, water dams and communication. Most of these infrastructures have to be erected on site before mining can commence.
Metallurgical factors or assumptions	• No metallurgical test work was undertaken by NGF on Mulgarrie Well. • Reasonable assumptions for metallurgical extraction are based on processing Mulgarrie Well ore through the Paddington processing plant between 1997 & 1998. • Ore from Mulgarrie Well will be delivered via road trains to NGF's Paddington mill for processing. • Paddington Mill is based on conventional carbon in pulp technology and has achieved an annual throughput of 3.72 million tonnes in 2014. The average feed grade and recovery is 1.67g/t and 88.88% respectively. • A recovery factor of 94% have been applied to Mulgarrie Well's oxide, transitional and fresh rock types as the ore will be blended with Paddington's other ore sources to be able to achieve this recovery factor.
Environmental	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. • All proposed operation and operational plans are within local historical practices and existing operational standards.

Criteria	Commentary
Infrastructure	• The site is serviced by a haul road which is capable of handling 100t road trains. • The site is considered a brownfield site thus before mining can commence infrastructure including electricity, water, offices, core facility, crib rooms, explosives storage, water dams and communications have to be in place.
Costs	• Mulgarrie Well's reserve estimate was based on a gold price of $AUD 1,400/Oz. • Allowance has been made for the 2.5% state government royalty. • Operating cost used was based on "NGF's large digger fleet cost model" with average processing cost of $24.24/t. • No penalties assumed and no deleterious elements in concentrate.
Revenue factors	• Financial analysis in this report is based on a gold price of $AUD 1,400/Oz. • The gold Dore is planned to be transported via recognized security service from gold room of Paddington processing plant to the gold refinery in Perth. • Contract payments and terms are expected to be typical of similar contracts for the refining and sale of Dore produced from other operations within Australia. • Allowance has been made for the 2.5% state government royalty.
Market assessment	• Historical gold price and forward looking estimates have been used for the gold price. Price flexing and sensitivity analysis have been carried out to determine the robustness of the project viability. • The cash flow was modelled in real terms and no price or cost escalations were applied.
Economic	• Inputs to economic analysis include factors described above including ore and metal quantities from mining/processing schedule (including described recovery/processing parameters), cost and price assumptions.
Social	• The majority of workforce will be sourced locally. • NGF will establish all relevant agreement with local stakeholders and government agencies.
Other	• Mulgarrie Well is an existing pit thus an updated Mine Management Plan will need to be submitted with the Western Australian Department of Mines pre-commencement of mining activity. There is no reason to suggest approvals and authorizations will not be granted.
Classification	• The Ore Reserve was classified as Probable in accordance with the JORC Code, corresponding to the resource classifications of Measured and Indicated. No Inferred Mineral Resources were included in the Ore Reserve estimate. • The estimated Ore Reserves and mining method are in the opinion of the Competent Person appropriate for this style of deposit.

Criteria	Commentary
Audits or reviews	• The resource and reserve was calculated by NGF personnel. The cost and mining parameters were reviewed internally against existing operations and consideration was made for current practice and cost structure. • It is not expected that practices assumed in the calculation of reserve will vary before the next annual reserve calculation.
Discussion of relative accuracy/ confidence	• All mining estimates are based on Australian costs, and relevant historical cost data. • The local estimate of Ore reserves available for technical and economic evaluation is 177.6Kt at 1.56g/t at a cutoff grade of 0.6.g/t for oxide, transitional and fresh prior to processing. • There are no unforeseen modifying factors at the time of this statement that will have any material impact on the Ore Reserve estimate.

Appendix 1: Table of Exploration Results – Mulgarrie Well 2014

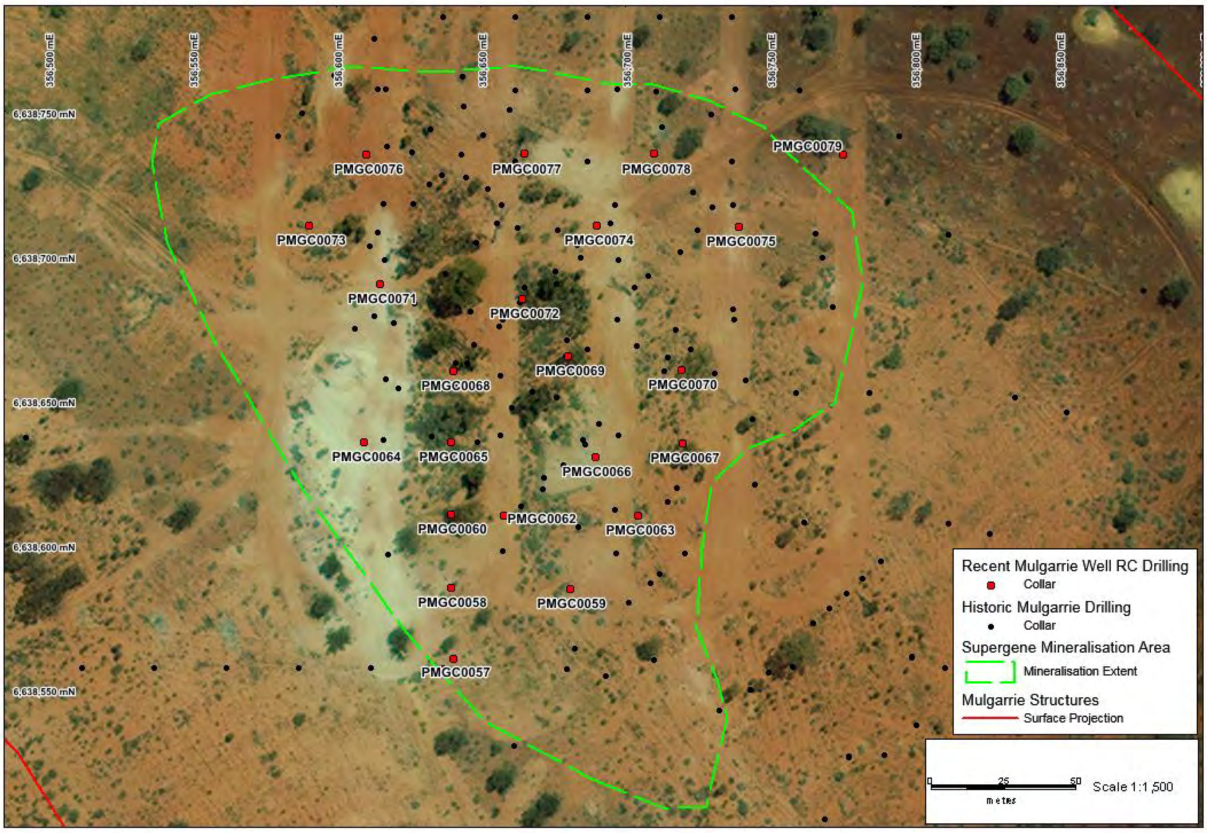
Hole_ID	MGA_East	MGA_North	RL	Dip	Azi	Depth	From (m)	To (m)	DH Width(m)	Grade g/t Au
PMPGC0057	356640.6	6638560.5	363.6	-60	270	96	28	29	1	2.54
							94	96	2	17.6
PMPGC0058	356639.6	6638584.9	363.6	-60	270	78	13	14	1	3.13
PMPGC0059	356681.0	6638584.6	363.4	-60	270	84	____	____	____	NSR
PMPGC0060	356639.6	6638610.4	363.6	-60	270	60	1	2	1	0.95
PMPGC0062	356657.9	6638610.0	363.4	-55	270	60	0	5	5	3.70
							18	25	7	1.42
							37	38	1	3.02
PMPGC0063	356704.5	6638609.9	363.4	-60	270	90	58	59	1	1.09
							71	72	1	0.85
PMPGC0064	356609.5	6638635.4	364.1	-60	270	36	16	17	1	0.80
							29	30	1	1.67
PMPGC0065	356639.7	6638635.2	363.5	-60	270	54	12	21	9	1.89
							28	30	2	1.80
							35	36	1	0.89
PMPGC0066	356689.6	6638630.3	363.5	-60	270	84	27	33	6	3.36
							39	43	4	6.96
							52	53	1	1.00
PMPGC0067	356720.1	6638634.9	363.2	-60	270	114	93	94	1	1.04
PMPGC0068	356640.5	6638660.0	363.7	-60	270	84	21	27	6	1.52
							30	36	6	1.83
							46	47	1	3.04
							56	57	1	1.10
PMPGC0069	356680.2	6638665.2	363.6	-60	270	90	39	48	9	3.54
							55	56	1	1.00
PMPGC0070	356719.5	6638660.3	363.6	-60	270	120	62	63	1	1.62
							69	70	1	4.35
							79	80	1	6.27
							87	88	1	4.29
PMPGC0071	356615.1	6638690.2	363.9	-60	270	102	32	33	1	9.95
PMPGC0072	356664.5	6638685.2	363.7	-60	270	78	45	50	5	0.96
PMPGC0073	356590.7	6638710.3	364.0	-60	270	66	9	10	1	1.16
							41	42	1	0.93
PMPGC0074	356690.2	6638710.4	364.1	-60	270	150	66	80	14	1.34
							84	87	3	0.95
							95	96	1	0.91
PMPGC0075	356739.5	6638710.1	364.2	-60	270	78	____	____	____	NSR
PMPGC0076	356610.3	6638735.1	364.1	-60	270	78	34	35	1	0.84
							43	45	2	1.48
PMPGC0077	356665.1	6638735.2	364.3	-60	270	114	32	33	1	0.87
							79	82	3	0.96
PMPGC0078	356710.0	6638735.2	364.6	-60	270	78	____	____	____	NSR
PMPGC0079	356775.5	6638735.0	364.6	-60	270	102	____	____	____	NSR

Analysis by 30g Fire Assay

Results compiled by using a 0.8 g/t cut-off grade, no top-cut grade

Maximum of 2m internal dilution , minimum interval of 1.0 m

Appendix 2: Collar Locations of Recent RC Drilling



JORC Code, 2012 Edition – Table 1 Report for the Mt Jewell Project Resource Estimates and Reserves (Hughes and Tregurtha Deposits)

Section 1 Sampling Techniques & Data

Criteria	Commentary
Sampling techniques	• Sampling for gold utilised a combination of Reverse Circulation (RC) and Diamond Core (DC) holes. Drilling and sampling for gold at Hughes and Tregurtha has been conducted by various companies since 2009. Sampling techniques is a summary of drilling and sampling methods as reported by Pioneer Resources Limited (Pioneer) and Carrick Gold Limited (Carrick). • Sample representivity is guided by field based observations from geological supervision, logging and other field records referring to sample quality, content and recovery. • Sampling for RC and DC was carried out as specified by Pioneer and Carrick sampling and QAQC procedures a per industry standard for that time. • RC chips and DC provide high quality representative samples for analysis. • RC drilling was logged and generally sampled at 1m intervals using riffle/cone/rotary splitter and dry sampled. In some drill programs 4m composite spear or scoop samples were taken through intervals considered unmineralised. Composite samples which returned an assay of > 0.1g/t Au were resampled on 1m intervals by collecting the corresponding 1m split samples and submitting them for analysis. • DC was logged and sampled at geological intervals of 0.01m to 1.35m and halved using a core saw. • All samples were sent to a commercial laboratory and analysed for Au by fire assay (FA30 and FA50).
Drilling techniques	• Assay data and geological logging data used for resource estimation were obtained from drill samples collected from only RC and DC drill holes. • RC sampling completed using a 5.25” or 5.5” diameter drill bit with a 5” bottom face sampling hammer. RC drilling rigs were equipped with a booster and auxiliary compressor. • DC sampling was a combination of HQ (63.5mm diameter) and/or NQ (50.5mm diameter) core sizes. Drilling was orientated utilizing either a bottom of hole spear, EZI-Mark or ACE system.
Drill sample recovery	• RC drillers are instructed to adopt an RC drilling strategy for the ground conditions advised by geologist expected for each hole to maximize sample recovery, minimize contamination and maintain specified spatial position. • RC drill sample recovery were recorded if very poor sample return or wet samples. Wet samples and water inflow were recorded. RC sample moisture was not routinely recorded. • DC contractors use a core barrel and wire line unit to recover the DC, adjusting drilling methods and rates to minimize core loss

Criteria	Commentary
	(e.g. changing rock type, broken ground conditions etc.). Core was orientated, length measured and compared to core blocks denoting drilling depths by the drilling contractor. Any recovery issues are recorded.
Logging	• RC samples are geologically logged. Specifically, each interval is inspected and the weathering, regolith, rock type, alteration, mineralisation and structure recorded. • The entire length of RC holes are logged on a 1m interval basis (i.e. 100% of the drilling is logged). Where no sample is returned due to voids or lost sample, it is logged and recorded as such. DC is logged over its entire length and any core loss or voids are recorded. • For DC, the oriented core was geologically logged, photographed wet and cut in half. Core loss is recorded in the logging process. • Geological logging is qualitative in nature.
Sub-sampling techniques & sample preparation	• Sub-sampling of both RC and DC drill samples prior to submission to the analytical laboratories is described in Sampling techniques. • Sample preparation of RC chips and DC adhered to best industry standards. It was conducted by commercial laboratories and involved oven drying, coarse crushing then total grinding to a grind size of 85% passing 75µm. • All sub-sampling procedures were carried out by commercial laboratories and are considered satisfactory. • RC field duplicates were collected routinely and for selected intervals. Field duplicate samples were taken at the time of cone/rotary/riffle splitting the bulk sample. These were submitted for the same assay process as the original samples. The laboratories are unaware of such submissions. • No/limited second half sampling was done for DC. • Sample sizes of 2.5 to 4kg are considered appropriate given the grain size of the material sampled (85% passing 75µm). • It is considered that sub-sampling and lab preparations were consistent with other commercial laboratories in Australia and are satisfactory for the intended purpose.
Quality of assay data & laboratory tests	• A 30g or 50g fire assay with AAS finish was used to determine gold content for RC and DC samples. This is a total digest method. • Certified reference material (CRM) consisting of standards and blanks were routinely inserted into the sampling sequence to assess laboratory accuracy and precision and check for possible contamination. The CRMs are unidentifiable to the laboratories. • QAQC data was checked to ensure the results were within acceptable limits. • No geophysical tools were used for reporting gold mineralisation. • The laboratories performed a number of internal processes including standards, blanks, repeats and checks. • Inter-laboratory analysis of selected or “umpire” samples has been carried out for the sampling.

<table>
<tr><th>Criteria</th><th>Commentary</th></tr>
<tr><td>Verification of sampling & assaying</td><td>

No holes were twinned.
Primary data was collated using Logchief and validated by the responsible Geologists to ensure it was correct. The data was exported into Access format.
No adjustments or calibrations were made to any assay data used in this report.
</td></tr>
<tr><td>Location of data points</td><td>

On completion of drilling, drill hole collar positions were surveyed by either contract or company surveyors. Survey was by differential GPS. 8 RC drill holes were not surveyed and have planned collar coordinates with RLs derived from the surface topography.
Down hole surveys consist of regular spaced electronic multishot surveys or north seeking gyro instruments obtained every 5m down hole.
Data was collected on MGA94 Zone 51 co-ordinates.
The topography was derived from LandGate Geospatial Data (September 2011) 2m contours and collar positions of surveyed drill holes.
</td></tr>
<tr><td>Data spacing & distribution</td><td>

Hughes drilling is on 20m spaced east-west lines with generally 20m drill hole spacing, with most holes dipping -60^{0} towards the west. Tregurtha drilling is on 20m spaced east-west lines with generally 20 to 40m drill hole spacing and holes dipping -60 towards the east.
Data spacing and distribution is considered acceptable for establishing geological continuity and grade variability appropriate for classifying a Mineral Resource.
The numbers of drill holes used in the estimations are:
<table>
<tr><th rowspan="2">Deposit</th><th colspan="2">RC</th><th colspan="2">Diamond</th><th colspan="2">Total</th></tr>
<tr><th>No Holes</th><th>Metres</th><th>No Holes</th><th>Metres</th><th>No Holes</th><th>Metres</th></tr>
<tr><td>Hughes</td><td>157</td><td>18,594</td><td>2</td><td>346</td><td>159</td><td>18,940</td></tr>
<tr><td>Tregurtha</td><td>141</td><td>16,233</td><td>4</td><td>583</td><td>145</td><td>16,816</td></tr>
</table>
The resources for Hughes and Tregurtha were estimated using only RC and DC drilling.
Sample compositing intervals are 1m.
</td></tr>
<tr><td>Orientation of data in relation to geological structure</td><td>

The drilling directions were designed to intersect the interpreted mineralisation trend at relatively steep angles.
No drilling orientation and sampling bias has been recognised at this time.
</td></tr>
<tr><td>Sample security</td><td>

Samples are assumed to have been under the security if the respective tenement holders or until delivered to the laboratory where they are assumed to have been under restricted access.
</td></tr>
</table>

Criteria	Commentary
Audits or reviews	• Internal and external reviews were completed on sampling techniques and data as part of the various operating companies' continuous improvement practices.

Section 2 Reporting of Exploration Results

Criteria	Commentary
Mineral tenement & land tenure status	• The Hughes and Tregurtha deposits are located within Exploration License E24/146. The tenements are 100% held by Kalnorth Gold Mines Limited who completed sale of the project to Norton Gold Fields Limited (NGF) in November 2014. The lease is currently Native Title cleared. The State Government royalty of 2.5% applies on gold produced. Mt Jewell has a royalty based on ore tonnes processed payable to a 3rd party. • An application for conversion to a mining lease of the part of E24/146 containing Hughes and Tregurtha is pending.
Exploration done by other parties	• There is no evidence of historic gold mining within the area. Various companies (Kennecott Australasia Pty Ltd, CSR Minerals Pty Ltd, Heron Resources Ltd, MPI Mines Pty Ltd, North Limited, Delta Gold, Pioneer Nickel Limited, Pioneer Resources Limited, Carrick Gold Limited and Kalnorth Gold Mines Limited) have held or joint ventured the area covered by the Hughes and Tregurtha deposits since the late 1960's exploring for both nickel and gold. First pass RC drilling for gold was undertaken in September 2009 by Pioneer. All subsequent RC and DC drilling has been done by Pioneer and Carrick.
Geology	Regional Geology • The Hughes and Tregurtha gold deposits are located in the south west corner of the NNW trending Rainbow Dam Granodiorite (RDG). The RDG is a plutonic body with an area of approximately 70sq km. It sits as a NNW orientated tear drop shaped body bound to the east by the Ringlock Dam greenstone belt and to the west by the west dipping Scotia Greenstone Belt. • Within the granodiorite zonation may be present as represented by zones of higher magnetic intensity that appear to form in roughly concentric bodies with the pluton. The higher magnetic zones may represent more magnetite rich phases of the granodiorite. • The existing gold deposits both are located within a strongly demagnetized zone, partially related to the closeness of the mineralisation to the contact with the Scotia Ultramafic Belt but it may also represent a more localized regional; feature related to the gold mineralisation as is the case at the Golden Cities Deposits in the Scotia Granodiorite. Local Geology • Hughes and Tregurtha are both wholly hosted within the Rainbow Dam Granodiorite. The area has a preserved weathering profile with weak weathering down to 60-70m vertical depth. A 30m thick depleted or leached zone is developed at the top of the profile that is devoid of gold. The mineralisation is shear associated with some mineralisation hosted within tensional settings.

Criteria	Commentary
	• The unaltered host rock is a medium grained biotite granodiorite. The highest grade gold mineralisation is usually located in the core of the intensely biotite-silica-pyrite or sericite-silica-pyrite altered shear zones. These zones grade out into sericite-chlorite altered zones that grade into distal chlorite-epidote alteration. Haematite dusting is locally present though does not display a consistent spatial relationship with the shears and may represent an earlier alteration event. The deposits are analogous to the Golden Cities deposits with gold most likely associated with thin quartz-pyrite veining. • In addition to granodiorite, altered and sheared semi-continuous mafic units are present. These mafic rocks may represent later dykes but may also be contemporaneous intrusive phases or large rafts and xenoliths. Feldspar porphyries and aplite are also present in the area. Alteration and Gold Mineralisation • Three phases of alteration have been recognized: 1. Hematite Alteration: Regional alteration seen in reconnaissance RAB drilling, and within 100-500m surrounding mineralised structures. Characterized by deep red coloration of feldspar and deep green chloritisation of amphibole. Varies from light dusting to total replacement of rock fabric. 2. Potassic Alteration: Generally restricted to dusting on feldspars and bitotite replacement of ferromagnesian minerals. Associated with shearing. 3. Sericite –Chlorite: Appears to be associated with gold mineralisation, intensity varies from greenish coloration of feldspars and replacement of biotite to a deep bottle green coloration of the granodiorite. • The alteration types are generally associated with foliation within the granodiorite and appear to form an outer halo to the mineralisation. The following mineralisation styles are present: 1. Pyrite –Quartz: Both minerals are intimately associated with gold mineralisation. On a volume basis pyrite is generally less than 1% and often recorded as trace. The pyrite is generally fine to very finer grained, disseminated euhedra or films upon foliation, associated with shearing. Quartz veining is generally in the trace to 5%, clear to white in colour and distinct from altered blue quartz present in the granite. 2. Biotite –Silica: Common throughout the mineralised structures, manifesting as black, foliated biotitic fine grained material generally associated with zones of stronger shearing. Commonly associated with pyrite and quartz veining. 3. Sericite –Silica: Associated with zones of intense shearing, probably representing post-mineralisation thrusting. Structure • The Hughes and Tregurtha deposits are associated with the 320-330 trending Lignum Dam Fault Zone (LDFZ), a north-northwest trending zone of shearing, mylonitisation and alteration which is most apparent as a zone of demagnetisation within regional aeromagnetic imagery.

Criteria	Commentary
	• The LDFZ manifests at Tregurtha as a series of anastomosing shears and mylonite zones oriented 320-330 degrees with a steep dip to the west. The shear zone at Tregurtha is present as a 15-30m thick zone of intense foliation with associated chlorite-sericite alteration, and peripheral zones of footwall hematite alteration. • The Hughes Deposit sits within a splay structure on a conjugate orientation to the main LDFZ and dips approximately 45 degrees towards 110 degrees. This structure is present as a 30-45m thick zone of intensely biotite-chlorite altered granodiorite with a strong submylonitic fabric, strongly associated with gold mineralisation. • A similar 45/110 orientation is suggested at Tregurtha as a conjugate structural set which may control shoot orientation as a plunge of -80/160 approximately. A biotite-altered structure similar to Hughes, but poorly mineralised, is present at the north of Tregurtha. Weathering • The Tregurtha and Hughes Deposits areas sit on the side of a gently sloping rise associated with the western contact of the granodiorite with the Scotia Greenstone Belt. The Tregurtha Deposit sits near the top of the rise and is covered by a 2-5 metre blanket of lateritised poorly cemented pisolite gravels, calcrete, rock fragments and red soil. This cover is a remnant of a broader laterite horizon related to Cainozoic weathering. • The Hughes Deposit is located to the south east toward the base of the slope with only a thin layer of soil over silcreted bedrock. The lateritised, calcrete horizon is denuded in this area and is absent over the vast majority of the Rainbow Dam Granodiorite. In the vicinity of the Hughes deposit outcrops of silcretised foliated granite porphyry occur.
Drill hole Information	• See Sections 1 and 3.
Other substantive exploration data	• No unreported exploration data has been collected relevant to these deposits considered material to this announcement.
Further work	• Further work will include re-estimation of the Hughes and Tregurtha mineral resources and mining studies appropriate to NGF's current open-cut mining methods.

Section 3 Estimation & Reporting of Mineral Resources

Criteria	Commentary
Database integrity	• Data is currently in Access format and in the process of being integrated into an SQL backend database with Geologists interfacing via a DataShed front end. User access to the database is controlled via user permissions which are configured both at the group level by Systems Administration and the user level by the Database Administrator. Field and project Geologists are responsible for data entry. Existing protocols maximize data functionality and quality whilst minimizing the likelihood of error introduction at primary data collection points and subsequent database upload, storage and retrieval points. Data templates with lookup tables and fixed formatting are used for collecting primary data on field laptops. The software has validation routines and data is subsequently imported into a secure central database. • The SQL server database is configured for validation through constraints, library tables, triggers and stored procedures. Data that fails these rules on import is rejected or quarantined until it is corrected. • Database is centrally managed by a Database Manager who is responsible for all aspects of data entry, validation, development, quality control and specialist queries. There is a standard suite of vigorous validation checks for all data.
Site visits	• The Competent Person is a full time employee of NGF and undertakes regular site visits ensuring industry standards of the Mineral Resource estimation process from sampling through to final block model.
Geological interpretation	• The high confidence of the geological interpretation is based on geological knowledge acquired from detailed geological DC and RC logging and assay data. • The dataset (geological mapping, RC and DC logging, assays etc.) is considered acceptable for determining a geological model. Key interpretation assumptions made for this estimation are the existence of depletion zones in the oxide and supergene zones at the oxide and transitional interfaces as distinct from the primary mineralisation. • The geological interpretation is considered robust overall, with no known alternative interpretations. • The geological interpretation is specifically based on identifying particular geological structures, weathering profiles, associated alteration and gold content. • Whilst the geological features are deemed to be continuous, the gold distribution within them can be highly variable.

Criteria | **Commentary**

Dimensions

- Mineral Resource dimensions for the deposits are:

Deposit	Mineralisation Length	Primary Mineralisation Dip	Primary Horizontal Mineralisation Width	Vertical Depth Extents
Hughes	650m striking 60°	-25° to -55° towards 135°	Multiple lodes, 3m up to 15m	From 20m to 200m below surface
Tregurtha	600m striking 310°	-70° towards 215°	Multiple lodes, 2m up to 25m	From 5m to 200m below surface

- Resource model extents are:

Deposit	Grid		Easting	Northing	Elevation
Hughes	MGA94	Minimum	352200	6650340	150
		Maximum	353100	6650770	450
Tregurtha	MGA94	Minimum	351560	6651000	150
		Maximum	352600	6651620	450

Estimation & modelling techniques

- Estimation techniques, block sizes and top cuts applied are:

Deposit	Estimation Method	Parent Block Size (Ym x Xm x Zm)	Minimum Block Size (Ym x Xm x Zm)	Top Cut (g/t Au)
Hughes	Ordinary Kriging	10 x 10 x 5	1.25 x 1.25 x1.25	5.5 and 10
Tregurtha	Ordinary Kriging	10 x 10 x 5	1.25 x 1.25 x1.25	5, 15 and 20

- No assumptions were made regarding recovery of by-products during the Mineral Resource estimate.
- The estimation of deleterious elements was not considered material to this style of mineralisation.
- No selective mining unit (SMU) dimensions were assumed.
- Interpreted wireframes for the estimation domains, and regolith and topographical files were used to define the resource estimate. Blocks within the models were coded based on these surfaces.

<table>
<tr><th>Criteria</th><th>Commentary</th></tr>
<tr><td></td><td>The Mineral Resource estimates were validated by:
<table>
<tr><th>Deposit</th><th>Validation Methods</th></tr>
<tr><td>Hughes</td><td rowspan="2">Visual against raw drill data and statistical analysis by global mean comparison and trend plot comparison.</td></tr>
<tr><td>Tregurtha</td></tr>
</table></td></tr>
<tr><td>Moisture</td><td>Tonnages are estimated on a dry basis.</td></tr>
<tr><td>Cut-off parameters</td><td>Reporting cut-off grades are:
<table>
<tr><th>Deposit</th><th>Reporting Cut-off Grade (g/t Au)</th></tr>
<tr><td>Hughes</td><td>0.7</td></tr>
<tr><td>Tregurtha</td><td>0.7</td></tr>
</table></td></tr>
<tr><td>Mining factors or assumptions</td><td>The resource is likely to be mined by open cut mining. Open cut mining scenario is likely to utilise an excavator to mine 2.5m or 5m flitches. Mining methods are based on current open pit for NGF.</td></tr>
<tr><td>Metallurgical factors or assumptions</td><td>No assumption or factors have been applied to the resource estimate regarding the metallurgical amenability.
Reasonable assumptions for metallurgical extraction are based on previous processing of ore from nearby Golden Cities deposits through the Paddington Mill (owned by NGF). The mill utilises a CIP extraction process.
Target gold recoveries would range from 93% to 96% recovery.</td></tr>
<tr><td>Environmental factors or assumptions</td><td>No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. This expectation is based on previous mining and milling history of nearby Golden Cities deposits.</td></tr>
<tr><td>Bulk density</td><td>Bulk densities applied to the resource estimates were based on a total of 324 density measurements consisting of samples from fresh rock and saprock. The density samples measurements did not cover transitional, oxide or transported material but it was assigned a density value based on typical Eastern Goldfields narrow vein gold mines.</td></tr>
<tr><td>Classification</td><td>The calculations utilised all available data.
JORC resource classification was based on search parameters including search distance and number of informing samples, and on data quality, including the existence, availability and quality of QAQC.
The classification result reflects the view of the Competent Person.</td></tr>
<tr><td>Audits or reviews</td><td>The Hughes and Tregurtha Mineral Resources have been externally and internally reviewed.</td></tr>
</table>

Criteria	Commentary
Discussion of relative accuracy/ confidence	• The Mineral Resources has been reported in accordance with the guidelines of the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves and reflects the relative accuracy of the Mineral Resources estimate. The Competent Person deems the process to be in line with industry standards for resource estimation and therefore within acceptable statistical error limits. • The statements relates to global estimates of tonnes and grade for likely open pit mining and processing scenarios.

Section 4 Estimation and Reporting of Hughes and Tregurtha Ore Reserves

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• A Whittle optimizations and pit design was carried out for Hughes and Tregurtha by NGF personnel in August 2013. The pit design parameter complies with safety parameters based on existing NGF's open pit procedures. The pit design for Hughes mineral deposit comprises Probable Reserves of 674.7Kt at 1.19g/t at a cutoff grade of 0.74g/t for oxide, transitional and fresh. The pit design for Tregurtha mineral deposit comprises Probable Reserves of 504.2Kt at 1.68g/t at a cutoff grade of 0.74g/t for oxide, transitional and fresh. • The Mineral Resources are reported inclusive of the Ore Reserves.
Site visits	• NGF representatives have visited the site within the last 6 months. • Hughes and Tregurtha is a Greenfield site and is situated north and between NGF's Mulgarrie and EXG's Zoroastrian
Study status	• NGF Technical Services Department created a pit design for Hughes and Tregurtha mineral deposits. The optimization study was based on Whittle optimization using a selling price of $AUD1, 400/Oz with 2.5% Royalty. • The block model used, for Hughes mineral deposit's Whittle optimization and Pit design is "hughes_may2013_v3_5m_reblock.mdl". • The block model used, for the Tregurtha mineral deposit's Whittle optimization and Pit design is "tregurtha_model_01092012_5m_reblock.mdl". • Modifying factors such as mining loss, mining dilution and recoveries have been applied. • Operating cost used was based on "NGF's small digger fleet cost model" with total processing cost of $27.80/t.

Criteria	Commentary
Cut-off parameters	• A cutoff grade of 0.74g/t for oxide, transitional and fresh rock. • The cutoff grade applied is shown by; $\text{Cut} - \text{off Grade} = \frac{\text{Mining Dilution x Processing Cost}}{\text{Processing Recovery x (Selling Price} - \text{Selling Cost)}}$ • Selling price = AUD$1,400/Oz. • State Royalty = 2.5%. • Metallurgical recovery = 94%. • Processing cost = $27.80/t.
Mining factors or assumptions	• The method used to convert Mineral Resource to Ore Reserves is based upon a pit optimization identifying the economic shell within which a practical mining design can be applied to. • The mining method will be based on conventional open pit mining with diesel trucks and excavator. For Hughes and Tregurtha, “NGF’s small digger fleet model” will be used to optimize the reserve. • As NGF is an owner operator for Hughes and Tregurtha then both pits will be mine by NGF. • The Ore reserve estimate was created using DCF methodology within “Whittle” open pit optimization software in order to select the most appropriate and economically viable pit shell taking into account minimum mining width for the chosen equipment fleet. • Geotechnical slope design parameters were applied based on geotechnical domains/zones within the mining model. • An ore loss allowance of 5% and a mining dilution of 10% are anticipated with this type of operation based upon historical data in similar scale and type of operation. • An overall minimum mining width of 25m was applied. • No inferred and or unclassified material has been included in the Ore Reserves. • Gold Price used = $AUD1, 400/Oz. • Infrastructure requirement for open pit mining includes; A workshop for all mobile equipment for maintenance requirements, offices, crib rooms and amenities, explosives storage, water dams and communication. Most of these infrastructures have to be erected on site before mining can commence.

Criteria	Commentary
Metallurgical factors or assumptions	• No metallurgical test work was undertaken by NGF on Hughes and Tregurtha. • Ore from Hughes and Tregurtha will be delivered via road trains to NGF's Paddington mill for processing. • Paddington Mill is based on conventional carbon in pulp technology and has achieved an annual throughput of 3.72 million tonnes in 2014 with average feed grade of 1.67g/t with average recovery of 88.88%. • A recovery factor of 94% have been applied to both mineral deposits' oxide, transitional and fresh rock types as the ore will be blended with Paddington's other ore sources to be able to achieve this recovery factor. • Processing cost = $27.80/t.
Environmental	• No significant environmental factors are expected to be encountered regarding the disposal of waste or tailing material. • All proposed operation and operational plans are within local historical practices and existing operational standards.
Infrastructure	• The site is considered a greenfield site thus before mining can commence infrastructure including electricity, water, offices, core facility, crib rooms, explosives storage, water dams and communications have to be in place.
Costs	• Hughes and Tregurtha's reserve estimate were based on a gold price of $AUD 1,400/Oz. • Allowance has been made for the 2.5% state government royalty. • Operating cost used was based on "NGF's small digger fleet cost model" with a total processing cost of $27.80/t. • No penalties assumed and no deleterious elements in concentrate.
Revenue factors	• Financial analysis in this report is based on a gold price of $AUD 1,400/Oz. • The gold Dore is planned to be transported via recognized security service from gold room of Paddington processing plant to the gold refinery in Perth. • Contract payments and terms are expected to be typical of similar contracts for the refining and sale of Dore produced from other operations within Australia. • Allowance has been made for the 2.5% state government royalty.
Market assessment	• Historical gold price and forward looking estimates have been used for the gold price. Price flexing and sensitivity analysis have been carried out to determine the robustness of the project viability. • The cash flow was modelled in real terms and no price or cost escalations were applied.
Economic	• Inputs to economic analysis include factors described above including ore and metal quantities from mining/processing schedule (including described recovery/processing parameters), cost and price assumptions.

Criteria	Commentary
Social	• The majority of workforce will be sourced locally. • NGF will establish all relevant agreement with local stakeholders and government agencies.
Other	• Mt Jewell is a Greenfield site thus a new Mine Management Plan will need to be submitted with the Western Australian Department of Mines pre-commencement of mining activity. There is no reason to suggest approvals and authorizations will not be granted.
Classification	• The Ore Reserve was classified as Probable in accordance with the JORC Code, corresponding to the resource classification of Indicated. No Inferred Mineral Resources were included in the Ore Reserve estimate. • The estimated Ore Reserves and mining method are in the opinion of the Competent Person appropriate for this style of deposit.
Audits or reviews	• The resource and reserve was calculated by NGF personnel. The cost and mining parameters were reviewed internally against existing operations and consideration was made for current practice and cost structure. • It is not expected that practices assumed in the calculation of reserve will vary before the next annual reserve calculation.
Discussion of relative accuracy/ confidence	• All mining estimates are based on Australian costs, and relevant historical cost data. • The local estimate of Ore reserves available, for the Hughes mineral deposit, for technical and economic evaluation is 674.7Kt at 1.19g/t for 25.8Koz at a cutoff grade of 0.74g/t prior to processing. • The local estimate of Ore reserves available, for the Tregurtha mineral deposit, for technical and economic evaluation is 504.2Kt at 1.68g/t for 27.3Koz at a cutoff grade of 0.74g/t prior to processing. • There are no unforeseen modifying factors at the time of this statement that will have any material impact on the Ore Reserve estimate.

January 2015
Mineral Resource & Ore Reserve Update

Corporate Directory

Board & Senior Management

Jinghe Chen
Non-Executive Chairman

Dianmin Chen
Managing Director
& Chief Executive Officer

Anne Bi
Non-executive Director

Xuelin Cai
Non-executive Director

Noel White
Non-executive Director

Mark Braghieri
General Manager Bullabulling Project

Terry Moylan
General Manager Projects & Business Development

Steven Phan
Chief Financial Officer

Peter Ruzicka
General Manager Exploration

Guy Simpson
General Manager Technical Services

Cullum Winn
General Manager Paddington Operations

Company Secretary
Richard Jones
General Counsel / Company Secretary

Media Relations
Warrick Hazeldine / Annette Ellis
Purple Communications
Tel: +61 (8) 6314 6300

ASX Listed Share Capital
931,850,665 million ordinary shares

Presentation and Rounding
Unless stated otherwise, all dollars shown are Australian dollars.

YTD
YTD means 2014 calendar year to date

Competent Persons Statement

The information in this report that relates to Mineral Resources is based on information compiled by Peter Ruzicka and Brad Daddow for Paddington, and Richard Sulway for Bullabulling. The information in this report that relates to Mineral Reserves is compiled by Guy Simpson and Elizabeth Jones. Exploration drilling results have been compiled by Peter Ruzicka.

Peter Ruzicka, Guy Simpson and Elizabeth Jones are all members of the Australasian Institute of Mining and Metallurgy and full-time employees of Norton Gold Fields Limited. Brad Daddow is a member of the Australian Institute of Geoscientists and a full-time employee of BM Geological Services PL, a consulting group to Norton Gold Fields Limited. Richard Sulway is a member of the Australasian Institute of Mining and Metallurgy, and a full-time employee of Snowden, a consulting group to Norton Gold Fields Limited.

Guy Simpson, Elizabeth Jones, Peter Ruzicka, Brad Daddow and Richard Sulway all have sufficient experience relevant to the styles of mineralisation and types of deposits which are covered in this report, and to the activity which they are undertaking to qualify as Competent Persons as defined in the 2012 edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Guy Simpson, Elizabeth Jones, Peter Ruzicka, Brad Daddow and Richard Sulway all consent to the inclusion in this report of matters based on their information in the form and context in which it appears.

Mount Morgan Project

The information in this report that relates to Mineral Resources of the Mount Morgan Mine project was prepared in accordance with the 2004 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves' ("JORC Code") and is based on, and fairly represents, information and supporting documents prepared by Troy Lowien, Resource Geologist, of consultants Coffey Mining Pty Ltd, who is a Member of The Australian Institute of Mining and Metallurgy ("AUSIMM") and has a minimum of five years of experience in the estimation, assessment and evaluation of Mineral Resources of this style and is the Competent Person as defined in the JORC Code. Troy Lowien conducted the geological modelling, statistical analysis, variography, grade estimation and report preparation. This report accurately summarises and fairly reports his estimations and he has approved and consented to the resource report in the form and context in which it appears. This information was prepared and first disclosed under the JORC Code 2004. It has not been updated since to comply with the JORC Code 2012 on the basis that the information has not materially changed since it was last reported.

Norton Ore Reserve and Mineral Resource statement (gold) as at 31 December 2014

Reserve	Mt	g/t	Moz
Proven	1.67	1.53	0.08
Probable	16.86	1.89	1.02
Total	18.53	1.86	1.11

Resource	Mt	g/t	Moz
Measured	2.32	1.80	0.14
Indicated	141.33	1.21	5.51
Inferred	103.22	1.42	4.71
Total	246.87	1.30	10.35

Mount Morgan Mineral Resource statement (gold) as at 31 December 2012

	Mt	g/t	Moz
Indicated	2.487	1.59	0.127
Inferred	5.861	1.07	0.199
Total	8.348	1.23	0.326

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Share Registry
Link Market Services
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Brisbane QLD 4000

Tel 1300 554 474 (within Australia)
Tel +61 1300 554 474 (overseas)

Please direct shareholding enquiries to the share registry