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GATEWAY MINING LTD

9 July 2015

Results from Recent Drilling

Highlights:

- **RC drilling intersects Reduced Intrusion Related gold, "Contact Zone" mineralisation on the inside margin of the Montague Granodiorite intrusion.**
- **Gateway to commence assessment of a 5km section of the Montague Granodiorite margin for Contact Zone high grade gold mineralisation**
- **Disseminated sulphide with elevated VMS multielements intersected in geophysical targets within The Cup stratigraphy**
- **Future exploration program planning underway**

Gateway Mining Limited ('Gateway' or 'the Company') recently completed approximately 2,000m of Reverse Circulation (RC) drilling on its Gidgee tenements in Western Australia targeting primarily geophysical Volcanogenic Massive Sulphide (VMS) prospects. In addition, several holes were drilled elsewhere on the project to meet minimum expenditure requirements.

In an unexpected, yet very pleasing, result for the Company, two of these holes intersected significant gold mineralisation on the Montague gold tenements. GRC303 and GRC304, intersected what is believed to be a Reduced Intrusive Related (RIR) gold mineralised system.

GRC303: 8m @ 0.63g/t Au from 49m
GRC304: 2m @ 2.31g/t Au from 41m

Intrusive related gold systems are a relatively newly defined class of gold mineralisation. The gold was intersected along the 'contact zone' between the basalts to the west and the Montague granodiorite to the east. These holes are approximately 1km apart yet are interpreted to be part of the same system, highlighting the significant potential for extensive gold mineralisation.

These intersections, while not the prime target of the recent program, open up an exciting exploration frontier as it has defined approximately 4km of untested strike length to both the north and south of these holes.

The geophysical targets within the VMS stratigraphy continued to intersect strong VMS geochemical anomalism with disseminated sulphides throughout. This provides further confirmation that the stratigraphy is host to VMS mineralised sulphides, however further work is required to delineate the more developed parts of the system, which the Company believes will host stronger mineralisation.

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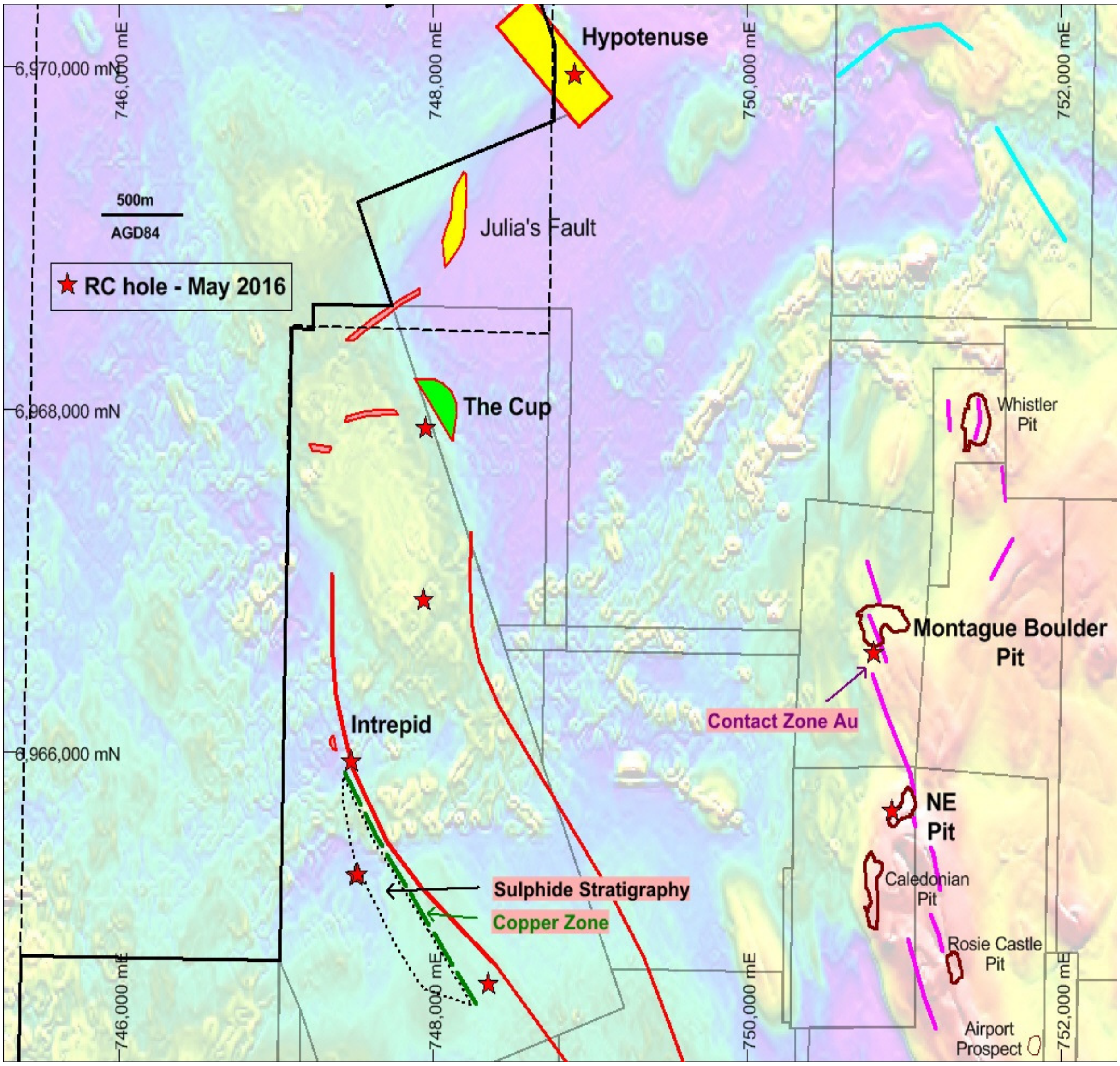

Overview of May/June programme 2015 – (background: Total Magnetic Intensity)

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Montague Granodiorite - Contact Zone

Two holes were drilled on the Montague gold tenements during the last program predominantly for expenditure purposes. However in an unexpected, yet very pleasing, surprise for the Company, both holes intersected significant gold mineralisation.

The Company has spent a lot of time very recently (and is continuing to spend time) analysing the apparent Reduced Intrusive Related (RIR) gold system which was intersected by holes GRC303 and 304. The current interpretation of the gold stratigraphy identified the possibility of this RIR style of gold to be running along the western edge of the granodiorite for up to 4km of largely untested strike.

Two holes which intersected significant gold mineralisation were:

GRC303: 8m @ 0.63g/t Au from 49m
GRC304: 2m @ 2.31g/t Au from 41m

The holes are approximately 1km apart however are interpreted to be part of the same continuous system, meaning there is significant scope for substantial gold mineralisation over an extensive strike. This result was not anticipated, but is a very pleasing surprise for the Company.

The vast majority of the 'contact zone' between the basalt and granodiorite has not been tested, despite historic gold mining in the region. Locating the contact was most likely quite problematic for previous explorers because gravity surveying would not have been available when most exploration was occurring on these tenements. This would have highlighted the gravity contrast between the granodiorite intrusion and basalt wall rock i.e. the target contact zone. Additionally, past efforts were hampered by piecemeal tenement holdings and almost no outcrop of gold.

Almost all exploration drilling for gold was conducted further to the west of this gold rich 'contact zone' with historic exploration focused on locating small gold deposits within basalts.

However, this re-interpretation of the historic gold results means there are likely to be two separate gold systems within the Montague tenements: (1) typical Yilgarn style orogenic gold; and (2) the recently identified Reduced Intrusion Related (RIR) Mesozonal Intrusion-Hosted mineralisation (Robert, F., et al. 2007). The ongoing geological interpretation would also support this hypothesis.

Historic exploration would likely not have been able to delineate between the two styles due to high limits of detection for subtle geochemical composition differences. However, determining geological differences between the two has significant implications for future exploration as drilling will be vectored to specifically target the contact zone between the basalt and granodiorite intrusion.

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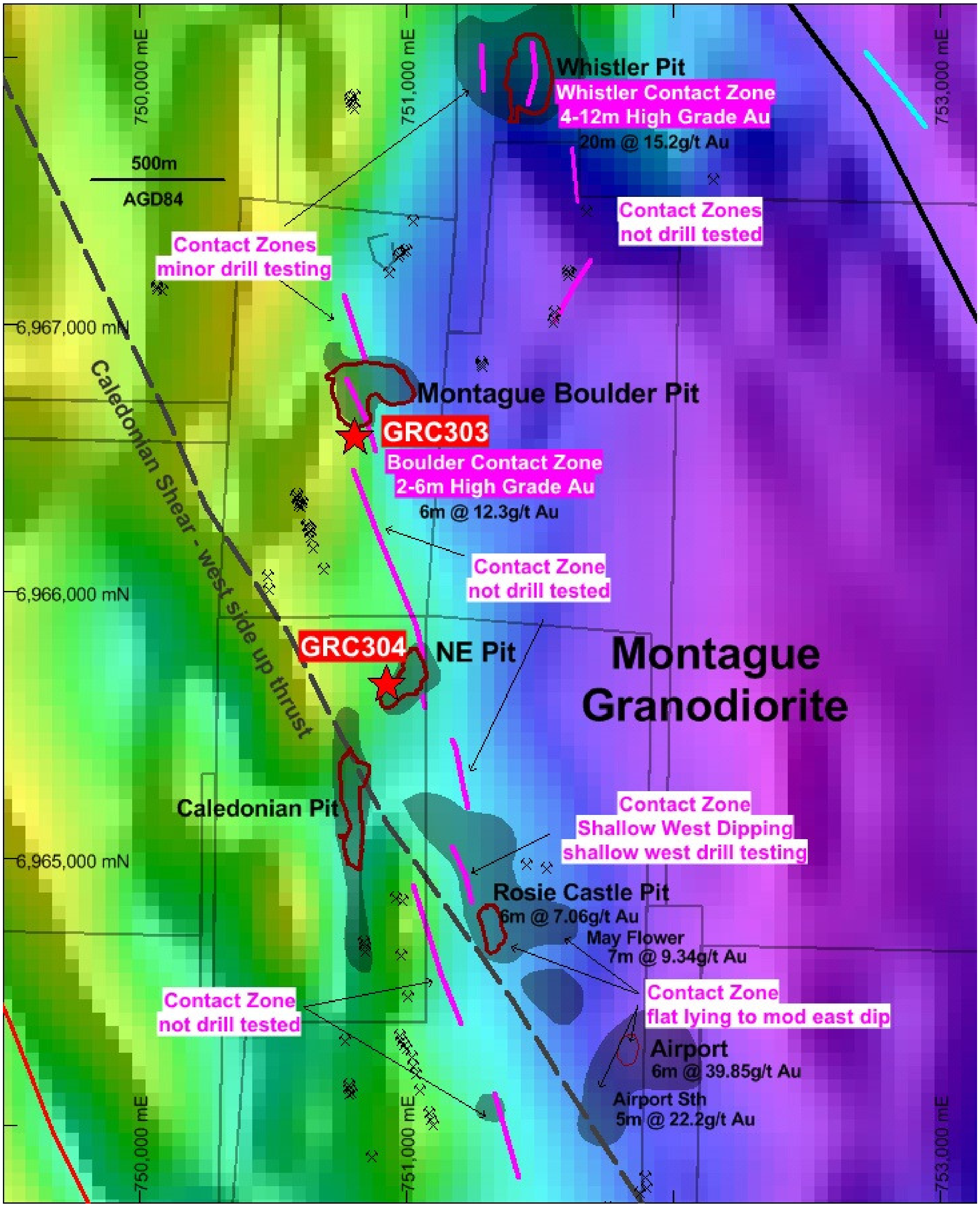

Montague Granodiorite Contact Zone, shaded areas are moderate to intensely drilled, unshaded areas have light to no drill hole coverage – (background: Gravity Survey)

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Key characteristics of the intersection in GRC303 supportive of an RIR model include:

- Mineralisation has close spatial and temporal association with a felsic to intermediate intrusion that is predominantly equigranular with porphyritic textures, and in the instance of the Contact Zone, **mineralisation sits within the intrusion fine grained chilled margin of such an intrusion**. Also, the Montague Granodiorite has a series of gold mineralisation occurrences that flank around the intrusion margin.

- Compared to porphyry style intrusion mineralisation, **sulphide abundance is relatively low** (<5% volume) **base metal concentrations are also much lower** (GRC303 - Cu to 304ppm, Pb to 38ppm and Zn to 285ppm).

- Gold mineralisation has associated quartz veining with **miarolitic cavities and aggregates of tourmaline**. Miarolitic cavities are indicative of a relatively shallow depth of formation and tourmaline indicative of a late phase magmatic affinity.

- Gold occurs in association with sheeted veining internal within the intrusion, such as occurs within the eastern section of the Montague Boulder Pit.

- Geochemical indicators are for **high Bi (up to 18.55ppm) and W (up to 13.3ppm), relatively low As** (up to 59ppm) and gold occurs in greater abundance than silver.

RIR mineralisation forms early in the structural deformation history which results in faulted offsetting and folding to the original continuity of mineralisation. Deformation is not expected to have effected mineralised tenor or diminished overall extent, only to have created discontinuity of the contact geology.

The Company has spent recent days sifting through historic drill holes to try to determine which historic results could be classified as part of the RIR system. It is **pleasing to note that many of the historic high grade intercepts (many of which are still open) most likely sit within the RIR system**, such as:

Boulder:	6m @ 12.3g/t Au
Whistler:	20m @ 15.2g/t Au
Rosie Castle:	3m @ 8.58g/t Au
Airport:	6m @ 39.85g/t

The grade of gold is expected to vary along the system, however the above results give an idea of the possibility of very high grades being intersected near surface.

GRC304 targeted intrusion 'contact zone' style mineralisation down dip from the strong shallow west dipping gold zone mined in NE Pit.

2m @ 2.31g/t Au from 41m was intersected in basaltic andesite. Granodiorite was not intersected suggesting that there is either a faulted offset occurring between the pit and GRC304, or that the NE Pit mineralisation is a basalt hosted occurrence of the "Late Fault Vein" subclass of RIR style mineralisation, such as is also interpreted at Caledonian Pit.

Two zones of anomalous bismuth were intersected in GRC304 and include a broad zone of Bi up to 4.58ppm located directly down dip and in alignment with the shallow west dipping gold zone in NE Pit. This apparent association suggests that the NE Pit gold zone is a Late Fault Vein occurrence hosted within basalt consisting of quartz veining (quartz tourmaline miarolitic cavity veining with Bi, Te enrichments) in association with fault structures active during late stages of crystallisation of the granodiorite intrusion. Better intersections in historic definition drilling inclusive within the mined out NE Pit include:

4m @ 36.84g/t Au from 21m
7m @ 13.99g/t Au from 18m
9m @ 12.41g/t Au from 23m
8m @ 17.84g/t Au from 22m

Two bismuth intersections in GRC304 are interpreted as west dipping fault zones, one shallow dipping and the other moderate with the majority of mineralisation in NE Pit lying along the shallow west dipping fault. The lineation defined by the intersection between the two faults, has shallow north dipping plunge and is interpreted as a strong control mechanism for the location of a higher grade "shoot" mined in the NE Pit. Repeat fault structures may result in further shoots at depth that are perhaps elongate along fault intersection lineations.

The basalt wall rock on the margin of the Montague Granodiorite has multiple late fault veining occurrences, often with shallow old workings dotted along that are prospective for high grade gold shoots. Limited shallow drill testing has been conducted.

While gold exploration was not the focus of the recent program, intersecting RIR style gold opens up a number of exciting development and exploration frontiers for Gateway to pursue in coming programs. Exploration and drilling will be designed with two goals in mind:

1. Work toward presentation of a JORC compliant resource based on existing drilling with further supplementary drilling for confirmation, definition and extension of resources. Suitable areas include the Rosie Castle and Airport Contact Zone.
2. Exploration targeting for new discoveries of high grade gold Intrusion Contact mineralisation in the large areas left untested or poorly tested along the granodiorite intrusion gravity contrast.

Given the apparent continuity of the gold system, the Company has increased confidence of locating further significant gold mineralisation along the contact zone in coming programs.

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The Cup/Intrepid VMS System

Recent drilling conducted south from The Cup prospect at Conductors 1, 2, 4, 6 and 7 has significantly advanced understanding of the stratigraphic succession in this section of the project.

GRC308 drilled at Conductor 1 intersected strongly carbonate altered footwall volcanics before intersecting a lower unit of carbonaceous shale with elevated As-Au. The dip of the As-Au enrichments in the area defined by shallow geochemical drilling and also within GRC308 is steeply WSW dipping and provides the best indication yet for the attitude of local stratigraphy.

GRC307, drilled at Conductor 2 intersected a broad expanse of sulphide rich shale to the end of hole. This sulphide intersection would appear to explain the extremely high level of conductance extending 1.4km along NNW-SSE strike as shown in the above plan. The spectacular width of strong multielement concentrations intersected, indicate this sulphidic shale is analogous to the shale/dacite stratigraphic package at The Cup ("Main Shale") where the strong copper zone is located at the base and is overlying a carbonate altered basaltic footwall sequence. If stratigraphy is dipping steeply WSW, which if correct, leaves at least 150m from the bottom of GRC307 to the east across strike to traverse before reaching the possible copper zone horizon. The high level of multielement rich sulphides encountered in the upper section of the shale at Conductor 2 is an encouraging sign for strongly elevated metal enrichments within the copper/silver horizon.

GRC306 was drilled at Conductor 4 and intersected a complete structural repetition of the Cup stratigraphic package intersecting 5m@0.2% Cu through the copper zone in an area with much lower conductance, multielement and sulphide concentrations than at Conductor 2.

<u>Conductor 1</u>

GRC308 (273m) was drilled east and abandoned at 273m, the RC rig had reached its limit of capacity resulting in slow ground penetration and wet sample return.

Basaltic andesite volcanics were intersected in the upper levels of the hole above a unit of sulphide rich carbonaceous shale from 249m with strong VMS multielement geochemistry, including very high levels of As. The hole did not continue far enough to be sure it had completely penetrated the shale unit. Anomalous geochemistry includes Zn to 0.11%, Ag to 0.57g/t, Au to 69ppb, Pb to 56ppm, As to 893ppm, Sb to 10.4ppm, Bi to 0.98 and Te to 1.90ppm. High Ca down the length of the hole is indicative of strong carbonate alteration in the footwall of The Cup Main Shale unit.

This "Lower Shale Unit" is enclosed within FII type basaltic andesite and is interpreted as sitting within the footwall in relation to The Cup Main Shale stratigraphic succession, it is also a relatively narrow unit of shale and is not expected to be the source of the extremely high conductance levels on this section (6964650N) detected in recent high powered MLTEM surveying. The high conductance is located further to the west and is expected to be in association with sulphidic Main Shale stratigraphy.

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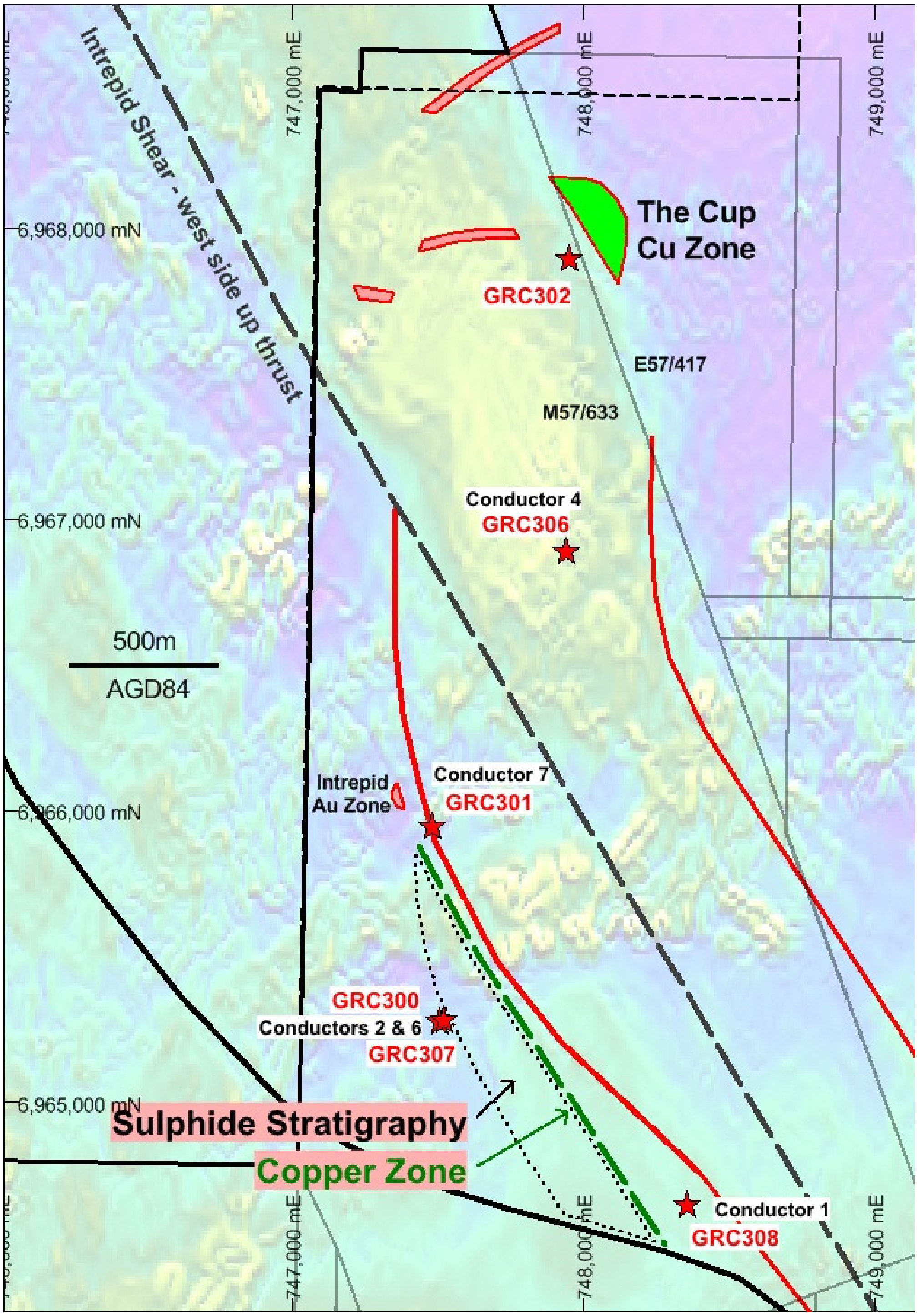

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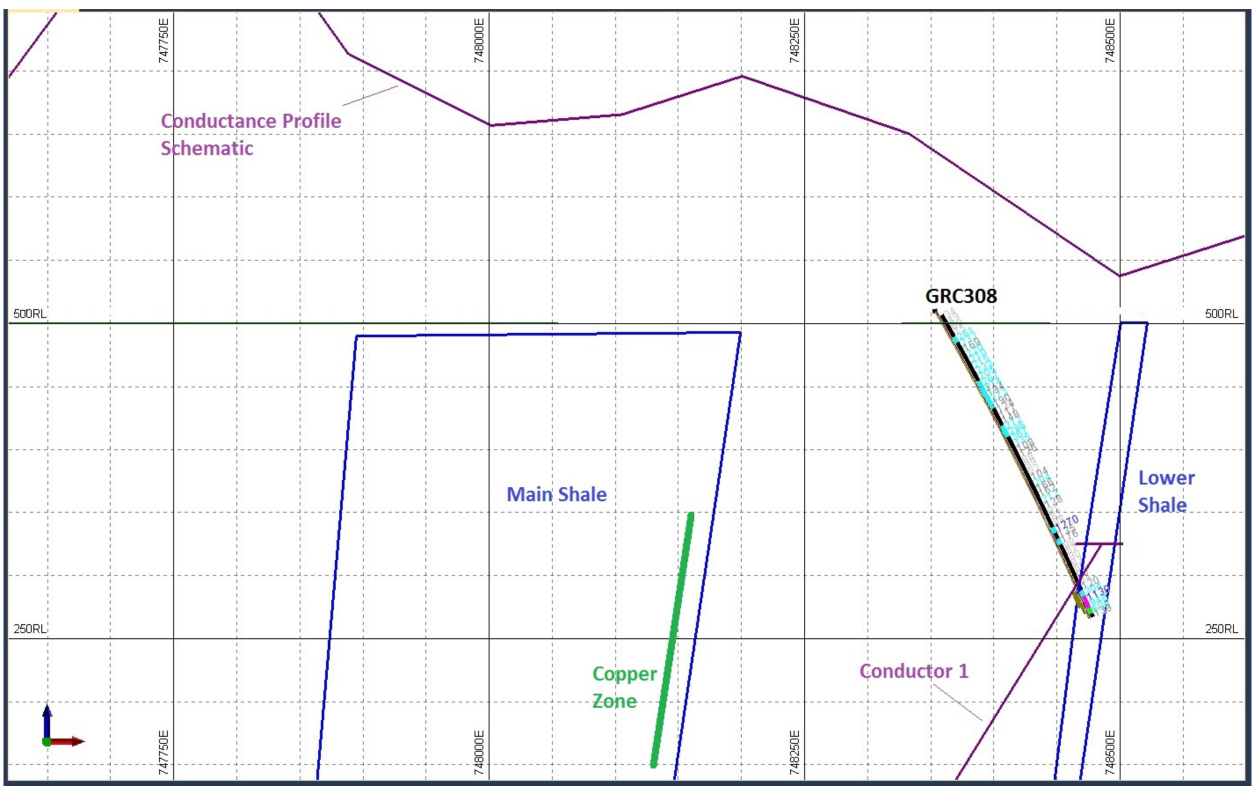
The Lower Shale Unit intersected in GRC308 is part of a high As-Au geochemical zone trending NNW toward Intrepid and SSE toward Gravel Pit, the intersection position in GRC308 delineates steep west dip. FII type stratigraphy in Canadian Archean terrain is documented as fertile for typical VMS (Cu, Zn, Au, Ag) style mineralisation in association with centres of felsic FII volcanism (D. Gadbury and V. Pearson, 2008).

The very high levels of conductance in the vicinity of Conductor 1 would appear to "drown out" elevated conductive signals returned from possible deposits along this VMS horizon in surface based EM work. Continued exploration suitable would include either geochemical vectoring in shallow aircore drilling and/or deep RC drilling geochemical vectoring with possible accompanying downhole EM.



Cross section 6964650N, downhole sulphide and gossan histogram, zinc assays, multielement colour trace

<u>Conductors 2 and 6</u>

GRC300 (305m, drilled west) and GRC307 (285m, drilled east) drilled on cross section 6965300N, see cross section below, targeted very strong EM conductance occurring in close proximity to a trend of elevated multielement concentrations in shallow drilling.

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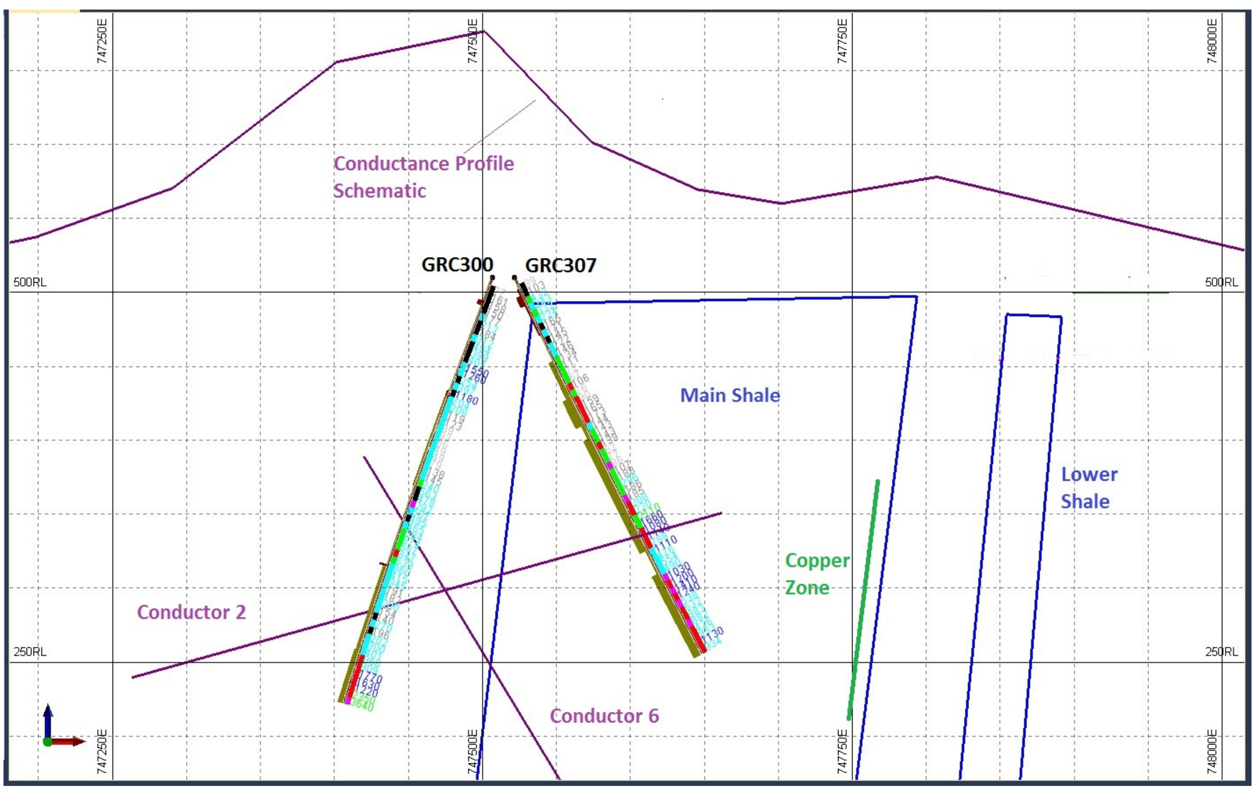
GRC307 intersected an impressive width of massive sulphides and sulphide bearing carbonaceous shale containing very high levels of multielement anomalism from 65m to the end of hole. Multielement anomalism generally increases toward the base of the hole and includes Zn to 0.21%, Ag to 1.46g/t, Au to 35ppb, Pb to 364ppm, As to 156ppm, Sb to 7.63ppm, Bi to 1.69 and Te to 3.30ppm.

This expanse of sulphide rich shale intersected in GRC307 appears to explain the extremely high conductance detected in recent high powered MLTEM work that extends along 1.4km of NNW-SSW strike as shown in the above plan. Stratigraphy at Intrepid is interpreted as dipping steeply to the west, which if correct, leaves at least 150m of sulphide/shale remaining untested to the east of GRC307.

The sulphide rich shale unit appears to be the same stratigraphic succession of shale (“Main Shale”) that occurs at The Cup where there is a strong copper/silver zone located at the base. Dacite volcanic rocks occur at the Cup which may or may not be the case at Intrepid. The shale/dacite stratigraphic position is distinct in that it is located at the transition between volcanic units with very different signature multielement concentration “patterns”. Multielement patterns of hangingwall rocks are aligned with FI signature type (calcalkaline), while footwall rocks are aligned to FII type (transitional between calcalkaline and tholeiitic) and this transition is evident at both The Cup and at Intrepid. Any copper zone equivalent unit at Intrepid remains untested.



Cross section 6965300N, downhole sulphide and gossan histogram, zinc assays, multielement colour trace

Additional to potential for occurrences of "Cup Style" (Cu, Ag) mineralisation at intrepid, similar Canadian Archean FI - FII type VMS districts have world class "giant" deposits such as Laronde (Au, Cu, Zn, Ag) and Horne (Cu, Au). These deposits comprise metal enrichments resulting from hydrothermal "zone refinement" in favourable subsea strata, in stacked lodes with replacement pyrrhotite concentrations that occur across relatively limited strike extent and are located at the outer limit of a volcanic centre.

At Intrepid, there is an intense and discrete magnetic anomaly located directly in the footwall stratigraphy that might fit the above exploration model description and is yet to be drill tested. The Intrepid magnetic anomaly, if validated, is probably in relation to pyrrhotite, especially given that magnetic stringer pyrrhotite has been found in association with the more diffuse magnetic anomaly located directly adjacent and to the north. It would also appear that Intrepid occurs at the verge of the dacite volcanic centre at The Cup.

GRC300 had begun to penetrate strongly multielement anomalous sulphidic carbonaceous shale before the hole was required to be abandoned at 305m ending in 0.36% Zn.

Conductor 3

Not drilled due to time constraints.

Conductor 4

GRC306 for 291m was drilled at Conductor 4 and appears to have traversed a repeat of the stratigraphic sequence at Intrepid dipping shallow to the west, however, geochemical anomalism and conductance are at lower levels.

5m of 0.20% Cu was intersected in the copper zone the base of the Main Shale unit from 115m down hole, associated anomalism includes Zn to 0.11%, Ag to 1.06g/t, As to 140ppm and Te to 1.44ppm.

The hole continued through to the lower carbonaceous shale unit intersecting elevated As-Au anomalism located within carbonate altered footwall mafic andesite. Anomalism in the lower shale unit includes Zn to 0.12%, Ag to 0.75g/t, Au to 25ppb, Pb to 128ppm, As to 134ppm, Sb to 10.3ppm, Bi to 1.01ppm and Te to 2.03ppm.

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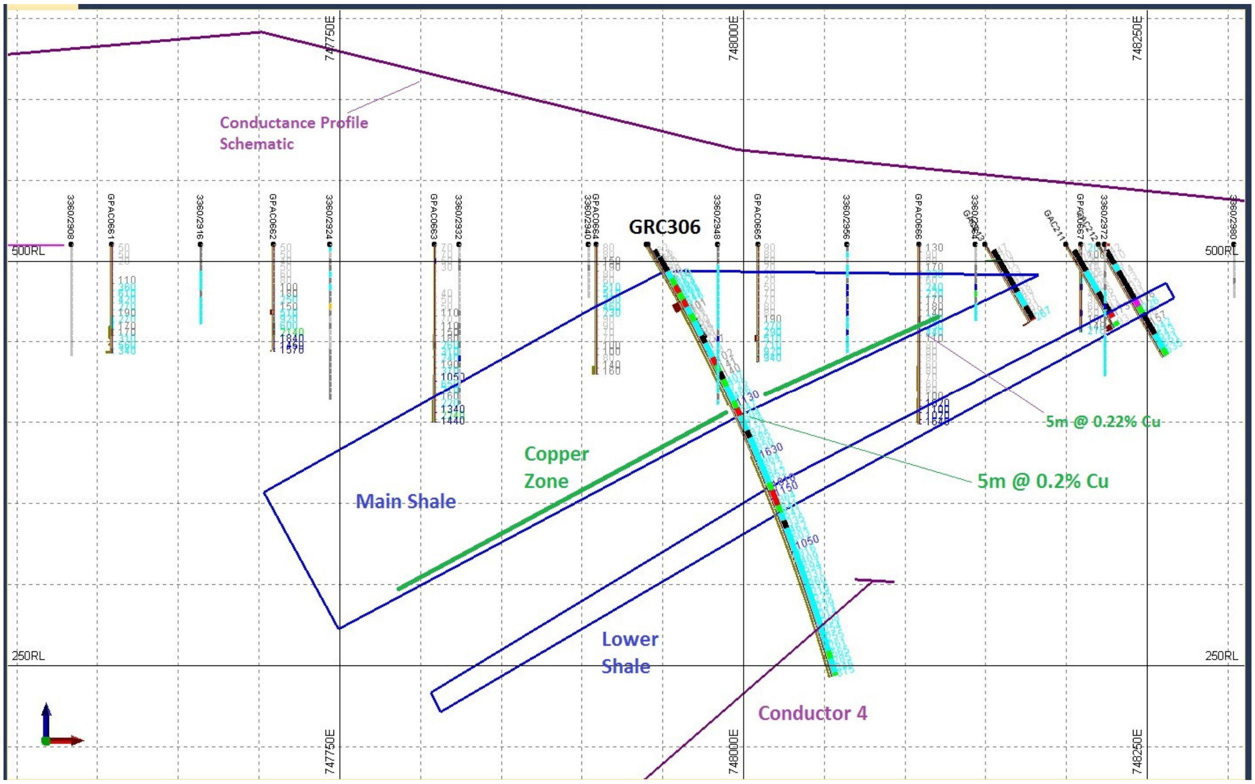

Cross section 6966900N, downhole sulphide and gossan histogram, zinc assays, multielement colour trace

Conductor 5

GRC305 (231m) was drilled at Hypotenuse prospect and intersected VMS related sulphidic carbonaceous shale at expected target depths in the hole. The hole then continued into a possible dacite felsic/intermediate unit before re-entering carbonaceous shale. The hole was abandoned at 231m with high water volumes in the ground. VMS multielement anomalism is generally increasing toward the base of the hole including up to 0.28% Zn, Ag to 0.75g/t, Au to 1.27ppb, Pb to 285ppm, As to 281ppm, Sb to 37.7ppm, Bi to 1.88ppm and Te to 3.95ppm. The hole did not pass into carbonate altered footwall mafic volcanics and so is not interpreted to have penetrated deeply enough to have intersected the possible copper horizon.

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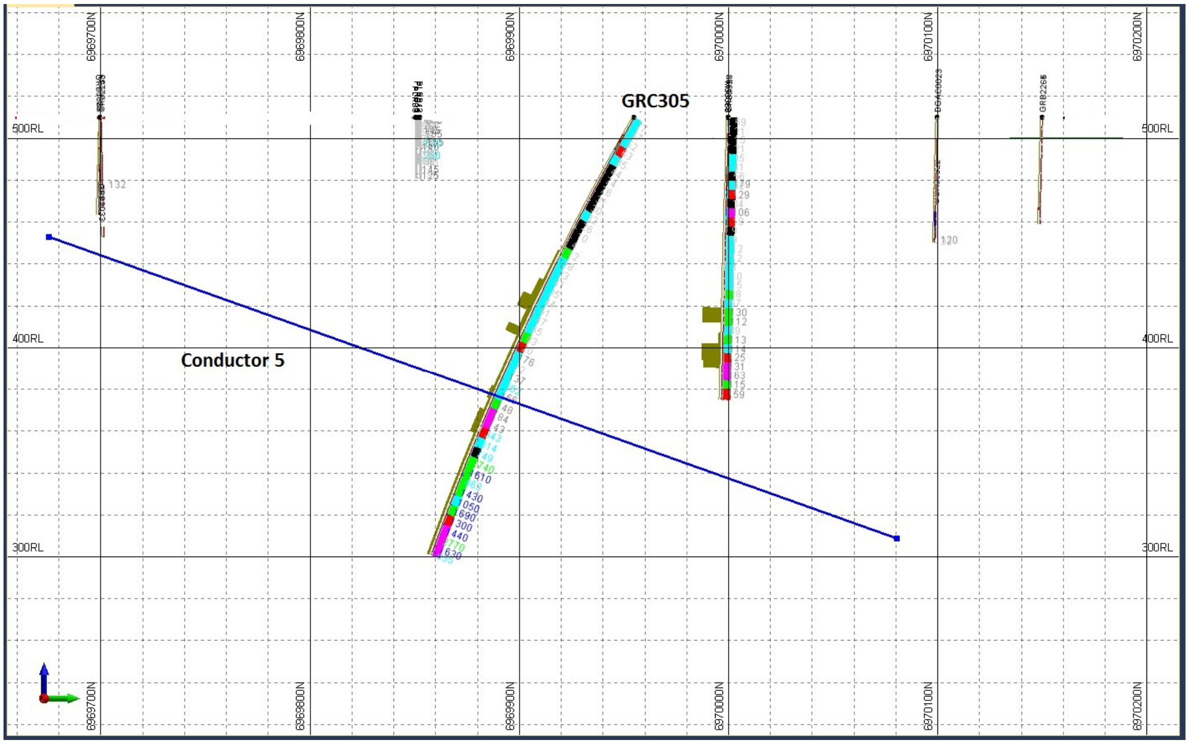
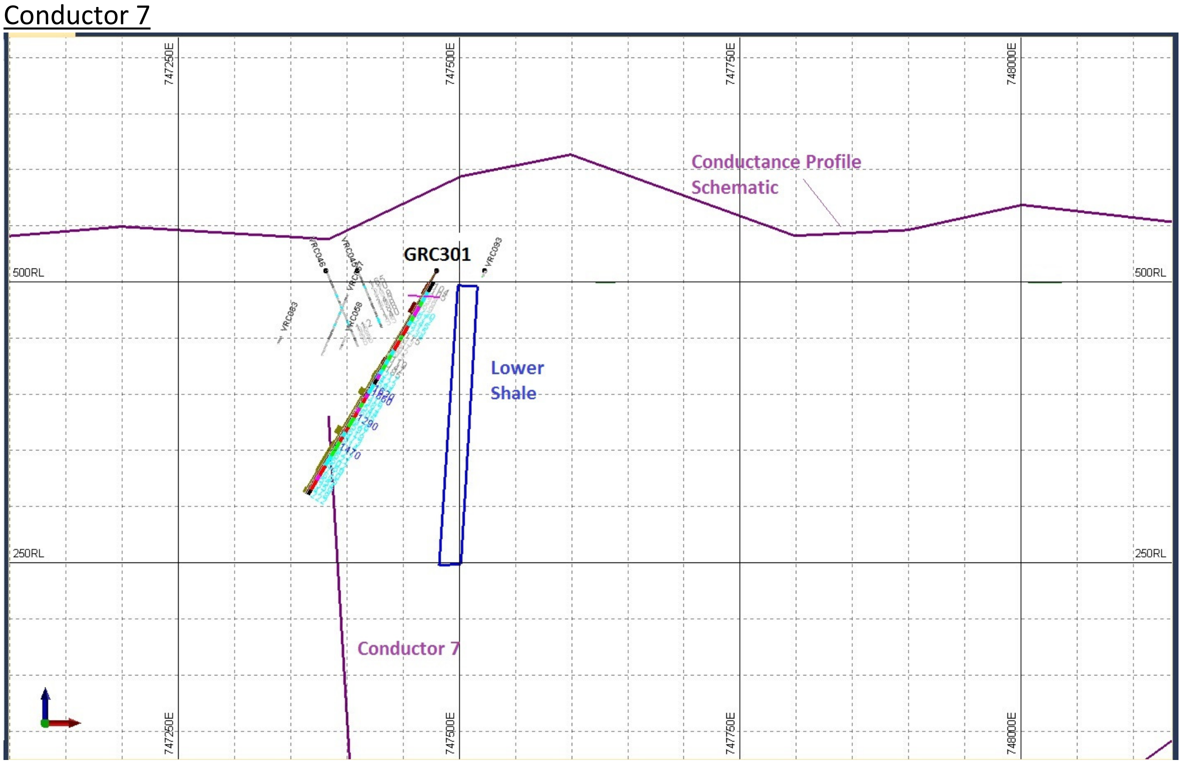


Cross section 748900E, downhole sulphide and gossan histogram, zinc assays, multielement colour trace

Conductor 7



Cross section 6965950N, downhole sulphide and gossan histogram, zinc assays, multielement colour trace

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Future Exploration Efforts

Given the continued difficult market conditions for junior explorers, the Company has decided to re-focus efforts on the gold exploration targets in the near future, as it believes this represents the highest likelihood of being able to move towards developing a strong resource base. The gold system appears to be quite well-defined by gravity and magnetic surveys, as well as some historic drilling. This means that exploration programs will be designed to intersect the 'contact zone' between the basalts and the granodiorite intrusion and the Company has a relatively high degree of confidence of intersecting the gold-bearing contact zone.

It is also expected that this strategy will yield better and more consistent gold results going forward given the stronger definition of the system.

The Company still remains very confident in its interpretation of the VMS system within the stratigraphy at The Cup and will look to start spending more substantial funds towards those targets when market conditions improve and capital is more readily available.

The Company is currently working on a presentation which highlights and explains the gold exploration strategy moving forward.

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JORC Compliance Tables

Criteria	JORC Code Explanation	Commentary
Sampling Techniques	*Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*	**The Cup-** intersections include Gateway Mining Ltd RC (GRC*), diamond (GDD*) and Aircore (GAC*) 2007-2015 and Panoramic Resources Ltd aircore (GPAC*) in 2011. **Intrepid-** intersections include Gateway Mining Ltd RC and AC 2014, Panoramic Resources Ltd aircore 2011, Arimco RC 1991-92 and RAB 1991-2001**.** The **HPMLTEM** survey at The Cup and Intrepid was completed on 300m line spacing with 100m spaced stations. **Montague Boulder** intersections include Gateway Mining Ltd RC, RAB (GRC*, GRB*) 2011-15, CRA RC (85MORC*) 1985, Herald Resources RC - rock roller bit (MOA*) 1988. **NE Pit** intersections include Gateway Mining Ltd RC, RAB (GRC*, GRB*) 2011-2015, CRA RC (85MORC*) 1985, Clackline (Herald) RC rock roller bit, diamond, RAB (RCM*, DDM*, CNE*) 1986. **Hypotenuse/Blind Bat-** includes Gateway RC, aircore, RAB, diamond (GRC*, GAC*, GRB*, GDD*) 2011-2015 and CRA RAB (PLRB* Pluto prospect) 1987.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	**Gateway** 1m RC samples- Split through a riffle or cone splitter under cyclone down to 3kg, wet sample sent directly into plastic bags for maximum sample return then spear or grab sampled down to 3kg. Occasional duplicate field split test work. RC, AC and RAB 5m composite samples- directly into bucket under cyclone and pile set on ground in rows for equal portion and best representation scoop

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		sampling for 3kg of sample. Diamond drilling- Typically half cut 1m NQ core samples. GDD003 is 1m half cut HQ3 samples from 45m depth, very soft clays split with hand tool, crumbling sample broken into smaller fragments for half sampling.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	**Gateway** RC drilling generates 3kg of sample from 1m intervals within zones of interest and 3kg of sample from 5m intervals outside zones of interest. Samples are pulverised to produce a 30g charge for fire assay (Au), a 30g charge for ICP analysis (PGE) and a 0.25g charge for ICP-MS analysis (multiple elements). 1kg size charge for Leachwell bulk leaching used 1m samples through zone of interest in GRC303, 4 at Boulder and NE Pits where high nugget gold is possible, very low variance was returned in 50g FA checks. **CRA** RC drilling was sampled on 1m, RAB on 5m intervals for 50g fire assay analysis and limited multielement analysis. **Herald / Clackline** RC, diamond sampled on 1m, RAB on 2m intervals all for aqua-regia acid digestion, AA analysis. **Panoramic** aircore drilling composite sampled on 4m intervals for Au and multielement analysis (ore grade detection limits). **Arimco** RC, RAB drilling composite sampled on 3m intervals, zones of interest sampled on 1m intervals in RC drill holes. Au analysis, variable As, Sb and limited analysis for other multielements.
Drilling Techniques	*Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of*	**The Cup-** Gateway RC/diamond drilling (GDD003-HQ3 triple tube, GDD001–NQ2. Core orientation via ACE tool) and Panoramic aircore

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	diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	drilling used for exploration evaluation. **Montague Boulder and NE Pit** Gateway RC & RAB, CRA RC, Herald/Clackline RC & RAB & diamond are used for exploration evaluation. **Intrepid**- Gateway RC and Panoramic aircore are used for exploration evaluation. **Hypotenuse/Blind Bat-** Gateway RC, aircore (GAC*) and CRA RAB (PLRB*) used for exploration evaluation. Gateway diamond is only drill testing of Blind Bat target (NQ3, ACE tool orientation).
Drill Sample Recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.*	**Gateway** RC/AC recoveries are logged visually as a volume percentage or G/F/P (good/fair/poor). Diamond drill core recoveries are measured and logged.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	**Gateway** RC/aircore - Every effort is made to ensure minimal return of wet sample and maximum sample recovery. Wet sample is delivered directly from the cyclone into plastic bags from which a spear sample is taken. The cyclone and splitter are regularly cleaned. Larger diameter (HQ3) core and triple tube diamond drilling method was used to drill through near surface clays at The Cup to attain best sample recovery.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	**Gateway** recoveries have generally been very good and a relationship between recovery and grade has not been established. A considerable population of samples of low recovery inside mineralised zones would be required to establish this relationship. One recently drilled diamond hole has twinned an RC hole at The Cup to

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		determine whether grades are underestimated in percussion drilling styles due to the presence of sooty chalcocite. The diamond hole returned copper grades about 10% higher.
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	**Gateway** RC logging includes recording of lithology type, weathering, colour, mineralogy, vein, structure (foliation), sample method, wetness and recovery (estimate by volume). Additional logging for diamond drilling includes RQD, Structural measurements, Geotechnical competency and photography of orientated core in trays.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.	**Gateway** RC logging records lithology, weathering, colour, mineralogy, vein, structure (foliation), sample wetness, sample method used and sample recovery estimate by volume. Extra logging for diamond drilling includes RQD, Structural measurements and Geotechnical competency.
	The total length and percentage of the relevant intersections logged.	**Gateway** drill holes are fully logged.
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.*	**Gateway** core is half cut sampled. Very soft clay in GDD003 were split using a hand tool, crumbling sample was broken into smaller fragments for half sampling.
	If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.	**Gateway** 5m percussion composite samples are scoop sampled wet or dry. 1m samples are split with a cone splitter when dry, and spear sampled when wet. **CRA, Herald/Clackline** 1m RC samples were riffle split.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	**Gateway** samples are submitted to Australian Laboratory Services in Perth. Sample preparation follows industry best practice, the whole

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		3kg sample is dried crushed and pulverised to 85% passing 75 micron to produce a homogeneous representative sub-sample for analysis. Diamond drill core is cut in half via core saw at ALS or Gidgee mine. **Herald/Clackline** samples submitted to Pilbara Laboratories Perth for FA 50 analysis 0.005 lower detection limit.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	**Gateway** via ALS have certified reference materials and/or in house laboratory controls, blanks and replicates analysed with each batch of samples. These quality control results are reported along with sample values. Gateway also submit certified reference materials sourced from Geostats Pty Ltd at a nominal 1/50 samples.
	Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.	**Gateway** field duplicates of 1m samples are generated from a cone splitter as nominated within mineralised zones.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	**Gateway** sample sizes are considered appropriate to give an accurate indication of mineralisation of this nature.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	**Gateway** - Four main analytical techniques have been used. 1) For gold only, 30g (50g) fire assay - total recovery and AAS analysis. 2) Gold and PGE elements, 30g fire assay – total recovery and ICP analysis. 3) Multiple elements, 0.25g four acid digestion – near full recovery and ICP-MS analysis. 4) Gold only 1kg leachwell bulk cyanide leach (for suitable leach recovery materials with possible high nugget gold occurrence)

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	For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc	**FLTEM Survey 2013:** 800 x 300 m loop with five lines 1,500m long and station spacing of 75m totalling 105 stations (CUP1) and 800 x 300m loop with two lines 1500m long and station spacing of 75m totalling 42 stations (CUP2). Time base 1 sec (.25Hz) B-Field Landtem sensor, Smartem 24 Receiver. Supervision and processing of results by Southern Geoscience and conducted by Outer-rim Exploration Services. **HPMLTEM survey 2015:** 300m line spacing 200 x 200m single turn loop, 100m spaced stations, Transmitter HPTX (100 amps), Smartem 24 & 3 component B field sensor ZXY (fluxgate) or landtem. Time base/Frequency: 0.5HZ, Fast Ramp. 2 repeatable readings stacks 128. Supervision and processing of results by Southern Geoscience and conducted by Outer-rim Exploration Services. **Gravity survey 2004:** Nominal station array @ 200m X 400m. Data collection at gravity stations was effected by the employment of a Trimble 5700 RTK GPS system. Gravity readings were taken with a LaCoste & Romberg G Meter (G607). A local gravity base was established with all gravity repeat stations looped back to this point. Processing included the GPS base station configured to collect raw static data @ 30 sec epochs, 24 hrs of this data was submitted to Auslig's AUSPOS service & post processed to generate corrected coords for the initially autonomous RTK base. The finally reprocessed coordinates & levels were then

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		married to the raw gravity data & reduced gravity data was generated. This was further bouguer corrected for assumed density 2.67g/cc.
	Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	**Gateway** internal certified reference materials and field duplicates sent for analysis were returned within acceptable limits of accuracy.
Verification of Sampling and Assaying	*The verification of significant intersections by either independent or alternative company personnel.*	Both the Exploration Manager and Head Geologist have verified significant intersections
	The use of twinned holes.	One recently drilled diamond hole has twinned an RC hole at The Cup to determine whether grades are underestimated in percussion drilling styles due to the presence of sooty chalcocite. The diamond hole returned copper grades about 10% higher.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	**Gateway** primary data is entered into a standard Excel template, loaded and stored in a MS Access relational database, further data validation in Micromine software and visual validation using Micromine plot generations. **Panoramic** drill data was supplied in Excel spreadsheet format and was imported into the Gateway Database. **CRA, Herald/Clackline** drill data acquired, and entered manually via open file annual reports and historic mine plan references.
	Discuss any adjustment to assay data.	No adjustments have been made.
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	**Gateway** collars located by handheld GPS. Expected accuracy is +/-5m for easting and northing and +/-10m for elevation coordinates. **CRA** drill holes were originally located via gridding survey and later

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		corrected via a known survey correction at Whistler with local variations determined via aerial photo observation. **Herald/Clackline** original work conducted in “pegged” grid in local co-ordinates, conversion via known point translation and aerial photo confirmation.
	Specification of the grid system used.	AGD84 (AMG), zone50.
	Quality and adequacy of topographic control.	500mRL is generally applied project wide where there is very flat terrain and GPS accuracy is only inaccurate to (+/-)10m.
Data spacing and distribution	*Data spacing for reporting of Exploration Results.*	See body of announcement - extreme variation of data spacing occurs, over project and prospect scales. Based on latest interpretations closest drill spacing includes:- **The Cup** – drill pattern within a small central zone closing to 50x40m. **Intrepid** – no holes intersect interpreted copper zone to date below highly weathered near surface base metal depleted zone. **Hypotenuse** – no holes intersect interpreted copper zone to date. **Boulder Contact Zone** – see body of announcement. **NE Pit** – N/A one hole drilled below historic pit.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	N/A - Neither a Mineral Resource or an Ore Reserve estimation has been applied.
	Whether sample compositing has been applied.	No compositing has been applied.

Orientation of data in relation to	*Whether the orientation of sampling achieves unbiased sampling of possible*	**The Cup, Boulder Contact Zone, NE Pit** - current interpretation of

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geological structure	*structures and the extent to which this is known, considering the deposit type.*	geological structure supports orientation of drilling/sampling as highly favourable and almost oblique to geological structures. **Intrepid** – see body of announcement.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No bias is known.

Sample security	*The measures taken to ensure sample security.*	Sample chain of custody is from Gateway Mining to trusted subcontracting companies including JPB contracting, Nexus Sadleir/McMahon Burnett Transport who deliver samples to Australian Laboratory Services.

Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	The Company completed a review of RC drilling data and drill chips to further develop and test a model to determine whether underestimation of copper grades has been caused by use of RC drilling only in areas where the dominant copper mineral is sooty chalcocite.

Table 1 – Section 2: Reporting of Exploration Results as required by the 2012 JORC Code

Criteria	JORC Code Explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	**The Cup-** Straddles E57/417 (Gateway 100%) and M57/633. Tenement M57/633 is subject to a Joint Venture with Panoramic Resources Ltd (refer Gateway announcement 12 August 2013 for details). **Intrepid-** Falls within M57/633 Panoramic JV. **Hypotenuse-** within M57/429 (Gateway 75% and Red 5 Ltd 25%) and E57/945 Gateway (100%).

		Boulder Contact Zone (of Montague Boulder Pit) is within M57/98 (Gateway 80% and GoldFan Ltd 20%). **NE Pit** within M57/48 (Gateway 80% and GoldFan Ltd 20%).
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	Tenements are in good standing

Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	Gold was first discovered at Montague in 1905 and historically the Gum Creek Greenstone Belt has produced 1.5 million ounces Au. Over the project area base metal exploration was first carried out in the 70's and 80's by INCO and CRA. Historic mining of approximately 100,000oz of gold occurred along the Airport Trend on the western flank of the Montague Granodiorite by Clackline/Herald Resources during the late 1980's early 1990's and at Whistler Pit mined by Polaris Pacific NL in the early 1990's. Little attention was paid to mineralisation other than gold. At The Cup/Intrepid prospects, gold was explored for by Arimco Mining (1991-1995), little attention was given to base metals apart from at The Cup prospect where strong copper anomalism was discovered in 1993 but was not pursued, and it does not appear as though a VMS model was even contemplated as a scenario for further possible exploration. Gateway Mining commenced exploration at The Cup prospect in 2006 close to the tenement boundary of E57/417. Panoramic Resources Ltd acquired

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		a package of Gidgee tenements in 2011 when it purchased the Gidgee Gold Project. One of these tenements included the Joint Venture tenement M57/633 where Panoramic conducted a program of vertical aircore drilling late in 2011 before entering a Joint Venture agreement with Gateway in 2013. Exploration for VMS mineralisation has been the focus for Gateway since 2006 with the discovery of The Cup prospect, the recent joint venture agreement with Panoramic Resources made for adjoining tenement M57/633 facilitated renewed VMS exploration endeavour. During this recent exploration at The Cup, intrusion related Cu-Ni-PGE mineralisation was intersected for which evaluation is in early stages.

Geology	*Deposit type, geological setting and style of mineralisation.*	The project is located in the Gidgee district of Western Australia approximately 630km NE of Perth and 70km north from the township of Sandstone on the eastern central portion of the Gum Creek Greenstone Belt, of the Southern Cross Province, of the Archean Yilgarn Craton. Local lithology includes volcanic andesitic basalt/dolerite and dacite, volcaniclastic sequences of felsic to intermediate composition, the Montague Granodiorite sub-volcanic intrusion and ultramafic intrusives. Key regional characteristics of a Volcanic Arc Extensional Basin include bimodal volcanic sequences associated with extensive iron formations. Mineralising styles within the project include:

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		1) **VMS Cu-Zn-Au-Ag** potential occurs widely across the project with up to 30km of prospective strike. The Cup, Bevan, Birthday and Gossans Galore systems include carbonaceous shale and massive sulphide units that are strongly base and VMS trace element fertile. 2) **Reduced Intrusion Related Au** mineralisation is flanking the felsic/intermediate granodiorite subvolcanic intrusion. Qtz tourmaline veining with miarolitic cavities, sheeted vein formations, free milling gold, <5% volume sulphides and (Au>Ag), Bi, Te, W element association. 3) **Atypical orogenic Au,** disseminated sulphide style at Victory Creek prospect Au-As-Sb anomaly, in stockwork vein system has adjacent magnetic alteration plume in conglomerate lithology with intruding felsic porphyries and is similar to Wallaby and Kanowna Belle deposits. 4) **Orogenic Au**, The Gidgee Gold Mine is 6.5km west from the NW project boundary and has past production of approx. one million oz. Mineralisation is associated with the NNW-SSE Birthday Fault regional shear structure/unconformity between mafic rock types and conglomerates at Hypotenuse prospect and trending through Gateway project, quartz-carbonate vein arrays

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		aligned to peak orogenic strain with arsenic enrichment. Hypotenuse/Victory Creek association is similar to Golden Mile/Kanowna Belle and Sunrise Dam/Wallaby associations. 5) **Mafic/ultramafic intrusion related Cu-Ni-PGE**, occurs at The Cup and within the northern portion of the project within the Bungarra Igneous Complex.

Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.*	Refer to tables below.
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	

Data Aggregation Methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.*	All reported assays have been length weighted. No top-cuts have been applied.

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	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	N/A
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	N/A, no metal equivalent is reported.

Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.* *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	Down hole lengths are close approximations of true width for **The Cup** Cu-Ag mineralised intercepts reported**, NE Pit** intersections and **Boulder Contact Zone** Au intercepts (projected on long section), down hole length, true width for intersections within the Montague Boulder Pit are otherwise not known.

Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	For The Cup prospect refer to announcements made on 29 November 2013 and 2 December 2013, For Apex refer to announcement made 28/01/2014.

Balanced Reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	Comprehensive results tables included below.

Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics;*	Refer to body of announcement.

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	potential deleterious or contaminating substances.	

Further work	*The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	Refer to body of announcement.

Full details of holes at Boulder Contact Zone, Au intersections (outside Montague Boulder Pit):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Au g/t
85MORC18	RC	28	6966608	750857	500	-60	0	11	13	2	0.89
85MORC18	RC	28	6966608	750857	500	-60	0	22	24	2	0.90
85MORC18	RC	28	6966608	750857	500	-60	0	26	28	2	1.00
85MORC24	RC	21	6966608	750817	500	-60	0				NSI
85MORC25	RC	41	6966586	750817	500	-60	0	27	29	2	0.59
85MORC25	RC	41	6966586	750817	500	-60	0	37	41	4	6.95
AGRC009	RC	137	6966869	750745	500	-60	99	20	25	5	0.99
GRB2426	RAB	21	6966000	750900	500	-60	90				NSI
GRB2427	RAB	21	6966000	750850	500	-60	90				NSI
GRB2428	RAB	39	6966000	750800	500	-60	90				NSI
GRB2429	RAB	41	6966500	750875	500	-60	90				NSI
GRB2430	RAB	27	6966500	750850	500	-60	90				NSI
GRB2431	RAB	10	6966500	750825	500	-60	90				NSI
GRB2432	RAB	22	6966500	750800	500	-60	90				NSI
GRB2433	RAB	27	6966500	750775	500	-60	90				NSI
GRB2434	RAB	30	6966500	750750	500	-60	90				NSI
GRB2435	RAB	29	6966500	750725	500	-60	90				NSI
GRC303	RC	111	6966586	750805	500	-60	75	49	57	8	0.63
MOA119R	RC	58	6966827	750723	500	-90	0	29	31	2	0.64
MOA135R	RC	76	6966637	750743	500	-90	0				NSI
MOA178P	RAB	24	6966927	750723	500	-90	0	4	6	2	2.79
MOA179P	RAB	40	6966927	750743	500	-90	0	30	36	6	1.19
MOA180P	RAB	40	6966927	750763	500	-90	0	0	2	2	0.65
MOA27R	RC	57.5	6966687	750823	500	-57.5	360	26	34	8	0.95

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MOA27R	RC	57.5	6966687	750823	500	-57.5	360	41	44	3	0.78
MOA28R	RC	42	6966725	750844	500	-59	360	22	24	2	1.03
MOA29R	RC	56	6966686	750823	500	-90	0	50	52	2	0.58
MOA29R	RC	56	6966686	750823	500	-90	0	54	56	2	1.39
MOA32R	**RC**	**62.8**	**6966688**	**750783**	**500**	**-90**	**0**	**45**	**50**	**5**	**4.08**
MOA33R	**RC**	**64.8**	**6966667**	**750783**	**500**	**-90**	**0**	**48**	**51**	**3**	**3.42**
MOA36R	**RC**	**65**	**6966688**	**750763**	**500**	**-90**	**0**	**55**	**58**	**3**	**3.03**
MOA43R	RC	64	6966748	750743	500	-90	0	55	57	2	1.95
MOA44R	RC	62.2	6966747	750729	500	-90	0	47	51	4	1.87
MOA49R	RC	64	6966808	750743	500	-90	0	39	41	2	1.70
MOA52R	RC	63	6966728	750743	500	-90	0	44	46	2	1.28
MOA52R	RC	63	6966728	750743	500	-90	0	48	50	2	0.67
MOA62R	RC	40	6966829	750761	500	-90	0	26	28	2	0.54
MOA62R	RC	40	6966829	750761	500	-90	0	30	32	2	0.52
MOA63R	**RC**	**48**	**6966827**	**750743**	**500**	**-90**	**0**	**28**	**35**	**7**	**2.61**
MOA64R	RC	48	6966687	750742	500	-90	0	17	20	3	1.21
MOA65R	RC	42	6966667	750743	500	-90	0	19	21	2	1.18
MOA66R	RC	42	6966647	750743	500	-90	0	22	27	5	3.50
MOA90R	RC	43	6966867	750743	500	-90	0				NSI
MOA91R	RC	36	6966868	750761	500	-90	0	0	2	2	0.66
MOA91R	RC	36	6966868	750761	500	-90	0	13	15	2	0.59
MOA92R	RC	56	6966867	750720	500	-90	0	29	32	3	2.17
MOA93R	RC	50	6966867	750703	500	-90	0	17	19	2	0.52
MOA93R	RC	50	6966867	750703	500	-90	0	30	32	2	2.27
MOA94R	RC	45	6966907	750744	500	-90	0	18	26	8	1.34
MOA94R	RC	45	6966907	750744	500	-90	0	24	26	2	1.96
MOA95R	RC	51	6966907	750723	500	-90	0				NSI

Full details of holes at Boulder Contact Zone, Au intersections (inside Montague Boulder Pit):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Au g/t
85MORC17	RC	21	6966630	750817	500	-60	0	6	8	2	6.55
MOA20R	RC	33	6966738	750802	500	-90	0	0	2	2	0.70
MOA20R	**RC**	**33**	**6966738**	**750802**	**500**	**-90**	**0**	**5**	**8**	**3**	**13.57**
MOA20R	RC	33	6966738	750802	500	-90	0	29	31	2	0.53
MOA21R	RC	39.5	6966697	750806	500	-59	360	27	35	8	1.88
MOA21R	RC	39.5	6966697	750806	500	-59	360	38	40	2	15.30
MOA22R	**RC**	**48.5**	**6966675**	**750807**	**500**	**-58**	**360**	**28**	**33**	**5**	**4.95**
MOA22R	RC	48.5	6966675	750807	500	-58	360	46	49	3	0.69

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MOA23R	RC	49	6966718	750783	500	-59.5	360	5	7	2	0.57
MOA23R	**RC**	**49**	**6966718**	**750783**	**500**	**-59.5**	**360**	**29**	**36**	**7**	**4.27**
MOA24R	**RC**	**51**	**6966697**	**750783**	**500**	**-60**	**360**	**35**	**43**	**6**	**12.30**
MOA24R	RC	51	6966697	750783	500	-60	360	47	49	2	2.43
MOA26R	RC	51	6966708	750823	500	-55	360	17	19	2	1.16
MOA26R	RC	51	6966708	750823	500	-55	360	25	27	2	2.45
MOA28R	**RC**	**42**	**6966725**	**750844**	**500**	**-59**	**360**	**6**	**10**	**3**	**12.53**
MOA29R	RC	56	6966686	750823	500	-90	0	21	25	4	0.60
MOA29R	RC	56	6966686	750823	500	-90	0	29	33	4	0.95
MOA29R	RC	56	6966686	750823	500	-90	0	36	42	6	1.49
MOA29R	RC	56	6966686	750823	500	-90	0	43	45	2	0.50
MOA30R	**RC**	**54**	**6966667**	**750823**	**500**	**-90**	**0**	**23**	**39**	**16**	**2.20**
									inc.	**4**	**3.96**
MOA30R	RC	54	6966667	750823	500	-90	0	42	46	4	1.05
MOA30R	RC	54	6966667	750823	500	-90	0	48	51	3	1.83
MOA31R	RC	59.2	6966667	750803	500	-90	0	20	22	2	1.11
MOA31R	RC	59.2	6966667	750803	500	-90	0	24	39	6	1.12
MOA31R	**RC**	**59.2**	**6966667**	**750803**	**500**	**-90**	**0**	**33**	**48**	**15**	**1.99**
									inc.	**3**	**5.22**
MOA31R	RC	59.2	6966667	750803	500	-90	0	52	54	2	0.93
MOA34R	RC	25	6966707	750763	500	-90	0				NSI
MOA35R	RC	31	6966704	750763	500	-90	0				NSI
MOA37R	RC	49	6966748	750762	500	-90	0	0	2	2	0.69
MOA37R	**RC**	**49**	**6966748**	**750762**	**500**	**-90**	**0**	**36**	**42**	**6**	**11.77**
MOA39R	RC	43	6966788	750762	500	-90	0	14	16	2	1.10
MOA39R	**RC**	**43**	**6966788**	**750762**	**500**	**-90**	**0**	**25**	**30**	**4**	**2.81**
MOA39R	RC	43	6966788	750762	500	-90	0	41	43	2	0.63
MOA41R	RC	36	6966748	750791	500	-90	0	0	2	2	0.79
MOA41R	RC	36	6966748	750791	500	-90	0	6	8	2	2.16
MOA41R	RC	36	6966748	750791	500	-90	0	13	17	4	0.70
MOA42R	RC	42	6966748	750772	500	-90	0	26	30	4	0.73
MOA48R	RC	48	6966808	750761	500	-90	0	19	21	2	1.41
MOA48R	**RC**	**48**	**6966808**	**750761**	**500**	**-90**	**0**	**26**	**32**	**5**	**6.98**
MOA50R	RC	60	6966787	750743	500	-90	0				NSI
MOA67R	RC	54	6966645	750823	500	-90	0	29	31	2	0.63
MOA72R	RC	42	6966667	750863	500	-90	0	29	32	3	0.95
MOA73R	RC	48	6966647	750862	500	-90	0				NSI

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Full details of holes at NE Pit, Au intersections (outside NE Pit):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Au g/t
85MORC27	RC	35	6965697	751084	500	-90	0	25	27	2	0.57
85MORC29	RC	35	6965737	751097	500	-90	0	27	29	2	0.50
CNE067	RAB	20	6965699	750679	500	-60	90				NSI
CNE068	RAB	20	6965699	750659	500	-60	90				NSI
CNE093	RAB	20	6965650	751056	500	-60	90				NSI
CNE103	RAB	20	6965650	750856	500	-60	90	17	20	3	0.63
CNE109	RAB	20	6965649	750739	500	-60	90				NSI
CNE110	RAB	20	6965649	750719	500	-60	90				NSI
CNE111	RAB	20	6965649	750699	500	-60	90				NSI
CNE117	RAB	20	6965849	750989	500	-60	90				NSI
CNE121	RAB	20	6965849	750909	500	-60	90				NSI
DDM002	DD	40.85	6965712	751006	500	-90	0	30	32	2	0.53
DDM003	DD	45.4	6965711	750997	500	-90	0	31	33	2	0.52
DDM003	DD	45.4	6965711	750997	500	-90	0	39	42	3	1.36
DDM006	DD	41.8	6965690	750996	500	-90	0	35	41	6	1.28
DDM007	DD	40.8	6965682	750986	500	-90	0	27	29	2	0.52
DDM007	DD	40.8	6965682	750986	500	-90	0	33	35	2	7.11
DDM008	DD	39.3	6965674	750966	500	-90	0	27	29	2	1.24
GRB1256	RAB	26	6965769	750860	500	-60	90				NSI
GRB1257	RAB	48	6965792	750807	500	-60	90				NSI
GRB1258	RAB	38	6965788	750779	500	-60	90				NSI
GRB1259	RAB	20	6965788	750723	500	-60	90				NSI
GRB1260	RAB	21	6965789	750655	500	-60	90				NSI
GRB1261	RAB	37	6965795	750604	500	-60	90				NSI
GRB1471	RAB	42	6965600	751100	500	-60	90				NSI
GRB1472	RAB	38	6965793	750827	500	-60	90	30	35	5	0.81
GRB1473	RAB	44	6965788	750792	500	-60	90				NSI
GRB1672	RAB	19	6965595	751050	500	-60	90				NSI
GRB1673	RAB	31	6965588	751000	500	-60	90				NSI
GRB1784	RAB	25	6965600	751075	500	-60	270	13	18	5	0.65
GRB1785	RAB	37	6965600	751100	500	-60	270				NSI
GRB1859	RAB	47	6965925	751050	500	-60	90				NSI
GRB1860	RAB	17	6965930	751000	500	-60	90				NSI
GRB1861	RAB	9	6965931	750950	500	-60	90				NSI
GRB1862	RAB	17	6965925	750900	500	-60	90				NSI
GRB1863	RAB	41	6965925	750850	500	-60	90				NSI

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GRB1864	RAB	42	6965925	750800	500	-60	90				NSI
GRB1865	RAB	43	6965925	750750	500	-60	90				NSI
GRB1866	RAB	41	6965550	751000	500	-60	270				NSI
GRB1867	RAB	32	6965550	751050	500	-60	270				NSI
GRB1868	RAB	32	6965550	751100	500	-60	270				NSI
GRB2420	RAB	27	6965500	750800	500	-60	90				NSI
GRB2421	RAB	42	6965500	750775	500	-60	90	20	30	10	1.62
GRB2422	RAB	47	6965500	750750	500	-60	90				NSI
GRB2423	RAB	15	6965500	750700	500	-60	90				NSI
GRB2424	RAB	12	6965515	750650	500	-60	90				NSI
GRB2425	RAB	27	6965500	750600	500	-60	90	20	27	7	0.67
GRB3012	RAB	48	6965800	751100	500	-60	90				NSI
GRB3013	RAB	48	6965800	751050	500	-60	90				NSI
GRC304	RC	117	6965663	750923	500	-60	90	41	43	2	2.31
RCM111	RC	19	6965652	751046	500	-70	90	17	19	2	0.52
RCM119	RC	17	6965632	751036	500	-70	90				NSI
RCM120	RC	22	6965632	751026	500	-70	90	4	6	2	1.15
RCM121	RC	25	6965632	751016	500	-70	90	15	17	2	1.28
RCM121	RC	25	6965632	751016	500	-70	90	23	25	2	0.89
RCM122	RC	23	6965632	751006	500	-70	90	21	23	2	0.65
RCM123	RC	18	6965642	751059	500	-70	89				NSI
RCM125	RC	18	6965652	751056	500	-70	90	7	9	2	0.70
RCM126	RC	15	6965672	751066	500	-70	88				NSI
RCM147	RC	30	6965730	751056	500	-70	89	15	17	2	1.07
RCM147	RC	30	6965730	751056	500	-70	89	22	25	3	2.14
RCM149	RC	35	6965750	751036	500	-90	0				NSI
RCM150	RC	24	6965750	751056	500	-70	89				NSI
RCM151	RC	34	6965750	751046	500	-70	89				NSI
RCM152	RC	46	6965770	751056	500	-70	89				NSI
RCM169	RC	28	6965672	750966	500	-90	0				NSI
RCM17	RC	69	6965708	751026	500	-70	65	22	25	2	0.55
RCM170	RC	42	6965672	750956	500	-90	0	25	32	7	0.99
RCM171	RC	57	6965675	750936	500	-90	0				NSI
RCM173	RC	44	6965692	750996	500	-90	0	38	41	3	0.91
RCM174	RC	44	6965692	750986	500	-90	0				NSI
RCM175	RC	43	6965692	750976	500	-90	0				NSI
RCM176	RC	44	6965710	750996	500	-90	0	32	34	2	1.10
RCM177	RC	48	6965710	750981	500	-90	0				NSI
RCM178	RC	42	6965730	751006	500	-70	89	**35**	**39**	**4**	**4.17**
RCM179	RC	47	6965730	750996	500	-90	0	24	26	2	1.99

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RCM179	RC	47	6965730	750996	500	-90	0	35	37	2	2.73
RCM18	RC	81	6965740	751011	500	-70	65	36	39	3	3.77
RCM18	RC	81	6965740	751011	500	-70	65	51	54	3	0.83
RCM182	RC	43	6965632	750956	500	-90	0	40	43	3	0.99
RCM185	RC	39	6965610	750936	500	-90	0	33	39	6	1.05
RCM191	RC	48	6965591	750916	500	-90	0	39	41	2	0.60
RCM192	RC	52	6965570	750916	500	-90	0				NSI
RCM193	RC	34	6965571	750896	500	-90	0				NSI
RCM194	RC	36	6965571	750936	500	-90	0	18	20	2	0.64
RCM206	RC	35	6965580	750926	500	-90	0	25	27	2	0.87
RCM208	RC	35	6965570	750956	500	-90	0				NSI
RCM209	RC	47	6965571	750876	500	-90	0				NSI
RCM210	RC	41	6965550	750875	500	-90	0				NSI
RCM211	RC	30	6965550	750896	500	-90	0				NSI
RCM212	RC	24	6965550	750915	500	-90	0				NSI
RCM213	RC	32	6965610	750916	500	-90	0				NSI
RCM214	RC	42	6965627	750915	500	-90	0	15	17	2	0.90
RCM33	RC	79.5	6965735	750991	500	-70	65	40	42	2	2.79
RCM33	RC	79.5	6965735	750991	500	-70	65	44	47	3	1.10
RCM75	RC	40	6965550	750942	500	-60	270	3	5	2	0.52
RCM76	RC	30	6965560	750931	500	-60	90	20	22	2	0.50
RCM78	RC	40	6965788	750994	500	-60	65				NSI
RCM90	RC	31	6965549	750769	500	-60	90				NSI

Full details of holes at NE Pit, Au intersections (inside NE Pit):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Au g/t
CNE094	RAB	20	6965650	751036	500	-60	90	5	11	6	2.69
CNE095	RAB	20	6965650	751016	500	-60	90	**5**	**14**	**9**	**12.97**
CNE096	RAB	20	6965650	750996	500	-60	90				NSI
DDM001	DD	36.3	6965710	751025	500	-90	0	**21**	**25**	**4**	**36.84**
DDM004	DD	36.4	6965693	751006	500	-90	0	21	25	4	1.22
DDM004	DD	36.4	6965693	751006	500	-90	0	28	31	3	1.31
DDM005	DD	33.3	6965690	751016	500	-90	0	**20**	**22**	**2**	**85.10**
DDM005	DD	33.3	6965690	751016	500	-90	0	**25**	**29**	**4**	**12.73**
DDM009	DD	30.3	6965632	750946	500	-90	0				NSI
GRC151	RC	75	6965669	750991	500	-60	90	4	12	8	0.66
GRC151	RC	75	6965669	750991	500	-60	90	27	29	2	0.69
GRC152	RC	75	6965629	750951	500	-60	90	12	14	2	0.71
GRC152	RC	75	6965629	750951	500	-60	90	25	27	2	1.04

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RCM100	RC	29	6965692	751015	500	-70	90	2	4	2	0.98
RCM101	RC	25	6965682	751036	500	-70	90				NSI
RCM102	RC	26	6965682	751025	500	-70	90	13	15	2	1.37
RCM102	RC	26	6965682	751025	500	-70	90	**18**	**25**	**7**	**13.99**
RCM103	RC	18	6965672	751046	500	-70	90	0	2	2	1.36
RCM103	RC	18	6965672	751046	500	-70	90	8	13	5	0.93
RCM104	RC	19	6965672	751036	500	-70	90	7	14	7	2.70
RCM105	RC	23	6965672	751026	500	-70	90	10	12	2	4.90
RCM105	RC	23	6965672	751026	500	-70	90	15	19	4	1.13
RCM106	RC	28	6965672	751016	500	-70	90	17	21	4	1.42
RCM106	RC	28	6965672	751016	500	-70	90	25	27	2	1.08
RCM107	RC	21	6965662	751036	500	-70	90	**6**	**11**	**5**	**7.20**
RCM108	RC	22	6965662	751025	500	-70	90	**9**	**14**	**5**	**7.57**
RCM109	RC	28	6965662	751016	500	-70	90	15	22	7	1.29
RCM110	RC	29	6965662	751006	500	-70	90	15	21	6	1.33
RCM111	RC	19	6965652	751046	500	-70	90	5	8	3	0.55
RCM111	RC	19	6965652	751046	500	-70	90	11	13	2	0.64
RCM112	RC	23	6965652	751026	500	-70	90	**5**	**11**	**6**	**4.05**
RCM112	RC	23	6965652	751026	500	-70	90	15	20	5	0.74
RCM113	RC	29	6965652	751006	500	-70	90	16	18	2	0.66
RCM113	RC	29	6965652	751006	500	-70	90	**21**	**25**	**4**	**4.57**
RCM114	RC	16	6965642	751046	500	-70	90	0	4	5	1.68
RCM114	RC	16	6965642	751046	500	-70	90	7	9	2	0.59
RCM115	RC	20	6965642	751036	500	-70	90	0	10	10	1.06
RCM116	RC	26	6965642	751026	500	-70	90	**3**	**10**	**7**	**3.49**
RCM116	RC	26	6965642	751026	500	-70	90	13	15	2	0.83
RCM117	RC	25	6965642	751016	500	-70	90	4	7	3	4.26
RCM118	RC	27	6965642	751006	500	-70	90	8	10	2	0.63
RCM118	RC	27	6965642	751006	500	-70	90	24	27	3	1.04
RCM124	RC	18	6965662	751046	500	-70	89	3	10	7	1.14
RCM127	RC	18	6965672	751056	500	-70	89	**4**	**9**	**5**	**8.83**
RCM128	RC	18	6965682	751066	500	-70	89	2	6	4	1.03
RCM129	RC	18	6965682	751056	500	-70	89	1	12	11	0.84
RCM130	RC	19	6965692	751066	500	-70	89				NSI
RCM131	RC	18	6965692	751061	500	-90	0	11	13	2	0.63
RCM132	RC	25	6965710	751041	500	-90	0	**3**	**7**	**4**	**26.10**
RCM133	RC	24	6965714	751056	500	-70	89				NSI
RCM134	RC	24	6965692	751046	500	-70	90	16	24	8	1.01
RCM135	RC	32	6965692	751006	500	-70	86	**23**	**32**	**9**	**12.41**
RCM136	RC	34	6965682	751015	500	-70	90	16	18	2	0.54

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RCM136	RC	34	6965682	751015	500	-70	90	21	24	3	1.91
RCM137	RC	31	6965682	751006	500	-70	90	**20**	**31**	**11**	**3.21**
RCM138	RC	29	6965672	751006	500	-70	269	20	23	3	1.27
RCM139	RC	28	6965662	750996	500	-90	0	20	26	6	3.61
RCM140	RC	27	6965652	750996	500	-90	0	21	24	3	2.60
RCM141	RC	25	6965642	750996	500	-90	0				NSI
RCM142	RC	30	6965710	751033	500	-70	269	28	30	2	0.51
RCM143	RC	30	6965710	751016	500	-70	89	**22**	**30**	**8**	**17.84**
RCM144	RC	36	6965710	751006	500	-70	89	21	23	2	0.71
RCM144	RC	36	6965710	751006	500	-70	89	**25**	**36**	**11**	**4.07**
RCM145	RC	30	6965730	751026	500	-70	269.5	19	21	2	2.62
RCM145	RC	30	6965730	751026	500	-70	269.5	24	30	6	1.98
RCM146	RC	36	6965730	751016	500	-70	89	25	27	2	1.02
RCM146	RC	36	6965730	751016	500	-70	89	29	35	6	2.62
RCM148	RC	33	6965730	751046	500	-90	0				NSI
RCM162	RC	28	6965652	751016	500	-70	89	4	6	2	0.64
RCM162	RC	28	6965652	751016	500	-70	89	12	15	3	0.90
RCM162	RC	28	6965652	751016	500	-70	89	**24**	**28**	**4**	**13.25**
RCM163	RC	31	6965652	750986	500	-90	0	21	23	2	0.51
RCM164	RC	35	6965652	750976	500	-90	0	**16**	**18**	**2**	**11.74**
RCM164	RC	35	6965652	750976	500	-90	0	33	35	2	0.55
RCM165	RC	51	6965652	750956	500	-90	0	22	24	2	1.66
RCM165	RC	51	6965652	750956	500	-90	0	34	36	2	1.23
RCM166	RC	34.5	6965672	750996	500	-90	0	21	27	6	1.88
RCM166	RC	34.5	6965672	750996	500	-90	0	32	35	3	0.81
RCM167	RC	33	6965672	750986	500	-90	0	20	29	9	1.51
RCM168	RC	35	6965672	750976	500	-90	0				NSI
RCM172	RC	37	6965682	750996	500	-90	0	**22**	**37**	**15**	**3.80**
RCM18	RC	81	6965740	751011	500	-70	65	22	27	5	1.62
RCM180	RC	27	6965632	750996	500	-90	0	5	7	2	1.36
RCM181	RC	29	6965632	750976	500	-90	0	16	20	4	1.12
RCM182	RC	43	6965632	750956	500	-90	0	**11**	**21**	**10**	**3.55**
RCM183	RC	27	6965610	750976	500	-90	0	17	19	2	0.72
RCM183	RC	27	6965610	750976	500	-90	0	23	25	2	0.87
RCM184	RC	30	6965610	750956	500	-90	0	14	23	9	1.40
RCM184	RC	30	6965610	750956	500	-90	0	26	28	2	0.51
RCM185	RC	39	6965610	750936	500	-90	0	14	16	2	1.18
RCM185	RC	39	6965610	750936	500	-90	0	19	21	2	1.56
RCM189	RC	33	6965591	750955	500	-90	0	17	19	2	0.60
RCM190	RC	33	6965590	750936	500	-90	0	5	20	15	2.06

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RCM202	RC	34	6965600	750946	500	-90	0	11	13	2	1.58
RCM202	RC	34	6965600	750946	500	-90	0	**16**	**20**	**4**	**6.14**
RCM202	RC	34	6965600	750946	500	-90	0	26	30	4	1.58
RCM204	RC	34	6965590	750946	500	-90	0	19	21	2	0.52
RCM205	RC	39	6965590	750926	500	-90	0	5	7	2	0.57
RCM205	RC	39	6965590	750926	500	-90	0	16	18	2	1.04
RCM205	RC	39	6965590	750926	500	-90	0	24	29	5	0.86
RCM206	RC	35	6965580	750926	500	-90	0	7	9	2	0.71
RCM207	RC	27	6965581	750936	500	-90	0	2	5	3	4.42
RCM207	RC	27	6965581	750936	500	-90	0	15	20	5	1.38
RCM77	RC	24	6965683	751046	500	-60	64	**10**	**17**	**7**	**5.38**
RCM77	RC	24	6965683	751046	500	-60	64	22	24	2	0.51
RCM98	RC	23	6965692	751036	500	-70	90	16	21	5	0.83
RCM99	RC	27	6965692	751026	500	-70	90	**19**	**25**	**6**	**3.82**

Full details of holes at The Cup, Cu and Ag intersections (Holes Analysed for Multi-Elements):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Cu%	Ag g/t
AGRC007	RC	162	6967997	747987	500	-90	0				NSI	NSI
GAC030	AC	101	6968500	748000	500	-60	90				NSI	NSI
GAC031	AC	42	6968500	747900	500	-60	90				NSI	NSI
GAC032	AC	105	6968500	747800	500	-60	90				NSI	NSI
GAC033	AC	76	6968500	747798	500	-90	0				NSI	NSI
GAC034	AC	56	6968070	747970	500	-90	0				NSI	NSI
GDD001	DD_RC	664.2	6967790	747498	500	-75	90	59	61	2	0.79	3.91
GDD003	**DD**	**120.6**	**6968001**	**747979**	**500**	**-60**	**90**	**87**	**114**	**27**	**1.55**	**0.95**
GPAC0618	AC	10	6968108	747859	500	-90	0				NSI	NSI
GPAC0619	AC	90	6968113	747839	500	-90	0				NSI	NSI
GPAC0620	AC	90	6968108	747759	500	-90	0	64	80	16	0.33	1.50
GPAC0621	AC	93	6968108	747659	500	-90	0				NSI	NSI
GPAC0622	AC	96	6968108	747559	500	-90	0				NSI	NSI
GPAC0623	AC	117	6968108	747459	500	-90	0				NSI	NSI
GPAC0624	AC	144	6968108	747349	500	-90	0				NSI	NSI
GPAC0626	AC	93	6967908	747159	500	-90	0				NSI	NSI
GPAC0627	AC	123	6967908	747259	500	-90	0				NSI	NSI
GPAC0628	AC	129	6967908	747359	500	-90	0				NSI	NSI
GPAC0629	AC	141	6967908	747459	500	-90	0				NSI	NSI
GPAC0630	AC	129	6967908	747559	500	-90	0	56	60	4	0.21	3.00
GPAC0631	AC	120	6967908	747659	500	-90	0	68	72	4	0.37	NSI
GPAC0632	**AC**	**129**	**6967908**	**747759**	**500**	**-90**	**0**	**64**	**76**	**12**	**0.74**	**NSI**

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GPAC0633	AC	141	6967908	747859	500	-90	0				NSI	NSI
GPAC0634	AC	115	6967908	747959	500	-90	0				NSI	NSI
GPAC0636	AC	90	6967708	747159	500	-90	0				NSI	NSI
GPAC0637	AC	105	6967708	747259	500	-90	0				NSI	NSI
GPAC0638	AC	135	6967708	747359	500	-90	0				NSI	NSI
GPAC0639	AC	129	6967708	747459	500	-90	0				NSI	NSI
GPAC0640	AC	156	6967708	747559	500	-90	0	44	48	4	0.23	3
GPAC0641	AC	123	6967608	747109	500	-90	0				NSI	NSI
GPAC0642	AC	105	6967608	747209	500	-90	0				NSI	NSI
GPAC0643	AC	126	6967608	747309	500	-90	0				NSI	NSI
GPAC0692	AC	63	6968408	747209	500	-90	0				NSI	NSI
GPAC0693	AC	92	6968408	747359	500	-90	0				NSI	NSI
GPAC0702	AC	102	6967883	747274	500	-90	0				NSI	NSI
GPAC0703	AC	102	6967894	747300	500	-90	0				NSI	NSI
GRB2361	RAB	50	6968600	748500	500	-60	90				NSI	NSI
GRB2478	RAB	32	6968000	748200	500	-60	90				NSI	NSI
GRB2479	RAB	42	6968000	748175	500	-60	90				NSI	NSI
GRB2480	RAB	49	6968000	748150	500	-60	90				NSI	NSI
GRB2481	RAB	36	6968000	748125	500	-60	90				NSI	NSI
GRB2482	RAB	26	6968000	748100	500	-60	90				NSI	NSI
GRB2483	RAB	38	6968000	748050	500	-60	90	35	38	3	0.3	1.2
GRB2484	RAB	45	6968000	748000	500	-60	90				NSI	NSI
GRB2485	RAB	30	6968000	747950	500	-60	90				NSI	NSI
GRB2486	RAB	49	6968200	748400	500	-60	90				NSI	NSI
GRB2487	RAB	45	6968200	748350	500	-60	90				NSI	NSI
GRB2488	RAB	50	6968200	748300	500	-60	90				NSI	NSI
GRB2489	RAB	55	6968200	748250	500	-60	90				NSI	NSI
GRB2490	RAB	25	6968200	748200	500	-60	90				NSI	NSI
GRB2493	RAB	51	6968400	748500	500	-60	90				NSI	NSI
GRB2494	RAB	20	6968400	748450	500	-60	90				NSI	NSI
GRB2495	RAB	48	6968400	748400	500	-60	90				NSI	NSI
GRB2565	RAB	38	6968500	748000	500	-60	90				NSI	NSI
GRB2566	RAB	16	6968500	747950	500	-60	90				NSI	NSI
GRB2567	RAB	29	6968500	747900	500	-60	90				NSI	NSI
GRB2568	RAB	18	6968500	747850	500	-60	90				NSI	NSI
GRB2569	RAB	8	6968500	747800	500	-60	90				NSI	NSI
GRB2570	RAB	22	6968500	747750	500	-60	90				NSI	NSI
GRB2624	RAB	39	6967950	748100	500	-60	90				NSI	NSI
GRB2625	RAB	35	6967950	748050	500	-60	90				NSI	NSI
GRB2626	RAB	38	6967950	748000	500	-60	90				NSI	NSI
GRB2627	RAB	34	6967950	747950	500	-60	90				NSI	NSI

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GRB2628	RAB	20	6967975	748152	500	-60	90				NSI	NSI
GRB2629	RAB	30	6967975	748142	500	-60	90				NSI	NSI
GRB2630	RAB	46	6968050	748100	500	-60	90				NSI	NSI
GRB2631	RAB	40	6968050	748050	500	-60	90				NSI	NSI
GRB2632	RAB	39	6968050	748000	500	-60	90				NSI	NSI
GRB2633	RAB	41	6968050	747950	500	-60	90				NSI	NSI
GRB2634	RAB	30	6968200	748150	500	-60	90				NSI	NSI
GRB2635	RAB	35	6968200	748100	500	-60	90				NSI	NSI
GRB2636	RAB	46	6968200	748050	500	-60	90				NSI	NSI
GRB2637	RAB	28	6968200	748000	500	-60	90				NSI	NSI
GRB2638	RAB	39	6968200	747950	500	-60	90				NSI	NSI
GRB2639	RAB	49	6968200	747900	500	-60	90				NSI	NSI
GRB2779	RAB	37	6967800	748200	500	-60	90				NSI	NSI
GRB2780	RAB	42	6967800	748150	500	-60	90				NSI	NSI
GRB2781	RAB	16	6967800	748100	500	-60	90				NSI	NSI
GRB2782	RAB	38	6967800	748050	500	-60	90				NSI	NSI
GRB2783	RAB	38	6967800	748000	500	-60	90				NSI	NSI
GRB2784	RAB	39	6967600	748300	500	-60	90				NSI	NSI
GRB2785	RAB	27	6967600	748250	500	-60	90				NSI	NSI
GRB2786	RAB	30	6967600	748200	500	-60	90				NSI	NSI
GRB2787	RAB	50	6967600	748150	500	-60	90				NSI	NSI
GRB2788	RAB	48	6967600	748100	500	-60	90				NSI	NSI
GRC182	RC	76	6968000	748050	500	-60	90	36	44	8	0.32	0.68
GRC183	**RC**	**150**	**6967991**	**748010**	**500**	**-60**	**90**	**74**	**92**	**18**	**1.48**	**2.17**
GRC197	RC	153	6968300	748000	500	-60	90	81	92	11	0.37	4.77
GRC198	RC	183	6968300	747900	500	-60	90	126	140	14	0.38	3.61
GRC199	**RC**	**171**	**6968070**	**748000**	**500**	**-60**	**90**	**58**	**99**	**41**	**0.53**	**7.94**
GRC200	**RC**	**171**	**6968000**	**747975**	**500**	**-60**	**90**	**89**	**116**	**27**	**1.42**	NSI
GRC201	**RC**	**170**	**6967950**	**748000**	**500**	**-60**	**90**	**25**	**31**	**6**	**0.78**	NSI
GRC209	RC	162	6968100	747950	500	-90	0	72	94	22	0.7	1.13
GRC226	RC	144	6968050	748110	500	-60	90	75	80	5	0.25	4.97
GRC239	**RC**	**140**	**6968048**	**747954**	**500**	**-60**	**90**	**73**	**86**	**13**	**1.28**	NSI
GRC240	RC	115	6968045	747947	500	-90	0	15	20	5	0.21	NSI
GRC254	RC	175	6968209	747909	500	-73	90	70	100	30	0.16	2.7
GRC255	**RC**	**150**	**6967947**	**748082**	**500**	**-60**	**90**	**93**	**100**	**7**	**0.84**	NSI
GRC256	RC	178	6967803	748041	500	-90	0				NSI	NSI
GRC257	RC	115	6967900	748240	500	-60	90				NSI	NSI
GRC258	**RC**	**130**	**6967899**	**748073**	**500**	**-60**	**90**	**92**	**100**	**8**	**0.78**	**1.17**
GRC259	RC	90	6967900	748165	500	-60	90				NSI	NSI
GRC260	**RC**	**155**	**6968002**	**748041**	**500**	**-60**	**90**	**81**	**95**	**14**	**0.93**	**2.24**
GRC274	RC	118	6967949	747982	500	-90	0				NSI	NSI

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GRC276	RC	208	6968000	747874	500	-60	90				NSI	NSI
GRC277	**RC**	**208**	**6968047**	**747872**	**500**	**-60**	**90**	**69**	**81**	**12**	**0.52**	**3.53**
GRC278	RC	204	6968103	747781	500	-60	90	125	160	35	0.18	3.07
GRC279	RC	213	6968195	747752	500	-60	90	160	190	30	0.15	3.35
GRC280	**RC**	**282**	**6968000**	**747713**	**500**	**-60**	**90**	**75**	**90**	**15**	**0.62**	**2.07**
GRC281	RC	328	6968206	747589	500	-60	90	185	200	15	0.16	2.11
GRC282	RC	148	6968102	747861	500	-60	90	85	100	15	0.23	3.08
GRC283	RC	223	6967797	747883	500	-60	90	See	Below	Table		
GRC285	RC	276	6967790	747802	500	-60	90	65	70	5	0.27	1.6
GRC287	RC	173	6968184	748002	500	-60	90	75	145	70	0.21	3.06
GRC302	RC	219	6967897	747951	500	-60	90				NSI	NSI

Full details of holes at The Cup, Cu, Ni, Pt, Pd intersections (Holes Analysed for Multi-Elements):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Cu%	Ni%	Pt g/t	Pd g/t
GRC283	**RC**	**223**	**6967797**	**747883**	**500**	**-60**	**90**	**137**	**141**	**4**	**1.03**	**0.44**	**0.32**	**0.55**

Full details of holes at The Cup South, Cu and Au intersections (Holes Analysed for Multi-Elements):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Cu%	Au g/t
GRC306	RC	291	6966894	747941	500	-60	90	115	120	5	0.20	NSI
GAC037	AC	52	6966000	748800	500	-90	0				NSI	NSI
GAC038	AC	78	6966000	748750	500	-90	0				NSI	NSI
GAC211	AC	59	6966907	748200	500	-60	90				NSI	NSI
GAC212	AC	80	6966907	748220	500	-60	90				NSI	NSI
GAC213	AC	55	6966914	748150	500	-60	90				NSI	NSI
GAC214	AC	68	6966910	747940	500	-60	90				NSI	NSI
GAC243	AC	49	6965997	748500	500	-60	90				NSI	NSI
GAC244	AC	74	6966000	748400	500	-60	90				NSI	NSI
GAC245	AC	60	6965995	748520	500	-60	90				NSI	NSI
GPAC0662	AC	66	6966908	747709.08	500	-90	0				NSI	NSI
GPAC0663	AC	110	6966908	747809.07	500	-90	0	92	96	4	NSI	1.38
GPAC0664	AC	80	6966908	747909.08	500	-90	0				NSI	NSI
GPAC0665	AC	72	6966908	748009.08	500	-90	0	48	52	4	0.22	NSI
GPAC0666	AC	111	6966908	748109.07	500	-90	0	44	48	4	0.22	NSI
GPAC0667	AC	54	6966908	748209.07	500	-90	0				NSI	NSI
GRB2792	RAB	29	6966000	748800	500	-60	90				NSI	NSI
GRB2793	RAB	21	6966000	748750	500	-60	90				NSI	NSI
GRB2794	RAB	37	6966000	748700	500	-60	90				NSI	NSI

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Full details of holes at Intrepid, Cu and Au intersections (Holes Analysed for Multi-Elements):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Cu%	Aug/t
GRC295	RC	181	6965900	747376	500	-60	90				NSI	NSI
GRC301	RC	230	6965950	747480	500	-60	270				NSI	NSI
GPAC0644	AC	48	6965808	747359	500	-90	0				NSI	NSI
GPAC0645	AC	34	6965808	747459	500	-90	0				NSI	NSI
GPAC0646	AC	66	6965808	747559	500	-90	0				NSI	NSI
GPAC0647	AC	32	6965808	747659	500	-90	0				NSI	NSI
GPAC0648	AC	120	6966008	747159	500	-90	0				NSI	NSI
GPAC0649	AC	79	6966008	747259	500	-90	0				NSI	NSI
GPAC0650	AC	99	6966008	747359	500	-90	0				NSI	NSI
GPAC0651	AC	90	6966008	747459	500	-90	0				NSI	NSI
GPAC0652	AC	96	6966008	747559	500	-90	0				NSI	NSI
GPAC0653	AC	82	6966208	747159	500	-90	0				NSI	NSI
GPAC0654	AC	30	6966208	747259	500	-90	0				NSI	NSI
GPAC0655	AC	31	6966208	747284	500	-90	0	24	28	4	NSI	0.55
GPAC0656	AC	101	6966208	747359	500	-90	0				NSI	NSI
GPAC0657	AC	32	6966208	747459	500	-90	0	28	32	4	NSI	0.62

Full details of holes at Intrepid South, Cu and Au intersections (Holes Analysed for Multi-Elements):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Cu%	Au g/t
GRC300	RC	305	6965281	747507	500	-70	270				NSI	NSI
GRC307	RC	285	6965287	747522	500	-65	90				NSI	NSI
GRC308	RC	273	6964651	748354	500	-60	90				NSI	NSI
GAC219	AC	68	6965082	748000	500	-60	90				NSI	NSI
GAC220	AC	68	6965121	747900	500	-60	90				NSI	NSI
GAC221	AC	42	6965118	747879	500	-60	90				NSI	NSI
GAC222	AC	25	6965098	747600	500	-60	90				NSI	NSI
GAC223	AC	64	6965092	747580	500	-60	90				NSI	NSI
GAC224	AC	38	6965110	747200	500	-60	90				NSI	NSI
GAC247	AC	33	6964797	748320	500	-60	90				NSI	NSI
GPAC0668	AC	107	6965108	747059.07	500	-90	0	8	12	4.00	NSI	0.82
GPAC0669	AC	79	6965108	747159.08	500	-90	0	28	32	4.00	NSI	0.92
GPAC0670	AC	32	6965108	747259.08	500	-90	0				NSI	NSI
GPAC0671	AC	111	6965108	747359.07	500	-90	0				NSI	NSI
GPAC0672	AC	78	6965108	747459.08	500	-90	0				NSI	NSI
GPAC0673	AC	53	6965108	747559.08	500	-90	0				NSI	NSI
GPAC0674	AC	26	6965108	747659.07	500	-90	0				NSI	NSI

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GPAC0675	AC	81	6965108	747759.08	500	-90	0				NSI	NSI
GPAC0676	AC	60	6965108	747859.07	500	-90	0				NSI	NSI
GPAC0677	AC	21	6965108	747959.07	500	-90	0	20	21	1.00	NSI	0.74
GPAC0678	AC	72	6965108	748059.08	500	-90	0	36	40	4.00	NSI	3.22
GPAC0678	AC	72	6965108	748059.08	500	-90	0				NSI	NSI
GPAC0679	AC	79	6965108	748159.07	500	-90	0				NSI	NSI
GPAC0679	AC	79	6965108	748159.07	500	-90	0				NSI	NSI
GPAC0680	AC	119	6965108	748259.07	500	-90	0				NSI	NSI
GPAC0680	AC	119	6965108	748259.07	500	-90	0				NSI	NSI
GPAC0681	AC	75	6965108	748359.07	500	-90	0				NSI	NSI
GPAC0682	AC	57	6965108	748459.07	500	-90	0				NSI	NSI
GPAC0683	AC	96	6965108	748559.07	500	-90	0				NSI	NSI
GPAC0684	AC	53	6965108	748659.06	500	-90	0				NSI	NSI
GPAC0685	AC	40	6965108	748759.07	500	-90	0				NSI	NSI

Full details of holes at Hypotenuse/Blind Bat, Cu and Au intersections (Holes Analysed for Multi-Elements):

Hole	Type	Total Depth	North	East	RL	Dip	Azim	From	To	Width	Cu%	Au g/t
GAC014	AC	117	6970800	749400	500	-60	90				NSI	NSI
GAC015	AC	125	6970800	749300	500	-60	90				NSI	NSI
GAC016	AC	76	6970800	749200	500	-60	90				NSI	NSI
GAC017	AC	94	6970800	749100	500	-60	90				NSI	NSI
GAC018	AC	98	6970800	749600	500	-60	90				NSI	NSI
GAC019	AC	80	6970450	748900	500	-60	90				NSI	NSI
GAC020	AC	80	6970450	748850	500	-60	90				NSI	NSI
GAC021	AC	74	6970450	748800	500	-60	90				NSI	NSI
GAC022	AC	71	6970450	748750	500	-60	90				NSI	NSI
GAC023	AC	53	6970450	748700	500	-60	90				NSI	NSI
GAC068	AC	114	6971000	749050	500	-60	90				NSI	NSI
GAC069	AC	114	6971000	749000	500	-60	90				NSI	NSI
GAC070	AC	112	6971000	748950	500	-60	90				NSI	NSI
GAC071	AC	88	6971000	748900	500	-60	90				NSI	NSI
GAC072	AC	95	6971000	748850	500	-60	90				NSI	NSI
GAC074	AC	78	6970600	748700	500	-60	90				NSI	NSI
GAC075	AC	84	6970600	748650	500	-60	90				NSI	NSI
GAC076	AC	84	6970600	748600	500	-60	90				NSI	NSI
GAC163	AC	104	6970000	749297	500	-60	180				NSI	NSI
GAC164	AC	94	6970097	749294	500	-60	190				NSI	NSI
GAC165	AC	122	6970198	749317	500	-60	180				NSI	NSI
GAC166	AC	131	6970293	749296	500	-60	170				NSI	NSI

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GAC167	AC	128	6970396	749290	500	-60	185				NSI	NSI
GAC248	AC	47	6969800	748800	500	-60	180				NSI	NSI
GAC249	AC	53	6969850	748800	500	-60	180				NSI	NSI
GAC250	AC	57	6969900	748800	500	-60	180				NSI	NSI
GDD004	DD	165.5	6970800	749204	500	-60	135				NSI	NSI
GDD005	DD	393.7	6970804	749200	500	-65	135	287	289	2	NSI	1.02
GRC187	RC	150	6970300	749090	500	-60	90				NSI	NSI
GRC215	RC	156	6970000	748890	500	-60	90				NSI	NSI
GRC228	RC	166	6970800	749050	500	-60	90				NSI	NSI
GRC305	RC	231	6969955	748899	510	-60	180				NSI	NSI
PLRB10	RAB	22	6969851	748935	500	-90	0				NSI	NSI
PLRB11	RAB	14	6969852	748975	500	-90	0				NSI	NSI
PLRB12	RAB	30	6969853	749015	500	-90	0				NSI	NSI
PLRB13	RAB	29	6969853	749055	500	-90	0				NSI	NSI
PLRB14	RAB	41	6969854	749095	500	-90	0				NSI	NSI
PLRB6	RAB	24	6969849	748795	500	-90	0				NSI	NSI
PLRB7	RAB	30	6969849	748815	500	-90	0				NSI	NSI
PLRB8	RAB	33	6969850	748855	500	-90	0				NSI	NSI
PLRB9	RAB	29	6969851	748895	500	-90	0				NSI	NSI

The information in this report that relates to Exploration Results, Mineral Resources or Ore Reserves is based on information compiled by Mr Scott Jarvis, a full time employee & Head Geologist at Gateway Mining, a member of the Australian Institute of Geoscientists. Mr Scott Jarvis has a minimum of 5 years' experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the "Australian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Scott Jarvis consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

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