



# AKELIKONGO: ASSAYS CONFIRM EXTENSIVE NEAR-SURFACE NICKEL-COPPER-COBALT SYSTEM

Broadest and highest grade intercepts returned to date with results providing a clear vector to target potential high-grade massive sulphide positions

### **Highlights:**

- New assay results received for the first four RC holes from the recently completed highly successful drilling program at the **Akelikongo nickel-copper prospect** in Uganda.
- The results include the highest grade and widest matrix to semi-massive intercepts drilled at the project to date, including a significant semi-massive sulphide intercept of:
  - 10m grading 1% Ni, 0.22% Cu, and 0.05% Co from 63m down-hole in AKD004
- The results also contain the widest disseminated intercepts obtained to date, ranging from 59m to 119m down-hole at grades of >0.3% Ni, >0.1% Cu and 0.02% Co. Results include:
  - 113m @ 0.36% Ni, 0.1% Cu, and 0.02% Co from 2m down-hole including 1m at 1.03% Ni, 0.09% Cu and 0.05% Co (AKC003);
  - 69m @ 0.43% Ni, 0.20% Cu and 0.02% Co from 4m down-hole including 10m @ 1% Ni, 0.22% Cu and 0.05% Co (AKC004);
  - 119m @ 0.40% Ni, 0.12% Cu and 0.02% Co from surface including 1m at 1.17% Ni, 0.39% Cu and 0.05% Co (AKC005);
  - 59m at 0.35% Ni, 0.22% Cu, and 0.02% Co from 24m down-hole including 4m @ 1.8% Cu, 0.5% Ni, and 0.03% Co (AKC006)
- Cobalt, at 2-3 times the current price of nickel, is now identified as an important metal in the system with assays commonly averaging over 0.02% Co and up to 0.05% Co in higher grade zones.
- The drilling has identified an embayment in the footwall which explains the larger volumes of shallow mineralisation and provides a vector for follow-up drilling targeting a basal high-grade massive sulphide position. This potential will be tested by follow-up drilling.
- At the nearby Pamwa zinc-lead-silver prospect, 10km to the south, assay results indicate broad zones averaging >25m of strongly anomalous zinc, lead (>1000ppm combined) plus silver and cadmium, with thinner higher grade zones 1-7m wide of up to 3.9% combined Pb plus Zn and up to 20 g/t Ag providing further evidence of a primary zinc-lead-silver system.
- Remaining assay results from the recent program expected within the next 2-3 weeks.



Sipa Resources Limited (ASX: SRI) is pleased to advise that it has received encouraging assay results from the recently completed drilling programs at the **Akelikongo nickel-copper prospect** and **Pamwa zinc-lead-silver prospect**, both of which form part of its Kitgum-Pader Base Metal Project in Uganda (Figure 1).

The results from the first four Reverse Circulation (RC) drill-holes the Akelikongo prospect include the highest grade and widest matrix to semi-massive intercepts drilled at the project to date, providing further clear evidence that Akelikongo hosts an extensive near-surface nickel-copper-cobalt system.

The results have further enhanced the Company's understanding of the emerging magmatic nickel-copper sulphide mineralised system at Akelikongo, providing some important insights into the structural controls and distribution of metal within the system – as well as providing vectors to potential accumulations of high-grade massive sulphides.

"The recently completed 12-hole RC program has allowed us to make some important advances in our understanding of the scale, structure and potential of the emerging Akelikongo prospect," said Sipa Resources Managing Director, Lynda Burnett.

"Results have so far been received for the first four holes, which have returned some of the most significant broad intercepts of disseminated mineralization we have seen to date, including narrower basal zones of matrix-to-semi-massive sulphides grading above 1 per cent nickel or 1 per cent copper.

"These higher grade zones are interpreted to represent the high-grade basal position of the Akelikongo Ultramafic Complex, and lie at the footwall of the wide and shallow zones of disseminated sulphides. This basal position is typically where massive sulphides form in large nickel-copper systems and represents a priority focus for ongoing drilling.

"Given the scale of the system and the width and grade of the disseminated sulphide intercepts, we are hopeful that we are now getting much closer to finding the high-grade core of the system and discovering an accumulation of high-grade massive nickel sulphides.

"All of the indicators so far suggest that we are on the right track, and we look forward to receiving the balance of results from the recent program over the coming weeks and planning the next stage of exploration and drilling."

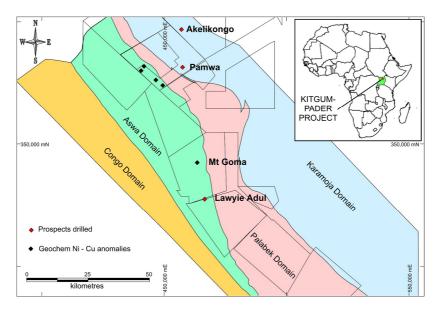


Figure 1. Project Location Map



# Akelikongo

The RC drill program was designed to test the shallow sparsely drilled area between AKD002 and AKD004 (Figure 2) where the Akelikongo Ultramafic Complex (AKUC) comes to surface and is represented by a strong in situ soil anomaly greater than 0.3% Ni and >500ppm Cu.

12 RC drill holes for 1007m were drilled with holes intersecting strong disseminated to blebby nickel and copper sulphides with a basal zone of matrix to semi massive sulphides (see Table 1 below). Results for the first four holes, AKC003 to AKC006, are presented here.

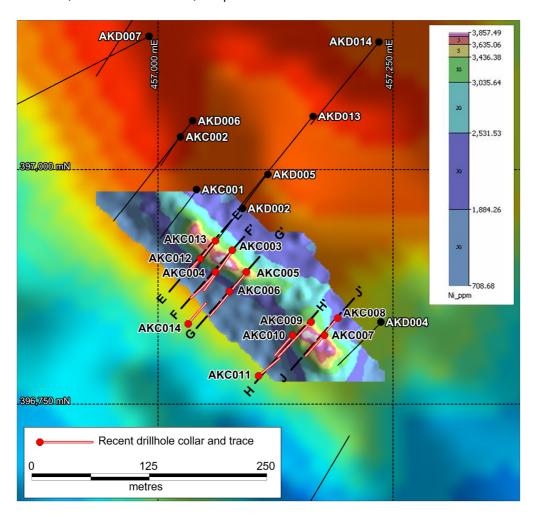


Figure 2. 5m by 5m in-fill soils over Akelikongo gravity image with existing drilling. New RC drill hole locations are shown in red and section lines shown as F-F' and G-G' shown as Figures 2 and 3

Table 1 – RC Drill holes location orientation and depth											
Hole ID	Easting	Northing	Elevation	Azimuth	Dip	Depth					
AKC003	AKC003 457079 396914 946 215 -60 12										
AKC004	457061	396891	946	220	-60	85					
AKC005	457094	396891	947	220	-60	122					



	Table 1 – RC Drill holes location orientation and depth											
Hole ID	Easting	Northing	Elevation	Azimuth	Dip	Depth						
AKC006	457076	396870	947	220	-60	88						
AKC007	457177	396823	948	220	-60	66						
AKC008	457191	396841	949	220	-60	89						
AKC009	457163	396837	949	220	-60	99						
AKC010	457143	396823	949	220	-60	58						
AKC011	457107	396780	949	45	-60	62						
AKC012	457045	396905	946	220	-60	54						
AKC013	457061	396924	946	220	-60	97						
AKC014	457032	396835	946	40	-60	60						

The matrix to semi-massive zones contain assays greater than 1% Ni or 1% Cu and range from 1m up to 10m wide. These zones are interpreted to represent the high grade basal position in the Akelikongo Ultramafic Complex and lie at the footwall of the wide and shallow zones of disseminated sulphides.

This basal position, in other better understood nickel deposits, is where massive sulphides, which have higher grades of nickel and copper, originally pooled during the initial formation of the deposit. Figures 3 and 4 show the geology of section lines F-F' and G-G' as shown on the plan on Figure 2.

Results from the first 4 holes are summarised as follows:

•	AKC003	113m @ 0.36% Ni, 0.11% Cu and 0.02% Co from 2m to 115m including 1m of semi-massive sulphide @ 1.03% Ni, 0.09% Cu and 0.05% Co from 114m to 115m
•	AKC004	69m @0.43% Ni, 0.20% Cu and 0.02% Co from 4m to 73m including 10m of semi-massive sulphide @ 1% Ni, 0.22% Cu and 0.05% Co from $63m$ to $73m$
•	AKC005	119m @0.40% Ni, 0.12% Cu and 0.02% Co from 0m to 119m including 1m of semi-massive sulphide @ 1.17% Ni 0.39% Cu and 0.05% Co from 118m to 119m
•	AKC006	59m at 0.35% Ni, 0.22% Cu 0.02% Co from 24m to 83m including 4m of semi-massive sulphide @ 0.50% Ni, 1.8% Cu and 0.03% Co from 79m to 83m

The discovery, during this drill program, of an embayment in the footwall, plus the knowledge of the existence of higher and thicker grades within the embayment now provides a clear focus for future drilling of this mineralised position along the shallow north westerly plunge of the chonolith.

Previous drilling and 3D modelling has indicated the chonolith is present over 1km of strike and plunges shallowly to the northwest, with only the top 250m of the strongly mineralised position tested at wide spacings.

The final batch of assay results are expected in the next two weeks. Complete results are included in Table 4.



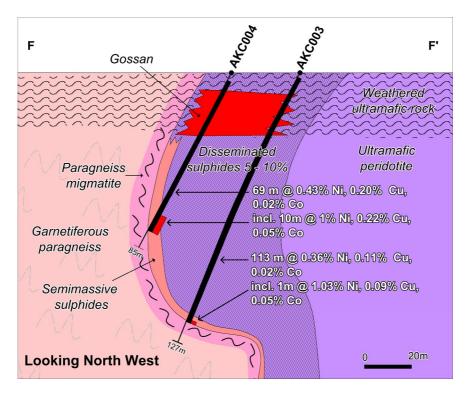


Figure 3 Drill hole section F-F' showing AKC003 and AKC004

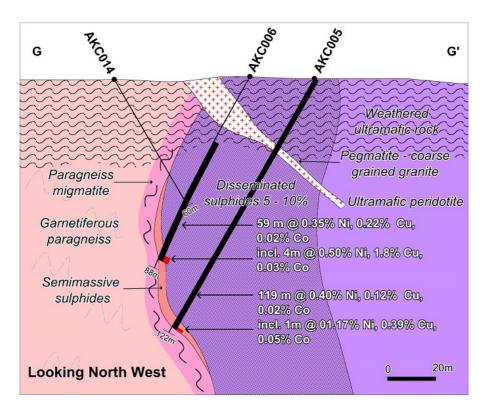


Figure 4 Drill hole section G-G' showing AKC014, AKC006 and AKC005 (Assays pending on AKC014)





Figure 5 Sieved chips from drill hole AKC006 79-80m showing coarse chalcopyrite with pyrrhotite and pentlandite assaying 4.6% Cu 0.58% Ni 0.04% Co

#### **Pamwa**

At the Pamwa base metal prospect, located 10km south of Akelikongo, drilling has previously intersected primary sphalerite and galena in lithostratigraphic horizons within a large >2km elongate Zn, Pb Ag, Cd, Mn soil anomaly.

A total of 22 aircore holes for 534m and 3 RC holes for 202m were drilled during April 2016 (see Table 2 and 3, Figures 6 and 7).

The program consisted of shallow RAB and RC drilling of many highly anomalous soil peaks >500ppm Zn + Pb. The assay results indicate broad zones >25m of strongly anomalous zinc plus lead (>1000ppm), silver and cadmium, with thinner higher grade zones 1-7m wide of up to 3.9% combined Pb plus Zn and up to 20 g/t Ag.

The mineralised zones generally occur around a stratigraphic contact in biotite hornblende gneiss beneath a garnet gneiss see Figure 8. As described previously, the soil anomaly is thought to represent a folded or thrust repeated horizon and the drilling confirms this view. It is thought that the eastern limb dips shallowly to the east whilst the western limb is overturned and dips more steeply to the east. The wider and better grade zinc, lead and silver intersections are located on the eastern limb.

Table 5 shows a collation of intercepts generally greater than 0.5% combined Pb plus Zn. Figure 9 is a plot showing all Pamwa assays and the strong correlation between Pb and Zn indicating a primary mineralised system.



Table 2 – Pamwa Aircore drill-holes location, orientation and depth											
Hole ID	Easting	Northing	Elevation	Azimuth	Dip	Depth					
PAA001	457514	381404	949	240	-60	39					
PAA002	457498	381398	949	240	-60	18					
PAA003	457499	381419	949	240	-60	18					
PAA004	457488	381410	949	240	-60	20					
PAA005	457515	381380	949	240	-60	19					
PAA006	457506	381377	949	240	-60	22					
PAA007	457511	381424	949	240	-60	22					
PAA008	457480	381406	949	240	-60	15					
PAA009	457596	381285	953	240	-60	27					
PAA010	457583	381279	953	240	-60	24					
PAA011	457475	381159	953	240	-60	26					
PAA012	457463	381153	953	240	-60	27					
PAA013	457307	381488	949	240	-60	26					
PAA014	457291	381482	949	240	-60	28					
PAA015	457676	381000	957	240	-60	22					
PAA016	457640	380994	957	0	-90	20					
PAA017	457605	380993	957	240	-60	22					
PAA018	457591	380984	957	235	-60	23					
PAA019	457325	381745	942	240	-60	26					
PAA020	457311	381741	943	240	-60	23					
PAA021	457358	381714	944	240	-60	31					
PAA022	457348	381702	944	240	-50	36					

Table 3 Pamwa RC drill hole location, orientation and depth											
Hole ID	Easting	Northing	Elevation	Azimuth	Dip	Depth					
PAC001	PAC001 457517 381444 949 240 -60 55										
PAC002	PAC002 457537 381379 949 240 -60 47										
PAC003	457540.2	381466.6	949	240	-60	100					

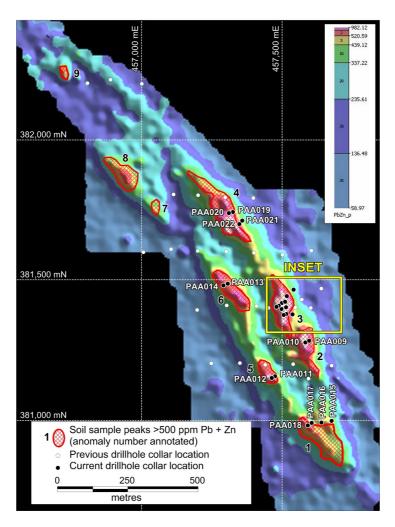


Figure 6 Pb plus Zn in soils with strong anomalies labelled with drill hole locations.

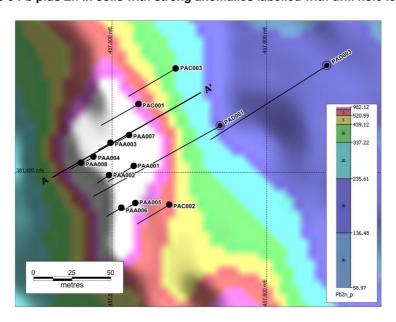


Figure 7 Plan inset, showing section line A-A'



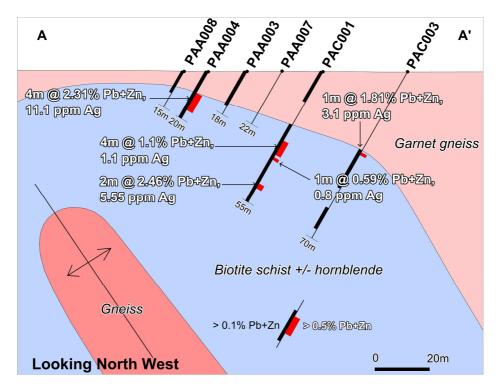


Figure 8 Section A-A'

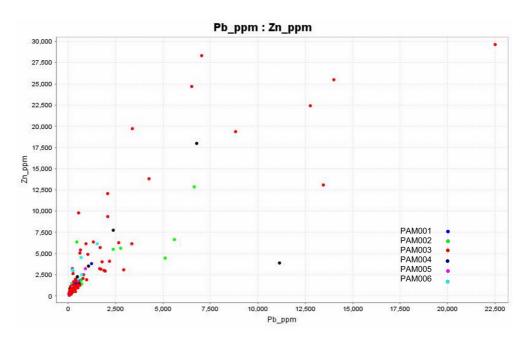


Figure 9 Plot of all drill hole assays Pb vs Zn. Points coloured by prospect number.

Figure 9 above shows an XY plot of all assays for the current Pamwa drill program. It clearly shows all samples are anomalous and are located within the mineralised system with a strong correlation between Pb and Zn at all levels of anomalism. The best mineralised results come from soil anomaly PAM003.



Gradient Array IP data collected in December 2014 shows a strong chargeability zone correlating with the eastern and western fold limbs and extending further to the south east than the geochemistry and drilling. Strong >60ms Pole-Dipole chargeability anomalies were also detected on two sections across this area however, the diamond drill holes drilled in 2015 did not satisfactorily explain these anomalies.

This current drilling program has assisted with the further understanding of the controls of the mineralisation. More drilling is likely if further geophysics can assist with targeting with this extensive mineral system. The existence of a pyrite halo to the mineralisation indicates further IP lines would be beneficial. It's also planned to conduct further gravity data here and at Akelikongo which will also assist targeting. These surveys would be conducted later in the second half of the year once the wet season is over.

## **Forward Plan**

Further drilling at Akelikongo and Pamwa is planned following receipt of the remainder of the results and pending access due to deteriorating wet season road conditions.

In the meantime, plans are well advanced to commence our exploration program at Paterson North where a strong copper anomaly will be tested. A WA Government Exploration Incentive Scheme co-funding drilling application has been submitted to support this program.

The information in this report that relates to Exploration Results is based on, and fairly represents, information and supporting documentation compiled by Ms Lynda Burnett, who is a Member of The Australasian Institute of Mining and Metallurgy. Ms Burnett is a full-time employee of Sipa Resources Limited. Ms Burnett has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which she is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Ms Burnett consents to the inclusion in this report of the matters based on his information in the form and context in which it appears.

#### For more information:

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## **Background**

Sipa Resources Limited has a track record of successful project generation and mineral discovery with the Western Australian Panorama base metal deposits, Mt Olympus gold deposits and the Enigma secondary copper system at Thaduna northwest of Sandfire's DeGrussa Copper Mine, among some of the mineral systems discovered or delineated by Sipa.

In Northern Uganda, the Kitgum-Pader Base Metals Project contains two new mineral discoveries both made by Sipa during 2014 and 2015.

The intrusive hosted Nickel-Copper sulphide mineralisation at Akelikongo is one of the most significant nickel sulphide discoveries globally for 2015.

The Broken Hill-style Lead-Zinc-Silver mineralisation, at Pamwa is less well defined and currently the focus of further drilling.

The Ugandan discoveries were made following the acquisition in 2011 of relatively new airborne magnetic/radiometric data sets over East Africa, and the subsequent geological/metallogenic interpretation of the data sets.

Field reconnaissance in December 2011 followed, with the recognition of rocks which according to the late Nick Archibald were strikingly similar to the host 'Mine Series' sequence at the giant Broken Hill Lead-Zinc-Silver Deposit in NSW, Australia, to the northwest of Kitgum in Northern Uganda.

First tenements were granted in 2012 and since that time, the company has collected over 60,000 soil samples, along with geological mapping by the late Nick Archibald, Brett Davies and Russell Mason and numerous geophysical surveys to define a number of base metal prospects. Diamond drilling in 2015 at Akelikongo has delineated an intrusive hosted chonolith Nickel Copper sulphide system which is outcropping and plunges shallowly to the north west for a distance of at least 500m and open to the north west. At Pamwa a number of identified soil anomalies have been drilled with primary Zinc Lead Silver Cadmium mineralisation intersected in both RC aircore and diamond drilling.

In March 2016 in Australia, Sipa farmed into Ming Gold's Paterson North project where extensive copper anomalism was intersected at the Obelisk prospect in primary bedrock adjacent to Rio/Antipa's Magnum and Citadel plus 1 million ounce Gold/Copper project.



TABLE 4 AKELIKONGO DRILLHOLE RESULTS AKC004 TO AKC006											
HOLE	FROM	ТО	WIDTH	Cu %	Ni %	Co %	Mg %	S %*			
AKC003	0	2	2	0.076	0.247	0.020	1.62	0.03			
AKC003	2	4	2	0.083	0.310	0.020	4.67	0.01			
AKC003	4	6	2	0.108	0.381	0.022	5.97	0.01			
AKC003	6	8	2	0.054	0.225	0.015	5.91	0.01			
AKC003	8	10	2	0.103	0.375	0.023	6.78	0.01			
AKC003	10	12	2	0.132	0.533	0.032	7.25	0.01			
AKC003	12	14	2	0.122	0.409	0.026	6.96	0.01			
AKC003	14	16	2	0.125	0.438	0.029	7.78	0.01			
AKC003	16	18	2	0.194	0.472	0.028	8.63	0.02			
AKC003	18	20	2	0.094	0.320	0.021	8.41	0.01			
AKC003	20	22	2	0.080	0.268	0.018	9.43	0.02			
AKC003	22	24	2	0.109	0.342	0.021	10.55	0.01			
AKC003	24	26	2	0.117	0.372	0.022	12.05	0.01			
AKC003	26	28	2	0.110	0.331	0.021	10.70	0.01			
AKC003	28	30	2	0.102	0.355	0.023	14.35	0.08			
AKC003	30	32	2	0.111	0.368	0.024	16.20	0.53			
AKC003	32	34	2	0.106	0.354	0.023	16.70	1.01			
AKC003	34	36	2	0.109	0.341	0.023	16.05	1.31			
AKC003	36	38	2	0.103	0.376	0.024	17.80	2.42			
AKC003	38	40	2	0.097	0.352	0.024	17.90	2.44			
AKC003	40	42	2	0.088	0.318	0.022	17.65	2.02			
AKC003	42	44	2	0.069	0.317	0.020	13.75	2.05			
AKC003	44	46	2	0.074	0.565	0.033	12.45	4.79			
AKC003	46	48	2	0.116	0.325	0.021	13.80	2.54			
AKC003	48	50	2	0.143	0.288	0.019	15.25	2.02			
AKC003	50	52	2	0.080	0.298	0.020	17.50	1.89			
AKC003	52	54	2	0.093	0.336	0.022	17.65	2.13			
AKC003	54	56	2	0.091	0.318	0.021	17.55	2.07			
AKC003	56	58	2	0.122	0.366	0.023	18.25	2.40			
AKC003	58	60	2	0.108	0.458	0.027	18.75	2.80			
AKC003	60	62	2	0.111	0.422	0.026	19.05	2.67			
AKC003	62	64	2	0.100	0.341	0.021	15.35	2.12			
AKC003	64	66	2	0.106	0.396	0.025	19.25	2.47			
AKC003	66	68	2	0.090	0.295	0.019	15.45	1.85			
AKC003	68	70	2	0.031	0.107	0.009	8.56	0.74			
AKC003	70	72	2	0.098	0.405	0.026	17.40	2.80			
AKC003	72	74	2	0.155	0.319	0.022	17.40	2.27			
AKC003	74	76	2	0.441	0.384	0.026	17.40	3.07			



TABLE 4 AKELIKONGO DRILLHOLE RESULTS AKC004 TO AKC006											
HOLE	FROM	TO	WIDTH	Cu %	Ni %	Co %	Mg %	S %*			
AKC003	76	78	2	0.020	0.045	0.006	6.14	0.36			
AKC003	78	80	2	0.091	0.438	0.028	18.65	3.49			
AKC003	80	82	2	0.097	0.367	0.024	19.05	2.62			
AKC003	82	84	2	0.084	0.361	0.024	18.15	2.59			
AKC003	84	86	2	0.107	0.381	0.026	18.55	2.91			
AKC003	86	88	2	0.098	0.341	0.024	17.75	2.58			
AKC003	88	90	2	0.082	0.302	0.021	15.25	2.20			
AKC003	90	92	2	0.096	0.336	0.023	17.90	2.53			
AKC003	92	94	2	0.091	0.324	0.023	19.20	2.29			
AKC003	94	96	2	0.103	0.341	0.024	18.00	2.39			
AKC003	96	98	2	0.108	0.355	0.024	16.65	2.54			
AKC003	98	100	2	0.120	0.359	0.023	16.80	2.40			
AKC003	100	102	2	0.116	0.363	0.025	16.50	2.84			
AKC003	102	104	2	0.076	0.249	0.019	16.60	1.71			
AKC003	104	106	2	0.096	0.346	0.022	16.65	2.29			
AKC003	106	108	2	0.096	0.384	0.024	15.35	3.03			
AKC003	108	110	2	0.100	0.355	0.021	14.90	2.75			
AKC003	110	112	2	0.097	0.374	0.022	13.45	3.05			
AKC003	112	114	2	0.064	0.456	0.027	9.83	3.31			
AKC003	114	115	1	0.088	1.030	0.054	4.57	8.17			
AKC003	115	117	2	0.043	0.047	0.005	2.97	1.69			
AKC003	117	119	2	0.060	0.055	0.005	3.05	1.55			
AKC003	119	121	2	0.061	0.048	0.004	2.84	1.22			
AKC003	121	123	2	0.100	0.310	0.017	2.41	3.05			
AKC003	123	125	2	0.034	0.040	0.004	2.85	0.90			
AKC003	125	127	2	0.024	0.010	0.002	2.14	0.97			
AKC004	0	2	2	0.157	0.182	0.014	0.34	0.18			
AKC004	2	4	2	0.118	0.192	0.013	0.30	0.10			
AKC004	4	6	2	0.198	0.428	0.023	0.79	0.18			
AKC004	6	8	2	0.121	0.184	0.015	0.46	0.52			
AKC004	8	10	2	0.195	0.258	0.020	0.95	0.50			
AKC004	10	12	2	0.241	0.308	0.018	1.03	1.09			
AKC004	12	14	2	0.166	0.331	0.025	1.73	0.79			
AKC004	14	16	2	0.225	0.401	0.027	1.21	0.90			
AKC004	16	17	1	0.306	0.835	0.038	0.93	0.20			
AKC004	17	19	2	0.257	0.489	0.026	0.49	1.08			
AKC004	19	21	2	0.222	0.216	0.012	1.17	1.97			
AKC004	21	23	2	0.268	0.267	0.017	3.91	1.06			
AKC004	23	25	2	0.242	0.134	0.010	10.00	0.49			



TABLE 4 AKELIKONGO DRILLHOLE RESULTS AKC004 TO AKC006											
HOLE	FROM	ТО	WIDTH	Cu %	Ni %	Co %	Mg %	S %*			
AKC004	25	27	2	0.398	0.279	0.014	8.86	0.25			
AKC004	27	29	2	0.601	0.310	0.015	9.38	0.15			
AKC004	29	31	2	0.518	0.270	0.015	8.07	0.58			
AKC004	31	33	2	0.238	0.342	0.021	9.21	2.50			
AKC004	33	35	2	0.146	0.473	0.028	12.85	4.20			
AKC004	35	37	2	0.307	0.484	0.030	13.05	4.21			
AKC004	37	39	2	0.109	0.470	0.029	14.80	4.48			
AKC004	39	41	2	0.137	0.369	0.024	14.25	3.03			
AKC004	41	43	2	0.100	0.385	0.025	13.75	3.32			
AKC004	43	45	2	0.096	0.351	0.023	14.95	2.97			
AKC004	45	47	2	0.085	0.374	0.024	14.15	3.29			
AKC004	47	49	2	0.040	0.089	0.006	3.47	0.86			
AKC004	49	51	2	0.143	0.293	0.021	14.65	2.81			
AKC004	51	53	2	0.094	0.302	0.022	15.25	2.60			
AKC004	53	55	2	0.093	0.322	0.022	15.30	3.09			
AKC004	55	57	2	0.095	0.315	0.023	15.45	2.81			
AKC004	57	59	2	0.082	0.264	0.021	15.90	2.44			
AKC004	59	61	2	0.078	0.258	0.021	15.30	2.17			
AKC004	61	63	2	0.099	0.372	0.024	10.00	3.50			
AKC004	63	64	1	0.224	0.748	0.043	5.85	5.75			
AKC004	64	65	1	0.100	0.257	0.018	13.50	2.31			
AKC004	65	66	1	0.156	0.434	0.027	9.88	3.97			
AKC004	66	67	1	0.183	1.200	0.063	3.17	9.85			
AKC004	67	68	1	0.282	1.765	0.093	3.15	15.05			
AKC004	68	69	1	0.238	1.170	0.062	2.46	8.79			
AKC004	69	70	1	0.267	1.460	0.079	1.81	12.05			
AKC004	70	71	1	0.192	0.195	0.012	1.90	2.03			
AKC004	71	72	1	0.278	1.770	0.093	3.10	14.95			
AKC004	72	73	1	0.271	0.936	0.052	2.58	7.79			
AKC004	73	74	1	0.158	0.108	0.007	1.19	1.57			
AKC004	74	76	2	0.038	0.034	0.003	2.12	1.26			
AKC004	76	78	2	0.021	0.019	0.003	2.75	1.23			
AKC004	78	80	2	0.011	0.008	0.003	2.14	1.20			
AKC004	80	82	2	0.014	0.009	0.004	3.22	1.23			
AKC004	82	85	3	0.008	0.007	0.003	2.42	1.14			
AKC005	0	2	2	0.145	0.453	0.027	2.55	0.04			
AKC005	2	4	2	0.166	0.539	0.031	3.23	0.03			
AKC005	4	6	2	0.158	0.626	0.041	3.97	0.28			
AKC005	6	7	1	0.227	1.170	0.081	7.26	0.02			



TABLE 4 AKELIKONGO DRILLHOLE RESULTS AKC004 TO AKC006											
HOLE	FROM	ТО	WIDTH	Cu %	Ni %	Co %	Mg %	S %*			
AKC005	7	8	1	0.348	1.100	0.052	8.51	0.14			
AKC005	8	10	2	0.203	0.252	0.011	2.69	0.06			
AKC005	10	12	2	0.052	0.107	0.005	1.43	0.01			
AKC005	12	14	2	0.105	0.462	0.029	6.93	0.01			
AKC005	14	16	2	0.095	0.481	0.028	7.46	0.01			
AKC005	16	18	2	0.091	0.467	0.028	8.54	0.01			
AKC005	18	20	2	0.223	0.406	0.023	10.40	0.01			
AKC005	20	21	1	0.103	0.505	0.029	11.05	0.01			
AKC005	21	22	1	0.094	0.852	0.041	8.38	0.01			
AKC005	22	23	1	0.118	1.110	0.053	9.71	0.01			
AKC005	23	25	2	0.114	0.495	0.028	9.84	0.02			
AKC005	25	27	2	0.099	0.424	0.024	12.45	0.01			
AKC005	27	29	2	0.100	0.386	0.023	13.30	0.01			
AKC005	29	31	2	0.097	0.457	0.026	13.45	0.03			
AKC005	31	33	2	0.177	0.308	0.013	3.38	0.37			
AKC005	33	35	2	0.131	0.240	0.011	2.14	0.81			
AKC005	35	37	2	0.100	0.379	0.022	15.90	1.56			
AKC005	37	39	2	0.106	0.349	0.022	17.55	2.36			
AKC005	39	41	2	0.084	0.364	0.023	17.75	2.09			
AKC005	41	43	2	0.068	0.267	0.018	14.45	1.69			
AKC005	43	45	2	0.142	0.443	0.025	8.40	3.30			
AKC005	45	47	2	0.090	0.326	0.022	18.25	2.27			
AKC005	47	49	2	0.100	0.359	0.023	18.60	2.37			
AKC005	49	51	2	0.074	0.328	0.022	18.40	2.23			
AKC005	51	53	2	0.094	0.337	0.022	18.15	2.13			
AKC005	53	55	2	0.157	0.323	0.021	18.25	2.27			
AKC005	55	57	2	0.117	0.382	0.023	18.25	2.44			
AKC005	57	59	2	0.070	0.290	0.020	18.95	1.79			
AKC005	59	61	2	0.106	0.290	0.020	19.20	1.85			
AKC005	61	63	2	0.068	0.249	0.018	18.45	1.57			
AKC005	63	65	2	0.045	0.189	0.016	19.70	1.06			
AKC005	65	67	2	0.047	0.203	0.017	19.50	1.16			
AKC005	67	69	2	0.077	0.314	0.021	19.90	1.79			
AKC005	69	71	2	0.272	0.376	0.024	18.50	2.79			
AKC005	71	73	2	0.085	0.363	0.023	18.25	2.19			
AKC005	73	75	2	0.091	0.307	0.021	16.95	2.02			
AKC005	75	77	2	0.169	0.318	0.020	16.35	1.92			
AKC005	77	79	2	0.102	0.277	0.019	15.50	1.99			
AKC005	79	81	2	0.103	0.387	0.024	17.55	2.69			



AKC005 81 83 2 0.165 0.446 0.028 16.95 3.4 AKC005 83 85 2 0.137 0.476 0.030 17.10 3.5 AKC005 85 87 2 0.124 0.473 0.030 18.15 3.6 AKC005 87 89 2 0.105 0.368 0.025 18.15 2.7 AKC005 89 91 2 0.110 0.346 0.023 17.75 2.5 AKC005 91 93 2 0.095 0.313 0.022 17.30 2.5 AKC005 95 97 2 0.089 0.313 0.022 17.35 1.9 AKC005 95 97 2 0.089 0.313 0.022 17.15 1.9 AKC005 99 101 2 0.116 0.389 0.025 17.20 2.4 AKC005 99 101 2 0.117 0.393 0.023 16.75 2.6 AKC005 99 101 2 0.117 0.393 0.023 16.75 2.6 AKC005 103 105 2 0.127 0.433 0.026 17.00 3.1 AKC005 103 105 2 0.127 0.433 0.026 17.00 3.1 AKC005 107 109 2 0.077 0.294 0.019 12.35 2.3 AKC005 107 109 2 0.077 0.294 0.019 12.35 2.3 AKC005 111 113 2 0.123 0.411 0.024 15.00 3.0 AKC005 115 117 2 0.123 0.443 0.025 14.35 3.6 AKC005 116 117 2 0.129 0.443 0.025 14.35 3.6 AKC005 117 118 1 0.389 1.170 0.056 2.07 8.1 AKC005 117 118 1 0.389 1.170 0.056 2.07 8.1 AKC005 118 119 1 0.389 1.170 0.056 2.07 8.1 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC006 0 2 2 0.060 0.145 0.012 0.71 0.1 AKC006 1 8 2 0.077 0.182 0.009 0.84 0.7 AKC006 1 18 119 1 0.389 1.170 0.056 2.07 8.1 AKC006 1 18 2 0.077 0.182 0.009 0.84 0.7 AKC006 1 18 119 1 0.389 1.170 0.056 2.07 8.1 AKC006 1 18 119 1 0.389 1.170 0.056 2.07 8.1 AKC006 1 18 2 0.071 0.167 0.006 0.89 0.4 AKC006 1 18 2 0.071 0.167 0.006 0.89 0.4 AKC006 1 18 2 0.072 0.194 0.009 0.84 0.7 AKC006 1 18 2 0.072 0.194 0.009 0.84 0.7 AKC006 1 18 2 0.072 0.194 0.009 0.82 0.6 AKC006 1 18 2 0.072 0.194 0.009 0.82 0.6 AKC006 1 18 2 0.071 0.167 0.006 0.89 0.4 AKC006 1 18 2 0.013 0.014 0.019 0.016 0.83 0.5 AKC006 2 2 2 0.047 0.182 0.010 0.95 0.5 AKC006 2 2 2 0.047 0.182 0.010 0.95 0.5 AKC006 2 2 2 0.047 0.181 0.017 1.66 0.6 AKC006 2 2 2 0.047 0.181 0.017 1.66 0.6 AKC006 2 2 2 0.047 0.181 0.017 1.66 0.6 AKC006 2 2 2 0.047 0.181 0.017 1.66 0.6 AKC006 2 2 2 0.047 0.043 0.027 9.06 0.1 AKC006 2 2 2 0.047 0.096 0.004 0.026 10.75 0.2	TABLE 4 AKELIKONGO DRILLHOLE RESULTS AKC004 TO AKC006											
AKC005 83 85 2 0.137 0.476 0.030 17.10 3.5 AKC005 85 87 2 0.124 0.473 0.030 18.15 3.6 AKC005 87 89 2 0.105 0.368 0.025 18.15 2.7 AKC005 89 91 2 0.110 0.346 0.023 17.75 2.5 AKC005 91 93 2 0.095 0.313 0.022 17.30 2.2 AKC005 93 95 2 0.096 0.258 0.018 9.63 AKC005 95 97 2 0.089 0.313 0.022 17.15 1.9 AKC005 97 99 2 0.116 0.389 0.025 17.20 2.4 AKC005 99 101 2 0.113 0.394 0.025 17.30 2.8 AKC005 101 103 2 0.117 0.393 0.023 16.75 2.6 AKC005 103 105 2 0.127 0.433 0.022 17.30 2.8 AKC005 105 107 2 0.122 0.433 0.027 16.15 3.2 AKC005 107 109 2 0.077 0.294 0.019 12.35 2.3 AKC005 109 111 2 0.123 0.411 0.024 15.00 3.0 AKC005 113 115 2 0.123 0.411 0.024 15.00 3.0 AKC005 115 117 2 0.174 0.571 0.032 12.75 4.6 AKC005 118 119 1 0.389 1.170 0.056 2.07 8.1 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC006 1 19 12 2 0.007 0.116 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.116 0.009 0.84 0.7 AKC006 1 19 12 2 0.009 0.009 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.116 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.116 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.116 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.116 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.116 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.116 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.116 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.119 0.009 0.84 0.7 AKC006 1 19 12 2 0.007 0.119 0.009 0.84 0.7 AKC006 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	HOLE	FROM	TO	WIDTH	Cu %	Ni %	Co %	Mg %	S %*			
AKC005 85 87 89 2 0.124 0.473 0.030 18.15 3.6 AKC005 87 89 2 0.105 0.368 0.025 18.15 2.7 AKC005 89 91 2 0.110 0.346 0.023 17.75 2.5 AKC005 91 93 2 0.095 0.313 0.022 17.30 2.2 AKC005 93 95 2 0.096 0.258 0.018 9.63 1.7 AKC005 95 97 2 0.089 0.313 0.022 17.15 1.9 AKC005 97 99 2 0.116 0.389 0.025 17.15 1.9 AKC005 99 101 2 0.113 0.394 0.025 17.30 2.8 AKC005 99 101 2 0.113 0.394 0.025 17.30 2.8 AKC005 101 103 2 0.117 0.393 0.023 16.75 2.6 AKC005 103 105 2 0.127 0.433 0.026 17.00 3.1 AKC005 107 109 2 0.077 0.294 0.019 12.35 2.3 AKC005 109 111 2 0.097 0.340 0.020 13.05 2.4 AKC005 109 111 2 0.097 0.340 0.020 13.05 2.4 AKC005 113 115 2 0.123 0.411 0.024 15.00 3.0 AKC005 113 115 2 0.129 0.443 0.025 14.35 3.6 AKC005 117 118 1 0.367 0.636 0.035 3.46 5.1 AKC005 118 119 1 0.389 1.170 0.056 2.07 8.1 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 11 1 18 1 0.367 0.636 0.035 3.46 5.1 AKC005 11 1 12 0.097 0.116 0.008 0.41 0.0 AKC006 1 1 1 1 1 1 0.389 0.117 0.096 0.44 0.009 0.84 0.7 AKC006 1 1 1 1 1 1 0.389 0.117 0.006 0.89 0.4 AKC006 1 1 1 1 1 1 0.389 0.117 0.006 0.89 0.4 AKC006 1 1 1 1 1 1 0.367 0.116 0.008 0.41 0.0 AKC006 1 1 1 1 1 1 0.389 0.117 0.006 0.89 0.4 AKC006 1 1 1 1 1 1 0.389 0.117 0.006 0.89 0.4 AKC006 1 1 1 1 1 1 0.006 0.009 1.08 1.0 AKC006 1 1 1 1 1 1 1 0.007 0.116 0.008 0.41 0.0 AKC006 1 1 1 0.009 0.21 0.016 0.83 0.5 AKC006 1 1 1 0.009 0.22 0.057 0.149 0.009 0.84 0.7 AKC006 1 1 1 0.009 0.21 0.016 0.83 0.5 AKC006 1 1 1 0.009 0.22 0.057 0.149 0.009 0.84 0.7 AKC006 1 1 1 0.009 0.22 0.057 0.149 0.009 0.84 0.7 AKC006 1 1 1 0.008 0.41 0.009 0.84 0.7 AKC006 1 1 1 0.009 0.22 0.057 0.149 0.009 0.84 0.7 AKC006 1 1 1 0.009 0.22 0.057 0.149 0.009 0.84 0.7 AKC006 2 2 2 0.057 0.149 0.009 0.85 0.5 AKC006 2 2 2 0.057 0.149 0.009 0.84 0.7 AKC006 2 2 2 0.057 0.149 0.009 0.84 0.7 AKC006 2 0.02 0.02 0.010 0.010 0.05 0.5 AKC006 2 0.02 0.02 0.02 0.02 0.02 0.02 0.02	AKC005	81	83	2	0.165	0.446	0.028	16.95	3.44			
AKC005 87 89 2 0.105 0.368 0.025 18.15 2.7 AKC005 89 91 2 0.110 0.346 0.023 17.75 2.5 AKC005 91 93 2 0.095 0.313 0.022 17.30 2.2 AKC005 93 95 2 0.096 0.258 0.018 9.63 1.7 AKC005 95 97 2 0.089 0.313 0.022 17.15 1.9 AKC005 97 99 2 0.116 0.389 0.025 17.20 2.4 AKC005 99 101 2 0.113 0.394 0.025 17.30 2.8 AKC005 101 103 2 0.117 0.393 0.023 16.75 2.6 AKC005 103 105 2 0.127 0.433 0.026 17.00 3.1 AKC005 105 107 2 0.122 0.433 0.027 16.15 3.2 AKC005 107 109 2 0.077 0.294 0.019 12.35 2.3 AKC005 109 111 2 0.097 0.340 0.020 13.05 2.4 AKC005 111 113 2 0.123 0.411 0.024 15.00 3.0 AKC005 113 115 2 0.129 0.443 0.025 14.35 3.6 AKC005 117 118 1 0.367 0.636 0.035 3.46 5.1 AKC005 117 118 1 0.367 0.636 0.035 3.46 5.1 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC006 0 2 4 2 0.074 0.116 0.008 0.41 0.1 AKC006 1 1 1 2 2 0.097 0.116 0.008 0.41 0.0 AKC006 1 1 1 1 1 2 0.097 0.116 0.008 0.41 0.0 AKC006 1 1 1 1 1 1 1 0.367 0.636 0.035 3.46 5.1 AKC005 1 1 1 1 1 1 0.367 0.636 0.035 3.46 5.1 AKC006 1 1 1 1 1 1 0.3 0.006 0.047 0.004 3.47 0.9 AKC006 1 1 1 1 1 1 1 0.3 0.006 0.047 0.004 3.47 0.9 AKC006 1 1 1 1 1 1 1 0.3 0.007 0.116 0.008 0.41 0.0 AKC006 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AKC005	83	85	2	0.137	0.476	0.030	17.10	3.52			
AKC005 89 91 2 0.110 0.346 0.023 17.75 2.5 AKC005 91 93 2 0.095 0.313 0.022 17.30 2.2 AKC005 93 95 2 0.096 0.258 0.018 9.63 1.7 AKC005 95 97 2 0.089 0.313 0.022 17.15 1.9 AKC005 97 99 2 0.116 0.389 0.025 17.20 2.4 AKC005 99 101 2 0.113 0.394 0.025 17.30 2.8 AKC005 101 103 2 0.117 0.393 0.023 16.75 2.6 AKC005 103 105 2 0.127 0.433 0.026 17.00 3.1 AKC005 105 107 2 0.122 0.433 0.027 16.15 3.2 AKC005 107 109 2 0.077 0.294 0.019 12.35 2.3 AKC005 109 111 2 0.097 0.340 0.020 13.05 2.4 AKC005 111 113 2 0.123 0.411 0.024 15.00 3.0 AKC005 113 115 2 0.129 0.443 0.025 14.35 3.6 AKC005 117 118 1 0.367 0.636 0.035 3.46 5.1 AKC005 117 118 1 0.389 1.170 0.056 2.07 8.1 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC006 0 2 0.007 0.149 0.008 0.41 0.0 AKC006 1 19 12 2 0.009 0.145 0.012 0.71 0.1 AKC006 1 19 12 2 0.009 0.145 0.012 0.71 0.1 AKC006 1 19 12 2 0.009 0.145 0.012 0.71 0.1 AKC006 1 19 12 2 0.009 0.145 0.012 0.71 0.1 AKC006 1 19 12 2 0.009 0.145 0.012 0.71 0.1 AKC006 1 19 12 2 0.009 0.145 0.012 0.71 0.1 AKC006 1 19 12 2 0.009 0.145 0.012 0.71 0.1 AKC006 1 1 19 12 2 0.009 0.149 0.009 0.84 0.7 AKC006 1 1 1 1 1 1 0.2 0.009 0.149 0.009 0.84 0.7 AKC006 1 1 1 1 1 1 0.2 0.009 0.149 0.009 0.84 0.7 AKC006 1 1 1 0.000 0.000 0.14 0.009 0.84 0.7 AKC006 1 1 1 0.000 0.000 0.100 0.95 0.5 AKC006 1 1 1 0.000	AKC005	85	87	2	0.124	0.473	0.030	18.15	3.66			
AKC005 91 93 2 0.095 0.313 0.022 17.30 2.2 AKC005 93 95 2 0.096 0.258 0.018 9.63 1.7 AKC005 95 97 2 0.089 0.313 0.022 17.15 1.9 AKC005 97 99 2 0.116 0.389 0.025 17.20 2.4 AKC005 99 101 2 0.113 0.394 0.025 17.30 2.8 AKC005 101 103 2 0.117 0.393 0.023 16.75 2.6 AKC005 103 105 2 0.127 0.433 0.026 17.00 3.1 AKC005 107 109 2 0.077 0.294 0.019 12.35 2.3 AKC005 107 109 2 0.077 0.294 0.019 12.35 2.3 AKC005 111 113 2 0.123 0.411 0.024 15.00 3.0 AKC005 113 115 2 0.129 0.443 0.025 14.35 3.6 AKC005 115 117 2 0.129 0.443 0.025 14.35 3.6 AKC005 116 117 2 0.174 0.571 0.032 12.75 4.6 AKC005 117 118 1 0.367 0.636 0.035 3.46 5.1 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC006 0 2 2 0.060 0.145 0.012 0.71 0.1 AKC006 1 4 6 2 0.074 0.116 0.008 0.41 0.0 AKC006 1 1 1 2 2 0.077 0.182 0.010 0.95 0.5 AKC006 1 1 1 2 2 0.077 0.182 0.010 0.95 0.5 AKC006 1 1 1 2 2 0.077 0.182 0.010 0.95 0.5 AKC006 1 2 14 2 0.107 0.182 0.010 0.95 0.5 AKC006 1 2 14 2 0.107 0.182 0.010 0.95 0.5 AKC006 1 2 14 2 0.107 0.182 0.010 0.95 0.5 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 1 2 14 2 0.107 0.182 0.010 0.95 0.5 AKC006 1 3 20 2 0.121 0.160 0.009 1.08 1.0 AKC006 1 4 6 2 0.072 0.194 0.009 0.84 0.7 AKC006 1 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AKC005	87	89	2	0.105	0.368	0.025	18.15	2.77			
AKC005         93         95         2         0.096         0.258         0.018         9.63         1.7           AKC005         95         97         2         0.089         0.313         0.022         17.15         1.9           AKC005         97         99         2         0.116         0.389         0.025         17.20         2.4           AKC005         101         103         2         0.117         0.393         0.025         17.30         2.8           AKC005         101         103         2         0.117         0.393         0.026         17.00         3.1           AKC005         103         105         2         0.127         0.433         0.026         17.00         3.1           AKC005         105         107         2         0.122         0.433         0.027         16.15         3.2           AKC005         107         109         2         0.077         0.294         0.019         12.35         2.4           AKC005         111         113         2         0.123         0.411         0.024         15.00         3.0           AKC005         113         115         2	AKC005	89	91	2	0.110	0.346	0.023	17.75	2.55			
AKC005         95         97         2         0.089         0.313         0.022         17.15         1.9           AKC005         97         99         2         0.116         0.389         0.025         17.20         2.4           AKC005         99         101         2         0.113         0.394         0.025         17.30         2.8           AKC005         101         103         2         0.117         0.393         0.023         16.75         2.6           AKC005         103         105         2         0.127         0.433         0.026         17.00         3.1           AKC005         105         107         2         0.122         0.433         0.027         16.15         3.2           AKC005         107         109         2         0.077         0.294         0.019         12.35         2.3           AKC005         119         111         2         0.097         0.340         0.020         13.05         2.4           AKC005         113         115         2         0.123         0.411         0.024         15.00         3.0           AKC005         113         115         17	AKC005	91	93	2	0.095	0.313	0.022	17.30	2.26			
AKC005         97         99         2         0.116         0.389         0.025         17.20         2.4           AKC005         99         101         2         0.113         0.394         0.025         17.30         2.8           AKC005         101         103         2         0.117         0.393         0.023         16.75         2.6           AKC005         103         105         2         0.127         0.433         0.026         17.00         3.1           AKC005         105         107         2         0.122         0.433         0.027         16.15         3.2           AKC005         107         109         2         0.077         0.294         0.019         12.35         2.3           AKC005         109         111         2         0.097         0.340         0.020         13.05         2.4           AKC005         111         113         2         0.123         0.411         0.024         15.00         3.0           AKC005         113         115         2         0.123         0.411         0.024         15.00         3.0           AKC005         118         119         1	AKC005	93	95	2	0.096	0.258	0.018	9.63	1.79			
AKC005 99 101 2 0.113 0.394 0.025 17.30 2.8 AKC005 101 103 2 0.117 0.393 0.023 16.75 2.6 AKC005 103 105 2 0.127 0.433 0.026 17.00 3.1 AKC005 105 107 2 0.122 0.433 0.027 16.15 3.2 AKC005 107 109 2 0.077 0.294 0.019 12.35 2.3 AKC005 109 111 2 0.097 0.340 0.020 13.05 2.4 AKC005 111 113 2 0.123 0.411 0.024 15.00 3.0 AKC005 113 115 2 0.129 0.443 0.025 14.35 3.6 AKC005 115 117 2 0.174 0.571 0.032 12.75 4.6 AKC005 118 119 1 0.389 1.170 0.056 2.07 8.1 AKC005 119 122 3 0.036 0.047 0.004 3.47 0.9 AKC006 0 2 2 0.060 0.145 0.012 0.71 0.1 AKC006 4 6 2 0.074 0.182 0.008 1.14 0.1 AKC006 8 10 2 0.072 0.194 0.009 0.84 0.7 AKC006 10 12 2 0.074 0.167 0.006 0.89 0.4 AKC006 10 12 2 0.057 0.149 0.009 0.82 0.6 AKC006 14 16 2 0.107 0.182 0.010 0.95 0.5 AKC006 15 14 2 0.12 0.109 0.210 0.016 0.83 0.5 AKC006 16 18 20 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 4 2 0.107 0.182 0.010 0.95 0.5 AKC006 16 18 20 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 4 2 0.174 0.181 0.019 2.47 0.7 AKC006 2 2 4 2 0.190 0.210 0.016 0.83 0.5 AKC006 16 18 20 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 4 2 0.190 0.241 0.019 2.47 0.7 AKC006 2 2 2 0.147 0.181 0.017 1.66 0.6 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 0.121 0.160 0.009 1.08 1.0 AKC006 2 2 2 1 0.147 0.181 0.017 1.66 0.6 AKC006 2 2 2 2 0.147 0.181 0.017 1.66 0.6 AKC006 2 2 2 2 0.147 0.181 0.017 1.66 0.6 AKC006 2 2 2 2 0.147 0.181 0.017 1.66 0.6 AKC006 2 2 2 2 0.147 0.181 0.017 1.66 0.6 AKC006 2 2 2 2 0.147 0.181 0.017 1.66 0.6	AKC005	95	97	2	0.089	0.313	0.022	17.15	1.94			
AKC005         101         103         2         0.117         0.393         0.023         16.75         2.6           AKC005         103         105         2         0.127         0.433         0.026         17.00         3.1           AKC005         105         107         2         0.122         0.433         0.027         16.15         3.2           AKC005         107         109         2         0.077         0.294         0.019         12.35         2.3           AKC005         109         111         2         0.097         0.340         0.020         13.05         2.4           AKC005         111         113         2         0.123         0.411         0.024         15.00         3.0           AKC005         113         115         2         0.129         0.443         0.025         14.35         3.6           AKC005         115         117         2         0.174         0.571         0.032         12.75         4.6           AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC006         19         2         2	AKC005	97	99	2	0.116	0.389	0.025	17.20	2.42			
AKC005         103         105         2         0.127         0.433         0.026         17.00         3.1           AKC005         105         107         2         0.122         0.433         0.027         16.15         3.2           AKC005         107         109         2         0.077         0.294         0.019         12.35         2.3           AKC005         109         111         2         0.097         0.340         0.020         13.05         2.4           AKC005         111         113         2         0.123         0.411         0.024         15.00         3.0           AKC005         113         115         2         0.129         0.443         0.025         14.35         3.6           AKC005         115         117         2         0.174         0.571         0.032         12.75         4.6           AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC005         119         122         3         0.036         0.047         0.004         3.47         0.9           AKC006         0         2         2	AKC005	99	101	2	0.113	0.394	0.025	17.30	2.81			
AKC005         105         107         2         0.122         0.433         0.027         16.15         3.2           AKC005         107         109         2         0.077         0.294         0.019         12.35         2.3           AKC005         109         111         2         0.097         0.340         0.020         13.05         2.4           AKC005         111         113         2         0.123         0.411         0.024         15.00         3.0           AKC005         113         115         2         0.129         0.443         0.025         14.35         3.6           AKC005         115         117         2         0.174         0.571         0.032         12.75         4.6           AKC005         117         118         1         0.367         0.636         0.035         3.46         5.1           AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         4         6         2	AKC005	101	103	2	0.117	0.393	0.023	16.75	2.63			
AKC005         107         109         2         0.077         0.294         0.019         12.35         2.3           AKC005         109         111         2         0.097         0.340         0.020         13.05         2.4           AKC005         111         113         2         0.123         0.411         0.024         15.00         3.0           AKC005         113         115         2         0.129         0.443         0.025         14.35         3.6           AKC005         115         117         2         0.174         0.571         0.032         12.75         4.6           AKC005         117         118         1         0.367         0.636         0.035         3.46         5.1           AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC005         119         122         3         0.036         0.047         0.004         3.47         0.9           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         4         6         2         <	AKC005	103	105	2	0.127	0.433	0.026	17.00	3.17			
AKC005         109         111         2         0.097         0.340         0.020         13.05         2.4           AKC005         111         113         2         0.123         0.411         0.024         15.00         3.0           AKC005         113         115         2         0.129         0.443         0.025         14.35         3.6           AKC005         115         117         2         0.174         0.571         0.032         12.75         4.6           AKC005         117         118         1         0.367         0.636         0.035         3.46         5.1           AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC006         119         122         3         0.036         0.047         0.004         3.47         0.9           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         4         6         2         0.	AKC005	105	107	2	0.122	0.433	0.027	16.15	3.23			
AKC005         111         113         2         0.123         0.411         0.024         15.00         3.0           AKC005         113         115         2         0.129         0.443         0.025         14.35         3.6           AKC005         115         117         2         0.174         0.571         0.032         12.75         4.6           AKC005         117         118         1         0.367         0.636         0.035         3.46         5.1           AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC005         119         122         3         0.036         0.047         0.004         3.47         0.9           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         2         4         2         0.047         0.116         0.008         0.41         0.0           AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         8         10         2         0.072<	AKC005	107	109	2	0.077	0.294	0.019	12.35	2.31			
AKC005         113         115         2         0.129         0.443         0.025         14.35         3.6           AKC005         115         117         2         0.174         0.571         0.032         12.75         4.6           AKC005         117         118         1         0.367         0.636         0.035         3.46         5.1           AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC005         119         122         3         0.036         0.047         0.004         3.47         0.9           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         2         4         2         0.047         0.116         0.008         0.41         0.0           AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         4         6         2         0.074         0.182         0.008         1.4         0.1           AKC006         8         10         2         0.072	AKC005	109	111	2	0.097	0.340	0.020	13.05	2.44			
AKC005         115         117         2         0.174         0.571         0.032         12.75         4.6           AKC005         117         118         1         0.367         0.636         0.035         3.46         5.1           AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC005         119         122         3         0.036         0.047         0.004         3.47         0.9           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         2         4         2         0.047         0.116         0.008         0.41         0.0           AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         8         10         2         0.072         0.194         0.009         0.84         0.7           AKC006         10         12         2         0.057	AKC005	111	113	2	0.123	0.411	0.024	15.00	3.03			
AKC005         117         118         1         0.367         0.636         0.035         3.46         5.1           AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC005         119         122         3         0.036         0.047         0.004         3.47         0.9           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         2         4         2         0.047         0.116         0.008         0.41         0.0           AKC006         4         6         2         0.074         0.182         0.008         0.41         0.0           AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         8         10         2         0.072         0.194         0.009         0.84         0.7           AKC006         10         12         2         0.057         0.149         0.009         0.82         0.6           AKC006         12         14         2         0.107	AKC005	113	115	2	0.129	0.443	0.025	14.35	3.67			
AKC005         118         119         1         0.389         1.170         0.056         2.07         8.1           AKC005         119         122         3         0.036         0.047         0.004         3.47         0.9           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         2         4         2         0.047         0.116         0.008         0.41         0.0           AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         6         8         2         0.071         0.167         0.006         0.89         0.4           AKC006         8         10         2         0.072         0.194         0.009         0.84         0.7           AKC006         10         12         2         0.057         0.149         0.009         0.82         0.6           AKC006         12         14         2         0.107         0.182         0.010         0.95         0.5           AKC006         14         16         2         0.109	AKC005	115	117	2	0.174	0.571	0.032	12.75	4.69			
AKC005         119         122         3         0.036         0.047         0.004         3.47         0.9           AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         2         4         2         0.047         0.116         0.008         0.41         0.0           AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         6         8         2         0.071         0.167         0.006         0.89         0.4           AKC006         8         10         2         0.072         0.194         0.009         0.84         0.7           AKC006         10         12         2         0.057         0.149         0.009         0.82         0.6           AKC006         12         14         2         0.107         0.182         0.010         0.95         0.5           AKC006         14         16         2         0.109         0.210         0.016         0.83         0.5           AKC006         16         18         2         0.131 <t< td=""><td>AKC005</td><td>117</td><td>118</td><td>1</td><td>0.367</td><td>0.636</td><td>0.035</td><td>3.46</td><td>5.18</td></t<>	AKC005	117	118	1	0.367	0.636	0.035	3.46	5.18			
AKC006         0         2         2         0.060         0.145         0.012         0.71         0.1           AKC006         2         4         2         0.047         0.116         0.008         0.41         0.0           AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         6         8         2         0.071         0.167         0.006         0.89         0.4           AKC006         8         10         2         0.072         0.194         0.009         0.84         0.7           AKC006         10         12         2         0.057         0.149         0.009         0.82         0.6           AKC006         12         14         2         0.107         0.182         0.010         0.95         0.5           AKC006         14         16         2         0.109         0.210         0.016         0.83         0.5           AKC006         16         18         2         0.131         0.198         0.013         0.84         1.1           AKC006         18         20         2         0.121	AKC005	118	119	1	0.389	1.170	0.056	2.07	8.16			
AKC006         2         4         2         0.047         0.116         0.008         0.41         0.0           AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         6         8         2         0.071         0.167         0.006         0.89         0.4           AKC006         8         10         2         0.072         0.194         0.009         0.84         0.7           AKC006         10         12         2         0.057         0.149         0.009         0.82         0.6           AKC006         12         14         2         0.107         0.182         0.010         0.95         0.5           AKC006         14         16         2         0.109         0.210         0.016         0.83         0.5           AKC006         16         18         2         0.131         0.198         0.013         0.84         1.1           AKC006         18         20         2         0.121         0.160         0.009         1.08         1.0           AKC006         20         22         2         0.147 <t< td=""><td>AKC005</td><td>119</td><td>122</td><td>3</td><td>0.036</td><td>0.047</td><td>0.004</td><td>3.47</td><td>0.90</td></t<>	AKC005	119	122	3	0.036	0.047	0.004	3.47	0.90			
AKC006         4         6         2         0.074         0.182         0.008         1.14         0.1           AKC006         6         8         2         0.071         0.167         0.006         0.89         0.4           AKC006         8         10         2         0.072         0.194         0.009         0.84         0.7           AKC006         10         12         2         0.057         0.149         0.009         0.82         0.6           AKC006         12         14         2         0.107         0.182         0.010         0.95         0.5           AKC006         14         16         2         0.109         0.210         0.016         0.83         0.5           AKC006         16         18         2         0.131         0.198         0.013         0.84         1.1           AKC006         18         20         2         0.121         0.160         0.009         1.08         1.0           AKC006         20         22         2         0.147         0.181         0.017         1.66         0.6           AKC006         24         25         1         0.172	AKC006	0	2	2	0.060	0.145	0.012	0.71	0.13			
AKC006         6         8         2         0.071         0.167         0.006         0.89         0.4           AKC006         8         10         2         0.072         0.194         0.009         0.84         0.7           AKC006         10         12         2         0.057         0.149         0.009         0.82         0.6           AKC006         12         14         2         0.107         0.182         0.010         0.95         0.5           AKC006         14         16         2         0.109         0.210         0.016         0.83         0.5           AKC006         16         18         2         0.131         0.198         0.013         0.84         1.1           AKC006         18         20         2         0.121         0.160         0.009         1.08         1.0           AKC006         20         22         2         0.147         0.181         0.017         1.66         0.6           AKC006         22         24         2         0.190         0.241         0.019         2.47         0.7           AKC006         24         25         1         0.172	AKC006	2	4	2	0.047	0.116	0.008	0.41	0.05			
AKC006         8         10         2         0.072         0.194         0.009         0.84         0.7           AKC006         10         12         2         0.057         0.149         0.009         0.82         0.6           AKC006         12         14         2         0.107         0.182         0.010         0.95         0.5           AKC006         14         16         2         0.109         0.210         0.016         0.83         0.5           AKC006         16         18         2         0.131         0.198         0.013         0.84         1.1           AKC006         18         20         2         0.121         0.160         0.009         1.08         1.0           AKC006         20         22         2         0.147         0.181         0.017         1.66         0.6           AKC006         22         24         2         0.190         0.241         0.019         2.47         0.7           AKC006         24         25         1         0.172         0.531         0.035         7.57         0.0           AKC006         25         26         1         0.212	AKC006	4	6	2	0.074	0.182	0.008	1.14	0.11			
AKC006         10         12         2         0.057         0.149         0.009         0.82         0.6           AKC006         12         14         2         0.107         0.182         0.010         0.95         0.5           AKC006         14         16         2         0.109         0.210         0.016         0.83         0.5           AKC006         16         18         2         0.131         0.198         0.013         0.84         1.1           AKC006         18         20         2         0.121         0.160         0.009         1.08         1.0           AKC006         20         22         2         0.147         0.181         0.017         1.66         0.6           AKC006         22         24         2         0.190         0.241         0.019         2.47         0.7           AKC006         24         25         1         0.172         0.531         0.035         7.57         0.0           AKC006         25         26         1         0.212         0.403         0.027         9.06         0.1           AKC006         26         27         1         0.399	AKC006	6	8	2	0.071	0.167	0.006	0.89	0.47			
AKC006         12         14         2         0.107         0.182         0.010         0.95         0.5           AKC006         14         16         2         0.109         0.210         0.016         0.83         0.5           AKC006         16         18         2         0.131         0.198         0.013         0.84         1.1           AKC006         18         20         2         0.121         0.160         0.009         1.08         1.0           AKC006         20         22         2         0.147         0.181         0.017         1.66         0.6           AKC006         22         24         2         0.190         0.241         0.019         2.47         0.7           AKC006         24         25         1         0.172         0.531         0.035         7.57         0.0           AKC006         25         26         1         0.212         0.403         0.027         9.06         0.1           AKC006         26         27         1         0.399         0.488         0.034         8.97         0.1           AKC006         27         28         1         0.132	AKC006	8	10	2	0.072	0.194	0.009	0.84	0.78			
AKC006         14         16         2         0.109         0.210         0.016         0.83         0.5           AKC006         16         18         2         0.131         0.198         0.013         0.84         1.1           AKC006         18         20         2         0.121         0.160         0.009         1.08         1.0           AKC006         20         22         2         0.147         0.181         0.017         1.66         0.6           AKC006         22         24         2         0.190         0.241         0.019         2.47         0.7           AKC006         24         25         1         0.172         0.531         0.035         7.57         0.0           AKC006         25         26         1         0.212         0.403         0.027         9.06         0.1           AKC006         26         27         1         0.399         0.488         0.034         8.97         0.1           AKC006         27         28         1         0.132         0.519         0.029         10.30         0.0           AKC006         28         29         1         0.096	AKC006	10	12	2	0.057	0.149	0.009	0.82	0.62			
AKC006         16         18         2         0.131         0.198         0.013         0.84         1.1           AKC006         18         20         2         0.121         0.160         0.009         1.08         1.0           AKC006         20         22         2         0.147         0.181         0.017         1.66         0.6           AKC006         22         24         2         0.190         0.241         0.019         2.47         0.7           AKC006         24         25         1         0.172         0.531         0.035         7.57         0.0           AKC006         25         26         1         0.212         0.403         0.027         9.06         0.1           AKC006         26         27         1         0.399         0.488         0.034         8.97         0.1           AKC006         27         28         1         0.132         0.519         0.029         10.30         0.0           AKC006         28         29         1         0.096         0.404         0.026         10.75         0.2	AKC006	12	14	2	0.107	0.182	0.010	0.95	0.51			
AKC006         18         20         2         0.121         0.160         0.009         1.08         1.0           AKC006         20         22         2         0.147         0.181         0.017         1.66         0.6           AKC006         22         24         2         0.190         0.241         0.019         2.47         0.7           AKC006         24         25         1         0.172         0.531         0.035         7.57         0.0           AKC006         25         26         1         0.212         0.403         0.027         9.06         0.1           AKC006         26         27         1         0.399         0.488         0.034         8.97         0.1           AKC006         27         28         1         0.132         0.519         0.029         10.30         0.0           AKC006         28         29         1         0.096         0.404         0.026         10.75         0.2	AKC006	14	16	2	0.109	0.210	0.016	0.83	0.58			
AKC006       20       22       2       0.147       0.181       0.017       1.66       0.6         AKC006       22       24       2       0.190       0.241       0.019       2.47       0.7         AKC006       24       25       1       0.172       0.531       0.035       7.57       0.0         AKC006       25       26       1       0.212       0.403       0.027       9.06       0.1         AKC006       26       27       1       0.399       0.488       0.034       8.97       0.1         AKC006       27       28       1       0.132       0.519       0.029       10.30       0.0         AKC006       28       29       1       0.096       0.404       0.026       10.75       0.2	AKC006	16	18	2	0.131	0.198	0.013	0.84	1.12			
AKC006       22       24       2       0.190       0.241       0.019       2.47       0.7         AKC006       24       25       1       0.172       0.531       0.035       7.57       0.0         AKC006       25       26       1       0.212       0.403       0.027       9.06       0.1         AKC006       26       27       1       0.399       0.488       0.034       8.97       0.1         AKC006       27       28       1       0.132       0.519       0.029       10.30       0.0         AKC006       28       29       1       0.096       0.404       0.026       10.75       0.2	AKC006	18	20	2	0.121	0.160	0.009	1.08	1.07			
AKC006       24       25       1       0.172       0.531       0.035       7.57       0.0         AKC006       25       26       1       0.212       0.403       0.027       9.06       0.1         AKC006       26       27       1       0.399       0.488       0.034       8.97       0.1         AKC006       27       28       1       0.132       0.519       0.029       10.30       0.0         AKC006       28       29       1       0.096       0.404       0.026       10.75       0.2	AKC006	20	22	2	0.147	0.181	0.017	1.66	0.69			
AKC006       25       26       1       0.212       0.403       0.027       9.06       0.1         AKC006       26       27       1       0.399       0.488       0.034       8.97       0.1         AKC006       27       28       1       0.132       0.519       0.029       10.30       0.0         AKC006       28       29       1       0.096       0.404       0.026       10.75       0.2	AKC006	22	24	2	0.190	0.241	0.019	2.47	0.70			
AKC006       26       27       1       0.399       0.488       0.034       8.97       0.1         AKC006       27       28       1       0.132       0.519       0.029       10.30       0.0         AKC006       28       29       1       0.096       0.404       0.026       10.75       0.2	AKC006	24	25	1	0.172	0.531	0.035	7.57	0.06			
AKC006     27     28     1     0.132     0.519     0.029     10.30     0.0       AKC006     28     29     1     0.096     0.404     0.026     10.75     0.2	AKC006	25	26	1	0.212	0.403	0.027	9.06	0.16			
AKC006 28 29 1 0.096 0.404 0.026 10.75 0.2	AKC006	26	27	1	0.399	0.488	0.034	8.97	0.11			
	AKC006	27	28	1	0.132	0.519	0.029	10.30	0.03			
AKC006 29 30 1 0.169 0.455 0.026 10.35 0.3	AKC006	28	29	1	0.096	0.404	0.026	10.75	0.25			
	AKC006	29	30	1	0.169	0.455	0.026	10.35	0.35			



	TABLE 4 AKELIKONGO DRILLHOLE RESULTS AKC004 TO AKC006											
HOLE	FROM	TO	WIDTH	Cu %	Ni %	Co %	Mg %	S %*				
AKC006	30	32	2	0.095	0.375	0.024	15.30	2.06				
AKC006	32	34	2	0.115	0.365	0.024	16.90	3.11				
AKC006	34	36	2	0.099	0.402	0.026	16.85	3.20				
AKC006	36	38	2	0.086	0.327	0.023	17.35	2.12				
AKC006	38	40	2	0.091	0.373	0.025	16.65	2.98				
AKC006	40	42	2	0.119	0.352	0.024	16.35	2.58				
AKC006	42	44	2	0.086	0.290	0.022	16.45	2.30				
AKC006	44	46	2	0.082	0.263	0.020	16.85	2.05				
AKC006	46	48	2	0.088	0.271	0.021	17.75	2.17				
AKC006	48	50	2	0.089	0.258	0.020	16.70	2.02				
AKC006	50	52	2	0.083	0.273	0.021	17.20	1.94				
AKC006	52	54	2	0.091	0.290	0.022	17.75	2.28				
AKC006	54	56	2	0.086	0.286	0.022	17.90	2.05				
AKC006	56	58	2	0.083	0.307	0.022	15.60	2.41				
AKC006	58	60	2	0.075	0.333	0.023	17.90	2.12				
AKC006	60	62	2	0.077	0.389	0.026	18.40	2.91				
AKC006	62	64	2	0.105	0.310	0.022	17.15	2.17				
AKC006	64	66	2	0.077	0.372	0.024	16.80	2.69				
AKC006	66	68	2	0.094	0.312	0.020	14.70	2.25				
AKC006	68	70	2	0.085	0.304	0.021	15.70	2.19				
AKC006	70	72	2	0.051	0.179	0.013	11.40	1.14				
AKC006	72	74	2	0.075	0.316	0.020	11.95	2.24				
AKC006	74	76	2	0.112	0.444	0.026	13.30	3.92				
AKC006	76	78	2	0.076	0.407	0.025	14.35	3.69				
AKC006	78	79	1	0.171	0.296	0.019	14.90	2.52				
AKC006	79	80	1	4.610	0.575	0.038	9.10	9.12				
AKC006	80	81	1	0.457	0.461	0.028	12.50	4.27				
AKC006	81	82	1	1.355	0.404	0.025	8.94	4.38				
AKC006	82	83	1	0.674	0.541	0.031	4.55	4.64				
AKC006	83	85	2	0.053	0.035	0.004	2.99	1.21				
			3									

<sup>\*</sup>due to incorrect heat treatment of the samples at the lab, some Sulphur may have been lost in the process, hence the Sulphur values may be underreporting.



TABLE	5 PAMW	A ASSA			PLES GENE B PLUS ZN		REATER	THAN 0.5%
HOLE	FROM	ТО	WIDTH	Ag ppm	Cd ppm	Pb %	Zn %	Combined Zn & Pb %
PAA002	10	15	5	2.70	3.10	0.217	0.407	0.624
PAA004	13	14	1	13.90	20.60	1.345	1.305	2.650
PAA004	14	15	1	26.50	138.00	2.250	2.960	5.210
PAA006	16	17	1	9.20	88.60	0.883	1.940	2.823
PAA006	18	19	1	0.70	51.90	0.055	0.976	1.031
PAA017	14	18	4	2.20	2.60	0.122	0.380	0.502
PAA001	32	33	1	2.20	47.70	0.208	1.205	1.413
PAA004	10	11	1	1.50	1.30	0.292	0.310	0.602
PAA004	12	13	1	2.50	8.30	0.132	0.635	0.767
PAA006	13	14	1	1.00	3.90	0.061	0.506	0.567
PAA006	14	15	1	2.40	6.10	0.336	0.617	0.953
PAA006	15	16	1	2.80	17.40	0.178	0.401	0.579
PAA009	22	23	1	5.90	43.90	0.512	0.446	0.958
PAA009	23	24	1	7.00	53.50	0.664	1.280	1.944
PAA009	24	25	1	2.80	17.70	0.236	0.552	0.788
PAA010	6	7	1	0.50	2.00	0.045	0.634	0.679
PAA010	7	8	1	2.00	1.70	0.559	0.662	1.221
PAA010	8	9	1	0.50	1.40	0.277	0.560	0.837
PAA013	20	21	1	0.60	2.60	0.068	0.452	0.520
PAA013	21	22	1	1.10	2.90	0.153	0.617	0.770
PAA022	21	22	1	4.80	108.50	0.678	1.800	2.478
PAA022	22	23	1	7.40	22.50	1.115	0.391	1.506
PAA022	31	32	1	0.50	41.40	0.238	0.771	1.009
PAC001	36	37	1	0.80	20.20	0.103	0.491	0.594
PAC001	47	48	1	7.20	109.00	0.651	2.470	3.121
PAC001	48	49	1	3.90	55.10	0.425	1.380	1.805
PAC002	34	38	4	2.30	27.20	0.265	0.625	0.890
PAC002	38	39	1	10.70	114.00	1.400	2.550	3.950
PAC003	34	35	1	3.10	52.70	0.209	0.933	1.142
PAC001	29	30	1	<0.5	23.40	0.064	0.542	0.606
PAC001	30	31	1	2.90	85.20	0.337	1.970	2.307
PAC001	31	32	1	0.50	27.00	0.093	0.617	0.710
PAC001	32	33	1	0.70	22.00	0.167	0.570	0.737



# **JORC Code, 2012 Edition – Table 1 report template**

# **Section 1 Sampling Techniques and Data**

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul> <li>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</li> <li>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</li> <li>Aspects of the determination of mineralisation that are Material to the Public Report.</li> <li>In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</li> </ul>	<ul> <li>See Sub sampling techniques (for drilling)</li> <li>Soil samples are taken initially at 1km line and 100m sample spacing. Infill soil sampling to 200m line and 50m sample spacing and where appropriate down to 25m by 25m. The samples are taken from about 30cm depth and sieved with a 250# sieve. Soil Sample size is around 150g.  If samples are wet or unsieved, the samples are brought back to camp, dried, then crushed and sieved to -250um.</li> <li>The sample is then placed in a small cup with a mylar film on the bottom and analysed by XRF</li> <li>One in eight soils were sent for laboratory analysis as a check.</li> </ul>
Drilling techniques	<ul> <li>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</li> </ul>	<ul> <li>4.5 Inch Reverse Circulation drilling with a 1170 cfm compressor and a face sampling hammer bit.</li> <li>3 inch Aircore drilling with face sampling hammer bit.</li> </ul>
Drill sample recovery	<ul> <li>Method of recording and assessing core and chip sample recoveries and results assessed.</li> <li>Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> <li>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</li> </ul>	<ul> <li>The recovery was very high, and the samples were generally dry and of high quality, with only rare occurrences of damp samples on some rod changes.</li> <li>Groundwater was encountered in many holes, but the compressor and the efficient use of additives was sufficient to keep the samples dry and recovery high in every hole.</li> </ul>



Criteria	JORC Code explanation	Commentary
Logging	<ul> <li>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> <li>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</li> <li>The total length and percentage of the relevant intersections logged.</li> </ul>	<ul> <li>Logging was conducted on all holes using a digital quantitative and qualitative logging system to a level of detail which would support a mineral resource estimation.</li> </ul>
Sub- sampling techniques and sample preparation	<ul> <li>If core, whether cut or sawn and whether quarter, half or all core taken.</li> <li>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</li> <li>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> <li>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</li> <li>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/secondhalf sampling.</li> <li>Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul>	<ul> <li>Each dry one metre sample was passed through a riffle splitter, with one sample taken for laboratory analysis.</li> <li>A second sample was sieved for pXRF analysis on site and one chip sample taken and stored in numbered chip trays as a reference.</li> <li>Samples selected for laboratory analysis based on XRF data were further riffle split at the Kitgum office to reduce the size of the sample sent to the laboratory. All samples sent to the laboratory are between 500g and 1kg in weight.</li> <li>Field duplicates and standards were used every 50 samples to ensure accuracy and precision.</li> </ul>



Criteria Quality of assay data and laboratory tests	<ul> <li>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</li> <li>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</li> <li>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</li> </ul>	<ul> <li>For soils and field analysis of RC and aircore samples, an Olympus Innov-X Delta Premium portable XRF analyzer was used with a Rhenium anode in soil and mines mode at a tube voltage of 40kV and a tube power of 200µA. The resolution is around 156eV @ 40000cps. The detector area is 30mm2 SDD2. A power source of Lithium ion batteries is used. The element range is from P (Z15 to U (Z92). A cycle time of 180 seconds Soil Mode was used and beam times were 60 seconds.</li> <li>Selected high samples were analysed in Mineplus Mode. A propylene3 window was used. Standards are used regularly to calibrate the instrument.</li> <li>For the samples selected for laboratory analysis multielement assaying is done via a commercial laboratory using a four Acid digest as a total technique with and ICP-AES finish. For selected samples additional assaying for Au Pt and Pd is by and 30g Fire Assay with ICP finish</li> <li>Lab Standards were analysed every 30 samples</li> </ul>
Verification of sampling and assaying	<ul> <li>alternative company personnel.</li> <li>The use of twinned holes.</li> <li>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</li> <li>Discuss any adjustment to assay data.</li> </ul>	<ul> <li>This is an early drill test into a newly identified prospect. No verification has been completed yet.</li> <li>Twinned holes are not undertaken</li> <li>Data entry is checked by Perth Based Data Management Geologist</li> <li>Assays have not been adjusted</li> <li>The soil data is reviewed by the independent consultant Nigel Brand, Geochemical Services, West Perth The data is audited and verified and then stored in a SQL relational data base.</li> </ul>
Location of data points	<ul> <li>Accuracy and quality of surveys used to locate drill holes (collar and downhole surveys), trenches, mine workings and other locations used in Mineral</li> </ul>	<ul> <li>Drill holes and soil and rock points have been located via hand held GPS.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<ul><li>Resource estimation.</li><li>Specification of the grid system used.</li><li>Quality and adequacy of topographic control.</li></ul>	
Data spacing and distribution	<ul> <li>Data spacing for reporting of Exploration Results.</li> <li>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</li> <li>Whether sample compositing has been applied.</li> </ul>	No Mineral Resource or Ore Reserve Estimation has been calculated
Orientation of data in relation to geological structure	<ul> <li>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</li> <li>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</li> </ul>	<ul> <li>Although this is an early stage drilling program the drilling has been design to cut at as orthogonal as possible to the mineralised bodies. The 20m spaced drilling was designed partly to understand these controls.</li> </ul>
Sample security	The measures taken to ensure sample security.	<ul> <li>Drill samples are accompanied to Entebbe by a Sipa employee. Until they are consigned by air to the laboratory in Perth.</li> </ul>
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	<ul> <li>No reviews have been undertaken as yet. A review is planned for the next quarter.</li> </ul>

# **Section 2 Reporting of Exploration Results**

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul> <li>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</li> <li>The security of the tenure held at the time of reporting along with any</li> </ul>	<ul> <li>The results reported in this Announcement are on granted Exploration Licences held by Sipa Exploration Uganda Limited, a 100% beneficially owned subsidiary of Sipa Resources Limited.</li> </ul>
	known impediments to obtaining a licence to operate in the area.	<ul> <li>At this time the tenements are believed to be in good standing. There are no known impediments to obtain</li> </ul>



Criteria	ORC Code explanation	Commentary
		a license to operate, other than those set out by statutory requirements which have not yet been applied for.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other p	<ul> <li>No previous mineral exploration activity has been conducted prior to Sipa.</li> </ul>
Geology	Deposit type, geological setting and style of mineralisati	on.  • The Kitgum-Pader Project covers reworked, high grade metamorphic, Archaean and Proterozoic supracrustal rocks heavily overprinted by the Panafrican Neoproterozoic event of between 600 and 700Ma. The tectonostratigraphy includes felsic orthoand para-gneisses and mafic and ultramafic amphibolites and granulites and is situated on the northeastern margin of the Congo Craton. The geology and tectonic setting is prospective for magmatic Ni, Broken Hill type base metal and orogenic Au deposits
Drill hole Information	A summary of all information material to the understand exploration results including a tabulation of the following Material drill holes:  o easting and northing of the drill hole collar o elevation or RL (Reduced Level – elevation above so of the drill hole collar o dip and azimuth of the hole o down hole length and interception depth o hole length.  If the exclusion of this information is justified on the basi information is not Material and this exclusion does not dunderstanding of the report, the Competent Person show why this is the case.	information for all a level in metres) s that the etract from the
Data aggregation methods	In reporting Exploration Results, weighting averaging tea and/or minimum grade truncations (eg cutting of high gr grades are usually Material and should be stated.	



Criteria	JORC Code explanation	Commentary
	<ul> <li>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</li> <li>The assumptions used for any reporting of metal equivalent values should be clearly stated.</li> </ul>	are reported generally above 5000ppm combined Pb plus Zn. Most of the data set are anomalous as shown by figure 8 where all assays are plotted for Pb vs Zn.
Relationship between mineralisatio n widths and intercept lengths	<ul> <li>These relationships are particularly important in the reporting of Exploration Results.</li> <li>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> <li>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').</li> </ul>	<ul> <li>It is interpreted that these widths approximate true width.</li> <li>The geometry is generally dipping vertically or moderately to the east. It is variable as the mineralised surface approximates a pipe and hence is curved.</li> </ul>
Diagrams	<ul> <li>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</li> </ul>	Reported in Text.
Balanced reporting	<ul> <li>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</li> </ul>	<ul> <li>All drill assay results are reported for Akelikongo. See data aggregation methods above.</li> <li>Soil data that are statistically important are shown (the database comprises more than 60000 samples)</li> </ul>
Other substantive exploration data	<ul> <li>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</li> </ul>	Not applicable
Further work	<ul> <li>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</li> <li>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</li> </ul>	As reported in the text

## Glossary

#### Chalcopyrite

Chalcopyrite is a copper iron sulphide mineral CuFeS<sub>2</sub>.

#### Cumulate

Cumulate rocks are the typical product of precipitation of solid crystals from a fractionating magma chamber. These accumulations typically occur on the floor of the magma chamber. Cumulates are typically found in ultramafic intrusions, in the base of large ultramafic lava tubes in komatiite and magnesium rich basalt flows and also in some granitic intrusions.

#### **Gneiss**

Gneiss is a high grade metamorphic rock, meaning that it has been subjected to higher temperatures and pressures than schist. It is formed by the metamorphosis of granite, or sedimentary rock. Gneiss displays distinct foliation, representing alternating layers composed of different minerals

#### MgO content

Method of mafic and ultramafic rock classification, with high MgO ultramafic rocks generally comprising greater than 25% MgO. The higher the MgO content the more Ni the rock can contain in silicate form with modifying factors up to 3000ppm.

#### Migmatite

Migmatite is a rock that is a mixture of metamorphic rock and igneous rock. It is created when a metamorphic rock such as gneiss partially melts, and then that melt recrystallizes into an igneous rock, creating a mixture of the unmelted metamorphic part with the recrystallized igneous part.

#### Nickel tenor

How much nickel in percentage terms within the sulphides as a percentage of the sulphide. If you have nickel tenor of 6% and you have 50% sulphide then the grade is 3% nickel

#### **Oikocrysts**

Part of the definition of poikilitic texture. Poikilitic texture is a texture in which small, randomly orientated, crystals are enclosed within larger crystals of another mineral. The term is most commonly applied to igneous rock textures. The smaller enclosed crystals are known as chadacrysts, whilst the larger crystals are known as oikocrysts.

#### **Paragneiss**

A metamorphic rock formed in the earth's crust from sedimentary rocks (sandstones and argillaceous schists) that recrystallized in the deep zones of the earth's crust

#### **Pentlandite**

Pentlandite is an iron-nickel sulphide mineral with the formula, (Fe,Ni)<sub>9</sub>S<sub>8</sub>.

#### **Peridotite**

Peridotite is a dense, coarse-grained igneous rock, consisting mostly of the minerals olivine and pyroxene. Peridotite is ultramafic, as the rock contains less than 45% silica.

#### Pyroxenite

Pyroxenite is an ultramafic igneous rock consisting essentially of minerals of the pyroxene group, such as augite and diopside, hypersthene, bronzite or enstatite. They are classified into clinopyroxenites, orthopyroxenites, and websterites which contain both clino and orthopyroxene.

#### **Pvrrhotite**

Pyrrhotite is an iron sulphide mineral with the formula  $Fe_{(1-x)}S$  (x = 0 to 0.2).

#### Xenomelt

Melt of a foreign rock typically the country rock, through which the hot ultramafic magma intrudes, interacts and partially melts and absorbs.