GRUYERE FEASIBILITY STUDY APPROVED

3.5 Moz Ore Reserve – 15 Year Project Life

Highlights

- Feasibility Study confirms Gruyere Gold Project as one of the longest life, lowest cost[1], undeveloped gold deposits in the world
- Updated Ore Reserve of 3.52 million ounces[2], supporting average annual gold production of 270,000 ounces over life-of-mine[3] (LOM) of 13 years, elevating Gold Road into the ranks of Australia's mid-tier gold producers
- Gruyere Open Pit averages more than 9,250 reserve ounces per vertical metre to a final depth of 380 metres
- Development to be based on a single large open-pit mine and conventional SAG/Ball Mill Circuit, gravity/carbon-in-leach plant with throughput of 7.5 Mtpa of fresh ore and up to 8.8 Mtpa of oxide ore
- Study findings indicate a technically sound and financially viable project generating in excess of A$1.2 billion in undiscounted free cash flow (pre-tax, at A$1,500 per ounce gold price) over an initial 15-year Project life[3]
- Total forecast capital cost of A$507 million[4,5] (**US$370 million**[6]) with an additional A$77 million (US$56 million[6]) of sustaining capital over LOM
- Estimated average all-in sustaining cost (**AISC**) of A$945 (US$690[6]) per ounce over LOM with a payback of less than one-third of LOM
- Net Present Value (pre-tax) (**NPV8%**[7]) of A$486 million (US$355 million[6]) and 24% Internal Rate of Return (pre-tax) (**IRR**) (at A$1,500 per ounce gold price)
- NPV8%[8] increases to A$910 million (US$664 million[6]) with 35% IRR at A$1,750 per ounce gold price
- Board approves Feasibility Study and progression to construction on completion of appropriate financing strategy

Gold Road Resources Limited (**Gold Road** or the **Company**) is pleased to announce the completion of the Feasibility Study (**FS**) for the development of its 6.16 million ounce[8] (**Moz**) Gruyere Gold Project (the **Project**), located 200 kilometres east of Laverton in Western Australia. The FS confirms the Project as one of Australia's most significant undeveloped gold deposits with an Ore Reserve in excess of 3.5 Moz over a 13-year Mine Life and a Project Life of 15 years.

ASX Code GOR

ABN 13 109 289 527

COMPANY DIRECTORS

Tim Netscher
Chairman

Ian Murray
Managing Director & CEO

Justin Osborne
Executive Director, Exploration & Growth

Martin Pyle
Non-Executive Director

Sharon Warburton
Non-Executive Director

Kevin Hart
Company Secretary

CONTACT DETAILS

Principal & Registered Office
Level 2, 26 Colin St
West Perth WA 6005

www.goldroad.com.au
perth@goldroad.com.au

T +61 8 9200 1600
F +61 8 9481 6405

[1] Australian Gold Miners – Australian equities in a global context – 10 October 2016, Macquarie Equities Research
[2] See Appendix 3: JORC Code 2012 Table 1 Section 4 page 44
[3] Project Life is duration from Construction to end of Processing. LOM is Mine Life duration of Mining and Processing for gold production
[4] Capital cost estimate is as at Q2 2016, and accuracy level is -10% to +15%
[5] Capital cost estimate includes A$43 million ($US31 million) of contingency, and excludes A$7 million escalation to Q4 2018
[6] A$:US$ exchange rate A$1:US$0.73
[7] 8% discount rate applied
[8] Gruyere Resource Increases to 6.2 Million Ounces (ASX announcement dated 22 April 2016)

The FS indicates a technically sound and financially viable project generating over A$1.2 billion in free cash flow (pre-tax) over the Project life (Table 1). The total forecast capital cost is estimated to be A$507 million[4,5] including a Project contingency of A$43 million. The FS is based on a pit design optimised at A$1,500 per ounce. All base-case financial analyses were completed assuming a A$1,500 per ounce gold price, representing the five-year historic average. Analysis at the more recent spot gold price (A$1,750 per ounce) demonstrates considerable project upside (Table 2 and Figure 1).

Table 1: *Summary of FS Financial Outcomes (all run at A$1,500/oz)*

Measure	Units	FS Outcome A$M	FS Outcome[8] US$M
Gold Produced	koz	3,212	
Gross Revenue	$M	4,817	3,516
Free Cash flow – Pre-Tax	$M	1,222	892
Free Cash flow – Post-Tax	$M	845	617
IRR (Pre-Tax)	%	24.0	
IRR (Post-Tax)	%	19.5	
NPV8% (Pre-Tax)[1]	$M	486	355
NPV8% (Post-Tax)[1]	$M	305	223
C1 Cash Costs[2]	$/oz	858	626
C2 Cash Costs[3]	$/oz	1,040	759
C3 Cash Costs[4]	$/oz	1,093	798
AISC[5]	$/oz	945	690
All in Cost (**AIC**)[6]	$/oz	1,103	805
Development Capital Cost[7]	$M	507	370
Development Capital Cost per ounce (Dev. Capex / Gold Produced)	$/oz	158	115
Capital Efficiency (Pre-Tax NPV/Development Capex)		1.0	
Total Project Payback	Months	48	
Payback: LOM	%	33	
Project LOM Costs[9]	$M	3,542	2,586

Notes:

1. *8% Discount rate applied*
2. *C1 = Mining + Processing Operating Expenditure + Site General and Administration Expenditure + Transport and Refining Costs.*
3. *C2 = C1 + Depreciation + Amortisation*
4. *C3= C2+ Royalties + Levies + Net Interest Costs*
5. *AISC = C1 + Royalties + Levies + Sustaining Capital + Project related offsite Corporate expenditure*
6. *AIC = AISC + Development Capital Expenditure*
7. *The Development Capital Cost is in Q2 2016 (FS) Real terms. The forecast capital cost including potential escalation of A$7 million to Project completion (Q4 2018) is estimated to be A$514M*
8. *A$:US$ exchange rate A$1:US$0.73*
9. *Excludes mine site closure costs of $54 million*

Completion of the positive FS allows the Company to declare an updated Ore Reserve for Gruyere of 3.52 Moz[9], which supports an average annualised gold production of 270,000 ounces over the LOM. Production at this rate would elevate Gold Road into the ranks of Australia's mid-tier gold producers.

Based on the positive FS outcome, the Gold Road Board has approved the FS and recommends progressing the Project to the construction phase pending successful completion of financing activities. The Company is in the final stages of assessing whether to opt for a combination of debt and equity arrangements or a Joint Venture with a third-party corporation. Project Finance discussions with a number of Australian and International Banking groups commenced in March 2016. The process is now well advanced and the Company is confident of receiving Credit Approved terms supporting a significant debt facility before the end of the year.

[9] See Appendix 3: JORC Code 2012 Table 1 Section 4 page 44

Parallel Joint Venture discussions have also been had with a select number of Australian and International gold mining companies since 2015. These talks are similarly well advanced and provide the Company with a number of potentially viable and attractive funding options.

Given the Company's strong financial position[10], the final financing decisions will be made at a time deemed most appropriate and beneficial to the Gold Road shareholder base.

The FS was compiled with the assistance of a number of independent, reputable and predominantly Western Australian-based engineering companies as well as other industry experts and qualified Gold Road personnel.

The FS has been evaluated at a A$1,500 per ounce gold price, representing the average price over the last five years. During the period of the FS the Australian dollar gold price traded between a low of A$1,592 to a high of A$1,839[11] per ounce, at an average price of A$1,717 per ounce, with the price above A$1,700 for 65% of the FS period. The Project is highly leveraged to the gold price, as identified in Table 2 below which displays the potential financial performance at a gold price of A$1,750 per ounce. At this price, the Project generates an additional A$777 million (+63.6%) in pre-tax cash flows while the NPV almost doubles (+87.2%). Figure 1 also illustrates the potential uplift in EBITDA generated by a A$1,750 per ounce gold price compared to A$1,500 per ounce over the life of the Project. This price compares favourably with the Company's existing modest hedging position of 50,000 ounces with a forward price of A$1,792 per ounce already secured for the Project.[12]

Table 2: *Summary of FS Key Financial Outcomes and Sensitivities – October 2016*

Measure	Units	FS Investment Case (A$1,500/oz)		FS Upside (A$1,750/oz)	
		A$	US$	A$	US$
Free Cash flow – Pre-Tax	$M	**1,222**	**892**	1,999	1,459
Free Cash flow – Post-Tax	$M	**845**	**617**	1,389	1,014
IRR (Pre-Tax)	%	**24**		35	
IRR (Post-Tax)	%	**19.5**		28.5	
NPV8% (Pre-Tax)	$M	**486**	**355**	910	665
NPV8% (Post-Tax)	$M	**305**	**223**	602	440
NPV5% (Pre-Tax)	$M	692	505	1,217	889
NPV5% (Post-Tax)	$M	457	334	825	602

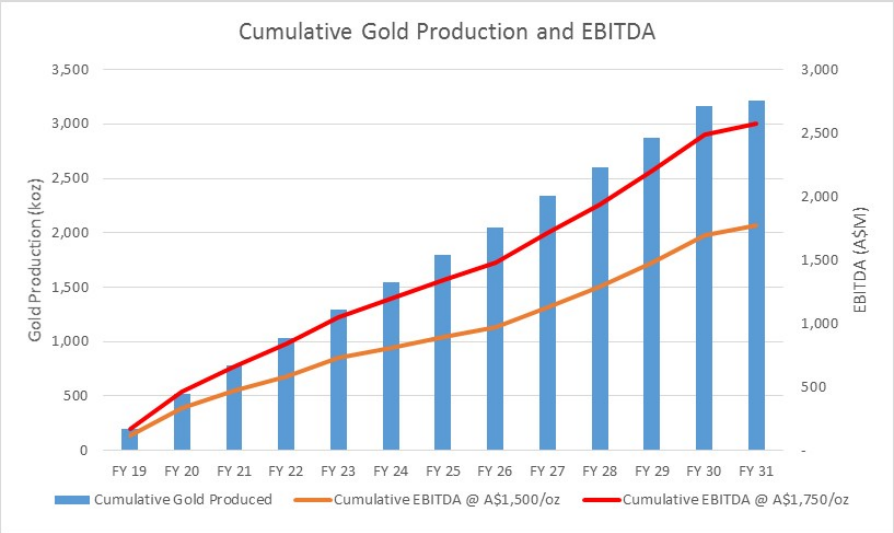


Figure 1: *Annual EBITDA (A$1,500/oz and showing increment to A$1,750/oz) versus AISC (A$/oz)*

[10] Cash on hand at 30 June 2016 of A$90 million

[11] A$ gold price as intraday bid asking price from Perth Mint records for the period 8 February to 30 September 2016

[12] Refer to ASX Announcement 1 September 2016

Ore Reserve[13]

On the basis of the completed FS Gold Road has updated the Ore Reserve for the Project from the previous Ore Reserve announced on completion of the PFS[14]. Set out below is a summary of the key information material to understanding the reported Ore Reserve. A summary of the FS key information, including material information for the Ore Reserve, is provided in the body of this release. Additional details of the material assumptions are set out in Appendix 3 (JORC 2012 Table 1).

Gold Road intends to publish a full and complete Technical Report, being compiled by Behre Dolbear Australia (**BDA**), to complement the Feasibility Study. The BDA report will provide technical data on the FS and is planned to be released to the ASX within four weeks of this current release.

Overview of the Ore Reserve

The Ore Reserve for the Project was reported according to the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (the JORC 2012 Code). The Ore Reserve was estimated from the Mineral Resource after consideration of the level of confidence in the Mineral Resource and taking account of material and relevant modifying factors. The Proved Ore Reserve estimate is based on Mineral Resource classified as Measured. The Probable Ore Reserve estimate is based on Mineral Resource classified as Indicated. No Inferred Mineral Resources have been included in the Ore Reserve.

Table 3 presents a summary of the Ore Reserves on a 100% Project basis at a A$1,500 per ounce gold price (US$1,095 per ounce at US$0.73:A$1.00).

Table 3: *Ore Reserves Statement*

Ore Reserve Category	Tonnes (Mt)	Grade (g/t Au)	Contained Gold (Moz)
Proved	14.9	1.09	0.52
Probable	76.7	1.22	3.00
Total Ore Reserve	**91.6**	**1.20**	**3.52**

Notes:

1. *The Ore Reserve conforms with and uses the JORC 2012 Code definitions*
2. *The Ore Reserve is evaluated using a gold price of A$1,500/oz*
3. *The Ore Reserve is evaluated using variable cut off grades: Oxide 0.35 g/t Au, Transitional 0.39 g/t Au and Fresh 0.43 g/t Au*
4. *Ore block tonnage dilution averages 3.2%; Ore block gold loss is estimated at 1.4%*
5. *All figures are rounded to reflect appropriate levels of confidence*
6. *Apparent differences may occur due to rounding*
7. *A total of 407 kt at 0.87 g/t Au for 11.4 koz at 0.5 g/t Au cut-off of Inferred Mineral Resource associated with the dispersion blanket Domain is contained within the FS pit design (with the majority located within Stage 2). This oxide material has not been included in the optimisation, the Ore Reserve estimate nor the FS processing schedule and presents potential upside subject to further definition with RC drilling*

[13] See Appendix 3: JORC Code 2012 Table 1 Section 4 page 44

[14] Gruyere Pre-Feasibility Study Confirms Long Life Gold Mine (ASX announcement dated 8 February 2016)

Pursuant to ASX listing Rule 5.9.1, and in addition to the information contained in the body of this release and in Appendix 3 of this release, the Company provides the following summary (Table 4):

Table 4: *Ore Reserves Material Assumptions*

Material Assumption	Outcome
Mineral Resources (Page 14 and Appendix 4)	The Mineral Resource estimate (refer ASX announcement 22 April 2016 and republished Appendix 4: JORC Code 2012 Table 1 Sections 1 to 3 page 53 in this announcement) for the Gruyere deposit which formed the basis of this Ore Reserve estimate was compiled by the Gold Road Competent Person(s). The estimate is based on 357 Reverse Circulation (RC) holes and 113 diamond holes and associated assay data. The data set, geological interpretation and model was validated using Gold Road's internal processes. An external review was completed by Ian Glacken (Director - Geology at Optiro consultants) who is satisfied that the Mineral Resource estimate has been reported and classified according to the guidelines set out in the JORC Code (2012) and in line with good to best industry practice. The Mineral Resources are reported inclusive of the Ore Reserve.
Mining Method and Assumptions (Page 15-19 and Appendix 3)	Gruyere will be mined by open pit mining methods utilising conventional mining equipment. The final pit design is the basis of the Ore Reserve estimate. The selected mining method, design and extraction sequence are tailored to suit orebody characteristics, minimise dilution and ore loss, defer waste movement and capital expenditure, utilise proposed process plant capacity and expedite free cash generation in a safe and environmentally sustainable manner. Mining operating and capital costs were estimated as part of the FS and referenced against contractor budget quotes. The open pit design(s) are based on the recommended geotechnical design parameters and assume dry slopes on the basis of adequate dewatering ahead of mining.
Processing Method and Assumptions (Page 20-23 and Appendix 3)	A single stage primary crush, Semi Autogenous Grinding and Ball Milling with Pebble Crushing (SABC) comminution circuit followed by a conventional gravity and carbon in leach (CIL) process is proposed. This process is considered appropriate for the Gruyere ore (which is classified as free-milling) and is commonly used in the Australian and international gold mining industry. Estimated plant gold recovery ranges from 87% to 95% depending on head grade, plant throughput, grind size and ore type. The values are based on significant comminution, extraction, and materials handling test work. No deleterious elements of significance have been determined from metallurgical test work and mineralogy investigations.
Cut-off Grades (Page 44 and Appendix 3)	Variable economic cut-off grades have been applied in estimating the Ore Reserve. Cut-off grade is calculated in consideration of the following parameters; gold price, operating costs, process recovery, transport and refining costs, general and administrative cost and royalty costs. The Ore Reserve is evaluated using variable cut off grades: Oxide 0.35 g/t Au, Transitional 0.39 g/t Au and Fresh 0.43 g/t Au.
Estimation Methodology (Appendix 4)	Ordinary Kriging was utilised to estimate the Measured component of the Mineral Resource and Localised Uniform Conditioning was utilised to estimate the Indicated and Inferred components of the Mineral Resource.
Material Modifying factors (Page 16 and Appendix 3)	Mining dilution and recovery modifying factors were simulated by modelling to a Selective Mining Unit (SMU) which represents the capability of the selected mining fleet. The modelling yielded the following results; mining tonnage dilution factor of 3.2%, mining grade dilution of 4.6% and mining recovery factor of 98.6%. These values reflect the continuity of the orebody with individual ore shape designs hundreds of metres along strike by 20 m to +50 m wide.

Commentary

Gold Road's Managing Director and CEO, Ian Murray said: *"Since the competion of the initial Scoping Study in 2015, a significant amount of work has been invested in the Gruyere Project Studies, culminating in this impressive Feasibility Study. The very thorough and high quality work delivered by the Owner's team is self evident as is the economic strength of the Project, with its demonstrated low costs, strong cashflows and rapid payback. This has all been achieved at a World-leading Reserve discovery cost of less than A$10 per ounce.*

While the Feasibility Study suggests a substantial Project life, the demonstrated exploration potential of Gruyere and the surrounding Yamarna region means that there is significant potential to extend the life beyond the current 15 years. Mineral Resources have previously been estimated for the Central Bore and Atilla-Alaric trends. None of this potential upside has been included in the scope of the Feasibility Study.

Again, we thank the Traditional Owners for their support in the work that we have undertaken on-country. We look forward to progressing the Gruyere Gold Project in a manner that cares for country and creates an enduring benefit for all involved.

We expect to be in a position to complete the funding aspects for the Project and make the associated investment decision in early 2017. It fills me with great pride to deliver, on behalf of our team, a 15-year Project within three years of its original discovery."

For further information please visit www.goldroad.com.au or contact:

Gold Road Resources
Ian Murray
Managing Director & CEO
Telephone: +61 8 9200 1600

Media and Broker Enquiries
Luke Forrestal
lforrestal@canningspurple.com.au
Cannings Purple
Telephone: +61 411 479 144

CONTENTS

Introduction

The Gruyere Gold Project is located within the Yamarna Greenstone Belt, approximately 200 kilometres east of Laverton in Western Australia. The Project can be accessed by road, via the Great Central Road, and by air (Figure 2). Gold Road holds an exploration tenement package of approximately 5,000 square kilometres in the area, of which approximately 2,900 square kilometres is covered by a joint venture agreement with Sumitomo Metal Mining Oceania Pty Ltd, (a subsidiary of Sumitomo Metal Mining Co., Limited), which has earned a 50% interest in the JV tenement holdings (Figure 20).

The Gruyere Deposit is situated on Mining Lease M38/1267, granted on 5 May 2016, which is 100% owned by Gold Road. The Mining Lease secures tenure over the Project for a period of 21 years (from the date of grant), renewable for a further period of 21 years. Planned infrastructure for the Project will be sited on an additional 14 Miscellaneous Licences which have been granted or are under application. Gold Road also owns the Yamarna Pastoral Lease within which the Gruyere Mining Lease and majority of project infrastructure will be located. The Pastoral Lease is surrounded by the Cosmo Newberry Aboriginal Reserves (numbers 25051, 22032, 25050 and 20396).

Tenure required for the Project is subject to the *Native Title Act 1993*. On 3 May 2016 Gold Road reached agreement on the Gruyere-Central Bore Native Title Agreement (**GCBNTA**), which allowed the Department of Mines and Petroleum (**DMP**) to grant the Mining Lease (M38/1267). The GCBNTA covers mining and infrastructure tenements associated with the Gruyere Gold Project, as well as granted mining leases over additional Mineral Resources at Central Bore and Attila-Alaric which do not form a part of the Gruyere Project FS.

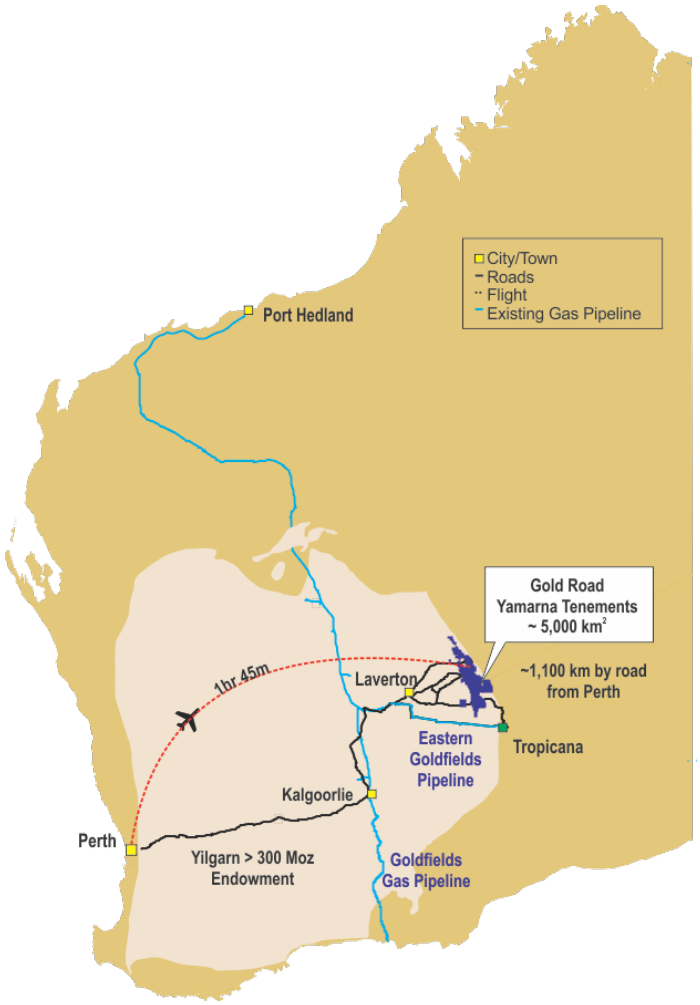


***Figure 2**: Location of Gold Road tenements relative to major cities, towns and relevant infrastructure within the Yilgarn Craton.*

Study Parameters

The FS is based on the following key parameters:

- JORC 2012 Code compliant Gruyere Mineral Resource of 147.71 Mt at 1.30 g/t Au, which at a 0.5 g/t Au cut-off grade equates to 6.16 Moz of gold and constrained within a A$1,700 per ounce optimised pit shell
- Open pit earthmoving mining operations conducted by Tier 1 mining contractors
- Process plant and infrastructure built under an Engineering, Procurement and Construction (**EPC**) contract and Owner operated / managed
- Power supply under a Build-Own-Operate (**BOO**) contract for a 40 MW gas-fired power station with the fuel supplied by gas pipeline
- Two water borefields (Yeo and Anne Beadell) identified to provide sufficient process and potable water beyond the life of the Project with a contingency borefield to draw on if required
- Management of project implementation by the Gold Road Owner's team (**Owner's team**) on a small number of large contracts.

Study Team

The FS commenced immediately after completion of the PFS in February 2016 and has been managed by the Owner's team working in conjunction with several specialised consultants as listed below to complete studies on all aspects of the Project. The FS was limited to investigating the technical and economic viability of an open pit operation. The FS was also limited to processing ore from the Gruyere deposit only and excluded the potential of processing ores from other regional ore bodies (apart from design of the layout of the ROM pad where consideration has been made for future haulage access).

Contributing consultants were as follows:

- GR Engineering Services Limited (**GRES**) – Process plant, associated infrastructure
- AMC Consultants Pty Ltd (**AMC**) – Mine planning and optimisation, Ore Reserve Statement and peer review of mine geotechnical engineering
- Dempers and Seymour Pty Ltd – Geotechnical engineering
- Optiro Mining Consultants (**Optiro**) – Third party review of Mineral Resource
- Orelogy – Third Party Review of Mining Study
- Axiom Project Services (**Axiom**) – Third party review of capital cost estimates and execution schedule
- MBS Environmental (**MBS**) – Environmental surveys and environmental approval documents
- Pennington Scott – Hydrogeology
- KPMG – Assistance with Operational Readiness
- PCF Capital – Financial modelling
- Coffey Mining Ltd (**Coffey**) – Tailings Storage Facility
- ALS Laboratories – Metallurgical testwork
- Gekko Systems – Gravity testwork
- Jenike & Johanson – Materials handling testwork
- Aquatech – Water bore drilling

- Aerodrome Management Services (**AMS**) Pty Ltd – Gruyere airstrip design
- Shawmac Pty Ltd – Access road design
- Wayne Trumble – Power supply
- Broadleaf Capital International – Cost and Schedule Risk Analysis

Key Outcomes of the Feasibility Study

Key FS outcomes for the Project, by comparison with the Pre-Feasibility Study (**PFS**) completed in February 2016, are included in Table 5. The estimated Ore Reserve constitutes 100% of the production target, and has been prepared by Competent Persons in accordance with JORC Code 2012[15].

Table 5: *Summary of FS Key Outcomes (compared with the PFS released 8 February 2016)*

Key Outcomes	Feasibility Study 7.5 – 8.8 Mtpa[16]	*Pre-Feasibility Study 7.5 – 8.8 Mtpa[17]*
Project Life (years)	**15**	*13*
Project Processing Life (years)	**13**	*11*
Stripping Ratio (waste:ore) (including pre-strip)	**2.8:1**	*3.0:1*
Stripping Ratio (waste:ore) (excluding pre-strip)	**2.7:1**	*2.9:1*
Final Pit Depth (m)	**380**	*340*
Gold Mined (Moz)	**3.52**	*3.16*
Average Gold ounces per Vertical Metre (OVM)	**9,260**	*9,300*
Gold Recovered (Moz)	**3.21**	*2.92*
Annualised Gold Production (average koz pa)	**270**	*265*
Grind Size P_{80} (µm)	**125**	*125*
Metallurgical Recovery (%)	**91 - 94**	*91 - 93*
Capital Cost (CAPEX) (A$M)	**507-514*^**	*455 – 470*^*
Sustaining Capital (Susex) (A$M)	**77^**	*141^*
Total LOM Capital Expenditure (A$M)	**584-591^**	*596-611^*
Total LOM Capital Expenditure per ounce recovered (A$/oz)	**182-184**	*205-211*
Mining Cost (A$/tonne ore delivered)	**13.40****	*13.70*
Processing Cost (A$/tonne ore)	**15.65**	*15.90*

Notes:

** This includes potential cost escalation to 2018 of A$7M which results in the total A$514M*

^ The capital cost estimate accuracy is -10% /+15% for FS and -15% /+25% for PFS

*** The FS unit mining cost at surface is ~A$3.12/t mined. The average mining cost increases by ~A$0.06/t per 10m bench over LOM. The LOM average mining operating cost is ~A$3.56/t mined*

The FS tonnage throughput range of 7.5 to 8.8 Mtpa reflects the variation in weathering of process plant feed material from the open pit. Softer oxide and transitional material mined in the early years of LOM will be processed at the higher rates. Fresh material, which represents more than 80% of material mined, will be processed at an annualised rate of 7.5 Mtpa. Key differences between the PFS and FS reflect a deeper open pit with a slightly lower stripping ratio which is driven by steeper pit wall slope angles, and results in an increase in gold mined and recovered, as well as lower mining costs.

The gold price used to calculate the Mineral Resource estimate was A$1,700 per ounce, while A$1,500 per ounce was used to calculate the Ore Reserve estimate. The financial modeling gold price was set at A$1,500 per ounce.

[15] See Appendix 3: JORC Code 2012 Table 1 Section 4 page 44
[16] See Appendix 1: Forward-Looking and Cautionary Statements on page 40
[17] See Appendix 1: Forward-Looking and Cautionary Statements on page 40

All of the material to be processed is classified as Proved and Probable Ore Reserve. No material classified as Inferred Mineral Resource is included in the Ore Reserve Estimate or processing schedule.

The key changes from the PFS to the FS are as follows:

- The FS was based on the updated Mineral Resource[18]
- Estimated plant gold recovery for the oxide ore (including saprock) has increased from 93% in the PFS to 94% in the FS based on additional testwork including bulk leach testwork carried out during the FS
- Increased pit wall slope angle on average 3 to 5 degrees steeper in the FS, contributing to an increased Ore Reserve and total mined tonnage, at a lower strip ratio
- "Adaptive Aquifer Management" of the Yeo Borefield was introduced to mitigate the impact on the stygofauna habitat by extending the potential design length of the Yeo Palaeochannel bores from 65 kilometres to 80 kilometres. The FS design increased access tracks, water pipelines and powerlines by approximately 7 kilometres to 65 kilometres
- The construction and permanent accommodation villages were combined into a single village, and the total number of rooms increased from 500 to 600 based on the FS estimated peak workforce
- The total Capital Expenditure estimate (excluding escalation but including contingency) has increased from A$455 million to A$507 million[19], which is largely due to expansion of the borefields and accommodation village mentioned above
- Potential escalation cost on capital to Q4 2018 decreased from A$15 million to A$7 million
- The total Sustaining Capital Expenditure decreased from A$141 million to A$77 million due largely to costing the mining of cover overburden to operating rather than Sustaining Capital
- The methodology to capitalise mining costs associated with the establishment of mining and processing prior to the commencement of gold production was changed to better align with accounting reporting standards. This resulted in the reduction of Sustaining Capital and operating costs in the first year of production and an increase in Capital Expenditure
- Increased loading (250 tonne to 360 tonne class excavators) and hauling (135 tonne to 180 tonne trucks) equipment size in FS to provide economies of scale
- Approximately 30% of total drill and blast is on 5 metre bench height (all ore zones) in FS instead of 10 metre bench height (in PFS), which increased drill and blast costs
- Reduced material movement in the first six years in FS corresponds with anticipated debt repayment period.

[18] Refer ASX announcement dated 22 April 2016

[19] Capital cost estimate is as at Q2 2016, and accuracy level is -10% to +15%

Project Approvals

The Project was referred to the Office of the Environmental Protection Authority (**OEPA**) during the FS and received a determination of API-A level of assessment under Part IV of the EP Act on 20 June 2016. This level of assessment from the OEPA means that the Project can proceed with the formal environmental applications and assessment without requiring a public environmental review. The final approval applications were submitted in October 2016.

The gas pipeline project was referred to the OEPA during the FS and on 18 July 2016 the OEPA determined the level of assessment being "not to be assessed under Part IV of the EP Act (No Appeals)". This level of assessment means the OEPA has recommended that the DMP manage the environmental approvals of the gas pipeline project.

Gold Road continues to work closely with all stakeholders to complete all formal environmental assessments and development approvals in accordance with Part IV of the EP Act and the *Mining Act 1978*. Progress on the environmental studies and the required approvals as part of the Native Title and Aboriginal heritage interests in the Project continue, together with conceptual closure planning.

Native Title and Aboriginal heritage aspects within the Project area were addressed by working with the registered native title claim group, Yilka, resulting in the GCBNTA being signed on 3 May 2016 and the subsequent Mining Lease, M38/1267, being granted on 5 May 2016.

On 29 June 2016, the Federal Court delivered a judgment in which native title was determined to exist over areas in which the Company has an interest as a result of native title claims brought by the registered Yilka native title claim group and the unregistered Sullivan and Edwards native title claim group. The final form of the determination, including the description of the native title holding community, is yet to be settled by the Federal Court. The Yilka native title claim group are obliged to procure the accession of all persons in the same native title holding community, which the Company considers includes the Sullivan and Edwards native title claim group, to the Company's Native Title Agreement in respect of the Gruyere, Central Bore, Attila and Alaric projects.

Until the final form of the determination is made by the Federal Court, the Company is unable to ascertain the effect of the judgment, if any, on the Company or its interests, including its Native Title Agreement with the Yilka native title claim group and any potential impact on the Project.

A work programme for the remainder of 2016 has been developed to complete all remaining environmental baseline studies and archaeological surveys and compile approval documents for submission in the December 2016 quarter so that assessment is completed by regulators in the March 2017 quarter.

Company Standards

Gold Road is committed to the development of the Project in a manner that benefits its shareholders, employees, contractors, suppliers, partners and the community.

Gold Road aims to achieve the best practice standards of environmental care in carrying out its exploration and mining activities. In order to achieve this the Company will:

- Fully comply with all laws, statutory regulations and standards with regard to the environment
- Minimise the effect that the Company's activities have on the environment and communities in which it operates, through diligent environmental planning, proper operating procedures and responsible rehabilitation programmes
- Ensure that employees and contractors are informed about and comply with or exceed Gold Road's standards and expectations
- Regularly review and audit the Company's standards and requirements with regard to environmental issues and continuously strive to achieve the highest standard of environmental care.

Gold Road also:

- Supports standard industry practices and responsible behaviour throughout the Project development and operation phases
- Seeks to maximise positive social impacts in areas relating to the Project and to avoid any negative impacts resulting from its activities
- Will work to ensure that operations contribute to the implementation of relevant local and regional development plans.

Project Execution

The Project development and execution will be managed by the Owner's team appropriately resourced to oversee the execution of the design, construction, commissioning and handover to operations. An Operational Readiness Plan, as part of the Whole of Business Framework, has been developed to ensure that Gold Road will have all the systems, standards and procedures in place and an operations team recruited, trained and ready to accept care, custody and control of the Project assets when handed over by the development team.

A Contracting Strategy has been developed to support the Project Execution Strategy which is based around an EPC contract model that delivers the design, engineering, construction and commissioning of the process plant and associated infrastructure. The Contracting Strategy aims to minimise the number of interfaces between contractors on the Project site. A Contracts Responsibility Matrix has been developed mapping the internal ownership of each contract development and award process, the management and administration, and the transitioning of the contracts into operations.

The Contract Tender process for the EPC, Bulk Earthworks, and Power Supply contracts has already commenced. It is anticipated these three major contracts will be ready for award in the December 2016 quarter.

The Project Execution Schedule is based on a five-month early works programme followed immediately by a 24-month construction and commissioning timeframe with the objective of achieving first gold production by the end of 2018. The Project Execution Strategy is based on Project Finance in place and Project Approval in March 2017 quarter.

Mineral Resource[20]

The Mineral Resource estimate for Gruyere has been reported and classified according to the guidelines set out in the JORC Code (2012) and is summarised in Table 6 below. Approximately 70% (4.31 Moz) of the Mineral Resource is in Measured and Indicated categories. The Mineral Resource includes 13.86 million tonnes at 1.18 g/t Au for 0.53 million ounces in the Measured Resource category, which represents 9% of the total resource metal, and is located in the upper 100 metres of the deposit. This represents approximately the first two years of production with only minimal additional grade control drilling being required.

The Mineral Resource is based on 357 RC holes for 41,264 metres and 113 diamond holes for 31,109 metres (including 14,694 metres of RC pre-collars) for a total of 87,066 metres drilled since the discovery in October 2013. The Mineral Resource estimate was constrained by an optimised pit shell to determine the portion of the total mineralised inventory within the geological model that has a reasonable prospect of eventual economic extraction. The optimisation utilised mining, geotechnical and processing parameters derived from the PFS, a A$1,700 per ounce gold price constraining pit shell, and is reported at a 0.5 g/t Au cut-off.

Table 6: *JORC Code 2012 Mineral Resource for Gruyere Project – April 2016*

Gruyere Project Mineral Resource Classification	Tonnes (Mt)	Grade (g/t Au)	Contained Metal (Moz Au)
Measured	13.86	1.18	0.53
Indicated	91.12	1.29	3.79
Measured and Indicated	**104.98**	**1.28**	**4.31**
Inferred	42.73	1.35	1.85
Gruyere Mineral Resource (0.5 g/t Au cut-off grade)	**147.71**	**1.30**	**6.16**

Notes:

1. *Mineral Resource conforms with and uses JORC Code 2012 definitions*
2. *Mineral Resource is estimated using a 0.5 g/t Au cut-off*
3. *Resource constrained within a A$1,700 optimised pit shell*
4. *All figures are rounded to reflect appropriate levels of confidence*
5. *Apparent differences may occur due to rounding*
6. *Refer ASX announcement dated 22 April 2016*

Geotechnical Assessment

Geotechnical studies were completed by consultant Dempers and Seymour. Information added to the study since completion of the PFS included more than 3,000 metres of targeted geotechnical diamond drilling, extra downhole optical and acoustic televiewer data, and new geotechnical and structural logging information.

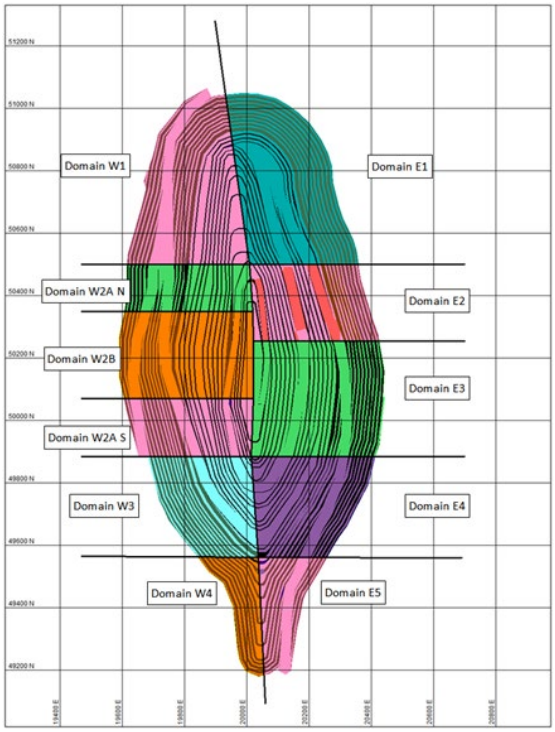
Summary conclusions of the study include:

- The rock mass is classified as Fair to Good and comprises dominant east dipping, sub-vertical foliation and low angle joints
- The oxide profile averages 40 metres in thickness but is variable from 5 to 77 metres which requires shallower pit slope angles
- The transitional profile averages 35 metres in thickness varying from 9 to 85 metres. The profile is highly fractured and has zones of highly weathered rock within good zones of transitional rock
- A 5 to 10 metre thick fault zone contiguous with the western wall which will impact on wall stability and requires mitigating design features to be incorporated into pit designs.

[20] Refer ASX announcement dated 22 April 2016 and Appendix 4: JORC Code 2012 Table 1 Sections 1 to 3 page 53

The ultimate FS pit and interim cutbacks were designed using a set of final pit slope configuration parameters unique for 11 separate geotechnical domains (Table 7). All pits were assessed for overall stability using numerical modelling techniques and conform to recommended factors of safety.

Table 7: *Summary Design Slope Angles by Geotechnical Domain and Final Pit Design*

Pit Wall	Geotechnical Domain	Material	Overall Slope Angle (°)	Pit Geotechnical Illustrated Domains on Final Pit Design
West Wall	W1	Weathered Fresh	38 49	
	W2A N	Weathered Fresh	41 55	
	W2B	Weathered Fresh	41 47	
	W2A S	Weathered Fresh	41 55	
	W3	Weathered Fresh	41 53	
	W4	Weathered Fresh	39 60	
East Wall	E1	Weathered Fresh	38 53	
	E2	Weathered Fresh	41 57	
	E3	Weathered Fresh	40 52	
	E4	Weathered Fresh	44 55	
	E5	Weathered Fresh	40 46	

Open Pit Mining

Mining activities will be conducted by a mining contractor with technical and managerial direction provided by Gold Road. The proposed mine operations model offers the Company the following advantages:

- Minimisation of upfront capex requirements by Gold Road
- Application of contractors' specialised open pit mining knowledge, systems and experience lowering operational risk.

The general mining method is summarised as follows:

- Clearing and stripping of suitable material from all disturbed areas into discrete stockpiles
- Drilling and blasting of ore and associated internal waste on 5 metre benches, while bulk waste which is outside the ore envelope is blasted on 10 metre benches
- Load and Haul utilising 360 tonne excavators and 180 tonne capacity haul trucks mining on 3 metre high flitches in ore zones and 3 to 4 metre high flitches in bulk waste zones
- Ore will be direct fed to the crusher or placed on stockpiles for future rehandle as required
- Pit dewatering is expected to be minimal and will be managed by a collection of external dewatering and depressurising bores and in-pit sumps for use within the mining operation
- RC grade control will be provided by a sub-contractor on a predominantly 25 metre by 25 metre RC drill pattern, and is campaigned during the mine life.

Open pit optimisation studies to identify the mineralised material inventory to guide final pit designs utilised a set of cost, processing and design criteria based on most up to date parameters. The final optimisation parameters are tabulated below (Table 8). There are some minor changes in the Mining Loss and Dilution factors from those reported in the PFS due to a difference in the methodology used in the FS.

Table 8: *Open Pit Optimisation Parameters*

Parameter	Units	Value	Source
Reference Gold Price	A$/oz	1,500	Gold Road
Gold Price	US$/oz	1,095	Gold Road
Exchange Rate	A$/US$	0.73	Gold Road
Transport and Refining Costs	A$/oz	1.60	Gold refinery/Gold Road
Process Gold Recovery – Oxide Ore	%	93	Metallurgical test work via Gold Road
Process Gold Recovery – Transitional Ore	%	92	
Process Gold Recovery – Fresh Ore	%	89% (0.6 g/t Au) to 92% (1.7 g/t Au) Based on grade vs recovery regression calculation	
Processing Cost – Oxide Ore	A$/t	13.72	Process engineering consultant via Gold Road
Processing Cost – Transitional Ore	A$/t	15.06	
Processing Cost – Fresh Ore	A$/t	16.07	
ROM Ore Rehandle Cost	A$/t	0.26	PFS
Grade Control	A$/t	0.05	Gold Road
General and Administration Costs	A$/t	1.08	Gold Road
Rehabilitation	A$/t	0.04	Benchmark
Mining Tonnage Dilution	%	3.2%	AMC
Mining Ore Loss	%	1.4%	AMC
Reference Mining Cost – Fresh Rock	A$/t	3.12	Mining contractor quote
Mining Cost Adjustment per 10m Bench - Fresh Rock	A$/t	0.06	
Overall Slope Angle		Varies by rock type by depth Oxide 38°-42° Fresh 38°-57°	Geotechnical consultant

Note: *Optimisation Parameters may differ from final FS Study outcomes due to timing*

Optimisation results demonstrate the Gruyere Deposit to be relatively insensitive to minor changes in input parameters which results in multiple potential pit shells generating similar cash flow outcomes. This allowed Gold Road the flexibility to select a final pit which satisfied a range of strategic hurdles.

The optimal pit shell selected as the guide to design the final pit was chosen for the following reasons:

- Satisfied Gold Road's strategic cost target of an operating cost of A$850 per ounce before amortisation, royalties and sustaining capital which was estimated to represent an all in cost of approximately A$1,100 per ounce
- The incremental operating cost increase to the next pit shell was above a desired maximum target of A$1,200 per ounce, resulting in larger shells presented diminishing returns. This effectively means the final pit can be designed to a maximum A$1,200 per ounce gold price
- The selected shell produced 98% of the discounted best value of the A$1,500 per ounce reference shell with only 77% of the total pit size (total rock movement). This effectively means the pit produces almost full value (-2%) for 23% less total material movement.

The open pit design process considered multiple pit stages and ramp access to the bottom of the pit subject to geotechnical recommendations and mining fleet requirements. The selection of interim pit shells was guided by the objective of maximising cash flows in the initial years of operation with due consideration for practical mining parameters. The final FS pit has been designed to be mined in four stages (Figure 3). Stages 1 and 2 comprise two independent pits, one in the northern end of the deposit and the other in the southern end. Stage 3 will combine the two starter pits and Stage 4 will cut back to the Final Pit Design (Figures 3 to 5). The Stage designs were prepared utilising optimum ramp exit points for waste material to ensure optimal haulage distances are maintained through the life of the mine.

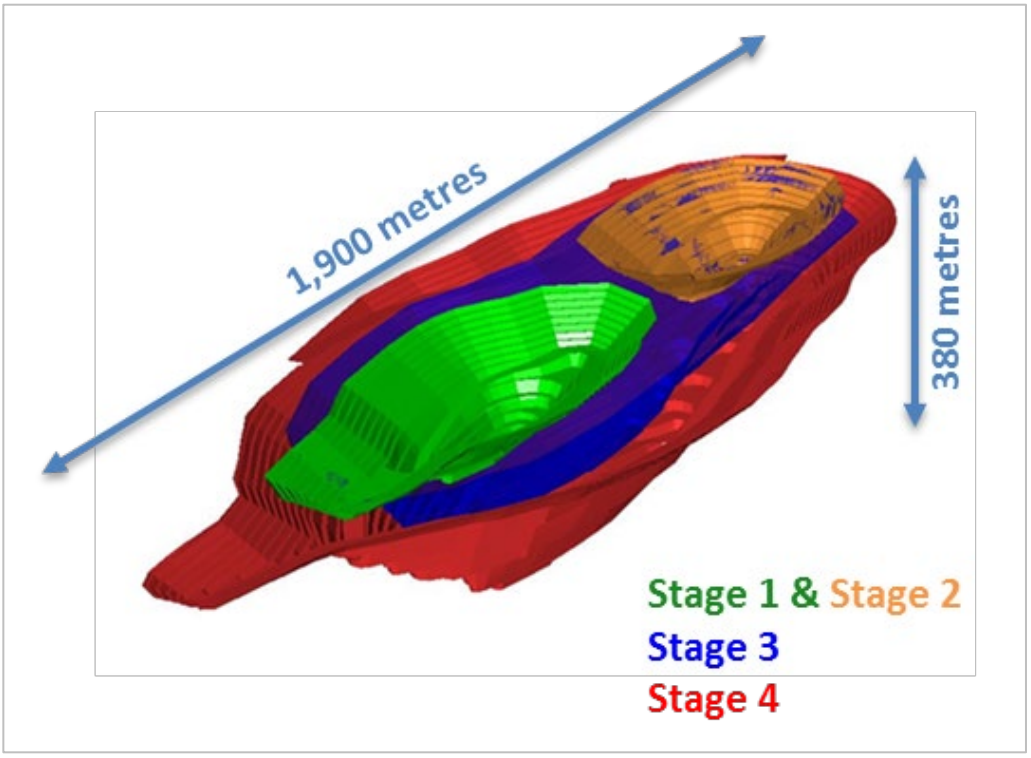


***Figure 3**: Three-dimensional isometric view to north-west illustrating 4 stage pit design for Gruyere Project*

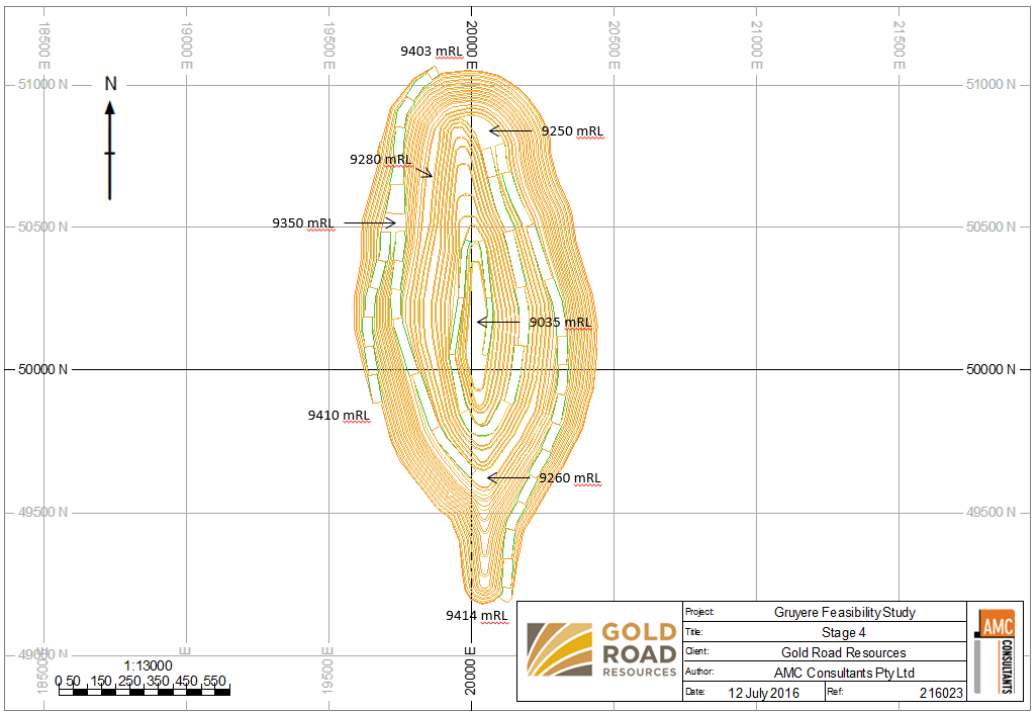


***Figure 4:** Plan view showing Stage 4 which will be the Final Pit Design*

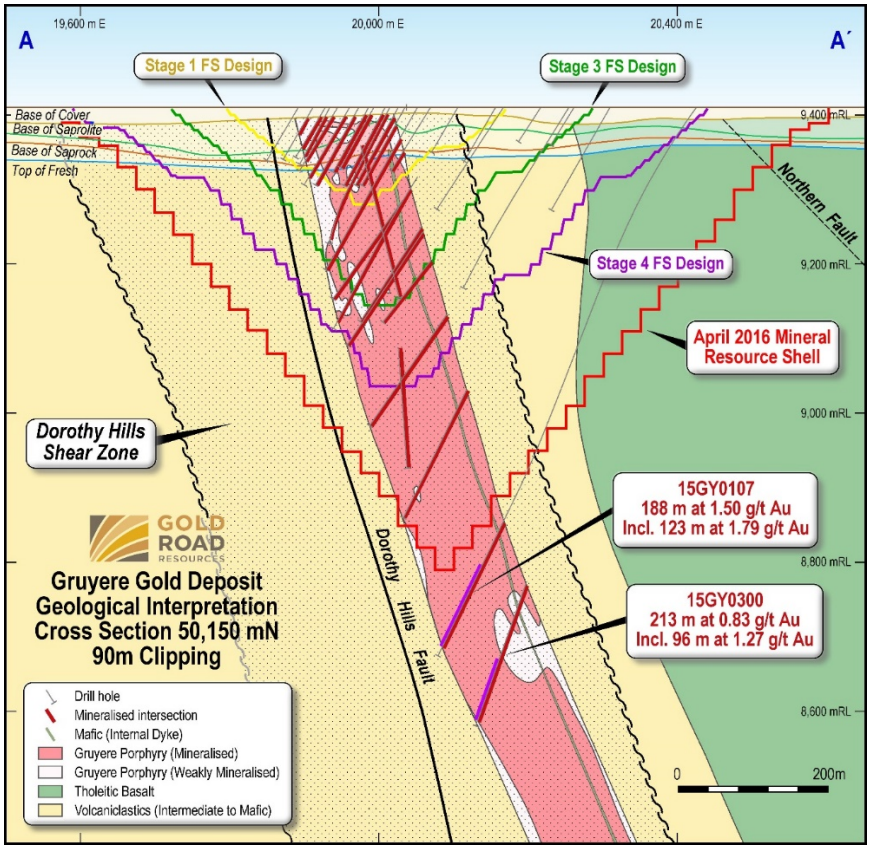


Figure 5: *Cross Sectional View (50,075N) showing FS Pit Stages, Resource Shell and Geology*

Mining Infrastructure

The design and operating strategy for mining infrastructure focussed on optimising development capital and operating costs whilst minimising environmental impacts. This is achieved by minimising haul lengths to the ROM pad and dumps where possible. Sterilisation drilling, waste rock characterisation and waste material movement optimisation studies have been conducted as part of the FS. Final Mine Site layouts are illustrated in Figure 6.

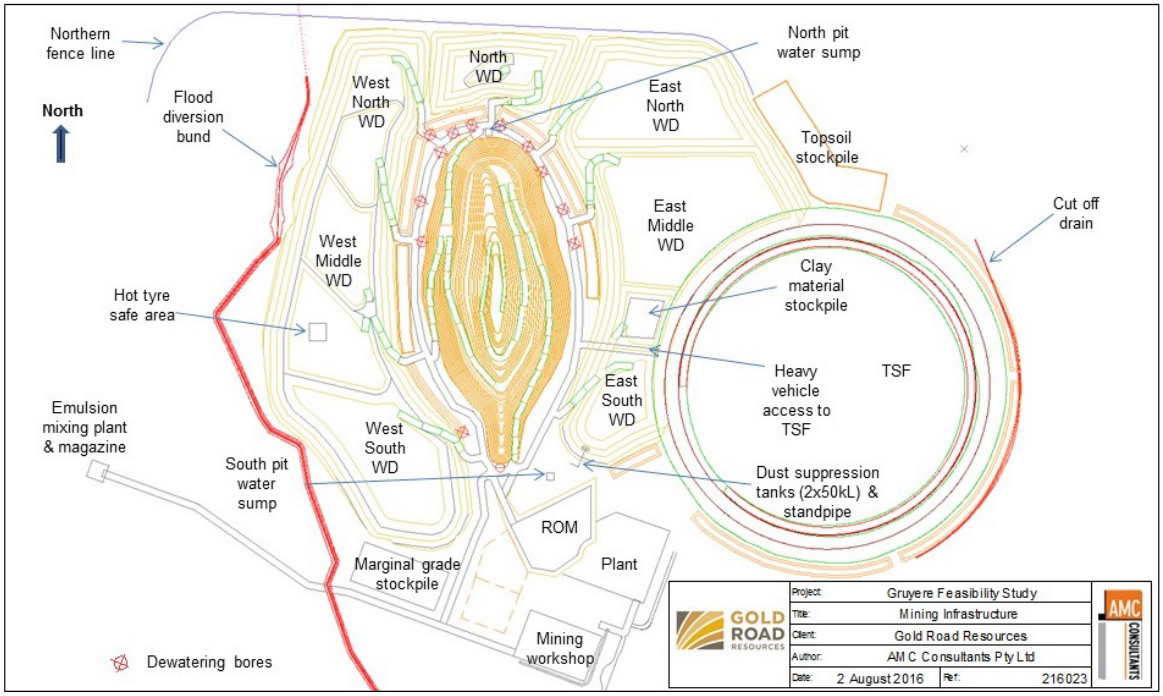


Figure 6: *Mine Site Layout*

Mining Schedule

The mining schedule adopts the following key parameters and assumptions:

- A primary loading fleet consisting of a maximum three hydraulic excavators in the 360 tonne class which is considered the largest option that could also practically excavate on three to four metre flitches
- The ore and waste haulage fleet will consist of 180 tonne mechanical drive haul trucks capable of direct tip to the primary crusher.
- The total material movement (**TMM**) per quarter was smoothed to ensure consistent TMM over each quarter (annually)
- A peak TMM of 7.25 Mt per quarter was set during the first five years of the schedule by testing the lowest TMM that ensured continuous ore supply. When the cut back for Stage 4 commences in year six, the TMM increases to 11 Mt per quarter to ensure ore supply in later years (Figure 7)
- The mining schedule has been constrained by setting a maximum vertical advance rate of 60 metres per annum in Stages 1 and 2 and 80 metres in Stages 3 and 4 (due to more bulk waste mining activity in Stages 3 and 4) to allow sufficient time for dewatering, grade control, drill and blast and load and haul
- Stages 3 and 4 are split into north and south to allow a lag in bench advancement
- The maximum vertical lag between benches is set at 20 metres
- The production schedule assumes variable process throughput rates ranging from 8.8 Mtpa for softer oxide ores to 7.5 Mtpa for fresh ore and varying grind sizes ranging from 106 µm to 150 µm
- The maximum process plant throughput rate is set at 2.2 Mt per quarter for a 100% oxide plant feed blend which is equivalent to 8.8 Mtpa
- The optimum grind size is determined by the scheduling software in consideration of net block values.

Initial mine development and pre-stripping activities are scheduled to defer capital expenditure and land disturbance and to provide sufficient material required to construct the TSF, site roads and ROM pad.

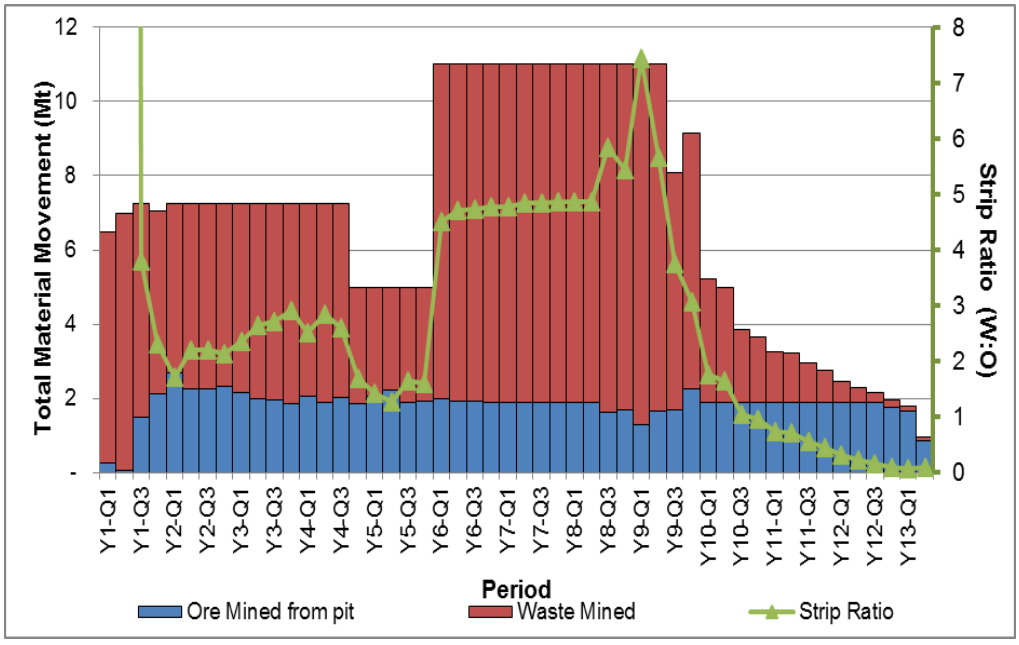


Figure 7: *Total Material Movement by Period and Strip Ratio*

Metallurgy

The process plant design is based on a conventional processing route using proven technology. Equipment selection has been based on testwork managed by Gold Road. Where no testwork was available, equipment selection has been based on reasonable assumptions and the experience of process engineers from GRES in consultation with Gold Road.

Nine major metallurgical testwork programs were carried out as part of the FS with seven metallurgical testwork programs at ALS Metallurgy, gravity testwork at Gekko Systems and materials handling testing at Jenike & Johanson. The objective of this phase of testwork was to complete the recommended work identified at the completion of the PFS and to expand on the PFS testwork to provide an adequate FS level of metallurgical information. Programmes included, but were not limited to: extractive work, communition studies, bulk gravity recoverable work, detailed mineralogical analysis, carbon adsorption testing, and materials handling properties.

A total of 50 composite samples were collected for the new programs, supplementing material already sampled and tested during Scoping and PFS programmes. A total approximate mass of 2,446 kilograms has been collected. A visual representation of all samples selected for metallurgical testwork is shown in Figure 8.

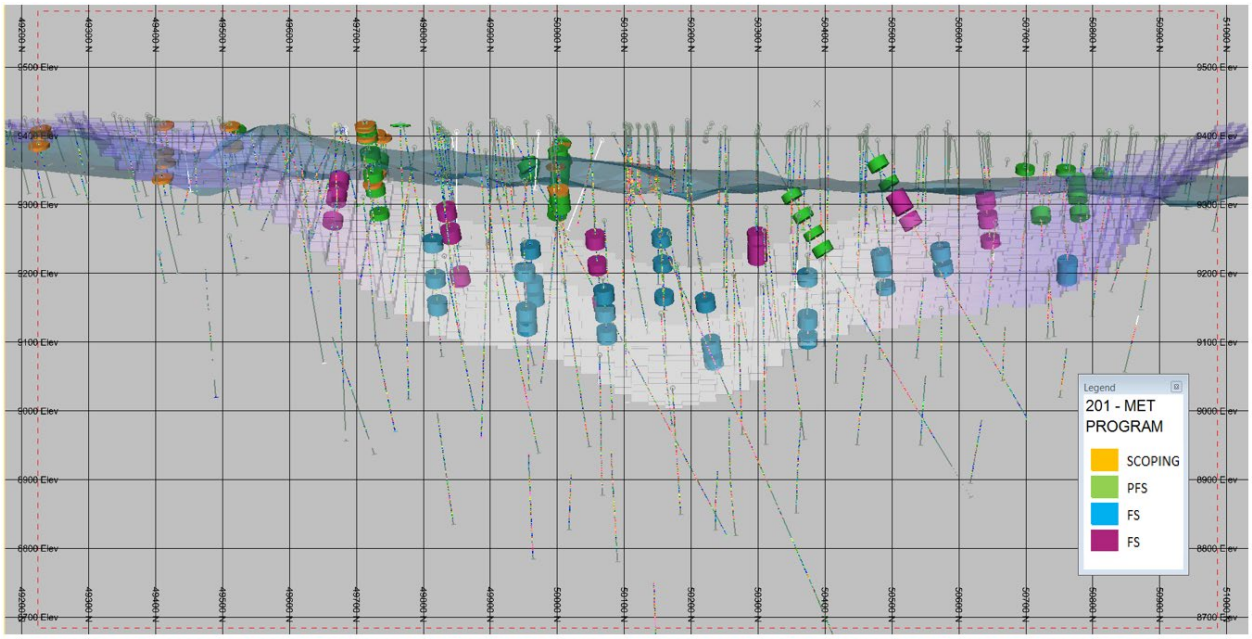


Figure 8: *Metallurgical Sample Selection for Gruyere - Longitudinal Projection Looking West. Pit Shell in purple and base of overburden as solid grey surface*

Comminution Testwork

A total of 35 fresh samples had comminution testing conducted across two campaigns at the ALS Metallurgy laboratory in Perth. The samples selected came from a range of depths from 85 to 372 metres downhole along the length of the deposit. Work focussed on the fresh rock zone which comprises 85% of the Mineral Resource and represents the hardest material component.

The fresh rock material is classified as “Hard” with Bond Ball Work Indices (**BBWi -** a measure of hardness and the ability of the ore to break during milling) varying between 16.6 and 18.5 (average of 17.3). This is regarded as similar to most milling operations in the Western Australian goldfields. The fresh rock is classified as “Abrasive” to “Highly Abrasive” which impacts on consumable consumption, such as mill steel (balls, liners, etc.) and crusher wear, and operating cost estimates have been calculated to allow for this.

Extractive Recovery Testwork

A total of 138 batch scale gravity-leach extraction tests were carried out. The level of gold extraction varied according to grind size. Highest extractions were generally observed at the finest grind sizes. Figure 9 illustrates gold extraction against the calculated head assay for all gravity-leach tests carried out at grind size P_{80} of 106 µm, 125 µm and 150 µm on the fresh ore. At the average LOM head grade of 1.20 g/t Au the total gold extraction by grind size is calculated as 93.3%, 91.8% and 90.4% respectively. The data has a standard error of approximately 2%.

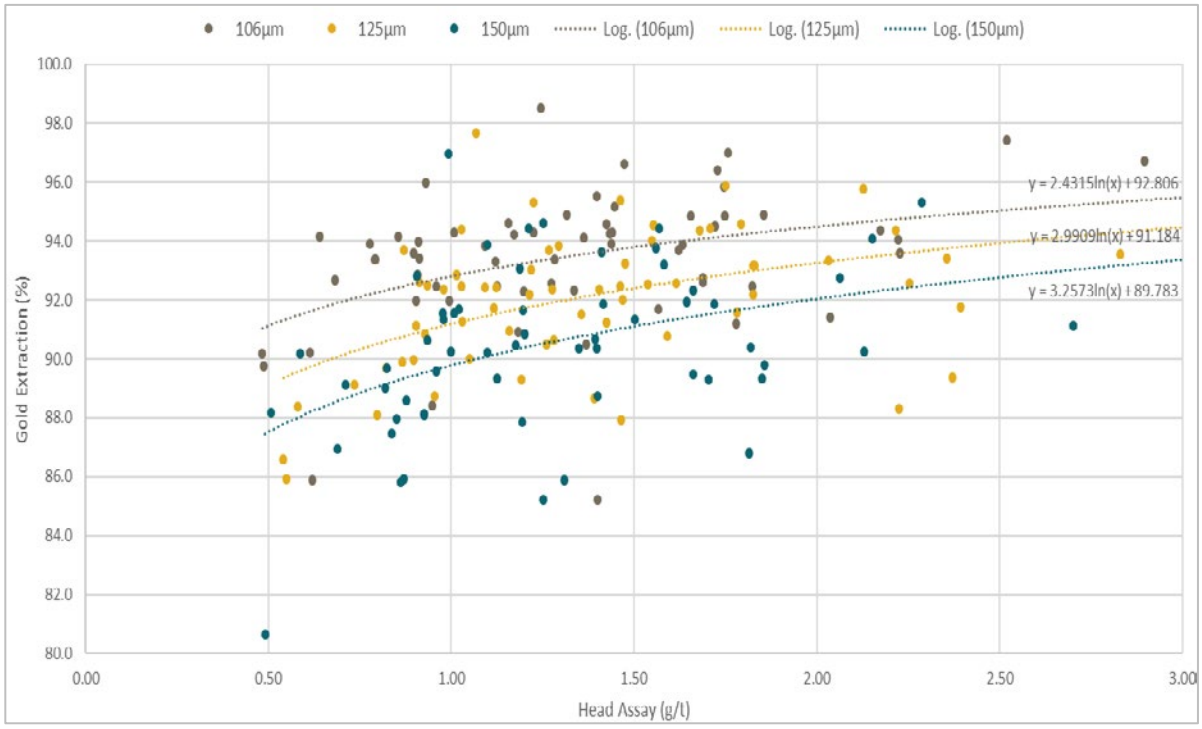


Figure 9: *Fresh Ore Regression Analysis – Gold Recovery (% Extraction) versus Gold Grade (g/t Au) at varying grind size*

Although the testwork on the fresh ore samples indicates the ore can be classified as free milling the level of gold extraction is considered moderately sensitive to grind size, particularly above a P_{80} of 125 µm. Based on the plant design throughput rates and LOM head grades, the estimated gold recoveries for the oxide, transitional and fresh ores at the target grind size of 125 µm are estimated to be 94%, 92% and 91% respectively.

In addition to total gold recoveries being relatively high, the Gruyere material is expected to yield a moderate gravity-recoverable component of gold, in the vicinity of 35 to 40% expected at the plant scale, which has positive operating cost implications. The ores also show rapid leach kinetics with the majority (>80%) of gold dissolution completed after only four hours of leaching residence time.

Ore Processing and Production[21]

The process facility is designed to process ore throughputs of 7.5 Mtpa of fresh ore, 8.0 Mtpa of transitional ore and up to 8.8 Mtpa of oxide and various rates for blended ore profiles (Figure 10). The process plant will be designed to operate seven days per week at a nominal treatment rate of 1,100 dry tonnes per hour (**dtph**) on oxide ore, 1,000 dtph on transitional ore and 937 dtph on fresh ore at a grinding circuit utilisation rate of 91.3%.

Estimated gold recovery based on differential ore-type recoveries at the target grind size of 125 µm is estimated to average approximately 91% over the LOM. Average LOM annualised gold production based on a nominal head grade of 1.20 g/t Au is approximately 270,000 ounces (Figure 11).

[21] See Appendix 1 "Forward-Looking and Cautionary Statements" on page 40

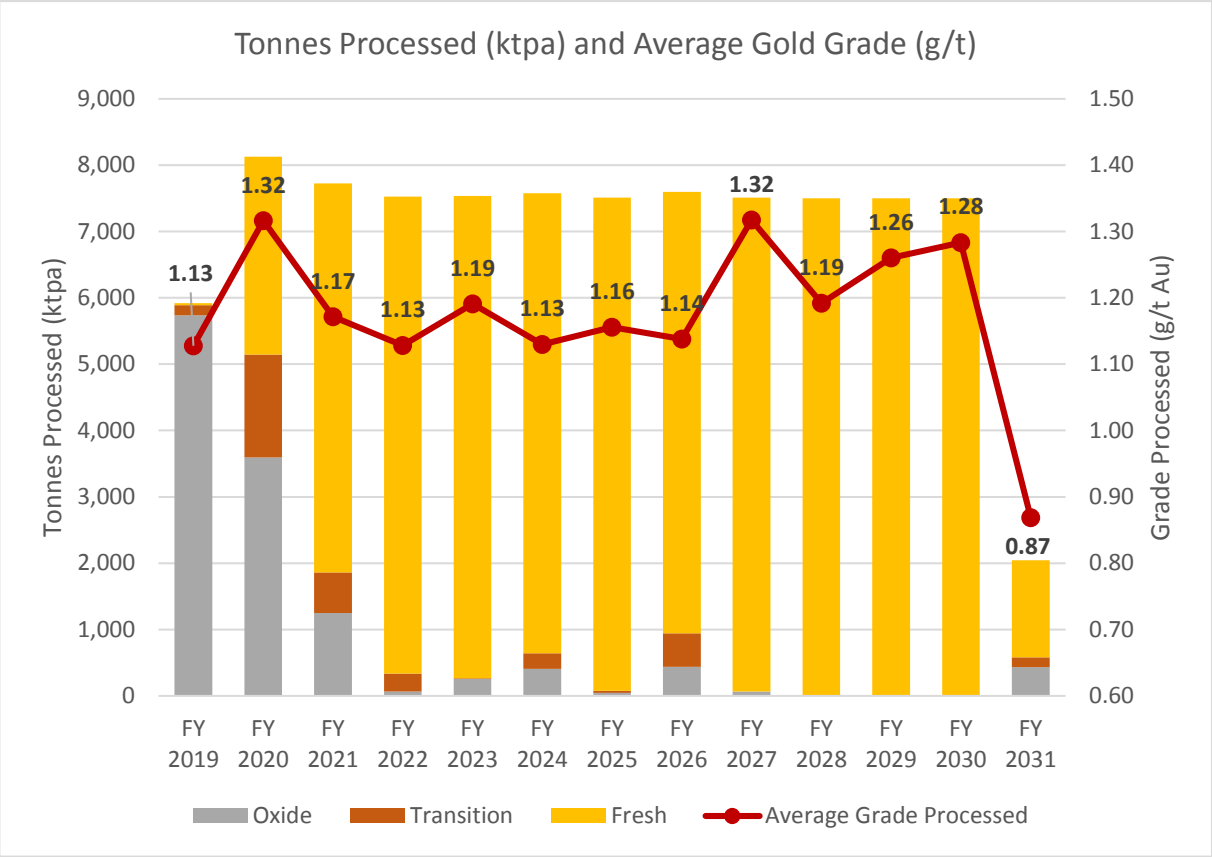


Figure 10: *Annual Processing Plant Throughput by Material Type and Average Grade Processed*

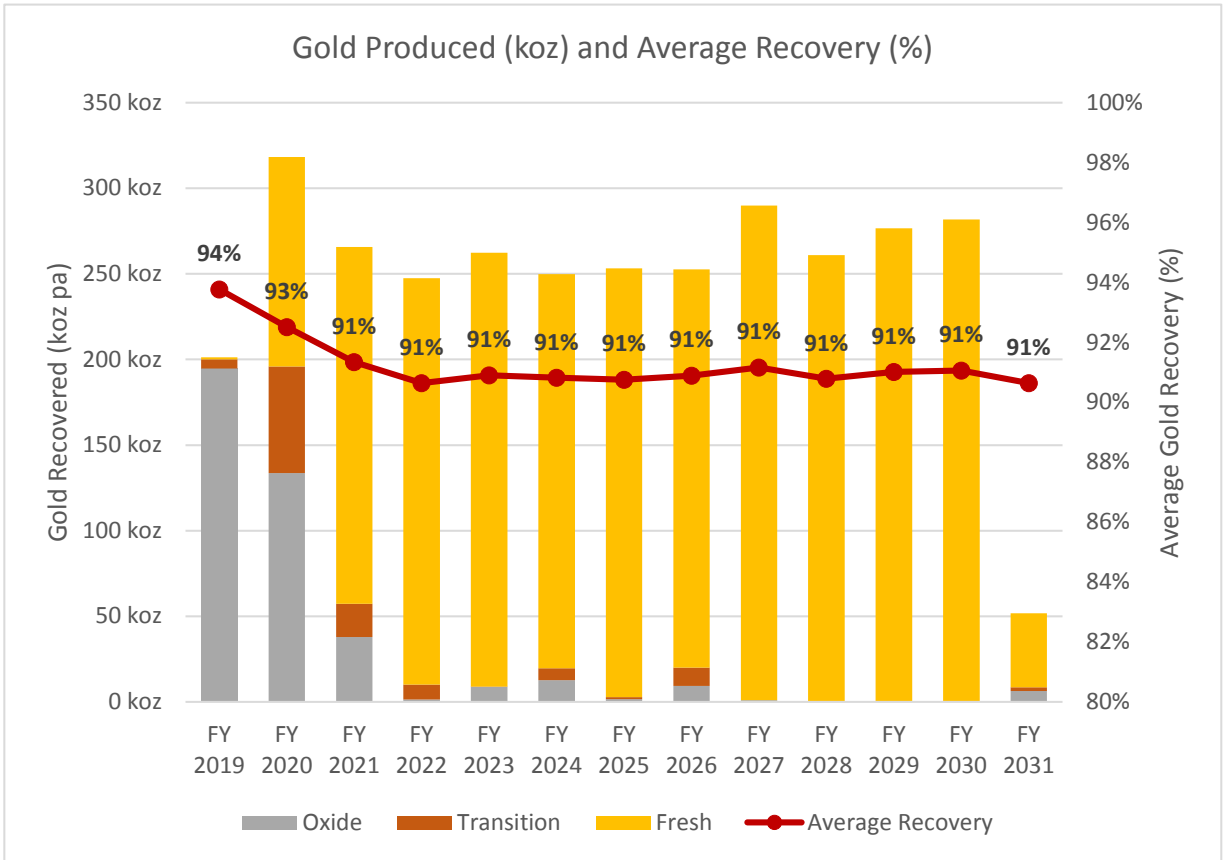


Figure 11: *Annual Gold Production and Average Gold Recovery*

The process plant design is based on well proven processing technology following a processing route of:

- Primary crushing by a gyratory crusher to product size P_{80} of 135 millimetres
- Grinding in a SABC to an average product size P_{80} of 125 µm (with capability to range from 106 µm to 150 µm), with pebble crushing for scats
- Treatment of a portion of the grinding circuit cyclone underflow by centrifugal gravity concentration, followed by batch intensive leaching of the gravity concentrate and electrowinning of the resulting pregnant solution
- Thickening in a high rate thickener of the grinding circuit classifier overflow to 50% solids (**w/w**) prior to treatment in a hybrid CIL circuit
- Acid washing and split Anglo American Research Laboratory elution of the resulting loaded carbon, followed by thermal regeneration of the barren carbon prior to its return to the CIL circuit
- Smelting of cathode sludge from electrowinning to produce a final product of gold doré
- Tailings thickening in a high rate thickener to 60% solids (w/w) prior to disposal of the tailings into the TSF located within an Integrated Waste Landform (**IWL**)
- Raw and process water will be sourced from remote borefields and transferred via a system of overland pipelines and transfer pumps.

The processing plant layout in Figure 12 reflects the sequential nature of the processing operations, with ROM ore received at one end of the facility, gold doré bars produced in the gold room and tailings disposal at the TSF.

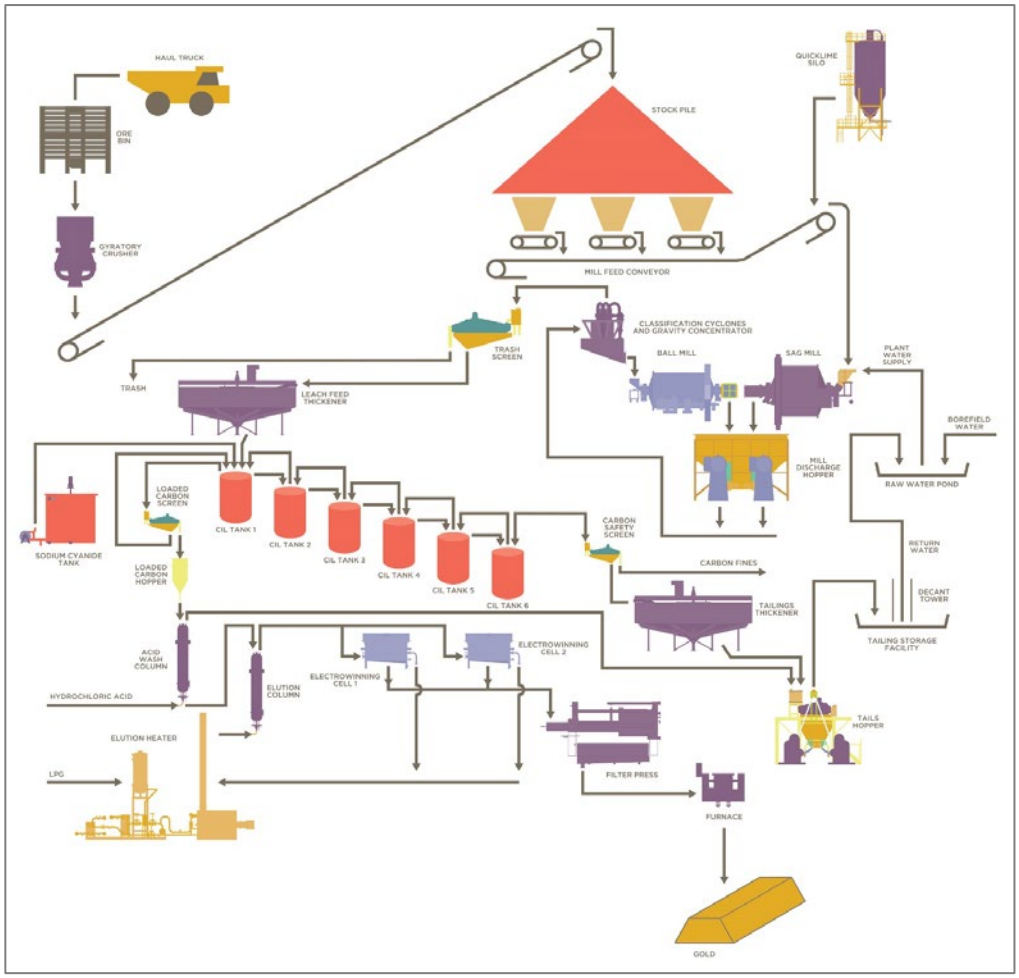


***Figure 12**: Gruyere Gold Plant Process Flowsheet*

Infrastructure, Transport and Services

Road Access, Accommodation and Airstrip

Road access to the Project site will be from Laverton along the Great Central Road, turning off 153 kilometres from Laverton (Figure 13). The site access road from Great Central Road will be 48 kilometres in length, comprising 19 kilometres on an upgraded section of the existing Mt Shenton-Yamarna Road, and 29 kilometres of the main Site Access Road (**SAR**) which is to be constructed to join the Mt Shenton-Yamarna Road to site. The SAR will terminate adjacent to the planned mine contractors' service area and to the southern entrance to the process plant site. A further 1.2 kilometres of plant access roads will connect the SAR to the mine contractors' service area and the power station. The accommodation village and airstrip access road will be located approximately 6 kilometres west of the end of the SAR.

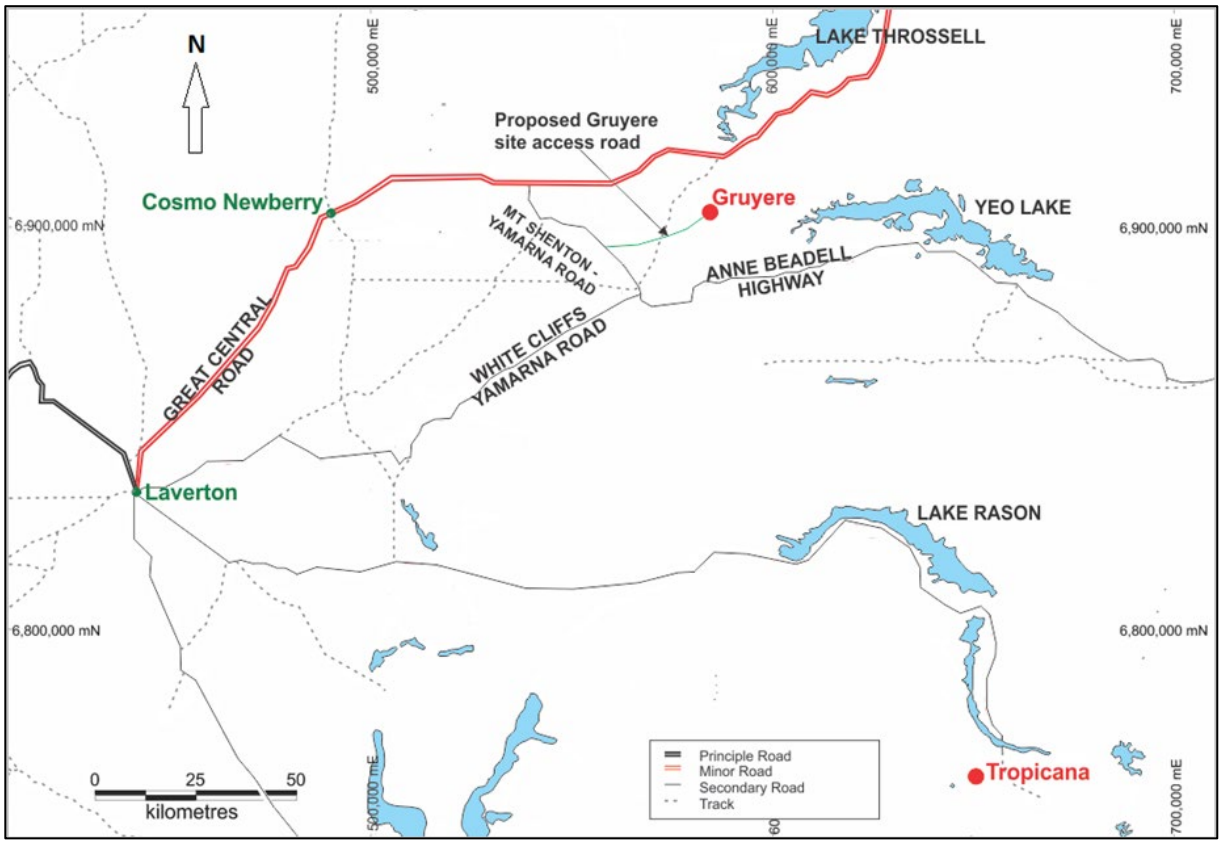


Figure 13: *Gruyere Regional Map illustrating main road network and location of Gruyere Project site*

An accommodation village, containing both temporary and permanent facilities, will be constructed approximately six kilometres south-west of the process plant and sited adjacent to the airstrip within a well-drained, elevated area 400 metres long and 400 metres wide. The earthworks will be a balanced cut to fill with disturbance of vegetation kept to a minimum.

The works will comprise the supply and site installation of 600 accommodations rooms and support services in total consisting of:

- 300 construction (temporary) rooms at the accommodation village
- Support services building, including administration, wet mess and dry mess
- 300 permanent rooms at the accommodation village.

The accommodation village will consist of a 300 person construction camp and a 300 person permanent village, and will be made available in two initial stages to facilitate the changes through the phases of the Project. A final third stage will focus on clean-up and the establishment of landscaping and sport facilities.

A 24-hour Civil Aviation Safety Authority compliant airstrip including a 2.1 kilometre long runway with bitumen seal, terminal and fuel facility to suit up to a 100 seat aircraft will be will be constructed adjacent to the accommodation village 6 kilometres south-west of the process plant. Access to the airstrip will be via the accommodation village/airstrip access road. The airstrip will be built as part of the early works during the construction phase to minimise the reliance on road transport for personnel access to and from the Project.

Power Generation

Development of the power generation solution for the Project followed a formal process to determine the most reliable and cost effective option. The PFS Power Options Study recommended a gas fired power station fuelled by gas pipeline, which has been followed as the preferred option in the FS. The power generation facility will be provided on a Build-Own-Operate basis under a Development Agreement followed by an Energy Supply Agreement.

Tenders for the provision of power were sought during 2016 with the Scope of Work including the acquisition and delivery of fuel, and design, construction, operation and maintenance of the power station. During the tender process tenderers were requested to provide proposals for two options:

- Option A: BOO and maintain a gas fired power station and provide all turnkey services for the acquisition and transport of gas and construction and operation of gas pipeline lateral to the site
- Option B: BOO and maintain a power station to start production based on a diesel-fired facility (including diesel supply and storage) with an ability to convert to gas delivered by pipeline at a later date.

Technical and financial analysis and evaluation of the proposals has shown that the gas-fired facility from day one provides the optimal cost result and remains the preferred option. The Company is in the final stages of evaluation of tenders with an expectation of provisional award being granted in November 2016.

The design of the 40 MW power station is based on a 35 MW peak load requirement, 32 MW average load producing 255 GWh per year, and capable of producing the peak load requirement at an N-2 level of reliability in all ambient conditions. This will provide generation capacity capable of meeting both the average and peak power demands of the process facilities in all circumstances with up to two of the units out of service.

Power will be generated at 11 kV and will be distributed to the various plant areas including warehouse, workshops, accommodation village, airstrip, administration and TSF. The Yeo Borefield will also be fed directly from the power station via 22 kV overhead powerlines.

An unencumbered allowance for a reduction in fuel fired energy was requested of all tenderers to allow for future possible use of alternative or renewable energy sources such as solar or wind generation.

Borefields and Water Supply

The Yeo Borefield, approximately 25 kilometres west of the plant (Figure 14), will consist of 32 water bores (23 operating at any one time and nine on standby for rotation into operation to maximise efficiency and to minimise impact of drawdown on the aquifer) installed along the 65 kilometre length of the borefield, providing 7.5 GL per annum of moderate to high salinity raw water to the processing plant for use as process water. The water quality is estimated to be in the range of 25,000 mg/L to 100,000 mg/L total dissolved solids, and is expected to average less than 50,000 mg/L.

The borefield will consist of two branches, each approximately 33 kilometres long stretching roughly north and south from the intersection point with the Mt Shenton-Yamarna Road. In addition to the planned Yeo Borefield, a 35 kilometre long section of palaeochannel immediately upstream of the Yeo Borefield has been identified for possible future borefield expansion as contingency required for licensing conditions.

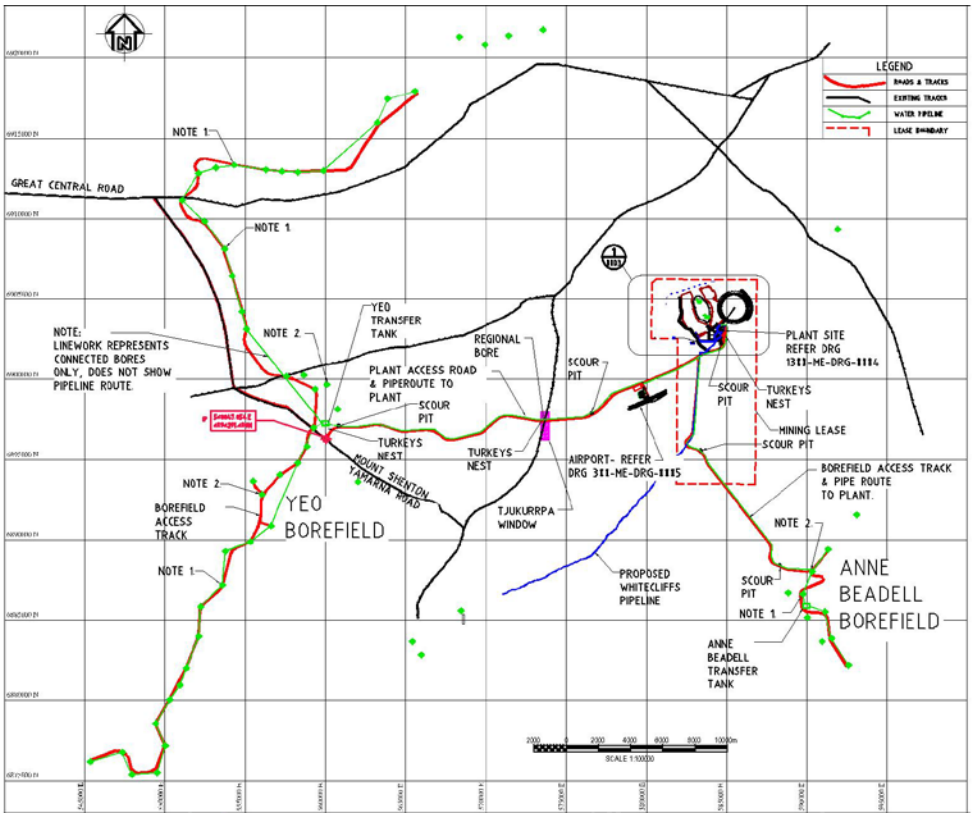


***Figure 14**: Gruyere Project Infrastructure - location of Bore Field Pipelines (green) and new roads and tracks (red) with existing roads in black*

The Anne Beadell Borefield, approximately 22 kilometres (average 29 kilometres by track) south-east of the plant site (Figure 14), will consist of six water bores (four operating at any one time and two on standby) providing brackish raw water to feed a Reverse Osmosis (**RO**) plant in the process plant area. This low salinity water will be processed at a rate of 1,100 m³ per day through the RO plant to produce 700 m³ per day of fresh water for the process facility for potable, safety shower and fresh water, and the accommodation village and offices. The high-saline by-product from the RO plant will be directed into the process plant water circuit.

All borefield pipelines will be buried wherever possible. If the pipeline routes encounter hard digging conditions that prevent cost effective excavation, alternative installation measures including installing the pipeline at ground level and covering with suitable spoil for fire protection will be considered. All pumps in the Yeo Borefield will be powered by a 22 kV overhead powerline from the power station at the process plant, and will be controlled by telemetry from the process plant. The Anne Beadell pumps will be powered by self-bunded power generating sets and will be controlled through a telemetry system at the process plant. Water flow monitoring of each input to the bore water pipeline will be incorporated to enable real-time monitoring of the water flows.

Tailings Storage Facility (TSF)

The TSF will be developed as part of an IWL, with a perimeter waste dump surrounding a centrally placed TSF. An IWL was selected as the preferred design configuration for the Project. IWL is a generic term for development of a TSF within a waste dump. The waste is placed within the dump using traditional dump construction techniques (i.e. paddock dumping and dozer spreading) and a compacted zone is constructed within the waste dump annulus forming the TSF. Based on the FS mining schedule it is anticipated there will be sufficient material from mining for use in the concurrent tailings storage construction.

The tailings parameters are based on laboratory testing carried out as part of the PFS and also considers tailings performance on similar gold tailings projects in the Western Australian Goldfields. The TSF design assumes total ore production 92.4 Mt[22], which relates to an average production rate of 8.0 to 8.2 Mtpa for the first three years, reducing to 7.5 Mtpa for the remaining 10 years. The tailings will be transferred from the CIL plant at 60% solids (w/w) and an average P80 of 125 µm.

The proposed process plant site is approximately one kilometre south–east of the open pit, with the proposed TSF situated immediately north of the plant site and east of the pit (Figure 15). The Project area terrain is flat to gently undulating. Drainage in the pit and plant areas is to the north-east and ultimately towards Yeo Lake approximately 20 kilometres to the east.

Waste Rock Characterisation test work completed by consultants MBS indicated that the mine waste to be used in TSF starter embankment and IWL construction is likely to be benign, with no significant metal enrichment, and was assessed as Non-Acid Forming. Results of geochemical testing of tailings from metallurgical sampling indicates the tailings solids are likely to have low levels of total sulphur at around 2 mg/L and are Non-Acid Forming. The results of geochemical characterisation test work indicate that the tailings will be relatively benign and lining of the TSF is not be required, provided seepage is adequately managed and controlled.

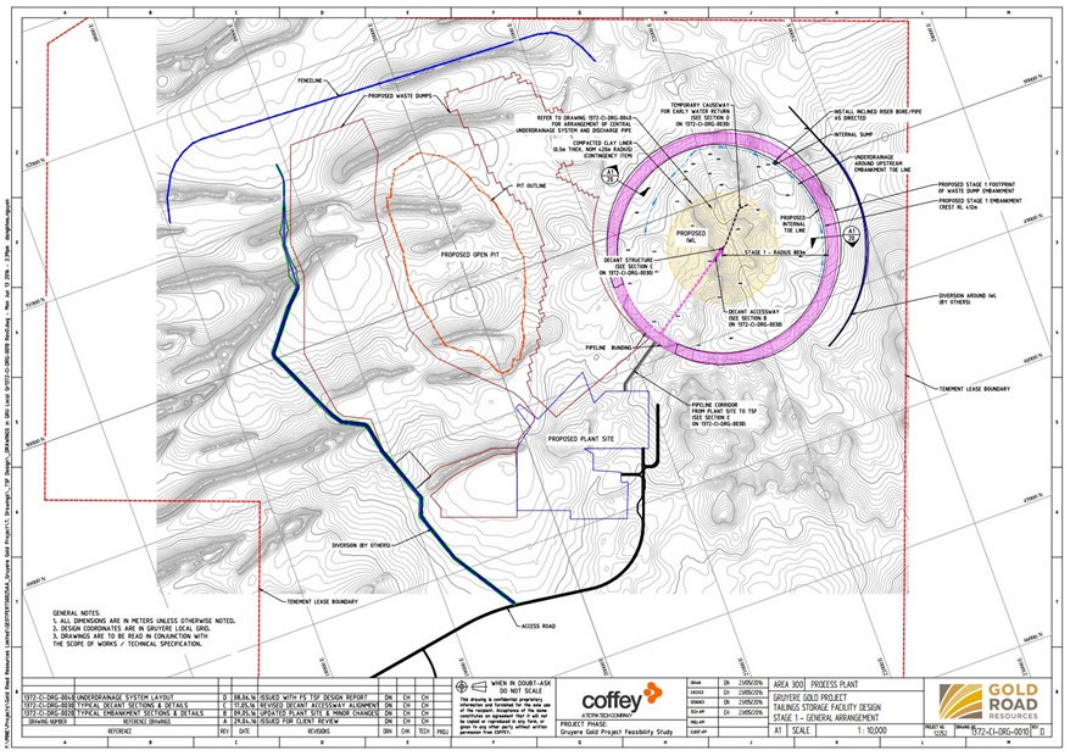


***Figure 15**: Proposed Location of Stage 1 TSF to north-east of Plant Site and east of Gruyere Open Pit*

[22] At the time of selecting the design tonnage for TSF storage, mine planning was still in progress, but understood to be accurate to approximately 1%. A design tonnage of 91.5Mt+1% (92.4 Mt) was selected for TSF design purposes.

Process Plant Infrastructure

The process plant and administration facilities will be contained in an area approximately 400 metres long by 400 metres wide (Figure 16) and located to avoid the major local water courses. The site will also be in close proximity to the ROM Pad. The site is naturally drained to the north-east and the most significant surface water flows will be intercepted by a major diversion drain constructed to the west of the process plant and open pit. The entire process plant site perimeter will be fenced with chainwire security fencing with vehicular and pedestrian access gates.

Main facilities and buildings include:

- Plant internal roads and hardstands
- ROM Area for run of mine ore stockpiles and primary crusher complex
- Administration office complex and Emergency response buildings
- Process plant workshop and store, and Reagent store
- Gold room building
- Assay laboratory
- Pressure swing absorption shed
- Light vehicle wash-down bay
- Diesel fuel storage
- Mining facilities area
- Landfill facility

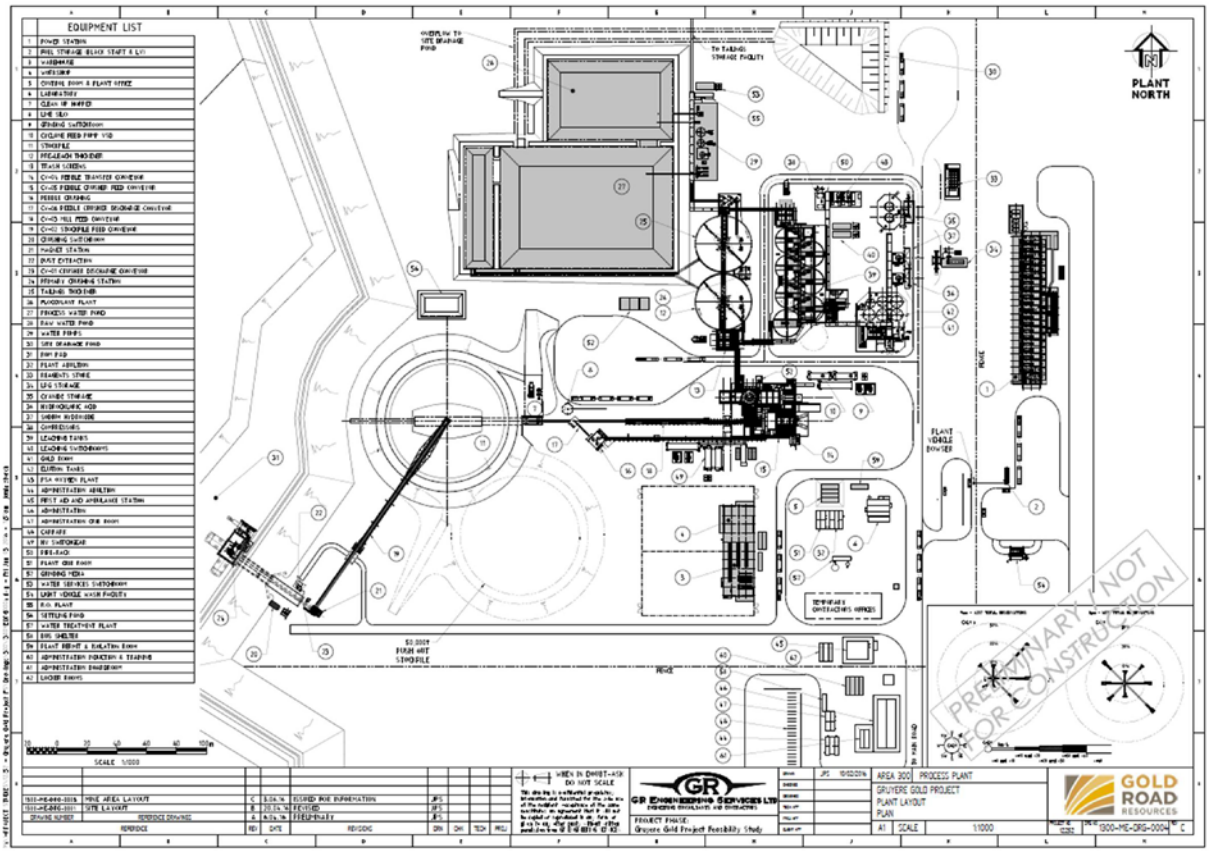


Figure 16: *Preliminary engineering design plans for Gruyere process plant, administration block and power station*

Capital Expenditure[23]

Capital Expenditure

The capital cost estimate represents costs for the overall Project development. The estimate includes direct costs for the open pit mine pre-strip and mine development, the process plant, non-process infrastructure (**NPI**), and indirect costs associated with the contractors, Owner's team and pre-production operations. The total estimated capital cost is approximately A$507 million, representing an increase of A$51 million compared to the PFS, and which includes contingency of A$43 million (Table 9). The forecast total capital expenditure (**Capex**), including potential escalation of A$7 million to Project completion in the December 2018 quarter, is estimated to be A$514 million. Approximately A$38 million is estimated to be directly exposed to foreign exchange variation.

Table 9 shows the summary variance between the PFS and FS while Table 10 details the source of variance from PFS to FS.

Table 9: *Summary of Total Capital Costs by Major Area as at Q3 2016 (excluding potential escalation to project completion in Q4 2018)*

Area	FS (A$M)	FS (US$M)	PFS (A$M)
Direct			
Process Plant & Infrastructure and TSF	178	130	186
Infrastructure and Utilities – Site General	79	58	59
Mine Development	36	26	33
Power Supply and Distribution	20	15	19
Site Development and Site Drainage	8	6	6
Subtotal Direct	**321**	**235**	**303**
Indirect			
Engineering and Contractors (Indirect)	86	63	81
Project Owner's Team& Pre-Production Operations	50	37	35
Capital, Operating and Commissioning Spares	7	5	4
Subtotal Indirect	**143**	**104**	**120**
Contingency	43	31	35
Total (Real) Capital Cost	**507**	**370**	**456**

Notes:

1. *All figures are rounded to reflect appropriate levels of confidence*
2. *Capital cost estimate is as at Q2 2016, and accuracy level is -10% to +15%*
3. *Apparent differences may occur due to rounding*
4. *Costs are estimated with a Q2 2016 Base Date*
5. *A$:US$ exchange rate of $1.00:$073*

[23] See Appendix 1: Forward-Looking and Cautionary Statements on page 40

Table 10: *Reasons for Variance from PFS to FS*

Area	Variance	Reason/s
Mining	A$3 million increase	The number of quarters of mining capex has increased from two in the PFS to four in the FS. This is partially offset by the amortisation of mining infrastructure as part of Opex over five years from commencement of mining.
Borefields	A$10 million increase	As part of the "adaptive management" strategy of the stygofauna habitat in the Yeo borefield, the length of the borefield has been extended by 15km with 10 additional bores and pumps, and 8km of additional water pipelines, access tracks and powerlines.
Accommodation village	A$8 million increase	Revised construction and pre-production operations manning figures has resulted in the need for an increase in the size of the camp from 500 rooms to 600 rooms. There have also been enhancements to the village layout and recreational facilities.
Pre-Production Operations	A$7 million increase	Pre-production operations have been extended by two-quarters to first-gold production. Operations manning ramp-up and labour rates have been revised since the PFS.
Owner's Costs	A$5 million increase	More detailed design during the FS indicates the communications operating costs during the construction phase was underestimated in the PFS. Owner's team staffing and durations have also been updated based on the current contracting strategy and Project Schedule.

The capital cost estimate includes:

- Direct costs of the Project development
- Indirect costs associated with the design, construction and commissioning of the new facilities
- Owner's cost associated with the management of the Project from design, engineering, construction up to the handover to operations and Project close-out
- Insurance, operating spares and first fills
- Costs associated with Operational Readiness and pre-production operations
- Growth allowance on quantity, pricing and unit rate variance
- Contingency on Project scope definition and risks.

The cost estimate has been developed with input primarily from GRES, AMC and the Owner's team. Axiom completed a peer review of the non-mining capital cost estimate. Broadleaf completed a capital cost and schedule risk analysis to determine the capital contingency over a range of probabilistic outcomes. The Project Execution Strategy is based on a 24-month construction and commissioning timeframe, beginning in the March 2017 quarter, with completion of commissioning and ramp-up in December 2018 quarter.

The estimate is based upon preliminary engineering, quantity take-offs, tendered price quotations for mills, crushers and accommodation village and budget price tendered quotations for major equipment and bulk commodities. Unit rates for installation were based on market enquiries specific to the Project and benchmarked to those achieved recently on similar projects undertaken in the Australian minerals processing industry.

The capital costs associated with the gas-fired power station and gas delivery pipeline are not included in the estimate as these are to be provided under a BOO contract and are captured in the power unit cost used in the operating cost estimates. Similarly, the capital cost estimate does not include the cost of the mining mobile equipment fleet as this will be incorporated in the mining contract rates.

Sustaining Capital Expenditure

The Sustaining Capital Expenditure (**Susex**) estimate represents cost expended to sustain and/or maintain the capital assets to perform to the Project design criteria during the LOM. The FS Susex estimate of A$77 million represents a decrease of A$64 million from the PFS. Table 11 shows the summary variance between the PFS and FS while Table 12 details the source of variance from PFS to FS.

Table 11: *Summary of Total Sustaining Capital Cost by Major Area PFS vs FS*

Area	FS Total LOM Cost (A$M)	PFS Total LOM Cost (A$M)	Variance (A$M)
Mine Development	31	80	-49
Processing and Infrastructure	16	30	-14
TSF	23	18	5
Contingency	7	13	-6
Total	**77**	**141**	**-64**

Note: *Apparent differences may occur due to rounding*

Table 12: *Reasons for Variance from PFS to FS*

Area	Variance	Reason/s
Pit Expansion	Decrease of A$62M from A$80M to A$18M. Note TSF overhaul costs are included in Mine Development in Table 9	PFS assumed that in the operations phase all mining costs incurred in moving cover material were sustaining capital costs. In the FS, cover material is treated as general waste and included as capital or operating costs.
Mechanical Equipment	Decrease of A$22M from A$22M to A$0M	PFS had an allowance of 2.5% of mechanical equipment cost for replacement cost. FS has no replacement of equipment necessary for LOM assuming an establishment of overall proactive sustainable asset management strategy is in place.
TSF Lifts	Increase of A$5M from A$18M to A$23M	PFS had five lifts in sustaining capital whereas FS has six lifts based on a smaller initial wall height.
TSF Overhaul	Increase of A$13M from A$0M to A$13M	This cost was allocated to operating costs during the PFS. In the FS overhaul distance beyond the waste dump has been reclassified as Susex so as to avoid overstating the mining cost.
Contingency	Decrease of A$6M from A$13M to $7M	Contingency is a 10% allowance and was reduced proportionally relative to the reduced estimated sustaining capital cost.

Accuracy of Estimates

The development, Susex and Capex estimates have been developed to a FS level definition based on a defined Estimating Plan and guidelines developed by Gold Road. Based on the current state of design and pricing, the accuracy of the estimate is classed as being within -10% to +15% of the most likely value of the estimated final Project costs including contingency. The accuracy of the estimate at -10% to +15% is per recommended practice No. 47R-11 for process industries set out by AACE International (**AACE**) - Cost Estimate Classification guidelines for Class 3 estimates. In the development of the capital cost estimate, some of the Project deliverables have been completed to a higher maturity level than a Class 3 Estimate requirement.

Operating Expenditure[24]

Operating costs are sub-divided into mining, processing, transport and refining, site and corporate General and Administration costs. All operating costs for the Project have been estimated based on costs prevailing in the Australian minerals industry for June 2016 quarter. No escalation has been applied as the LOM operating costs are estimated in real terms consistent with the Financial Model. All costs were estimated to a level of accuracy of - 10% to +15%.

The total estimated LOM operating cost for mining, processing, transport and refining, general and administration is approximately A$2,788M. Summary of the operating costs are shown in Table 13 and Figure 17.

Table 13: *Operating Costs Summary*

Item	LOM Cost (A$M)	LOM Cost (A$/oz)	% LOM Cost
Mining	1,229	383	44.1
Processing	1,433	446	51.4
Transport and Refining	5	2	0.2
General and Administration	121*	38	4.3
Total Operating Costs	**2,788**	**868**	**100.0**

Notes:

- **General and Administration costs in the table above include site and corporate costs relating to the Project*
- *All figures are rounded to reflect appropriate levels of confidence*
- *Apparent differences may occur due to rounding*

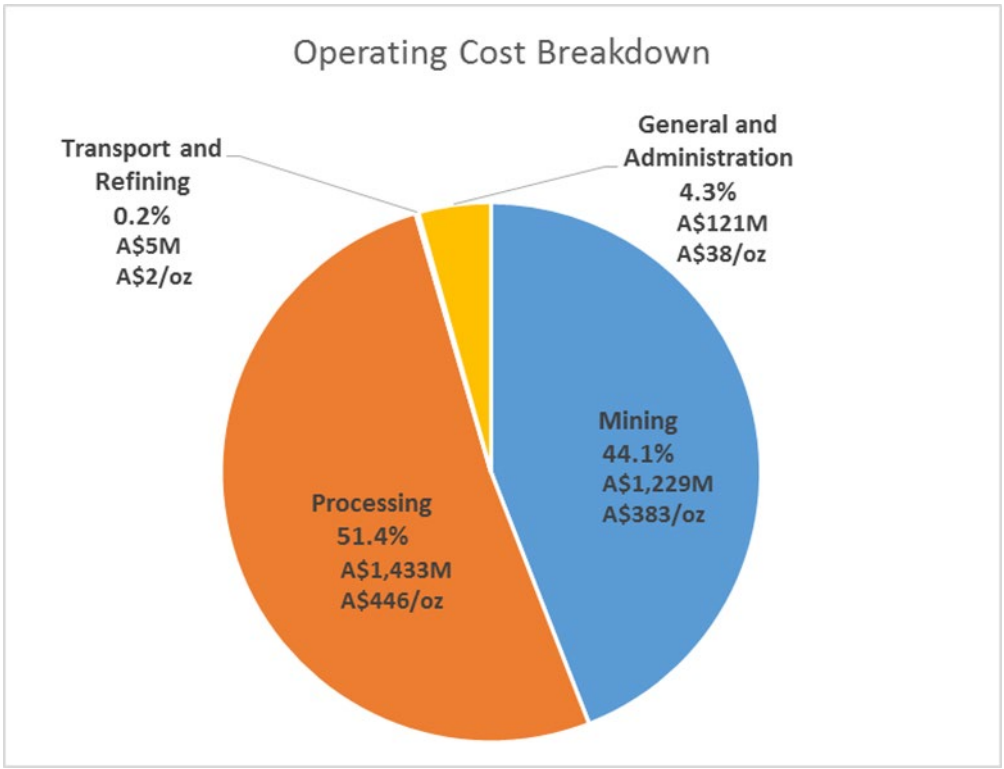


Figure 17: *Proportional Operating Cost Breakdown Financial Evaluation*

[24] See Appendix 1: Forward-Looking and Cautionary Statements on page 40

Mine Operating Costs

Mining costs for the Project were estimated by AMC based on the quarterly mining schedule and prepared using AMC's proprietary cost estimation system, with a summary breakdown tabulated below (Table 14). The Mine Cost Model was refined by comparison against a range of projects including both owner mining and contract mining estimates. The operating costs for drilling, blasting, loading and hauling, topsoil removal and replacement and crusher feed activities were developed from first principles. This includes operating hours, haul cycles, labour rates, fuel consumption, maintenance requirements and consumables. The mining cost estimate incorporates costs from the December 2018 quarter, which is the quarter during which gold production commences. All mining costs incurred prior to this date are classed as capital costs and included in the Capital Cost estimate described above.

Table 14: *Life-of-Mine Operating Cost Summary*

Activity	LOM Cost (A$M)	LOM Cost (A$/t mined)	LOM Cost (A$/bcm mined)	LOM Cost (A$/t processed)	LOM Cost (A$/oz)	Proportional Cost (%)
Load and Haul	468.4	1.35	3.35	5.12	146	38%
Drill and Blast	389.1	1.13	2.79	4.25	121	32%
Other Mining	169.6	0.50	1.20	1.85	53	15%
Management and Overheads	201.4	0.58	1.44	2.19	62	15%
Total	**1,228.6**	**3.56**	**8.79**	**13.42**	**383**	**100%**

Notes:

1. *The A$/t mined and A$/bcm mined reported in Table 13 is calculated to include material mined during the construction period for which the estimated cost is capitalised*
2. *Apparent differences may occur due to rounding*

Process Operating Costs

The LOM operating cost estimate for the process plant was completed for a blend of different ore types (fresh, transition and oxide) and grind sizes (P_{80} of 125 µm and 150 µm) at various throughput rates. This was based on the annual operating cost estimates for the different ore types and grind sizes completed by GRES. Table 15 provides a summary of the LOM operating cost by cost centre based on the process plant feed schedule of the LOM.

Table 15: *Life-of-Mine Average Process Operating Cost Estimate Summary by Cost Centre (for fresh, transitional and oxide material)*

Cost Centre	LOM Cost (A$M)	Unit Cost (A$/t processed)	Unit Cost (A$/oz)	Proportional Cost
Power	639.2	6.98	199	45%
Reagents and Grinding Media	434.8	4.75	135	30%
Labour	124.4	1.36	39	9%
Wear Materials	111.3	1.22	35	8%
Maintenance Spares, Consumables and Contractors	64.7	0.71	20	4%
Other	59.1	0.65	18	4%
Total	**1,433.5**	**15.65**	**446**	**100%**

Note: *Apparent differences may occur due to rounding*

Financial Modelling and Evaluation[25]

PCF Capital Group (**PCF**) was commissioned to undertake the Project financial modelling for the PFS and FS. The financial model incorporates a start date of August 2016 when commitments to long lead items commence. All Owner's team expenditures related to studies prior to January 2017 are treated as sunk costs including all Project study costs (PFS and FS). Table 16 highlights the key financial inputs and assumptions used.

Table 16: *Key Financial Assumptions*

Parameter	Units	Assumptions
Gold Price	A$/oz	1,500
Exchange Rate	A$1:US$	0.73
Accumulated Tax Losses	A$	90M*
Corporate Income Tax	%	30
Power Cost (based on gas source)	A$/KWh	0.21
Diesel Price (after rebate)	A$/litre	0.65

Note: ** Estimated Tax Losses as at end of 2016 financial year*

The financial analysis was undertaken using A$1,500 per ounce (five year average historic gold price) and assumes a constant gold price throughout the LOM. Table 17 below shows the Project financial outcomes.

Table 17: *Summary of FS Financial Outcomes (all run at A$1,500/oz)*

Measure	Units	FS Outcome A$M	FS Outcome[8] US$M
Gold Produced	koz	3,212	
Gross Revenue	$M	4,817	3,516
Free Cash flow – Pre-Tax	$M	1,222	892
Free Cash flow – Post-Tax	$M	845	617
IRR (Pre-Tax)	%	24.0	
IRR (Post-Tax)	%	19.5	
NPV (Pre-Tax)[1]	$M	486	355
NPV (Post-Tax)[1]	$M	305	223
C1 Cash Costs[2]	$/oz	858	626
C2 Cash Costs[3]	$/oz	1,040	759
C3 Cash Costs[4]	$/oz	1,093	798
AISC[5]	$/oz	945	690
AIC[6]	$/oz	1,103	805
Development Capital Cost[7]	$M	507	370
Development Capital Cost per ounce (Dev. Capex / Gold Produced)	$/oz	158	115
Capital Efficiency (Pre-Tax NPV/Development Capex)		1.0	
Payback	Months	48	
Payback: LOM	%	33	
Project LOM Costs[9]	$M	3,542	2,586

Notes:

1. *8% Discount rate applied*
2. *C1 = Mining + Processing Operating Expenditure + Site General and Administration Expenditure + Transport and Refining Costs*
3. *C2 = C1 + Depreciation + Amortisation*
4. *C3= C2+ Royalties + Levies + Net Interest Costs*
5. *AISC = C1 + Royalties + Levies + Sustaining Capital + Project related offsite Corporate expenditure*
6. *AIC = AISC + Development Capital Expenditure*
7. *The Development Capital Cost is in Q3 2015 (PFS) and Q2 2016 (FS) Real terms. The forecast capital cost including potential escalation to Project completion (Q4 2018) is estimated to be A$514M*
8. *A$:US$ exchange rate A$1:US$0.73*
9. *Excludes mine site closure costs of $54 million*

[25] See Appendix 1: Forward-Looking and Cautionary Statements on page 40

The Gruyere Project generates very strong annual cash flows at A$1,500 per ounce gold price, at significant margins above the All-In Sustaining Cost measures. The LOM AISC of A$945 per ounce would position Gruyere in the lower cost quartile of gold producers. Figure 18 shows the estimated annual EBITDA against the annual AISC at a gold price of A$1,500 per ounce.

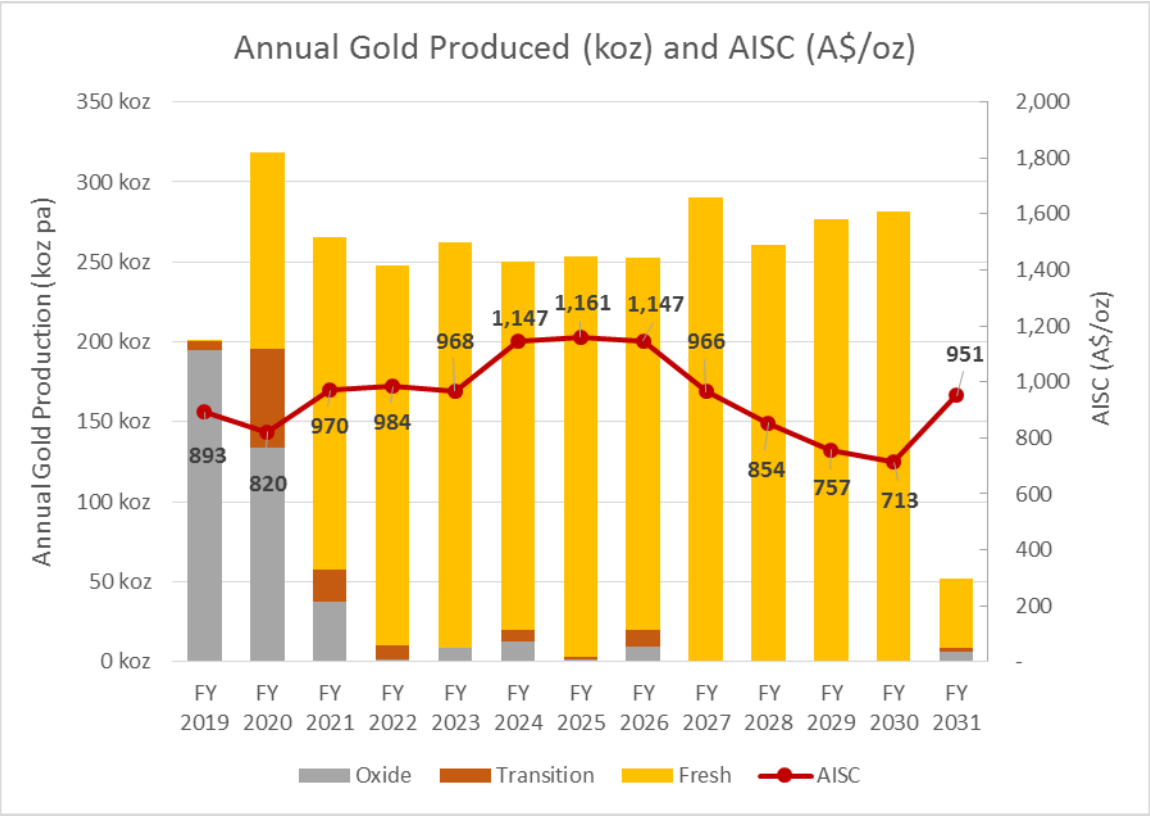


Figure 18: *Annual EBITDA (at A$1,500/oz) versus AISC (A$/oz)*

Financial Sensitivity

Sensitivity analysis was completed on a number of inputs to identify key areas of potential financial variance. Changes in gold price (Table 18) was identified as the major area of sensitivity on both the upside and downside, followed by gold grade as the next most sensitive (Figure 19).

Table 18: *Gold Price Sensitivity*

% Var	Gold Price (A$/oz)	Pre-Tax IRR (%)	Pre-Tax $NPV_{8\%}$ (A$M)	Post-Tax IRR (%)	Post-Tax $NPV_{8\%}$ (A$M)
-17	1,250	10.4	62	8.2	5
-13	1,300	13.4	147	10.8	66
-6	1,400	19.0	317	15.4	186
0	**1,500**	**24.0**	**486**	**19.5**	**305**
6	1,600	28.7	656	23.3	424
12	1,700	33.2	826	26.8	543
17	1,800	37.4	995	30.2	662
21	1,900	41.5	1,165	33.5	781

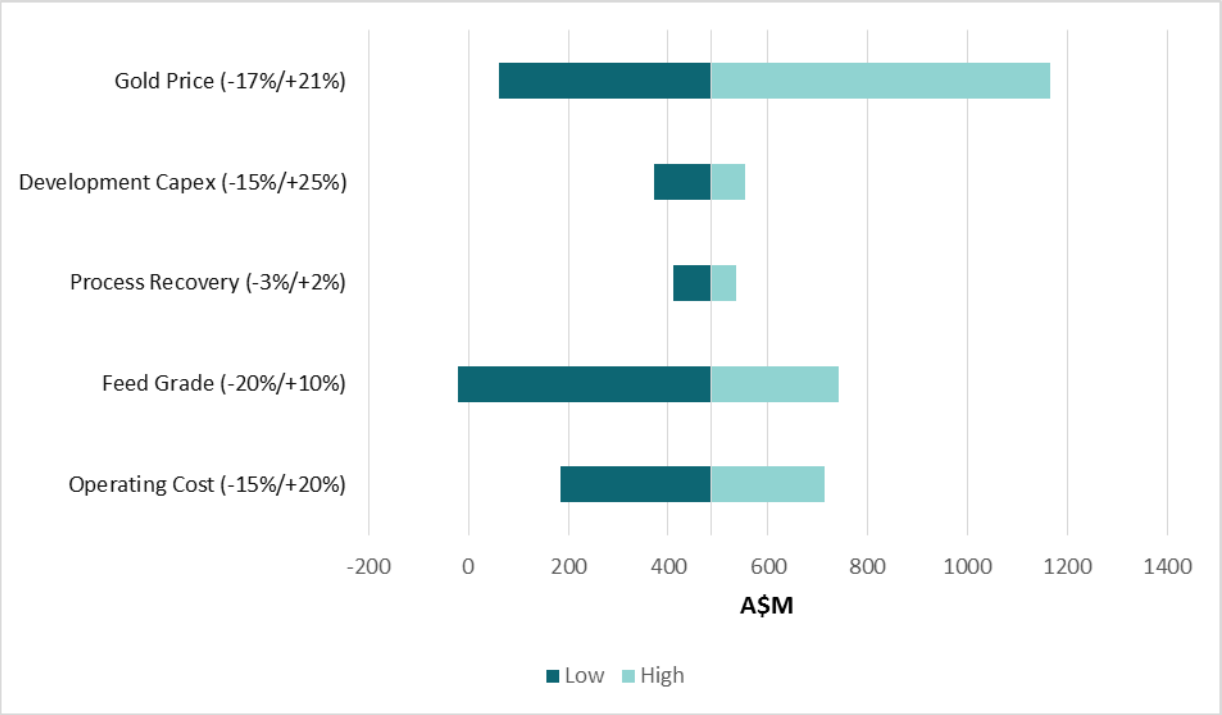


Figure 19: *Pre-Tax Net Present Value Sensitivity Chart*

Funding Options

To achieve the production targets and forecast financial information contained in the FS the Company will require a suitable funding solution. Gold Road's proposed financing strategy for the development of the Project will include, but not be limited to, the following factors:

- Securing a fully funded solution for the development of the Project
- Minimising potential dilution to existing Gold Road shareholders
- Providing flexible funding solutions to:
  - Ensure the continuation of exploration activities
  - Facilitate additional development opportunities
  - Capitalise on favourable external factors such as gold price (e.g. hedging when the spot price is substantially above the FS gold price assumptions).

The Company is reviewing and assessing the available funding options in order to maximise the benefits to shareholders and is confident, based on the work done to date, that the Project's strong economic and technical characteristics will enable the Company to secure approriate funding on competitive terms.

Potential funding options being considered include:

- **Traditional debt and equity structures:** Advanced discussions have been held with a number of local and international banking groups which have been shortlisted from 12 banks to seven. The process has revealed an extremely competetive funding environment for good quality Australian resource projects providing the Company with a high level of confidence that the Project will attract significant debt funding. The Company expects to be in a position to decide on a final syndicate selection to fund the debt component for the Project in the December 2016 Quarter. As with the debt markets, there remains good equity support for quality Australian resource projects. The Company, which currently has 63% Institutional shareholders, continues to receive indications of interest and support from existing and potential investors.

- **Sale of potential Gruyere joint venture project interest:** The Company has been in potential Joint Venture discussions with a selected group international and domestic mining companies since 2015. A number of indicative, incomplete and non-binding proposals have been received which reflect the quality and unique nature of the Gruyere investment. The Company has not made any decision in relation to these proposals and will consider them, at the appropriate time, in the context of the Company's various alternate funding options.

Community and Employment

The nearest town to the Project is Laverton, which has a population of 1,023 residents, of which 417 people permanently reside in the township (2011 census).

Cosmo Newberry, locally referred to as Cosmo, is a small indigenous Australian community with a population of 71 (2011 census), located approximately 80 kilometres north-west of Gruyere. The community is managed through its incorporated body, Cosmo Newberry Aboriginal Corporation (CNAC), incorporated under the Aboriginal Councils and Associations Act 1976 in 1991.

The Project is located within the Yilka Native Title claim area. The common law of Australia recognises a form of Native Title which reflects the entitlement of indigenous people, in accordance with their laws or customs, to enjoy their traditional lands. In May 2016, Gold Road entered into a comprehensive native title agreement, which includes extensive protections for Aboriginal heritage, for the Gruyere Project with the Yilka people.

On 29 June 2016, the Federal Court determined that the Yilka people (registered native title group) and the Sullivan Edwards group (unregistered native title group) were entitled to hold together native title in the area of the Gruyere Project. Gold Road considers that the Court's decision means that the Yilka people and the Sullivan Edwards group will hold native title together as a single group. Gold Road has been in discussions with the Sullivan Edwards group about how they may be able to participate in the benefits from Gold Road's native title agreement for the Gruyere Project. However, that is ultimately an intra-Indigenous decision, requiring agreement between the Yilka people and the Sullivan Edwards group.

Gold Road values the relationship that has been established with the majority of the traditional owners of the land on which the Project is located. Through an extensive engagement process that began in 2009, the Company has formed good working relations with the Yilka people and acquired a sound understanding of their cultural heritage.

Gold Road is committed to maintaining a long-term partnership with the traditional owners to ensure the Project can bring a range of benefits to the traditional owners, including direct and indirect employment.

Gold Road recognises the positive impacts that a long-term and large-scale mining operation such as Gruyere can bring to remote communities, such as possible business opportunities, and economic benefits through rates, taxes, charges and community investment. These aspects will be revisited during the construction and operations phase and additional opportunities will be explored.

Conclusion and Recommendations

The Board has approved the FS outcomes which indicate a technically sound and financially viable Project.

The optimum case for the Project is the development of a 15 year project, with conventional SABC CIL process plant and associated infrastructure for throughputs of 7.5 Mtpa of fresh ore and up to 8.8 Mtpa of transitional, oxide ores and blends powered by a gas fired power station.

Opportunities to optimise and enhance the financial performance of the Project will continue to be assessed and evaluated as the Project moves through development.

Next Steps

The immediate next step is the completion of the funding options analysis, which includes Project Finance and potential Joint Venture, before making the Financial Investment Decision.

The OEPA approval for the Project is anticipated to be granted in the March 2017 quarter, with construction likely to commence thereafter.

The Project development will be based on the Project execution strategy. It is planned that the Owner's team, utilising external contractors, will manage the Project execution. The EPC contract will include elements of lump sum and target cost arrangements. The gas-fired power station and associated gas pipeline will be built and operated by others through a BOO contract.

The high-level Project schedule is based on a five-month early works program followed immediately by a 24-month construction and commissioning timeframe with the objective of achieving first gold pour in the December 2018 quarter.

The execution strategy assumes assessment of the need for, and consideration given to, approval for early commitment items in the second half of 2016 and a Final Investment Decision, Project Financing in place and Project approval in the March 2017 quarter. The Company has the cash available for initial early works programmes from an equity capital raising completed in May 2016[26] specifically for this purpose.

Key milestones, subject to market conditions, for the execution of the Project are:

- December 2016 quarter:
  - Limited early works on site (accommodation village, access roads, communication towers)
  - Early commitment to the gas supply and conditional gas pipeline construction contract
  - Conditional award of EPC and Bulk Earthworks contract
- March 2017 quarter:
  - Project Finance or Joint Venture confirmed
  - Project approval from OEPA
  - Request for Tender for Mining Contract

[26] Refer ASX release 19 May 2016 – A$74M Equity Raising Successfully Completed

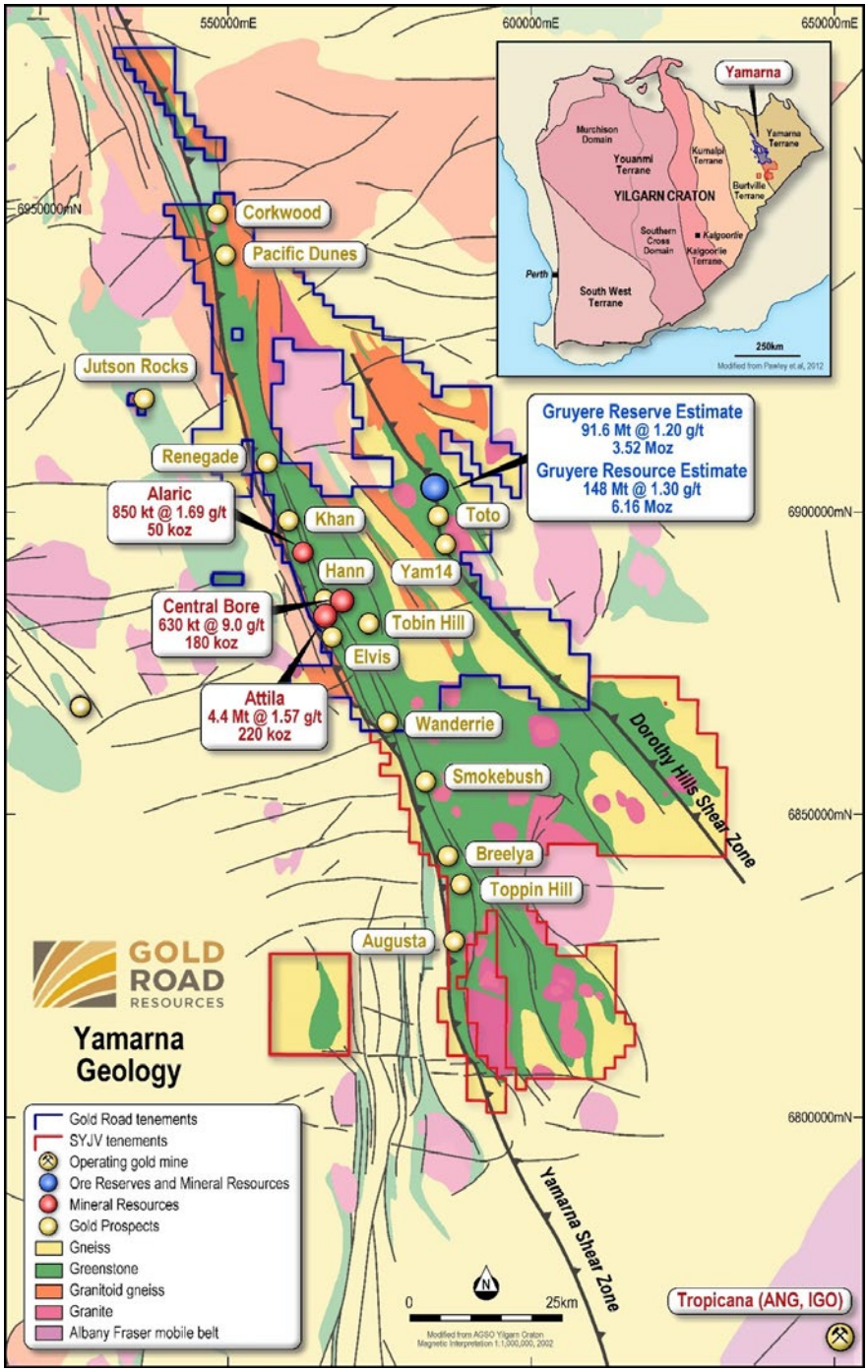


Figure 20: *Map showing the location of the Gruyere Project and Geology of Yamarna Belt, Gold Road's 100% tenements (blue outline) and Gold Road-Sumitomo South Yamarna Joint Venture tenements (red outline), September 2015 Mineral Resources, Gruyere Ore Reserve and main exploration projects. Note: Renegade previously named Khan North.*

APPENDIX 1: FORWARD-LOOKING AND CAUTIONARY STATEMENTS

Some statements in this report regarding estimates or future events are forward-looking statements. They include indications of, and guidance on, future earnings, cash flow, costs and financial performance. Forward-looking statements include, but are not limited to, statements preceded by words such as "planned", "expected", "projected", "estimated", "may", "scheduled", "intends", "anticipates", "believes", "potential", "could", "nominal", "conceptual" and similar expressions. Forward-looking statements, opinions and estimates included in this announcement are based on assumptions and contingencies which are subject to change without notice, as are statements about market and industry trends, which are based on interpretations of current market conditions. Forward-looking statements are provided as a general guide only and should not be relied on as a guarantee of future performance. Forward-looking statements may be affected by a range of variables that could cause actual results to differ from estimated results, and may cause the Company's actual performance and financial results in future periods to materially differ from any projections of future performance or results expressed or implied by such forward-looking statements. These risks and uncertainties include but are not limited to liabilities inherent in mine development and production, geological, mining and processing technical problems, the inability to obtain mine licenses, permits and other regulatory approvals required in connection with mining and processing operations, competition for among other things, capital, acquisitions of reserves, undeveloped lands and skilled personnel, incorrect assessments of the value of acquisitions, changes in commodity prices and exchange rate, currency and interest rate fluctuations, various events which could disrupt operations and/or the transportation of mineral products, including labour stoppages and severe weather conditions, the demand for and availability of transportation services, the ability to secure adequate financing and management's ability to anticipate and manage the foregoing factors and risks. There can be no assurance that forward-looking statements will prove to be correct.

Statements regarding plans with respect to the Company's mineral properties may contain forward-looking statements in relation to future matters that can only be made where the Company has a reasonable basis for making those statements.

This announcement has been prepared in compliance with the JORC Code (2012) and the current ASX Listing Rules.

The Company believes that it has a reasonable basis for making the forward-looking statements in this announcement, including with respect to any production targets and financial estimates, based on the information contained in this announcement and in particular:

The FS which was completed by independent engineering firm, GRES and AMC, who are considered to be Western Australian experts, together with Gold Road's Project Development Team under the direction of Sim Lau, Gold Road Project Director (BEng.(Civil) Monash University 1981). As is normal for this type of study, the FS has been prepared to an overall level of accuracy of approximately -10% to +15% .

The Company has a Mineral Resource Estimate for the Gruyere[27] Resource of 147.71 Mt at 1.30 g/t Au for 6.16 Moz (at a 0.5 g/t Au cut-off grade) of which 70%, being 104.98 Mt at 1.28g/t Au for 4.31 Moz, is classified in the Measured and Indicated Mineral Resource category under the JORC Code (2012).

The Gruyere Mineral Resource was estimated by Mr Justin Osborne and Mr John Donaldson of Perth, Western Australia in April 2016[28].

Metallurgical testwork, consistent with that required for this level of study, which forms the basis for estimates of metallurgical recoveries was managed by Gold Road's Principal Metallurgist, Mr Max Briggs who is a competent person and a Member of The Australasian Institute of Mining and Metallurgy, and performed by a number of specialist laboratories in Australia. Based on a nominal head grade of 1.20 g/t, estimated gold recoveries for the oxide, transitional and fresh ores are 94%, 92% and 91% respectively at the target grind size of 125 µm.

The mine planning and scheduling for the 7.5 Mtpa to 8.8 Mtpa production range was supervised by Mr David Varcoe of AMC Consultants, Mr Wayne Foote, General Manager – Operations, Mr Andrew Hollis, Project Mining

[27] Gruyere Resource Increases to 6.16 Million Ounces (ASX announcement dated 22 April 2016)
[28] Gruyere Resource Increases to 6.16 Million Ounces (ASX announcement dated 22 April 2016)

Manager and Mr Asam Shaibu, Principal Mining Engineer of Gold Road (mining engineers with considerable mine planning and operations experience and Members of the Australasian Institute of Mining and Metallurgy) utilising the Whittle Optimisation software (for open pit mine optimisation) and Studio 3 (for open pit mine planning). The entire mining inventory[29] is in Proved and Probable Ore Reserve categories, accounting for the entire 13 years of mine life.

GRES prepared the detailed process flowsheet based on metallurgical test work.

Geotechnical Engineering has been completed by Clive Seymour of Dempers and Seymour using modern geotechnical techniques and methods, and based on testwork consistent with this level of study. Dempers and Seymour are industry recognised experts in the field of mining geotechnical engineering.

The Project has been granted Lead Agency Status Level 2 by the Government of Western Australia. This means, by way of recognition of the size and significance of the Project to the State of Western Australia, all necessary State approval processes will be coordinated by specific individuals within the Department of Mines and Petroleum.

The Company believes that the investigations and studies carried out on the process flowsheet and the mine planning for this Study meet or exceed what would normally be expected for a FS.

Gold Road has had a very successful track record of adding Mineral Resources through greenfields and brownfields exploration across its tenements within the Yamarna Greenstone Belt. Gold Road is confident that there is a reasonable probability that it will continue to increase the Mineral Resources at the Project through exploration to extend the mine life past what is currently assumed in the FS. Attila and Central Bore resources have not been contemplated in the FS. The Gruyere deposit is located in the Yamarna Greenstone Belt which is highly prospective.

The Project's positive technical and economic fundamentals provide a platform for Gold Road to advance discussions with potential strategic partners and traditional financiers. Continued support from key institutional shareholders and strategic partners, current market conditions and an encouraging outlook for the global gold market enhance the Company's view of the fundability of the Project. The Board is confident the Company will be able to finance the Project through a combination of debt and equity or strategic partnerships.

Gold Road's Board and Management team includes Managing Director and CEO, Mr Ian Murray a qualified Chartered Accountant and mining industry professional with 20 years international corporate and mining experience, Executive Director Exploration and Growth, Mr Justin Osborne a geologist with more than 26 years exploration, mining, development and corporate experience, Non-Executive Chairman, Mr Tim Netscher who has extensive mining operational, project development and business development experience primarily with the larger international mining companies, General Manager Operations, Mr Wayne Foote, a mining engineer, who has more than 29 years' experience in the mining industry, the last 16 years at senior and executive management level. Gold Road Non-Executive Director, Sharon Warburton is a highly regarded company director, who has predominantly worked in the construction, mining and infrastructure sectors throughout a career that has spanned more than 25 years.

Additional experience is added by Gruyere Steering Committee Chairman, and Consultant to the Board, Mr Robin Marshall, who has more than 40 years' experience in the Mining and Mineral Processing Industry in Project Development, Execution and Operations/Engineering.

[29] See "Ore Reserve" on page 4

The Board and Management are well qualified and experienced to deal with any funding and project development challenges as they occur. In addition, the current state of the mining professional labour market is such that expert specialist input, when required, is available in Western Australia and can be sourced by Gold Road on a part-time or full-time basis.

The Study is based on the assumption that all gold produced will be refined at and sold to the Perth Mint, a statutory authority of the Government of Western Australia. The Perth Mint refines almost all gold doré bars produced in Western Australia. The gold market is a highly liquid international market with no need for offtake agreements.

PREVIOUSLY REPORTED INFORMATION

This annoucement includes information that relates to Mineral Resources and exploration results which were prepared and first disclosed under the JORC Code (2012). This information was included in the Company's previous annoucements as follows:

- ASX announcement dated 4 August 2014, Maiden Gruyere Resource
- ASX announcement dated 15 October 2014, Annual Report To Shareholders
- ASX announcement dated 20 January 2015, Mineralisation At Gruyere Extended To 750 Metres Depth
- ASX announcement dated 27 January 2015, Gruyere Scoping Study confirms long life Gold Project
- ASX announcement dated 28 May 2015, Gruyere Resource Grows To 5.51 Million Ounces Gold
- ASX announcement dated 3 August 2015, Gruyere Pre-Feasibility Study Stage 1 completed
- ASX announcement dated 16 September 2015, Gruyere Resource Increases To 5.62 Million Ounces
- ASX announcement dated 7 February 2016, Gruyere Pre-Feasibility Study confirms long life Gold Mine
- ASX announcement dated 22 April 2016, Gruyere Resource Increases To 6.16 Million Ounces (JORC Code 2012 Table 1 Sections 1 to 3 republised in Appendix 4 of this annoucement).

These announcements are available at the Company's website www.goldroad.com.au.

The Company confirms that it is not aware of any new information or data that materially affects the information included in the original market announcements and, in the case of estimates of Mineral Resources, that all material assumptions and technical parameters underpinning the estimates in the relevant market announcement continue to apply and have not materially changed. The Company confirms that the form and context in which the Competent Persons' findings are presented have not materially changed from the original market announcement.

APPENDIX 2: COMPETENT PERSONS

The information in this report that relates to the Mineral Resource Estimation for Gruyere is based on information compiled by Mr Justin Osborne, Executive Director for Gold Road and Mr John Donaldson, Geology Manager for Gold Road. Mr Osborne is an employee of Gold Road, as well as a shareholder and share option holder, and is a Fellow of the Australasian Institute of Mining and Metallurgy (FAusIMM 209333). Mr Donaldson is an employee of Gold Road as well as a shareholder, and is a Member of the Australian Institute of Geoscientists and a Registered Professional Geoscientist (MAIG RPGeo Mining 10147). Messrs Osborne and Donaldson have sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as Competent Persons as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Messrs Osborne and Donaldson consent to the inclusion in the report of the matters based on this information in the form and context in which it appears.

The information in this announcement that relates to process engineering design work and costing was prepared by GR Engineering Services Limited and was compiled under the guidance of Mr Bill Gosling who is a Fellow of the Australasian Institute of Mining and Metallurgy. Mr Gosling has sufficient experience that is relevant to the style of mineralisation and proposed processing and to the activity currently being undertaken to qualify as a Competent Persons as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Gosling consents to the inclusion in this announcement of the matters based on his information in the form and context in which it appears.

The information in this report that relates to Ore Reserves is based on information compiled by David Varcoe of AMC Consultants, a competent person who is a Member of The Australasian Institute of Mining and Metallurgy. Mr Varcoe has sufficient experience that is relevant to the style of mineralisation and type of deposits under consideration and to the activity currently being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Varcoe consents to the inclusion in this announcement of the matters based on his information in the form and context in which it appears.

APPENDIX 3: JORC CODE 2012 TABLE 1 – SECTION 4

Section 4 Estimation and Reporting of Ore Reserves

The Company has relied upon its previously reported information, in particular the announcement of 22 April 2016, as set out in the announcements listed in Appendix 1, in respect of the matters related to sections 1, 2 and 3.

(Criteria listed in section 1, and where relevant in sections 2 and 3, also apply to this section.)

Criteria	JORC Code (2012) explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve. *Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.*	The Mineral Resource estimate for the Gruyere deposit which formed the basis of this Ore Reserve estimate was compiled by the Gold Road Competent Person(s) utilising relevant data. The estimate is based on 357 Reverse Circulation (RC) holes and 113 diamond holes of exploration drilling and assay data. The data set, geological interpretation and model was validated using Gold Road's internal and Quality Assurance and Quality Control (QAQC) processes and reviewed by an independent external consultant. Ordinary Kriging was utilised to estimate the Measured component of the resource and Localised Uniform Conditioning was utilised to estimate the Indicated and Inferred components of the resource. The individual block size for estimation was 5 mE x 12.5 mN x 5 mRL for both methods. The Mineral Resources are reported inclusive of the Ore Reserve (refer ASX announcement 22 April 2016).
Site visits	Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is the case.	The Competent Person conducted a site visit in October 2015. The following activities were completed: ▪ Gained general familiarisation with the site including likely mining conditions, proposed pit location, waste dump location, site drainage and site access ▪ Assessed proposed locations of mining related infrastructure relative to the designed open pit ▪ Observed resource drilling activities ▪ Inspected air core drill hole sites to get an understanding of the variations in weathering profiles across the deposit ▪ Viewed diamond drill core from selected samples.
Study status	The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves. The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.	The Ore Reserve estimate is the result of a detailed Feasibility Study (FS) completed by a team consisting of Gold Road personnel and independent external consultants. The proposed mine plan is technically achievable. All technical proposals made for the operational phase involve the application of conventional technology which is widely utilised in the goldfields of Western Australia (WA). Financial modelling completed as part of the FS shows that the project is economically viable under current assumptions. Material Modifying Factors (mining, processing, infrastructure, environmental, legal, social and commercial) have been considered during the Ore Reserve estimation process.

Criteria	JORC Code (2012) explanation	Commentary
Cut-off parameters	The basis of the cut-off grade(s) or quality parameters applied.	Variable economic cut-off grades have been applied in estimating the Ore Reserve. Cut-off grade is calculated in consideration of the following parameters: ▪ Gold price ▪ Operating costs ▪ Process recovery ▪ Transport and refining costs ▪ General and administrative cost ▪ Royalty costs.
Mining factors or assumptions	The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design). The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.	Gruyere will be mined by open pit mining methods utilising conventional mining equipment. Final pit and interim stage designs were completed as part of the FS. The final pit design is the basis of the Ore Reserve estimate. The selected mining method, design and extraction sequence are tailored to suit orebody characteristics, minimise dilution and ore loss, defer waste movement and capital expenditure, utilise proposed process plant capacity and expedite free cash generation in a safe and environmentally sustainable manner. Mining operating and capital costs were estimated as part of the FS and referenced against contractor budget quotes.
	The assumptions made regarding geotechnical parameters (e.g. pit slopes, stope sizes, etc), grade control and pre-production drilling.	Geotechnical modelling has been completed by an external consultant on the basis of field logging and laboratory testing of selected dedicated diamond drill core samples. The recommended geotechnical design parameters assume dry slopes on the basis of adequate dewatering ahead of mining. Eleven geotechnical domains were identified: ▪ Domain West 1: - Weathered material: batter heights of 10m, batter angles of 50° - 55° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 60° - 75° and berm widths of 9m. ▪ Domain West 2AN: - Weathered material: batter heights of 10m, batter angles of 55° - 60° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 70° - 80° and berm widths of 6m. ▪ Domain West 2B: - Weathered material: batter heights of 10m, batter angles of 55° - 60° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 60° - 80° and berm widths of 12m. ▪ Domain West 2AS: - Weathered material: batter heights of 10m, batter angles of 55° - 60° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 60° - 80° and berm widths of 6m. ▪ Domain West 3, East 4: - Weathered material: batter heights of 10m, batter angles of 55° - 60° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 60° - 80° and berm widths of 9m. ▪ Domain West 4: - Weathered material: batter heights of 10m, batter angles of 50° - 55° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 60° - 80° and berm widths of 8m. ▪ Domain East 1: - Weathered material: batter heights of 10m, batter angles of 50° - 55° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 60° - 80° and berm widths of 9m.

Criteria	JORC Code (2012) explanation	Commentary
		▪ Domain East 2: - Weathered material: batter heights of 10m, batter angles of 55° - 60° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 60° - 80° and berm widths of 8m. ▪ Domain East 3: - Weathered material: batter heights of 10m, batter angles of 55° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 60° - 80° and berm widths of 11m. ▪ Domain East 5: - Weathered material: batter heights of 10m, batter angles of 55° and berm widths of 5m - Fresh material: batter heights of 20m, batter angles of 55° and berm widths of 6m. A separate hydrogeological report was prepared by independent consultants which considered the infrastructure required to effectively dewater the open pit and pit slopes. This study was supported by the development of test bores and field test pumping analysis.
	The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate). The mining dilution factors used. The mining recovery factors used. Any minimum mining widths used.	Mining dilution and recovery modifying factors were simulated by modelling to a Selective Mining Unit (SMU) then applying a dilution skin at each ore to waste contact across the orebody, and then re-estimating the resultant tonnes and grades of neighbouring blocks due to the impact of including dilution at that contact. A configuration of 5 mE x 12.5 mN x 5 mRL with a 0.5 m dilution skin was applied which represents the capability of the selected mining fleet. The modelling yielded the following results: ▪ Mining tonnage dilution of 3.2% ▪ Mining grade dilution of 4.6% ▪ Mining recovery factor of 98.6% (gold loss of 1.4%) These values reflect the fact that Gruyere is a relatively simple continuous orebody with individual ore shape designs of hundreds of metres along strike and 20 to 50 m wide.
Mining factors or assumptions	The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.	The mining schedule is based on supplying variable throughput rates to a processing plant with a name plate capacity of 7.5 Mtpa for fresh ore material with the capability to treat up to 8.0 Mtpa of transition material and up to 8.8 Mtpa of oxide material. The mining schedule is based on realistic mining productivity and equipment utilisation estimates and also considered the vertical rate of mining development. Inferred Mineral Resources were considered as waste during the pit optimisation and production scheduling process. Waste material from mining activities will be disposed of as follows: ▪ Topsoil will be disposed of at designated stockpiles for application in on-going rehabilitation activities; ▪ Initial saprolite waste will be utilised to construct the base and starter embankment of the Tailings Storage Facility (TSF); ▪ Some waste rock will be utilised to construct the Run Of Mine (ROM) pad; ▪ Some waste rock will be utilised to construct on-going TSF lifts; ▪ Excess waste rock will be disposed of at designated waste rock dumps.

Criteria	JORC Code (2012) explanation	Commentary
	The infrastructure requirements of the selected mining methods.	The proposed mine plan includes waste rock dumps, a ROM pad, a surface water diversion channel, surface dewatering bores, light and heavy vehicle workshop facilities, explosives storage and supply facilities and technical services and administration facilities.
Metallurgical factors or assumptions	The metallurgical process proposed and the appropriateness of that process to the style of mineralisation. Whether the metallurgical process is well-tested technology or novel in nature. The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied. Any assumptions or allowances made for deleterious elements. The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole. For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?	A processing flowsheet, materials balance, water balance, equipment identification, mechanical and electrical layouts were all developed to FS standard. A single stage primary crush, Semi Autogenous Grinding and Ball Milling with Pebble Crushing (SABC) comminution circuit followed by a conventional gravity and carbon in leach (CIL) process is proposed. This process is considered appropriate for the Gruyere ore, which is classified as free-milling. The proposed metallurgical process is commonly used in the Australian and international gold mining industry and is considered to be well-tested and proven technology. Significant comminution, extraction, and materials handling testing has been carried out on approximately 2,000kg of half-NQ (NQ core diameter = 47.6mm) diamond drilling core samples, and 480kg of RC chip samples. This has been carried out on oxide, saprock, transitional, and fresh ore types which were obtained across the Gruyere deposit (South to North) and to a depth of approximately 300m. Estimated plant gold recovery ranges from 87% to 95% depending on head grade, plant throughput, grind size and ore type. Significant comminution, extraction, and materials handling testing has been carried out on material selected from approximately 2,000kg of half-NQ core. No deleterious elements of significance have been determined from metallurgical test work and mineralogy investigations.
Environmental	The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.	Baseline environmental studies of flora, vegetation, vertebrate fauna, short-range endemic invertebrates and subterranean fauna are all completed. Environmental approvals for the mining and water supply aspects of the project will be assessed by the EPA and the Department of Mines and Petroleum WA (DMP). The approvals document to EPA has and the approvals document to the DMP will be submitted in Q4 2016. Environmental approvals for the gas pipeline aspect of the project has been assessed by the EPA, and will be assessed by the DMP for a petroleum pipeline licence and clearing permit in 2017. Waste rock and tailings characterisation work has been completed and all waste types and tailings are non-acid forming and have limited metal leachate potential. Waste rock and tailings storage locations have been selected based on suitable geographical characteristics and proximity to the pit and plant.
Infrastructure	The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.	The project site is within economic distances of existing infrastructure of the Eastern Goldfields region. Services and consumable supplies will be delivered by existing roads from Laverton some 150km to the west. A gas supply lateral from the Eastern Goldfields Pipeline will be built from Laverton to site to supply gas to a purpose built gas fired power station. The workforce will be Fly In-Fly Out (FIFO) and based at a camp on site during rostered days on. An on-site airstrip is to be built as part of the project. Pump testing and modelling of the potential yield from the Yeo and Anne Beadell borefields indicate that there is sufficient groundwater to service the needs of the Project for the life-of-mine. The primary source of water for the project will be developed over approximately 65 km of tested palaeochannel. In addition to the tested palaeochannel length, approximately 100 km of palaeochannel is available for potential development on tenements with granted miscellaneous water search licences.

Criteria	JORC Code (2012) explanation	Commentary
		Miscellaneous licence applications have been lodged to secure the tenure required for the water and gas pipelines and a new section of road for site access. Granting of the remaining miscellaneous licence applications for the Yeo borefield is expected in Q4 2016 and for the gas pipeline infrastructure is expected in Q1 2017.
Costs	The derivation of, or assumptions made, regarding projected capital costs in the study	All capital estimates are based on market rates as at the second quarter of 2016. It is assumed that all mining equipment required for the project will be supplied by a mining contractor. It is assumed that power infrastructure will be supplied by a third party under a Build-Own-Operate arrangement to supply power at a cost to the project. The capital cost estimate accuracy is -10% /+15%. Mine development costs were developed from a combination of inputs from Gold Road, AMC Consultants, GR Engineering Services and Pennington Scott Hydrogeologists. The basis of estimate is: ▪ Contract mining ▪ Mobilisation of mining equipment and personnel from Perth ▪ Earthworks quantities determined from detailed site inspections by a competent civil engineer and geological modelling ▪ Mine dewatering requirements developed from FS level hydrogeological modelling ▪ A mining schedule developed on a quarterly basis ▪ A contingency allowance on capital cost items calculated to reflect the relevant level of confidence in the estimate Processing and infrastructure development capital costs have been estimated by GR Engineering Services (GRES) on the basis of: ▪ Earthworks quantities determined from detailed site inspections by a competent civil engineer ▪ Concrete and structural quantities developed from site layouts and similar designs from other projects ▪ A mechanical equipment list developed from the recommended process design criteria ▪ Budget pricing from local and international suppliers ▪ Contingency allowances calculated on a line by line basis relevant to the source and confidence in market rates

<table>
<tr><th>Criteria</th><th>JORC Code (2012) explanation</th><th>Commentary</th></tr>
<tr><td rowspan="4">Costs</td><td>The methodology used to estimate operating costs.</td><td>The operating cost estimate accuracy is -10% /+15%.
Operating costs assume a FIFO scenario with various rosters on site.
Mining operating costs have been estimated by AMC on the basis of scheduled material movement and mining rates for a contractor mining scenario with technical services supplied by Gold Road employees. Mine design and scheduling was prepared by competent mining engineers.

Process and infrastructure operating costs have been estimated by GRES on the assumption that:
▪ A conventional SABC circuit will be utilised to treat ore at a rate of 7.5 Mtpa for fresh ore with the capability to treat up to 8.8 Mtpa of oxide material
▪ Comminution grind sizes will be in the range of 106µm to 150µm for all material types
▪ Power will be generated on site utilising gas delivered by pipeline
▪ The process plant will be operated by Gold Road employees.
The operating cost estimate is considered to be appropriate for the current market in the eastern goldfields of WA.</td></tr>
<tr><td>Allowances made for the content of deleterious elements.</td><td>No allowance is made for deleterious elements since testwork to date on ore from Gruyere has not shown the presence of deleterious elements.</td></tr>
<tr><td>The source of exchange rates used in the study.</td><td>Capital Costs for process plant and infrastructure are estimated in 2016 Australian dollars.
Foreign currency exchange rates were derived as tabled below.
<table>
<tr><th>Currency</th><th>Rate (A$1 = X)</th><th>Source</th></tr>
<tr><td>United States Dollar</td><td>0.75</td><td>Gold Road</td></tr>
<tr><td>Euro</td><td>0.66</td><td>online</td></tr>
<tr><td>Chinese Renminbi</td><td>4.87</td><td>online</td></tr>
</table></td></tr>
<tr><td>The derivation of, or assumptions made, regarding projected capital costs in the study. Derivation of transportation charges.
The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.
The allowances made for royalties payable, both Government and private.</td><td>Transport charges - Gold bullion transportation charges are derived on the basis of a quote provided by a leading industry bullion shipment organisation.
Treatment and refining charges are estimated on the basis of a quote from a leading Perth Gold Refinery.
An allowance has been made for all royalties, including an allowance of 2.5% of revenue for royalties payable to the Western Australian State Government and an allowance for other royalties payable to private parties (these royalties being commercially sensitive and covered by confidentiality).</td></tr>
<tr><td>Revenue factors</td><td>The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.
The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.</td><td>The mined ore head grades are estimated utilising industry accepted geostatistical techniques with the application of relevant mining modifying factors.
Gold price and exchange rates have been determined by an external financial expert group on the basis of current market trends.
A Life-of-mine (LOM) gold price forecast of A$1,500/oz (Real 2016) is applied in the financial modelling for the Ore Reserve calculation process. This price forecast was established by Gold Road on the basis of historical A$ gold price trends over the last 5 years. Over that review period the price of gold has ranged between A$1,300/oz and A$1,800/oz and averaged approximately A$1,500/oz.</td></tr>
</table>

<table>
<tr><th>Criteria</th><th>JORC Code (2012) explanation</th><th>Commentary</th></tr>
<tr><td>Market assessment</td><td>The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.
A customer and competitor analysis along with the identification of likely market windows for the product.
Price and volume forecasts and the basis for these forecasts.
For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.</td><td>There is a transparent market for the sale of gold.</td></tr>
<tr><td>Economic</td><td>The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.
NPV ranges and sensitivity to variations in the significant assumptions and inputs.</td><td>▪ Discounted cash flow modelling and sensitivity analysis has been completed to evaluate the economic performance of the Ore Reserve. Key value driver inputs into the financial model included:
▪ Gold price at A$1,500/oz based on historical trends over the last 5 years.
▪ Discount rate of 8% as determined by the Board of Directors of Gold Road.
▪ The Ore Reserve returns a positive NPV of A$305M (post-tax) under the assumptions detailed herein.
▪ The table below shows the results of sensitivity analysis on key project variables.
<table>
<tr><th>% Change in Variable</th><th>-10%</th><th>0%</th><th>10%</th></tr>
<tr><td></td><td colspan="3">% Change in Project NPV (Post-Tax)</td></tr>
<tr><td>Gold Price</td><td>-59%</td><td>-</td><td>59%</td></tr>
<tr><td>Process Recovery</td><td>-59%</td><td>-</td><td>59%</td></tr>
<tr><td>Mining Cost</td><td>16%</td><td>-</td><td>-16%</td></tr>
<tr><td>Processing Cost</td><td>18%</td><td>-</td><td>-18%</td></tr>
<tr><td>Development Capex</td><td>12%</td><td>-</td><td>-12%</td></tr>
</table>
▪ The project NPV (Post Tax) is most sensitive to variations in the gold price and process recovery.
▪ A 10% reduction in gold price or process recovery reduces NPV by 59%. A 10% increase in gold price or process recovery increases NPV by 59%.</td></tr>
<tr><td>Social</td><td>The status of agreements with key stakeholders and matters leading to social licence to operate.</td><td>A Native Title Mining Agreement has been signed for the Project (ASX Announcement 4 May 2016: Historic Native Title Agreement In Place for Gruyere Project). Subsequent to the Native Title Agreement, a Mining Lease was granted over the project area (ASX Announcement 9 May 2016: Yamarna Mining Leases Granted). Several key miscellaneous licences have also been granted (ASX Announcement 29 September 2016: Gruyere Gold Project to Commence Limited Early Works).</td></tr>
</table>

Criteria	JORC Code (2012) explanation	Commentary
Other	To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves: Any identified material naturally occurring risks. The status of material legal agreements and marketing arrangements. The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.	▪ Flooding risk has been analysed by an independent external expert and appropriate mitigation strategies have been included in the FS. ▪ No significant species have been identified that would be significantly impacted by the Project in a manner that could not be adequately managed. ▪ Mining and gas pipeline contract negotiations have commenced. There are reasonable prospects to anticipate that contract terms as assumed in the Ore Reserves estimate will be achieved. Project commissioning is estimated for 2018.
Classification	The basis for the classification of the Ore Reserves into varying confidence categories. Whether the result appropriately reflects the Competent Person's view of the deposit. The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).	The main basis of classification of Ore Reserves is the underlying Mineral Resource classification. All Proved Ore Reserves derive from Measured Mineral Resources and all Probable Ore Reserves derive from Indicated Mineral Resources in accordance with JORC Code (2012) guidelines. The results of the Ore Reserve estimate reflect the Competent Person's view of the deposit. No Probable Ore Reserves are derived from Measured Mineral Resources. No inferred Mineral Resource is included in the Ore Reserves. 16% of the Ore Reserve is in the Proved category with the balance (84%) being Probable.
Audits or reviews	The results of any audits or reviews of Ore Reserve estimates.	The FS which forms the basis of the Ore Reserve estimate was subjected to various reviews and audits: ▪ Metallurgical testwork was reviewed by Gold Road metallurgists and process engineers and confirmed to be adequate for a FS. ▪ Geotechnical input was reviewed by external independent consultants and found to be acceptable for a FS. ▪ Open pit designs, production schedules and mining cost models were reviewed through AMC's internal peer review system and externally by an independent technical expert. ▪ The basis of design for the process plant and infrastructure was reviewed by Gold Road metallurgists and process engineers and was deemed appropriate for a FS. ▪ Capital cost estimates were reviewed by an external independent consultant and were considered to be appropriate for a FS. ▪ The financial model applied for project valuation was reviewed by Gold Road financial accountants and was considered to be appropriate for a FS. ▪ The overall FS was reviewed by an independent technical expert and was considered to be appropriate.

Criteria	JORC Code (2012) explanation	Commentary
Discussion of relative accuracy/ confidence	Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate. The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used. Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage. It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	The Gruyere FS resulted in a technically robust and economically viable business case. This is deemed to be an appropriate basis for a high level of confidence in the Ore Reserves estimate. In the opinion of the Competent Person, cost assumptions and modifying factors applied in the process of estimating Ore Reserves are reasonable. Gold price and exchange rate assumptions were set out by Gold Road and are subject to market forces and present an area of uncertainty. In the opinion of the Competent Person, there are reasonable prospects to anticipate that all relevant legal, environmental and social approvals to operate will be granted within the project timeframe.

APPENDIX 4: JORC CODE 2012 TABLE 1 – SECTIONS 1 TO 3[30]

Section 1 Sampling Techniques and Data

Note: Details for drilling data used in the Gruyere Mineral Resource has previously been reported in ASX Announcements released between 14 October 2013 and 27 January 2016. These announcements are listed in Appendix 2 of this release. The data for the 25 by 25 m RC program has not been publicly released as it is considered to be operational in nature. These holes were treated with the same geological protocols as described in Table 1 below.

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	*Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*	The sampling has been carried out using a combination of Reverse Circulation (**RC**) and Diamond Drilling (**DDH**). RC drill samples are collected through a rig-mounted cone splitter designed to capture a one metre sample with optimum 3 to 4kg sample weight. Drill core is logged geologically and marked up for assay at approximate one metre intervals based on geological observation. Drill core is cut in half by a diamond saw and half core samples submitted for assay analysis. Detailed descriptions of drilling orientation relative to deposit geometries, and full sample nature and quality are given below.
	Include reference to measures taken to ensure sample representation and the appropriate calibration of any measurement tools or systems used.	Sampling was carried out under Gold Road's protocols and QAQC procedures as per industry best practice. See further details below.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	RC holes were drilled with a 5.25 inch face-sampling bit, 1 m samples were collected through a cyclone and cone splitter to form a 2-4 kg sample. All holes with reported assays from RC drilling are from the original 1 m samples collected from the splitter except for 1% of RC samples, which were four metre composite samples collected through logged waste zones. The 4 m composite samples were created by spear sampling of the total 1 m samples collected in large plastic bag from the drilling rig and were deposited into separate numbered calico bags for sample despatch. No assays collected by four metre composite sampling were used in the Resource estimation. Diamond drilling was completed using an HQ or NQ drill bit for all holes. Core is cut in half for sampling, with a half core sample sent for assay at measured intervals. Both RC and diamond samples were fully pulverised at the laboratory to -75um, to produce a 50g charge for Fire Assay with an AAS finish up until May 2014 and ICPES finish post this date.
Drilling techniques	*Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	RC drilling rigs, owned and operated by Raglan Drilling, were used to collect the RC samples. The face-sampling RC bit has a diameter of 5.25 inches (13.3 cm). Diamond drilling rigs operated by Terra Drilling Pty Ltd collected the diamond core as NQ or HQ size. The majority of diamond holes used RC pre-collars to drill through barren hanging-wall zones to specified depth, followed by diamond coring at NQ size from the end of the pre-collar to the end of hole. This ensured diamond core recovery through the mineralised zones within the Gruyere Porphyry. Core is oriented using downhole Reflex surveying tools, with orientation marks provided after each drill run.

[30] Refer ASX announcement dated 22 April 2016

Criteria	JORC Code explanation	Commentary
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.*	The majority of RC samples were dry. Ground water egress occurred in some holes at variable depths between 100 and 400 m. Drill operators ensured that water was lifted from the face of the hole at each rod change to ensure that water did not interfere with drilling and that all samples were collected dry. When water was not able to be isolated from the sample stream the drill hole was stopped and drilling was completed with a diamond tail. RC recoveries were visually estimated, and recoveries were recorded in the log as a percentage. Recovery of the samples was good, generally estimated to be close to 100%, except for some sample loss at the top of the hole. All diamond core collected is dry. Drill operators measure core recoveries for every drill run completed using a 3 m core barrel. The core recovered is physically measured by tape measure and the length recovered is recorded for every 3 m "run". Core recovery is calculated as a percentage recovery. Close to 100% recoveries were achieved for the majority of diamond drilling completed at Gruyere.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	RC face-sampling bits and dust suppression were used to minimise sample loss. Drilling air pressure lifted the water column above the bottom of the hole to ensure dry sampling. RC samples were collected through a cyclone and rotary cone splitter. The rejects were deposited in a large plastic bag and retained for potential future use. The sample required for assay is collected directly into a calico sample bag at a designed 3 - 4 kg sample mass which is optimal for whole-of-sample pulverisation at the assay laboratory. Diamond drilling results in uncontaminated fresh core samples which are cleaned at the drill site to remove drilling fluids and cuttings to present clean core for logging and sampling.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	All RC samples were dry with the exception of a few samples (<5%) that were reported as slightly damp to the end of the hole. Apart from the tops of the holes while drilling through the sand dune cover, there is no evidence of excessive loss of material and at this stage no information is available regarding possible bias due to sample loss. There is no significant loss of material reported in any of the Diamond core.
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	All chips and drill core were geologically logged by Gold Road geologists, using the Gold Road logging scheme. This provides data to a level of detail adequate to support Mineral Resource Estimation activities. Approximately 30% of holes have been surveyed using downhole optical (OTV) and/or acoustic (ATV) televiewer tools which provide additional information suitable for geotechnical and specific geological studies. A full set (49,425 to 50,950 mN) of 25 m spaced manually interpreted cross-sections were geo-referenced and used to guide digital construction of material type wireframes. A weathering profile guide was developed as part of the process in order to document the features and provide a guide for further logging and open pit mapping. Nine specific geotechnical diamond holes were drilled to support the PFS and a further 12 drilled to support the FS. The holes were designed and logged in geotechnical detail by Dempers and Seymour Pty Ltd Geotechnical Mining Consultants. Collaboration between the geological and geotechnical groups has resulted in refinement of the geological interpretation, particularly the understanding of significant faults and shear zones. Metallurgical composite samples selected over the life of the project have been based on the detailed logging information, gold grades and geological interpretation.

Criteria	JORC Code explanation	Commentary
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.	Logging of RC chips records lithology, mineralogy, mineralisation, weathering, colour and other features of the samples. All samples are wet-sieved and stored in a chip tray. Logging of drill core records lithology, mineralogy, mineralisation, weathering, colour and other features of the samples, along with structural information from oriented drill core. All samples are stored in core trays. All core is photographed in the trays, with individual photographs taken of each tray both dry, and wet; all photos are uploaded to and stored in the Gold Road server database.
	The total length and percentage of the relevant intersections logged	All RC and diamond holes were logged in full.
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.*	Core samples were cut in half using an automated Corewise diamond saw. Half core samples were collected for assay, and the remaining half core samples are stored in the core trays.
	If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.	One metre RC drill samples are collected via a rotary cone-splitter, installed directly below a rig mounted cyclone, and an average 2-3 kg sample is collected in an un-numbered calico bag, and positioned on top of the plastic bag. >95% of samples were collected dry (dry to slightly damp). Four-metre composite samples were created by spear sampling of the total one metre samples collected in large plastic bag from the drilling rig and deposited into separate numbered calico bags for sample despatch. A number of RC holes utilised 4 m composite samples for waste intervals. *If composite samples returned anomalous gold values, the intervals were resampled as one metre samples by collecting the sample produced from the rotary cone-splitter.* No 4 m sample assays were used in this Mineral Resource Estimate.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	Samples were prepared at the Intertek Laboratory in Kalgoorlie. Samples were dried, and the whole sample (both RC and DDH) was pulverised to 80% passing 75um, and a sub-sample of approx. 200g was retained. A nominal 50g was used for the analysis. The procedure is better than industry standard for this type of sample as most labs split the 2-3 kg prior to pulverising.
	Quality control procedures adopted for all sub-sampling stages to maximise representation of samples.	A duplicate RC field sample is taken from the cone splitter at the same time as the primary sample a rate of approximately 1 in 40 samples. A twinned half core sample is taken at a frequency of 1 in 40 samples, with one half representing the primary result and the second half representing a twinned result. At the laboratory, regular laboratory-generated repeats and check samples are assayed, along with laboratory insertion of its own standards and blanks.
	Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.	Duplicate samples were collected at a frequency of 1 in 40 for all drill holes. RC duplicate samples are collected directly from the rig-mounted rotary cone splitter. Core duplicate samples utilise the second half of core after cutting.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Sample sizes are considered appropriate to give an indication of mineralisation given the particle size and the preference to keep the sample weight below a targeted 3kg mass which is the optimal weight to ensure the requisite grind size in the LM5 sample mills used by Intertek in sample preparation.

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td rowspan="3">Quality of assay data and laboratory tests</td><td>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</td><td>Samples were analysed at the Intertek Laboratory in Perth. The analytical methods used for RC and diamond drilling methods for raw (not composited) samples in a 10km square region surrounding the deposit were as follows:
<table><tr><th>Azimuth (Gruyere Grid)</th><th>DDH</th><th>RC</th><th>Total</th></tr><tr><td>50 gram Fire Assay with AAS finish</td><td>6,295</td><td>13,888</td><td>20,183</td></tr><tr><td>50 gram Fire Assay with ICPES finish</td><td>17,206</td><td>20,337</td><td>37,543</td></tr><tr><td>Total</td><td>23,501</td><td>34,225</td><td>57,726</td></tr></table>
Fire Assay with either AAS or ICPES finish for gold is considered to be appropriate for the Gruyere material and mineralisation. The method gives a near total digestion of the material intercepted in diamond core drilling. ICPES provides improved quality compared to AAS and all fire assay protocols for Gold Road samples were changed to this finish during May 2014.</td></tr>
<tr><td>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</td><td>Calibration of the hand-held XRF tools is applied at start-up. XRF results are only used for indicative assessment of lithogeochemistry and alteration to aid logging and subsequent interpretation.

Downhole survey of rock property information for selected holes reported has been completed. ABIMS is the contractor which compiled this work. This involved downhole surveying using a variety of tools with real time data capture and validation. The tools were calibrated on a regular basis. This data was used in conjunction with other data in the determination of specific gravity (SG) data for the Resource Model.</td></tr>
<tr><td>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</td><td>The Gold Road protocol for RC programs is for Field Standards (Certified Reference Materials) and Blanks to be inserted at a rate of 3 Standards and 3 Blanks per 100 samples. RC Field Duplicates and DDH Field Twins are generally inserted at a rate of approximately 1 in 40. Samples are processed at Intertek Laboratories, where regular assay Repeats, Laboratory Standards, Checks and Blanks are inserted and analysed in addition to the blind Gold Road QAQC samples.

For the reported resource the relevant assays and QAQC numbers are as follows:
<table><tr><th rowspan="2">Assay and QAQC Numbers</th><th colspan="2">April 2016</th></tr><tr><th>Number</th><th>Comment</th></tr><tr><td>Total Sample Submission</td><td>58,137</td><td></td></tr><tr><td>Field Blanks</td><td>1,536</td><td></td></tr><tr><td>Field Standards</td><td>1,526</td><td></td></tr><tr><td>Filed Duplicates</td><td>1,148</td><td></td></tr><tr><td>Laboratory Blanks</td><td>1,259</td><td>including 98 Acid Blanks</td></tr><tr><td>Laboratory Checks</td><td>1,855</td><td></td></tr><tr><td>Laboratory Standards</td><td>1,868</td><td></td></tr><tr><td>Umpire Checks - Minanalytical</td><td>236</td><td>including 5 Laboratory Blanks and 10 Laboratory Standards</td></tr><tr><td>Umpire Checks - ALS Laboratories</td><td>62</td><td>including 4 Laboratory Blanks and 6 Laboratory Standards</td></tr></table></td></tr>
</table>

Criteria	JORC Code explanation	Commentary
		Results of the Field and Laboratory QAQC assays were checked on assay receipt using QAQCR software. All assays passed QAQC protocols, showing acceptable levels of contamination or sample bias, including diamond half core v. half core Field Twins. QAQC Audits for each major drill program and associated resource update have been completed and reported by Mr David Tullberg (Grassroots Data Services Pty Ltd) and by Dr Paul Sauter (in-house consultant Sauter Geological Services Pty Ltd).
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.*	Significant results were compiled by the Database Manager and reported for release by the Exploration Manager/Executive Director. Data was routinely checked by the Senior Exploration and Project Geologist, Principal Resource Geologist or Consulting Geologists during drilling programs. All results, except for the 25 by 25 m RC data, which is considered operational, have been reported in ASX announcements listed in Appendix 2.
	The use of twinned holes.	Three twin RC holes were completed and data analysed in the reported resource, with their collars being less than 5 metres distant from the parent collar. ▪ 14GYRC0026A (twin pair with hole 13GYRC0026) ▪ 14GYRC0033A (twin pair with hole 14GYRC0033) ▪ 14GYRC0060A (twin pair with hole 13GYRC0060) Two twin RC vs DDH sub-parallel holes were completed and data analysed in the reported resource, with their collars being less than 10 metres distant from the parent collar. ▪ 13GYDD0003 (twin pair with hole 13GYRC0027) ▪ 13GYDD0002 (twin pair with hole 13GYRC0049) One diamond pair (14GYDD0012A and 14GYDD0012B) provide a twin data set over a length of 120 m at a spacing of less than less than 4 m apart. This twinned data provided accurate data for validating the nugget effect at Gruyere. As part of the Maiden Mineral Resource reported in August 2014 a detailed drill program was completed which included a number of holes on an approximate 12.5 by 12.5 m to 25 by 25 m drill spacing. The data derived from this drilling and the recent 25 by 25 m drilling was used to confirm short scale mineralisation continuity and refine statistical and geostatistical relationships in the data which are useful in resource estimation.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	All field logging is carried out on Toughbooks using LogChief data capture software. Logging data is submitted electronically to the Database Geologist in the Perth office. Assay files are received electronically from the Laboratory. All data is stored in a Datashed/SQL database system, and maintained by the Gold Road Database Manager.
	Discuss any adjustment to assay data.	No assay data was adjusted. The laboratory's primary Au field is the one used for plotting and resource purposes. No averaging is employed.
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	The drill hole locations were initially picked up by handheld GPS, with an accuracy of 5m in northing and easting. All holes were later picked using DGPS to a level of accuracy of 1 cm in elevation and position. For angled drill holes, the drill rig mast is set up using a clinometer, and rigs aligned by surveyed positions and/or compass. Drillers use an electronic single-shot camera to take dip and azimuth readings inside the stainless steel rods, at 50 m intervals, prior to August 2014, and 30 m interval, post August 2014. Downhole directional surveying using north-seeking gyroscopic tool was completed on site and live (down drill rod string) or after the rod string had

Criteria	JORC Code explanation	Commentary
		been removed from the hole. Most diamond drill holes were surveyed live whereas most RC holes were surveyed upon exiting the hole.
	Specification of the grid system used.	A local grid (Gruyere Grid) was established by contract surveying group Land Surveys. The purpose of the local grid is to have an accurate and practical co-ordinate system along strike of the deposit. A high density survey control network and an accurate transformation between Gruyere Grid and MGA94-51 has been established. All ongoing studies, geological and resource activities are now conducted in Gruyere Grid.
	Quality and adequacy of topographic control.	An Aerial Lidar and Imagery Survey was completed January 2016 by Trans Wonderland Holdings as part of the ongoing FS covering 2,558 km^2 over the project area. One metre contours from this survey were used to construct a new topography surface to constrain the resource model. The survey showed good agreement with the existing DGPS drill hole collar data. All drill holes used in the resource grade estimate have a final collars survey by DGPS which are has a 1cm elevation accuracy.
Data spacing and distribution	*Data spacing for reporting of Exploration Results.*	Drill spacing is at an approximate 50 m section spacing and 40 - 80 m on section over the top 200 vertical metres of the deposit; the spacing is at a 100 m sections at 50 - 100 m spacing from 150 - 600 vertical metres. Approximately 75 % of the pit strike length has been drilled to 25 by 25 m spaced holes to a depth of 70 - 100 m below surface. Drill spacing in relation to Resource Classification is discussed further in Section 3 below.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Spacing of the reported drill holes is sufficient to demonstrate the geological and grade continuity of the deposit, and is appropriate for resource estimation procedures. Detailed description of the relationship between drill spacing and Resource classification is provided in Section 3 below.
	Whether sample compositing has been applied.	A total of 246 RC samples (out of a total 22,072 RC samples) featured compositing over waste intervals. This is the equivalent of <1% of all RC sample collected. None of these composited samples have been used in the Resource Estimate. No compositing has been employed in the diamond drilling. No sample compositing has been used during reporting – all reported intersections represent full length weighted average grades across the intersection length.

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td rowspan="2">Orientation of data in relation to geological structure</td><td>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</td><td>Drill sections are oriented west to east (270° to 090° Gruyere Grid) with the majority of holes oriented approximately perpendicular to dip and strike at -60° to 270°, 14 holes in this orientation are shallow to dip and four are steep to dip. A small component of drilling has been drilled in a northward orientation, five of these are deep diamond drill holes drilled along the strike of the deposit (-60 towards 010°) to specifically test along strike continuity. Twenty-six holes are drilled to the northeast and east, and six are drilled to the south. The table below details the drilling orientation by drill type.
<table>
<tr><th>Azimuth (Gruyere Grid)</th><th>Dip</th><th>DDH</th><th>RC</th><th>Total</th><th>Comment</th></tr>
<tr><td>250 to 290</td><td>-40 to -50</td><td>7</td><td>7</td><td>14</td><td>Perpendicular to strike and shallow to dip</td></tr>
<tr><td>250 to 290</td><td>-51 to -75</td><td>69</td><td>291</td><td>360</td><td>Perpendicular to strike and dip</td></tr>
<tr><td>250 to 290</td><td>-76 to -85</td><td>2</td><td>2</td><td>4</td><td>Perpendicular to strike and steep to dip</td></tr>
<tr><td>291 to 020</td><td>-55 to -70</td><td>11</td><td></td><td>11</td><td>Along strike / down dip - includes 1 wedge</td></tr>
<tr><td>021 to 100</td><td>-60 to -80</td><td>12</td><td>14</td><td>26</td><td>To northeast and east</td></tr>
<tr><td>101 to 249</td><td>-60 to -70</td><td>2</td><td>4</td><td>6</td><td>To south</td></tr>
<tr><td>na</td><td>-90</td><td></td><td>2</td><td>2</td><td>Water bores</td></tr>
<tr><td></td><td>Total</td><td>103</td><td>320</td><td>423</td><td></td></tr>
</table>
</td></tr>
<tr><td>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</td><td>Detailed structural logging of diamond drill core identified important quartz veins sets with an approximate shallow dip to the east. Drilling angled at either -60 to the east or west does not introduce any directional bias given the current understanding of the structural orientations and the dip and strike of mineralisation.</td></tr>
<tr><td>Sample security</td><td>The measures taken to ensure sample security.</td><td>For all RC drilling and diamond drilling pre-numbered calico sample bags were collected in plastic bags (five calico bags per single plastic bag), sealed, and transported by company transport to the Intertek laboratory in Kalgoorlie. Prepared pulps were then despatched by Intertek to its laboratory in Perth for assaying.</td></tr>
<tr><td>Audits or reviews</td><td>The results of any audits or reviews of sampling techniques and data.</td><td>Sampling and assaying techniques are industry-standard. Internal and Consultant reviews of QAQC have been completed and documented.
Company laboratory audits have been complete at the Intertek Laboratory in Perth.
No independent laboratory or sample audits have been completed.</td></tr>
</table>

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	The RC and diamond drilling occurred within tenement E38/2362, which is fully owned by Gold Road. The tenement is located on the Yamarna Pastoral Lease, which is owned and managed by Gold Road. Tenement E38/2362 is located inside the Yilka Native Title Claim, WC2008/005, registered on 6 August 2009. The 2004 "Yamarna Project Agreement" between Gold Road and the Cosmo Newberry Aboriginal Corporation governs the exploration activities respectively inside the Pastoral Lease. As part of the ongoing FS Yilka and Gold Road reached an in-principle native title mining agreement in December 2015 and are working to sign the final agreement within Q2 2016 as a precursor to grant of the lodged mining lease application.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	The tenement is in good standing with the WA DMP.
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	No previous exploration has been completed on this prospect by other parties.
Geology	*Deposit type, geological setting and style of mineralisation.*	The Gruyere Deposit comprises a narrow to wide porphyry intrusive dyke (Gruyere Porphyry – a Quartz Monzonite) which is between 35 and 190 m in width and which strikes over a current known length of 2,200 m. The Gruyere Porphyry dips steeply (65-80 degrees) to the east. A sequence of intermediate to mafic volcaniclastic rocks defines the stratigraphy to the west of the intrusive and intermediate to mafic volcanics and a tholeiitic basalt unit occur to the east. Mineralisation is confined ubiquitously to the Gruyere Porphyry and is associated with pervasive overprinting albite-sericite-chlorite-pyrite (±pyrhhotite±arsenopyrite) alteration which has obliterated the primary texture of the rock. Minor fine quartz-carbonate veining occurs throughout. Pyrite is the primary sulphide mineral and some visible gold has been observed in logged diamond drill core. The Gruyere Deposit is situated at the north end of the regional camp-scale South Dorothy Hills Target identified by Gold Road during its regional targeting campaign completed in early 2013. The Gruyere Deposit comprises coincident structural and geochemical targets within a major regional-scale structural corridor associated with the Dorothy Hills Shear Zone. This zone occurs within the Dorothy Hills Greenstone Belt at Yamarna in the eastern part of the Archaean Yilgarn Craton. The Dorothy Hills Greenstone is the most easterly known occurrence of outcropping to sub-cropping greenstone in the Yilgarn province of Western Australia.
Drill hole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ▪ easting and northing of the drill hole collar ▪ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar ▪ dip and azimuth of the hole ▪ down hole length and interception depth ▪ hole length. *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	Appendix 2 outlines previous general ASX announcements that contain reported drill hole information for all relevant RC and Diamond holes included in the reported resource estimation. The 25 by 25 m RC data has not been reported in detail as it is considered operational.

Criteria	JORC Code explanation	Commentary
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.*	All drill assay results (except for the previously mentioned 25 by 25 m RC holes) used in this estimation of this resource have been published in previous releases; refer to Appendix 2 for a list of previous releases.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	All drill assay results (except for the previously mentioned 25 by 25 m RC holes) used in this estimation of this resource have been published in previous releases; refer to Appendix 2 for a list of previous releases.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalent values are used.
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.* *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	Mineralisation is hosted within a steep east-dipping, N-S striking porphyry. The porphyry is mineralised almost ubiquitously at greater than 0.3 g/t Au and is characterised by pervasive sub-vertical shear fabrics and sericite-chlorite-biotite-albite alteration with accessory sulphides dominated by pyrite-pyrrhotite-arsenopyrite. Higher grade zones occur in alteration packages characterised by albite-pyrrhotite-arsenopyrite alteration and quartz and quartz-carbonate veining. These vein packages dip at approximately -45^0 to the SSE, with strike extents of over 100 m. The general drill direction of 60^0 to 270^0 is approximately perpendicular to the main alteration packages and is a suitable drilling direction to avoid directional biases.
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Refer to Figures and Tables in the body of the release.
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	All drill assay results (except for the previously mentioned 25 by 25 m RC holes) used in this estimation of this resource have been published in previous releases; refer to Appendix 2 for a list of previous releases.
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Drill hole location data are plotted in Figures in the body text.
Further work	*The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	Possible extensions at depth and to the south at depth will be tested in a strategic manner.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	*Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*	Geological metadata is stored centrally in a relational SQL database with a DataShed front end. Gold Road employs a Database Manager who is responsible for the integrity and efficient use of the system. Only the Database Manager or their Data Entry Clerk has permission to modify the data. Sampling and geological logging data is collected in the field using LogChief software and uploaded digitally. The software utilises lookup tables, fixed formatting and validation routines to ensure data integrity prior to upload to the central database. Sampling data is sent to, and received from, the assay laboratory in digital format. Drill hole collars are picked up by differential GPS (DGPS) and delivered to the database in digital format. Down hole surveys are delivered to the database in digital format. The Mineral Resource estimate only uses Gold Road RC and DDH assay data. There is no historical data.
	Data validation procedures used.	DataShed software has validation procedures that include constraints, library tables, triggers and stored procedures. Data that does not pass validation tests must be corrected before upload. The LogChief software utilises lookup tables, fixed formatting and validation routines to ensure data integrity prior to upload to the central database. Geological logging data is checked visually in three dimensions against the existing data and geological interpretation. Assay data must pass laboratory QAQC before database upload. Gold Road utilises QAQR software to further analyse QAQC data, and batches which do not meet pass criteria are requested to be re-assayed. Sample grades are checked visually in three dimensions against the logged geology and geological interpretation. Drill hole collar pickups are checked against planned and/or actual collar locations. A hierarchical system is used to identify the most reliable down hole survey data. Drill hole traces are checked visually in three dimensions. The project geologist and resource geologist are responsible for interpreting the down hole surveys to produce accurate drill hole traces.
Site visits	*Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is the case.*	Justin Osborne is one of the Competent Persons and is Gold Road's Executive Director. He conducts regular site visits and is responsible for all aspects of the project. John Donaldson is the second Competent Person and is Gold Road's Principal Resource Geologist. He conducts regular specific site visits to focus on understanding the geology as it is revealed in the drilling data. Communication with the site geologists is key to ensuring the latest geological interpretations are incorporated into the resource models. Both Competent Persons contribute to the continuous improvement of sampling and logging practices and procedures.

Criteria	JORC Code explanation	Commentary
Geological interpretation	*Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.*	The predominance of diamond drilling at Gruyere has allowed a robust geological interpretation to be developed, tested and refined over time. Early establishment of lithology and alteration coding and detailed structural logging has given insight into geological and grade trends that have been confirmed with geostatistical analysis, (including variography). Other sources of data (see next commentary) have also added confidence to the geological interpretation. The type and thickness of host lithology and main hangingwall mafic dyke is predictable. Other non-mineralised mafic and intermediate dykes are less predictable. The footwall and hangingwall lithologies are less well known due to the focus of drilling on mineralised units. However, the hangingwall lithologies are understood better as holes are collared on this side of the deposit. Results from the EIS hole (ASX announcement dated 8 September 2015) have improved the understanding of hangingwall lithologies and this will improve with further study. Continued drilling has shown that the approximate tenor and thickness of mineralisation is also predictable, but to a lesser degree than the geology. Results from the 25 by 25 m RC grade control drilling data have confirmed the geological interpretation and mineralisation model. As the deposit has good grade and geological continuity, which has been confirmed by grade control drilling, the Competent Persons regard the confidence in the geological interpretation as high.
	Nature of the data used and of any assumptions made.	All available data has been used to help build the geological interpretation. This includes geological logging data (lithology and structure), gold assay data (RC and DDH), portable XRF multi-element data (Niton and laboratory), geophysics (airborne magnetics and gravity), down hole Televiewer data (optical images and structural measurements, specific gravity, resistivity and natural gamma) and mineral mapping and multi-element data from research conducted in partnership with the CSIRO. An assumption regarding some gold remobilisation has been made at the more deeply weathered northern end of the deposit where a small flat lying gold dispersion blanket has been interpreted near the saprolite / saprock boundary. This is believed to represent dispersion of gold due to weathering processes. Justification for this interpretation lies in the lack of visual control to the mineralisation and its position in the weathering profile.
	The effect, if any, of alternative interpretations on Mineral Resource estimation.	A model constrained only by lithology (Gruyere Porphyry) was run to compare against the implicitly (and lithologically) constrained at 0.3 g/t model (actual model). Results showed that at 0 g/t cut-off the estimate of ounces was within 2%, and, as expected the lithologically constrained model had higher tonnage at lower grade. At 0.5 g/t, grade is 10% less and ounces are 7% less, and at 1.0 g/t grade is 1% less and ounces are 19% less in the lithologically constrained model. Moreover, in previous updates, one other potential mineralised trend, keeping all other constraints constant, was been modelled and showed little effect on the global estimate of volume.
	The use of geology in guiding and controlling Mineral Resource estimation.	Regionally the deposit is hosted in an Archaean basin to the East of the crustal scale Yamarna Shear Zone. The Gruyere deposit is located on an inflection of the NW (MGA) striking Dorothy Hills Shear Zone which transects the basin. The Dorothy Hills Shear Zone is the first order control into which the host Gruyere Porphyry has intruded. The bulk of the mineralisation has been constrained to the host intrusive below the base of Quaternary and Permian cover.

Criteria	JORC Code explanation	Commentary
		Several NNE dipping cross-cutting arcuate and linear faults have been interpreted from airborne magnetics, the distribution of lithology and diamond core intersections of faults. The Alpenhorn Fault and to a lesser degree the Northern Fault have been used to constrain the distribution of mineralisation. Mineralisation within the intrusive host has been implicitly modelled to the mineralisation trends discussed below at a constraining 0.3 g/t cut-off. The cut-off was established using two lines of reasoning: 1. All of the assay data internal to the host rock was plotted on a log probability plot; a value of 0.3 g/t was recognised as an inflection point subdividing the non-mineralised and mineralised populations. This is further supported through a reduction in the CV in the unconstrained case from 1.0 to 0.9 in the constrained case i.e. a reduction in stationarity supporting the domaining. 2. 0.3 g/t corresponds to the approximate grade cut-off between barren to very weakly mineralised hematite-magnetite alteration and weak to strongly mineralised albite-sericite-carbonate ± pyrite, pyrrohotite, arsenopyrite alteration. Three mineralisation Domains have been modelled; Primary, Weathered and the minor Dispersion Blanket. 1. The Primary Domain corresponds to mineralisation hosted in fresh, transitional and saprock Gruyere Porphyry. The mineralisation trend is along strike and steeply down dip. The trend was established using observations of alteration, sulphide and gold grade distribution, together with the following structural observations from diamond core: ▪ The along strike component corresponds to the main foliation within the intrusive host. ▪ The steep down dip component corresponds to a strong down-dip lineation parallel to the axes of tight to isoclinal folds of the pre-existing foliation within the intrusive host. The strike and dip components for the Primary Domain were readily confirmed in the variography. 2. A secondary Domain corresponds to mineralisation hosted in deeply weathered (saprolite) Gruyere Porphyry. The mineralisation trend is flat lying, reflecting the weathering processes. The trend was established using observations of gold grade distribution and the position relative to the weathering profile. The strike and dip components for the Weathered Domain were readily confirmed in the variography. 3. A minor third Domain corresponds to a flat lying, 4 – 5 m thick, gold dispersion blanket interpreted near the saprolite boundary and hosted within hangingwall and footwall lithologies.
	The factors affecting continuity both of grade and geology.	Apart from the controls discussed previously, one narrow (1 to 5 m wide), steeply dipping non-mineralised internal mafic dyke has been modelled as barren within the intrusive host. Other narrow (generally less than 1 m wide) mafic and intermediate intrusives / dykes occur but have very short scale continuity and insignificant to the scale of mineralisation.
Dimensions	*The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	Length along strike: 1,800 m Horizontal Width: 7 to 190 m with an average of 90 m. The vertical depth of Mineral Resource from surface to the upper limit is 2 m and to the lower limit is 600 m. The Mineral Resource has been constrained by an optimised Whittle shell that considers all available mineralisation in the geological model. The optimisation utilises realistic mining, geotechnical and processing parameters from the latest information available from the ongoing FS. The gold price used was A$1,700/oz Au. Only Measured, Indicated and Inferred categories within this shell have been reported as Mineral Resource. Mineralisation in the geology model outside the shell has not been reported. Approximately 39,000 oz of unclassified* mineralisation falls within the shell and is not reported.

Criteria	JORC Code explanation	Commentary
		*Low confidence mineralisation within the geological model that does not satisfy the criteria for Mineral Resource has been flagged as unclassified.

	The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.	**Software used:**
		▪ Datashed – frontend to SQL database
		▪ Mapinfo – geophysics and regional geology
		▪ Stereonet – compilation and interpretation of diamond structural data.
		▪ Core Profiler – compilation of downhole photographs in core trays for geo-referencing in 3D software.
		▪ Leapfrog Geo – Drill hole validation, material type, lithology, alteration and faulting wireframes, domaining and mineralisation wireframes, geophysics and regional geology
		▪ Snowden Supervisor - geostatistics, variography, declustering, kriging neighbourhood analysis (KNA), validation
		▪ Datamine Studio RM – Drill hole validation, cross-section, plan and long-section plotting, block modelling, geostatistics, quantitative kriging neighbourhood analysis (QKNA), OK estimation (for validation and input to LUC), block model validation, classification, and reporting.
		▪ Datamine Studio RM Uniform Conditioning Module – LUC grade estimation. The module is an interface to the code in Isatis software for change of support, information effect calculation, uniform conditioning and grade localisation. Isatis is the most highly regarded geostatistical software in the industry and is used by many of the top gold mining companies worldwide.
		Localised Uniform Conditioning:
		▪ LUC was selected as at technique to estimate the Indicated and Inferred areas of this resource update as the method provides estimates of Selective Mining Units (SMU) from widely spaced data. The LUC model is globally accurate but the estimate of the grade tonnage curve is not over smoothed (as in conventional OK) resulting in less tonnes at higher grade above a given cut-off (ie. an estimate of the grade control grade tonnage curve).
		▪ The improved resolution of LUC adds value to economic evaluation at higher cut-offs (e.g. 1.0 g/t): however, at lower cut-offs (e.g. 0.5 g/t) used for reporting there are no significant differences between the direct block (OK) estimate and the LUC estimate.
		▪ In models prior to September 2015 grades were estimated using an OK methodology into large parent blocks resulting in a globally accurate but smoothed grade tonnage curve (more tonnes at lower grade above cut-off).
		Block model and estimation parameters:
		▪ Treatment of extreme grade values – Top-cuts (all samples included method) were applied to 2m composites selected within mineralisation wireframes. The top-cut level was determined through the analysis of histograms, log histograms, log probability plots and spatial analysis.
		  ▪ Primary - one sample was cut using a 30 g/t top-cut resulting in a 0.1% reduction in mean grade.
		  ▪ Weathered - 3 samples were cut using a 10 g/t top-cut resulting in a 1.0% reduction in mean grade.
		  ▪ Dispersion Blanket - no samples were top-cut.

Criteria	JORC Code explanation	Commentary

		▪ Estimation technique for Measured – OK – at this data spacing (25 by 25 m grade control) OK is the appropriate technique, where LUC is appropriate for broader spaced drilling. The data is sufficiently dense for a correct direct block estimate.
		▪ Estimation for technique Indicated and Inferred - LUC - with an OK estimate (25 m X by 50 m Y by 10 m Z panels) required as input.
		▪ KNA was undertaken to optimise the search neighbourhood used for the estimation and to test the parent block size. The search ellipse and selected samples by block were viewed in three dimensions to verify the parameters.
		▪ Model rotation – none required – local Gruyere Grid used.
		▪ Parent block size for Measured estimation of gold grades by OK - 5 m X by 12.5 m Y by 5 m Z (parent cell estimation with full subset of points).
		▪ LUC inputs for Indicated and Inferred estimation of gold grades (note that 6 estimation scenarios were tested and analysed before deciding on the final input parameters);
		  ▪ 12.5 m X by 25 m Y by 5 m Z declustering of input data in Supervisor (the declustering weight is inversely proportional to the number of data points in each cell). Note that change in grade through declustering with respect to the use of the cell size optimiser is minimal.
		  ▪ Discretisation 3 X by 5 Y by 2 Z
		  ▪ Information Effect planned sample spacing 25 m X by 25 m Y by 1 m Z, and 9 X by 9 Y by 5 Z planned number of samples
		  ▪ 40 SMUs (5 m X by 12.5 m Y by 5 m Z) per panel (25 m X by 50 m Y by 10 m Z)
		  ▪ 70 cut-offs at 0.1 g/t intervals
		  ▪ 7 iso-frequencies
		▪ Smallest sub-cell – 1 m X by 12.5 m Y by 1 m Z (a small X dimension was required to fill internal mafic dyke and a small Z dimension was required to fill to material type boundaries).
		▪ Panel discretisation - 3 X by 5 Y by 2 Z (using the number of points method)
		▪ Measured Search ellipse – aligned to mineralisation trend, dimensions;
		  ▪ Fresh - 35 m X by 60 m Y by 15 m Z.
		  ▪ Weathered – 50 m X by 80 m Y by 15 m Z.
		  ▪ Dispersion Blanket - 50 m X by 80 m Y by 15 m Z.
		▪ Indicated and Inferred Search ellipse – aligned to mineralisation trend, dimensions;
		  ▪ Fresh - 200 m X by 350 m Y by 60 m Z (the longest range in variogram is 350 m).
		  ▪ Weathered - 50 m X by 80 m Y by 15 m Z (the longest range in variogram is 80 m).
		  ▪ Dispersion Blanket - 50 m X by 80 m Y by 15 m Z.
		▪ Measured - number of samples:
		  ▪ Fresh – maximum per drill hole = 4, first search 16 min / 36 max, second search 16 min / 36 max and a volume factor of 2, third search 8 min / 36 max with a volume factor of 2

Criteria	JORC Code explanation	Commentary
		▪ Weathered– maximum per drill hole = 5, first search 30 min / 60 max, second search 30 min / 60 max and a volume factor of 2, third search 10 min / 60 max with a volume factor of 2 ▪ Dispersion Blanket – maximum per drill hole = 5, first search 30 min / 60 max, second search 30 min / 60 max and a volume factor of 2, third search 6 min / 60 max with a volume factor of 2 ▪ Indicated and Inferred - number of samples: ▪ Fresh – maximum per drill hole = 7, first search 30 min / 60 max, second search 15 min / 60 max and a volume factor of 1, third search 5 min / 60 max with a volume factor of 3 ▪ Weathered – maximum per drill hole = 5, first search 30 min / 60 max, second search 30 min / 60 max and a volume factor of 2, third search 1 min / 60 max with a volume factor of 3 ▪ Dispersion Blanket – maximum per drill hole = 5, first search 20 min / 60 max, second search 10 min / 60 max and a volume factor of 2, third search 2 min / 60 max with a volume factor of 3 ▪ Maximum distance of extrapolation from data points – 50 m from sample data to Inferred boundary Domain boundary conditions – Hard boundaries are applied at all domain boundaries.
	The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.	Several internal models and three public models were produced prior to the publication of this Mineral Resource. These were used to plan drilling programs, manage performance and expectation and test geological interpretation on an ongoing basis during and after the various drilling campaigns. Analysis shows that this model has performed well globally and locally against the original internal and publically released models. In particular, and locally at a 0.5 g/t cut-off, in the Measured (grade control defined) portion of this model (13.9 Mt at 1.18 g/t for 526 koz) the variance has been minimal +4% for tonnes, -4 % for grade and +1% for ounces in comparison to the same volume in the previous model (Indicated). There is no previous production.
	The assumptions made regarding recovery of by-products.	There are no economic by-products.
	Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).	No deleterious elements of significance have been determined from metallurgical test work and mineralogical investigations. Waste rock characterisation work has been completed and all waste types and tailings are non-acid forming and have limited metal leachate potential.
	In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.	For the Measured (OK estimate). The parent block size of 5 m X by 12.5 m Y is approximately: • 50% of the maximum drill spacing of 25 m X by 25 m Y in Measured areas For the Indicated and Inferred (OK estimate as input to LUC) The parent block size of 25 m X by 50 m Y is approximately: • 25% of the minimum drill spacing of 50 m X by 100 m Y in Indicated areas • 12.5% of the maximum drill spacing of 100 m X by 100 m Y in Inferred areas
	Any assumptions behind modelling of selective mining units.	The selective mining unit (SMU) of 5 m X by 12.5 m Y by 5 m Z was chosen as it gives 40 SMU's per 25 m X by 50 m Y by 10 m Z parent cell (a minimum of around 24 SMU's are required for adequate grade / tonnage definition) and corresponds well with mining equipment and mining flitch sizes selected in the PFS. A separate fleet sizing study will be completed during the FS.
	Any assumptions about correlation between variables.	No correlation between variables was analysed or made.

Criteria	JORC Code explanation	Commentary
	Description of how the geological interpretation was used to control the resource estimates.	The geological interpretation was used at all stages to control the estimation. If geostatistics, variography and/or visual checks of the model were difficult to interpret then the geological interpretation was questioned and refined.
	Discussion of basis for using or not using grade cutting or capping.	Top-cuts were used in the estimate as this is the most appropriate way to control outliers when estimating block grades from assay data.
	The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.	The following validation checks were performed: ▪ QQ plots of RC vs DDH input grades. ▪ Statistical comparison of different drilling orientations including local spot checks. ▪ Comparison of twinned RC, twinned DDH and twinned RC v DDH holes. ▪ Comparison of the volume of wireframe vs the volume of block model. ▪ Checks on the sum of gram metres prior to compositing vs the sum of gram metres post compositing ▪ A negative gold grade check ▪ Comparison of the model average grade and the declustered sample grade by Domain. ▪ Generation of swath plots by Domain, northing and elevation. ▪ Comparison of LUC estimate to OK estimate. ▪ Visual check of drill data vs model data in plan, section and three dimensions. ▪ Comparison to previous models ▪ Comparison to alternative interpretations (see above) All validation checks gave suitable results. There has been no mining so no reconciliation data available.
Moisture	*Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	Average bulk density values have been modified by a moisture percentage so that dry tonnage is reported. These are: overburden and saprolite 5%, saprock 3%, transition 2% and fresh 1 %.
Cut-off parameters	*The basis of the adopted cut-off grade(s) or quality parameters applied.*	The cut-off grade used for reporting is 0.5 g/t gold. This has been determined from mining and processing parameters and input costs from the latest information available from the ongoing FS.
Mining factors or assumptions	*Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	The mining method assumed is conventional open pit with a contract mining fleet appropriately scaled to the size of the deposit. Whittle optimisation input parameters are outlined in Table 11 of the main text. The de facto minimum mining width is a function of parent cell size (25m X by 50m Y by 10m Z). No allowance for dilution or mining recovery has been made in the Mineral Resource estimate.

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td>Metallurgical factors or assumptions</td><td>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</td><td>A single stage primary crush, Semi Autogenous Grinding and Ball Milling with Pebble Crushing (SABC) comminution circuit followed by a conventional gravity and carbon in leach (CIL) process is proposed. This process is considered appropriate for the Gruyere ore, which has been classified as free-milling.

The proposed metallurgical process is commonly used in the Australian and international gold mining industry and is considered to be well-tested technology.

Metallurgical recovery is applied to the resource model by material type and grind size (106µm, 125µm and 150µm) according to test work values for weathered material and grade recovery curves for fresh rock. 106µm was selected for input to optimisation. No recovery factors are applied to the Mineral Resource numbers themselves.

Significant comminution, extraction, and materials handling testing has been carried out on over 4,500 kg of half-core diamond drilling core samples (NQ core diameter = 47.6mm). The testing has been carried out on saprolite (oxide), saprock, transitional and fresh ore types which were selected to represent different grade ranges along the strike length of the deposit and to a depth of around 410 m. For the fresh rock samples, 62 composites representing four major mineralised zones (South, Central, North and High Grade North) were subjected to gold extractive test work by gravity separation and direct cyanidation of gravity tails. In total, 183 individual gravity-leach tests were completed at various grind size P80 ranging from 106 µm to 150 µm. Gravity gold recoveries are estimated at 35%.

Estimated plant gold recovery ranges from 87% to 96% depending on head grade, plant throughput, grind size and ore type and are summarised in the table below.

<table>
<tr><th rowspan="2">Material Type</th><th colspan="4">Metallurgical Recovery at P80</th></tr>
<tr><th>106 µm</th><th>125 µm</th><th>150 µm</th><th>Comments</th></tr>
<tr><td>Saprolite (oxide)</td><td>94%</td><td>93%</td><td>92%</td><td></td></tr>
<tr><td>Saprock</td><td>94%</td><td>93%</td><td>92%</td><td></td></tr>
<tr><td>Transition</td><td>93%</td><td>92%</td><td>91%</td><td></td></tr>
<tr><td>Fresh</td><td>2.6130 x ln head grade (g/t) + 92.199 %</td><td>3.1818 x ln of head grade (g/t) + 90.362 %</td><td>3.3997 x ln of head grade (g/t) + 88.929 %</td><td>capped at 96%</td></tr>
</table>

No deleterious elements of significance have been determined from metallurgical test work and mineralogical investigations.</td></tr>
<tr><td>Environmental factors or assumptions</td><td>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</td><td>Surface waste dumps and infrastructure (e.g. tailings dam) will be used to store waste material from open pit mining.

Conventional storage facilities will be used for the process plant tailings.

Test work has been completed for potential acid mine drainage material types. Results show that all material types are non-acid forming and are unlikely to require any special treatment.

Baseline environmental studies of flora, vegetation, vertebrate fauna, short-range endemic invertebrates and subterranean fauna have commenced and are due for completion within the timeframe of the FS schedule.</td></tr>
</table>

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td rowspan="3">Bulk density</td><td>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</td><td>Bulk density has been determined using 2 main methods and cross checked with data from recent metallurgical test work:
1. RC drilling – downhole rock property surveys completed by ABIMS Pty Ltd which provide a density measurement every 0.1 m downhole.
2. DDH drilling – weight in air / weight in water – measurements every 1 m in weathered every 10 m in fresh rock, using approximate 0.1 m core lengths.
The physical measurements derived from the air/water method were compared to the down hole tool measurements and metallurgical test work. Good correlation was observed between methods for saprolite, saprock and transitional. The down-hole tool values for fresh rock did not match the other two methods and so was set aside pending review by the provider.</td></tr>
<tr><td>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</td><td>Vacuum sealed bags were used where required to account for void spaces in the core.
Bulk density has been applied by lithology and weathering type.</td></tr>
<tr><td>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</td><td>Data was coded by method, lithology (including mineralisation and cover) and weathering type. The three methods were compared and found to be in agreement except for the down hole tools values for fresh rock. Averages were derived both by lithology and weathering type. Assumptions for moisture percentages were made and accounted for in the final value used for bulk density.</td></tr>
<tr><td rowspan="3">Classification</td><td>The basis for the classification of the Mineral Resources into varying confidence categories.</td><td>The Mineral Resource has been constrained within an optimised Whittle pit shell. Blocks in the geological model within that shell have been classified as Measured, Indicated or Inferred. Several factors have been used in combination to aid the classification;
▪ Drill hole spacing:
<table>
<tr><th>Domain</th><th>Criteria</th><th>Measured</th><th>Indicated</th><th>Inferred</th><th>Unclassified</th></tr>
<tr><td rowspan="5">Primary</td><td>Target Spacing</td><td>25 m X by 25 m Y</td><td>50 m X by 100 m Y</td><td>100 m X by 100 m Y</td><td></td></tr>
<tr><td rowspan="2">Actual Spacing</td><td rowspan="2">12.5 m X by 12.5 m Y to 25 m X by 25 m Y</td><td rowspan="2">25 m X to 65 m X by 100 m Y with extra holes on 50 m Y</td><td>100 m X by 100 m Y</td><td>"Potential" beyond Inferred to limits of geological model.</td></tr>
<tr><td>Footwall contact of along strike hole 14GYDD0061</td><td></td></tr>
<tr><td rowspan="2">Boundary Extension</td><td>10 to 15 m along strike</td><td>25 m along strike</td><td>50 - 100 m along strike</td><td></td></tr>
<tr><td>Closet 5 m Rl from bottom of hole</td><td>Minimal down dip - except North end 30 m from drilling. Drilling needs to define full width of intrusive host.</td><td>Minimal down dip - except North end 50 m from Indicated boundary</td><td></td></tr>
<tr><td rowspan="2">Weathered</td><td>Target Spacing</td><td>12.5 to 25 m X by 25 m Y</td><td>50 m X by 100 m Y</td><td></td><td></td></tr>
<tr><td>Actual Spacing</td><td>12.5 m X by 12.5 m Y to 25 m X by 25 m Y</td><td>25 m X to 50 m E by 100 m Y with extra holes on 50 m Y</td><td></td><td></td></tr>
<tr><td>Dispersion Blanket</td><td>Actual Spacing</td><td></td><td></td><td>25 to 50 m X by 25 to 100 m Y</td><td>"Potential" beyond Inferred to limits of geological model.</td></tr>
</table>
▪ Level of geological continuity.
▪ Level of grade continuity.
▪ Consideration of estimation quality parameters derived from the OK process.</td></tr>
<tr><td>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</td><td>All relevant factors have been taken into account in the classification of the Mineral Resource.</td></tr>
<tr><td>Whether the result appropriately reflects the Competent Person’s view of the deposit.</td><td>The Mineral Resource estimate appropriately reflects the Competent Person’s view of the deposit.</td></tr>
</table>

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td>Audits or reviews</td><td>The results of any audits or reviews of Mineral Resource estimates.</td><td>Ian Glacken (Director - Geology at Optiro consultants) was engaged to externally review the technical aspects of this update, and the three previous Mineral Resource estimates. A formal review was undertaken and suggestions for improvement were sought and applied where appropriate.

An endorsement letter/summary report of the review has been completed for this update and the three previous Mineral Resource estimates. Optiro is satisfied that the Mineral Resource estimate has been reported and classified according to the guidelines set out in the JORC Code (2012) and in line with good to best industry practice.

An external database audit was not undertaken for this update due to the operational nature of the drilling. Lisa Bascombe of Optiro conducted audits for the three previous Mineral Resource estimates.

Internal geological peer review by the Executive Director, Exploration manager and/or geological team, and handover meetings with the development and operational teams were held and documented at appropriate times. An informal internal peer review, as part of a board briefing, was conducted with the Non-executive Directors on the Gold Road board, who are also geologists, for the previous Mineral Resource estimate.

A QAQC report was completed by Dr Paul Sauter (internal consultant – Sauter Geological Services Pty Ltd) for data collected for this update to the resource. Results are acceptable and an improvement on previous results. Recommendations include further umpire lab testing and changing the blanks to a more appropriate material.

A QAQC report was completed by Mr Dave Tullberg (Grassroots Data Services Pty Ltd) for data collected for the maiden resource. A QAQC report was completed by Dr Paul Sauter (internal consultant – Sauter Geological Services Pty Ltd) for data collected for the previous two updates to the resource. This included analysis of umpire lab test-work.</td></tr>
<tr><td>Discussion of relative accuracy/ confidence</td><td>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</td><td>Variances to the tonnage, grade and metal of the Mineral Resource estimate are expected with further definition drilling. It is the opinion of the Competent Persons that these variances will not significantly affect economic extraction of the deposit.

The mean grade of raw assay data in the mineralised domains compare extremely well upon the collection of additional data;

<table>
<tr><th>Model Release</th><th>Number of Mineralised Samples (>0.3 g/t)</th><th>Mean g/t</th></tr>
<tr><td>April 2016</td><td>32,293</td><td>1.245</td></tr>
<tr><td>September 2015</td><td>24,156</td><td>1.305</td></tr>
<tr><td>May 2015</td><td>22,490</td><td>1.268</td></tr>
<tr><td>August 2014</td><td>15,320</td><td>1.266</td></tr>
<tr><td>February 2014*</td><td>4,240</td><td>1.230</td></tr>
</table>
*in house model

Previous tests to determine the performance of the Inferred category as it has been upgraded with drilling to Indicated and Measured have been made. The results showed that a robust estimate of Inferred can be made as acceptable variances of tonnage, grade and/or metal were calculated from the original Inferred model in comparison to the same area in the Indicated or Measured model.</td></tr>
</table>

Criteria	JORC Code explanation	Commentary
		Performance of the Indicated category has been assessed in this update compared to previous estimates. At a 0.5 g/t cut-off, the Measured (grade control defined) portion of this model (13.9 Mt at 1.18 g/t for 526 koz) has performed well against the same volume in the previous model (Indicated). The variance is minimal at +4% for tonnes, -4 % for grade and +1% for ounces. The model performance was also assessed visually. As new drilling data came in it was compared to the existing model; in the majority of cases the existing model matched the tenor and thickness of the new assay data.
	The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.	Confidence in the Mineral Resource estimate is such that the Measured portions of the model will provide adequate accuracy for ore block design, monthly mill reconciliation and short to medium term scheduling. For the Indicated and Inferred portions it will provide adequate accuracy for global resource evaluation and for more detailed evaluation at a large scale. Bench evaluations show that tonnages greater than 5 million may be mined over a 20 m vertical height. This is twice the parent cell vertical height of 10 m, so an unbiased estimate at that scale is expected. For Indicated this equates to annual and quarterly production windows and to an annual production window for Inferred. Relative accuracy is expected to decrease at depth as smaller tonnages are mined as the pit width decreases.
	These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	No previous mining.