ASX Announcement

23 June 2016

Significant Resource Upgrade for Mulga Rock Project

Vimy Resources Limited ("**Vimy**" **ASX: VMY**) is pleased to announce the results from the updated Ambassador Resource Estimate for its **Mulga Rock Project** (**MRP**). The estimate was completed in-house and validated by the independent resource consultant, AMC Consultants. The estimate is based on an extensive in-fill drill program completed and announced earlier this year.

The Ambassador resource currently makes up more than half of the total uranium Mineral Resource for the MRP, and the significant increase in the proportion of Indicated Mineral Resource in the resource base will underpin the Ore Reserve update that will support the Definitive Feasibility Study (**DFS**) currently in progress.

The key highlights are:

- **Greater than 80% of Ambassador classified as Indicated:** Over 80% of the metal in the Ambassador resource is now in the Indicated Mineral Resource category, totalling 19.8Mt at 720ppm U_3O_8 for 31.5Mlbs U_3O_8;
- **Good continuity of Indicated status material:** This is an important characteristic given continuous strip mining is being proposed at Mulga Rock;
- **Overall increase in the Resource:** the Mineral Resource Estimate is increased to 66.5Mt at 520ppm U_3O_8 for a contained 76.2Mlbs U_3O_8;
- **High conversion expected from Indicated Mineral Resources to Probable Ore Reserve.**

Managing Director, Mike Young said, *"This resource update is a critical milestone for the DFS that is currently underway. The exploration team has completed all the drilling necessary to support the DFS. We will shortly be releasing the Mineral Resource updates with Shogun and Emperor where we are expecting increases in overall metal and resource classification.*

"We are currently working on the Ore Reserve for Ambassador and expect this to increase markedly and this will underpin future project financing and offtake contract discussions. The DFS is progressing on-schedule and on-budget and the Project Team is doing a stellar job. We are on-track to be first uranium mine in Western Australia".

Mulga Rock Project

The Mulga Rock Project is 100% owned and operated by Vimy and lies approximately 240km east northeast of Kalgoorlie, situated on two granted Mining Leases (ML39/1080 and ML39/1081). Vimy holds title to approximately 757 square kilometres of exploration ground across the MRP.

The Mulga Rock East Deposit comprises the Princess and Ambassador resources and will form the first stage of the potential mine development for the Mulga Rock Project (Figure 1). The Ambassador resource is a large, flat-lying deposit that is approximately 9km in length and 1km wide. It has been extensively drilled with 1,331 aircore and reverse circulation (**RC**) holes completed for a combined total depth of 89,498 metres, and 288 diamond holes for 16,062 metres. A complete list of all drill-hole co-ordinates is appended at the end of this release.

Please consider the environment before printing this announcement past Page 8.

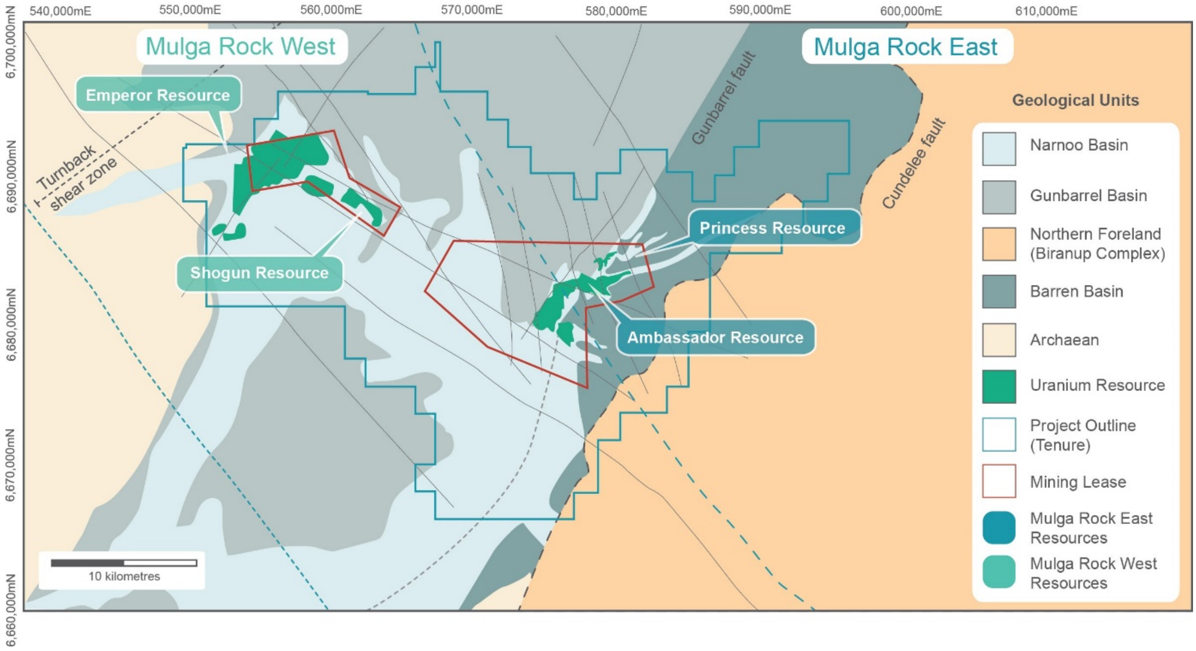


Figure 1: Location of the Mulga Rock Uranium Deposits

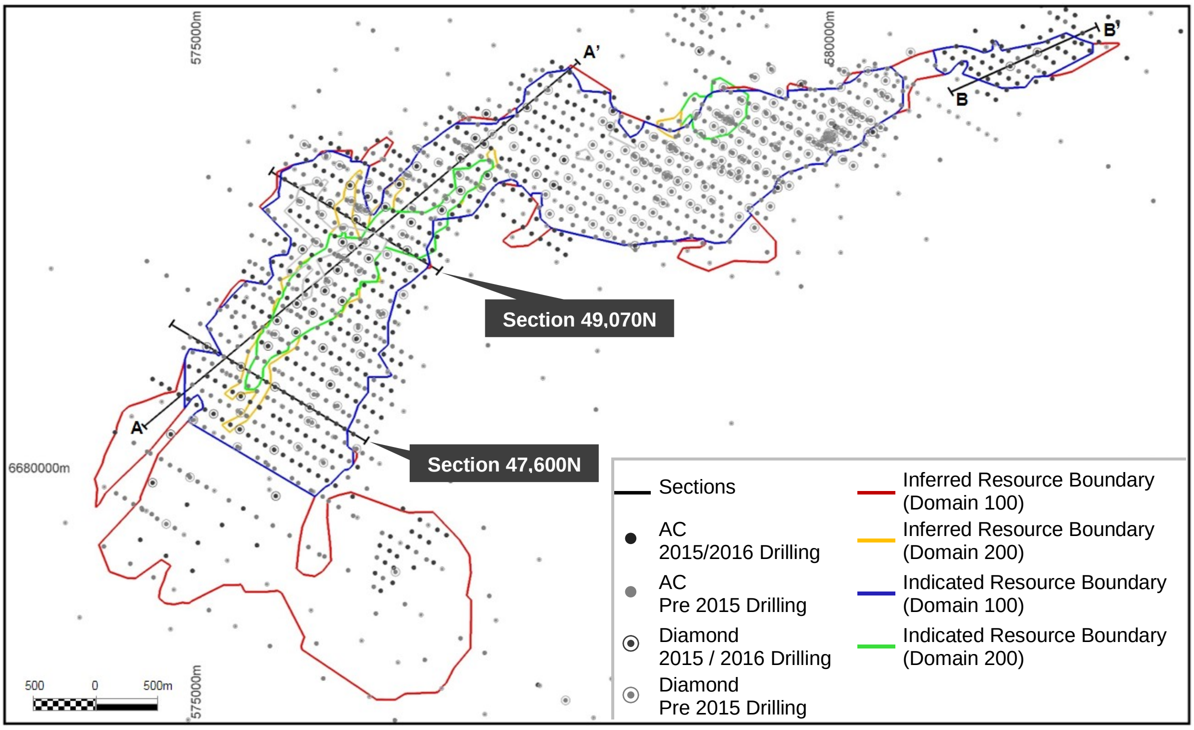


Figure 2: Ambassador – Collar location map and drill hole type

The 2016 Ambassador Resource has been reported in accordance with the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves, (JORC Code 2012).
The updated Resource Estimate has significantly increased the overall geological confidence of the Mulga Rock Project and enables advanced mining studies to be undertaken. An executive summary of the Resource Estimate follows this section, and the JORC Table 1 is appended to this announcement.

Mulga Rock East Resource Upgrade

An extensive in-fill drilling program at Ambassador was completed earlier this year, as announced to the ASX on 25 February 2016. The program comprised 425 air core and 52 diamond core holes for a total of 27,350 metres The drill results reaffirm Ambassador as an outstanding uranium resource with a total of 65 drill holes returning intercepts above 1,000 ppm (0.10%) U_3O_8. The best intercept was recorded from drill-hole NNA6020, with 2.5m at 5,547 ppm (0.55%) U_3O_8 from 41.0 metres.

The drill program has improved the geological understanding of the Ambassador resource in addition to providing further information to improve bulk density estimates, and adjustment of downhole geophysical logging U_3O_8 measurements used in the Resource Estimate.

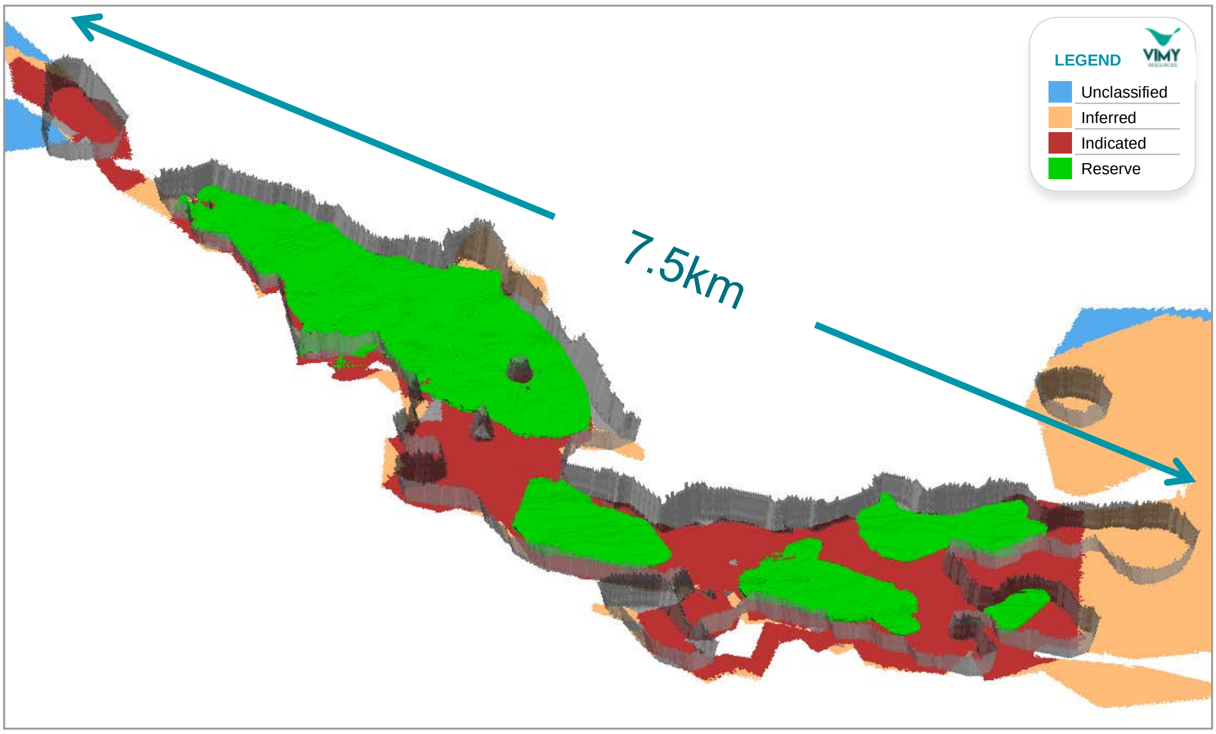


Figure 3: Ambassador – Probable Ore Reserve and Resource classification within Optimised Pit Shell (Oblique view looking from Ambassador West to Ambassador East)

The Ambassador Mineral Resource Estimate (Table 1) has increased to 30.3Mt at 590ppm U_3O_8 for a contained 39.2Mlbs U_3O_8 which represents a 3% increase in contained metal compared to the Mineral Resource Estimate released in September 2015 as well as a 45% increase in the amount of Indicated material.

Table 1: Ambassador Mineral Resource Estimate – June 2016

Classification	Cut-off Grade (ppm U_3O_8)	Tonnes (Mt)	U_3O_8 (ppm)	U_3O_8 (Mlb)
Indicated	150	19.8	720	31.5
Inferred	150	10.4	330	7.7
		30.3	**590**	**39.2**

Greater than 80% of the total contained uranium metal in the Ambassador resource is now classified at Indicated status. The Indicated resource is associated with two high-grade domains which were the focus of diamond drilling. In Figure 3 the optimised pit shell from the Pre-Feasibility Study (PFS released to the ASX in November 2015) is used to show the location of material classed as Probable Ore Reserves (see ASX release February 2016), as well as the material now classed as Indicated and Inferred in this release.

The Indicated Resource and Probable Ore Reserve show excellent continuity along the entire length of the PFS Ambassador optimised pit shell. It is expected there will be a very good conversion from Indicated to Probable Ore Reserve and this will support the DFS mine design, which is proposing to use continuous strip mining methods.

Pit optimisation studies, mine design and scheduling are underway using the updated resource.

Mulga Rock Mineral Resource Estimate and Ore Reserve

The Mineral Resource for the entire Mulga Rock Project (Table 2) comprises 66.5Mt at 520ppm U_3O_8 and 76.2Mlbs contained U_3O_8. Approximately 44% of the total resource is now in the Indicated category, at an aggregate grade of 720 ppm U_3O_8. The total contained uranium metal has also increased from 75.0Mlbs to 76.2Mlbs U_3O_8, as a result of a 3% increase in the Ambassador resource when compared to the contained metal in the September 2015 Mineral Resource Estimate.

Table 2: Mulga Rock Uranium Project Total Resource – June 2016

Deposit / Resource	Classification	Cut-off Grade (ppm U_3O_8) [4]	Tonnes (Mt) [3]	U_3O_8 (ppm) [4]	U_3O_8 (Mlb)
Mulga Rock East					
Princess [1]	Indicated	150	1.3	690	1.9
Princess [1]	Inferred	150	2.5	380	2.1
Ambassador	Indicated	150	19.8	720	31.5
Ambassador	Inferred	150	10.4	330	7.7
Sub-Total			**34.1**	**580**	**43.2**
Mulga Rock West					
Emperor [2]	Inferred	150	28.4	450	28.1
Shogun [2]	Inferred	150	4.1	550	4.9
Sub-Total			**32.5**	**460**	**33.0**
Total Resource			**66.6**	**520**	**76.2**

1. Princess resource estimate was reviewed by Coffey Mining and announced to the ASX on 18 December 2014.
2. Emperor and Shogun estimates were prepared by Coffey Mining and initially disclosed to the ASX on 13 January 2009 under the JORC Code 2004. They have subsequently been reviewed by Coffey Mining and re-released to the ASX on 18 December 2014 in accordance with the JORC Code 2012.
3. t = metric dry tonnes; appropriate rounding has been applied.
4. Using cut combined U_3O_8 composites (combined chemical and radiometric grades).

The information in Table 2 above that relates to the Emperor, Shogun and Princess Resources is extracted from ASX announcement entitled "Improved economics for the Mulga Rock Project increases the Mineral Resource Estimate" released on 17 September 2015 and is available to view on asx.com.au ASX:VMY. The Company confirms that it is not aware of any new information or data that materially affects the information included in the original market announcement and, in the case of estimates of Mineral Resources or Ore Reserves that all material assumptions and technical parameters underpinning the estimates in the relevant market announcement continue to apply and have not materially changed. The Company confirms that the form and context in which the Competent Person's findings are presented have not been materially modified from the original market announcement.

Table 3: Mulga Rock Project Ore Reserves – 29 March 2016

Deposit / Resource	Classification	Cut-off Grade (ppm U_3O_8)	Tonnes (Mt) [1,2]	U_3O_8 (ppm) [3]	Total Metal U_3O_8 (Mlb)
Mulga Rock East					
Princess	Probable	150	1.3 [1]	640 [1]	1.8
Ambassador	Probable	150	13.9 [1]	660 [1]	20.2
Total Reserve			**15.2** [1]	**660** [1]	**22.1**

1. Tonnages and grades are reported including mining dilution.
2. t = metric dry tonnes; appropriate rounding has been applied and rounding errors may occur.
3. Using cut combined U_3O_8 composites (combined chemical and radiometric grades).
4. Metallurgical plant recovery factors are not applied to Total Metal content.

The information in Table 3 above is extracted from ASX announcement entitled "Maiden Ore Reserve at Mulga Rock" released on 30 March 2016 and is available to view on asx.com.au ASX:VMY. The Company confirms that it is not aware of any new information or data that materially affects the information included in the original market announcement and, in the case of estimates of Mineral Resources or Ore Reserves, that all material assumptions and technical parameters underpinning the estimates in the relevant market announcement continue to apply and have not materially changed. The Company confirms that the form and context in which the Competent Person's findings are presented have not been materially modified from the original market announcement.

By-Products Resource Estimates

Base metals within the uranium mineralisation domains at Mulga Rock East are presented in Table 4. Base and other metals outside of the uranium domains are not economically recoverable and are therefore not included in the Resource.

Analysis of recent drilling data is ongoing to establish whether base metal resource estimation at the Mulga Rock West Deposit (Emperor and Shogun) is warranted; previous explorers did not assay for base metals during drilling.

Table 4: Base Metal Resource – Mulga Rock East

Deposit / Resource	Tonnes (Mt)	Cu (ppm) [1]	Zn (ppm) [1]	Ni (ppm) [1]	Co (ppm) [1]
Mulga Rock East – tonnes and grade					
Princess - Indicated	1.3	750	1280	440	210
Princess - Inferred	2.5	270	500	250	140
Ambassador - Indicated	19.8	340	1340	630	310
Ambassador - Inferred	10.4	110	320	250	140
Total	**34.1**	**280**	**960**	**480**	**240**

Deposit / Resource	Classification	Cu (kt)	Zn (kt)	Ni (kt)	Co (kt)
Mulga Rock East – contained metal					
Princess	Indicated	0.9	1.6	0.6	0.3
Princess	Inferred	0.7	1.3	0.6	0.4
Ambassador	Indicated	6.8	26.5	12.5	6.1
Ambassador	Inferred	1.2	3.3	2.6	1.5
Total		**9.6**	**32.7**	**16.3**	**8.2**

1 The base metal resource is contained wholly within the uranium resource. It is reported using the same cut-off grade of 150ppm U_3O_8 with no additional base metal grade cut-offs applied.

Geology of the Mulga Rock Uranium Deposit

The Mulga Rock uranium deposits are hosted by Cretaceous to Late-Eocene, lacustrine and estuarine sediments comprising fine-grained clastic sands, silts and clays, and carbonaceous matter derived from plants. Uranium and base-metal minerals are predominantly associated with supergene enrichment within carbonaceous-rich sediments at, or just below, the weathering horizon.

The sediments have been strongly oxidised by weathering to depths of between 25 - 45 metres. The uranium and base metals have been leached from the weathered zone and re-precipitated in horizontal zones at the reduction-oxidation (redox) boundary. The uranium mineralisation is mostly amorphous and has been absorbed on to the carbonaceous material or precipitated as very fine-grained uraninite (UO_2).

The mineralised zones are similar in geology, mineralogy and host rock material across all deposits.

Typical cross sections for the western portion of the Ambassador Mineral Resource are shown in Figures 4 and 5, with a long section of the Ambassador North deposit, a small satellite resource to the main Ambassador East deposit, and included in this Mineral Resource. The cross sections show the resource block model with a 150ppm U_3O_8 cut-off grade. The upper uranium domain is located directly below the redox boundary that is predominantly located within younger, Eocene sediments. Uranium grade in the upper domain is typically higher than the uranium domains located in the lower, older, Eocene and Cretaceous sedimentary basement material.

Long sections for the Ambassador Mineral Resource are shown in Figures 6 and 7. Again, the vast majority of the uranium mineralisation is located in the upper domain at, or near, the redox boundary within carbonaceous material. The upper uranium domain ranges in thickness from 2-8 metres.

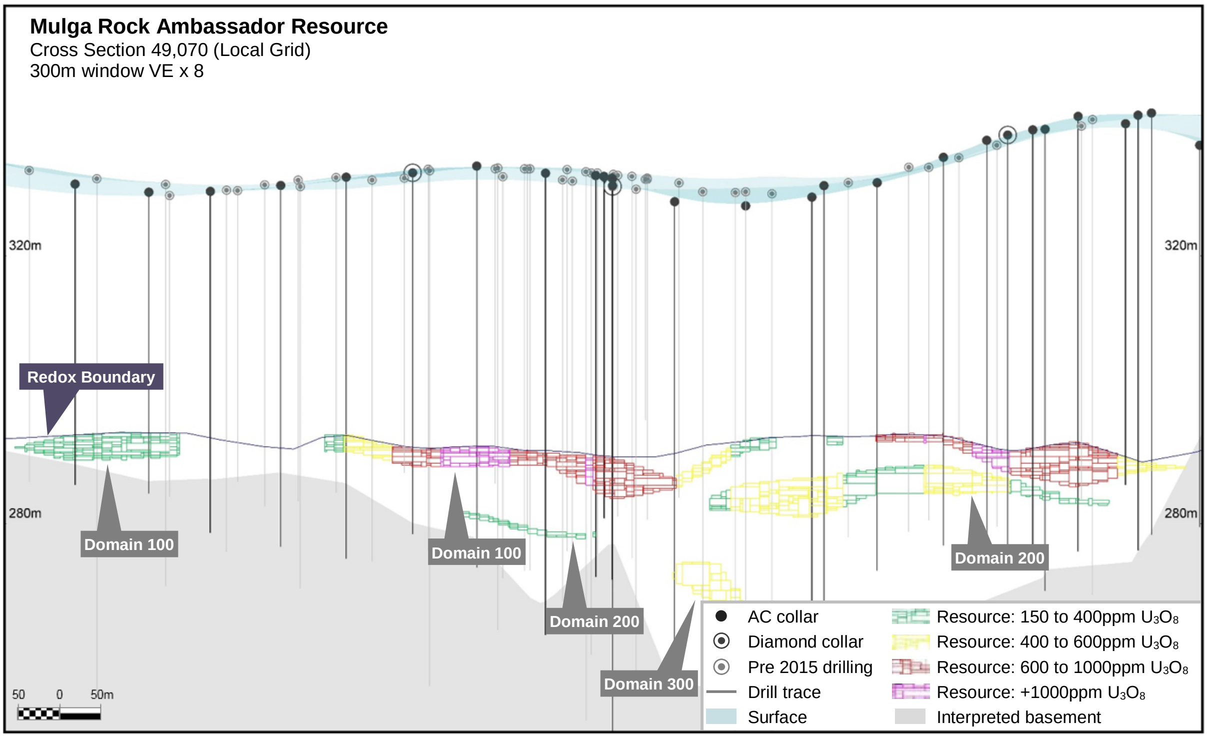


Figure 4: Ambassador Resource – Schematic cross section 49,070N – vertical exaggeration 8x

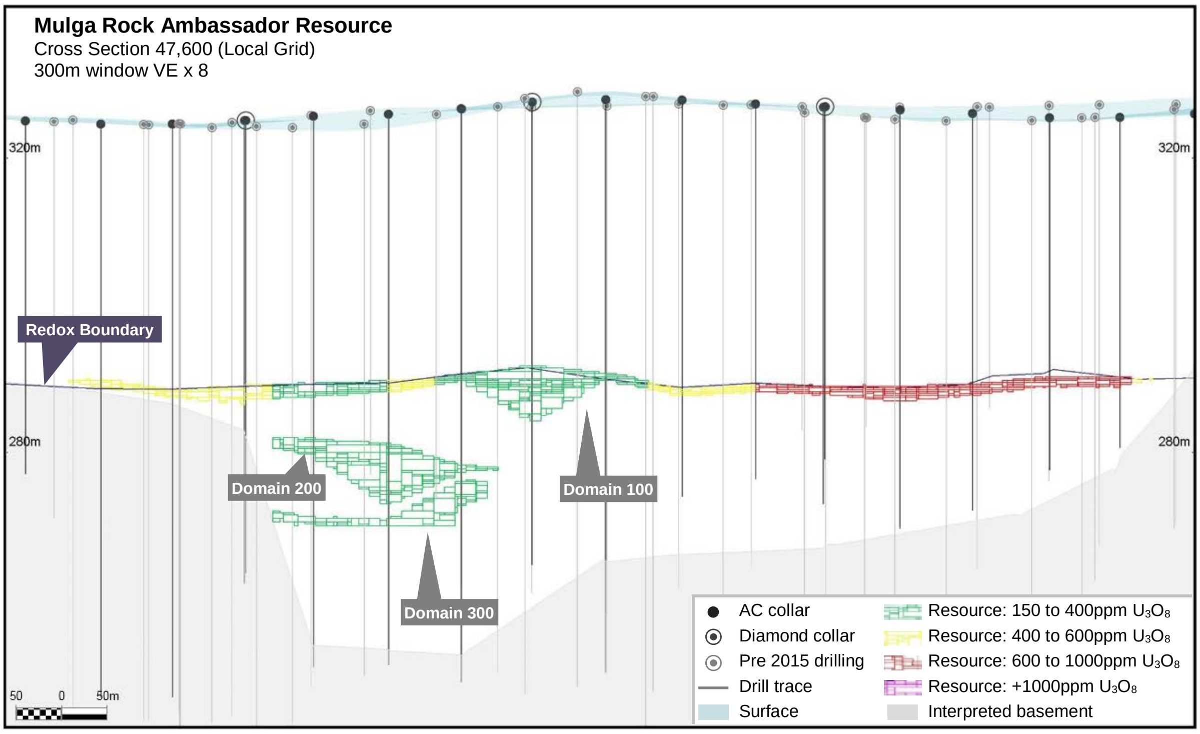


Figure 5: Ambassador Resource – Schematic cross section 47,600N – vertical exaggeration 8x

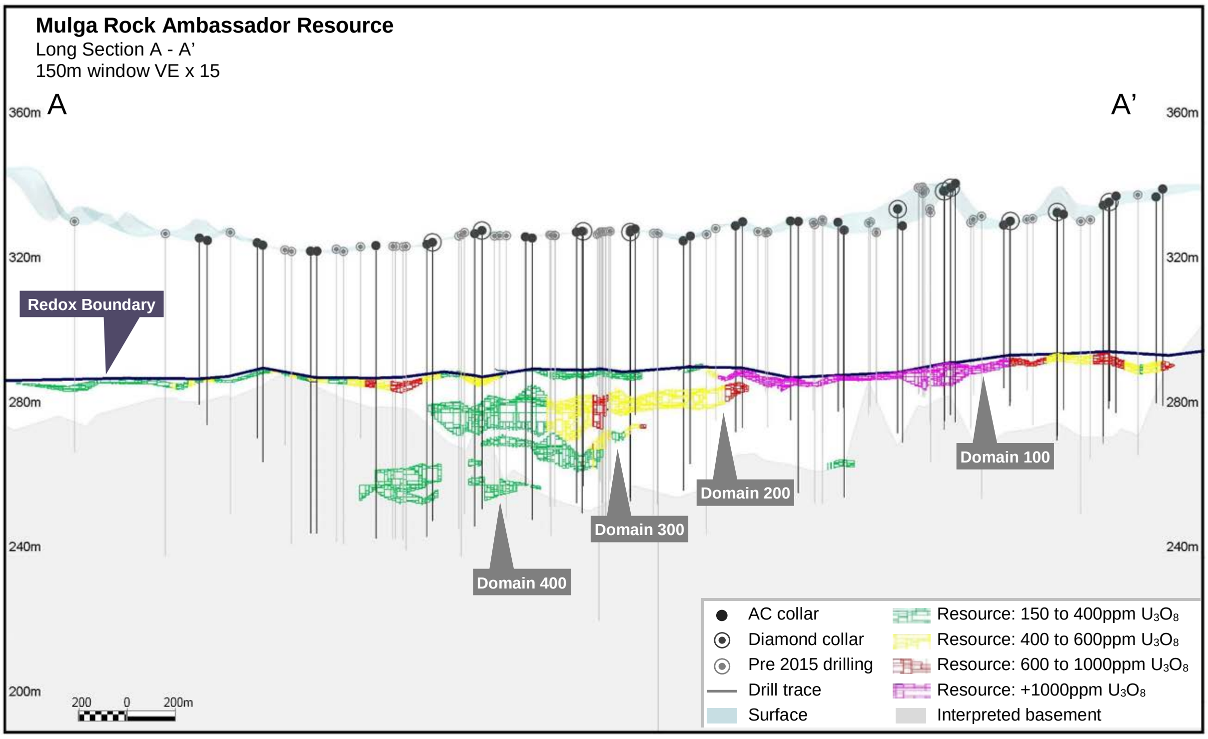


Figure 6: Ambassador Resource – Long section (A'-A), vertical exaggeration 15x

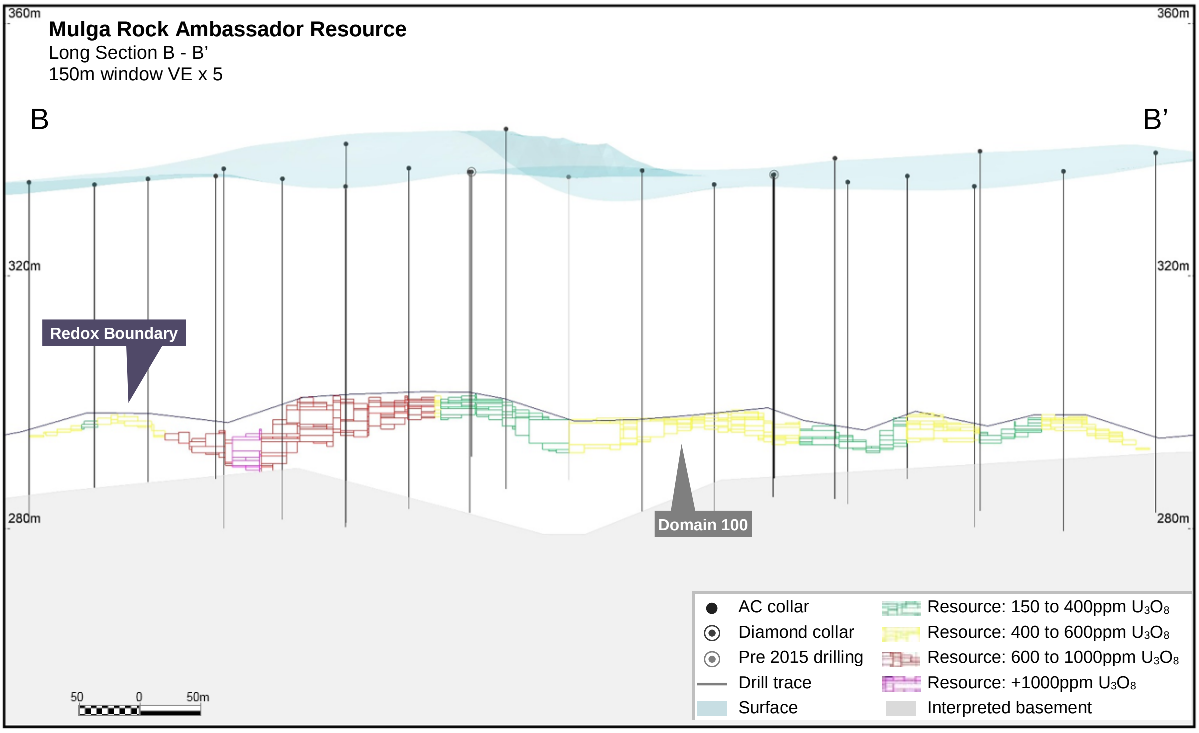


Figure 7: Ambassador North Satellite Resource – Long section (B-B'), vertical exaggeration 5x

Mike Young
Managing Director and CEO

Dated: 23 June 2016

The information in this announcement that relates to the Exploration Results for the Mulga Rock Resource Estimate (U_3O_8), Resource Database, Geology and Bulk Densities is based on information compiled by Xavier Moreau, who is a Member of the Australian Institute of Geoscientists. Mr Moreau is a full time employee of Vimy Resources. Mr Moreau has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which is being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the JORC 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Moreau consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears.

The information in this announcement that relates to the Mulga Rock Mineral Resource estimates (U_3O_8) is based on information compiled under the supervision of AMC Consultants as consultants to the Company and reviewed by Ingvar Kirchner, an employee of AMC Consultants. Mr Kirchner consents to the inclusion, form and context of the relevant information herein as derived from the original resource reports. Mr Kirchner has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which is being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the JORC 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'.

Executive Summary

Ambassador is one of several uranium deposits comprising the Mulga Rock Project (MRP). The area of the Ambassador Deposit was subject to uranium exploration by PNC Exploration Australia Pty Ltd (PNC) during 1979 to 1988, which resulted in the discovery of uranium and the MRD. The MRP is located approximately 240km east-northeast of Kalgoorlie in Western Australia. The MRD currently comprise the Emperor, Shogun, Ambassador and Princess uranium deposits which are located within the Mining Leases (ML) 39/1080 and 39/1081.

This report documents an updated 2016 Mineral Resource for the Ambassador uranium deposit completed by Vimy Resources Ltd (Vimy) under the supervision of AMC Consultants (AMC). The report complies with disclosure and reporting requirements set forth in the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves of December 2012 (the JORC Code) as prepared by the Joint Ore Reserves Committee of the Australasian Institute of Mining and Metallurgy, Australian Institute of Geoscientists and Mineral Council of Australia (JORC).

Coffey Mining Pty Ltd (Coffey) generated the Mineral Resource for Ambassador in January 2009 following Vimy drilling programmes in 2008 and 2009. Uranium data only was examined. In 2010, Coffey was commissioned by Vimy to update resource modelling for the uranium and base and other metals (BOM) for Ambassador.

Utilising further Vimy extensive drilling over the eastern portion of the Ambassador deposit in 2014, this new Mineral Resource is to be used to form the basis of an updated Scoping Study and Pre-Feasibility Study.

The Ambassador and Princess deposits are supergene deposits associated with multiple phases of weathering, the most recent of which have occurred within the last 300,000 years. The mineralogy of the MRP is complex, with over 50 minerals being recognised at Shogun in addition to the common rock-forming minerals. The bulk of the uranium occurs as diffuse concentrations, too fine to be resolved by scanning electron microscopy (SEM), and disseminated evenly throughout the organic rich sediments. The major zone of uranium accumulation within the deposit occurs as a sub-horizontal planar body that is strongly correlated with both the unpressurised groundwater surface and fine textured, carbonaceous sediments such as lignites and lignitic clays. It is theorised that uranium (and other base metals within the deposit) were transported laterally from source materials in oxidised form by acidic, meteoric flow. The metals were then concentrated and eventually fixed (reduced) in the anoxic, capillary fringe at the surface of the water table. Uranium reduction and fixation (U^{6+} to U^{4+}) is thought to be largely biogenic (enzymatically catalysed reduction by U-bacteria). The anoxic (reduced) capillary fringe is much thicker in fine textured sediments (such as lignites) than in coarser textured sediments such as carbonaceous sands. As such, most uranium accumulation in the MRP is similarly correlated with lignitic materials at the water table surface. Uranium accumulation does occur at the water table surface in medium to coarse sands, but is generally too thin to be of commercial value. More redox active metals (such as Cu, Ni and Zn) tend to reduce and fix at redox interfaces below the water table surface. Mineralisation, therefore, is controlled by the lithological and geochemical properties of the sediments rather than by stratigraphy. Suitable lithological and geochemical environments for significant metal accumulation occur in both remnant carbonaceous Cretaceous sediments and Eocene palaeochannel sediments.

The water table surface, and associated uranium and base-metal mineralisation, exist within carbonaceous, Cretaceous sediments in the north-eastern portion of the Ambassador East deposit and in some fringing parts of the deposit. Eocene palaeochannel sediments dominate the mineralisation in the central and southern portions of the deposit. Uranium mineralisation commences at depths ranging from 35m to 45m.

Vimy is responsible for the drillhole database and geology used in the resource estimate with data compiled in a Datashed database system. The Mineral Resource for the Ambassador Deposit contains a total of 1696 drillholes (totalling 106.6km of drilling); of which 1471 drillholes (totalling 90km) were used, and comprising a mixture of data including:

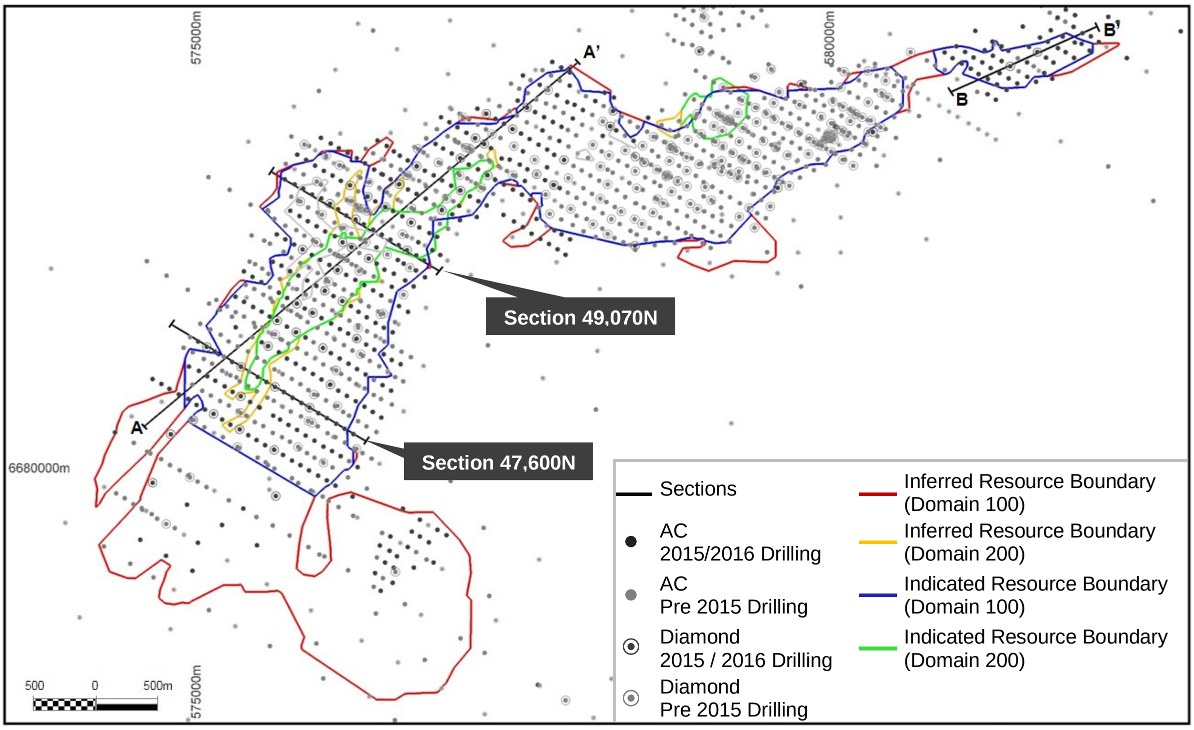
- Recent radiometric probe data primarily from aircore (AC) and reverse circulation (RC) holes.
- Historical and recent chemical assay data primarily from diamond core holes (DC).
- Some historical radiometric data for PNC drillholes.

The drillholes within the uranium Mineral Resource boundary comprise:

- 1,036 AC holes (68,686m total; 1035 holes for 64,425m used);
- 288 DC holes (16,062m total; 279 holes for 15,015m used);
- 295 RC holes (20,812m total; 144 holes for 9,881m used);
- 11 face discharge AC and 5 sonic holes; (1,012m total; 13 holes for 703m used).

Drillholes that were omitted tended to lack both radiometric and/or assay data for a variety of reasons. The drill locations and types are shown on Figure 1.

Figure 1 Ambassador – Collar location map and drill hole type



The mineralised zones were defined by interpretation of stratigraphy, geology, and anomalous grades.

Using geology and stratigraphic positions, the uranium mineralised zones were further defined using an eU_3O_8 > 100ppm cut-off grade (prior to disequilibrium correction, for percussion drilling) and/or chemical U_3O_8 > 100ppm cut-off grade (for diamond drilling). A minimum thickness of 0.5m and maximum 1m internal dilution was allowed for in definition of the mineralisation domains. This protocol defined four uranium mineralised zones of which the upper Domain 100 zone is both the most laterally extensive and highest grade. The successively stratigraphically lower Domains 200, 300, and 400 zones tend to be both progressively lower in grade and less extensive. Schematic cross sections and long sections of the mineralisation relative to the palaeochannels and stratigraphy are shown in Figure 2, Figure 3, Figure 4 and Figure 5.

Base and Other Metal (BOM) zones were variably mobile within the weathering profile and stratigraphy, and therefore were independently constrained using a variety of lower cut-off grades which attempt to discern anomalous metal grades from essentially un-mineralised background material. The BOM zones were modelled using Leapfrog for each element using the following lower cut-off grades:

- Cu—100ppm; 3 sub-domains
- Co—100ppm; 4 sub-domains
- Ni—300ppm; 4 sub-domains
- Zn—1500ppm; 3 sub-domains
- Sc—50ppm; 2 sub-domains

Figure 2 Ambassador Resource – Schematic cross section 49,070N – vertical exaggeration 8x

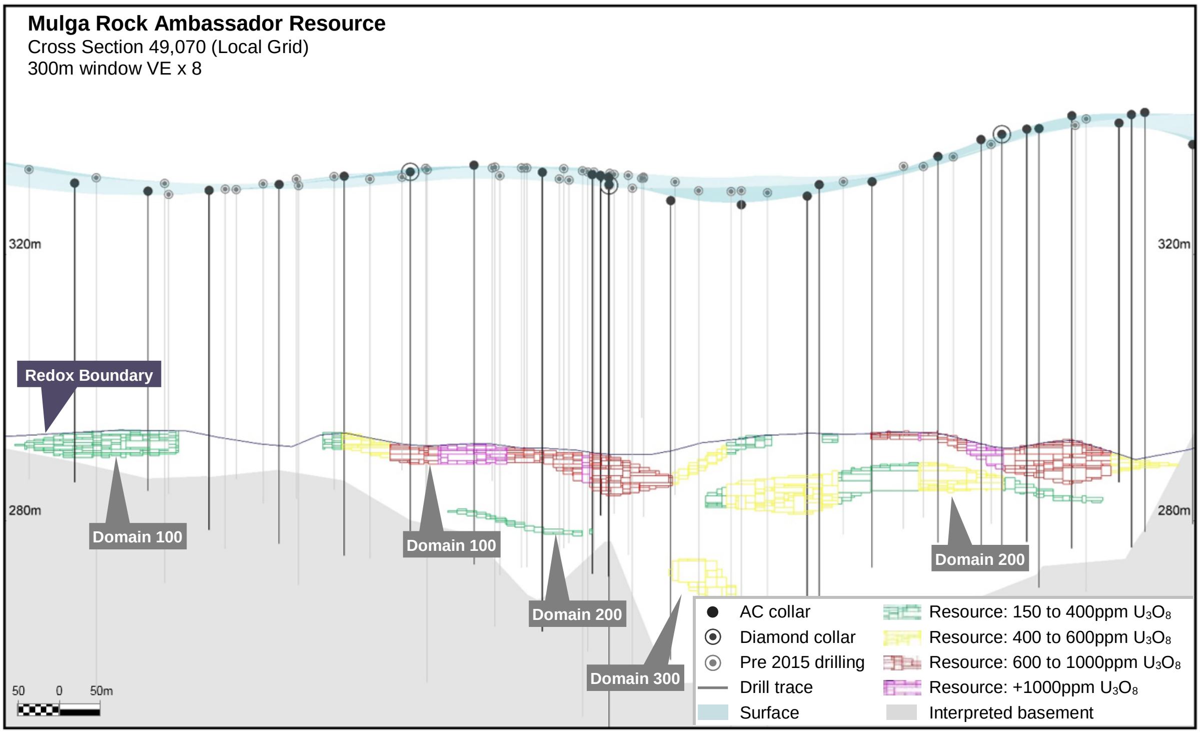


Figure 3 Ambassador Resource Schematic cross section 47,600N – vertical exaggeration 8x

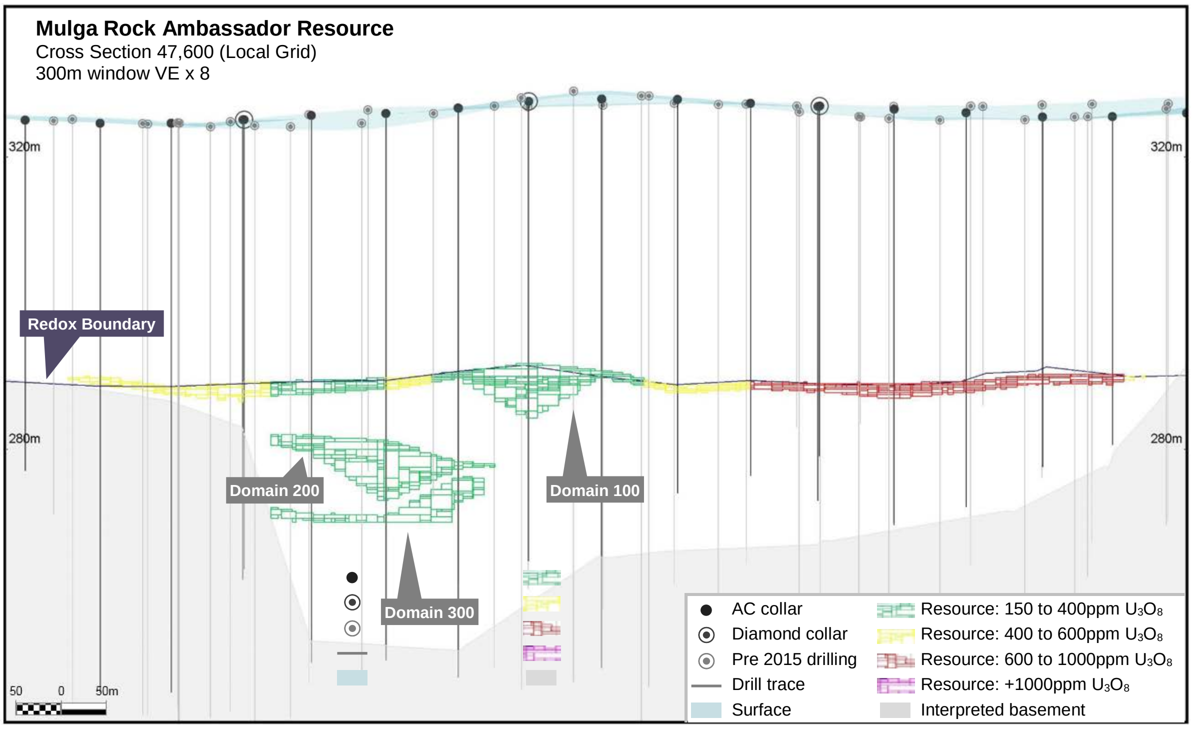


Figure 4 Ambassador Resource – Long section (A-A') – vertical exaggeration 15x

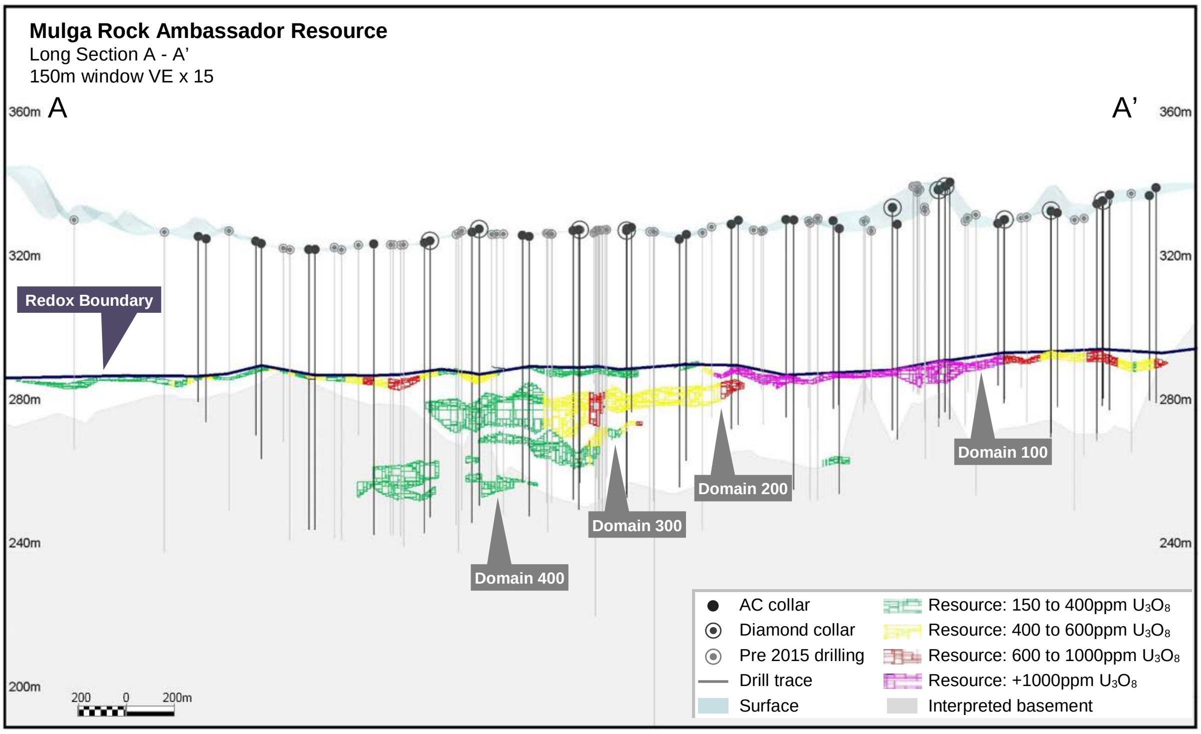
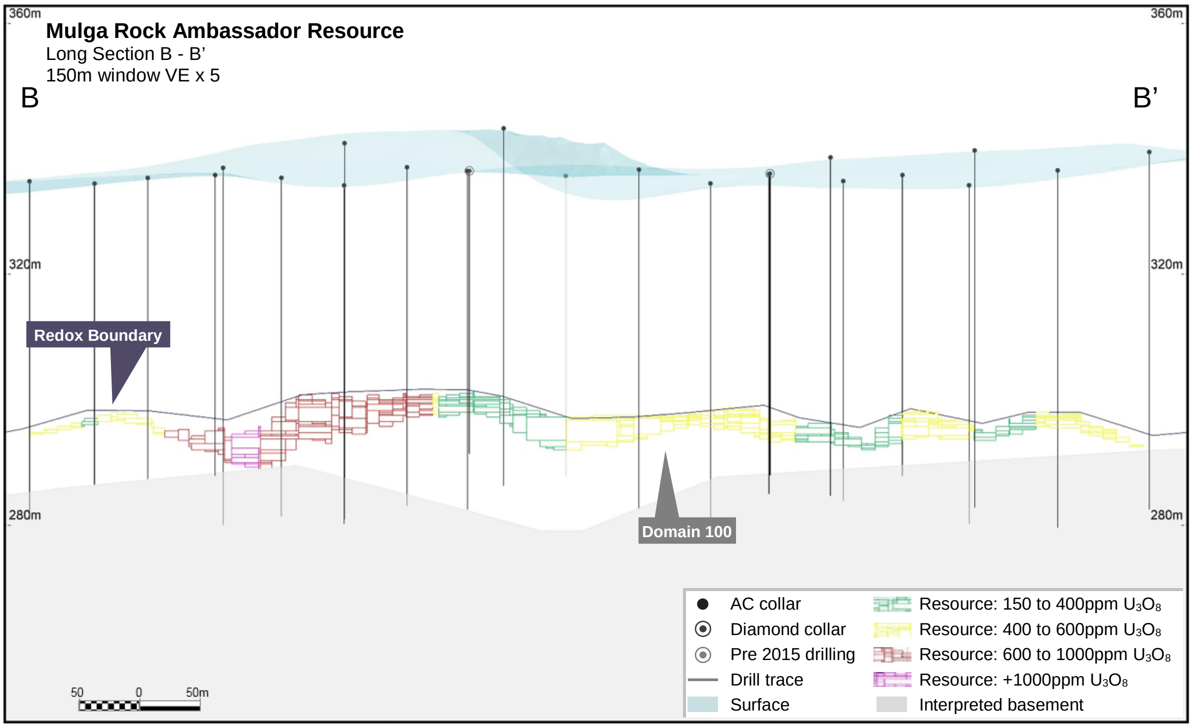


Figure 5 Ambassador North Satellite Resource – Long section (B-B') – vertical exaggeration 5x



In order to address potential disequilibrium and sample quality issues, 30 "twin" DC and AC holes were completed in 2015-2016 at the Ambassador deposit. A detailed study was completed to assess the following aspects:

- Gamma-derived eU_3O_8 between the DC and AC holes. Outcomes were as follows:
  - Global statistical calculations confirmed earlier reports that the gamma-derived eU_3O_8 from the twin DC and AC holes were comparable despite possible variations in hole diameters, casing, hole condition etc. Minor variations between twin holes are noted, but are assumed to be caused by short range variability in both geology and mineralisation—those assumptions were validated by other testwork.
- Chemical assay-derived U_3O_8 between the DC and AC holes. Outcomes were as follows:
  - Samples derived from the DC holes are of reasonable to good quality.
  - The effects of sample smearing in the 2015 study are apparent within a number of the AC holes from the 2016 study, although there are also examples where this effect is either minimal or absent.
  - As a result, U_3O_8 values derived from AC holes are likely to be low biased in terms of grade and high biased in terms of interval width.
  - For the purposes of resource estimation, eU_3O_8 (corrected for disequilibrium) should be used in preference to U_3O_8 assays for the AC holes. This would also apply to other drilling techniques such as RC and rotary mud, where the likelihood of smearing and/or sample contamination is typically high.
- Base metal assays between the DC and AC holes. Outcomes were as follows:
  - Smearing and/or metal loss also affects the other metals at the MRP (cobalt, copper, nickel and to a lesser extent zinc) in AC holes to varying degrees, particularly for pre-2015 aircore drill holes.

- Where present, this smearing and/or metal loss can lead to both a low biasing of the metal in question and also a high biasing of the mineralised interval width.

The net conclusions from the twin hole study—as it affects the data used for the resource estimate--are as follows:

- AC eU_3O_8 data (corrected for disequilibrium) should be used in preference to the AC chemical assay U_3O_8 data due to sample quality/potential smearing issues where possible.
- Chemical U_3O_8 data should be used from the DC holes where possible.
- Disequilibrium corrections derived from DC eU_3O_8/U_3O_8 sample interval pairs are valid to be extrapolated from the DC holes to the AC holes.
- AC chemical assay data for the BOMs, for which there is no equivalent radiometric determination, will be used "as-is" under the assumption that metal and grades reporting within the uranium domains are likely to be low and conservative as reported within the uranium domains.

As is normal for most uranium deposits, the radiometric equivalent U_3O_8 (eU_3O_8) grades require adjustment for disequilibrium using regression equations derived from the comparison of paired assay results with composited radiometric logging from the various phases of DC drilling. In the majority of cases at Ambassador, the radiometric eU_3O_8 grades for similar intervals are lower than the corresponding chemical assays for U_3O_8, requiring general positive adjustments to the radiometric data to emulate the accurate chemical assay data. To obtain a robust global estimate of the disequilibrium, each of the four uranium domains was first split into groups (based on the data type/vintage) and then further split into distinct grade bins. These grade bins were determined based on apparent "natural breaks" in the dataset identified in Q-Q plots and statistics. Specifically, disequilibrium corrections (regression formulae for the Q-Q data) were derived for:

- Domain 100 PNC data where eU_3O_8 data was derived from digitised logs. Two grade bins were considered and the following factors utilised:
  - Low grade (100-450ppm eU_3O_8): $y = 8E\text{-}08x^4 - 1E\text{-}04x^3 + 0.0428x^2 - 5.8682x + 349.83$
  - High grade (>450ppm eU_3O_8): $y = 3E\text{-}09x^3 + 1E\text{-}05x^2 + 1.4022x - 150$
- Domain 100 PNC data where the holes were re-logged in 2008. Three grade bins were considered and the following factoring used:
  - Low grade (100-180ppm eU_3O_8): $y = 1.653x - 77.9$
  - Mid grade (180-350ppm eU_3O_8): $y = 2.4645x - 231.21$
  - High grade (>350ppm eU_3O_8) $y = 9E\text{-}05x^2 + 1.3132x + 169.03$
- Domain 100 for Vimy data and holes drilled between 2008 and 2014. Three grade bins were considered:
  - Low grade (100-210ppm eU_3O_8): $y = 0.0043x^2 + 0.2615x + 67.185$
  - Mid grade (210-750ppm eU_3O_8): $y = 9E\text{-}10x^4 - 3E\text{-}06x^3 + 0.00335x^2 - 0.3449x + 135.87$
  - High grade (>750ppm eU_3O_8): $y = 1.8771x + 400$
- Domain 100 for Vimy data Ambassador West holes drilled between 2015 and 2016. Four grade bins were considered:
  - Very low grade (44-60ppm eU_3O_8): $y = 3.3992x - 104.69$
  - Low grade (60-295ppm eU_3O_8): $y = -0.0005x^2 + 1.9955x -23.345$
  - Mid grade (295-778ppm eU_3O_8): $y = 8E\text{-}06x^3 - 0.0145x^2 + 9.9305x - 1264.4$
  - High grade (>778pm eU_3O_8): $y = 2514.3\ln(x) - 15343$

- Domain 200 for Vimy data Ambassador West holes drilled between 2015 and 2016. Four grade bins were considered:
  - Very low grade (52-57ppm eU_3O_8): y = 3.5402x - 111.81
  - Low grade (57-240ppm eU_3O_8): $y = 0.0076x^2 - 0.2674x + 91.306$
  - Mid grade (240-350ppm eU_3O_8): $y = -0.0108x^2 + 9.2041x - 1191.3$
  - High grade (>350pm eU_3O_8): $y = -0.0055x^2 + 7.598x - 1265.8$
- Combined lower uranium Domains 300, and 400 Vimy data Ambassador holes drilled between 2015 and 2016. Four grade bins were considered:
  - Very low grade (45-76ppm eU_3O_8): y = 1.1808x + 6.4643
  - Low grade (76-160ppm eU_3O_8): $y = 0.0096x^2 - 1.4138x + 156.95$
  - Mid grade (160-318ppm eU_3O_8): $y = 0.0036x^2 + 0.2674x + 16.313$
  - High grade (>318ppm eU_3O_8): $y = -0.0043x^2 + 6.1315x - 1128.3$
- Combined lower uranium Domains 200, 300, and 400, for Vimy data and holes drilled between 2008 and 2014. Three grade bins were considered:
  - Low grade (100ppm to 145ppm eU_3O_8): y = 0.6331x + 50.342.
  - Mid grade (145ppm to 500ppm eU_3O_8): y = 2.478x - 200.
  - High grade (>500ppm eU_3O_8): y = 1.2599x + 300.
- Domain 100 Vimy data for holes drilled at Ambassador NE between 2015 and 2016. Two grade bins were considered:
  - Very low to low grade (60-350ppm eU_3O_8): y = 1.0126x + 34.242
  - Low to high grade (350-2500ppm eU_3O_8): y = 3.3209x – 921.21

Any Vimy radiometric data below eU_3O_8=45ppm within the uranium domains were not corrected for disequilibrium as the material was considered to be internal dilution and the corrections applied within that grade range were likely to be both minimal and inaccurate. The disequilibrium adjustments were validated by the domains. When compared to the raw eU_3O_8 dataset, the disequilibrium corrected data (hereafter referred to as eU_3O_8d) is significantly closer statistically to the assay-derived U_3O_8 data.

The hybrid data set (eU_3O_8d data primarily from the AC/RC holes, and U_3O_8 data primarily from the DC holes) and BOM data were composited to 0.5m intervals utilising a residual retention process to avoid loss of data at the downhole margins. Relatively light high grade cuts were applied to the hybrid U_3O_8 and BOM composite data. Top-cuts for the U_3O_8 were evaluated for both the Ambassador East and West areas for Domains 100 and 200, and then Domains 300 and 400 which only occur in the West area. The BOM elements were statistically evaluated by element over the entire Ambassador deposit.

For Domains 100 and 200, which are essentially relatively thin and flat-lying zones, the 0.5m U_3O_8 composite data (plus any residuals) were re-composited to the full vertical width of the domains such that a single composite of variable width represents each drillhole.

The block model dimensions cover a region of roughly 10.5km x 9km. Parent block dimensions are 50mE x 50mN x 10mZ with sub-celling down to 10mE x 10mN x 0.25mZ.

For Domains 100 and 200, an Accumulation Estimation process using Ordinary Kriging (OK) is used to estimate the hybrid U_3O_8 data. The full thickness composite intervals of varying lengths are used to calculate [grade x thickness] accumulation variables; the thickness is expressed as millimetres in order to keep the thickness roughly the same order of magnitude values as the U_3O_8 grades. Variogram models are generated for the U_3O_8 [grade x thickness] accumulation variables. Estimation of the [grade x thickness] accumulation variable and [thickness] service variable is done using OK and identical search and variogram model parameters. Block grades for U_3O_8 are then back-calculated from the block accumulation and service variables (grade = [grade x thickness] / [thickness]). The accumulation estimate was run in a parent block utilising an exaggerated height to prevent inadvertent different parent block estimates in the Z dimension. The resultant blocks were then cut back to the original sub-cells and parent blocks governing the remainder of the model.

For Domains 300 and 400, and the BOM domains, Ordinary Kriging (OK) was used as the estimation method due to the thicker zones, quality, quantity and spacing of the available data and the interpreted controls on the mineralisation under review. Variogram models were generated for each of the relevant U_3O_8 and BOM elements.

Bulk density data (wet, dry, and moisture) was attributed to the resource model based upon an analysis of immersion bulk density data, wireline density logs for DC holes, and ultimately a hybrid data set coded for the key lithologies (basement, claystone, conglomerate, carbonaceous sandstone, laterite, lignitic clay, sandstone and siltstone). Use of the wireline density data in conjunction with the [weight/volume] methods generated a more comprehensive data set across the range of lithologies for use in modelling without some of the biases related to selection of competent units of core for weight/volume measurements. Dry bulk density values range from 0.69t/m^3 (for lignitic clay) to 1.45 t/m^3 (for sandstone) in the range of material associated with the uranium mineralisation.

Bulk densities were estimated in the block model using indicator derived fractions for the eight key lithologies (basement, claystone, conglomerate, carbonaceous sandstone, laterite, lignitic clay, sandstone, and siltstone). The indicators were estimated into the block model using Inverse Distance (Power=1) method. The indicator estimates were constrained within the Domains 100-400, and background material separately above and below Domain 100. Results between the indicator lithology fields were normalised to 1, and a lithology based bulk density assigned on a majority basis to the blocks. Therefore, bulk density values can be variable within the uranium domains, dependent on variations in lithology.

Average bulk densities and moistures for the classified portions of the domains are given in Table 1.

Table 1 Average density and moisture values for the classified portions of the uranium mineralisation domains

Deposit	Domain	Bulk density dry (t/m^3)	Moisture (% of dry BD)	Bulk density wet (t/m^3)
Ambassador West	100	1.07	0.49	1.56
Ambassador East	100	1.12	0.45	1.58
Ambassador West	200	1.21	0.39	1.63
Ambassador East	200	1.30	0.38	1.76
Ambassador West	300	1.38	0.32	1.81
Ambassador West	400	1..41	0.32	1.84

Note: Appropriate rounding has been applied.

Redox, water table, and stratigraphy were flagged in the block model based on interpreted wireframe surfaces provided by Vimy geologists.

The summarised Ambassador Mineral Resource Statement in Table 2 has been determined as at 1 June 2016 and is reported in accordance with the guidelines as set out in the JORC Code (2012). The resource estimate has been classified as a combination of Indicated and Inferred Resource based on the confidence of the input data, drillhole spacing, geological interpretation, and grade estimation. The resource classification assumes potential exploitation by conventional open cut mining methods.

The base and other metals (BOMs) are also reported as part of the Mineral Resource as potential by-products. The BOM elements Co, Cu, Ni, Sc, and Zn are reported for the corresponding portions of the uranium domains using the U_3O_8 cut-off of 150ppm. Classification of the BOM by-products is considered to be the same as the U_3O_8; however, the BOM material is not currently considered to be economically independent of the U_3O_8 mineralisation. Table 3 contains the concentration and contained metal for each BOM element associated with the classified tonnages for the uranium domains.

Table 2 Ambassador Mineral Resource table by uranium domain, June 2016

June 2016 Ambassador Mineral Resource

U_3O_8 Reported by Uranium Domains using a Lower Cutoff of 150ppm U_3O_8

Assuming open cut mining all mineralisation

Accumulation method / Ordinary Kriging Grade Estimates within Parent Cells of 50m by 50m by 10m

Using Cut U_3O_8 Composites (combined chemical and radiometric grades)

Rounded figures, sums may vary slightly

Uranium Domain	Resource Classification						Total		
	Indicated			Inferred					
	Tonnage (Mt)	U_3O_8 (ppm)	Metal (Mlb)	Tonnage (Mt)	U_3O_8 (ppm)	Metal (Mlb)	Tonnage (Mt)	U_3O_8 (ppm)	Metal (Mlb)
100	15.10	830	27.5	5.4	380	4.5	20.5	710	32.0
200	4.80	380	4.0	0.4	300	0.3	5.2	370	4.3
300	0	0	0	3.8	300	2.5	3.8	300	2.5
400	0	0	0	0.8	200	0.4	0.8	200	0.4
Total	**19.8**	**720**	**31.5**	**10.4**	**330**	**7.7**	**30.3**	**590**	**39.2**

Table 3 Base and Other Metals reported within the uranium mineralised zones

June 2016 Ambassador Mineral Resource

Base and Other Metals Grades

Reported by Uranium Domains using a Lower Cutoff of 150ppm U_3O_8

Ordinary Kriging Grade Estimates within Parent Cells of 50m by 50m by 10m

Using Cut Composites (chemical assay data)

Rounded figures, sums may vary slightly

Resource Classification	Tonnage (Mt)	Cu (ppm)	Cu metal (Kt)	Zn (ppm)	Zn metal (Kt)	Ni (ppm)	Ni metal (Kt)	Co (ppm)	Co metal (Kt)
Indicated	19.8	340	6.8	1340	26.5	630	12.5	310	6.1
Inferred	10.4	110	1.2	320	3.3	250	2.6	140	1.5
Total	**28.2**	**260**	**7.9**	**980**	**29.8**	**500**	**15.1**	**250**	**7.6**

Table 4 Footnotes for Table 2 and Table 3

Notes

- Appropriate rounding has been applied in the tables above.
- The Ambassador Mineral Resource is reported in accordance with the JORC Code 2012 guidelines.
- The Mulga Rock Project is located approximately 240km east-northeast of Kalgoorlie in the state of Western Australia.
- Ambassador, Princess, Emperor and Shogun are sediment-hosted uranium deposits. The mineralisation is hosted primarily by reduced sediments of Eocene age preserved within a complex set of sedimentary troughs overlying an extensive long-lived palaeodrainage referred to as the Mulga Rock palaeochannel.

- Drill spacing at Ambassador varies from nominal 100 m spaced WNW-ESE fences and typical 40 to 80m drill spacing along the fences, with some local close space infill, hole twinning.
- The current Mulga Rock Ambassador drilling database comprises 1,696 drillholes. Of these 1696 drillholes, 288 were DC holes, 10 8" DC bulk sample drillholes, 295 were RC, 1097 were AC, and 5 were sonic drillholes.
- Hole types are a mix of diamond core, reverse circulation, air core holes, and sonic holes. Due to concerns regarding sample collection quality and recovery, the use of aircore chemical assays in the 2016 Resource estimate is very limited. Radiometric eU_3O_8 data adjusted for disequilibrium is used in preference for the aircore type holes.
- 2008-2016 Vimy and historical PNC chemical data and radiometric data were used in the 2016 resource estimate of U_3O_8.
- Multi-element data used for estimates of the base and other metals is sourced from Vimy chemical assay data.
- AMC note that the quality of the PNC assay data ranges from moderate to good, with many of the diamond drillholes chemical assays having been sourced from hard-copy laboratory certificates. However, it also noted that there is a lack of QA/QC data regarding standards and blanks in particular, as well as little information being available regarding exact laboratory analytical procedures. However, the laboratories used were well regarded at the time and the use of XRF and ICP-MS for uranium analysis is an industry standard today.
- QA/QC of Vimy assay samples since 2008 are of current industry standard and outlined in the JORC Code 2012 Table 1 Section 1 below. Field duplicates, standards, and blanks were routinely submitted.
- Radiometric logging of the PNC and Vimy drillholes was conducted. Appropriate post-processing was completed on the data for conversion to a standardised eU_3O_8 value for all drillholes.
- In the majority cases at Ambassador and Princess, the radiometric eU_3O_8 grades for similar intervals are lower than the corresponding chemical assays for U_3O_8, requiring positive adjustments to the radiometric data to emulate the accurate chemical assay data. Data for each of the four uranium domains were split into groups (based on the data type/vintage) and then further split into distinct grade bins. These grade bins were determined based on apparent natural breaks in the dataset identified in Q-Q plots and statistics. Specifically, disequilibrium corrections (regression formulae for the Q-Q data) were derived for:
  - Domain 100 PNC data where eU_3O_8 data was derived from digitised logs.
  - Domain 100 PNC data where the holes were re-logged in 2008.
  - Domain 100 Vimy data, sub-domains AE, for holes drilled from 2008 to 2014.
  - Domain 100 Vimy data, sub-domains ANE, AE, and AW, for holes drilled from 2015 to 2016.
  - Domain 200 Vimy data, sub-domains AE and AW, for holes drilled from 2015 to 2016.
  - Combined lower uranium Domains 200, 300, and 400 Vimy data for holes drilled from 2008 to 2014.
  - Any radiometric data below eU_3O_8 =60ppm within the uranium domains were not corrected for disequilibrium.
- The Ambassador mineralisation boundaries were based upon a combination of geology/stratigraphy and a nominal 100ppm U_3O_8 lower cut-off (chemical assay data, and non-disequilibrium corrected eU_3O_8 data) defining a mineralised zone of at least 0.5m thickness and honouring, where possible, the geology. This value was chosen as it represents a natural break in the distribution of grades distinguishing mineralisation from unmineralised material.
- As the assay database consists of both chemical U_3O_8 data and radiometric eU_3O_8 data, the combined dataset is used with priority given to chemical assay data from the diamond drillholes; otherwise the factored radiometric data was used.
- Statistical analyses were completed on the raw sample data and the 0.5m composite data. High grade cuts were applied as follows:
  - Domain 100 Ambassador East – 8,000ppm U_3O_8
  - Domain 100 Ambassador West – 5,500ppm U_3O_8
  - Domain 200 Ambassador East – 1,100ppm U_3O_8
  - Domain 200 Ambassador West – 1,700ppm U_3O_8
  - Domain 300 – 1,100ppm U_3O_8
  - Domain 400 – 650ppm U_3O_8
- Relatively light high grade cuts were also applied to the base and other metal elements.
- Grade variography was generated for the grade estimation by Accumulation Method via Ordinary Kriging and/or Ordinary Kriging. The directional variography was moderately well-structured for Domains 100, 200 and weakly structured for 300 and 400.
- Grade estimates were generated for parent blocks of size 50m (X) x 50m (Y) x 10m (Z) with sub-blocks of size 10m x 10m x 0.25m. The block XY dimensions are approximately half of the nominal drill spacing in some areas.
- Grade estimates were generated by Accumulation Method via Ordinary Kriging for Domains 100 and 200 U_3O_8, and Ordinary Kriging for other domains and other metals. Appropriately cut and composited data was used for the various methods utilised.
- Bulk densities were estimated in the block model using indicator fractions flagging the key rock types present. Bulk density values were derived from analysis of Archimedean data and selective use of corrected gamma probe data as documented by Vimy. Lithology dry bulk densities range from 0.7 t/m^3 for lignitic clay material to 1.9 t/m^3 for basement material. The uranium domains contain a mix of lithology types, and the domain average densities reflect that.
- The grade estimates for all zones have been classified as Indicated and Inferred under the JORC Code 2012 guidelines based on the confidence levels of the key criteria that were considered during the resource estimation.
- The reporting cut-off grade of 150ppm U3O8 currently reflects an expected open pit mining scenario reliant on mechanised strip mining equipment to allow bulk removal of overburden. Feasibility Study level mining studies are currently in progress.

JORC Code, 2012 Edition – Table 1 Ambassador Resource (June 2016)

Material discussed in Sections 1 and 2 below refer primarily to 2015-2016 drilling. Sections relevant to historical datasets have been addressed in past releases to the ASX, in particular that dated 20 April 2015.

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	• The sampling method of drill-cuttings was determined by the location of the sample relative to the weathering front. • Samples from a few metres above the weathering front were recovered directly from the cyclone into plastic bags. The bags were labelled, then left open for a few weeks for the sample to dry. Samples were taken at half metre intervals from a few metres above the weathering front to several metres below the uranium mineralised zone. Sampling then reverted to 1m samples until EOH. • Half core sampling was used for diamond drill holes. Due to the soft and friable nature of the mineralised zones the core was frozen prior to cutting using a diamond saw to prevent core from breaking up. • Downhole logging of natural gamma was used to determine an equivalent U_3O_8 grade, using gamma probes calibrated for uranium on 5 August 2015 at the South Australian Government's Department of Water, Land and Biodiversity Conservation calibration facility (test pits and related facilities) in the Adelaide suburb of Frewville. Wireline density probes used to measure in-situ bulk density were also calibrated at the same facilities at the time. Daily calibrations on the gamma tools were carried out using a Cs^{137} jig, with additional calibrations run through a calibration bore at Mulga Rock during the drilling program.
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• The drilling program at Ambassador West, North and South comprised both aircore and diamond core techniques. • A range of aircore drill bits was used, to deal with varying formation hardness, ranging from tungsten carbide blades arranged around an opening in the face of the bit to bits fitted with PCD buttons. • The diamond drilling was completed using the triple tube method, which comprises outer PQ3 diameter (~122mm) drill rods and an internal core orientation was not attempted due to the vertical drilling and the friable nature of the material.

Criteria	JORC Code explanation	Commentary
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• Recovery of air-core samples can be uneven due to the variable density, moisture, clay and organic matter content of the sediments intersected. Sample flow from the cyclone is continually monitored, and drilling suspended and sample scraped out of the cyclone where adhesion is evident. • Zones of diamond drilling core loss were recorded. Where the location of the loss was known it was recorded as a separate interval. Otherwise the recovery was recorded for the drill run. Overall recovery in diamond drill holes within the mineralised zones has been good with losses occurring predominantly in loose sands, either low in grade or barren. • Evaluation of gamma log equivalent U_3O_8 grade in areas of core loss allowed the grade bias due to core loss to be assessed on a hole by hole basis.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Lithological logging of drill samples was carried out to record main lithological, sedimentological, weathering, colour, and redox features. Stratigraphy is also tentatively assigned while drilling and revised following re-logging. The stratigraphic boundaries determined from these graphic logs and associated cross-sections were used to model deposit geology and to delimit the ore bodies. • Diamond core was logged and photographed prior to cutting.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	**Site Based Work** • Selection of sample composites for chemical analysis was carried out using a combination of lithological data, down-hole gamma and the portable XRF data. • After drying, the bagged samples over the mineralised zone were weighed then split using a single tier riffle splitter. Duplicates were taken as a 50% riffle split from the original sample. • Samples were dispatched and transported to the assay laboratory in steel drums and in accordance with conditions specified in the Company's Radiation Management Plan. • Diamond core sample intervals were determined based on drill runs and geological information. **Laboratory Based Work** • Following sorting and drying at the laboratory, samples were crushed to 3mm, split to produce a 2.2kg fraction and pulverised to 75microns. A small mass of the pulverised sample was then split for assay, with the coarse fraction and pulverised residue also preserved.

Criteria	JORC Code explanation	Commentary
		• Samples from the main mineralised interval were submitted and analysed for uranium and a range of trace and major elements via fused bead laser ablation, using a combination of atomic emission spectroscopy (ICP-AES) and mass spectroscopy (ICP-MS). The sample was fused with a 12:22 lithium borate flux including 5% $LiNO_3$.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	**QA/QC of Assay Samples** • A comprehensive QA/QC program was carried out, comprising the use of in-house and external standards, field and laboratory duplicates, and external pulp duplicates (umpire assays). • The in-house standards were manufactured and certified by Geostats Pty Ltd in 2010 using Mulga Rock composites generated from 2009 drill cuttings (matrix matched). Other matrix-matched standards were also used. A 1:20 radio for standards and 1:30 duplicates were included in the samples despatched, while the laboratory also used in-house standards and performed repeats. Field duplicates were selected on the basis of down-hole gamma and portable XRF data (to ensure a meaningful grade range was achieved) and collected in the same manner as the original sample.
Discussion of relative accuracy/ confidence		• A number of diamond twin holes have been completed to determine whether (if any) sample bias is occurring between aircore and diamond drilling, with analysis on-going.
Portable XRF Logging		• All drill cuttings were analysed by portable XRF through ~50 micron plastic bags on site to guide future drilling and for sample compositing purposes. The portable XRF data is not used directly for any purpose other than determining mineralised zones for sampling, and grade variability. Portable XRF data is not used in Resource estimation.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• The depth of down hole gamma data was checked for discrepancy between the recorded total hole depth and maximum depth of gamma logging. The difference was less than 1m on average. • Correlation of core assay data and probe derived equivalent U_3O_8 grade is used to determine a radiometric disequilibrium correction.

Criteria	JORC Code explanation	Commentary
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• All drill holes were surveyed using a Differential Global Positioning System in Real-Time Kinematics (RTK) mode, with a sub decimetre horizontal resolution. The MGA94, zone 51 grid system was used. • Azimuth and inclination data from wireline tools were used in to calculate the approximate deviation of each drillhole.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Drill spacing is at a nominal 100 x 80m along WNW-ESE trending traverses. • Sample compositing was used occasionally outside of the mineralised zones.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Drilling to-date has also adequately tested the tabular nature of the mineralisation at Ambassador. However, it is possible that steeply-dipping structures may control the distribution of zones of high grade and thickness bodies of uranium mineralisation in sands underlying the upper mineralised lens (by controlling the upward and lateral migration of hydrogen sulphide). These may require angled drilling for full evaluation. • Aircore and diamond were consistently drilled at least 6m past the base of uranium mineralisation to allow for effective wireline logging of mineralised intervals.
Sample security	• *The measures taken to ensure sample security.*	• Samples are sealed in a drum and transported by transport contractor from Kalgoorlie to the assay laboratory, with full chain of custody maintained throughout transport.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• Coffey Mining Consultants have conducted an audit of drilling and sampling processes, confirming the reliability of the procedures described above. • AMC Consultants have similarly reviewed the drilling and sampling processes.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• The Ambassador Deposit is located about 240 km ENE of Kalgoorlie within Mining Lease M39/1080, held by Narnoo Mining Pty Ltd, a wholly owned subsidiary of Vimy Resources Limited (Vimy). • Mining Lease M39/1080 is located on Vacant Crown Land and is not subject to a native title claim.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• The area of the Ambassador Deposit was subject to uranium exploration by PNC Exploration Australia Pty Ltd (PNC) during the 1980's, which resulted in the discovery of the Mulga Rock Deposits. The bulk of PNC's exploration effort was focused on the Ambassador and the eastern side of the Mulga Rock Project between 1982 and 1985. • A trial mining program took place within the Shogun deposit in late 1983 to obtain a bulk sample of mineralised lignite. • During 2008 and 2009, Vimy carried out a twin drill hole program followed by an extensive infill drilling and sampling program, with statistics as follows: o 417 aircore drillholes for 27,144m o 27 diamond drillholes for 1,693m o 5 sonic drillholes for 306m. • During 2014, Vimy carried a further twin and resource drill-out program (primarily at Ambassador East, with a number of diamond tails drilled at Princess), as follows: o 144 aircore drill holes for a total of 9,461m o 42 diamond drill holes for 2,589m • In 2015, Vimy carried out an additional infill drill-out program, primarily focused on Ambassador West, for the following totals: o 1,035 aircore drillholes for 64,425m o 144 reverse circulation drillholes for 9,881m • The complete dataset used for resource estimation purpose was on the following combined number of drill holes and metres: o 1,035 aircore drillholes for 64,425m o 144 reverse circulation drillholes for 9,881m o 5 sonic drillholes for 265m o 279 diamond drillholes for 15,015m o A total of 1,471 drillholes and 90,025m.

Criteria	JORC Code explanation	Commentary
Geology	• *Deposit type, geological setting and style of mineralisation.*	• Ambassador is a sediment-hosted uranium resource. The mineralisation that comprises the Ambassador resource is hosted by reduced Late Eocene sediments preserved within the Narnoo Basin. The Narnoo Basin Sequence consists of multiple fining upwards packages including sandstone, claystone (typically carbonaceous) and lignite which were deposited in alluvial and lacustrine environments. The mineralisation is hosted by reduced sediments of Eocene age preserved within a complex set of sedimentary troughs overlying an extensive long-lived paleodrainage referred to as the Mulga Rock paleochannel, itself likely to represent a dead arm of the Lake Reside regional paleodrainage. • Overlying the Narnoo Basin Sequence is a succession of oxidised sediments which at Ambassador are about 35 to 55m thick. Pre-Eocene basement in the Ambassador area consists of both Cretaceous and Carboniferous sedimentary successions, as well as Paleoproterozoic metasediments to the east of the Gunbarrel fault.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* o *easting and northing of the drill hole collar* o *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* o *dip and azimuth of the hole* o *down hole length and interception depth* o *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• All relevant drill hole collar data pertaining to this release is provided in the table attached to this announcement. • The dip and azimuth of drill holes are not included in the tables appended to this announcement given that all holes were drilled vertically and the shallowness of the drilling and mineralised intervals.

Criteria	JORC Code explanation	Commentary
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• For the purpose of this estimate, the minimum intercept used was 0.5m or greater above 100ppm eU_3O_8 (0.01%eU_3O_8), with a maximum 2m waste length (with grades lower than 100ppm eU_3O_8). The value of 100ppm was chosen as it represents a natural break in the assay data. • All uranium assays within the mineralised zones were composited initially to 0.5m for statistical analyses and estimation. Following application of high grade cuts to the 0.5m composite data, the uranium data were re-composited to full-zone width, variable length composites for Domains 100 and 200 for use in the Accumulation Method estimate applicable to those relatively narrow mineralised zones. Other zones and metals utilised the 0.5m composites. • All composites for base metals were prepared on a 0.5m basis, following a statistical analysis. • Mineralised zones for base and other metals were defined using a grade threshold boundary for each element, with the following grades applied to manage subsequent estimations: o Ni: 300ppm o Co: 100ppm o Zn: 1,500ppm o Cu: 100ppm
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	• Mineralisation is tabular in habit and horizontal. The vertical drill hole intersections represent true mineralisation thickness. • While studies are currently in progress, it is apparent that the downhole probes used to measure the eU_3O_8 data in the aircore holes tend to provide slightly exaggerated thicknesses at lower grades (after disequilibrium corrections) for similar contained metal compared to corresponding twin diamond drillholes with chemical assays. This is considered to be due to the increased "window" and relative sample support for the probe data, particularly in low density material typical of the Domain 100 and 200 mineralisation. The difference in contained metal for the different analyses is not currently found to be significant.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• Four representative cross sections and a plan view of all drill collars are provided in the main text.

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td>Balanced reporting</td><td>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</td><td>The drilling program underpinning this mineral resource update infills a previously defined resource envelope and chemical grades and intercepts are consistent with earlier results.</td></tr>
<tr><td>Other substantive exploration data</td><td>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</td><td>Radiometric disequilibrium
In order to quantify the disequilibrium corrections required for the Ambassador resource update, all suitable diamond drill holes with both assay and radiometric data available in these areas have been compiled and examined. There are several vintages and types of diamond drill hole data available in these areas, including:
Original PNC diamond drill holes (CD series), drilled between 1979 and 1988, using original assay data and radiometric data derived from digitised paper logs.
Original PNC diamond drill holes (CD series), drilled between 1979 and 1988, which were re-entered and re-logged with modern gamma tools in 2008. Original assay data was used, and deconvolved eU_3O_8 calculated using the modern gamma logs.
A limited number of diamond holes completed by Vimy in 2008-2009 (NND series). Original assay and deconvolved eU_3O_8 calculated from gamma are available for these holes.
The diamond drill holes (37) completed as part of the 2014 Ambassador East and 52 completed in the 2015 Ambassador West infill programs by Vimy. Original assay and deconvolved eU_3O_8 calculated from gamma are available for these holes.
Suitable diamond data was divided up based on the new mineralised domains, and the assay data that occurred within these domains was composited to 50cm (with a 20cm tolerance). The average e U_3O_8 value over the same interval (using depth shifted radiometric data where appropriate) was then calculated so it could be compared to the assay data. There are four domains within the Ambassador deposits (Domain 100, Domain 200, Domain 300 and Domain 400) which contain a mixture of the old and new data described above. The domains were further subdivided into Ambassador East (AE), Ambassador West (AW), and Ambassador Northeast (ANE) areas for analysis.
In order to obtain the most accurate estimate of disequilibrium, each of these four domains was first split into groups (based on the data type/vintage) and then split further into distinct grade bins. These grade bins were determined based on apparent “natural breaks” in the dataset.</td></tr>
</table>

Criteria	JORC Code explanation	Commentary
		• Polynomials were derived from Q-Q plots that provided the best fit to the data, for particular grade ranges, with the adjusted radiometric dataset checked graphically and through residual mean squares to ensure that the curve was forced through the point of original and high correlation (R^2) were achieved. Excellent results were achieved using that method, with lower correlations associated with data-poor domains (typically 200, 300 and 400). Data from these three domains was aggregated for the purpose of disequilibrium analysis. • In order to validate the disequilibrium adjustments on a global level, the various datasets have been recombined according to domain and analysed statistically. When compared to the raw eU_3O_8 dataset, the disequilibrium corrected data is significantly closer statistically to the assay-derived U_3O_8 data. • For all four domains estimated, there is a very good correlation between the U_3O_8 and the factored eU_3O_8 datasets.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Additional work is planned to: o Derive factors for equivalent grade determination more relevant to high porosity/low bulk density sediments commonly encountered in the Mulga Rock Project ore zones. o Accurately measure moisture values for different ore types and insitu bulk densities. o Relate the density data to logged lithologies for use in composite data analysis. o Refine base metal domains. o Generate additional infill and extension drilling in the Ambassador South area. • Generate a pattern of very close spaced drilling for evaluation of short range variability of the mineralisation, evaluation of drilling and grade control spacing and different hole types and data types.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	• The resource estimation was based on both the available historical exploration and more recent drillhole database. Data is managed by Vimy in a Datashed database system. • Vimy has assumed responsibility for the validity of the drill hole data and geology. • The database was reviewed and validation checks were completed prior to commencing the resource estimation study. • Changes that were made to the database prior to loading into mining software included: o Replacing less than detection samples with a value equal to half the detection level o Identifying intervals with no samples/assays/radiometric data and setting appropriate bespoke priorities for those intervals. • The deconvolved radiometric eU_3O_8 grades (prior to disequilibrium factoring) were composited to 0.5m intervals in conjunction with the assay data to make processing, comparison and modelling more efficient. • A final table of ranked assays data was used for the resource estimation with priority placed on: o Diamond drilling with chemical data, then o Disequilibrium factored radiometric grades. • For base and other metal (BOM) data, analyses have been collected since 2009 aircore and diamond drilling program. Validation and conversions for modelling purposes would have followed similar procedures as outlined above for U_3O_8 apart from the fact that chemical assay data was used for all BOM estimates.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	• Ingvar Kirchner (Coffey Mining; now AMC Consultants) visited site in November 2014, while Ellen Maidens, Vimy Resources estimation geologist, visited site in November 2015. • Several other people employed by Coffey Mining visited site during 2010 and 2012. • Xavier Moreau undertook multiple site visits during the 2015 to 2016 drilling programs and during the sampling phase.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	• Geology (lithology) was not modelled, but was used in defining the mineralised zones. • Stratigraphy was modelled, and influences the limits of the interpreted mineralised zones. • Diamond drilling has improved the geological understanding of the deposit. Previously the interpretation was complicated by the overprint of oxidation/lithology and stratigraphy. A simplified stratigraphic interpretation has been completed and is the basis for mineralised domain definition. • The deposit grades are very closely associated with the reduction-oxidation front and are concentrated close to this sub-horizontal boundary.

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td></td><td>For the purpose of the resource estimation, the mineralisation boundaries were based on a lithological logging and a nominal 100ppm U_3O_8 lower cut-off defining a mineralised zone of at least 0.5m thickness and honouring, where possible, the geology/stratigraphy. This value was chosen as it represents a natural break in the distribution of grades distinguishing mineralisation from un-mineralised material. Four uranium mineralised zones were defined for the Ambassador deposit defining progressively deeper and lower grade mineralisation—Domains 100, 200, 300, and 400. The domains were further subdivided into Ambassador East (AE), and Ambassador West (AW) for estimation purposes.
The BOM zones were modelled using Leapfrog for each element using the following lower cut-off grades:
Cu—100ppm
Co—100ppm
Ni—300ppm
Zn—1500ppm
Resultant BOM interpretations were sub-horizontal and partly coincident with portions of the uranium mineralised zones. Each of the BOM elements was interpreted independently. BOM grades were also estimated for background material.</td></tr>
<tr><td>Dimensions</td><td>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</td><td>The block model is not rotated.
The block model extents are tabulated below:
<table>
<tr><th colspan="4">Mulga Rock Uranium Deposits – Ambassador Prospect
June 2016 Block Model Construction Parameters</th></tr>
<tr><th></th><th>Origin
(m)</th><th>Extent
(m)</th><th>Parent/Sub Block
Size (m)</th></tr>
<tr><td>Easting</td><td>573000</td><td>10500</td><td>50/10</td></tr>
<tr><td>Northing</td><td>6676000</td><td>9000</td><td>50/10</td></tr>
<tr><td>Elevation</td><td>230</td><td>170</td><td>10/0.25</td></tr>
</table></td></tr>
<tr><td>Estimation and modelling techniques</td><td>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.
The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</td><td>Vimy, under the supervision of AMC Consultants, has estimated the Mineral Resource for the Ambassador deposit as at June 2016.
U_3O_8 grade estimation was completed using a combination of accumulation process involving Ordinary Kriging (OK) for the thin high grade upper mineralised zones and normal OK for the lower mineralised zones.
Base and other metals (BOM) were also estimated using OK in domains unique to each of the elements.
The estimation was appropriately constrained with geological mineralisation interpretations and sub-domains.</td></tr>
</table>

Criteria	JORC Code explanation	Commentary
	• *The assumptions made regarding recovery of by-products.* • *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulfur for acid mine drainage characterisation).* • *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* • *Any assumptions behind modelling of selective mining units.* • *Any assumptions about correlation between variables.* • *Description of how the geological interpretation was used to control the resource estimates.* • *Discussion of basis for using or not using grade cutting or capping.* • *The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.*	• In the majority of cases at Ambassador and Princess, the radiometric e U_3O_8 grades for similar intervals are lower than the corresponding chemical assays for U_3O_8, requiring positive adjustments to the radiometric data to emulate the accurate chemical assay data. Data for each of the four uranium domains and corresponding area subdomains were split into groups (based on the data type/vintage) and then further split into distinct grade bins. These grade bins were determined based on apparent natural breaks in the dataset identified in Q-Q plots and statistics. Specifically, disequilibrium corrections (regression formulae for the Q-Q data) were derived for: o Domain 100 PNC data where eU_3O_8 data was derived from digitised logs o Domain 100 PNC data where the holes were re-logged in 2008 o Domain 100 Vimy data, sub-domains AE, for holes drilled from 2008 to 2014. o Domain 100 Vimy data, sub-domains ANE, AE, and AW, for holes drilled from 2015 to 2016. o Domain 200 Vimy data, sub-domains AE and AW, for holes drilled from 2015 to 2016. o Combined lower uranium Domains 200, 300, and 400 Vimy data for holes drilled from 2008 to 2014. o Any radiometric data below eU_3O_8 =100ppm within the uranium domains were not corrected for disequilibrium. • All samples within the mineralised wireframes were composited to 0.5m samples. • High grade cuts were applied to the e U_3O_8d 0.5m composite data for the various uranium domains and sub-domains. Similarly, high grade cuts were applied to the composite data for the BOM elements. • The resource estimates for the BOM elements are based on chemical assay data only. • The Accumulation Method OK and normal OK estimates were completed using grade variogram models and a set of ancillary parameters controlling the source and selection of composite data from the domains and sub-domains. The sample search parameters were defined based on the estimation methods, variography and the data spacing. • A two pass search strategy with hard boundaries was used for the domains 100, 200, 300 and 400 and corresponding sub-domains AE and AW. • A single pass search strategy with hard boundaries was used for the BOM domains and corresponding sub-domains AE and AW. • Mining is currently planned to be by shallow open pit cut and fill mining. Details are currently the subject of an updated Feasibility Study. • Mining is expected to be more selective than the current drill spacing and supported block estimation size. • Block estimates were visually compared to the input composite samples in section views. Global average grades for estimates and declustered composite mean grades show a good correspondence.

Criteria	JORC Code explanation	Commentary
		• Mining has not commenced so no reconciliation data is available for the deposit. • No assumptions were made concerning recovery of by-products. • No known deleterious elements were estimated. • The block size of 50m x 50m x 10m is considered appropriate given the drillhole spacing, • No assumptions have been made regarding SMU. • The 2016 Ambassador Mineral Resource has changed from the previous Resource primarily due to the following items: o Increased area due to extension drilling (ANE) o Increased drill spacing and diamond drilling density due to infill drilling primarily within the western portion of the Ambassador mineral resource (AW). o Changes to interpretations related to infill drilling and improved geological knowledge. Some of the domains have decreased slightly in volume while others have increased. o Changes to bulk density values applied and method of applying the densities according to estimated dominant lithologies. Bulk densities for some domains will have increased slightly on average, while others will have decreased. o Improved disequilibrium factors generated from recent DC holes and twin holes, primarily in the Ambassador West area. The disequilibrium studies have been thorough in distinguishing the various radiometric data types, tools, and domains. The purpose of the disequilibrium factors applied to the various data and domains is to get the consistently low biased eU_3O_8 radiometric data to be statistically comparable to the "umpire/correct" chemical assay data. It is anticipated that the disequilibrium factors will continue to change with additional data. However, the current factors are expected to be unchanged on an order of magnitude basis. • The revised 2016 Mineral Resource has increased by approximately 3% in terms of contained U_3O_8 metal compared to the September 2015 estimate.
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages and metal are reported on a dry basis, requiring a dry insitu bulk density. Wet density and moisture are also estimated in the block model for mining studies and metallurgical purposes.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The nominal 100ppm U_3O_8 lower cut-off used to define the mineralisation was chosen as it represents a natural break in the assay data. • A cut-off grade of 150ppm U_3O_8 is currently applied for reporting purposes assuming open-pit mining methods. Mining studies are currently in progress. • The BOM tonnages are reported only for the portions of the BOM zones that are coincident with reportable portions of the uranium mineralised zones above cut-off grade. The BOM elements are only considered here to be potential by-products from the uranium processing, and are not likely to be individually economic commodities.

Criteria	JORC Code explanation	Commentary
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• Relatively shallow open pit mining, incorporating in-pit waste and tailings disposal is assumed for the bulk of the deposit. • No recovery factor has been applied to either the U_3O_8 or the BOM elements in this estimate.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	• No factors have been applied regarding metallurgy. • At Ambassador, spectral, mineralogical, deportment and metallurgical studies show that the bulk of the uranium is in a hexavalent ionic state and adsorbed onto organic matter, with a negligible fraction contained in refractory minerals. • Recent test-work at Ambassador has shown potential recoveries greater than 90% for both lignite and sandstone-hosted mineralised material, using an atmospheric acid leach (tested in a resin-in-pulp configuration).
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• The November 2015 Pre-Feasibility Study identified that the most effective management of overburden storage would be to employ strip mining with the majority of waste placed in the mining void as the pit advances. This would minimise the size of above ground overburden storage areas. • The Mulga Rock Project Public Environmental Review (PER) document was lodged and accepted for public comment by the EPA on 12 November 2015. The public comment period closed on 8 March 2016. The Project will continue to progress through the regulatory approval process with the necessary lead agencies.

Criteria	JORC Code explanation	Commentary
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	• Bulk density has been determined by using both gamma downhole geophysical logging of diamond drill holes in the Ambassador deposit and Archimedean data from core samples. • The Archimedean density measurements have been used to validate and correct the downhole geophysical data where applicable. Downhole gamma data has been used selectively where issues have been identified. • Dry bulk density values were determined by converting the geophysical density with moisture values for the corresponding lithology and mineralised domain type. • A probability based lithological model has been used to assign variable bulk density values to the block model. • Density values assigned to the Ambassador deposit are consistent with density of similar materials for other deposits in the area.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	• The Mineralised Resource has been classified as a combination of Indicated and Inferred material, in accordance with JORC Code 2012 guidelines based on the confidence levels of the key criteria considered during the resource estimation such as data quality, drilling density, and apparent grade and/or spatial continuity of the mineralisation. • The resource classification for Ambassador is applied to the BOM elements as well as the uranium. The current estimates for the BOM elements are considered to be less precise than for the uranium, but, as reported, are still within the realms of an Indicated and Inferred Resource categories. The BOM elements are considered to be strictly by-products from the metallurgical processing.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• AMC have audited the 2016 Ambassador Mineral Resource model and determined that the model is fit for purpose.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.*	• The resource classification represents the relative confidence in the resource estimate as determined by the Competent Person. Issues contributing to or detracting from that confidence are discussed above. • No quantitative approach has been conducted to determine the relative accuracy of the resource estimate. • The Ordinary Kriged estimate is considered to be a global estimate with no further adjustments for Selective Mining Unit (SMU) dimensions. Accurate mining scenarios are yet to be determined by feasibility type studies. • No production data is available for comparison to the estimate. • The local accuracy of the resource is adequate for the expected use of the model in the pre-feasibility study. • Due to the nature of the uranium mineralisation, the degree of radiochemical disequilibrium is likely to vary considerably between drillholes and with depth down each drillhole. The disequilibrium factoring applied for the 2016 resource estimate has resulted in satisfactory global results but local variations are expected.

Criteria	JORC Code explanation	Commentary
	• *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• Diamond drilling has improved the geological, physical property (density and moisture) and disequilibrium adjustment confidence in the Ambassador deposit. • Further investigation into bulk density determination, radioactive disequilibrium (both vertical and lateral) and infill drilling will be required to raise the level of resource classification further.

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
AC1012	574401.90	6679326.14	338.7	104.5	AC
AC1014	575870.33	6678695.79	329.3	80.5	AC
AC1016	576239.58	6677329.68	341.1	92.5	AC
AC1020	577198.97	6678621.62	333.9	62.5	AC
AC1021	576323.86	6679143.69	327.1	56.5	AC
AC1022	575396.71	6679695.66	323.9	56.5	AC
AC1023	574534.48	6680210.05	330.0	61.0	AC
AC1024	575893.95	6679399.01	318.1	71.5	AC
AC1025	575488.12	6680104.58	322.2	108.0	AC
AC1027	574823.29	6681029.87	327.4	56.5	AC
AC1029	575485.81	6682116.97	329.1	72.0	AC
AC1031	577224.95	6681050.31	333.4	38.5	AC
AC1032	578076.01	6680542.58	346.2	44.5	AC
AC1035	576906.80	6682700.97	340.5	90.0	AC
AC1036	578004.65	6682046.89	346.7	124.5	AC
AC1224	579429.46	6681784.56	341.6	77.0	AC
AC1226	575343.64	6681710.10	327.8	71.0	AC
AC1227	576930.07	6679979.18	329.2	35.0	AC
AC1228	577190.37	6679608.44	329.0	59.0	AC
AC1230	579695.97	6681514.95	343.0	45.0	AC
AC1231	579725.19	6683125.42	333.1	32.0	AC
AC1232	579769.23	6683072.36	329.1	71.0	AC
AC1233	580108.22	6682893.49	331.9	95.2	AC
AC1234	580443.85	6682688.52	342.9	46.2	AC
AC1235	580793.13	6682512.75	341.5	41.3	AC
AC1236	579440.32	6683268.59	335.4	40.1	AC
AC1237	580755.28	6683258.48	332.1	95.0	AC
AC1238	581086.08	6683050.64	337.0	41.3	AC
NBSP04	580137.00	6682875.00	332.4	51.0	AC
NBSP05	578668.00	6682609.00	334.8	54.0	AC
NBSP06	579057.15	6682858.57	339.1	69.0	AC
NBSP07	577049.33	6682609.87	342.2	57.0	AC
NBSP08	576233.00	6682121.00	332.0	51.0	AC

Hole ID	Easting	Northing	RL	Depth	Type [1]
NN0034	576316.95	6683535.49	335.0	78.0	AC
NN0035	576269.52	6684525.62	342.2	66.0	AC
NN0036	576605.01	6684309.17	340.1	68.0	AC
NN0037	576851.86	6684149.09	335.4	90.0	AC
NN0053	575018.16	6682377.33	336.4	45.0	AC
NN0054	575185.11	6682276.56	333.9	41.0	AC
NN0055	575350.04	6682160.71	331.0	66.0	AC
NN0056	575386.77	6681195.58	326.0	81.0	AC
NN0057	574532.93	6681714.29	336.6	51.0	AC
NN0058	574688.94	6681599.09	334.7	44.0	AC
NN0059	575023.24	6681378.70	327.5	71.0	AC
NN0060	574855.58	6681488.03	331.9	50.0	AC
NN0061	575204.78	6681275.05	326.0	99.0	AC
NN0102	575109.28	6681329.69	326.3	99.0	AC
NNA5021	575160.00	6680827.00	324.6	94.0	AC
NNA5022	576041.42	6681754.54	330.0	69.0	AC
NNA5023	576148.26	6681690.10	330.2	69.0	AC
NNA5024	578558.56	6682437.73	334.7	69.0	AC
NNA5085	578669.58	6682378.83	337.5	75.0	AC
NNA5086	579150.00	6682822.00	339.7	82.0	AC
NNA5087	579138.00	6682817.00	339.5	78.0	AC
NNA5088	576062.33	6681749.62	330.0	81.0	AC
NNA5089	576053.56	6681754.53	330.0	75.0	AC
NNA5090	576043.00	6681762.00	330.0	81.0	AC
NNA5091	576117.19	6681718.41	330.1	81.0	AC
NNA5092	576184.67	6681675.34	330.2	66.0	AC
NNA5093	576250.15	6681627.59	330.5	81.0	AC
NNA5094	576322.92	6681592.90	331.4	75.0	AC
NNA5095	575977.38	6681798.57	329.9	75.0	AC
NNA5096	575909.84	6681839.20	329.9	78.0	AC
NNA5097	575842.58	6681879.41	330.0	75.0	AC
NNA5098	575774.82	6681913.89	330.1	63.0	AC
NNA5099	575491.42	6682104.24	329.0	75.0	AC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5100	575948.26	6681571.49	329.0	75.0	AC
NNA5101	576016.19	6681529.51	329.0	56.0	AC
NNA5102	576087.68	6681490.24	328.9	64.0	AC
NNA5103	576152.68	6681450.07	328.9	75.0	AC
NNA5104	575881.67	6681620.10	329.2	75.0	AC
NNA5105	575812.08	6681662.49	329.6	75.0	AC
NNA5106	575743.96	6681698.56	329.9	69.0	AC
NNA5107	575856.02	6681409.61	328.8	78.0	AC
NNA5108	575924.30	6681368.52	328.9	72.0	AC
NNA5109	575995.37	6681325.80	328.8	61.0	AC
NNA5110	576062.93	6681285.82	328.1	72.0	AC
NNA5111	576130.61	6681244.57	327.6	70.0	AC
NNA5112	576198.90	6681203.96	327.3	57.0	AC
NNA5113	575787.50	6681450.26	328.9	78.0	AC
NNA5114	575716.71	6681492.47	328.9	69.0	AC
NNA5115	575648.07	6681533.52	328.7	75.0	AC
NNA5116	575744.51	6681274.71	330.3	78.0	AC
NNA5117	575801.62	6681231.55	330.1	69.0	AC
NNA5118	575878.40	6681189.62	328.8	69.0	AC
NNA5119	575953.29	6681143.57	328.0	66.0	AC
NNA5120	575669.83	6681319.86	329.8	78.0	AC
NNA5121	575605.94	6681360.67	328.8	81.0	AC
NNA5122	575525.76	6681393.43	327.9	78.0	AC
NNA5123	575587.06	6681099.76	327.1	50.0	AC
NNA5124	575649.91	6681062.89	328.0	78.0	AC
NNA5125	575719.71	6681027.76	329.2	69.0	AC
NNA5126	575791.55	6680984.54	330.7	75.0	AC
NNA5127	575520.92	6681139.51	326.0	72.0	AC
NNA5128	575444.67	6681192.34	325.9	81.0	AC
NNA5129	575676.82	6680784.16	327.1	69.0	AC
NNA5130	575743.90	6680743.65	327.3	66.0	AC
NNA5131	575603.46	6680821.13	326.9	66.0	AC
NNA5132	575538.61	6680860.87	326.7	65.0	AC
NNA5133	575400.85	6680686.89	326.0	52.5	AC

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5134	575333.37	6680726.89	324.6	75.0	AC
NNA5135	575265.68	6680766.20	324.2	81.0	AC
NNA5136	575804.04	6682138.17	330.3	60.0	AC
NNA5137	575880.36	6682098.61	331.3	57.0	AC
NNA5138	575731.47	6682188.83	329.8	54.0	AC
NNA5139	575672.50	6682223.06	329.0	45.0	AC
NNA5140	575383.91	6680443.92	324.3	81.0	AC
NNA5141	575320.78	6680490.92	322.7	63.0	AC
NNA5142	575249.59	6680533.04	321.7	48.5	AC
NNA5143	575469.36	6680124.91	322.0	78.0	AC
NNA5144	575405.64	6680161.92	321.5	78.0	AC
NNA5145	575264.15	6680238.97	321.0	66.0	AC
NNA5146	575132.87	6680325.05	322.1	72.0	AC
NNA5147	574987.15	6680404.06	325.0	81.0	AC
NNA5148	575538.90	6680075.94	322.6	75.0	AC
NNA5149	575678.21	6680000.47	322.0	66.0	AC
NNA5150	575527.38	6680358.92	327.5	84.0	AC
NNA5151	575661.19	6680289.06	328.1	75.0	AC
NNA5152	575796.51	6680198.42	324.9	66.0	AC
NNA5153	575535.04	6680611.57	329.0	81.0	AC
NNA5154	575669.26	6680526.95	327.2	81.0	AC
NNA5155	575804.53	6680452.87	325.5	81.0	AC
NNA5156	575881.81	6680408.94	325.1	78.0	AC
NNA5157	575806.97	6680695.15	327.3	63.0	AC
NNA5158	575947.19	6680614.72	326.9	57.0	AC
NNA5159	576081.92	6680523.39	327.1	51.0	AC
NNA5160	575401.93	6680952.04	325.8	78.0	AC
NNA5161	575248.78	6681040.83	324.6	81.0	AC
NNA5162	575114.18	6681133.92	325.4	42.0	AC
NNA5163	575191.18	6680812.29	324.1	81.0	AC
NNA5164	575459.76	6680922.68	326.4	49.5	AC
NNA5165	575331.35	6681001.77	324.9	81.0	AC
NNA5166	576014.36	6681096.48	327.4	66.0	AC
NNA5167	576088.77	6681051.29	327.0	63.0	AC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5168	575673.53	6681741.57	329.3	57.0	AC
NNA5169	576014.34	6682018.10	331.8	60.0	AC
NNA5170	576072.27	6681975.88	331.3	63.0	AC
NNA5171	576147.87	6681930.72	329.9	72.0	AC
NNA5172	576216.68	6681890.40	329.6	78.0	AC
NNA5173	575628.74	6682482.32	332.8	46.5	AC
NNA5174	575769.15	6682398.83	330.7	60.0	AC
NNA5175	575905.66	6682318.44	331.3	48.0	AC
NNA5176	576042.13	6682243.79	332.9	57.0	AC
NNA5177	576184.84	6682158.84	332.9	57.0	AC
NNA5178	576216.16	6682140.49	332.4	57.0	AC
NNA5179	576251.36	6682118.98	331.9	57.0	AC
NNA5180	576110.11	6682194.88	333.1	69.0	AC
NNA5181	575673.27	6682699.16	336.1	57.0	AC
NNA5182	575811.65	6682624.85	333.3	51.0	AC
NNA5183	575947.04	6682535.79	331.6	51.0	AC
NNA5184	576085.71	6682461.24	330.6	54.0	AC
NNA5185	576218.45	6682372.38	330.7	57.0	AC
NNA5186	576368.19	6682293.72	330.7	54.0	AC
NNA5187	576291.16	6682338.81	330.9	54.0	AC
NNA5188	576602.18	6682388.23	332.9	66.0	AC
NNA5189	576736.37	6682302.90	332.6	52.0	AC
NNA5190	576884.21	6682228.27	333.7	81.0	AC
NNA5191	576950.91	6682188.38	334.7	66.0	AC
NNA5192	576460.33	6682468.56	331.9	54.0	AC
NNA5193	576534.05	6682436.29	332.6	51.0	AC
NNA5194	576681.90	6682348.95	332.3	53.0	AC
NNA5195	576812.39	6682270.46	332.8	78.0	AC
NNA5196	576716.60	6682572.37	334.8	57.0	AC
NNA5197	576852.52	6682485.55	335.6	54.0	AC
NNA5198	575538.78	6682048.38	329.0	75.0	AC
NNA5199	578636.13	6682399.20	336.1	69.0	AC
NNA5200	578613.65	6682404.91	336.2	78.0	AC
NNA5201	578623.35	6682398.33	336.1	75.0	AC
NNA5202	579156.00	6682806.00	339.8	81.0	AC
NNA5203	579109.31	6682835.68	339.3	81.0	AC
NNA5204	579146.08	6682814.13	339.8	81.0	AC
NNA5205	576922.75	6682448.58	332.8	51.0	AC
NNA5206	576987.46	6682410.68	330.0	47.5	AC
NNA5207	577128.72	6682327.33	332.6	69.0	AC
NNA5208	577192.30	6682286.96	333.8	60.0	AC
NNA5209	577232.24	6682509.95	334.8	68.0	AC
NNA5210	577308.43	6682464.05	334.7	66.0	AC
NNA5211	577374.17	6682425.13	333.9	54.0	AC
NNA5212	577442.14	6682388.80	334.6	51.0	AC
NNA5213	577173.75	6682538.83	335.3	69.0	AC
NNA5214	577099.47	6682590.90	341.3	57.0	AC
NNA5215	577027.34	6682624.75	342.3	73.0	AC
NNA5216	576962.95	6682671.86	341.9	65.0	AC
NNA5217	576821.47	6682755.36	338.1	63.0	AC
NNA5218	577074.22	6682833.18	332.9	60.0	AC
NNA5219	577143.68	6682792.25	332.1	63.0	AC
NNA5220	577209.70	6682753.99	332.6	57.0	AC
NNA5221	576270.95	6681161.78	326.8	63.0	AC
NNA5222	576337.43	6681122.87	326.3	57.0	AC
NNA5223	576407.20	6681079.87	326.0	51.0	AC
NNA5224	576470.72	6681041.67	326.3	36.0	AC
NNA5225	576542.57	6680999.35	326.7	33.0	AC
NNA5226	576154.79	6681008.89	326.9	60.0	AC
NNA5227	576236.48	6680966.78	327.0	49.5	AC
NNA5228	576292.70	6680926.30	327.4	51.0	AC
NNA5229	576367.12	6680885.49	327.8	48.0	AC
NNA5230	576433.73	6680844.14	328.7	45.0	AC
NNA5231	576556.34	6680765.95	329.9	39.0	AC
NNA5232	576492.86	6680799.27	329.4	39.0	AC
NNA5233	575879.06	6680658.17	327.0	81.0	AC
NNA5234	576018.79	6680570.22	327.0	63.0	AC
NNA5235	575003.53	6679931.77	328.1	66.0	AC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5236	574932.79	6679973.55	327.7	55.5	AC
NNA5237	574859.60	6680023.20	328.1	60.0	AC
NNA5238	574792.15	6680063.09	330.5	60.0	AC
NNA5239	574713.96	6680104.40	330.5	75.0	AC
NNA5240	574644.71	6680151.04	329.6	75.0	AC
NNA5241	575525.96	6679627.16	323.0	69.0	AC
NNA5242	575659.34	6679547.69	322.3	69.0	AC
NNA5243	575806.87	6679457.77	318.0	60.0	AC
NNA5244	575934.05	6679383.25	318.6	60.0	AC
NNA5245	575859.00	6680945.58	331.4	63.0	AC
NNA5246	575924.16	6680898.25	331.5	60.0	AC
NNA5247	578599.14	6682904.96	338.9	69.0	AC
NNA5248	578731.18	6682819.10	337.6	51.0	AC
NNA5249	578862.79	6682740.25	338.0	54.0	AC
NNA5250	579004.60	6682663.54	337.7	79.0	AC
NNA5251	578930.15	6682699.12	338.1	63.0	AC
NNA5252	579078.43	6682613.01	336.4	75.0	AC
NNA5253	579142.74	6682575.58	335.9	72.0	AC
NNA5254	579210.79	6682534.49	337.9	78.0	AC
NNA5255	579283.70	6682497.33	338.4	81.0	AC
NNA5256	579320.04	6682709.81	335.5	81.0	AC
NNA5257	579348.16	6682451.49	337.8	93.0	AC
NNA5258	579411.14	6682413.76	336.1	72.0	AC
NNA5259	579484.18	6682377.76	333.4	48.5	AC
NNA5260	579552.04	6682337.85	333.0	48.0	AC
NNA5261	579391.50	6682675.81	333.8	69.0	AC
NNA5262	579463.52	6682632.58	333.1	69.0	AC
NNA5263	579598.63	6682551.32	333.2	64.0	AC
NNA5264	579670.07	6682508.17	333.2	48.0	AC
NNA5265	579735.65	6682460.83	334.0	48.0	AC
NNA5266	579797.13	6682433.13	335.1	38.5	AC
NNA5267	579751.04	6682682.45	332.7	78.0	AC
NNA5268	579825.32	6682636.64	333.1	69.0	AC
NNA5269	579247.54	6682760.70	338.5	81.0	AC

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5270	579181.24	6682793.10	340.0	75.0	AC
NNA5271	579040.45	6682875.52	338.9	72.0	AC
NNA5272	578974.53	6682915.88	339.1	54.0	AC
NNA5273	578914.27	6682951.74	342.0	60.0	AC
NNA5274	579415.82	6682888.15	334.1	67.0	AC
NNA5275	579343.21	6682925.00	336.7	75.0	AC
NNA5276	579807.28	6683065.71	328.7	48.0	AC
NNA5277	579862.07	6683026.55	328.6	60.0	AC
NNA5278	579896.75	6682601.96	333.4	60.0	AC
NNA5279	579966.25	6682560.28	334.8	54.0	AC
NNA5280	580038.93	6682517.17	337.1	48.0	AC
NNA5281	579686.92	6682719.74	332.0	81.0	AC
NNA5282	579613.58	6682770.49	331.7	69.0	AC
NNA5283	579544.20	6682804.40	331.6	65.0	AC
NNA5284	579477.93	6682849.77	332.0	54.0	AC
NNA5285	579795.97	6682891.44	329.9	81.0	AC
NNA5286	580272.78	6682599.17	340.4	48.0	AC
NNA5287	580205.64	6682639.22	337.9	60.0	AC
NNA5288	580120.44	6682689.05	334.4	69.0	AC
NNA5289	579987.77	6682770.10	331.3	81.0	AC
NNA5290	579857.11	6682847.17	330.2	69.0	AC
NNA5291	579946.01	6682986.24	329.6	48.0	AC
NNA5292	579724.00	6682933.00	329.6	81.0	AC
NNA5293	579645.65	6682971.31	329.7	60.0	AC
NNA5294	580001.63	6682949.25	330.5	48.0	AC
NNA5295	580280.00	6683272.00	335.4	72.0	AC
NNA5296	580376.56	6683234.12	335.1	60.0	AC
NNA5297	580451.44	6683190.31	333.9	81.0	AC
NNA5298	580284.70	6683063.66	332.4	81.0	AC
NNA5299	580341.49	6683022.51	334.7	81.0	AC
NNA5300	580082.88	6682911.80	331.5	66.0	AC
NNA5301	580153.40	6682865.75	332.5	84.0	AC
NNA5302	580219.23	6682830.57	333.8	63.0	AC
NNA5303	580292.04	6682790.26	336.2	45.0	AC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5304	579574.98	6682996.64	330.6	54.0	AC
NNA5305	579305.66	6683176.17	345.2	66.0	AC
NNA5306	580517.76	6683160.42	334.3	75.0	AC
NNA5307	580582.18	6683109.40	334.9	78.0	AC
NNA5308	580689.40	6683299.71	332.0	51.0	AC
NNA5309	580830.51	6683223.54	331.8	45.0	AC
NNA5310	580364.99	6682756.80	339.1	48.0	AC
NNA5311	579937.11	6683262.70	331.5	48.0	AC
NNA5312	579997.67	6683226.45	331.0	39.0	AC
NNA5313	580417.19	6682984.72	338.1	81.0	AC
NNA5314	580071.09	6683189.20	330.2	45.0	AC
NNA5315	580152.31	6683141.73	330.4	69.0	AC
NNA5316	580484.06	6682945.26	340.2	51.0	AC
NNA5317	580203.92	6683110.69	330.9	60.0	AC
NNA5318	580627.09	6682858.67	338.9	45.0	AC
NNA5319	579945.85	6682802.11	330.7	72.0	AC
NNA5320	580077.88	6682724.26	333.1	72.0	AC
NNA5321	579933.42	6682697.65	332.1	81.0	AC
NNA5322	579111.96	6682932.36	339.6	70.0	AC
NNA5323	579515.84	6682600.14	332.9	81.0	AC
NNA5324	578795.94	6682780.21	337.8	54.0	AC
NNA5325	578616.10	6682655.85	335.9	51.0	AC
NNA5326	578551.72	6682692.89	336.2	48.0	AC
NNA5327	578481.29	6682735.85	336.2	51.0	AC
NNA5328	579207.95	6682996.16	341.6	81.0	AC
NNA5329	579523.14	6683051.08	332.9	60.0	AC
NNA5330	578859.99	6682842.86	337.4	72.0	AC
NNA5331	578705.76	6682696.97	336.4	75.0	AC
NNA5332	578698.64	6682599.69	334.6	73.0	AC
NNA5333	579283.63	6682959.92	338.4	81.0	AC
NNA5334	578757.00	6682562.00	335.3	75.0	AC
NNA5335	578832.40	6682526.99	337.7	75.0	AC
NNA5336	578905.16	6682483.40	341.2	78.0	AC
NNA5337	579009.62	6682479.49	340.9	78.0	AC

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5338	579077.39	6682456.51	339.4	81.0	AC
NNA5339	578406.61	6682772.59	336.0	45.0	AC
NNA5340	578345.56	6682816.10	335.1	42.0	AC
NNA5341	578278.25	6682855.49	333.9	48.0	AC
NNA5342	579128.18	6682416.11	340.6	78.0	AC
NNA5343	579206.56	6682379.57	341.2	81.0	AC
NNA5344	579270.01	6682337.66	341.0	81.0	AC
NNA5345	579323.80	6682242.56	342.1	66.0	AC
NNA5346	579382.79	6682197.29	341.2	51.0	AC
NNA5347	579231.31	6682518.83	338.3	78.0	AC
NNA5348	577998.40	6683016.84	337.1	69.0	AC
NNA5349	577792.52	6683138.40	340.2	72.0	AC
NNA5350	577722.82	6683180.39	338.3	54.0	AC
NNA5351	577655.69	6683221.42	336.3	81.0	AC
NNA5352	578569.00	6682541.00	334.0	78.0	AC
NNA5353	578138.34	6682939.27	333.4	51.0	AC
NNA5354	578440.00	6682518.00	336.8	57.0	AC
NNA5355	577968.77	6682791.35	334.8	60.0	AC
NNA5356	577820.41	6682885.98	331.9	57.0	AC
NNA5357	577751.19	6682930.42	332.2	57.0	AC
NNA5358	577682.91	6682959.64	333.3	66.0	AC
NNA5359	578376.86	6682547.32	338.9	60.0	AC
NNA5360	578511.41	6682474.38	334.8	78.0	AC
NNA5361	578580.41	6682432.85	334.9	72.0	AC
NNA5362	578926.71	6682226.87	336.8	72.0	AC
NNA5363	577606.43	6682990.90	332.8	81.0	AC
NNA5364	577860.06	6682620.44	335.3	56.5	AC
NNA5365	579004.72	6682180.46	337.1	69.0	AC
NNA5366	579064.93	6682138.14	335.8	63.0	AC
NNA5367	577000.71	6682877.14	333.2	81.0	AC
NNA5368	576646.45	6682615.83	333.4	60.0	AC
NNA5369	577531.04	6682810.07	334.9	63.0	AC
NNA5370	577452.52	6682863.28	333.6	57.0	AC
NNA5371	577395.57	6682897.14	333.4	47.0	AC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5372	577315.24	6682938.30	334.6	81.0	AC
NNA5373	577539.51	6683041.87	338.1	69.0	AC
NNA5374	577406.21	6683115.15	337.2	46.5	AC
NNA5375	577471.39	6683075.91	338.4	49.5	AC
NNA5376	576910.24	6681970.55	331.6	51.0	AC
NNA5377	576845.54	6682008.23	331.0	60.0	AC
NNA5378	576773.87	6682051.00	330.3	69.0	AC
NNA5379	576513.01	6682199.13	330.0	58.0	AC
NNA5380	576427.30	6682256.74	330.3	57.0	AC
NNA5381	576317.98	6682565.65	332.6	60.0	AC
NNA5382	577060.24	6682366.94	330.9	72.0	AC
NNA5383	577265.98	6682246.33	334.9	54.0	AC
NNA5384	576402.89	6682516.84	331.0	54.0	AC
NNA5385	576258.05	6682601.78	331.2	60.0	AC
NNA5386	576935.81	6682916.56	333.9	57.0	AC
NNA5387	576702.20	6682093.27	330.3	72.0	AC
NNA5388	576638.97	6682123.62	330.0	54.0	AC
NNA5389	575360.00	6681918.00	330.8	54.0	AC
NNA5390	576358.47	6681317.06	331.6	66.0	AC
NNA5391	576490.58	6681234.18	333.2	51.0	AC
NNA5392	575611.43	6681787.72	329.1	56.0	AC
NNA5393	575507.91	6681421.05	327.8	81.0	AC
NNA5394	575453.29	6681450.25	326.9	81.0	AC
NNA5395	575379.86	6681494.42	326.0	51.0	AC
NNA5396	575312.36	6681526.94	325.8	45.0	AC
NNA5397	575033.58	6681175.88	325.8	60.0	AC
NNA5398	575458.98	6681875.30	329.7	45.0	AC
NNA5399	575503.26	6681852.60	329.3	48.0	AC
NNA5400	575582.04	6681573.57	328.1	60.0	AC
NNA5401	575492.18	6681613.37	327.1	54.0	AC
NNA5402	575443.94	6681655.43	327.3	51.0	AC
NNA5403	575386.94	6681691.12	327.5	51.0	AC
NNA5404	575377.57	6681225.44	326.0	81.0	AC
NNA5405	575300.20	6681276.38	326.1	72.0	AC
NNA5406	575232.89	6681311.27	326.1	57.0	AC
NNA5407	575164.80	6681357.76	326.4	57.0	AC
NNA5408	575079.90	6681408.73	327.4	48.0	AC
NNA5409	576616.44	6680956.23	327.2	42.0	AC
NNA5410	575046.29	6680905.11	325.0	54.0	AC
NNA5411	574894.33	6680994.69	326.6	54.0	AC
NNA5412	574982.31	6680941.73	325.6	48.0	AC
NNA5413	575958.11	6680355.16	325.1	72.0	AC
NNA5414	576020.26	6680324.77	325.6	63.0	AC
NNA5415	574954.32	6681219.86	327.0	54.0	AC
NNA5416	576128.11	6680493.99	327.2	60.0	AC
NNA5417	576199.47	6680450.79	327.3	57.0	AC
NNA5418	576265.32	6680410.11	326.7	54.0	AC
NNA5419	576345.15	6680365.42	325.8	48.0	AC
NNA5420	575855.59	6680163.00	323.1	56.0	AC
NNA5421	575922.02	6680131.47	322.0	81.0	AC
NNA5422	575997.85	6680085.38	322.0	78.0	AC
NNA5423	576119.46	6680006.44	323.3	51.0	AC
NNA5424	576094.46	6680280.95	326.6	57.0	AC
NNA5425	576173.54	6680235.45	328.2	57.0	AC
NNA5426	576235.42	6680198.08	329.5	51.0	AC
NNA5427	576306.93	6680155.30	330.8	48.0	AC
NNA5428	574560.54	6680195.83	329.8	66.0	AC
NNA5429	574429.33	6680279.45	332.9	64.0	AC
NNA5430	576120.24	6679273.03	321.3	78.0	AC
NNA5431	576568.52	6679005.72	334.5	61.0	AC
NNA5432	577008.40	6678735.76	331.0	81.0	AC
NNA5433	576340.30	6678932.18	329.5	59.0	AC
NNA5434	576269.48	6679918.07	325.5	45.0	AC
NNA5435	575727.34	6679962.24	322.0	63.0	AC
NNA5436	575827.24	6679903.34	322.0	60.0	AC
NNA5437	575920.57	6679856.12	321.1	48.0	AC
NNA5438	575966.49	6679820.06	320.9	75.0	AC
NNA5439	576045.41	6679773.04	320.5	69.0	AC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5440	575502.76	6678676.31	331.5	64.0	AC
NNA5441	575924.23	6678419.81	329.4	78.0	AC
NNA5442	576490.18	6678090.00	326.7	78.0	AC
NNA5443	577235.30	6679071.43	331.2	54.0	AC
NNA5444	576740.00	6679358.98	330.2	60.0	AC
NNA5445	576389.00	6679568.95	325.3	57.0	AC
NNA5446	576726.00	6678567.00	334.2	75.0	AC
NNA5447	574752.74	6679606.57	334.9	64.0	AC
NNA5448	574613.55	6679681.30	334.6	63.0	AC
NNA5449	574497.59	6679751.49	334.9	81.0	AC
NNA5450	574426.65	6679794.81	334.4	66.0	AC
NNA5451	576160.37	6679703.86	321.8	69.0	AC
NNA5452	574358.17	6679842.52	333.3	65.0	AC
NNA5453	574290.93	6679881.36	334.6	81.0	AC
NNA5454	575599.77	6680324.26	328.1	81.0	AC
NNA5455	575734.99	6680234.54	326.6	81.0	AC
NNA5456	575451.45	6680412.92	326.2	81.0	AC
NNA5457	575022.09	6678958.17	331.0	87.0	AC
NNA5458	574584.55	6679217.36	336.8	84.0	AC
NNA5459	574192.64	6679461.52	338.4	87.0	AC
NNA5460	575482.81	6680636.02	328.1	81.0	AC
NNA5461	575996.34	6680863.88	331.5	78.0	AC
NNA5462	576065.86	6680823.54	331.2	60.0	AC
NNA5463	576131.23	6680782.83	329.3	57.0	AC
NNA5464	576185.63	6680742.97	328.7	69.0	AC
NNA5465	575178.59	6680575.24	322.4	81.0	AC
NNA5466	575110.16	6680609.86	324.5	81.0	AC
NNA5467	576252.15	6680709.39	328.8	60.0	AC
NNA5468	576323.75	6680658.70	329.0	54.0	AC
NNA5469	576379.52	6680625.75	329.0	51.0	AC
NNA5470	576467.42	6680582.62	328.9	39.0	AC
NNA5471	575036.76	6680653.05	326.8	81.0	AC
NNA5472	575256.17	6680528.00	321.8	81.0	AC
NNA5473	575316.90	6680492.77	322.7	81.0	AC
NNA5474	575603.63	6680565.56	328.4	81.0	AC
NNA5475	575749.11	6680487.66	326.2	81.0	AC
NNA5476	575126.82	6680849.65	324.6	81.0	AC
NNA5477	575177.19	6681081.53	325.2	81.0	AC
NNA5478	574890.62	6680737.78	329.8	78.0	AC
NNA5479	574969.10	6680690.51	329.3	81.0	AC
NNA5480	575712.63	6681959.00	330.1	63.0	AC
NNA5481	575626.06	6681993.61	329.7	69.0	AC
NNA5482	576221.14	6681396.91	329.7	75.0	AC
NNA5483	576285.33	6681357.59	330.6	75.0	AC
NNA5484	576090.56	6681732.98	330.0	81.0	AC
NNA5485	576151.00	6682189.00	333.0	60.0	AC
NNA5486	577079.04	6682604.06	341.8	57.1	AC
NNA5487	579121.21	6682820.51	339.3	57.0	AC
NNA5488	575890.85	6683058.76	335.2	81.0	AC
NNA5489	576084.00	6681738.00	330.0	81.0	AC
NNA5490	576143.00	6682188.00	333.0	60.0	AC
NNA5491	575597.00	6681093.57	327.3	81.0	AC
NNA5492	577071.87	6682608.10	342.3	56.0	AC
NNA5505	576253.94	6681876.78	329.5	156.0	AC
NNA5506	574570.41	6679717.01	334.2	65.0	AC
NNA5507	575719.43	6681290.23	330.2	132.0	AC
NNA5508	575238.78	6680797.41	324.3	126.0	AC
NNA5510	574490.41	6679764.54	334.8	114.0	AC
NNA5733	579141.00	6683046.00	350.1	101.0	AC
NNA5734	579089.00	6683078.00	350.1	81.0	AC
NNA5735	579007.95	6683126.10	348.0	72.0	AC
NNA5736	578866.23	6683217.70	342.3	54.0	AC
NNA5737	578014.70	6682528.77	339.0	89.0	AC
NNA5738	578208.92	6682412.95	345.1	99.0	AC
NNA5756	578780.33	6683030.88	346.1	51.0	AC
NNA5757	578852.00	6682991.00	346.4	93.0	AC
NNA5758	578935.86	6683166.80	345.1	39.0	AC
NNA5765	577323.63	6682686.66	334.2	78.0	AC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5766	576969.00	6682660.00	342.1	64.0	AC
NNA5770	581406.31	6683316.58	335.7	48.0	AC
NNA5771	581533.09	6683252.76	338.8	57.0	AC
NNA5772	576013.59	6681770.29	329.2	42.0	AC
NNA5778	579015.14	6682480.33	340.0	48.0	AC
NNA5805	580128.46	6682876.21	332.0	45.0	AC
NNA5806	579862.42	6682624.43	333.3	48.0	AC
NNA5807	579013.00	6682458.00	340.7	84.0	AC
NNA5808	578663.68	6682625.77	335.3	63.0	AC
NNA5810	577805.11	6682145.51	341.4	63.0	AC
NNA5811	577923.97	6682071.77	344.6	61.0	AC
NNA5813	578127.32	6681971.53	346.0	60.0	AC
NNA5814	578223.52	6681897.35	337.5	51.0	AC
NNA5815	578294.00	6681864.28	333.5	63.0	AC
NNA5816	578388.53	6681803.89	337.3	48.0	AC
NNA5817	577854.25	6682254.62	336.6	60.0	AC
NNA5818	577923.22	6682214.55	341.0	51.0	AC
NNA5819	577988.71	6682169.22	345.0	57.0	AC
NNA5820	578061.25	6682134.02	343.8	60.0	AC
NNA5821	578129.65	6682092.03	336.3	54.0	AC
NNA5823	578265.49	6682007.33	340.4	66.0	AC
NNA5824	578349.48	6681953.17	334.0	57.0	AC
NNA5825	578398.63	6681923.82	335.6	54.0	AC
NNA5826	578470.10	6681883.12	340.5	54.0	AC
NNA5829	577978.26	6682290.67	341.8	84.0	AC
NNA5830	578046.06	6682247.01	344.3	66.0	AC
NNA5831	578159.56	6682181.13	344.6	81.0	AC
NNA5832	578225.99	6682140.95	343.2	57.0	AC
NNA5834	578499.35	6681974.91	341.2	57.0	AC
NNA5835	578569.06	6681935.99	347.2	63.0	AC
NNA5836	578628.95	6681897.76	350.1	60.0	AC
NNA5837	578698.90	6681857.87	351.8	54.0	AC
NNA5838	577900.87	6682465.25	335.7	90.0	AC
NNA5839	577964.95	6682430.49	337.0	69.0	AC

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5840	578033.10	6682389.59	339.9	60.0	AC
NNA5841	578103.53	6682349.41	342.6	76.0	AC
NNA5843	578241.54	6682274.16	345.5	75.0	AC
NNA5844	578308.69	6682220.95	344.3	76.0	AC
NNA5844R	578307.00	6682219.00	344.1	60.0	AC
NNA5845	578394.17	6682170.05	338.3	72.0	AC
NNA5845R	578389.06	6682171.34	338.5	51.0	AC
NNA5846	578454.13	6682136.90	337.3	115.0	AC
NNA5848	578585.53	6682058.97	344.7	57.0	AC
NNA5849	578653.04	6682015.95	349.2	63.0	AC
NNA5849R	578657.00	6682010.00	349.6	39.0	AC
NNA5850	578722.95	6681975.23	352.9	78.0	AC
NNA5851	578785.45	6681937.92	354.7	63.0	AC
NNA5852	578831.09	6681914.28	354.4	60.0	AC
NNA5853	578920.05	6681856.28	346.3	60.0	AC
NNA5854	578982.77	6681819.00	344.8	63.0	AC
NNA5855	577713.70	6682688.59	338.3	54.0	AC
NNA5857	578341.17	6682331.97	348.5	96.0	AC
NNA5858	578447.83	6682277.84	348.7	72.0	AC
NNA5859	578544.87	6682212.18	338.5	66.0	AC
NNA5861	578713.90	6682113.33	336.8	90.0	AC
NNA5862	578797.94	6682069.95	337.1	54.0	AC
NNA5863	578858.54	6682029.18	340.3	93.0	AC
NNA5864	578926.70	6681983.30	345.4	60.4	AC
NNA5865	578994.37	6681945.79	346.9	63.1	AC
NNA5866	579059.29	6681914.10	349.5	63.0	AC
NNA5867	579132.59	6681868.79	346.6	60.0	AC
NNA5868	577856.66	6682749.42	337.5	57.0	AC
NNA5869	577920.44	6682707.62	338.6	60.0	AC
NNA5871	578122.48	6682580.80	339.7	87.0	AC
NNA5873	578254.88	6682506.83	342.1	60.0	AC
NNA5874	578323.31	6682467.52	344.9	72.0	AC
NNA5876	578466.30	6682375.82	347.5	120.0	AC
NNA5877	578537.80	6682337.91	346.5	84.0	AC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5878	578584.93	6682307.44	346.8	81.0	AC
NNA5880	578738.86	6682217.66	333.5	66.0	AC
NNA5882	578932.58	6682107.64	333.9	72.0	AC
NNA5883	578997.67	6682070.63	336.1	63.0	AC
NNA5884	579068.79	6682031.12	339.0	54.0	AC
NNA5885	579144.95	6681991.35	342.9	93.0	AC
NNA5887	578048.58	6682868.65	332.1	51.0	AC
NNA5890	578519.12	6682586.20	335.7	67.0	AC
NNA5892	578733.05	6682467.42	335.5	66.2	AC
NNA5894	578866.11	6682387.99	342.5	71.3	AC
NNA5895	578926.90	6682338.11	337.9	71.0	AC
NNA5896	578997.44	6682301.89	339.1	66.0	AC
NNA5897	579065.75	6682259.51	343.3	120.0	AC
NNA5898	579135.60	6682218.92	340.8	75.0	AC
NNA5899	579212.69	6682170.87	340.4	60.0	AC
NNA5901	579350.19	6682091.52	341.0	57.0	AC
NNA5902	579418.39	6682053.24	342.5	63.0	AC
NNA5903	578594.60	6682788.17	336.9	54.0	AC
NNA5904	578659.54	6682748.11	337.4	60.0	AC
NNA5905	578728.25	6682706.99	336.7	60.0	AC
NNA5907	578867.90	6682628.35	338.0	72.0	AC
NNA5908	578926.73	6682587.14	339.6	60.0	AC
NNA5909	578994.71	6682546.46	340.1	63.0	AC
NNA5911	579131.70	6682469.56	339.5	63.0	AC
NNA5913	579278.33	6682381.59	340.4	71.0	AC
NNA5914	579344.09	6682342.27	339.1	75.0	AC
NNA5915	579414.48	6682296.58	337.3	65.0	AC
NNA5916	579484.86	6682261.35	335.5	43.0	AC
NNA5918	578869.67	6682866.16	337.8	62.5	AC
NNA5919	578933.94	6682819.20	337.2	70.0	AC
NNA5922	579143.49	6682701.13	338.6	78.0	AC
NNA5924	579288.22	6682612.91	335.4	71.0	AC
NNA5926	579409.42	6682533.38	335.1	74.3	AC
NNA5927	579480.88	6682496.04	334.1	72.0	AC

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5928	579555.35	6682450.58	332.8	43.0	AC
NNA5929	579618.86	6682415.08	332.9	51.0	AC
NNA5930	579686.70	6682374.35	334.3	51.0	AC
NNA5934	579278.42	6682849.31	337.0	76.0	AC
NNA5936	579412.34	6682764.39	333.0	69.0	AC
NNA5937	579482.30	6682722.14	332.3	68.3	AC
NNA5938	579554.03	6682683.07	332.0	87.0	AC
NNA5939	579621.64	6682650.43	332.0	57.0	AC
NNA5940	579688.60	6682603.93	331.9	57.0	AC
NNA5942	579828.57	6682517.77	333.0	57.0	AC
NNA5943	579891.61	6682475.10	334.6	57.0	AC
NNA5946	579407.77	6683001.62	336.3	93.0	AC
NNA5948	579542.84	6682919.10	332.0	63.0	AC
NNA5949	579612.03	6682878.84	331.1	54.0	AC
NNA5950	579681.83	6682839.05	331.7	51.0	AC
NNA5951	579744.92	6682793.70	332.0	57.0	AC
NNA5952	579888.06	6682715.32	332.3	119.0	AC
NNA5954	580093.65	6682595.42	336.1	57.0	AC
NNA5955	580162.67	6682554.55	339.1	51.0	AC
NNA5956	580291.25	6682466.51	342.4	74.0	AC
NNA5957	579738.74	6683021.74	328.6	51.0	AC
NNA5958	579810.98	6682984.47	328.2	51.0	AC
NNA5959	579878.23	6682941.81	329.0	51.0	AC
NNA5960	579945.09	6682902.09	330.0	51.0	AC
NNA5961	580014.91	6682861.89	330.7	72.0	AC
NNA5963	580152.13	6682781.53	333.1	93.0	AC
NNA5965	580298.78	6682700.79	338.9	58.0	AC
NNA5966	579935.66	6683127.89	330.0	59.0	AC
NNA5968	580077.39	6683045.74	330.9	54.0	AC
NNA5969	580145.64	6683006.07	331.4	93.0	AC
NNA5971	580291.49	6682927.57	335.1	90.0	AC
NNA5972	580363.87	6682887.11	337.6	57.0	AC
NNA5973	580432.89	6682851.55	338.1	54.0	AC
NNA5974	580153.16	6683256.06	331.2	78.0	AC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NNA5976	580292.04	6683176.91	331.7	54.0	AC
NNA5978	580430.31	6683097.24	333.8	54.0	AC
NNA5979	580500.09	6683056.36	335.5	60.0	AC
NNA5980	577625.27	6682136.44	340.6	57.0	AC
NNA5982	577803.62	6682044.71	341.7	93.0	AC
NNA5983	577895.28	6681999.23	344.2	60.0	AC
NNA5984	577980.05	6681949.76	346.2	63.0	AC
NNA5985	578075.71	6681904.86	346.9	60.0	AC
NNA5986	578540.60	6681840.38	344.8	43.0	AC
RC0001	577116.00	6676657.72	321.4	143.0	RC
RC0021	577160.21	6677328.91	325.1	71.0	RC
RC0035	577373.83	6676601.77	323.9	93.0	RC
RC0036	577204.00	6676903.28	321.5	76.0	RC
RC0037	576880.53	6676698.11	330.4	83.0	RC
RC0047	577252.00	6677128.00	323.1	77.0	RC
RC0048	576728.25	6677237.27	336.7	97.0	RC
RC0055	576369.07	6680114.58	331.0	48.5	RC
RC0061	574001.65	6678901.19	341.0	101.0	RC
RC0064	577107.00	6677667.00	326.2	83.0	RC
RC0145	576590.40	6677771.32	327.3	77.0	RC
RC0153	576289.34	6678275.81	329.0	83.0	RC
RC0299	573329.73	6680189.36	341.6	65.0	RC
RC0300	574195.78	6679931.20	335.4	101.0	RC
RC0301	574826.14	6679555.14	336.0	125.0	RC
RC0324	575160.96	6680830.75	324.6	137.0	RC
RC0357	575480.88	6679163.36	323.3	95.0	RC
RC0471B	575160.00	6680830.00	324.7	80.0	RC
RC0651	575062.16	6680358.70	323.6	89.0	RC
RC0656	574412.88	6680488.70	332.2	95.0	RC
RC0657	575065.05	6679901.90	328.1	61.5	RC
RC0658	574528.26	6679742.32	334.5	66.0	RC
RC0661	573889.50	6679648.14	337.0	89.0	RC
RC0662	574746.28	6679120.70	334.5	85.0	RC
RC0663	575229.78	6678832.24	331.5	95.0	RC

Hole ID	Easting	Northing	RL	Depth	Type [1]
RC0664	574858.11	6678092.13	350.1	99.5	RC
RC0755	574650.26	6680603.65	329.4	89.0	RC
RC1011	575167.43	6679350.36	324.1	56.0	RC
RC1013	574719.45	6678808.32	336.0	68.5	RC
RC1015	575846.23	6677913.68	338.4	90.0	RC
RC1026	575597.22	6680570.48	328.4	104.5	RC
RC1028	575492.17	6681153.66	326.0	84.0	RC
RC1030	576389.50	6681553.93	333.1	86.0	RC
RC1034	576020.68	6683224.33	338.8	72.0	RC
RC1037	577750.44	6682192.57	340.0	84.0	RC
RC1040	580398.06	6683507.67	335.5	65.0	RC
RC1129	576514.87	6678546.49	334.0	83.0	RC
RC1140	576859.25	6678341.04	333.4	100.0	RC
RC1141	576228.03	6678717.62	327.0	83.0	RC
RC1142	575826.98	6678956.88	327.6	88.0	RC
RC1143	578970.45	6682451.03	341.8	89.0	RC
RC1144	579312.28	6682244.04	342.0	77.0	RC
RC1145	575846.31	6679894.73	321.9	71.0	RC
RC1146	576193.90	6679689.89	322.4	65.0	RC
RC1147	576532.86	6679490.20	326.8	77.0	RC
RC1148	576004.01	6680325.77	325.5	71.0	RC
RC1149	576207.52	6680728.41	328.6	71.0	RC
RC1150	575863.18	6680950.11	331.5	53.0	RC
RC1151	576374.94	6681103.25	326.0	59.0	RC
RC1152	576022.22	6681298.90	328.1	83.0	RC
RC1153	576035.16	6681753.87	329.5	107.0	RC
RC1154	576734.60	6681347.01	335.5	47.0	RC
RC1155	576753.99	6679630.83	329.5	83.4	RC
RC1156	577090.81	6681604.27	329.3	36.0	RC
RC1157	576725.45	6681838.30	340.4	71.0	RC
RC1158	576390.54	6682025.22	329.3	83.0	RC
RC1159	576039.00	6682234.66	332.7	77.0	RC
RC1160	576059.27	6682722.41	336.9	53.0	RC
RC1161	576386.15	6682519.23	331.1	59.0	RC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
RC1162	576729.75	6682320.85	332.0	77.0	RC
RC1163	577072.46	6682108.27	337.7	72.0	RC
RC1164	577416.98	6681904.30	336.9	96.0	RC
RC1165	577766.98	6681706.62	341.0	41.0	RC
RC1166	578343.73	6681843.26	334.6	53.0	RC
RC1167	577590.91	6682295.44	338.7	47.0	RC
RC1168	577243.67	6682494.79	334.8	71.0	RC
RC1169	576571.91	6682907.34	333.3	113.0	RC
RC1170	576909.77	6683191.57	334.7	101.0	RC
RC1171	577231.39	6682987.61	335.9	77.0	RC
RC1172	577604.05	6682775.99	336.3	72.0	RC
RC1173	577933.87	6682564.24	337.3	66.0	RC
RC1174	578283.09	6682369.47	347.1	98.0	RC
RC1175	578641.13	6682156.38	336.1	113.0	RC
RC1176	578627.07	6682654.15	335.7	68.0	RC
RC1177	578272.37	6682855.43	333.9	59.0	RC
RC1178	577942.03	6683052.57	340.5	77.0	RC
RC1179	577599.18	6683223.49	335.3	59.0	RC
RC1207	579636.53	6682035.99	346.9	83.0	RC
RC1208	577199.33	6678138.16	330.4	50.0	RC
RC1209	576697.44	6678920.83	334.0	85.0	RC
RC1210	576863.05	6679284.31	330.3	89.0	RC
RC1211	576558.59	6680528.36	328.8	29.0	RC
RC1212	576716.32	6680886.66	328.9	41.5	RC
RC1213	575684.42	6681498.05	328.8	71.0	RC
RC1214	575697.39	6682439.35	331.5	77.0	RC
RC1215	579072.68	6682082.42	336.1	71.5	RC
RC1216	578629.59	6683116.34	339.4	53.0	RC
RC1217	578966.92	6682922.94	339.3	64.3	RC
RC1218	579307.62	6682715.66	336.0	87.0	RC
RC1219	579661.40	6682503.06	333.4	66.0	RC
RC1220	579981.23	6682311.26	338.2	56.0	RC
RC1262	576206.90	6681635.49	330.3	63.5	RC
RC1278	575498.65	6679909.46	323.2	100.0	RC

Hole ID	Easting	Northing	RL	Depth	Type [1]
RC1279	575498.48	6679995.20	322.2	100.0	RC
RC1284	577288.03	6678878.23	332.7	106.0	RC
RC1291	577593.11	6683741.21	335.1	59.0	RC
RC1292	577658.64	6680791.58	339.3	35.0	RC
RC1293	577261.05	6683939.90	343.1	89.0	RC
RC1294	576807.66	6682053.17	329.8	53.0	RC
RC1295	578107.01	6681494.40	348.5	63.0	RC
RC1296	578433.09	6681285.56	352.0	47.0	RC
RC1297	576457.72	6682727.21	331.0	89.0	RC
RC1298	577338.35	6682192.68	334.4	41.0	RC
RC1299	577502.01	6682087.97	335.6	33.0	RC
RC1300	577687.71	6681993.67	341.2	89.0	RC
RC1301	578608.59	6681686.37	343.3	41.0	RC
RC1302	576731.76	6682797.52	335.2	89.0	RC
RC1303	578799.76	6681796.75	348.6	59.0	RC
RC1304	576925.43	6682925.55	334.0	59.0	RC
RC1305	577767.23	6682410.70	334.5	71.0	RC
RC1306	577906.70	6682329.71	337.4	57.0	RC
RC1307	578975.13	6681700.52	343.1	63.0	RC
RC1308	576200.36	6683589.91	338.0	89.0	RC
RC1309	576506.82	6683387.28	334.3	53.0	RC
RC1310	578193.52	6682646.51	342.0	53.0	RC
RC1311	576925.92	6683613.51	335.1	89.0	RC
RC1312	577269.24	6683418.00	331.0	77.0	RC
RC1313	580010.00	6681781.73	336.5	41.0	RC
RC1314	578737.08	6682819.14	337.9	59.0	RC
RC1315	577944.35	6683537.33	343.6	65.0	RC
RC1316	578287.14	6683332.78	332.7	35.1	RC
RC1317	580202.49	6683099.26	331.0	71.0	RC
RC1318	580548.16	6682900.86	339.2	65.0	RC
RC1322	580927.02	6683149.02	337.0	57.0	RC
RC1337	578043.36	6682759.48	336.2	50.0	RC
RC1338	576978.67	6681928.32	331.2	47.0	RC
RC1348	579151.65	6681593.85	342.6	46.0	RC

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
RC1411	576048.32	6682462.59	331.0	53.0	RC
RC1412	576452.39	6682232.95	329.9	59.0	RC
RC1451	581224.91	6683427.77	343.0	53.0	RC
RC1452	581573.41	6683217.52	339.9	76.5	RC
RC1453	576008.02	6681108.44	327.1	60.0	RC
RC1454	576433.72	6680834.99	328.8	65.0	RC
RC1455	575574.07	6680843.96	327.0	77.0	RC
RC1456	575943.42	6681552.85	329.0	83.0	RC
RC1457	576215.29	6681407.98	329.7	83.0	RC
RC1458	576518.05	6681216.06	333.1	59.0	RC
RC1459	576905.25	6681718.90	327.8	47.0	RC
RC1460	577739.40	6681208.01	343.3	47.0	RC
RC1461	578089.77	6681004.80	352.0	59.0	RC
RC1462	579511.35	6681619.27	350.7	59.0	RC
RC1463	579673.18	6681781.22	338.0	41.0	RC
RC1464	580009.14	6682059.39	339.0	59.0	RC
RC1465	580685.97	6681886.16	341.0	35.0	RC
RC1466	580465.37	6682248.33	346.8	83.0	RC
RC1467	580350.05	6682548.86	342.9	107.0	RC
RC1469	581414.77	6682875.50	330.0	29.0	RC
RC1470	581745.80	6682659.38	331.6	29.0	RC
RC1476	575693.26	6682934.73	336.0	59.0	RC
RC1477	575333.18	6682657.51	338.0	59.0	RC
RC1534	575643.00	6681332.00	329.1	89.0	RC
RC1535	575319.61	6681427.27	325.7	71.0	RC
RC1536	575273.25	6681123.36	325.9	53.0	RC
RC1537	576918.55	6682658.40	341.0	65.0	RC
RC1538	577099.49	6682583.05	340.7	59.0	RC
RC1539	577284.26	6682492.62	335.0	47.0	RC
RC1540	576741.34	6682537.04	335.5	53.0	RC
RC1541	576900.22	6682442.26	333.0	53.0	RC
RC1542	577083.06	6682368.11	331.4	47.0	RC
RC1543	576634.95	6682360.65	333.0	45.0	RC
RC1544	576792.96	6682266.38	333.1	59.0	RC
RC1545	575861.11	6682588.50	332.4	47.0	RC
RC1546	576007.96	6682486.67	331.0	44.0	RC
RC1547	576200.76	6682385.72	330.3	52.0	RC
RC1548	576370.56	6682284.88	330.6	53.0	RC
RC1549	576537.18	6682183.83	330.0	38.0	RC
RC1550	575935.59	6682279.48	331.7	47.0	RC
RC1551	576111.06	6682202.75	333.0	47.0	RC
RC1552	576299.28	6682089.29	330.9	47.0	RC
RC1553	576473.38	6681985.66	330.9	53.0	RC
RC1554	576626.34	6681895.34	336.5	57.0	RC
RC1555	579901.18	6682728.22	331.5	47.0	RC
RC1556	579905.90	6682719.13	331.7	47.0	RC
RC1557	579931.73	6682671.12	332.7	53.0	RC
RC1558	579936.15	6682662.45	332.7	47.0	RC
RC1559	579996.32	6682632.74	333.4	47.0	RC
RC1560	579935.25	6682729.95	331.6	47.0	RC
RC1561	579868.88	6682667.77	333.1	47.0	RC
RC1562	579851.47	6682658.05	333.3	50.0	RC
RC1563	579835.05	6682648.79	333.1	45.0	RC
RC1564	579832.45	6682752.14	332.4	53.0	RC
NN0172	579475.95	6683217.06	334.3	66.0	FDAC
NSA0165	577094.52	6682582.52	340.6	56.2	FDAC
NSA0166	577027.36	6682626.08	342.4	70.0	FDAC
NSA0167	579103.22	6682830.41	339.0	51.0	FDAC
NSA0168	579107.51	6682827.85	339.0	66.0	FDAC
NSA0169	579099.78	6682832.46	339.0	53.0	FDAC
NSA0170	579094.62	6682835.54	339.0	26.0	FDAC
NSA0171	579090.33	6682838.10	339.0	50.0	FDAC
AS2000	579129.34	6682824.42	339.3	55.0	SO
AS2001	579525.00	6682648.00	332.4	56.5	SO
AS2002	578643.00	6682390.00	336.7	49.0	SO
AS2003	576226.04	6681645.47	330.5	48.0	SO
AS2005	577083.76	6682597.78	341.8	56.6	SO
CD0001	577116.10	6676657.72	321.4	172.1	DDH

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
CD0779	574892.98	6680459.63	326.1	81.2	DDH
CD0780	574686.15	6679638.65	334.8	90.2	DDH
CD0859	575247.66	6680248.04	321.0	42.3	DDH
CD0860	574871.99	6680008.70	328.0	45.2	DDH
CD0861	576713.26	6676993.53	331.0	47.0	DDH
CD1247	579946.99	6682973.31	329.4	45.0	DDH
CD1248	579494.90	6682617.69	332.7	47.5	DDH
CD1249	579142.62	6682401.76	340.9	54.0	DDH
CD1250	575806.92	6680453.52	325.5	42.0	DDH
CD1251	576203.54	6682133.46	332.4	72.0	DDH
CD1252	577421.71	6682394.25	334.5	45.0	DDH
CD1253	577877.55	6682125.92	343.5	48.3	DDH
CD1254	578400.00	6682290.00	348.6	54.1	DDH
CD1255	578877.26	6682126.83	333.0	45.2	DDH
CD1256	578793.69	6682535.44	336.3	51.2	DDH
CD1257	579099.43	6682833.84	339.0	54.3	DDH
CD1258	577085.24	6682595.05	341.5	56.9	DDH
CD1259	576576.91	6682398.23	332.4	54.3	DDH
CD1260	576896.01	6682207.79	334.4	57.3	DDH
CD1261	576550.62	6681927.01	333.2	52.8	DDH
CD1262	576206.98	6681635.49	330.3	42.5	DDH
CD1263	576200.38	6681188.39	327.1	42.5	DDH
CD1264	576026.13	6680850.47	331.5	45.6	DDH
CD1265	576187.12	6680232.33	328.5	44.1	DDH
CD1266	576494.04	6679261.09	324.6	42.3	DDH
CD1269	580559.98	6683363.33	331.1	46.4	DDH
CD1360	576260.54	6681863.61	329.6	75.0	DDH
CD1361	576283.25	6682335.66	330.6	65.0	DDH
CD1362	576620.80	6682134.06	329.7	44.3	DDH
CD1363	576834.30	6682493.70	335.6	51.4	DDH
CD1364	577001.15	6682392.64	329.8	45.3	DDH
CD1365	577256.43	6682715.01	333.4	48.4	DDH
CD1366	577429.98	6682620.90	338.2	45.4	DDH
CD1367	577593.34	6682514.86	335.4	42.4	DDH

Hole ID	Easting	Northing	RL	Depth	Type [1]
CD1368	578110.08	6682207.80	344.7	49.2	DDH
CD1369	578275.95	6682105.94	343.0	46.7	DDH
CD1370	578389.07	6682538.61	338.4	48.2	DDH
CD1371	578556.10	6682438.10	334.6	42.4	DDH
CD1372	578722.64	6682342.95	340.7	50.1	DDH
CD1373	578939.56	6682300.41	337.0	45.8	DDH
CD1374	579078.01	6682621.31	336.1	51.3	DDH
CD1375	579245.52	6682511.46	338.3	51.2	DDH
CD1376	579229.40	6682983.37	339.8	48.0	DDH
CD1377	579423.02	6682879.93	333.7	49.9	DDH
CD1378	579593.38	6682780.72	331.5	44.9	DDH
CD1379	579855.06	6682856.87	329.9	43.8	DDH
CD1387	576085.81	6681975.59	331.2	54.5	DDH
CD1388	576429.31	6681765.76	333.2	54.5	DDH
CD1389	575874.46	6682344.37	330.6	48.0	DDH
CD1390	576672.21	6682599.16	333.6	48.3	DDH
CD1391	577171.04	6682294.32	333.5	48.0	DDH
CD1392	577027.65	6682852.99	333.3	49.3	DDH
CD1393	578439.65	6682008.08	337.5	46.8	DDH
CD1394	578531.82	6682695.29	336.1	48.9	DDH
CD1395	578906.25	6682718.83	337.8	48.3	DDH
CD1396	579421.99	6682414.65	335.4	49.8	DDH
CD1397	579762.07	6682681.76	332.8	45.2	DDH
CD1398	579683.21	6682949.48	329.3	40.8	DDH
CD1399	580017.26	6682746.11	331.5	45.3	DDH
CD1400A	580247.53	6682824.85	334.5	36.5	DDH
CD1400B	580247.53	6682824.85	334.2	45.3	DDH
CD1401	580376.57	6683008.89	335.7	48.3	DDH
CD1402	576035.28	6680571.60	326.9	41.0	DDH
CD1403	575925.76	6680121.79	322.0	36.0	DDH
CD1404	578307.65	6682589.71	340.8	52.8	DDH
CD1405	578460.30	6682492.73	336.0	45.3	DDH
CD1406	578642.52	6682392.35	336.6	49.3	DDH
CD1407	578795.49	6682304.85	342.3	49.8	DDH

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
CD1408	578987.26	6682195.45	337.4	49.9	DDH
CD1409	578711.07	6682585.49	334.3	42.1	DDH
CD1410	578890.31	6682479.21	340.7	51.1	DDH
CD1413	579067.99	6682422.21	340.4	51.3	DDH
CD1414	579196.30	6682369.65	341.8	53.0	DDH
CD1415	579157.50	6682567.97	336.2	51.0	DDH
CD1416	579935.34	6682577.74	333.8	41.0	DDH
CD1417	579083.01	6683086.07	350.0	78.2	DDH
CD1480	575272.54	6680516.15	322.0	38.0	DDH
CD1481	575725.50	6680247.68	327.0	46.8	DDH
CD1482	575851.43	6680661.56	327.0	44.0	DDH
CD1483	576219.74	6680981.06	326.8	41.0	DDH
CD1484	576377.60	6681294.00	332.0	45.3	DDH
CD1485	575869.31	6681863.06	329.8	41.0	DDH
CD1486	576558.06	6681450.30	337.4	48.0	DDH
CD1487	576608.07	6681662.70	339.4	56.0	DDH
CD1488	575914.80	6682081.25	331.6	44.0	DDH
CD1489	575744.30	6682184.90	329.8	43.5	DDH
CD1489a	575744.30	6682184.90	329.8	43.5	DDH
CD1490	575948.41	6682546.17	331.6	47.0	DDH
CD1491	578169.10	6681928.01	341.6	50.0	DDH
CD1492	578111.66	6682462.46	342.0	47.0	DDH
CD1493	579328.96	6681977.19	338.5	50.0	DDH
CD1494	579454.11	6682145.98	340.0	44.0	DDH
CD1495	579603.44	6682309.27	333.6	47.1	DDH
CD1496	580108.15	6682466.56	339.4	48.3	DDH
CD1497	580194.05	6682645.07	337.1	47.0	DDH
CD1498	580035.28	6683210.91	330.4	50.0	DDH
CD1501	579523.76	6683046.80	332.1	53.0	DDH
CD1502	579331.70	6683165.14	344.0	120.0	DDH
CD1503	575775.31	6682635.68	333.6	51.3	DDH
CD1506	580332.02	6683039.62	333.6	47.0	DDH
CD1507	580026.47	6682933.04	330.8	44.0	DDH
CD1508	580178.77	6682849.98	332.8	45.1	DDH

Hole ID	Easting	Northing	RL	Depth	Type [1]
CD1509	579933.29	6682801.41	330.5	45.1	DDH
CD1510	580062.91	6682703.86	333.0	44.0	DDH
CD1511	579485.77	6682835.36	331.5	44.0	DDH
CD1512	579676.32	6682731.23	331.7	45.1	DDH
CD1513	579834.19	6682632.18	332.9	45.1	DDH
CD1514	579236.34	6682766.80	338.8	54.0	DDH
CD1515	579398.36	6682662.62	333.7	50.0	DDH
CD1516	579588.61	6682549.73	333.2	47.0	DDH
CD1517	579019.80	6682656.57	337.1	47.5	DDH
CD1518	579343.81	6682462.61	337.7	52.2	DDH
CD1519	579518.40	6682359.29	332.7	53.0	DDH
CD1520	579208.72	6682066.47	338.4	48.5	DDH
CD1521	580323.91	6682769.65	337.5	44.0	DDH
CD1522	578560.73	6682203.62	337.2	45.0	DDH
CD1523	579335.06	6682926.80	336.5	46.2	DDH
CD1524	580024.71	6682514.62	336.6	44.0	DDH
CD1525	579028.54	6682879.67	338.4	51.0	DDH
CD1565	579910.43	6682710.73	331.8	43.5	DDH
CD1566	579912.80	6682705.95	331.8	44.0	DDH
CD1567	579914.89	6682702.15	332.0	43.0	DDH
CD1569	579917.61	6682697.82	332.1	43.0	DDH
CD1570	579918.78	6682695.15	332.0	43.2	DDH
CD1571	579920.07	6682693.34	332.0	43.5	DDH
CD1572	579904.63	6682698.15	332.5	43.5	DDH
CD1573	579922.42	6682688.90	332.2	43.5	DDH
CD1574	579924.90	6682684.49	332.4	42.0	DDH
CD1575	579927.08	6682679.98	332.4	45.0	DDH
CD1576	579951.67	6682713.85	331.4	42.0	DDH
CD1577	579942.81	6682708.94	331.4	43.5	DDH
CD1578	579912.28	6682722.68	331.8	42.0	DDH
CD1579	579929.73	6682701.44	331.8	40.3	DDH
CD1580	579925.48	6682699.14	331.9	45.0	DDH
CD1581	579923.23	6682697.87	332.0	44.5	DDH
CD1582	579920.99	6682696.70	332.0	41.8	DDH

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
CD1583	579916.49	6682694.10	332.1	44.3	DDH
CD1584	579914.25	6682693.16	332.2	42.0	DDH
CD1585	579912.16	6682691.91	332.2	47.5	DDH
CD1586	579907.71	6682689.31	332.4	46.5	DDH
CD1587	579903.43	6682687.15	332.6	44.7	DDH
CD1588	579894.78	6682682.19	332.8	46.5	DDH
CD1589	579886.02	6682677.50	332.8	47.7	DDH
CD1590	579909.01	6682706.64	332.0	43.5	DDH
CD1591	579912.84	6682698.45	332.1	43.3	DDH
CD1592	579917.17	6682689.05	332.2	42.0	DDH
CD1593	579921.59	6682679.64	332.5	43.5	DDH
CD1594	579460.30	6683229.88	334.5	81.0	DDH
NBS0004	580129.71	6682874.27	332.2	44.0	DDH
NBS0005	578664.80	6682602.52	334.9	49.0	DDH
NBS0006	579056.57	6682858.88	339.0	52.0	DDH
NBS0007	577050.00	6682610.53	342.0	56.9	DDH
NBS0008	576230.50	6682127.30	332.2	47.9	DDH
NND5000	576196.68	6682134.30	332.6	82.0	DDH
NND5001	579124.09	6682823.13	339.3	75.0	DDH
NND5014	574901.82	6680460.85	325.9	81.0	DDH
NND5015	575834.87	6680439.29	325.3	81.0	DDH
NND5016	576023.85	6680852.61	331.5	81.0	DDH
NND5017	578723.72	6682350.54	340.1	80.0	DDH
NND5018	578631.18	6682392.53	336.3	80.0	DDH
NND5019	578455.59	6682493.94	336.4	93.0	DDH
NND5020	578385.83	6682540.76	338.6	80.0	DDH
NND5028	576087.20	6681735.09	330.0	62.0	DDH
NND5029	575965.22	6681553.91	329.0	60.5	DDH
NND5030	575544.37	6681137.09	326.2	68.4	DDH
NND5031	579499.00	6682610.00	332.9	57.1	DDH
NND5032	578631.67	6682381.98	337.6	53.1	DDH
NND5033	579137.56	6682818.68	339.6	52.4	DDH
NND5034	576399.16	6681300.10	332.3	47.0	DDH
NND5035	576053.00	6682472.00	331.0	50.1	DDH

Hole ID	Easting	Northing	RL	Depth	Type [1]
NND5036	576590.88	6682390.75	332.9	53.0	DDH
NND5037	578681.64	6682608.88	334.8	46.7	DDH
NND5038	579230.88	6682522.03	338.3	56.0	DDH
NND5039	579795.78	6682656.01	333.1	53.0	DDH
NND5040	580034.34	6682734.10	332.1	47.0	DDH
NND5041	580092.20	6682899.15	331.6	45.0	DDH
NND5075	579115.84	6682823.05	339.3	49.6	DDH
NND5076	579131.20	6682834.90	339.5	48.5	DDH
NND5077	576147.80	6682189.32	333.0	54.3	DDH
NND5078	577075.96	6682605.99	342.4	57.0	DDH
NND5773	576264.99	6682110.08	331.4	36.0	DDH
NND5774	576583.71	6681912.39	334.6	42.0	DDH
NND5775	576993.28	6682651.43	342.5	48.0	DDH
NND5776	578168.92	6682436.23	343.5	39.0	DDH
NND5777	578664.76	6682627.04	335.0	47.2	DDH
NND5779	579067.97	6682859.33	339.0	52.0	DDH
NND5780	579277.35	6682735.45	337.0	45.0	DDH
NND5781	579860.89	6682623.72	333.1	45.5	DDH
NND5782	580129.26	6682877.58	331.9	44.0	DDH
NND5794	579015.36	6682480.30	340.0	57.5	DDH
NND5809	577680.08	6682239.52	339.9	55.4	DDH
NND5812	578053.00	6682005.87	346.0	55.4	DDH
NND5822	578199.06	6682045.13	338.2	62.9	DDH
NND5828	577859.49	6682369.16	334.7	63.9	DDH
NND5833	578381.64	6682045.37	334.9	46.4	DDH
NND5839	577966.31	6682433.50	337.0	83.0	DDH
NND5842	578169.75	6682319.88	344.3	59.8	DDH
NND5847	578526.99	6682096.46	340.6	67.4	DDH
NND5860	578607.16	6682173.04	336.6	66.9	DDH
NND5870	578052.08	6682632.61	339.9	72.7	DDH
NND5872	578179.79	6682550.59	339.7	57.7	DDH
NND5875	578387.06	6682425.06	346.6	89.1	DDH
NND5879	578673.49	6682263.79	336.5	65.5	DDH
NND5881	578822.07	6682167.01	332.9	62.8	DDH

List of holes used in 2016 Ambassador Resource Estimation - Grid GDA94 Zone 51

Hole ID	Easting	Northing	RL	Depth	Type [1]
NND5888	578130.52	6682818.26	332.8	50.9	DDH
NND5889	578445.38	6682624.33	336.8	52.4	DDH
NND5891	578656.78	6682505.65	333.9	66.6	DDH
NND5893	578794.37	6682428.84	338.6	75.1	DDH
NND5900	579286.09	6682134.43	340.3	56.6	DDH
NND5906	578802.71	6682673.01	336.8	49.2	DDH
NND5910	579067.39	6682507.23	338.5	62.7	DDH
NND5912	579204.76	6682422.39	340.8	173.4	DDH
NND5920	579007.05	6682779.86	337.5	67.4	DDH
NND5921	579074.55	6682744.17	337.9	65.9	DDH
NND5923	579208.75	6682657.86	336.9	68.9	DDH
NND5925	579344.64	6682569.48	335.5	65.6	DDH
NND5933	579197.84	6682883.53	338.8	66.4	DDH
NND5935	579348.00	6682813.00	334.6	62.2	DDH
NND5941	579753.76	6682560.78	332.2	50.5	DDH
NND5947	579479.54	6682963.18	333.5	52.4	DDH
NND5953	579956.00	6682674.00	334.8	47.9	DDH
NND5962	580084.75	6682819.07	331.5	50.1	DDH
NND5964	580225.20	6682735.05	335.9	49.0	DDH
NND5967	580009.05	6683087.56	330.5	46.5	DDH
NND5970	580225.55	6682969.44	332.6	52.2	DDH
NND5975	580224.91	6683216.16	331.6	45.1	DDH
NND5977	580362.11	6683138.98	332.4	50.9	DDH
NND5981	577711.92	6682087.88	339.7	58.3	DDH

[1] AC – Aircore drill hole; FDAC – Face discharge aircore; RC – Reverse circulation drill hole; SO – Sonic drillhole; and DDH – Diamond drill hole