

9 September 2016

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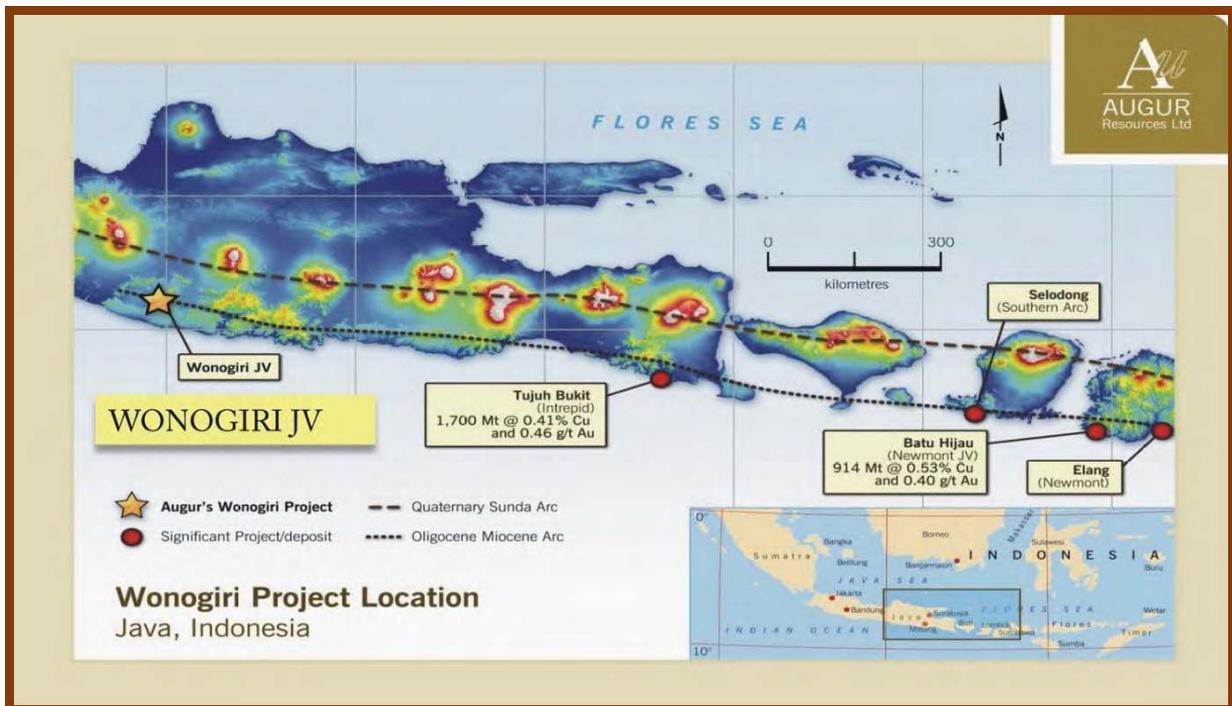
(25 pages by email)

**ADDITIONAL INFORMATION RE RANDU KUNING RESOURCE ESTIMATE  
(ASX: AUK)**

Augur Resources Limited ('Augur') refers to the announcement dated 30 August 2016 and provides the following additional information, as required by ASX Listing Rule 5.8.1 in relation to the updated JORC 2012 compliant resource estimate of the Randu Kuning deposit.

**Geology and Geological Interpretation**

The Wonogiri Project lies within the Sunda-Banda arc and covers an area of 3,928 hectares. The Randu Kuning deposit is one of six mineralised targets that occupy a northwest trending composite intrusive at the northern end of the Wonogiri Project.

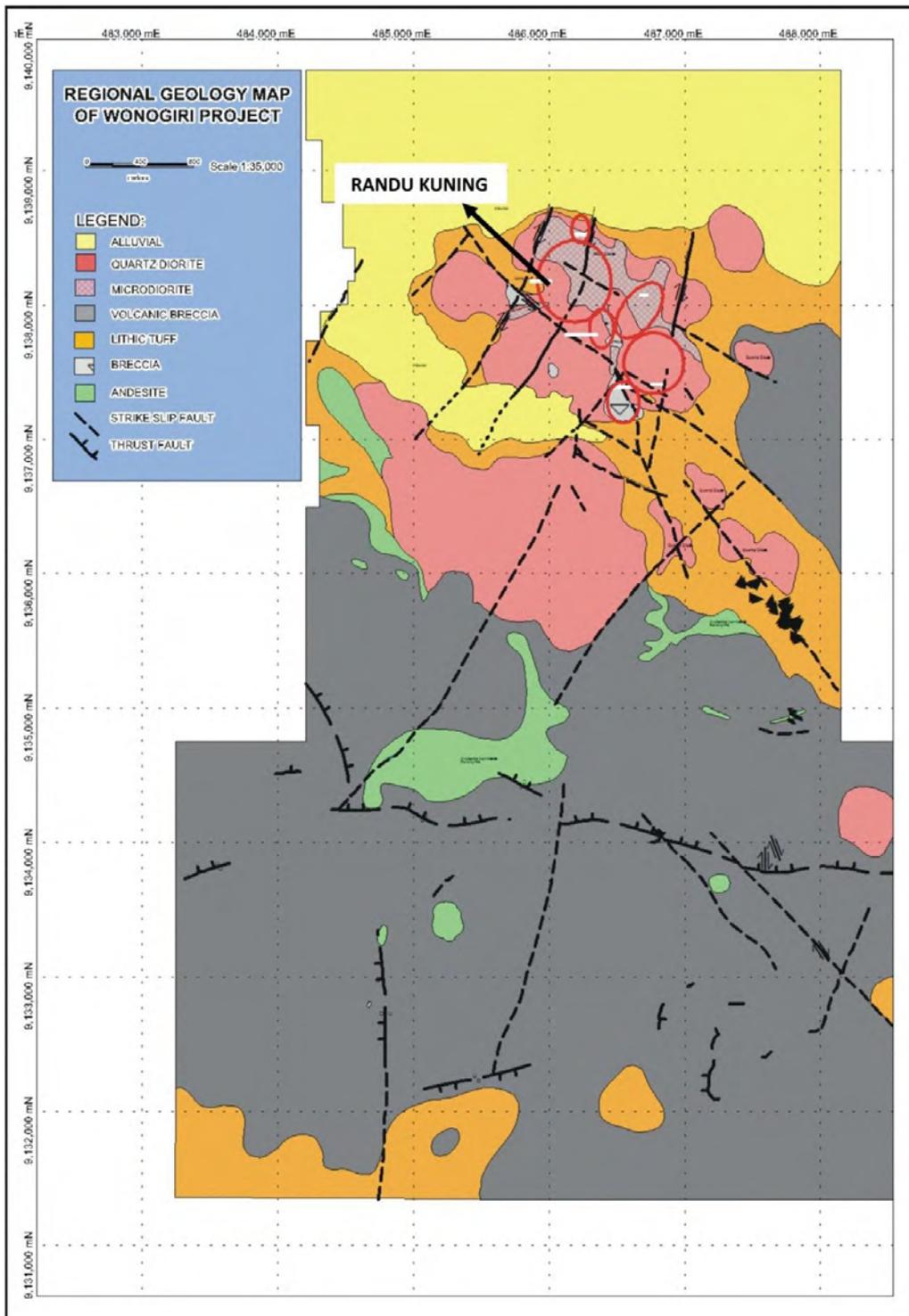


**Project location**

There are no forestry restrictions over the IUP nor any known social or environmental issues. There are no known impediments to exploration and mining development.

## GEOLOGY

The Sunda Banda Arc comprises both Miocene to Pliocene volcanics and younger Quaternary volcanics. Over time, the Arc has migrated from west to east as well as from south to north. It is segmented by a series of arc-normal structures that trend NNE and which are evident in the topography. Tectonic factors appear to have localised volcanic centres of the Miocene arc at positions near the southwest margins of these transfer structures. Contemporaneous continental to deep-ocean clastic sediments were deposited on the margins of the volcanic centres. The Wonogiri Project is surrounded by several Quaternary volcanos - Gunung Lawu, Merapi and Merbabu.



**Project geology**

## STRATIGRAPHY

The stratigraphic column at Wonogiri consists of (from young - old) Alluvium, Merapi Volcanic Rock, Lawu Volcanic Rock, Wonosari-Punung Formation, Oyo Formation, Ngalinggran Formation, Semilir Formation, Mandalika Formation, and the Gamping Wungkal Formation.

The Mandalika Formation dominates and consists of dacite and andesite lavas, tuffaceous dacite and diorite. The Semilir Formation crops out in the south, and consists of tuff, dacite breccia and tuffaceous sandstone. The local structural geology in the project area is dominated by northeast-southwest strike slip faults and east west thrust faults.

The geology of the Wonogiri Project area was mapped by PT. Oxindo Exploration during 2009-2010. They identified a series of multiple diorite intrusions which intruded the early volcanic sequence of lithic tuffs, volcanic breccia and andesite. Alluvial deposits represent the latest stage of the geologic history.

The Randu Kuning Deposit consists of a carapace breccias sitting astride a polyphasal diorite/microdiorite intrusion. The breccia is also polyphasal. The diorite is slightly elliptical in plan view and has a northwest trend.

### HYDROTHERMAL ALTERATION (after Corbett, 2011):

**Outer propylitic alteration** is common as magnetite-chlorite alteration of the Wonogiri diorite. This is a weak intrusion-related hydrothermal alteration and includes some epidote. It hosts elevated copper-gold mineralisation in the deep drill hole WG002 and the barren sheeted laminated quartz-magnetite veins in WDD019 and WDD020.

**Inner propylitic alteration** is defined as magnetite-epidote dominant varying to chlorite at lower temperatures and actinolite closer to the intrusion heat source.

**Potassic alteration** dominates much of the Randu Kuning mineralisation as a flooding of magnetite with one or both secondary K-feldspar and/or biotite. It is characterised as a pink colour or dark brown dusting respectively. Much of this alteration is overprinted by crackle breccias comprising magnetite and possible actinolite with associated bleaching of the prograde alteration. In many instances these crackle breccias also contain chalcopyrite.

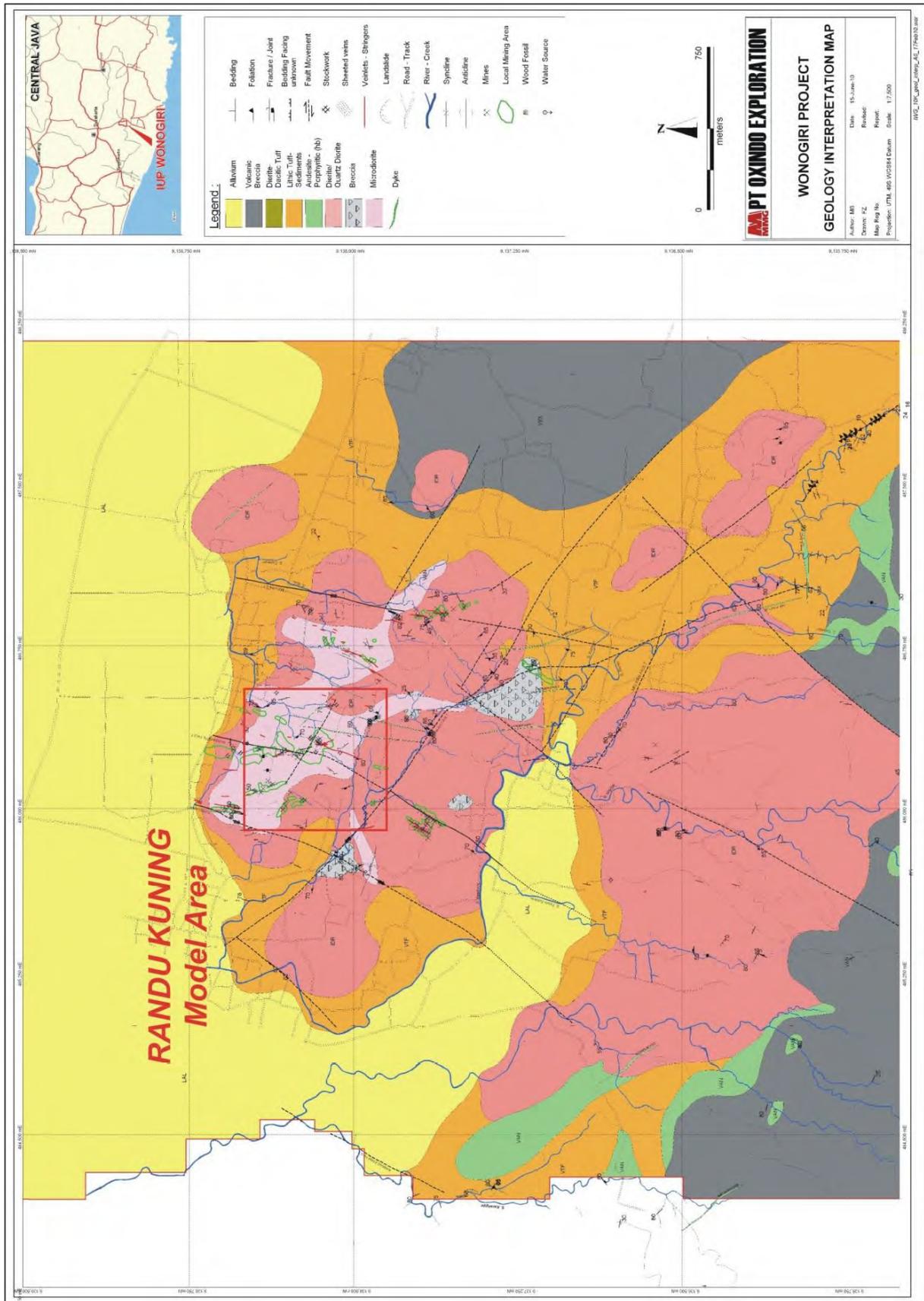
**Phyllic alteration** is characterised by retrograde silica-sericite-pyrite. It is recognised adjacent to the later stage porphyry style B veins and the low temperature stage epithermal quartz-sulphide veins.

### MINERALISATION (after Corbett, 2011):

Throughout Randu Kuning, the copper-gold grades developed as an accumulation effect of a combination of several overprinting events and styles of mineralisation, characterised as (Corbett,2011):

**Disseminated chalcopyrite** is common, generally associated with clots of magnetite and/or chlorite-epidote which locally contribute towards the development of early magnetite-chalcopyrite stringers which pre-date quartz vein formation. These sulphides are interpreted to have been locally derived from the cooling host intrusion (Corbett, 2011).

**Early quartz veins** are characterised as A veins comprising mostly saccharoidal quartz and lesser magnetite with sinuous gradational vein margins developed as stockwork or sheeted vein arrays. The gradational vein margins are indicative of formation during cooling of the host intrusion. Some linear A type quartz veins contain disseminated chalcopyrite, deposited during vein formation.



Detailed Project geology showing area of resource estimation model

**Most quartz veins** contain sulphides introduced from the cooling magmatic source at depth, after the original quartz + magnetite vein formation, and bled into the source intrusion. Sheeted veins occur as dilatant fractures which aid in the transport of ore fluids from source intrusions at depth to higher crustal level intrusions to locally form wallrock porphyry systems.

Consequently, AB veins develop by the filling of earlier A veins by later chalcopyrite, while M veins, massive stockwork A veins and laminated linear A veins may all contain significant components of sulphides introduced after initial vein formation. Feeder sulphide (chalcopyrite-pyrite) veins termed C veins in the geological literature therefore supply copper-gold mineralisation to brittle quartz veins which fracture as ideal brittle hosts. AB veins formed by the filling with sulphide of a central termination within A veins.

Copper-gold grades increase passing from disseminated to stringer magnetite-chalcopyrite veins derived from the source intrusion, to quartz veins characterised by increased quantities of sulphide derived from magmatic source rocks at depth. Sheeted vein arrays aid metal transport. Elevated metal grades may result from the mixing of collapsing low pH fluids responsible for the development of silica-sericite-pyrite (phyllic) alteration with mineralised fluids such as those responsible for the disseminated copper-gold in the deep drill hole WG002.

**Barren laminated and sheeted quartz magnetite veins** - These laminated veins are likened to M veins in porphyry systems while sheeted A style quartz-magnetite veins are also present. Both lack sulphide, although pyrite-carbonate fill occurs in some veins and one instance of yellow sphalerite was recognised.

The strong lamination and sheeted character of these veins is typical of a dilatant structural environment of formation. In each case, veins at the margins of the zones are oriented at low angles to the core axis and rotate to angles of 090 as veins become thicker in the centre of the zone. It is interpreted this combined change in vein orientation and intensity is indicative of the development of a dilatant character for the central vein portion.

**Epithermal veins**, comprising quartz, pyrite, chalcopyrite yellow to pale red sphalerite, lesser galena and carbonate fill, clearly cut the porphyry veins, commonly with sericite alteration halos. The yellow sphalerite within many of these veins is indicative of a low temperature of formation, and the common low angles to the core axis suggest these veins trend EW and at a high angle to the overall trend of the porphyry mineralisation. While some sparse epithermal veins display elevated gold grades, the overall contribution to the metal budget of these veins is small. Two possible mechanisms for the formation of low temperature epithermal veins overprinting the earlier porphyry system suggests:

1. The epithermal veins were deposited by a low temperature fluid venting from the cooling magmatic source at depth as a late stage event of the main porphyry system. A relaxation in the kinematic conditions active during porphyry vein formation may have facilitated formation of epithermal veins within a different orientation; or
2. There has been renewed magmatism, possibly after erosion, to result in the emplacement of a new magmatic source at depth for these later overprinting veins. A continuum is envisaged in associated mineralisation and alteration between the prograde potassic alteration and porphyry veins and later epithermal veins retrograde alteration derived from the same cooling magmatic source.

## **DRILLING**

A total of 17,215 metres has been drilled at the Wonogiri Project in 55 drill holes. Forty-two of these holes are located at Randu Kuning and were drilled over two exploration phases.

Initial drilling was completed by PT Oxindo in 2009-2010, for which 3 drill holes intersected the Randu Kuning deposit. A further 39 holes were drilled by Augur in 2011-2012 for a total of 12,207 metres. Two holes, WDD009 and WDD050 were deepened to fully transect the mineralisation, for a further 256.5 metres in 2014.

Program	Number of Holes Drilled	Total Meters Drilled	Average	Minimum/Maximum
2009-2010	3	1,151.7	383.9 ± 112.2	273.2 to 537.65
2011-2012	39	12,207.0	313.0 ± 130.0	157.6 to 854.95
2014	2 extensions	256.5	-	82.55 to 173.95
Total	42	13,615.2		

Holes were generally collared using PQ tool (nominal core diameter of 75mm) and then reduced to HQ and then NQ tool depending on drilling conditions. At Randu Kuning, drill holes were collared on nominal 50 x 50 metre drill spacing with azimuths of 090° or 270°. Hole dips were generally 45° 60° with some holes at 50°, 55°, 70° and 75°. Average drill depths were 318.0 ± 130.0 metres ranging from 157.6 to 854.95 metres.

### CORE SAMPLE PREPARATION

Drill core preparation commenced at the drill site by trained technicians who recorded the drill runs and recovery, numbered and inserted the core-blocks and secured the aluminium core boxes for delivery to the lay-down area at the site office. At the site office, the core boxes were weighed and photographed (wet and dry), logged, and then marked-up for half-core cutting and sampling by trained technicians. All work was directly supervised by the Site Geologist.

Drill core was logged by geologists for major lithological units and alteration zones to determine sampling intervals. All sample intervals were marked by core blocks, entered into a ledger and assigned a unique sample number. After cutting and sampling detailed logging continued using standardised forms which were entered into the database and verified daily.

Core was cut in half using an electric powered, water cooled diamond blade core cutter located at the site office. Core samples were cut carefully to minimise breakage and to prevent parts of the sample being washed away during cutting. Core intervals that were clay rich and broken or friable were not cut but representatively sampled by spatula and spoon.

Half core was bagged according to the sample specifications. PQ core was generally sampled in 0.5 metre lengths while HQ and NQ core was sampled in 1 metre lengths where mineralised and 2 metre lengths elsewhere. Sampling intervals were constrained to major lithologic boundaries.

Split core was placed into plastic bags along with a sample ticket. The sample number was written onto the outside of each plastic bag using a permanent marker. Blank samples were inserted into the sampling stream at every 40th sample starting at sample 1 of any batch. Standards were also inserted at every 40th sample starting at sample 20. All sample bags were weighed prior to dispatch to the lab. Sample batches of 400 were packed into sealed and annotated rice sacks (10 per sack) and road transported by the Company to the Intertek laboratory in Jakarta. Samples were subjected to full security from drilling through processing till delivery to the laboratory. Intertek standard sample submission forms were cross-checked with Sample Receipt Confirmation notes issued by the laboratory. Laboratory results were emailed to the site office as well as the corporate offices in Jakarta and Sydney.

Core recovery was recorded in the Geotechnical Log against run length. The average core recovery from 50 drillholes (15,218.8 metres) was  $97 \pm 13\%$ . Ninety-five percent of the drilling has core recovery greater than 90% and 1.5% was recorded with zero recovery.

## **SAMPLE ASSAYING**

The majority of samples were assayed by PT. Intertek Utama Services at its Jakarta laboratory, a member of the worldwide Intertek Group. PT. Intertek Utama Services is accredited for chemical testing under ISO 17025:2005 (General requirements for the competence of testing and calibration laboratories) by Akreditasi National (KAN). Their accreditation number is LP-130-IDN (renewed on 30 April 2007) and is equivalent to NATA certification in Australia.

PT. SGS [Jakarta] (accredited for chemical testing under ISO/ICE 17025:2005) was used for the initial sampling program and for the early part of the drill program. PT. SGS and Geoservices Laboratory (also of Jakarta, and also accredited for chemical testing under ISO/ICE 17025:2005) were used for independent checks and comparison with Intertek.

## **METHOD**

At the Intertek laboratory, samples were checked against the Sample Submission sheet, oven dried at  $105^{\circ}\text{C}$ , weighed then jaw crushed to 95%  $<2\text{mm}$ . A 1.5 kg subsample was riffle spit for pulverising to 95% $<200\#$ . Two splits were taken from this product, one for analysis the other for QAQC.

Samples were analysed for gold using method FA51, a lead collection fire assay using a 50g charge with an AAS finish. Base metals contents were estimated by method IC01, which used an aqua regia digest with ICP-OES finish.

## **QAQC**

A structured Quality-Assurance-Quality-Control program has been conducted during all drill phases. The program has consisted of regular submission of blanks and prepared standards and comparative sample runs with other laboratories. Standards were purchased from Ore Research & Exploration Pty Ltd [Bayswater North, Australia].

## **Blanks**

Four hundred and thirty-seven (437) blank samples were submitted to SGS and Intertek during Phase 2 of the drill program at a rate of  $9.5 \pm 3.4$  samples per drill hole. The average grade of the 420 Intertek samples was 0.004 g/t gold and 21 ppm copper with data ranges from BLD (0.004 g/t) to 0.94 for gold and 14 to 1980 for copper. The average grade of the 17 SGS samples was 0.004 g/t Au and 48 ppm Cu with data ranges from 0.002 to 0.012 for gold and 18 to 135 for copper.

Three samples have gold grades in excess of 0.1 g/t gold. Sample BB007267 (0.11 g/t Au) follows BB007266 with gold grade of 0.02 g/t gold; sample BB003702 (0.15 g/t gold) follows BB003701 with gold grade of 0.06 g/t gold; and sample BB005277 (0.94 g/t gold) follows BB005276 with gold grade of 0.24 g/t gold. Two samples have copper grades in excess of 1,000 ppm copper. Sample BB003742 (1240ppm copper) follows BB003741 with copper grade of 633ppm Cu; and sample BB007267 (1980ppm copper) follows BB007266 with copper grade of 238ppm copper.

There is no consistent pattern of cross-contamination within these samples suggesting that they are anomalous in their composition.

**Table 1: Summary Statistics for Blanks**

Descriptor	Hole Statistics	Intertek		SGS	
		Au g/t	Cu ppm	Au g/t	Cu ppm
Count	48	437	401	17	17
Mean	9.5	0.004	21	0.004	48
Stdev	3.4	0.047	139	0.004	29
Min	4	0.004	14	0.002	18
Max	25	0.94	1980	0.012	135

## Standards

A group of 11 standards covering the range of gold and copper grades encountered at the deposit have been regularly submitted to SGS and Intertek as part of a comprehensive QAQC program. A total of four hundred and twenty-two (422) standards were submitted at a rate of  $9.1 \pm 3.7$  samples per drill hole. The average gold grade of these standards is within  $\pm 5\%$  of the expected value, although the variance within the individual standard populations can be outside the expected variance as defined by the manufacturer. Control charts of the individual standards are generally within expected limits. The various standards indicate that assaying of the Randu Kuning material should return values that are representative of the grade of the material.

**Table 2: Summary Statistics for Standards**

	STANDARD	ORE_Au	ORE_Cu	Au_Int	Cu_int	AU ratio	CU ratio
Count	STD10C			32	28		
Mean		6.6		6.43	179	97%	
Stdev		0.16		0.34	4	214%	
Min		6.52		5.72	168		
Max		6.67		7.15	184		
Count	STD19A			27	22		
Mean		5.49		5.50	144	100%	
Stdev		0.1		0.20	5	197%	
Min		5.45		5.07	131		
Max		5.54		5.86	151		
Count	STD501			29	24		
Mean		0.204		0.21	2660	104%	
Stdev		0.011		0.01	88	70%	
Min				0.2	2440		
Max				0.23	2780		
Count	STD502			7	7		
Mean		0.491		0.50	7667	103%	
Stdev		0.02		0.02	73	95%	

	STANDARD	ORE_Au	ORE_Cu	Au_Int	Cu_int	AU ratio	CU ratio
Min				0.48	7590		
Max				0.54	7820		
Count	STD504			7	7		
Mean		1.48		1.53	11114	103%	
Stdev		0.04		0.05	254	135%	
Min				1.48	10800		
Max				1.64	11500		
Count					33	33	
Mean	STD52C	0.346		0.35	3443	101%	
Stdev		0.017		0.02	50	110%	
Min				0.29	3330		
Max				0.39	3550		
Count					13	13	
Mean	STD61D	4.76		4.81	108	101%	
Stdev		0.14		0.11	3	80%	
Min				4.59	104		
Max				4.93	117		
Count					40	35	
Mean	STD62D	10.5		10.59	48	101%	
Stdev		0.33		0.32	2	98%	
Min		10.36		9.94	45		
Max		10.64		11.4	52		
Count					65	60	
Mean	STD66A	1.237	121	1.26	122	102%	101%
Stdev		0.054	7	0.06	4	117%	63%
Min		1.211	117	1.01	114		
Max		1.263	124	1.5	134		
Count					85	79	
Mean	STD67A	2.238		2.24	333	100%	
Stdev		0.096		0.08	7	88%	
Min		0		2.04	314		
Max		0		2.49	353		
Count					84	78	
Mean	STD68A	3.89	392	3.89	394	100%	100%
Stdev		0.15	15	0.14	14	94%	92%
Min		2.82	384	3.56	305		
Max		3.95	400	4.5	417		
Count							

## Inter-Laboratory Checks

Two separate groups of mineralised sample pulps were sent to PT.Geoservices and PT.SGS to test for laboratory scale systematic errors. Fifty-two samples were assayed by PT. Geoservices for gold (using method FAA50) and Ag, As, Cu, Fe, Mo, Pb, S, Zn using method GAI01.

The average gold grade of the sample set was 0.99 g/t gold compared with the Intertek assays which averaged 1.01 g/t gold (Table 7). RPE<sup>2</sup> statistics for gold have an average value of  $0.69 \pm 8.07\%$  with a data range from -22 to +24%; 80% of samples are within  $\pm 10\%$ .

The average copper grade of the sample set was 2006 ppm copper compared with the Intertek assays which averaged 2018 ppm copper. RPE statistics have an average value of  $-0.51 \pm 4.73\%$  with a data range from -20 to +7%; 88% of samples are within  $\pm 5\%$ .

**Table 3: Sample Statistics for PT.Geoservices Check Samples**

	Number	Mean	StdDev	Min	Max
Intertek_Au	52	1.01	0.68	0.32	3.94
Geoservices_Au	52	0.99	0.54	0.36	2.62
RPE_Au	52	0.69	8.07	-22.33	23.96
Intertek_Cu	52	2018	1289	84	5750
Geoservices_Cu	52	2006	1283	82	5583
RPE_Cu	52	-0.51	4.73	-19.42	6.81

Fifty-five samples were assayed by PT.SGS for gold (by method FAA515) and Ag, Cu, Pb and Zn by method AAS20B. The average gold grade of the sample set was 1.58 g/t gold compared with the Intertek assays which averaged 1.80 g/t gold. RPE statistics for gold have an average value of  $-6.43 \pm 13.93\%$  with a data range from -60 to +17%; 73% of samples are within  $\pm 10\%$ .

The average copper grade of the sample set was 4,449 ppm copper compared with the Intertek assays which averaged 4,267 ppm copper. RPE statistics have an average value of  $1.47 \pm 6.96\%$  with a data range from -16 to +18%; 88% of samples are within  $\pm 5\%$ .

**Table 4: Sample Statistics for PT.SGS Check Samples**

	Number	Mean	StdDev	Min	Max
Intertek_Au	55	1.80	1.26	0.44	6.65
SGS_Au	55	1.58	1.13	0.49	6.29
RPE_Au	55	-6.43	13.93	-60.00	17.39
Intertek_Cu	55	4267	6079	120	46500
SGS_Cu	55	4449	6440	120	49200
RPE_Cu	55	1.47	6.96	-16.11	17.82

## Specific Gravity

One hundred and eighty-two (182) samples were selected by a geologist for specific gravity analysis. A 10cm sample of half core was cut and tightly wrapped in plastic to prevent breakage. The sample was marked with a sample identifier and dispatched to Intertek in Jakarta for analysis using the specific gravity method. The samples were weighed in air, coated with wax to seal voids, then re-weighed in air and water. The SG is calculated as the ratio of the weight in air to the difference of the weights in air and water, compensated for the weight of wax.

The database consists of 182 measurements from 40 drill holes at a rate of  $4.6 \pm 2.0$  per drill hole. Drill holes at Randu Kuning account for 152 measurements. Compositing of the data to nominal 1 metre sample lengths to allow allocation of oxidation code generates 160 composites with comparable statistics. The data is well distributed across the depth profile of the deposit. Although some lower values (2.3 to 2.6) occur in the top 200 metres of the deposit the number of these in the current data set is small and they do not form a meaningful statistical population. The majority of the population fall within the data range 2.60 to 2.82 and have an average value of  $2.7 \text{ Kg/m}^3$ .

**Table 5 SG Data Statistics**

SAMPLE TYPE	NUMBER	AVERAGE	STD DEVIATION	MINIMUM	MAXIMUM
TOTAL	182	2.70	0.10	2.31	2.87
SGS	152	2.707	0.101	2.31	2.87
SGC	160	2.697	0.102	2.31	2.87
Oxide	10	2.613	0.153	2.31	2.82
Transition	9	2.762	0.036	2.71	2.80
Fresh	132	2.698	0.099	2.35	2.87

The SG data was merged into the Sample Database using the midpoint of the sample interval to control the assignment routine (i.e. if the mid-point of an SG sample occurred within an assay interval the drill sample was assigned that SG value). Rock codes were then assigned based on the sample's geographic location within the interpreted oxidation model. The Oxide zone accounts for only 10 samples with an average value of  $2.61 \pm 0.15$  and the Transition for 9 samples with an average value of  $2.76 \pm 0.04$ . The average of all oxidised material is  $2.68 \text{ Kg/m}^3$ .

These separate assignments lead to a smoothing of the Bulk Density data. The initial calculation based on tray weight may include multiple rock types which are averaged over the interval. The allocation to sample interval does not take into account any variation of rock type that may occur within the sample interval. The allocation of rock code is most valid in areas where the interpretation of the rock model is well constrained.

### Bulk Density

Bulk Density values were also estimated during core preparation from the ratio of core weight to core volume for individual core boxes. The data has been selected from 35 of the first 50 drill holes with an average of  $72 \pm 29$  trays per drill hole. The database includes PQ, HQ and NQ sized whole core. A number of inconsistencies between related data fields have reduced the usefulness of this database such that it cannot be relied upon as a validated data source, however the global statistics are useful in determining order of magnitude variations between the two methods of density (and hence tonnage) determination.

**Table 6 Bulk Density Statistics**

SAMPLE TYPE	NUMBER	AVERAGE	STD DEVIATION	MINIMUM	MAXIMUM
ALL	2460	2.56	0.21	1.24	2.97
Oxide*	1654	2.61	0.09	2.31	2.87
Transition*	34	2.54	0.11	2.33	2.81
Fresh*	26	2.42	0.08	2.31	2.59

\* constrained within SG data range (2.31 – 2.87) for comparative purposes

## DRILL HOLE SURVEYS

All survey data is in UTM format based on the WGS84 UTM Zone 49S Projection. Collar coordinates were located by PT. Surtech Prima, Indonesia using a total station unit with Differential GPS capability. When signal was available, trigonometric methods were used. Collar orientations were surveyed by the geologist using compass and clinometer. Downhole surveys were collected using a Cameq downhole electronic survey tool, with readings at 25 metre intervals down to 100 metres then at 50 metre interval to the end of hole. An end-of-hole reading was not taken.

Rate of change calculations on the downhole survey data have an average value of  $0.27^\circ \pm 0.25^\circ$  within a data range from 0 to  $1.45^\circ/6$  meters. There were only 2 cases (in WDD42 and WDD46) where the difference between adjacent surveys was  $5^\circ$ . In general, the drill holes were drilled straight and the estimation of their loci should be accurate.

## TOPOGRAPHY

Digital topographic coverage was collected in November 2011 by PT. Surtech Prima, Indonesia using LiDAR technology. Average data spacing is 1.6 metres.

## RESOURCE ESTIMATION

### *METHODOLOGY*

#### **Model Boundary**

A three dimensional block model was defined over the extent of mineralisation with orientation and dimensions as listed in the Table below.

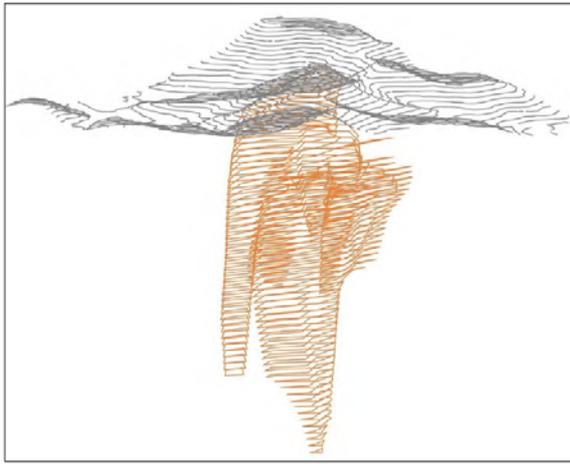
	Origin	Orientation	Number	Size (metres)
<b>RANDU KUNING</b>				
Bench	-400 RL	345°	140	5
Row	9137850 N		65	10
Columns	485900 E		65	10

#### **Topography**

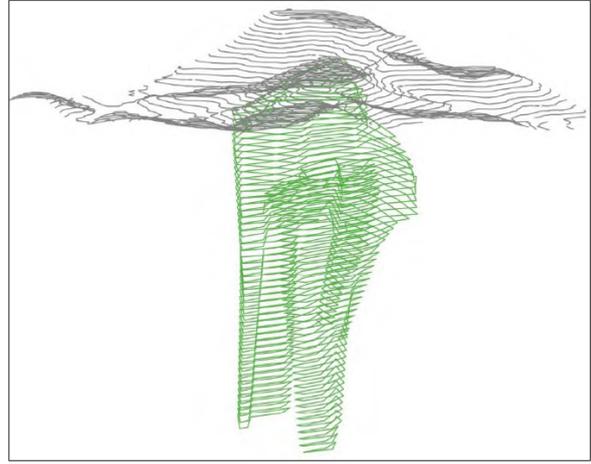
Topographic modelling is based on the results of a LiDAR survey. The LiDAR data files have an average data spacing of 1.6 metres. This data was paged to extract and average all data points occurring within each of the 10x10 metre cells of the defined model. Cell averages were then interpolated using a direchlet triangulation and gridded on to the cell origin.

#### **Geology**

Sectional interpretations of the gold and copper mineralisation, as defined by the 0.3 g/t gold and 800ppm copper cut-offs, were interpreted on both east-west and north-south sections. The mineralisation outlines were converted to plan intercepts at 10 metre levels and reinterpreted in plan-view to ensure continuity along strike. The plan-view polygons were then used to code the rock model using a point in polygon algorithm. Mineralised gold blocks were coded with "10", mineralised copper blocks with 3 and the host with "1" in separate gold and copper models. Oxidation coding was interpreted on all drill sections and extrapolated laterally away from the drilled areas using topography as a guide. The sectional interpretations were used to interpolate Base of Oxide [BOO] and Base of Transition [BOT] surfaces. A rock model was coded using these surfaces as control.



**Gold Model - looking Northwest**



**Copper Model - looking Northwest**

### Compositing and Statistics

Although stratigraphically sampled with respect to major lithology boundaries the most common sample lengths are 0.5, 1.0 and 2.0 metres. This reflects nominal one metre sampling through the mineralised zones and 2 metre sampling in barren zones. This is supported by the broad relation of higher grades occurring in the shorter sample lengths.

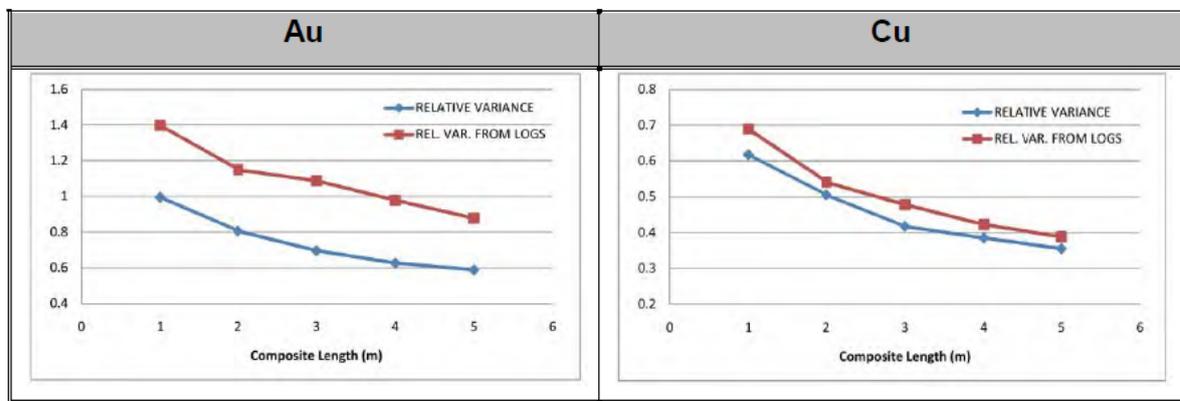
Sample gold grade vary from BLD<sup>3</sup> to 11.2 g/t with an average value of  $0.24 \pm 0.5$  g/t gold. The sample distribution is bimodal with a threshold at 0.3g/t gold partitioning the population into waste (80% of data) and mineralised (20% of data). There are 19 samples with grades in excess of 5 g/t gold and 4 samples with values in excess of 10 g/t gold. The population distribution does not support the need to cut any sample value.

Sample copper grades vary from BLD to 46,500 ppm with an average value of  $679 \pm 1,062$  ppm copper. The sample distribution is bimodal with a threshold at 823 ppm copper partitioning the population into waste (75% of data) and mineralisation (25% of data). Eleven copper samples whose assays exceeded 1.00% copper were considered anomalous to the general population and their values were cut to 10,000 ppm.

Bench Height Analysis indicates that a significant change occurs in the relative variance for both gold and copper at a bench height of 2.5 metres. Compositing to this value will incorporate the majority of short scale grade variation into the basic modelling unit. For modelling purposes at Randu Kuning sample data was drill-hole composited to 2.5 metre intervals with a minimum composite length of 0.5 metres. This process reduced the gold variance by 32%, from 0.29 g/t gold to 0.20 g/t gold, whilst having minimal effect on the mean grade (-2%, 0.27 g/t gold to 0.26 g/t gold). For copper the variance was reduced by 27% and the mean by 3%. In both cases the form of the distribution as mapped by the cumulative frequency curve was not significantly altered.

Element	Number	Arithmetic		Log		Log Mean	Min	Max	# BLD Samples
		Mean	StdDev	Mean	StdDev				
Au	17,137	0.24	0.50	-2.50	1.38	0.21	0.00	11.17	1,071
Cu	18,063	679	1062	6	2	936	2	46500	145
Pb	15,231	18	90	2	1	13	1	4510	2,977
Zn	18,208	169	505	5	1	137	3	36000	0
Ag	8,098	1.08	1.55	-0.19	0.65	1.02	0.20	66.40	10,110
As	10,525	37	228	3	1	22	2	12400	7,683
Mo	11,470	4	10	1	1	4	0	344	6,145
Fe	18,208	5.93	1.59	1.75	0.26	5.94	0.95	24.90	0
S	16,685	1.12	1.44	-0.68	1.45	1.45	0.00	26.20	248

HoleID	From	To	Au g/t	Original Cu ppm	Cut Cu ppm
WDD01	17.9	18.4	4.81	12800	10000
WDD01	39.75	40.25	6.29	16900	10000
WDD02	33.5	34	4.6	10500	10000
WDD04	33	33.5	3.43	11600	10000
WDD04	38	38.5	1.74	16100	10000
WDD04	38.5	39	6.65	46500	10000
WDD04	39	39.5	2.1	16000	10000
WDD04	50.5	51	0.68	17200	10000
WDD05	31	31.5	4.49	13100	10000
WDD05	41.5	42	10.9	18700	10000
WDD10	74	75	5.72	12200	10000

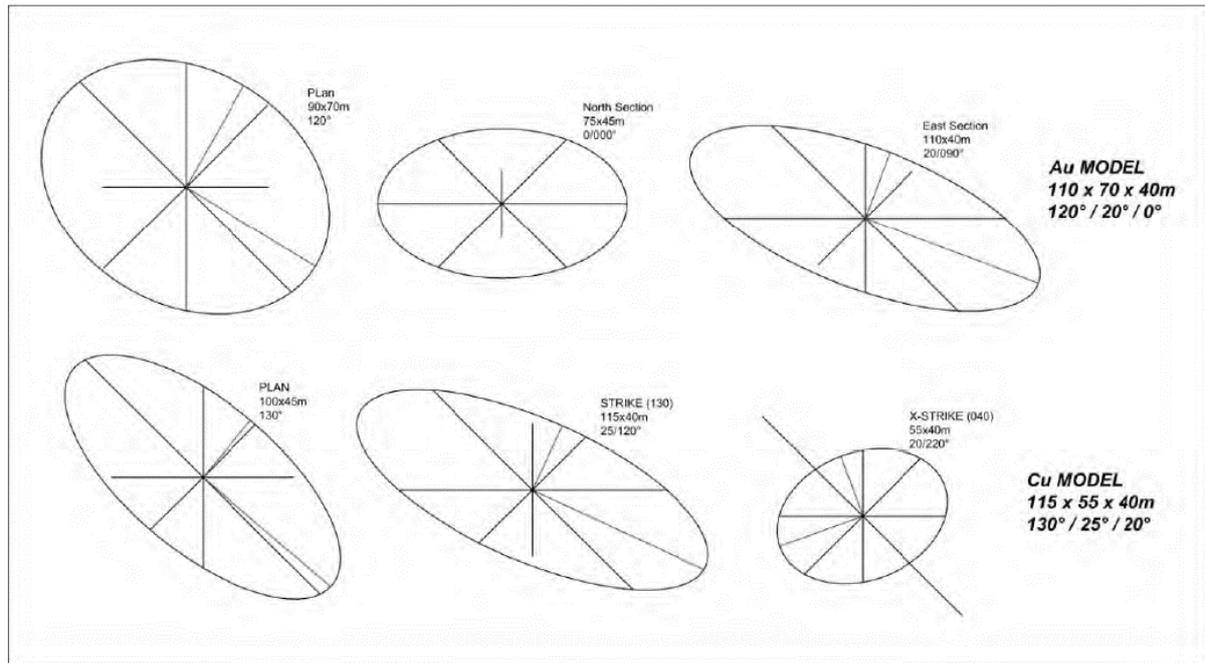


### Summary Statistics Comparison for Gold and Copper

Zone	Sample Type	Number	Mean	Variance	Log Mean Estimate	Minimum	Maximum
Au	Sample	13,873	0.27	0.29	0.26	0.01	11.17
	Composite	5,173	0.26	0.20	0.26	0.01	5.09
Cu	Sample	14,460	823	1,126,450	1049	2	17200
	Composite	5,317	796	820,736	974	1	17412

### Variography

Log variograms were calculated on mineralised gold and mineralised copper composites for a variety of three dimensional vectors in the strike and cross-strike directions to enable the modelling of data anisotropy. Variograms were generally well defined due to the tight data density and their form confirms the data selection is from a reasonably homogeneous population. The figure below presents the geometric anisotropy models for gold and copper.



**Gold** - The gold variograms have a relatively low nugget effect at 27% of the total data variance; they define a geometric anisotropy model of dimension 110 x 70 x 40 oriented with strike 030 and dip 20° east. The variograms also exhibit a weak zonal anisotropy which has a geographic range from 112% transverse to plunge to 91% in the cross-strike direction. Hole effects are evident in the horizontal variograms at ranges of approximately 100 metres and in the vertical direction at approximately 40 metres.

**Copper** - Copper variograms have a high nugget effect at 46% of the total data variance. Although not modelled in detail there is a suggestion that up to 50% of the total variance could be accounted for by short range structures within 10 metres. The copper variograms define a geometric anisotropy of 115 x 55 x 40 metres oriented with strike of 040, dip 25° east and a northerly plunge of 20°. The copper variograms display minimal zonal anisotropy but do have definite hole-effects at 120-130 metres.

## Discussion

The gold and copper variography are reasonably consistent suggesting that they reflect the same mineralising event. The small zonal anisotropy in both dataset indicates that the modeled populations are reasonably homogeneous. The hole effects indicates the presence of repetitive zones of mineralisation which matches with the interpreted structure of a mineralised carapace breccia sitting over a barren intrusive.

## Grade Modelling

Block grades for gold and copper were interpolated using an inverse distance squared interpolator acting within an oriented and scaled search ellipsoid. Both the interpreted mineralised zone (code 30 for gold, code 3 for copper) and the inferred halo mineralisation (code 1) were modelled for both gold and copper. Search ellipsoids were initially defined by the variography but the results contained significant sub-horizontal grade trends that could not be validated against the geology and the drill assays at the scale of the study. It is believed that the variogram models reflect trends that will become important at the mining grade control scale. Search ellipsoids were ultimately defined by combining the primary strike and the 2:1:1 ellipsoid ratio defined by the variography with the vertical alignment that was apparent from the geology. This orientation provided much tighter control on the grade model.

Each block in the model was interpolated by selecting composites of like code, by sector search (3 composites within each of 6 sectors) from within an anisotropic search equal to the maximum search distance. A minimum of 3 composites was required for a determination.

Four models were calculated for both gold and copper. Within the defined mineralised zones separate models were estimated at various maximum search ranges to simulate Measured, Indicated and Inferred category responses. These models were then overlain such that Measured grades, where they existed, took precedence over Indicated grades, and Indicated over Inferred. Outside of the mineralised zones, an Inferred model was estimated using the broader search range.

#### Summary of Search Ellipsoid Parameters for Gold

Class	Code	Ellipsoid Dimension			Ellipsoid Orientation			Maximum Search Distance
		Strike	X-Strike	Dip	Strike	Strike Plunge	Dip	
Measured	30	200	100	100	120	0	90	65
Indicated	30	200	100	100	120	0	90	110
Inferred	30	200	100	100	120	0	90	150
Inferred	1	200	100	100	120	0	90	150

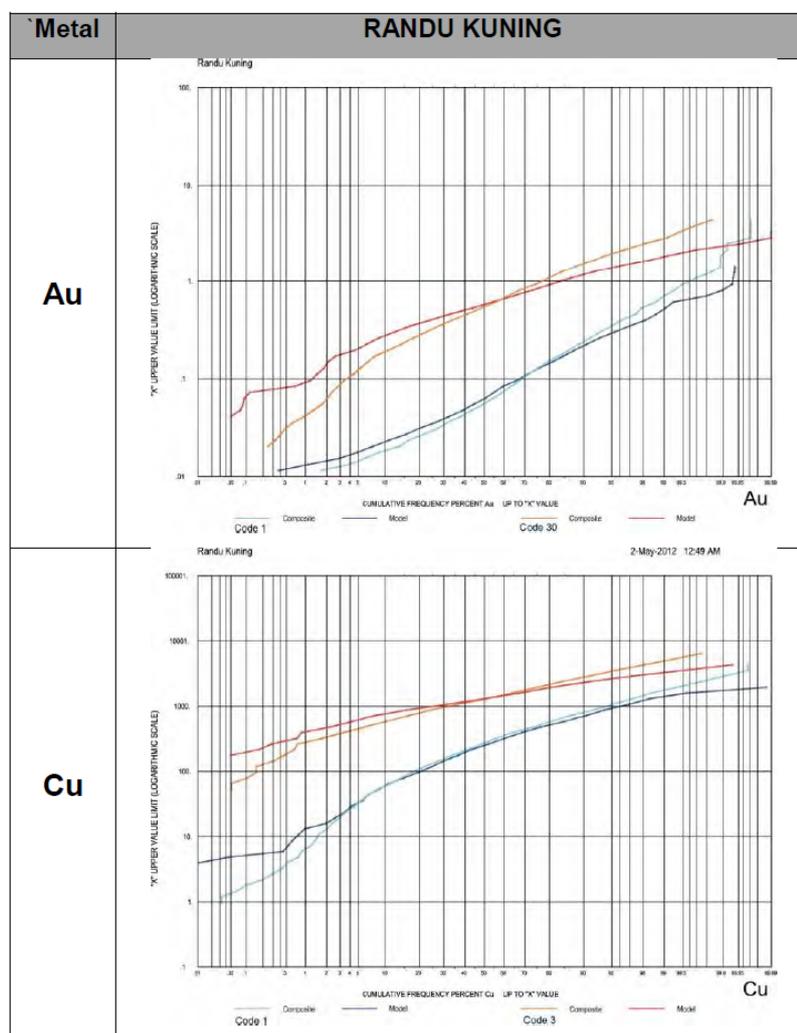
#### Summary of Search Ellipsoid Parameters for Copper

Class	Code	Ellipsoid Dimension			Ellipsoid Orientation			Maximum Search Distance
		Strike	X-Strike	Dip	Strike	Strike Plunge	Dip	
Measured	3	200	100	100	130	0	90	65
Indicated	3	200	100	100	130	0	90	110
Inferred	3	200	100	100	130	0	90	150
Inferred	1	200	100	100	130	0	90	150

#### Model Validation

The models were validated by visual comparison of model sections against drill hole section plots. The tenor and orientation of the grade trends were considered to adequately reflect the original data. This visual comparison is supported by statistical comparison of composite with model statistics which show that the model grades are, on average, within 10-15% of the original data, that they have similar distributions and do not suffer too greatly from regression effects.

Element	Rocktype	Number	Mean	Variance	Log Mean	Minimum	Maximum
Au	30	19,702	0.66	0.14	0.67	0.04	3.81
	1	175,281	0.10	0.01	0.10	0.01	1.63
Cu	3	28,376	1436	397,767	1,443	153	5,844
	1	169,379	334	86,589	370	2	2,474
<b>Comparison with Equivalent Composite Grade (model / composite)</b>							
Au			91%	35%	89%		
			93%	41%	96%		
Cu			93%	41%	93%		
			89%	64%	85%		



## **METALLURGY**

Preliminary metallurgical test work on the Randu Kuning mineralisation suggests that the primary ore can produce a flotation concentrate with saleable copper grades and high gold grades. Since nearly all the deposit is primary and there are suitable smelters to accept this concentrate within 300km by road from Wonogiri, flotation offers a potentially commercial process route with minimal environmental and permitting impacts.

## Flotation Test Work

Five samples were collected for preliminary metallurgical test work in early 2012. Full reports of this test work are available in Metcon's report No. 2546 and a review report by Robert Jenkins of Rofee Pty Ltd, both dated May 2012.

Two of these were oxide and the remaining three were primary sulphides. The three primary samples were composited into a single sample with average grades of 1.26 g/t gold and 0.31% copper. Rougher and cleaner flotation tests were carried out on this composited sample at Metcon's laboratory in Sydney, Australia. The main outcomes were:

- Rougher flotation followed by cleaner flotation produced concentrate with 15% to 18% copper and 60 to 70 g/t gold.
- Recoveries were 85% for copper and 80- 90% for gold.

The reports concluded that the process was bringing a large portion of pyrite into the concentrate which was reducing the copper grade. A test to suppress the pyrite was unsuccessful but there was insufficient sample and time to further optimise the pyrite suppression. Jenkins recommended a number of pyrite suppression methods that could be tried in future tests.

## RESOURCE SUMMARY

The geologic resource is calculated as the summation of all blocks within the metal grade models whose value is greater than or equal to the specified cut-off grade. The resource is categorised as Measured, Indicated and Inferred dependent upon the quality of the information used to define the block's geology and grade.

A Measured Mineral Resource is defined by the Australian JORC code as:

*"that part of a Mineral Resource for which quantity, grade, densities, shape, and physical characteristics are estimated with confidence sufficient to allow the application of Modifying Factors to support detailed mine planning and final evaluation of the economic viability of the deposit."*

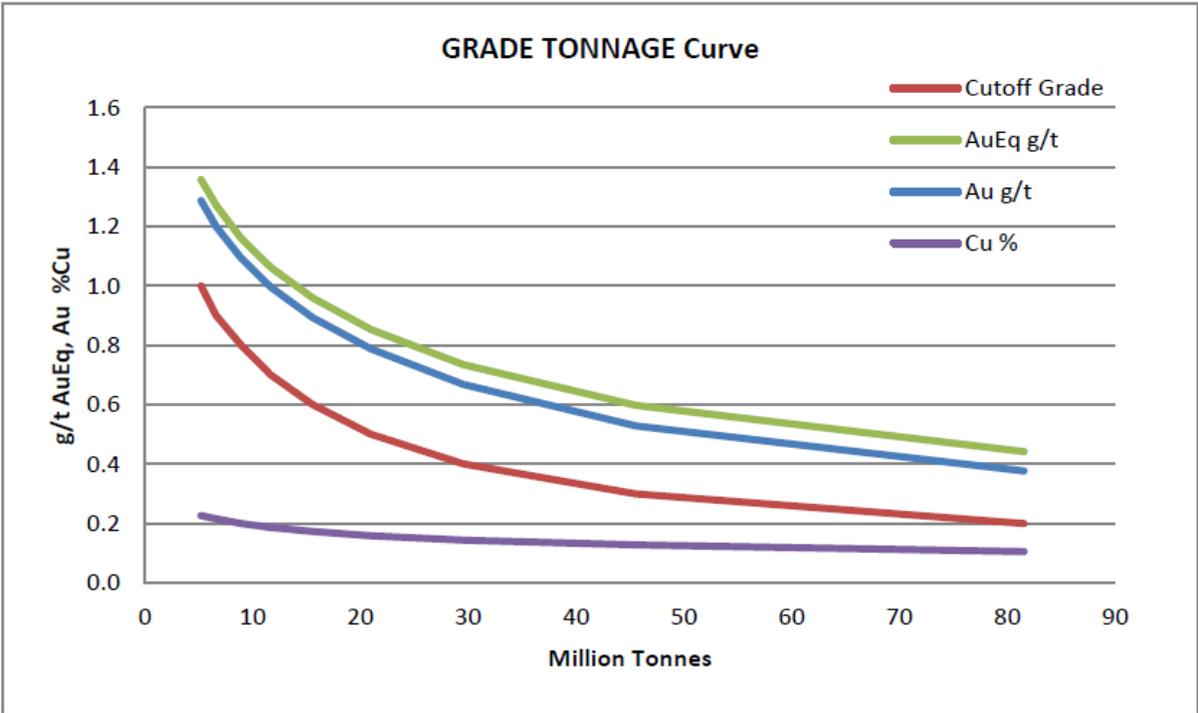
The close spaced diamond drilling at Randu Kuning has enabled good definition of the geologic structure and geostatistical character of the gold-copper mineralisation. As a result of this the grade models are well defined and adequately reflect both tenor and trends in the mineralisation. For resource summary purposes a gold equivalent [AuEq] was calculated from the gold and copper models. The AuEq combines the gold and copper grades weighted by their respective recoveries and using US\$1,250/ounce gold and US\$5,500/tonne copper as metal prices. The equation is:

$$AuEq = (Au\_g/t * \$40.204 * 85\% + Cu\_ppm * \$0.0055 * 85\%) / (\$40.20)$$

The resource was calculated as the tonnage weighted average of all blocks with values greater than or equal to the specified cut-off grade. Tonnages were calculated by applying the average bulk density of 2.7 Kg/m<sup>3</sup> to the block volumes. CAG estimates a resource of 21 million tonnes grading 0.85g/t gold equivalent at a gold equivalent cut-off grade of 0.5 g/t AuEq; comprised of 0.79g/t gold and 0.16% copper. At a 0.2 g/t AuEq cut-off the resource is 81 million tonnes at 0.44g/t AuEq, 0.38g/t Au and 0.16% Cu.

A resource summary by cut-off grade is listed below a Grade-Tonnage curve is presented. Based on drill density and the quality of the exploration database 83% of the resource within the modelled gold and copper zones is categorised as Measured or Indicated based on the interpolation parameters used to estimate the block grade. Any mineralisation outside the modelled zones is categorised as Measured or Indicated based on the interpolation parameters used to estimate the block grade. Any mineralisation outside the modelled zones is categorised as Inferred. Only 5% of the resource is found within the Oxide-Transition zone.

Category	OXIDE				TRANSITION				FRESH				TOTAL			
	Mt	AuEq g/t	Au g/t	Cu %	Mt	AuEq g/t	Au g/t	Cu %	Mt	AuEq g/t	Au g/t	Cu %	Mt	AuEq g/t	Au g/t	Cu %
MEASURED	0.5	1.14	1.06	0.20	0.3	1.21	1.11	0.23	14.8	0.90	0.82	0.17	15.7	0.91	0.83	0.17
INDICATED	0.0	0.65	0.52	0.18	0.0	0.70	0.45	0.27	1.7	0.74	0.73	0.11	1.7	0.74	0.73	0.11
INFERRED	0.0	0.65	0.48	0.21	0.0	0.68	0.35	0.33	3.6	0.67	0.63	0.11	3.6	0.67	0.62	0.12
TOTAL	0.5	1.10	1.02	0.20	0.3	1.20	1.09	0.23	20.1	0.84	0.78	0.16	21.0	0.85	0.79	0.16



## Resource Summary by Classification

Category	cog g/t AuEq	Tonnes Millions	g/t AuEq	g/t Au	% Cu
MEASURED	1.0	4.88	1.36	1.28	0.23
	0.9	6.10	1.28	1.20	0.22
	0.8	7.73	1.18	1.11	0.21
	0.7	10.00	1.09	1.01	0.20
	0.6	12.74	0.99	0.91	0.18
	0.5	15.65	0.91	0.83	0.17
	0.4	18.54	0.84	0.76	0.16
	0.3	20.58	0.79	0.72	0.16
	0.2	21.59	0.77	0.69	0.15
INDICATED	1.0	0.25	1.37	1.39	0.16
	0.9	0.31	1.28	1.29	0.15
	0.8	0.43	1.16	1.17	0.15
	0.7	0.60	1.04	1.04	0.14
	0.6	0.92	0.90	0.89	0.12
	0.5	1.67	0.74	0.73	0.11
	0.4	2.43	0.65	0.64	0.10
	0.3	2.91	0.60	0.58	0.09
	0.2	3.08	0.58	0.56	0.09
INFERRED	1.0	0.10	1.37	1.49	0.09
	0.9	0.19	1.15	1.18	0.13
	0.8	0.80	0.92	0.91	0.13
	0.7	1.10	0.87	0.86	0.12
	0.6	1.90	0.78	0.75	0.12
	0.5	3.64	0.67	0.62	0.12
	0.4	8.59	0.54	0.47	0.12
	0.3	22.07	0.42	0.35	0.11
	0.2	56.89	0.31	0.25	0.09
TOTAL	1.0	5.22	1.36	1.29	0.23
	0.9	6.61	1.27	1.20	0.22
	0.8	8.95	1.16	1.09	0.20
	0.7	11.70	1.06	1.00	0.19
	0.6	15.57	0.96	0.89	0.17
	0.5	20.95	0.85	0.79	0.16
	0.4	29.56	0.73	0.67	0.14
	0.3	45.56	0.60	0.53	0.13
	0.2	81.56	0.44	0.38	0.11

Yours faithfully



Peter J. Nightingale  
Director

pjn8607

## Statement of Compliance

The information in this report that relates to Exploration Results and Mineral Resources is based on information compiled by Augur staff and contractors and approved by Michael C Corey, geoscientist, who is a Member of the Association of Professional Geoscientists of Ontario, Canada. Michael Corey is employed by the Company and has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Michael Corey has consented to the inclusion in this report of the matters based on his information in the form and context in which they appear. Mr Trevor Leahey, of Computer Aided Geoscience Pty Ltd, whom is a consultant to the Company, prepared the updated JORC 2012 Randu Kuning Resource Estimation. Mr Leahey has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Leahey consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

Mineralisation cut-off used for the Wonogiri project is 0.2 Gold Equivalent with a maximum contiguous dilution interval of 4.0 metres. Sample intervals are generally either 1.0 metre or 2.0 metres. Assaying has been completed by PT Intertek Utama Services, a subsidiary of Intertek Group Inc and Pt. Geoservices. Blanks and/or independent standards are used in each sample batch at approximately each 10 sample interval.

2 The Relative Percentage Error [RPE] is used to measure the variability between samples. An unbiased comparison has an average RPE of zero with a minimal spread about this average. The RPE is calculated as:

$$RPE = \frac{AVERAGEVALUE - val_1}{AVERAGEVALUE} * 100\%$$

which for two samples reduces to:

$$RPE = \frac{val_2 - val_1}{val_2 + val_1} * 100\%$$

The RPE is comparable to the HARD statistic of other workers

3 BLD Below Level Detection, for statistical purposes BLD values were replaced by 40% of their nominal value; <0.01 g/t Au by 0.004 and <2ppm Cu by 0.8.

## JORC Code, 2012 Edition – Table 1 report template

### Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> <li>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</li> <li>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</li> <li>Aspects of the determination of mineralisation that are Material to the Public Report.</li> <li>In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</li> </ul>	<ul style="list-style-type: none"> <li>Diamond drill core was logged by geologists for major lithological units and alteration zones to determine sampling intervals. All sample intervals were marked by core blocks, entered into a ledger and assigned a unique sample number. After cutting and sampling detailed logging continued using standardized forms which were entered into the database and verified daily. Diamond drill core samples are collected from electric saw cut half core at intervals generally either 1.0 metre or 2.0 metres.</li> <li>At the site office the core boxes were weighed and photographed (wet and dry), logged, and then marked-up for half-core cutting and sampling by trained technicians. All work was directly supervised by the Site Geologist.</li> <li>Samples were oven dried at 105°C, weighed then jaw crushed to 95% &lt;2mm. A 1.5 kg subsample was riffle split for pulverizing to 95%&lt;200#. Two splits were taken from this product, one for analysis the other for QAQC. Samples were analysed for gold using method FA51, a lead collection fire assay using a 50g charge with an AAS finish. Base metals contents were estimated by method IC01, which used an aqua regia digest with ICP-OES finish.</li> </ul>
Drilling techniques	<ul style="list-style-type: none"> <li>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</li> </ul>	<ul style="list-style-type: none"> <li>Diamond drill including PQ, HQ and NQ core collection utilizing standard triple-tube wire line equipment. Holes are surveyed upon completion using a downhole camera.</li> </ul>
Drill sample recovery	<ul style="list-style-type: none"> <li>Method of recording and assessing core and chip sample recoveries and results assessed.</li> <li>Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> <li>Whether a relationship exists between sample recovery and grade and</li> </ul>	<ul style="list-style-type: none"> <li>Core was cut in half using an electric powered, water cooled diamond blade core cutter located at the site office. Core samples were cut carefully to minimise breakage and to prevent parts of the sample being washed away during cutting. Core intervals that were clay rich and broken or friable were not cut but representatively sampled by spatula and spoon.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p>whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</p>	<ul style="list-style-type: none"> <li>Drilling supervisors informed prior to start of hole where intersection expected.</li> <li>Half core was bagged according to the sample specifications. PQ core was generally sampled in 0.5 metre lengths whilst HQ and NQ core was sampled in 1 metre lengths where mineralised and 2 metre lengths elsewhere. Sampling intervals were constrained to major lithologic boundaries.</li> <li>There is no significant relationship between recovery and grade.</li> <li>Core recovery is measured against run length and averages 97%.</li> </ul>
Logging	<ul style="list-style-type: none"> <li>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> <li>Whether logging is qualitative or quantitative in nature. Core (or coasteam, channel, etc) photography.</li> <li>The total length and percentage of the relevant intersections logged.</li> </ul>	<ul style="list-style-type: none"> <li>Diamond drill core was logged by geologists for lithological units and alteration zones and structural features to determine sampling intervals. All sample intervals were marked by core blocks, entered into a ledger and assigned a unique sample number. After cutting and sampling detailed logging continued using standardized forms which were entered into the database and verified daily. Core logging is both qualitative and quantitative. Core is logged descriptively and codes are used to describe alteration type/ intensity, quartz type and intensity as well as various percentages of minerals. Structural data including veins, shears, fractures are recorded relative to the core axis.</li> <li>Core recovery and RQD are recorded in the Geotechnical log. The average core recovery from 60 drillholes (metres) is 96%. Recoveries of less than 90% are (depending on the cause of reduced recovery) redrilled to obtain better recovery if necessary. At the site office the core boxes were weighed and photographed (wet and dry), logged, and then marked-up for half-core cutting and sampling by trained technicians. All work was directly supervised by the Site Geologist.</li> </ul>
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> <li>If core, whether cut or sawn and whether quarter, half or all core taken.</li> <li>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</li> <li>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> <li>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</li> </ul>	<ul style="list-style-type: none"> <li>Drill core was sawn perpendicular to local structure to ensure representivity.</li> <li>Selected core, based on lithology, alteration and visible mineralization was cut in half using an electric powered, water cooled diamond blade core cutter located at the site office. Half core samples are collected at 1m or in some cases 2 metre intervals. In some cases where 2m sample assays were considered significant (&gt;0.5g/t) the same interval was resampled at 1m</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</li> <li>Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul>	<p>intervals using quarter core.</p> <p>Blanks and/or independent standards are used in each sample batch at approximately each 10 sample interval. Standards were purchased from Ore Research &amp; Exploration Pty Ltd [Bayswater North, Australia]. At the Intertek laboratory samples were oven dried at 105°C, weighed then jaw crushed to 95% &lt;2mm. A 1.5 kg subsample was riffle split for pulverizing to 95%&lt;200#. Two splits were taken from this product, one for analysis the other for QAQC. Samples were analysed for gold using method FA51, a lead collection fire assay using a 50g charge with an AAS finish. Base metals contents were estimated by method IC01, which used an aqua regia digest with ICP-OES finish.</p>
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> <li>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</li> <li>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</li> <li>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</li> </ul>	<ul style="list-style-type: none"> <li>Assaying is completed by PT Intertek Utama Services in Jakarta, a subsidiary of Intertek Group Inc. (accredited for chemical testing under ISO/IEC 17025:2005).</li> <li>A structured Quality-Assurance-Quality-Control program has been conducted during all drill phases. The program has consisted of regular submission of blanks and prepared standards and comparative sample runs with other laboratories. Standards were purchased from Ore Research &amp; Exploration Pty Ltd [Bayswater North, Australia]</li> <li>Assays falling outside of acceptable ranges are re-assayed. Intertek Laboratories also carry out routine internal quality control, and review of this data suggests there are no issues with either precision or accuracy.</li> <li>Separate groups of mineralised sample pulps are sent on a routine basis to other accredited laboratories in Jakarta to test for laboratory scale systematic errors.</li> <li>A full QAQC program was completed using blanks, standards and inter-laboratory checks. There is no significant variation within the assays.</li> </ul>
Verification of sampling and assaying	<ul style="list-style-type: none"> <li>The verification of significant intersections by either independent or alternative company personnel.</li> <li>The use of twinned holes.</li> <li>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</li> <li>Discuss any adjustment to assay data.</li> </ul>	<ul style="list-style-type: none"> <li>In 2011 Corbett Geoscience reviewed the geological /deposit model and also evaluated the assay database and QAQC protocols.</li> <li>As the drilling to date has been entirely by diamond drill no twinned holes have been completed.</li> <li>All field and laboratory data is entered into an Excel database with QA/QC templates included.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Drill databases are stored in industry standard formats in Access. Initial data entry was performed by trained technicians and validated by senior personnel. For modelling purposes drill assays were reloaded into Foxpro databases directly from laboratory csv files using the unique sample number as a primary key.</li> <li>During modelling 11 copper samples were cut to a value of 1%Cu to match the cumulative distribution function.</li> <li>No adjustments to the assay data has occurred.</li> </ul>
Location of data points	<ul style="list-style-type: none"> <li>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</li> <li>Specification of the grid system used.</li> <li>Quality and adequacy of topographic control.</li> </ul>	<ul style="list-style-type: none"> <li>Initially collars are located with hand held GPS devices. Drill collar elevations and hole locations are later recorded with differential GPS equipment by a licensed surveyor.</li> <li>The mapping grid is WGS 84, Zone 49 South. Topographic control is by Lidar survey and differential GPS.</li> </ul>
Data spacing and distribution	<ul style="list-style-type: none"> <li>Data spacing for reporting of Exploration Results.</li> <li>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</li> <li>Whether sample compositing has been applied.</li> </ul>	<ul style="list-style-type: none"> <li>Drilling was undertaken on a nominal 50 x 50m grid with toe spacing at nominal 50m.</li> </ul>
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> <li>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</li> <li>If the relationship between the drilling orientation and the orientation of key mineralized structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</li> </ul>	<ul style="list-style-type: none"> <li>The Randu Kuning mineralization occupies an oblate elliptical annulus around a multiphase intrusion that strikes East-Southeast. Drilling is oriented east-west with both east dipping and west dipping holes. The slight variance in these orientations will not bias the disseminated mineralization that has been modelled for the deposit. High grade structural trends that are known to occur have not been adequately tested by the drilling. These trends have not been included in the model and may provide a bonus to the resource.</li> </ul>
Sample security	<ul style="list-style-type: none"> <li>The measures taken to ensure sample security.</li> </ul>	<ul style="list-style-type: none"> <li>Drill samples were under the direct supervision of company personnel from drilling at site, through sample preparation up until delivery to the assay laboratory in Jakarta.</li> <li>Intertek standard sample submission forms were cross-checked with Sample Receipt Confirmation notes issued by the Laboratory. Laboratory results were emailed to the site office as well as the corporate offices in Jakarta and Sydney.</li> </ul>

Criteria	JORC Code explanation	Commentary
Audits or reviews	<ul style="list-style-type: none"> <li>The results of any audits or reviews of sampling techniques and data.</li> </ul>	<ul style="list-style-type: none"> <li>An audit of sampling techniques and the drill database was completed as part of the resource study.</li> </ul>

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> <li>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</li> <li>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</li> </ul>	<ul style="list-style-type: none"> <li>The 3,928 hectare Wonogiri Property tenure is under the Indonesian National Izin Usaha Pertambangan or Mining Business License (IUP) system. The Wonogiri IUP (545.21/054/2009) is held 100% by PT Alexis Perdana Mineral ('Alexis'). Augur's subsidiary, Wonogiri Pty Ltd, directly holds a 90% interest in Alexis.</li> <li>The IUP is currently in the process of transfer to an IUP Exploitation license expected before January 2017.</li> <li>There are no forestry restrictions over the IUP nor any social or environmental issues known.</li> <li>There are no known impediments to exploration and mining development.</li> </ul>
Exploration done by other parties	<ul style="list-style-type: none"> <li>Acknowledgment and appraisal of exploration by other parties.</li> </ul>	<ul style="list-style-type: none"> <li>Diamond drilling by PT Oxindo in 2009-10 intersected 40m grading 1.1g/tAu, 0.3%Cu from 92m and 15m at 1.6g/tAu, 0.2%Cu from 137m in WG001, and 37m at 1.8g/tAu, 0.2%Cu from 458m in drillhole WG002.</li> </ul>
Geology	<ul style="list-style-type: none"> <li>Deposit type, geological setting and style of mineralisation.</li> </ul>	<ul style="list-style-type: none"> <li>The Randu Kuning deposit consists of a mineralized polyphasal carapace breccia sitting astride a polyphasal diorite / micro-diorite intrusion. The deposit is one of a number of mineralized occurrences within the Mioocene-Pliocene aged Sunda Banda Arc.</li> </ul>
Drill hole	<ul style="list-style-type: none"> <li>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill</li> </ul>	<ul style="list-style-type: none"> <li>See Appendix A, this report.</li> </ul>

Criteria	JORC Code explanation	Commentary
Information	<ul style="list-style-type: none"> <li>holes: <ul style="list-style-type: none"> <li>easting and northing of the drill hole collar</li> <li>elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>dip and azimuth of the hole</li> <li>down hole length and interception depth</li> <li>hole length.</li> </ul> </li> <li>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</li> </ul>	
Data aggregation methods	<ul style="list-style-type: none"> <li>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.</li> <li>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</li> <li>The assumptions used for any reporting of metal equivalent values should be clearly stated.</li> </ul>	<ul style="list-style-type: none"> <li>Assay data was drillhole composited to 2.5m, using length weighted averaging, to reduce sample variance in the population without unduly affecting the form of the distribution.</li> </ul>
Relationship between mineralisation widths and intercept lengths	<ul style="list-style-type: none"> <li>These relationships are particularly important in the reporting of Exploration Results.</li> <li>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> <li>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').</li> </ul>	<ul style="list-style-type: none"> <li>The mineralization consists of a broad zone of disseminated material displaying gradational boundaries with the host material. There is no confusion of geometry with drillhole intercept angle.</li> </ul>
Diagrams	<ul style="list-style-type: none"> <li>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</li> </ul>	<ul style="list-style-type: none"> <li>See Appendix B, this report</li> </ul>
Balanced reporting	<ul style="list-style-type: none"> <li>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</li> </ul>	<ul style="list-style-type: none"> <li>Summary statistics are listed in the relevant section of this report.</li> </ul>

Criteria	JORC Code explanation	Commentary
Other substantive exploration data	<ul style="list-style-type: none"> <li>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</li> </ul>	<ul style="list-style-type: none"> <li>All pertinent information is included in the report.</li> </ul>
Further work	<ul style="list-style-type: none"> <li>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</li> <li>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</li> </ul>	<ul style="list-style-type: none"> <li>Not applicable.</li> </ul>

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	<ul style="list-style-type: none"> <li>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</li> <li>Data validation procedures used.</li> </ul>	<ul style="list-style-type: none"> <li>Assay data was loaded directly from laboratory text files.</li> <li>Statistical analysis and hard copy plotting of all data in plan &amp; section view to check for inconsistencies in distribution</li> </ul>
Site visits	<ul style="list-style-type: none"> <li>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</li> <li>If no site visits have been undertaken indicate why this is the case.</li> </ul>	<ul style="list-style-type: none"> <li>No site visit was completed. The field work was supervised by known colleagues with substantial field experience in this environment and style of mineralization.</li> </ul>
Geological interpretation	<ul style="list-style-type: none"> <li>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</li> <li>Nature of the data used and of any assumptions made.</li> <li>The effect, if any, of alternative interpretations on Mineral Resource estimation.</li> <li>The use of geology in guiding and controlling Mineral Resource estimation.</li> <li>The factors affecting continuity both of grade and geology.</li> </ul>	<ul style="list-style-type: none"> <li>3D domains of gold and copper mineralization were built from section and plan view interpretations of the assay and geological data. These domains show good continuity between drillhole intersections.</li> <li>The domains were used to control data selection for the interpolation process.</li> </ul>

Criteria	JORC Code explanation	Commentary
Dimensions	<ul style="list-style-type: none"> <li>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</li> </ul>	<ul style="list-style-type: none"> <li>The copper and gold domains have plan view dimensions of 350x180m and extend from surface for 500m. The model changes from a pipe to an annulus around RL50, equivalent to 200m below surface. The domains strike SSE and plunge near vertically.</li> </ul>
Estimation and modelling techniques	<ul style="list-style-type: none"> <li>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</li> <li>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</li> <li>The assumptions made regarding recovery of by-products.</li> <li>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterization).</li> <li>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</li> <li>Any assumptions behind modelling of selective mining units.</li> <li>Any assumptions about correlation between variables.</li> <li>Description of how the geological interpretation was used to control the resource estimates.</li> <li>Discussion of basis for using or not using grade cutting or capping.</li> <li>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</li> </ul>	<ul style="list-style-type: none"> <li>Grades were estimated using an Inverse Distance algorithm working within a scaled and oriented search ellipsoid defined by variography and geology. Block grades were estimated from 2.5m composites of like geology code (i.e. ore for ore, waste for waste) selected by sector search from within the ellipsoid. A minimum of 3 composites was required for a determination from a maximum of 18 (3 per sector for 6 sectors).</li> <li>This report upgrades a previous JORC estimate by CAG in 2012.</li> <li>There are no significant recovery by-products.</li> <li>No information is currently available on AMD.</li> <li>The block size of 10x10x5m represents a selective mining unit of 1,350 tonnes equivalent to 6 truckloads in a small scale open pit. The block size represents 20% of the drill data spacing.</li> <li>The interpreted copper and gold domains were used to code the composites and the block geology.</li> <li>Gold grades were not cut as they formed a single log-normal population. A small number of copper samples, in excess of 1% were cut to 1% to ensure a single homogenous log-normal population for copper.</li> <li>The topography, rock and grade models were validated using statistical techniques and visual scanning of hard copy plots to ensure the models were a reasonable representation of the original data.</li> </ul>
Moisture	<ul style="list-style-type: none"> <li>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</li> </ul>	<ul style="list-style-type: none"> <li>Tonnages are estimated on a dry basis.</li> </ul>
Cut-off parameters	<ul style="list-style-type: none"> <li>The basis of the adopted cut-off grade(s) or quality parameters applied.</li> </ul>	<ul style="list-style-type: none"> <li>Cutoff grades were selected to reflect mining operations of comparable deposits.</li> </ul>
Mining factors or assumptions	<ul style="list-style-type: none"> <li>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when</li> </ul>	<ul style="list-style-type: none"> <li>The deposit has potential to be mined by bulk mining methods from an open pit. Metal extraction could use either Carbon-In-Leach technology to recover gold only or Flotation to recover a copper-gold concentrate.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p>estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</p>	
Metallurgical factors or assumptions	<ul style="list-style-type: none"> <li>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>Preliminary metallurgical testwork has identified recoveries of 85% for copper and 80- 90% for gold.</li> </ul>
Environmental factors or assumptions	<ul style="list-style-type: none"> <li>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>Environmental impacts will be included as Modifying Factors in the Mining Reserve report</li> </ul>
Bulk density	<ul style="list-style-type: none"> <li>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</li> <li>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</li> <li>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</li> </ul>	<ul style="list-style-type: none"> <li>Bulk Density was estimated using large (core-tray scale) samples. This natural estimate incorporates both void and moisture observations.</li> <li>Detailed check measurements of wax-coated core specimens were taken by Intertek using the specific gravity method.</li> <li>As there is no significant statistical difference between the sub-populations the average SG of 2.7 has been used in the tonnage estimate.</li> </ul>
Classification	<ul style="list-style-type: none"> <li>The basis for the classification of the Mineral Resources into varying confidence categories.</li> <li>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</li> <li>Whether the result appropriately reflects the Competent Person's view of the deposit.</li> </ul>	<ul style="list-style-type: none"> <li>Classification into confidence categories based on interpolation parameters which adequately reflect the changing drill density with depth. The majority of the mineral resource is categorized as Measured &amp; Indicated in response to the tight drill density and confidence in the geologic model.</li> </ul>

Criteria	JORC Code explanation	Commentary
Audits or reviews	<ul style="list-style-type: none"> <li>The results of any audits or reviews of Mineral Resource estimates.</li> </ul>	<ul style="list-style-type: none"> <li>No external audit of the Mineral Resource estimate has been undertaken.</li> </ul>
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> <li>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</li> <li>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</li> <li>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</li> </ul>	<ul style="list-style-type: none"> <li>The Mineral Resource estimate is believed to meet industry standards of accuracy and confidence as the spatial data distribution on which it is calculated is well within the geostatistical range of the mineralization (based on variography), the assay quality meets/exceeds industry standards and the geological interpretation is a reasonable interpretation of the available data.</li> <li>Various interpolation methods and geological orientations of the search ellipsoid were tested to map the grade distribution, including indicator and ordinary kriging. The final IDS method produced the most reasonable representation of the raw data.</li> <li>The Mineral Resource is a global estimate of the contained mineralization within the deposit. Summary figures for mineralization above cutoff grade provide an indication of the percentage of the deposit that could be economic under various economic scenarios which may/may not be specified. These summary figures are calculated as the sum of block tonnages for blocks whose grade is in excess of the specified cutoff, with the average grade as a tonnage weighted estimate of the block grades.</li> </ul>

#### Section 4 Estimation and Reporting of Ore Reserves

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	<ul style="list-style-type: none"> <li>Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.</li> <li>Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.</li> </ul>	<ul style="list-style-type: none"> <li><b>NOT APPLICABLE TO THIS REPORT</b></li> </ul>

#### Section 5 Estimation and Reporting of Diamonds and Other Gemstones

Criteria	JORC Code explanation	Commentary
Indicator minerals	<ul style="list-style-type: none"> <li>Reports of indicator minerals, such as chemically/physically distinctive garnet, ilmenite, chrome spinel and chrome diopside, should be prepared by a suitably qualified laboratory.</li> </ul>	<ul style="list-style-type: none"> <li><b>NOT APPLICABLE TO THIS REPORT</b></li> </ul>