



## ASX RELEASE

19 November 2013

# HIGH GRADE URANIUM RESOURCE CONFIRMED AT EXPANDED WILUNA PROJECT

Toro Energy Limited (ASX: TOE) is pleased to confirm a significant resource upgrade at the expanded Wiluna Uranium Project, incorporating the Lake Maitland Uranium Project acquired today.

### Key highlights<sup>1</sup>

- 27% increase in the previously reported high grade Lake Maitland U<sub>3</sub>O<sub>8</sub> resource to 15.7 Mlb (at 500 ppm cut-off).
- Lake Maitland adds scale and quality to **pre-acquisition** Resources at Wiluna. The total Resource base is reported as:
  - **42.3 Mlb at 898 ppm** (500 ppm cut-off) including **36.7 Mlb at 930 ppm** from the first four planned mines – Centipede, Lake Way, Millipede and Lake Maitland; and
  - **76.5 Mlb at 479 ppm** (200 ppm cut-off).
- Higher grade mine development able to be pursued at the Centipede, Lake Way, Millipede and Lake Maitland deposits – 97% of resource from these deposits is now categorised as Measured or Indicated.

The Wiluna Uranium Project now comprises six deposits – the already approved Centipede and Lake Way deposits, as well as Millipede, Lake Maitland, Dawson Hinkler and Nowthanna.

This resource update incorporates all drilling data and re-interpretation of previous resource models at Lake Maitland and the results of the Company's 2013 drilling campaign at the Dawson Hinkler deposit.

The results confirm high grade inventory is contained within at least four of Wiluna's deposits – Centipede, Lake Way, Millipede and Lake Maitland - and is of sufficient scale to suggest the potential to pursue a high grade mining strategy for the first 10-13 years of operations at Wiluna at a 1.3 million tonne per annum processing rate. Total Measured and Indicated Resource at a 500 ppm cut-off is 17.6 Mt @ 930 ppm for 36.0 Mlb.

Figure 1 shows the resource shells for the Lake Maitland deposit, which highlight the continuity of the high grade mineralisation that significantly improves the scale and quality of the Wiluna Resource.

*"The acquisition of Lake Maitland is a critical step in the development of the Wiluna Project. Toro Managing Director, Dr Vanessa Guthrie, said today. The potential for a higher grade mining operation at 800+ ppm head grade may now be realised from the initial four mines at Wiluna (the already approved Centipede and Lake Way deposits, as well as Millipede and Lake Maitland).*

<sup>1</sup> All Resource information is quoted in accordance with the 2012 JORC code. Refer to the attached compliance statements.

*“With the addition of lower grade stockpiled material from these mines, as well as the resources at Dawson Hinkler and Nowthanna deposits, we have the resource base capable of supporting mining operations at Wiluna for more than 20 years.”*

Toro has commenced initial mining studies and economic modelling to provide a basis for design for a definitive feasibility study on the new enlarged and improved Wiluna Project.

The 2013 drilling program at Dawson Hinkler has resulted in a small increase in total resource whilst converting at least two thirds of the Resource into the Indicated category.

Figure 1 and Tables 1 and 2 provide details of the resource estimates.

**Vanessa Guthrie**  
Managing Director

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Toro Energy is a modern Australian uranium company with progressive project development, acquisition and growth. The company is based in Perth, Western Australia.

Toro’s flagship and wholly-owned Wiluna uranium project is located southeast of Wiluna in Central Western Australia.

Toro’s wholly owned Theseus Project is a recent discovery with results to date indicating the potential for a high grade mineralised system. The Company also owns uranium assets in the Northern Territory and in joint venture in Namibia, Africa.

**Competent / Qualified Persons’ Statements**

*The information presented here that relates to Mineral Resources of the Centipede, Millipede, Lake Way, Lake Maitland, Dawson Hinkler and Nowthanna deposits is based on information compiled by Dr Greg Shirliff of Toro Energy Limited (with the aid of Mega Uranium Limited geologists Mr Stewart Parker and Mr Robin Cox in the case of Lake Maitland) and Mr Robin Simpson and Mr Daniel Guibal of SRK Consulting (Australasia) Pty Ltd. Mr Guibal takes overall responsibility for the Resource Estimate, and Dr Shirliff takes responsibility for the integrity of the data supplied for the estimation. Dr Shirliff is a Member of the Australasian Institute of Mining and Metallurgy (AusIMM), Mr Guibal is a Fellow of the AusIMM and Mr Simpson is a Member of the Australian Institute of Geoscientists (AIG) and they have sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity they are undertaking to qualify as Competent Persons as defined in the 2012 Edition of the ‘Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code 2012)’. The Competent Persons consent to the inclusion in this release of the matters based on the information in the form and context in which it appears.*

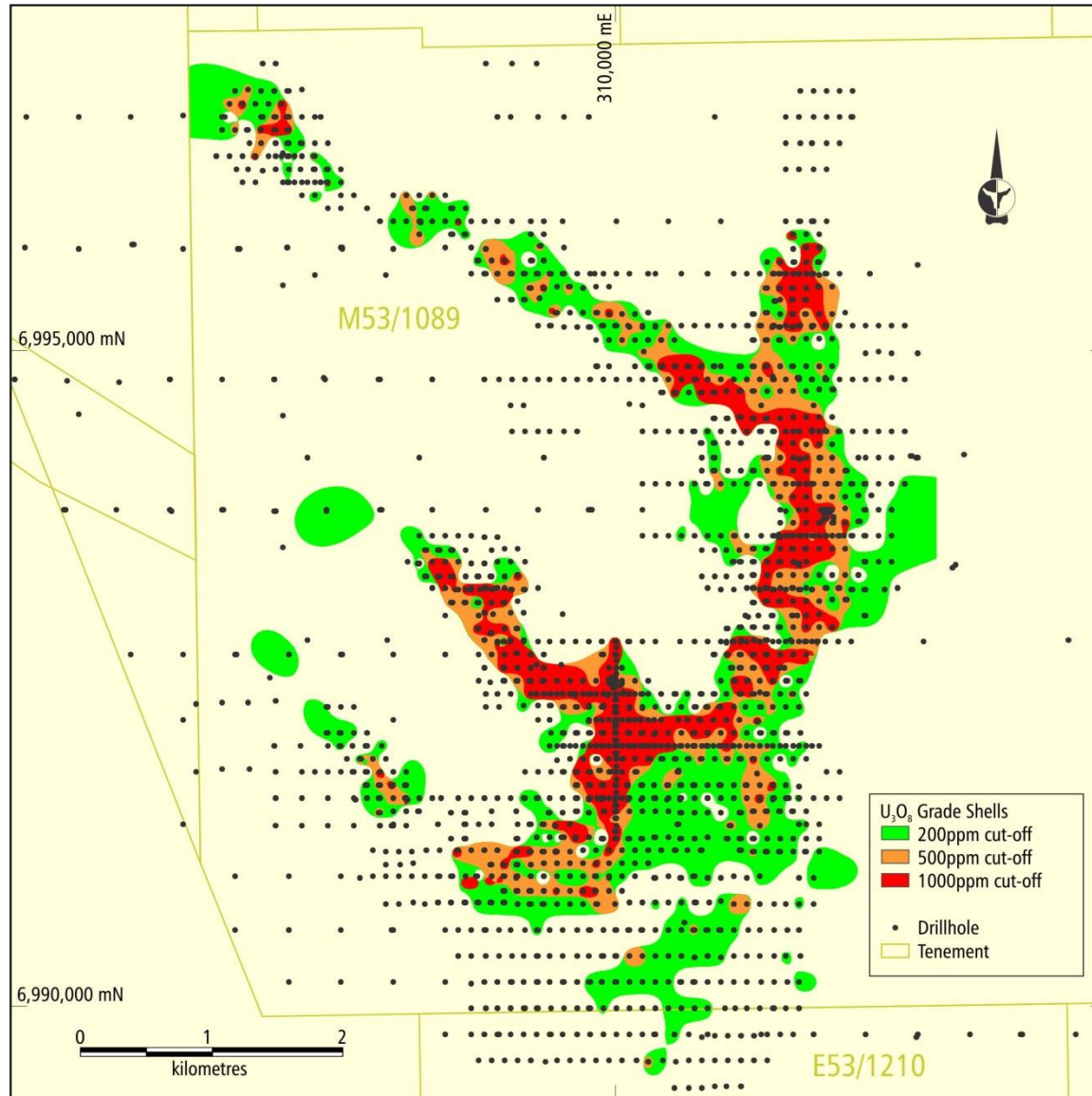


Figure 1 Resource grade shells for the Lake Maitland deposit - plan view of a Leapfrog generated model

## New Resource Estimate Details<sup>2</sup>

Table 1 – November 2013 – Wiluna Uranium Project Resources (500 ppm U<sub>3</sub>O<sub>8</sub> cut-off)

November 2013 - The Wiluna Uranium Project																
500PPM U3O8 cut-off																
Deposit	JORC code	Measured			Indicated			Total Measured and Indicated			Inferred			Total		
		Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>	Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>	Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>	Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>	Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>
Centipede	2012	1.2	872	2.3	3.1	943	6.5	4.3	923	8.8	-	-	-	4.3	923	8.8
Lake Way	2012	-	-	-	4.2	883	8.2	4.2	883	8.2	-	-	-	4.2	883	8.2
Millipede	2012	-	-	-	1.6	956	3.3	1.6	956	3.3	0.4	887	0.7	1.9	943	4.0
Lake Maitland	2012	-	-	-	7.5	956	15.7	7.5	956	15.7	-	-	-	7.5	956	15.7
Sub-total		1.2	872	2.3	16.3	935	33.7	17.6	930	36.0	0.4	887	0.7	17.9	930	36.7
Dawson Hinkler	2012	-	-	-	0.9	596	1.1	0.9	596	1.1	0.3	628	0.4	1.1	603	1.5
Nowthanna	2012	-	-	-	-	-	-	-	-	-	2.3	794	4.1	2.3	794	4.1
Total Regional Resource		1.2	872	2.3	17.2	918	34.8	18.4	915	37.1	2.9	791	5.1	21.4	898	42.3

Table 2 – November 2013 - Wiluna Uranium Project Resources (200 ppm U<sub>3</sub>O<sub>8</sub> cut-off)

November 2013 - The Wiluna Uranium Project																
200PPM U3O8 cut-off																
Deposit	JORC code	Measured			Indicated			Total Measured and Indicated			Inferred			Total		
		Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>	Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>	Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>	Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>	Tonnes M's	Grade PPM	Mlb's U <sub>3</sub> O <sub>8</sub>
Centipede	2012	2.9	551	3.5	7.5	572	9.5	10.4	566	13.0	-	-	-	10.4	566	13.0
Lake Way	2012	-	-	-	10.3	545	12.3	10.3	545	12.3	-	-	-	10.3	545	12.3
Millipede	2012	-	-	-	4.5	530	5.3	4.5	530	5.3	1.9	382	1.6	6.4	486	6.9
Lake Maitland	2012	-	-	-	19.9	555	24.3	19.9	555	24.3	-	-	-	19.9	555	24.3
Sub-total		2.9	551	3.5	42.2	553	51.4	45.1	553	55.0	1.9	382	1.6	47.0	546	56.6
Dawson Hinkler	2012	-	-	-	8.4	336	6.2	8.4	336	6.2	5.2	282	3.2	13.6	315	9.4
Nowthanna	2012	-	-	-	-	-	-	-	-	-	11.9	399	10.5	11.9	399	10.5
Total Regional Resource		2.9	551	3.5	50.6	517	57.7	53.5	519	61.2	19.0	365	15.3	72.5	479	76.5

<sup>2</sup> Tonnes and pounds are quoted to one decimal place which may cause rounding errors when tabulating.

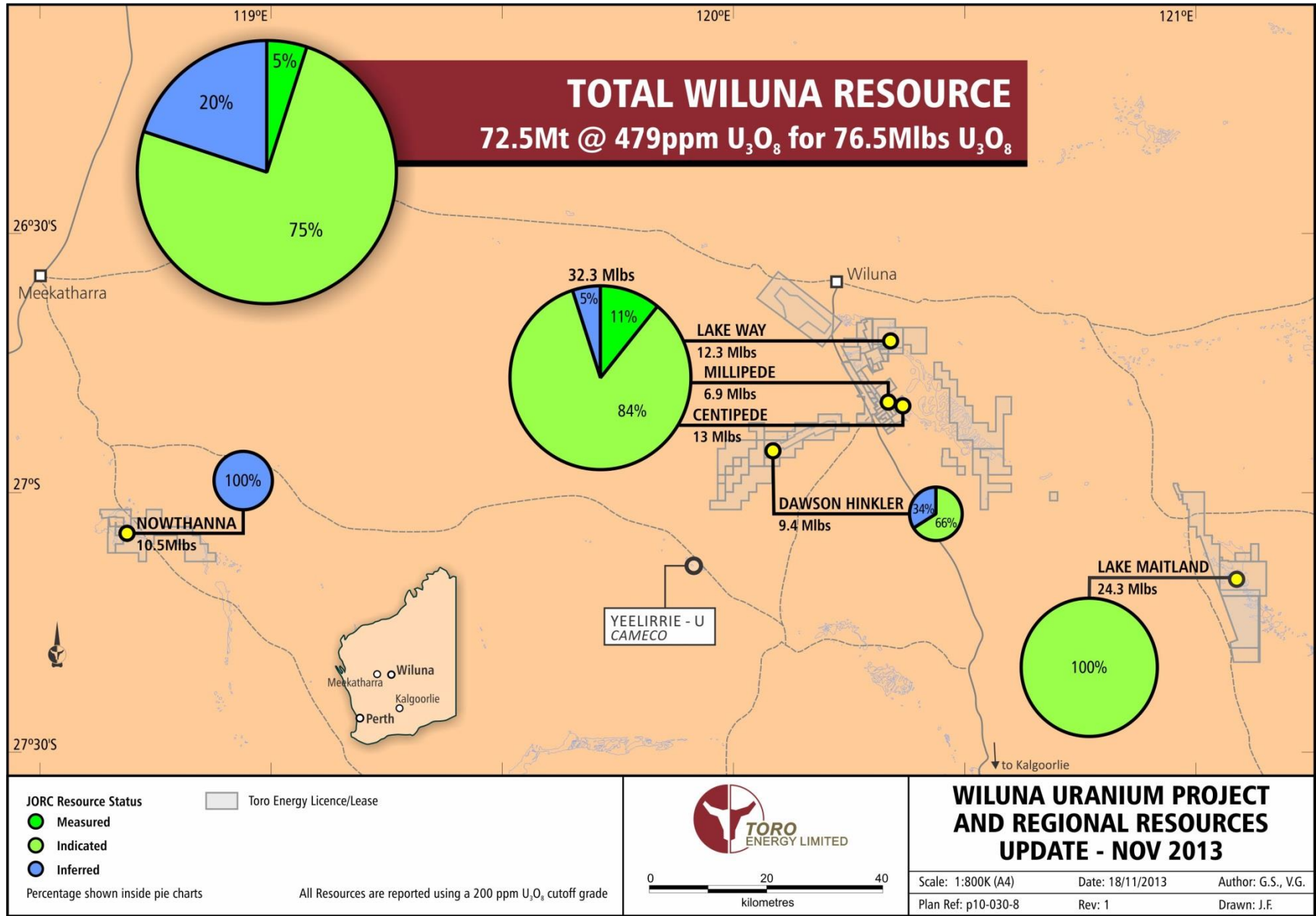


Figure 2 Total Wiluna Uranium Project Resource Inventory (200 ppm cut-off)

# JORC Code, 2012 Edition – Table 1 report – Lake Maitland deposit only

## Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> <li>• <i>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i></li> <li>• <i>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</i></li> <li>• <i>Aspects of the determination of mineralisation that are Material to the Public Report.</i></li> <li>• <i>In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</i></li> </ul>	<ul style="list-style-type: none"> <li>• <math>U_3O_8</math> values are calculated from U values derived from both geochemistry and down-hole gamma radiation measurements.</li> <li>• <b>Geochemistry</b> – Mega's geochemical samples on the Lake Maitland deposits represent 0.25 m full core lengths of 83 mm diamond drill core (PQ3). Weights of the geochemical samples range from 2-5 kg approximately. Intervals are determined during core mark-up and identified with plastic core blocks. Samples are dried at 110 °C before weighing and then crushing. After crushing a sub-sample is split using a rotary splitter for milling (pulverizing) to 90% passing 75 micron, before taking an aliquot for U analysis by 4 acid digest ICPMS. All samples with ICPMS results for U above 500 ppm were then re-analysed by fused disc XRF so that all <math>U_3O_8</math> values from the extensive 2011 drilling program used in the estimation were from fused disc -XRF if at or above 500 ppm or 4 acid digest ICPMS if below 500 ppm.</li> <li>• Due to full core sampling no duplicates are needed to measure in-field sampling error. Duplicates are instead taken at the first sample split at the lab, directly after the initial crush, these duplicates are taken with a rotary splitter after pushing the sample back through the crusher after the initial split at a rate of 1 in 20 or 5% of all non-standard samples. Differences in U concentrations between the duplicates and their corresponding samples are used to produce a mean standard sampling error (results from 2011 are below 10% error).</li> <li>• Lab duplicates are taken at every stage of the sub-sampling process prior to analysis at the rate of 1 in 20.</li> <li>• Geochemical samples are taken through the entire length of each drill hole. The 0.25 m intervals are determined from marking up 0.25 m intervals down the full length of the core from the surface.</li> <li>• Other elements analysed include Ba, Th, Al, Ca, Fe, K, Mg, Mn, S, Sr, Ti and V.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>• Depth corrections are made to geochemistry samples where appropriate, these are based on comparing the down-hole geochemistry to the down-hole gamma U values and assuming the down-hole depth as measured by the gamma probe during probing is correct. Winch cable stretch is not considered an issue at Lake Maitland drilling due to the shallow depth of (3-9 m on average). No depth corrections were deemed necessary in the most recent and extensive drilling program (2011).</li> <li>• <b>Gamma derived eU<sub>3</sub>O<sub>8</sub></b> – Mega uses a 33 mm Auslog natural gamma probe (S691) 'in-house', to measure down-hole gamma radiation. Measurements are made every 1 or 2 cm with a logging speed of approximately 2 m per minute.</li> <li>• The gamma probes are used on all drill holes, diamond, sonic and aircore.</li> <li>• Prior to the drilling program all gamma probes are calibrated at the Adelaide Calibration Model pits in Adelaide, South Australia. During probing operations selected holes are logged twice as a duplicate log. Some selected holes across the deposits are used as reference holes for relogging to detect drift in the instrument during each program.</li> <li>• Probing is done as close as practicable after drilling.</li> <li>• Gamma measurements are converted to equivalent U<sub>3</sub>O<sub>8</sub> values (eU<sub>3</sub>O<sub>8</sub>) by an algorithm that takes into account the probe and crystal used, density, hole diameter, ground water where applicable and PVC pipe thickness.</li> <li>• Down-hole gamma probe data is also deconvolved to more accurately reflect what would be expected in nature for down-hole response (gamma curves).</li> <li>• All gamma data is compared with geochemistry data both via down-hole comparisons and overall populations bivariate analysis, and distribution analysis to check for potential error or disequilibrium. To adequately compare with geochemistry gamma probe data is composited into 0.25 m composites at the same intervals represented by the corresponding geochemical samples.</li> <li>• Significant differences between gamma derived eU<sub>3</sub>O<sub>8</sub> and geochemical U<sub>3</sub>O<sub>8</sub> have been noted in 2011 and historically. Disequilibrium analysis by an independent consultant group (On Site Technology Pty. Ltd.) found a global positive disequilibrium across</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>the entire deposit of 1.18 (average). This factor that was confirmed by the comparison of assays to eU values has been applied to all eU<sub>3</sub>O<sub>8</sub> used in the estimation.</p>
<p><i>Drilling techniques</i></p>	<ul style="list-style-type: none"> <li><i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i></li> </ul>	<ul style="list-style-type: none"> <li>Diamond, sonic, auger core and air core drilling techniques have all been utilized on the Lake Maitland deposit.</li> <li>The sonic drilling utilizes a 100mm core barrel (inside diameter) with outside casing where needed, producing a 150mm hole diameter and 100mm core. Depending on the ground conditions and thus quality of core being produced, core is retrieved from the 3m barrel in either 1 to 3m length, 1m at a time. Upon exiting the barrel, core is transferred into tubular plastic bags that fit the core before being placed in core trays. On occasions where the sonic core was being used for density measurements a hard plastic (clear) cylinder that fits the core was used instead to ensure lasting core integrity.</li> <li>Aircore drilling is conventional with a 72mm bit producing an approximate 100mm diameter hole.</li> <li>Diamond drilling is PQ3, which utilizes an 83.18 mm core barrel (inside diameter) and produces an 83 mm diameter core with an approximate 123 mm diameter hole.</li> </ul>
<p><i>Drill sample recovery</i></p>	<ul style="list-style-type: none"> <li><i>Method of recording and assessing core and chip sample recoveries and results assessed.</i></li> </ul>	<ul style="list-style-type: none"> <li>Sonic core recoveries are estimated based on the drillers direction to definitive lost core, observations made on quality of sample during geological logging and sample weight comparisons to average weights and rock type. It should be noted that precise core recovery estimation on sonic drillcore at Lake Maitland is inherently difficult due to expansion and contraction of soft sediments during drilling and during recovery of core from the barrel.</li> <li>Historically, chip sample recoveries have not been recorded in the database.</li> <li>Diamond core recoveries have been determined by conventional techniques of identification of loss core by driller and geologist at the rig and during core mark up and measure. Core trays are also weighed without and then with core to estimate core recovery based on assumed SG for particular lithology.</li> </ul>
	<ul style="list-style-type: none"> <li><i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i></li> </ul>	<ul style="list-style-type: none"> <li>During sonic core drilling core loss is minimized by 'casing as we drill' through all ore zones or any zone where the geological information is critical such as for geotechnical purposes.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li><i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i></li> </ul>	<ul style="list-style-type: none"> <li>To date Toro cannot find any correlation between estimated core loss and grade in the Lake Maitland data.</li> <li>Grade in geochemical samples is also checked against composited gamma derived grades (see above), which acts as another check on errors in the geochemistry that may (or may not) be due to core recovery.</li> </ul>
Logging	<ul style="list-style-type: none"> <li><i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i></li> <li><i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i></li> <li><i>The total length and percentage of the relevant intersections logged.</i></li> </ul>	<ul style="list-style-type: none"> <li>Geology is not used in the resource estimation process other than to apply density to individual blocks in the block model post-estimation. The reasons for this are explained in more detail below, however, basically the deposit has been found to be correlated more to groundwater and depth from the surface than to any geological unit. Thus the geological logging is adequate for resource estimation.</li> <li>Current geological logging (both on-ground logging by Mega geologists and interpretation of down-hole spectral mineralogical analysis via Hy-logger) is considered to be adequate for the stage of mine planning that Toro is currently at on the Wiluna Project and as such with the Lake Maitland deposit.</li> <li>Current logging is both qualitative (subjective geological opinion of rock type and colour and objective mineral identification by spectral analysis) and quantitative (recording of specific depth intervals and percentages and quantification of mineralogy by spectral analysis via Hy-logger). Core photographs have been taken for the entire 2011 drilling program, which consists of a total of 201 holes and is spread across the entirety of the deposit.</li> <li>Historical costeans were not always geologically logged. Geological logs of more recent costeans reported in the 2009 Annual Report were found to be consistent with lithological logging from drill holes. In some circumstances photographs of costean walls were taken and stored on the company drive.</li> <li>All drilling intersections have been logged geologically.</li> </ul>

Criteria	JORC Code explanation	Commentary
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> <li>• <i>If core, whether cut or sawn and whether quarter, half or all core taken.</i></li> <li>• <i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i></li> <li>• <i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i></li> <li>• <i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i></li> <li>• <i>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</i></li> <li>• <i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i></li> </ul>	<ul style="list-style-type: none"> <li>• As described above, geochemical samples represent 0.25 m full core lengths of 100mm sonic drill core or 83mm diamond core.</li> <li>• Sample preparation has been described above under 'sampling techniques', it is considered that all sub-sampling and lab preparations are consistent with other laboratories in Australia and overseas and are satisfactory for the intended purpose.</li> <li>• Lab duplicates are taken by the lab to test their own sub-sampling techniques, for full core geochemical samples the lab duplicate taken at the first split after the initial crush (sampled with a rotary splitter) is used by Mega to calculate the sampling error.</li> <li>• See above in 'sampling techniques' for procedures - Total sampling errors for the first split at the lab in case of full core sampling are typically 5% but no more than 10%.</li> <li>• The laboratory used for Mega's geochemical analysis of all samples from Lake Maitland bases all crushing grain sizes and subsequent sub-sampling weights on being inside accepted Gy safety lines for sample representivity. These grains sizes and sub-sample weights have been described above under 'sampling techniques'.</li> </ul>
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> <li>• <i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i></li> </ul>	<ul style="list-style-type: none"> <li>• In the extensive 2011 diamond drilling program a four acid digest followed by ICPMS was employed for analysis for U geochemistry (ALS laboratories, Perth)– this was assumed to be an almost total rock digest technique although with recognition that highly resistant minerals are sometimes not entirely digested. Due to these potential issue and the fact that ICPMS has in earlier times had issues dealing with high U concentrations due to dilution factors (etc), the Mega geologists decided to re-analyse all samples with ICPMS results for U of greater than 500 ppm utilizing the XRF technique at the same laboratory (ALS, Perth), regarded by Mega geologists as a better whole rock technique. Performance against standards is acceptable.</li> <li>• Historical geochemistry data is almost entirely XRF.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>• <i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i></li> <li>• <i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Down-hole gamma tools are used as explained above. All tools are Auslog natural gamma probes calibrated at the Adelaide Calibration Model pits in Adelaide, South Australia.</li> <li>• “Off the shelf” OREAS U standards are used to check analyses at the lab at a rate of 2% or 1 in 50 samples.</li> <li>• Coarse quartz sand is used as blanks and these are used at a rate of 2% or 1 in 50 samples.</li> <li>• Lab duplicates are used as already explained in detail above, from the primary crush stage and every other sub-sampling stage.</li> <li>• Limited laboratory checks have been made – from the most recent drilling (2011) a total of 138 samples were re-analysed for U by 4 acid digest ICPMS by a different commercial laboratory (Genalysis, Perth). The samples were chosen as representative of the following U<sub>3</sub>O<sub>8</sub> concentrations – 10% between 100 and 200 ppm U<sub>3</sub>O<sub>8</sub>, 40% from between 200 and 500 ppm U<sub>3</sub>O<sub>8</sub>, and 50% from above 500 ppm U<sub>3</sub>O<sub>8</sub>. Differences between the labs were satisfactory, the largest being approximately 5% on average higher values from the XRF derived U<sub>3</sub>O<sub>8</sub> by ALS over the ICPMS U<sub>3</sub>O<sub>8</sub> by Genalysis, this was taken into consideration during estimations.</li> </ul>
<p><i>Verification of sampling and assaying</i></p>	<ul style="list-style-type: none"> <li>• <i>The verification of significant intersections by either independent or alternative company personnel.</i></li> <li>• <i>The use of twinned holes.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Limited interlab geochemistry analytical checks are completed for each drilling campaign, the last interlab check is explained directly above in “quality of assay data and laboratory checks”. Mega has two calibrated (at the Adelaide Calibration Model pits in Adelaide, South Australia) Auslog gamma probes to check the probing results achieved by a single probe.</li> <li>• A limited number of holes have been twinned. These include twinned holes drilled by both sonic and diamond core methods.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li><i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i></li> <li><i>Discuss any adjustment to assay data.</i></li> </ul>	<ul style="list-style-type: none"> <li>All primary data (gamma log las files, geochemical sample lists, final collar files, geological logs, core photographs, electronic geochemical results, driller's plods, probing plods, deconvolved gamma files, gamma gamma density logs, disequilibrium analysis results etc) are stored on the company server in the appropriate drive and folders. At this moment in time not all of the Mega folder system has been transferred to Toro Energy. Any hardcopy data, such as official geochemistry results or any paper copy geological logs, are kept in hardcopy in folders and archives.</li> <li>Data entry procedures are described in some detail below in section 3 under 'data integrity'.</li> <li>To date, there have been no adjustments made to geochemical assay <math>U_3O_8</math> data (or to any other elements).</li> <li>Based on the findings from a disequilibrium analysis by On Site Technologies Pty Ltd in 2011 all gamma data used in the estimation has been multiplied by 1.18, the average positive disequilibrium found across the deposit. It is important to note that this has not been applied to the <math>eU_3O_8</math> data within the database, it has only been applied to data during the estimation process.</li> </ul>
<p><i>Location of data points</i></p>	<ul style="list-style-type: none"> <li><i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i></li> <li><i>Specification of the grid system used.</i></li> <li><i>Quality and adequacy of topographic control.</i></li> </ul>	<ul style="list-style-type: none"> <li>At the end of the drilling campaigns all collars are picked up using RTK GPS by an external qualified surveyor (MHR Surveyors) for the final collar locations that are entered into the database. Accuracy of the GPS as defined by the surveyor is 50 mm both on the horizontal and the vertical.</li> <li>Due to all drill holes being shallow (approximately 3-9 m deep) and vertical no down-hole surveying is required.</li> <li>The grid system used on the Lake Maitland deposit is Geocentric Datum of Australia (GDA) 94, zone 51.</li> <li>Topographic control is largely achieved by the DGPS with base station. As stated above this gives good and adequate accuracy for the resource estimation. Drill hole collar 3D locations also have expected spatial relationships with geomorphology on aerial photographs. All holes are checked for topographic correlation prior to estimation during the data analysis phase, where needed they are</li> </ul>

Criteria	JORC Code explanation	Commentary
		'pinned' to a topographic surface created from the most recent and accurate (and trusted) collar surveys. A total of 328 holes within the bounds of the estimation envelope had to be 'pegged' to a modelled surface in this way.
<i>Data spacing and distribution</i>	<ul style="list-style-type: none"> <li><i>Data spacing for reporting of Exploration Results.</i></li> <li><i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i></li> <li><i>Whether sample compositing has been applied.</i></li> </ul>	<ul style="list-style-type: none"> <li>No exploration results, resource drilling only.</li> <li>The data spacing and distribution (drilling grids on average of 100m x 100 m and in some places as close as 5 m x 5 m) has been considered appropriate for the Mineral Resource estimation procedures and classifications applied to this Lake Maitland estimation by the external consultant doing the resource and is based mainly on variography and continuity shown in the statistical analysis of the data. See below in resource section for further information.</li> <li>Sample compositing to 0.25 m composites has been applied to the 1 and 2 cm interval eU3O8 data to match the 0.25 m geochemical core samples.</li> </ul>
<i>Orientation of data in relation to geological structure</i>	<ul style="list-style-type: none"> <li><i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i></li> <li><i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i></li> </ul>	<ul style="list-style-type: none"> <li>Sampling is non-subjective down-hole sampling from the surface, either at 1 cm or 2 cm intervals in the case of gamma probe data or 0.25 m samples in the case of geochemistry. Historical geochemistry represents a similar non-bias down-hole process. The sampling orientation employed provides no bias to the groundwater related distribution of mineralization.</li> <li>No bias suspected, ore lenses are horizontal and drilling is vertical, cutting mineralization at an approximate right angle (90 degrees).</li> </ul>
<i>Sample security</i>	<ul style="list-style-type: none"> <li><i>The measures taken to ensure sample security.</i></li> </ul>	<ul style="list-style-type: none"> <li>Core length is measured by drillers and blocks are put in at the end of runs. The core is then picked up by the geologist at the end of hole and taken to the core shed where it is divided into 25cm whole samples and allocated a sample ID tag, this is done by the geologist and field assistant. The core is then logged and core loss is recorded. Core, in the core trays, is then stacked on to pallets (approximately 3 holes per pallet). For sample security, steel lids are used on the top row of trays before the entire pallet is plastic wrapped and steel strapped. Core was then picked up at site and delivered to ALS Perth, where it underwent spectral logging, weighing and assay.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>• Additionally, upon transfer of the database from Mega to Toro for estimation, all data was converted to raw text files and delivered directly to SRK for the data review prior to estimation so as to avoid any loss of information by converting files into different database formats (Toro and Mega use different databases and database structures).</li> </ul>
<p><i>Audits or reviews</i></p>	<ul style="list-style-type: none"> <li>• <i>The results of any audits or reviews of sampling techniques and data.</i></li> </ul>	<ul style="list-style-type: none"> <li>• A review by Toro geologists of the Mega drill core sampling techniques (both for geochemistry and gamma measurements [gamma gamma for density and gamma for eU<sub>3</sub>O<sub>8</sub> calculations) for the 2011 drilling program found no errors that would affect the resource estimate in any significant way. The spectral analysis based geological model, which has been used to assign density in the block model was found to be highly predictive across the deposit with a limited amount of drill holes, however given the nature of the deposit as shown in a review of multi-element geochemistry (by Toro geologists) and Toro's experience with all of the similar style Wiluna deposits, the model is considered by Toro to be a reasonable interpretation of Lake Maitland geology and in fact in most circumstances a more accurate representation of the geology and geological relationships.</li> <li>• SRK reviewed the database that was to be used for the resource estimation and excluded any errors from the estimation. The number of exclusions was considered too small to have affected the estimation.</li> </ul>

## Section 2 Reporting of Exploration Results

NOT APPLICABLE TO THIS RESOURCE UPDATE

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	<ul style="list-style-type: none"> <li>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</li> <li>Data validation procedures used.</li> </ul>	<ul style="list-style-type: none"> <li>All geological logging and sampling is entered into a Toughbook laptop with an offline aQuire data entry program, which contains fixed lithological codes, carry over sample ID's, fixed core lengths and recorded core loss intervals. The program does not allow errors such as overlaps, or sample miss match. At the end of each day (whether for gamma data from probing or geological logging) all data is extracted and sent to the Perth office where it is automatically entered to the sequel server database. This can only be accessed by the externally based database manager, Dusan Dammer of Advanced Data Care Pty. Ltd. or the Mega geologist in charge of Lake Maitland.</li> <li>All data has undergone a thorough 2 week long validation and integrity check by SRK in consultation with Toro Energy prior to data preparation for resource estimation, including all U<sub>3</sub>O<sub>8</sub> and eU<sub>3</sub>O<sub>8</sub> values, density values, lithology and lithology models (Vector files etc) and geospatial information (drill hole collars etc).</li> </ul>
Site visits	<ul style="list-style-type: none"> <li>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</li> <li>If no site visits have been undertaken indicate why this is the case.</li> </ul>	<ul style="list-style-type: none"> <li>The competent person responsible for the resource estimate, Daniel Guibal, has not had a visit to site. It is considered that a site visit is not necessary given Mr Guibal's experience with The Lake Maitland deposits in the past (2009 resource estimate) and some 6 years estimating Toro's other Wiluna uranium deposits.</li> </ul>
Geological interpretation	<ul style="list-style-type: none"> <li>The use of geology in guiding and controlling Mineral Resource estimation.</li> </ul>	<ul style="list-style-type: none"> <li>The geological model is not used in the resource estimate since it has been found that mineralization is not necessarily correlated to any particular rock type, despite being often associated with carbonate or carbonated sediments. The mineralization has been found to be associated with the water table and so is more correlated to depth from the surface than any given lithology, maintaining grade across different lithologies. Thus the geological model for estimation is a simple mineralization envelope based on a concentration of U that represents that concentration where the background population of U ends and the U mineralization exists (in a classic bimodal distribution). In the Wiluna deposits this is 70 ppm U<sub>3</sub>O<sub>8</sub> for the Centipede and Millipede deposits and 80 ppm U<sub>3</sub>O<sub>8</sub> for the Lake Way,</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"><li>• <i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i></li><li>• <i>Nature of the data used and of any assumptions made.</i></li></ul>	<p>Dawson Hinkler and Nowthanna deposits. At Lake Maitland, this has been determined to be 100 ppm <math>U_3O_8</math>.</p> <ul style="list-style-type: none"><li>• Examination of 3D LeapFrog models of different grade shells of the resource give a high level of confidence to the above interpretation of a ground water controlled deposit.</li><li>• No geological data used in estimation, all data used is based on U values from deconvolved gamma derived equivalents and geochemistry. U geochemistry is mostly 4 acid digest ICPMS and fused disc XRF. A large number of cored drill holes (diamond and sonic) have been used to test the validity of the gamma measurements (via geochemistry) – for example all of the 2011 drilling, some 201 diamond holes. Where there is geochemistry data available it is given priority over gamma derived equivalents in the resource estimation. Prior to estimation all deconvolved gamma derived data has been multiplied by 1.18 according to the average positive disequilibrium found by independent research (see above for further details).</li><li>• The advantage of using a mineralization envelope based on U concentrations only (both chemistry and deconvolved gamma derived equivalents) is that there are no assumptions made. Domains are based on variance within the data and so in effect, real changes in the behavior of the data and data distribution, there is no forcing statistical predictions into domains based on lithology that is not necessarily correlated spatially at all times.</li><li>• Density values used in the resource estimate are derived from gamma gamma probe measurements calibrated to real wet and dry density measurements of reference sonic hole cores. The densities are averaged to the different main lithologies in the geological model and applied to the block model according to within the boundaries of each lithological unit (acting as density domains). Further information below under 'bulk density'.</li><li>• A different geological interpretation, if used in the resource estimate, may affect the results of the resource estimate slightly, however, since geology is not used in estimations a change in geological interpretations would make no difference.</li></ul>
	<ul style="list-style-type: none"><li>• <i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i></li></ul>	



Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li><i>The factors affecting continuity both of grade and geology.</i></li> </ul>	<ul style="list-style-type: none"> <li>Grade Continuity can be affected by numerous factors, including drilling density, which varies from 5m x 5m to 100m x 200m, nugget effect, itself linked to the type of measurement (geochemical data are more variable than deconvolved radiometric data), uncertainties on the data themselves due to calibration problems or/and disequilibrium for the radiometric values, sampling/assaying issues for the geochemical measurements (controlled by QA/QC), and geological continuity, which is reasonably established at Lake Maitland</li> </ul>
<i>Dimensions</i>	<ul style="list-style-type: none"> <li><i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i></li> </ul>	<ul style="list-style-type: none"> <li>The Lake Maitland deposit is surficial with a vertical thickness of less than approximately 8 meters</li> </ul>
<i>Estimation and modelling techniques</i>	<ul style="list-style-type: none"> <li><i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i></li> </ul>	<ul style="list-style-type: none"> <li>Estimation technique is Uniform Conditioning using the specialised geostatistical software, Isatis. The various steps of the estimation are as following: <ol style="list-style-type: none"> <li>1) Use of combined radiometric and geochemical data, after correction of the radiometric data to take into account the average disequilibrium (the radiometric value of eU3O8 is multiplied by 1.18), with priority given to geochemistry in the case when both exist,</li> <li>2) Creation of a mineralisation envelope using Leapfrog 3D at a cut-off of 100 ppm eU3O8 to define the hanging wall and the footwall</li> <li>3) Compositing to 0.5m</li> <li>4) Domaining in 3 zones defined essentially by the strike orientation: NS, NE and NW</li> <li>5) No top-cuts used.</li> <li>6) Block model based on 50m x 50m x 0.5m panels. The panel sizes are chosen in relation to the average drilling density</li> <li>7) Ordinary Kriging estimation of panels, after neighbourhood analysis to optimise quality of kriging.</li> <li>8) Validation of Kriging results through statistics and swath plots</li> <li>9) Uniform conditioning (UC) for 10m x 10m x 0.5m Selective Mining Units (SMU), which is a realistic assumption for a future operation where</li> </ol> </li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>• <i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i></li>   <li>• <i>The assumptions made regarding recovery of by-products.</i></li>   <li>• <i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i></li>   <li>• <i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i></li>   <li>• <i>Any assumptions behind modelling of selective mining units.</i></li>   <li>• <i>Any assumptions about correlation between variables.</i></li>   <li>• <i>Description of how the geological interpretation was used to control the resource estimates.</i></li> </ul>	<p>grade control using radiometric information will be possible.</p> <p>10) Localised Uniform Conditioning: creation of a 10m x 10m x 0.5m block model based on the results of UC.</p> <ul style="list-style-type: none"> <li>• Previous resource estimates (public 2009 estimate by SRK - Mr Daniel Guibal and Mr Peter Gleeson, and in-house non-public check estimates with the aid of various consultants) have been available to both Toro and SRK and are considered in the current estimation.</li>   <li>• No by-products are assumed to be recovered nor are any planned to be recovered.</li>   <li>• Currently there are no geostatistical estimations made on deleterious elements, however, such elements have been included in the analysis of drill core samples from the 2011 drilling campaign and so such estimations will be able to be accomplished in the future. Current analysis of drill core geochemistry and Metallurgical samples strongly suggests there are no significant economic issues related to deleterious elements and materials within the ore targeted by Toro Energy at Lake Maitland.</li>   <li>• See above</li>   <li>• See above</li>   <li>• No assumptions</li>   <li>• See above – no geological control used in estimation, just for applying density across the deposit as explained above.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>• <i>Discussion of basis for using or not using grade cutting or capping.</i></li> <li>• <i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i></li> </ul>	<ul style="list-style-type: none"> <li>• See above</li> <li>• See above</li> </ul>
Moisture	<ul style="list-style-type: none"> <li>• <i>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The tonnage are estimated using a constant dry density per lithology, based on the average value of existing measurements</li> </ul>
Cut-off parameters	<ul style="list-style-type: none"> <li>• <i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Grade-tonnage curve are provided for a range of cut-offs. Optimal cut-off will be determined from the mining studies.</li> </ul>
Mining factors or assumptions	<ul style="list-style-type: none"> <li>• <i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The Lake Maitland deposit will be incorporated into Toro Energy's greater Wiluna Project, which includes the Centipede, Millipede, Lake Way, Dawson Hinkler and Nowthanna deposits further to the north and northwest. Therefore, to a large extent the proposed mining methods, metallurgy/processing and environmental management/factors will be the same as those publically outlined by Toro for the Wiluna Project. Any differences specific to Lake Maitland are noted where necessary.</li> <li>• Mining technique has been tested successfully on site, the main points follow.</li> <li>• Shallow strip mining to 15m maximum depth (approximately 8 m at Maitland) using a combination of a Vermeer surface miner, loader and articulated trucks.</li> <li>• 25-50cm benches</li> <li>• De-watering of pits for process water</li> <li>• In-pit tailings disposal below natural ground surface in lined pits,</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>progressive compartmental mining, tailings and rehabilitation</p> <ul style="list-style-type: none"> <li>• Current - strip 3.8:1, using 250 ppm cut-off</li> <li>• Up to a 14 year life of mine, regional resources increase to 20+ years dependent on future approvals</li> <li>• 5 years at Centipede followed by Lake Way – Lake Maitland at some point subsequent to these deposits.</li> </ul>
<i>Metallurgical factors or assumptions</i>	<ul style="list-style-type: none"> <li>• <i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The Lake Maitland deposit will be incorporated into Toro Energy's greater Wiluna Project, which includes the Centipede, Millipede, Lake Way, Dawson Hinkler and Nowthanna deposits further to the north and northwest. Therefore, to a large extent the proposed mining methods, metallurgy/processing and environmental management/factors will be the same as those publically outlined by Toro for the Wiluna Project. Any differences specific to Lake Maitland are noted where necessary.</li> <li>• Laboratory scale pilot plant has been successfully trialled that includes all of the currently proposed process from crushing/grinding to product – actual product produced. Every part of the processing circuit has been tested and/or had research associated with it. Main factors follow.</li> <li>• Alkaline tank leach with direct precipitation.</li> <li>• Target production is 780 tpa U<sub>3</sub>O<sub>8</sub></li> <li>• Processing 1.3 Mtpa at a head grade of 716 ppm U<sub>3</sub>O<sub>8</sub></li> <li>• Processing facility to be located near to the Centipede deposit.</li> </ul>
<i>Environmental factors or assumptions</i>	<ul style="list-style-type: none"> <li>• <i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The Lake Maitland deposit will be incorporated into Toro Energy's greater Wiluna Project, which includes the Centipede, Millipede, Lake Way, Dawson Hinkler and Nowthanna deposits further to the north and northwest. Therefore, to a large extent the proposed mining methods, metallurgy/processing and environmental management/factors will be the same as those publically outlined by Toro for the Wiluna Project. Any differences specific to Lake Maitland are noted where necessary.</li> <li>• Two of the Wiluna deposits have been approved for mining by the West Australian EPA as part of the Wiluna Uranium Project and thus the project has gone through the Environmental Review and Management Programme process (The ERMP and all of the</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>associated documents can be found on the Toro Energy website at <a href="http://www.toroenergy.com.au/sustainability/health-safety/environmental-review-and-management-programme-erp/">http://www.toroenergy.com.au/sustainability/health-safety/environmental-review-and-management-programme-erp/</a></p> <p>Main factors follow.</p> <ul style="list-style-type: none"> <li>• Shallow open pit mining</li> <li>• Progressive compartmental mining and rehabilitation.</li> <li>• In-pit tailings disposal in lined pits</li> <li>• Tailings integrity modelled for 10,000 years</li> <li>• Mining footprint returned as close as practicable to natural land surface level</li> <li>• No standing landforms remain post closure</li> </ul>
<i>Bulk density</i>	<ul style="list-style-type: none"> <li>• <i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i></li> <li>• <i>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i></li> <li>• <i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Density determined by calibrated gamma gamma probe measurements down drill holes from across the entirety of the deposit (predominantly the 2011 drilling campaigns). Gamma gamma probe calibrated directly with reference sonic core holes whereby both dry and wet density measurements were obtained. Gamma gamma measurements were found to be matching wet density and so all measurements were re-calibrated to a dry density using both the wet and dry density determinations on the sonic core. Density was then averaged over geological units (determined as explained above) so that each geological domain within the block model had a single average dry density.</li> </ul>
<i>Classification</i>	<ul style="list-style-type: none"> <li>• <i>The basis for the classification of the Mineral Resources into varying confidence categories.</i></li> <li>• <i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i></li> <li>• <i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The classification as Indicated is based on the consideration of drill spacing, existence of geochemical data in such numbers that the radiometric data are well supported and finally the quality of the estimation as measured by kriging slope of regression.</li> <li>• Average drill hole spacing within the resource as determined to be Indicated is 100 m x 100 m, however there are two locations where drill hole spacing is down to 5m x 5 m.</li> </ul>
<i>Audits or reviews</i>	<ul style="list-style-type: none"> <li>• <i>The results of any audits or reviews of Mineral Resource estimates.</i></li> </ul>	<ul style="list-style-type: none"> <li>• There has been no external audit of this mineral resource estimate by SRK other than internal Toro assessment and geological interpretation.</li> </ul>

Criteria	JORC Code explanation	Commentary
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> <li>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</li> <li>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</li> </ul>	<ul style="list-style-type: none"> <li>As mentioned, the classification is partly based on the quality of kriging. In addition, since 2005, various drilling campaigns took place at Lake Maitland and there has been a good consistency of the estimates</li> <li>There is clearly more uncertainty at the individual panel level. Other factors having an impact on the estimation are: Disequilibrium: current measurements (2011) suggest that a significant positive disequilibrium exists. This has been established at 1.186 by consultant On Site Technologies and confirmed by further Golder Associates analysis of downhole gamma work compared with laboratory analysis of diamond core.</li> <li>The relationship between radiometric values and geochemical data can be variable at the local scale.</li> <li>The assaying methods, as there are indications that XRF tends to overestimate grades by about 5% (by comparison to 4 acid digest ICPMS).</li> <li>The cut-off grades: due to the estimation method (UC), the high cut-off grades (over 500 ppm) which depend on the modelling of the tail of the grade distributions are more uncertain at local level.</li> </ul>
	<ul style="list-style-type: none"> <li>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</li> </ul>	<ul style="list-style-type: none"> <li>No production statistics available – not an operating mine.</li> </ul>

## Section 4 Estimation and Reporting of Ore Reserves

NOT APPLICABLE – NO RESERVES REPORTED

## Section 5 Estimation and Reporting of Diamonds and Other Gemstones

NOT APPLICABLE – URANIUM ONLY

# JORC Code, 2012 Edition – Table 1 report – Dawson Hinkler Deposit Only

## Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> <li>• <i>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i></li> <li>• <i>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</i></li> <li>• <i>Aspects of the determination of mineralisation that are Material to the Public Report.</i></li> <li>• <i>In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</i></li> </ul>	<ul style="list-style-type: none"> <li>• U<sub>3</sub>O<sub>8</sub> values are calculated from U values derived from both geochemistry and down-hole gamma radiation measurements.</li> <li>• <b>Geochemistry</b> – Toro's geochemical samples on all of the Wiluna deposits (inclusive of Dawson Hinkler) represent 0.5m half core lengths (prior to 2013) or full core lengths (2013 and planned into the future) of 100mm sonic drill core. Full core samples provide an 8-10kg sample to the lab, half core samples are half this weight approximately. After crushing the lab splits a 2.5 kg sub-sample for milling (pulverizing) to 90% passing 75micron, before taking an aliquot for U analysis by 4 acid digest ICPMS (prior to 2013) or fusion-ICPMS (2013 and into the future).</li> <li>• In the case of half core samples field duplicates of the core are taken to ensure sample representivity, these field duplicates are the other half of the core that has been sampled. In the case of full core samples, duplicates are taken at the first sample split at the lab, directly after the initial crush, these duplicates are taken with a rotary splitter after pushing the sample back through the crusher after the initial split. It should be noted that due to the size of the sample supplied to the lab, the initial crushing is a two-step process, a primary crush to 10mm and a secondary crush to 3mm. Both these duplicates are taken at a rate of 1 in 20 or 5% of all non-standard samples. Differences in U concentrations between the duplicates and their corresponding samples are used to produce a mean standard sampling error.</li> <li>• Lab duplicates are taken at every stage of the sub-sampling process prior to analysis at the rate of 1 in 20.</li> <li>• Geochemical samples are taken through the ore zones as determined by hand-held scintillometers and if available at the time of sampling, down-hole gamma measurements. The half metre intervals are determined from marking up half metre intervals down the full length of the core from the surface. This is completed at the rig so that any</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>drilling issues can be observed and the geologist can have direct communication 'on the spot' with the driller. To gain geochemical and mineralogical information of waste material or for metallurgical purposes etc, often the entire hole is sampled for geochemistry and a larger suite of elements are analysed for, some having to employ different analytical techniques.</p> <ul style="list-style-type: none"> <li>• Depth corrections are made to geochemistry samples where appropriate, these are based on comparing the down-hole geochemistry to the down-hole gamma U values and assuming the down-hole depth as measured by the gamma probe during probing is correct. Winch cable stretch is not considered an issue in the Wiluna drilling due to the shallow depth of almost all drilling (maximum depth of approximately 25m).</li> <li>• <b>Gamma derived eU<sub>3</sub>O<sub>8</sub></b> – Toro uses Auslog natural gamma probes, either in-house or from external contractors, to measure down-hole gamma radiation. Measurements are made every 2 cm with a logging speed of 3.5m per minute.</li> <li>• The gamma probes are used on all holes, which include sonic holes also used for geochemical sampling and air core holes drilled specifically for gamma probe measurements. 100mm sonic core holes are usually 150mm in diameter and air core holes are usually 100mm in diameter. Approximately 95% of all holes are aircore.</li> <li>• Prior to the drilling program all gamma probes are calibrated at the Adelaide Calibration Model pits in Adelaide, South Australia. During probing operations every 10<sup>th</sup> hole is logged twice as a duplicate log. Selected holes across the deposits are used as reference holes for relogging to detect drift in the instrument during each program. In 2013 over 50% of all holes drilled at Dawson Hinkler were re-logged with a different probe (from the same contractor) over 3 months after they were drilled to confirm results (results were confirmed).</li> <li>• As protection from hole collapse and to protect the probe, all logging is done inside 40mm or 50mm PVC pipe (unless larger diameter has been used for water bores) with an average wall thickness of 1.9 mm.</li> <li>• Gamma measurements are converted to equivalent U<sub>3</sub>O<sub>8</sub> values (eU<sub>3</sub>O<sub>8</sub>) by an algorithm that takes into account the probe and crystal used, density, hole diameter, ground water where applicable and PVC pipe thickness.</li> </ul>



Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Down-hole gamma probe data is also deconvolved to more accurately reflect what would be expected in nature for down-hole response (gamma curves).</li> <li>All gamma data is compared with geochemistry data both via down-hole comparisons and overall populations bivariate analysis, and distribution analysis to check for potential error or disequilibrium. To adequately compare with geochemistry gamma probe data is composited into half metre composites at the same intervals represented by the corresponding geochemical samples.</li> </ul>
<i>Drilling techniques</i>	<ul style="list-style-type: none"> <li><i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i></li> </ul>	<ul style="list-style-type: none"> <li>Both sonic and aircore drilling techniques are utilized on the Wiluna Project.</li> <li>The sonic drilling utilizes a 100mm core barrel (inside diameter) with outside casing where needed, producing a 150mm hole diameter and 100mm core. Depending on the ground conditions and thus quality of core being produced, core is retrieved from the 3m barrel in either 1 to 3m length, 1m at a time. Upon exiting the barrel, core is transferred into tubular plastic bags that fit the core before being placed in core trays.</li> <li>Aircore drilling is conventional with a 72mm bit producing an approximate 100mm diameter hole.</li> </ul>
<i>Drill sample recovery</i>	<ul style="list-style-type: none"> <li><i>Method of recording and assessing core and chip sample recoveries and results assessed.</i></li> <li><i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i></li> <li><i>Whether a relationship exists between sample recovery and grade</i></li> </ul>	<ul style="list-style-type: none"> <li>Chip sample recoveries are not recorded as the chips are not used for any systematic analysis of uranium concentrations.</li> <li>Sonic core recoveries are estimated based on the drillers direction to definitive lost core, observations made on quality of sample during geological logging and sample weight comparisons to average weights and rock type. It should be noted that precise core recovery estimation on sonic drillcore in the Wiluna deposits is inherently difficult due to expansion and contraction of soft sediments during drilling and during recovery of core from the barrel.</li> <li>Core loss is minimized by 'casing as we drill' through all ore zones or any zone where the geological information is critical such as for geotechnical purposes.</li> <li>There is no correlation between estimated core loss and grade</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p><i>and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i></p>	<ul style="list-style-type: none"> <li>Grade in geochemical samples is also checked against composited gamma derived grades (see above), which acts as another check on errors in the geochemistry that may (or may not) be due to core recovery.</li> </ul>
Logging	<ul style="list-style-type: none"> <li><i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i></li> <li><i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i></li> <li><i>The total length and percentage of the relevant intersections logged.</i></li> </ul>	<ul style="list-style-type: none"> <li>Geology is not used in the resource estimation process, the reasons for this are explained in more detail below, however, basically the deposit has been found to be correlated more to groundwater and depth from the surface than to any geological unit. Thus the geological logging is adequate for resource estimation.</li> <li>Current geological logging (all Toro, 2013 onwards at Dawson Hinkler) is considered to be adequate for the stage of mine planning that Toro is currently at on the Wiluna Project. Further work is considered necessary to amalgamate or align historical geology logs and geology to current. This can be achieved with the results of the 2013 drilling campaign, which was Toro's largest at Wiluna and first on the Dawson Hinkler deposit.</li> <li>Current logging is both qualitative (subjective geological opinion of rock type and colour) and quantitative (recording specific depth intervals and percentages of grain sizes). Core photographs are taken for each individual metre (prior to 2013) and half metre (2013) after core has been split down the middle for logging and so as to see sedimentological features for logging (avoiding clay smear on outer surface of core made by drill rods).</li> <li>Toro has not costeamed at Dawson Hinkler.</li> </ul>
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> <li><i>If core, whether cut or sawn and whether quarter, half or all core taken.</i></li> <li><i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i></li> <li><i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i></li> </ul>	<ul style="list-style-type: none"> <li>As described above, geochemical samples represent 0.5m half core lengths (prior to 2013) or full core lengths (2013 and planned into the future) of 100mm sonic drill core. Aircore chips were not sampled for geochemistry.</li> <li>Sample preparation has been described above under 'sampling techniques, it is considered that all sub-sampling and lab preparations are consistent with other laboratories in Australia and overseas and are satisfactory for the intended purpose.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>• <i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i></li> <li>• <i>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</i></li> <li>• <i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Lab duplicates are taken by the lab to test their own sub-sampling techniques, for full core geochemical samples the lab duplicate taken at the first split after the initial crush (sampled with a rotary splitter) is used by Toro to calculate the sampling error.</li> <li>• Total sampling errors calculated from half core field duplicates typically range from <math>\pm 10-20\%</math>. Total sampling errors for the first split at the lab in case of full core sampling typically range from <math>\pm 1-5\%</math>.</li> <li>• The laboratory used for Toro's geochemical analysis bases all crushing grain sizes and subsequent sub-sampling weights on being inside accepted Gy safety lines for sample representivity. These grains sizes and sub-sample weights have been described above under 'sampling techniques'.</li> </ul>
<p><i>Quality of assay data and laboratory tests</i></p>	<ul style="list-style-type: none"> <li>• <i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i></li> <li>• <i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Prior to 2013 a four acid digest followed by ICPMS was employed for analysis for geochemistry on the other Wiluna deposits – this was assumed to be an almost total rock digest technique although with recognition that highly resistant minerals are sometimes not entirely digested. In 2012 a test was done to compare four acid digest/ICPMS with sodium peroxide fusion followed by ICPMS with fused glass XRF. Analysis of a number of standards suggested that the Fusion/ICPMS was the most accurate. So in 2013, fusion/ICPMS has been used as the bases for all U analyses, however on a number of samples four acid digest/ICPMS and fused glass XRF are still used for comparative purposes. Performance against standards is excellent.</li> <li>• Historical geochemistry data is almost entirely XRF.</li> <li>• Down-hole gamma tools are used as explained above. All tools are Auslog natural gamma probes calibrated at the Adelaide Calibration Model pits in Adelaide, South Australia.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li><i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i></li> </ul>	<ul style="list-style-type: none"> <li>Certified matrix matched standards are used to check analyses at the lab at a rate of 5% or 1 in 20 samples.</li> <li>Coarse quartz sand is used as blanks and are used at a rate of 5% or 1 in 20 samples as well as being strategically placed in front of and behind samples expected to have high concentrations of U so that thresholds for potential cross-contamination within preparations can be obtained.</li> <li>Duplicates are used as already explained in detail above.</li> <li>Limited laboratory checks have been made – in 2013 these represented approximately 3% of all samples.</li> </ul>
<i>Verification of sampling and assaying</i>	<ul style="list-style-type: none"> <li><i>The verification of significant intersections by either independent or alternative company personnel.</i></li> <li><i>The use of twinned holes.</i></li> <li><i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i></li> </ul>	<ul style="list-style-type: none"> <li>Limited interlab geochemistry analytical checks are completed for each drilling campaign, the last interlab check represented 3% of all the geochemical samples. Toro has a calibrated (at the Adelaide Calibration Model pits in Adelaide, South Australia) Auslog gamma probe to check the probing results achieved by external contractors.</li> <li>Hole twinning has not been practiced on the Dawson Hinkler deposit by Toro thus far, rather infill drilling between historical holes.</li> <li>All primary data (gamma log las files, geochemical sample lists, final collar files, geological logs, core photographs, electronic geochemical results, driller's plods, probing plods, deconvolved gamma files, gamma gamma density logs, disequilibrium analysis results etc) are stored on the company server in the appropriate drive and folders. Any hardcopy data, such as official geochemistry results or any paper copy geological logs, are kept in hardcopy in folders and archives as well as being scanned and kept on the company server in the appropriate drives and folders.</li> <li>Data entry procedures are described in some detail below in section 3 under 'data integrity'.</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>• <i>Discuss any adjustment to assay data.</i></li> </ul>	<ul style="list-style-type: none"> <li>• To date, there have been no adjustments made to geochemical assay U<sub>3</sub>O<sub>8</sub> data (or to any other elements).</li> <li>• All gamma data within the region covered by the 2013 drilling program (which represents a single domain in this resource estimation) has been multiplied by a factor of 1.2 according to the consistent difference found between geochemistry and gamma, further explanation follows - The 2013 drilling was targeted at a single domain within the Dawson Hinkler deposit. The results from the 2013 drilling show a marked difference of some 20% (conservative approximation) between geochemistry and gamma suggesting a positive disequilibrium. QAQC of geochemistry (see above) confirmed the geochemistry results from the 2013 drilling. Re-logging over 50% of the 2013 drill holes with a different probe (same make and model) from an external contractor confirmed the gamma results from the recent drilling. Examination of historical drill data within the same domain revealed a similar difference between gamma and geochemistry. Examination of historical drill data from outside the domain within the rest of the deposit revealed an even greater difference between geochemistry and gamma derived eU<sub>3</sub>O<sub>8</sub> values (geochemistry greater than gamma). As a result it was concluded that gamma derived eU<sub>3</sub>O<sub>8</sub> values are consistently under-estimating U<sub>3</sub>O<sub>8</sub> in the ground and so a factor needed to be applied to the gamma derived values. However, to be conservative, only data within the region where the recent 2013 drilling could confirm this underestimation was multiplied by the factor, and so historical results was not relied upon. Therefore, the factor applied was that found within the domain drilled only (and not the greater factor found outside) and that factor was 1.2, to represent the 20% greater geochemistry derived values over the gamma derived values.</li> <li>• Slight adjustments are made to some geochemical assay data to account for depth corrections if an interval error is discovered, this is rare and always restricted to the near surface above mineralized zones.</li> </ul>
<i>Location of data points</i>	<ul style="list-style-type: none"> <li>• <i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i></li> </ul>	<ul style="list-style-type: none"> <li>• All drill hole collars are pegged to the planned collar location using a differential GPS (DGPS) with base station (currently an Austech ProMark500 and ProFlex500). At the end of the drilling campaigns all collars a picked up using the same DGPS equipment for the final</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li><i>Specification of the grid system used.</i></li> <li><i>Quality and adequacy of topographic control.</i></li> </ul>	<p>collar locations that are entered into the database. Accuracy of the DGPS is approximately to 100mm in the vertical and 50mm on the horizontal.</p> <ul style="list-style-type: none"> <li>Due to all drill holes being shallow (maximum depth of 25m) and vertical no down-hole surveying is required.</li> <li>The grid system used on the Wiluna Project is Geocentric Datum of Australia (GDA) 94, zone 51 for the Dawson Hinkler deposit, although the western edge of the deposit is close to the zone 50 border.</li> <li>Topographic control is largely achieved by the DGPS with base station. As stated above, all Toro drill holes are accurate to approximately 100mm on the vertical. At Dawson Hinkler all drill holes have been 'pinned' to a topographic surface created from current drill hole collars surveyed in a with a DGPS and base station.</li> </ul>
<i>Data spacing and distribution</i>	<ul style="list-style-type: none"> <li><i>Data spacing for reporting of Exploration Results.</i></li> <li><i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i></li> <li><i>Whether sample compositing has been applied.</i></li> </ul>	<ul style="list-style-type: none"> <li>No exploration results, resource drilling only</li> <li>Dawson Hinkler: No Measured resource; Indicated resources 100 x 100 m with some limited 100 m x 200 m drill spacing; Inferred resources greater than 100 x 200 m drill spacing.</li> <li>Sample compositing to 0.5m composites has been applied to the 2cm interval eU3O8 data to match the 0.5m geochemical core samples,</li> </ul>
<i>Orientation of data in relation to geological structure</i>	<ul style="list-style-type: none"> <li><i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i></li> <li><i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i></li> </ul>	<ul style="list-style-type: none"> <li>Sampling is non-subjective down-hole sampling from the surface, either at 2cm intervals in the case of gamma probe data or 0.5m samples in the case of geochemistry. Historical geochemistry represents a similar non-bias down-hole process. The sampling orientation employed provides no bias to the groundwater related distribution of mineralization.</li> <li>No bias suspected.</li> </ul>

Criteria	JORC Code explanation	Commentary
<i>Sample security</i>	<ul style="list-style-type: none"> <li><i>The measures taken to ensure sample security.</i></li> </ul>	<ul style="list-style-type: none"> <li>Sampling of drill core for geochemistry is achieved in the field directly after drilling at the drill site. All samples are bagged firstly in plastic and then again in calico (double bagged). A unique non-descript identifier number is used to number each sample that bears no relation to the deposit or the drill hole. All sample details are entered into a fixed format file ready for later import into the database. Samples are immediately transported by utility to the field camp where they are weighed before being packed into steel 44 gallon drums with lock-down lids and tested for radiation for transport classification. The drums are then fitted on timber pallets and transported to the local transport dock at Wiluna for delivery to Perth. Approximate time between sampling and transport to the laboratory is 4 weeks.</li> <li>Sampling of gamma derived measurements is achieved by a single contractor using a gamma probe (see sampling techniques above). Raw gamma probe data is converted into a las file and sent to a Perth based office on a daily basis by email. This data is then packaged and sent to the Toro Energy Database Manager, who sends it to the analyst (consultant) for calculation into U concentrations and deconvolution.</li> </ul>
<i>Audits or reviews</i>	<ul style="list-style-type: none"> <li><i>The results of any audits or reviews of sampling techniques and data.</i></li> </ul>	<ul style="list-style-type: none"> <li>An internal review of geochemical sampling techniques in 2012 led to a change in practice from non-selective half-core sampling to full core sampling so as to reduce total sampling error. This recommendation was followed in 2013 and has satisfactorily reduced sampling error to below <math>\pm 10\%</math>.</li> </ul>

## Section 2 Reporting of Exploration Results

NOT APPLICABLE TO THIS RESOURCE UPDATE

## Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	<ul style="list-style-type: none"> <li>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</li> <li>Data validation procedures used.</li> </ul>	<ul style="list-style-type: none"> <li>Logging and sampling data is entered into a template with fixed formatting and fixed lithological choices (selected from fixed drop-down lists) by the geologist responsible for logging each hole. The template is formatted so that it can be imported directly into a DataShed database. All importing and exporting into and from the database is achieved by a single point of entry/exit responsible for the database (database manager), access for such tasks is restricted to the database manager. All files are transferred from the field to the database manager using a secure commercial based DropBox folder system with automatic back-up and error correction functions. Data files for resource estimation are transferred in a single zip file to the resource consultant, direct from the database manager.</li> <li>All geological interval and gamma data is validated via a systematic check of down-hole gamma to down-hole scintillometer readings (made for each lithological unit) for every hole (both sonic and aircore). A secondary check on actual lithology logging is made by examining core and chip photographs cross-referenced to the geological logs. All historical data is validated in ISATIS against the same data used in previous estimations.</li> </ul>
Site visits	<ul style="list-style-type: none"> <li>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</li> <li>If no site visits have been undertaken indicate why this is the case.</li> </ul>	<ul style="list-style-type: none"> <li>The competent person responsible for the resource estimate, Daniel Guibal, has not had a visit to site. It is considered that a site visit is not necessary given Mr Guibal's experience with Toro's Wiluna uranium deposits, some 6 years, including numerous estimations, as well as experience elsewhere with calcrete associated surficial uranium deposits, such as Lake Maitland.</li> </ul>



Criteria	JORC Code explanation	Commentary
<p><i>Geological interpretation</i></p>	<ul style="list-style-type: none"> <li>• <i>The use of geology in guiding and controlling Mineral Resource estimation.</i></li>   <li>• <i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i></li>   <li>• <i>Nature of the data used and of any assumptions made.</i></li>   <li>• <i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i></li>   <li>• <i>The factors affecting continuity both of grade and geology.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The geological model is not used in the resource estimate since it has been found that mineralization is not necessarily correlated to any particular rock type, despite being often associated with carbonate or carbonated sediments. The mineralization has been found to be associated with the water table and so is more correlated to depth from the surface than any given lithology, maintaining grade across different lithologies. Thus the geological model for estimation is a simple mineralization envelope based on a concentration of U that represents that concentration where the background population of U ends and the U mineralization exists (in a classic bimodal distribution). In the Dawson Hinkler deposit this is 80 ppm U<sub>3</sub>O<sub>8</sub>.</li>   <li>• Examination of 3D LeapFrog models of different grade shells of the resource give a high level of confidence to the above interpretation of a ground water controlled deposit.</li>   <li>• No geological data used in estimation, all data used is based on U values from deconvolved gamma derived equivalents and geochemistry. A minimum of 5% of all drill holes are required to test the validity of gamma and to introduce into the estimation. Density values used in the resource estimates are single values representing average densities for the entire mineralization envelope. The advantage of using a mineralization envelope based on U concentrations only (both chemistry and deconvolved gamma derived equivalents) is that there are no assumptions made. Domains are based on variance within the data and so in effect, real changes in the behavior of the data and data distribution, there is no forcing statistical predictions into domains based on lithology that is not necessarily correlated spatially at all times.</li>   <li>• A different geological interpretation, if used in the resource estimate, may affect the results of the resource estimate slightly, however, since geology is not used in estimations a change in geological interpretations would make no difference.</li>   <li>• Grade Continuity can be affected by numerous factors, including drilling density (down to 100m x 100m for Dawson Hinkler), nugget effect, itself linked to the type of measurement (geochemical data are</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>more variable than radiometric deconvolved radiometric data), uncertainties on the data themselves due to calibration problems or/and disequilibrium for the radiometric values, sampling/assaying issues for the geochemical measurements (controlled by QA/QC), and geological continuity, which is reasonably established at Wiluna. Geology has been controlled by recent to Quaternary sediment deposition with overprinting calcretisation being controlled by the ground water flow.</p>
Dimensions	<ul style="list-style-type: none"> <li>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</li> </ul>	<ul style="list-style-type: none"> <li>The Wiluna deposits are superficial with a vertical thickness of a few meters at most. Occasionally deeper (15 to 25m below surface) mineralization exists, but its continuity is not proved, because of the lack of deep drilling</li> </ul>
Estimation and modeling techniques	<ul style="list-style-type: none"> <li>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</li> </ul>	<ul style="list-style-type: none"> <li>Estimation technique is Uniform Conditioning followed by Localised Uniform Conditioning using the specialised geostatistical software, Isatis. The various steps of the estimation are the following: <ol style="list-style-type: none"> <li>Use of combined radiometric and geochemical data, with priority given to geochemistry in the westernmost zone (in the infrequent case when both exist). In the other zones, conservatively, only radiometric data are used. As discussed above the 2013 gamma data in the westernmost zone was corrected by a 1.2 factor to account for a systematic discrepancy with geochemical data.</li> <li>Creation of a mineralisation envelope using Leapfrog 3D at a cut-off of 70 ppm eU3O8 to define the hanging wall and the footwall For the westernmost zone, this envelope was created prior to factoring of the 2013 data .</li> <li>Compositing to 0.5m.</li> <li>Domaining by zones of reasonably consistent grade.</li> <li>Top-cuts used at Dawson-Hinkler: 500 ppm in an eastern domain. The top-cut has very little impact on mean grade (less than 1%) and variance.</li> <li>Block model based on 200m x 100m x 0.5m panels for Dawson-Hinkler. The panel sizes are chosen from the drilling density.</li> <li>Ordinary Kriging estimation of panels, after neighbourhood analysis</li> </ol> </li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>• <i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i></li>   <li>• <i>The assumptions made regarding recovery of by-products.</i></li>   <li>• <i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i></li>   <li>• <i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i></li>   <li>• <i>Any assumptions behind modelling of selective mining units.</i></li>   <li>• <i>Any assumptions about correlation between variables.</i></li> </ul>	<p>to optimise quality of kriging.</p> <p>(8) Validation of Kriging results through statistics and swath plots</p> <p>(9) Uniform conditioning (UC) for 10m x 10m x 0.5m Selective Mining Units (SMU), which is a realistic assumption for a future operation where grade control using radiometric information will be possible.</p> <p>(10) Localised Uniform Conditioning: creation of a 10m x 10m x 0.5m block model based on the results of UC</p> <p>(11) The tonnage are estimated using a constant dry density (1.7) per deposit, based on the average value of existing measurements</p> <ul style="list-style-type: none"> <li>• Previous resource estimates (prepared for a number of years by SRK and Mr Daniel Guibal) are available and are considered in all current estimations.</li>   <li>• No by-products are assumed to be recovered nor are any planned to be recovered.</li>   <li>• Currently there are no geostatistical estimations made on deleterious elements, however, such elements have been included in the analysis of drill core samples in 2013 and so such estimations will be able to be accomplished in the future as more coverage across the deposits is achieved. Current analysis of drill core geochemistry and Metallurgical samples strongly suggests there are no significant economic issues related to deleterious elements.</li>   <li>• See above</li>   <li>• See above</li>   <li>• No assumptions</li> </ul>

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>• <i>Description of how the geological interpretation was used to control the resource estimates.</i></li> <li>• <i>Discussion of basis for using or not using grade cutting or capping.</i></li> <li>• <i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i></li> </ul>	<ul style="list-style-type: none"> <li>• See above – no geological control in any of the 2012 JORC compliant resources.</li> <li>• See above</li> <li>• See above</li> </ul>
Moisture	<ul style="list-style-type: none"> <li>• <i>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Tonnages are dry tonnages</li> </ul>
Cut-off parameters	<ul style="list-style-type: none"> <li>• <i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Grade-tonnage curve are provided for a range of cut-offs. Optimal cut-off will be determined from the mining studies.</li> </ul>
Mining factors or assumptions	<ul style="list-style-type: none"> <li>• <i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Mining technique has been tested successfully on site at the Centipede deposit, the main points follow.</li> <li>• Shallow strip mining to 15m maximum depth using a combination of a Vermeer surface miner, loader and articulated trucks.</li> <li>• 25-50cm benches</li> <li>• De-watering of pits for process water</li> <li>• In-pit tailings disposal below natural ground surface in lined pits, progressive compartmental mining, tailings and rehabilitation – however, no tailings disposal planned for Dawson Hinkler site.</li> <li>• Current - strip 3.8:1, using 250 ppm cut-off</li> <li>• Up to 14 year life of mine, regional resources (of which Dawson Hinkler is part of) increase to 20+ years dependent on future approvals</li> <li>• 5 years at Centipede followed by Lake Way – Dawson Hinkler later</li> </ul>
Metallurgical factors or assumptions	<ul style="list-style-type: none"> <li>• <i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions</i></li> </ul>	<ul style="list-style-type: none"> <li>• Laboratory scale pilot plant has been successfully trialled that includes all of the currently proposed process from crushing/grinding to product – actual product produced. Every part of the processing circuit has been tested and/or had research associated with it. Main</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p><i>regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i></p>	<p>factors follow.</p> <ul style="list-style-type: none"> <li>• Alkaline tank leach with direct precipitation.</li> <li>• Target production is 780 tpa U<sub>3</sub>O<sub>8</sub></li> <li>• Processing 1.3 Mtpa at a head grade of 716 ppm U<sub>3</sub>O<sub>8</sub></li> <li>• Processing plant is planned to be located on the Centipede deposit related tenements.</li> </ul>
Environmental factors or assumptions	<ul style="list-style-type: none"> <li>• <i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Two of the Wiluna deposits have been approved for mining by the West Australian EPA as part of the Wiluna Uranium Project and thus the project has gone through the Environmental Review and Management Programme process (The ERMP and all of the associated documents can be found on the Toro Energy website at <a href="http://www.toroenergy.com.au/sustainability/health-safety/environmental-review-and-management-programme-ermp/">http://www.toroenergy.com.au/sustainability/health-safety/environmental-review-and-management-programme-ermp/</a>)</li> <li>• Main factors follow.</li> <li>• Shallow open pit mining</li> <li>• In-pit tailings disposal below natural ground surface in lined pits, progressive compartmental mining, tailings and rehabilitation – no tailings disposal planned for Dawson Hinkler deposit site.</li> <li>• Tailings integrity modelled for 10,000 years</li> <li>• Mining footprint returned as close as possible to natural land surface level</li> <li>• No standing landforms remain post closure</li> </ul>
Bulk density	<ul style="list-style-type: none"> <li>• <i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i></li> <li>• <i>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i></li> <li>• <i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Density has been averaged so that a single density is applied to across the block model.</li> <li>• Density derived by consensus from surrounding deposits for Dawson Hinkler.</li> </ul>
Classification	<ul style="list-style-type: none"> <li>• <i>The basis for the classification of the Mineral Resources into varying confidence categories.</i></li> <li>• <i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality,</i></li> </ul>	<ul style="list-style-type: none"> <li>• The classification is based on the consideration of drill spacing, existence of geochemical data in such numbers that the radiometric data are well supported and finally the quality of the estimation as measured by kriging slope of regression.</li> <li>• Dawson Hinkler: No Measured resource; Indicated resources 100 x</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p><i>quantity and distribution of the data).</i></p> <ul style="list-style-type: none"> <li>• <i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i></li> </ul>	<p>100 m with limited 100 x 200 m drill spacing; Inferred resources greater than 100 x 200 m drill spacing.</p>
Audits or reviews	<ul style="list-style-type: none"> <li>• <i>The results of any audits or reviews of Mineral Resource estimates.</i></li> </ul>	<ul style="list-style-type: none"> <li>• There has been no audit of the resources reporting material change within this ASX release, other than internal Toro assessment and geological interpretation.</li> </ul>
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> <li>• <i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i></li> <li>• <i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i></li> <li>• <i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i></li> </ul>	<ul style="list-style-type: none"> <li>• As mentioned, the classification is partly based on the quality of kriging. In addition, since 2009, various drilling campaigns took place at Wiluna in particular and there has been a good consistency of the estimates.</li> <li>• There is more uncertainty at the individual panel level.</li> <li>• Other factors having an impact on the estimation are: <ul style="list-style-type: none"> <li>(1) Possible disequilibrium - current measurements suggest that it is likely to be significant, particularly in the west;</li> <li>(2) Relationship between radiometric values and geochemical data can be variable;</li> <li>(3) The assaying methods, as there are indications that XRF tends to overestimate grades by about 5% (by comparison to mass spectrometry) – XRF is mostly in historical data;</li> <li>(4) The cut-off grades- due to the estimation method (UC), the high cut-off grades (over 500 ppm) which depend on the modelling of the tail of the grade distributions are more uncertain at local level.</li> </ul> </li> <li>• No production statistics available – not an operating mine</li> </ul>

## Section 4 Estimation and Reporting of Ore Reserves

NOT APPLICABLE – NO RESERVES REPORTED

## Section 5 Estimation and Reporting of Diamonds and Other Gemstones

NOT APPLICABLE – URANIUM ONLY