

## UPDATE ON MAIDEN JORC RESOURCE FOR THE GOLD BASIN PROJECT, ARIZONA USA

25 October 2019

Greenvale Energy Limited (ASX: GRV) is pleased to provide the following additional in relation to the Maiden JORC Resource (JORC) for the Gold Basin oxide gold project in Mohave County Arizona announcement the Company dated October 22<sup>nd</sup> 2019 (Announcement).

### 1. 2019 drilling has been included in the JORC.

The Announcement included:

- *Cyclopic and Stealth deposits* - a list of all holes included in the estimated Resource for the Cyclopic and Stealth deposits. It is noted that 32 out of 33 current (2019) holes were included in the Cyclopic Resource (highlighted in Yellow in the included table in Appendix 1 to this announcement).
- *Stealth Deposit* – the Resource comprised of all historical holes as no holes were drilled there in 2019.

### 2. QAQC measures that were taken in relation to the historical samples.

As per JORC Table 1 in the Announcement it is unknown what combination of quality assurance process or set of processes used to measure and assure the quality the Resource (QAQC) measures were taken on the historical samples. However, the original assay certificates were obtained from American Assay labs and reviewed against digital data files for accuracy.

The Company plans to complete an infill drilling program in the resource area that will also twin a number of the historical holes. This will allow a comparison new results to historical results for the purposes of assessing QAQC. The planned drilling program will be managed in accordance with the JORC Code.

The Company understands the limited QAQC was a key reason for the Competent Person classifying the JORC in the “Inferred” category.

### 3. Additional information on bulk density assumptions

A typical industry standard was used for the typical rock in the deposits - gneiss. The value was based on the lower end of the AusIMM’s typical density range for gneiss or 2.59 to 3.00 (AusIMM, 2011. Field Geologists’ Manual, Fifth edition, Monograph 9. Tables 9.2.3, pp 287).

### 4. Additional Information under LR 5.8.1

Set out below is a summary of the material information required to understand the JORC:

#### Geology and Geological Interpretation

The Gold Basin Mining District is situated in the Basin and Range province, just south of Lake Mead and west of the Colorado Plateau. The edge of the Colorado Plateau is situated approximately 10 miles west of the mining district where gently eastward dipping to flat-lying lower Paleozoic basal formations of the Colorado Plateau crop out along the Grand Wash Cliffs.

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According to Theodore *et al.* (1987), “the district is located within a structurally complex area near the leading edge of the North American platform, straddling several north-trending ranges of mostly Proterozoic basement rocks from which the rocks of the Paleozoic stable platform have been removed by erosion stretching from Canada to Mexico and passing through the area. This belt is characterized by tensional tectonism of mid-Tertiary age, during which rocks overlying the metamorphic cores were transported along low-angle detachment faults of regional extent. The most recent significant tectonic event, normal faulting during the Miocene Period, gave rise to the ‘Basin and Range’ topography that is characteristic of much of the southwestern United States. This region is underlain by metamorphic rocks of Proterozoic age (1.7 billion years) that have been intruded by granitic to dioritic rocks of Cretaceous to Tertiary age (55 to 85 Ma).

Rhyolitic, andesitic and basaltic dikes, flows and pyroclastic rocks of Tertiary age have limited distribution in the area. The gneisses are interpreted to have been involved in two periods of deformation: the Mazatzal (Hudsonian in Canada) at about 1.7 b.y., with associated metamorphism that reached upper-amphibolite grade, and the Laramide of Late-Cretaceous to early Tertiary age coincident with the emplacement of undeformed crystalline intrusives.”

#### **Gold Mineralisation**

Based on the gold mineralisation observed at Stealth and Cyclopic, the Gold Basin mineralisation is best classified as low sulfidation and shallow epithermal. Sulfide is recorded in several holes but is generally not present above depths of 100 to 200m. Alteration products consist of hematitic clay and silica, although carbonate veining/alteration in several holes at Stealth and Red Cloud is associated with the highest grade drill intervals and may be indicative of boiling. The gold mineralization zone possesses a fairly well defined top and bottom, which often occurs in shallow, hydrostatically open epithermal systems.

Both gold grade and distribution are strongly controlled by faulting. The primary mineralization control consists of near-horizontal detachment fault planes cutting the Precambrian gneissic basement, with mineralization being localized within breccia, gouge, and shatter zones ranging from 1m to 30m thick. Based on the drill data, at least four separate detachment planes occur within a package of stacked shear planes that totals about 200m aggregate thickness, but only two of these planes are important with respect to localizing significant gold mineralization. The most important detachment plane, termed the “Cyclopic Detachment”, is a major host for mineralization at the Stealth, Cyclopic, Cyclopic NW, areas. Between 35m and 75m below the Cyclopic Detachment lies the Minus 45m Detachment, which is also an important gold host at Stealth, PLM and Owens Mine.

High-angle faults appear to host only a minor amount of gold mineralization, but they played vital roles in providing feeders for tapping hydrothermal solutions (as at Stealth) and in providing better ground preparation within the mineralized detachment structure (as at Cyclopic). The main feeder faults at Stealth and Cyclopic strike northwest and are either vertical or dip steeply west. Where these northwest feeder structures are cut by northeast to east-west trending cross faults, we see much higher gold grades and grade-thicknesses.

#### **Sampling and Sub-Sampling Techniques (From JORC Table 1 included in Announcement)**

##### ***All historical sampling***

- 11,073 soil samples: sample techniques and QAQC unknown.
- 5,474 rock chip samples: sample techniques and QAQC unknown.
- 936 trench samples: sample techniques and QAQC unknown.
- 22,573 RC drill samples: 1,010 samples representing a 3.05m (10') sample interval, and 21,543 samples representing a 1.52m (5') sample interval. All analyses are by fire assay, 30g and 50g charges. Sample techniques, measures, and QAQC unknown.



- 1,774 diamond core samples: 1.52m (5') sample intervals, sample technique and QAQC unknown. Analyses by fire assay, 30g charge.
- No nugget effect seen in duplicate assay results. Of 2297 drill samples analyzed in 1996 by American Assay Lab (FA60 fire assay procedure), 159 duplicate assays were run, of which 70 average in excess of 100ppb Au (range 100-6570ppb). In these 70 duplicates, the Mean Percent Difference (MPD) ranges from 0 to 25% and averages 9%. MPD for samples in the 1000-6570ppb range (24 total) averages 9%.

#### **2019 Drilling**

- Drilling conducted in March-April 2019 was reverse circulation with samples collected every 5 feet. Samples were split using a riffle splitter. Samples were collected based on 5 foot intervals and may cross geological boundaries. The same sample collection and splitting techniques were used for each sample collected and supervised by the Competent Person.
- Each split sample was placed into a separate sample bag with a unique sample number and the depth of each sample was recorded.

#### **Sub-Sampling**

##### **Historical drilling**

- Core and RC sampling techniques unknown.
- Sample preparation techniques and QAQC measures unknown.

#### **2019 Drilling**

- All samples were collected dry and were split via a Gilson bar and Jones riffle splitters and placed in heavy cloth sample bags. Sample weights shipped for analysis ranged from 5 to 8 lbs/sample and were adequate for the very fine-grained type of gold mineralization being tested. Samples were processed by ALS Chemex at its Reno, Nevada laboratory utilizing a standard preparation (ALS code PREP-61) and a 30gm fire assay (ALS code Au-AA23). Field duplicates were inserted on a 1-in-30 sample basis.

##### **Drilling Techniques**

- Reverse circulation center return hammer drilling, 5.5" diam bit.

##### **Criteria Used for Classification**

See point 6 below.

#### **Sample Analysis Method**

##### **All historical data**

- Assay labs used were reputable, and their analytical techniques were appropriate for the time. QAQC procedures are unknown.
- All analyses were by fire assay utilizing 30g and 50g charges and generally using an AA finish. Of the 18,880 RC drill sample analyses documented in preserved assay certificates, 16,825 are reported in ppb while 2,045 are reported in OPT (ounces per ton).
- Detection limits for drill sample analyses range from 2 to 20ppb and 0.001 to 0.005opt.

## 2019 Drilling

- Three different types of OREA gold standards were inserted into the sample stream in the field on a 1-in-30 sample basis, and coarse field blanks were also inserted in the field on a 1-in-30 sample basis.
- All samples were collected dry and were split via a Gilson bar and Jones riffle splitters and placed in heavy cloth sample bags. Sample weights shipped for analysis ranged from 5 to 8 lbs/sample and were adequate for the very fine-grained type of gold mineralization being tested. Samples were processed by ALS Chemex at its Reno, Nevada laboratory utilizing a standard preparation (ALS code PREP-61) and a 30gm fire assay (ALS code Au-AA23). Field duplicates were inserted on a 1-in-30 sample basis.

## Mining Factors and Assumptions

- Until the deposits have been explored further, with a clearer impression developed of scale and particularly metallurgy, there is no fixed assumption of potential mining method.
- However as it is understood that all past mining in the area was effectively open cut. This would suit the current geological models and near surface situation. Open cut mining would be presumed by the Competent Person to apply to Cyclopic and Stealth. This is partially based on past permitting (see below) and its applicability would clearly be demonstrated by pit optimization.
- Heap leaching is presumed by the to be the treatment process. This is based on a combination of factors, the relatively modest grades, the expected oxide nature of ore, and its low cost.

## Cut-off Grade

- The principal low 0.25 g/t cut-off value was supplied by Centric and justified as being in line with other similar oxide gold deposits in Arizona and Nevada. The assumes those include heap leaching operations and thus does not disagree with the Centric on this.
- Higher 0.4 and 0.5 g/t cut-offs are also reported, and the would generally maintain that the higher 0.5 g/t cut-off would be more applicable for the Stealth deposit. This would be given its shape and depth and the possibility its material would be treated differently from Cyclopic's.

## Metallurgy

- Historical metallurgical testwork undertaken in the mid 1990s indicated a +90% recovery for the gold using a cyanidation common in oxide gold deposits in the Western United States.
- Metallurgical testwork is planned for the next phase of work on the project.

## Estimation Methodology

- Initial inspection of drill holes indicated that many were drilled on NE oriented vertical cross-sections, mostly at 50 m spacing. Consequently, geological interpretations were performed on drill holes and grades plotted on ~33 1 km long vertical cross-sections covering an ~1,650 m NW/SE distance.
- Anomalous higher grades (essentially >~0.2 g/t) were clearly concentrated (and contiguous down-hole) and aligned in a series of thin sub-horizontal and sub-parallel layers. Higher grades were generally concentrated in specific sub-areas with greater thickness, with grades petering out and thinning laterally. Layers were separated by barren intervals.
- Iterative interpretation finally allowed 8 layers to be interpreted from a total of ~620 layer intercepts from 320 drill holes. Each interval was identified by name (CY1 to CY8 downwards) and domain number (the name suffix) for segregation during grade estimation. The lowest layer (CY8) was not incorporated into the block modelling due to its limited size and number of intercepts.
- As gold grade mineralisation was clearly layer-bound the layers were modelled with roof (upper) and floor (lower) gridded DTM surfaces from the drill hole intercepts.
- Surfaces were interpolated in 3D using a 'growth' algorithm to best suit geological habits.



- A 5\*5 m mesh was chosen to adequately represent the typical drill hole spacing (typically 20-100 m).
- Lateral extrapolation was conservatively restricted to 30 m outside bounding drill holes.
- Layers were all thin and slightly sinuous whilst being flattish overall.
- Layer vertical thicknesses vary from minimums of ~1 m to maximums of ~20 m, with the mean thicknesses being in the range ~2.5 to 4.0 m.
- The currently interpreted layers occupy a zone ~50 m deep below surface (a drill depth limitation rather than a verified mineralisation limitation).
- The total plan area (within the blue boundary in Figure 2) covered by all of the vertically stacked layers is 810,000 m<sup>2</sup>.
- Composite drill hole gold grades over the intervals vary between minimums of 0.0 g/t and maximums of 13.5 g/t, with the means in the range 0.5 to 1.0 g/t.
- No geostatistical variography was attempted in this first-pass estimation. This was largely determined by the closeness of many drill holes (considered to be well short of expected ranges) and the necessity to rigorously finalise the NS and BD assay situation.

#### **UN-FOLDING GRADE CONTROL**

- To honour (and subsequently control grade estimation) the observed grade continuity along layers a 3D 'unfolding' block model was built within the layer surfaces.

#### **5. Flag the historical drill holes.**

See point 2 above and Appendix 1 table.

#### **6. Discussion on Drillhole extrapolation and spacing.**

**JORC (2012 Edition) Resource classification:** The Competent Person Consultant considers that all Resources should be classified as **Inferred** – a classification for a Mineral Resource for which quantity and grade may be estimated from 'limited' geological evidence and sampling. Here all documented geological evidence and data implies grade continuity between drill holes, particularly clearly at Cyclopic. The low Inferred classification is chosen predominantly as that continuity has not yet been verified (outside the small shallow mine in a corner of the Cyclopic Project where it has). Additional factors in the low classification is the lack of (or documentation of) density data, mineralogical data (material physical properties generally) and metallurgical data.

*Classification support:* As this Resource is predominantly classified as Inferred the Code requires specific details to support the classification and allow an appreciation of the risk of the estimate. Those supporting details are:

- Cyclopic:
  - Simply the great number of drill holes (and the relative closeness of the greater majority of them) with similar results (high consistency) lends great confidence to the layer interpretation and to clear continuity between holes along and between cross-sections. Although this level of confidence would normally fit within the higher Indicated classification that classification is not yet applied here for the lack of the data mentioned above and for the lack of the additional exploration and Consultant's analysis mentioned in the last point below here.
  - The layer interpretation is supported by the shape and style of the old mine within the area.
  - Confidence is held for the high probability of increasing the Resources as many holes were not drilled deep enough within the modelled area to encounter already interpreted or probably deeper layers. This confidence is further bolstered by the clear potential to extend

the models laterally as well. These comments mesh with the Consultant's opinion that the deposit is generally still 'open' in all directions (see 'Layer intercepts' above).

- The Consultant's opinion is that increasing the classification (to at least Indicated) for a considerable portion of the Resources is highly probable with relatively little extra exploration and analysis. This would include twinning some historic drill holes; in-fill drilling in various areas and line extension drilling in others; and a verification site visit by the Consultant. Without a specific up-grade classification percentage in mind the Consultant would nevertheless presume that the number of (say) 100 m deep drill holes actually required to contribute significantly could be of the order of 20 to 40.
- **Stealth:**
  - Although there are relatively few densely drilled cross-sections, and the actual clarity of the geological explanation for the mineralisation is poor, the similarity and presence of extensive more massive mineralisation in a contiguous zone between adjacent drill holes indicates very little possibility of an alternative interpretation to the wire-framed one.
  - The openness of the model lends confidence for a high probability of increasing the Resource with extension drilling.

*Extrapolation:* Effectively very little grade interpolation or extrapolation has been done beyond drill holes or internally over distances greater than the average drill hole spacing.

- Cyclopic extrapolation was completely prevented around the perimeter of the layer intercept interpretations by the imposition of a short 30 m limit. And although those outside holes had layer intercepts in them there were effectively no more drill holes beyond. Internal extrapolation (or more correctly here valid interpolation) at Cyclopic was limited to a relatively smallish internal 200\*500 m area where the distance to closest drill holes was up to 200 m (approximately double the typical wider spaced drill hole spacing of 100 m).
- Stealth extrapolation was restricted principally by the tight wire-frame model.

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#### COMPETENT PERSONS' STATEMENTS

The information in this report that relates to Exploration Targets, Exploration Results, Mineral Resources or Ore Reserves is based on information compiled by **Robin Rankin**, a Competent Person who is a Member (#110551) of the Australasian Institute of Mining and Metallurgy (MAusIMM) and accredited since 2000 as a Chartered Professional () by the AusIMM in the Geology discipline. Robin Rankin provided this information to his Client **Centric Minerals Management Pty Ltd** has paid consulting work in his capacity as Principal Consulting Geologist and operator of independent geological consultancy GeoRes. He and GeoRes are professionally and financially independent in the general sense and specifically of their Client and of the Client's project. This consulting was provided on a paid basis, governed by a (in this case very generalised) scope of work and a fee and expenses schedule, and the results or conclusions reported were not contingent on payments. Robin Rankin has sufficient experience that is relevant to the style of mineralization and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person () as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves' (the JORC Code). Robin Rankin consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

The information in this report that relates to Mineral Reserves, Mineral Resources and Exploration Results is based on information compiled by Mr Charles Straw, Director of Centric Minerals Management Pty Ltd. Mr Straw is a Member of The Australasian Institute of Mining and Metallurgy. Mr Straw has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Straw consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

## Appendix 1 – Cyclopic deposit drill hole listing & collar surveys

The following listing gives name and collar details of the drill holes within the Cyclopic model area. 2019 Holes are highlighted in yellow

Drill hole	Easting (m)	Northing (m)	Elevation (m)	Depth (m)	Azimuth (°)	Dip (°)
C95_01	748,747.4	3,963,618.4	1,347.0	74.68	0	-90
C95_02	748,724.7	3,963,612.0	1,346.0	60.96	83	-45
C95_03	748,712.7	3,963,638.4	1,347.0	60.96	83	-45
C95_06	748,951.6	3,963,206.9	1,320.0	38.10	0	-90
C95_07	748,949.6	3,963,204.9	1,320.0	85.34	230	-50
C95_08	748,948.3	3,963,293.8	1,323.0	18.29	230	-50
C95_09	748,921.7	3,963,277.6	1,322.0	30.18	230	-50
C95_10	748,898.7	3,963,257.3	1,324.0	60.96	230	-50
C95_11	748,873.3	3,963,238.4	1,325.0	64.01	230	-50
C95_12	748,846.2	3,963,222.3	1,326.0	76.20	230	-50
C95_13	748,825.2	3,963,199.9	1,328.0	86.87	230	-50
C95_14	748,797.0	3,963,182.0	1,329.0	91.44	230	-50
C95_15	748,786.2	3,963,324.2	1,331.0	48.77	230	-50
C95_16	748,738.0	3,963,283.4	1,334.0	79.25	230	-50
C95_17	748,714.8	3,963,264.7	1,336.0	85.65	230	-50
C95_18	748,690.7	3,963,245.1	1,337.0	103.63	230	-50
C95_19	748,738.8	3,963,439.4	1,333.0	18.29	230	-50
C95_20	748,715.1	3,963,418.6	1,336.0	42.67	230	-50
C95_21	748,691.1	3,963,398.6	1,337.0	42.67	230	-50
C95_22	748,667.6	3,963,378.4	1,339.0	67.06	230	-50
C95_23	748,642.4	3,963,358.3	1,340.0	106.68	230	-50
C95_24	748,620.5	3,963,339.6	1,342.0	109.73	230	-50
C95_25	748,598.9	3,963,529.4	1,341.0	45.72	230	-50
C95_26	748,575.4	3,963,509.6	1,344.0	60.96	230	-50
C95_27	748,551.1	3,963,490.2	1,345.0	73.15	230	-50
C95_28	748,527.6	3,963,470.7	1,347.0	91.44	230	-50
C95_29	748,503.9	3,963,451.1	1,350.0	97.54	230	-50
C95_30	748,480.3	3,963,431.1	1,352.0	109.73	230	-50
C95_31	748,458.4	3,963,412.6	1,354.0	121.92	230	-50
C95_32	748,642.0	3,963,545.1	1,340.0	36.58	230	-50
C95_33	748,582.1	3,963,569.6	1,345.0	39.62	230	-50
C95_34	748,478.3	3,963,615.5	1,352.0	48.77	230	-50
C95_35	748,453.7	3,963,595.1	1,351.0	54.86	230	-50
C95_36	748,430.6	3,963,575.1	1,353.0	60.96	230	-50
C95_37	748,409.8	3,963,552.3	1,353.0	67.06	230	-50
C95_38	748,384.0	3,963,536.5	1,357.0	76.20	230	-50
C95_39	748,360.4	3,963,516.3	1,358.0	97.54	230	-50
C95_40	748,340.4	3,963,499.2	1,359.0	115.82	230	-50
C95_41	748,432.7	3,963,658.3	1,351.0	30.48	230	-50
C95_42	748,408.9	3,963,640.5	1,354.0	39.62	230	-50
C95_43	748,385.3	3,963,621.4	1,357.0	51.82	230	-50
C95_44	748,361.6	3,963,601.7	1,356.0	67.06	230	-50
C95_45	748,340.7	3,963,583.5	1,359.0	83.82	230	-50
C95_46	748,314.3	3,963,563.0	1,362.0	96.01	230	-50
C95_49	747,945.3	3,964,028.1	1,381.0	83.82	0	-90
C95_50	748,899.3	3,963,211.2	1,323.0	51.82	230	-50
C95_51	748,927.2	3,963,184.6	1,320.0	48.77	230	-50
C95_52	748,969.2	3,963,180.2	1,318.0	51.82	230	-55
C95_53	747,975.9	3,964,027.9	1,379.0	152.40	0	-90
C95_54	747,976.1	3,963,998.3	1,376.0	131.06	0	-90
C95_55	748,928.9	3,963,187.7	1,320.0	30.48	0	-90
C95_56	748,826.7	3,963,236.6	1,328.0	30.48	230	-50
C95_57	748,817.5	3,963,260.7	1,328.0	48.77	230	-50
C95_58	748,797.6	3,963,282.1	1,330.0	67.06	230	-50
C95_59	748,762.5	3,963,302.7	1,332.0	60.96	230	-50
C95_60	748,934.5	3,963,339.8	1,321.0	9.14	0	-90
C95_61	748,924.1	3,963,327.4	1,322.0	18.29	0	-90
C95_62	748,914.4	3,963,315.6	1,322.0	19.81	0	-90
C95_63	748,920.9	3,963,369.8	1,324.0	7.62	0	-90
C95_64	748,913.1	3,963,361.7	1,322.0	10.67	0	-90
C95_65	748,900.5	3,963,347.0	1,321.0	19.81	0	-90
C95_66	748,890.9	3,963,335.3	1,321.0	18.29	0	-90
C95_67	748,881.6	3,963,323.6	1,320.0	27.43	0	-90
C95_68	748,897.2	3,963,389.5	1,325.0	9.14	0	-90
C95_69	748,887.0	3,963,377.9	1,323.0	10.67	0	-90



Drill hole	Easting (m)	Northing (m)	Elevation (m)	Depth (m)	Azimuth (°)	Dip (°)
C95_70	748,877.6	3,963,366.3	1,321.0	15.24	0	-90
C95_71	748,867.6	3,963,354.6	1,321.0	30.48	0	-90
C95_72	748,857.8	3,963,343.3	1,321.0	36.58	0	-90
C95_73	748,846.5	3,963,330.9	1,328.0	36.58	0	-90
C95_74	748,872.7	3,963,410.2	1,327.0	12.19	0	-90
C95_75	748,863.4	3,963,398.6	1,327.0	12.19	0	-90
C95_76	748,853.8	3,963,386.7	1,326.0	10.67	0	-90
C95_77	748,844.0	3,963,374.6	1,323.0	15.24	0	-90
C95_78	748,834.6	3,963,362.6	1,321.0	15.24	0	-90
C95_79	748,821.8	3,963,348.3	1,329.0	39.62	0	-90
C95_80	748,838.3	3,963,417.5	1,327.0	9.14	0	-90
C95_81	748,829.0	3,963,405.1	1,327.0	10.67	0	-90
C95_82	748,819.4	3,963,392.9	1,328.0	15.24	0	-90
C95_83	748,809.8	3,963,379.4	1,330.0	24.38	0	-90
C95_84	748,799.7	3,963,368.4	1,331.0	24.38	0	-90
C95_85	748,814.3	3,963,435.4	1,329.0	9.14	0	-90
C95_86	748,805.4	3,963,424.2	1,329.0	10.67	0	-90
C95_87	748,795.7	3,963,412.4	1,329.0	13.72	0	-90
C95_88	748,786.1	3,963,400.6	1,330.0	18.29	0	-90
C95_89	748,776.9	3,963,389.2	1,331.0	67.06	0	-90
C96_01	747,902.2	3,964,053.1	1,381.0	67.06	0	-90
C96_02	747,939.8	3,963,951.2	1,378.0	68.58	0	-90
C96_03	748,071.1	3,963,921.9	1,371.0	60.96	0	-90
C96_04	748,789.7	3,963,453.0	1,330.0	35.05	0	-90
C96_05	748,780.5	3,963,441.7	1,329.0	44.20	0	-90
C96_06	748,771.3	3,963,430.2	1,328.0	12.19	0	-90
C96_07	748,761.0	3,963,418.5	1,330.0	18.29	0	-90
C96_08	748,753.0	3,963,407.1	1,332.0	19.81	0	-90
C96_09	748,751.3	3,963,404.9	1,332.0	30.48	220	-45
C96_10	748,777.1	3,963,482.5	1,332.0	6.10	0	-90
C96_11	748,767.3	3,963,469.5	1,332.0	9.14	0	-90
C96_12	748,758.1	3,963,458.6	1,331.0	12.19	0	-90
C96_13	748,747.5	3,963,445.9	1,330.0	7.62	0	-90
C96_14	748,737.8	3,963,433.9	1,331.0	15.24	0	-90
C96_15	748,729.0	3,963,422.8	1,333.0	19.81	0	-90
C96_16	748,732.2	3,963,477.9	1,332.0	7.62	0	-90
C96_17	748,723.7	3,963,464.9	1,331.0	9.14	0	-90
C96_18	748,714.1	3,963,453.5	1,333.0	13.72	0	-90
C96_19	748,704.1	3,963,441.9	1,334.0	25.91	0	-90
C96_20	748,694.1	3,963,430.2	1,335.0	38.10	0	-90
C96_21	748,708.0	3,963,493.3	1,335.0	10.67	0	-90
C96_22	748,697.9	3,963,481.4	1,336.0	12.19	0	-90
C96_23	748,688.8	3,963,470.2	1,337.0	16.76	0	-90
C96_24	748,678.3	3,963,457.4	1,337.0	25.91	0	-90
C96_25	748,668.6	3,963,445.8	1,336.0	39.62	0	-90
C96_26	748,661.1	3,963,436.9	1,335.0	42.67	0	-90
C96_27	748,659.3	3,963,434.4	1,335.0	67.06	220	-45
C96_28	748,686.4	3,963,514.7	1,337.0	9.14	0	-90
C96_29	748,674.1	3,963,500.4	1,338.0	19.81	0	-90
C96_30	748,664.1	3,963,488.4	1,338.0	28.96	0	-90
C96_31	748,654.6	3,963,477.0	1,340.0	33.53	0	-90
C96_32	748,643.3	3,963,463.6	1,340.0	73.15	220	-45
C96_33	748,669.9	3,963,544.7	1,338.0	10.67	0	-90
C96_34	748,659.5	3,963,531.4	1,338.0	16.76	0	-90
C96_35	748,649.7	3,963,518.6	1,339.0	21.34	0	-90
C96_36	748,640.4	3,963,507.0	1,340.0	25.91	0	-90
C96_37	748,631.4	3,963,495.4	1,341.0	28.65	0	-90
C96_38	748,630.3	3,963,494.2	1,341.0	54.86	220	-45
C96_39	748,654.0	3,963,574.4	1,338.0	9.14	0	-90
C96_40	748,644.9	3,963,562.4	1,341.0	12.19	0	-90
C96_41	748,636.0	3,963,550.8	1,341.0	18.29	0	-90
C96_42	748,626.4	3,963,538.1	1,340.0	33.53	0	-90
C96_43	748,607.8	3,963,513.9	1,342.0	30.48	0	-90
C96_44	748,597.5	3,963,500.9	1,342.0	33.53	0	-90
C96_45	748,630.9	3,963,592.3	1,339.0	9.14	0	-90
C96_46	748,623.6	3,963,583.2	1,340.0	12.19	0	-90
C96_47	748,613.2	3,963,572.2	1,343.0	19.81	0	-90
C96_48	748,603.5	3,963,559.9	1,343.0	21.34	0	-90
C96_49	748,585.2	3,963,536.2	1,343.0	38.10	0	-90
C96_50	748,567.0	3,963,512.7	1,344.0	36.58	0	-90

Drill hole	Easting (m)	Northing (m)	Elevation (m)	Depth (m)	Azimuth (°)	Dip (°)
C96_51	748,011.6	3,964,046.6	1,375.0	76.20	0	-90
C96_52	747,907.7	3,964,011.9	1,384.0	54.86	0	-90
C96_53	748,004.5	3,963,935.7	1,377.0	50.29	0	-90
C96_54	748,598.5	3,963,600.9	1,341.0	10.67	0	-90
C96_55	748,590.1	3,963,590.0	1,343.0	19.81	0	-90
C96_56	748,581.3	3,963,579.2	1,344.0	22.86	0	-90
C96_57	748,571.2	3,963,567.5	1,344.0	36.58	0	-90
C96_58	748,550.0	3,963,541.3	1,347.0	35.05	0	-90
C96_59	748,540.3	3,963,530.2	1,347.0	38.10	0	-90
C96_60	748,575.6	3,963,622.4	1,343.0	15.24	0	-90
C96_61	748,552.8	3,963,592.8	1,346.0	36.58	220	-45
C96_62	748,536.3	3,963,572.8	1,346.0	30.48	0	-90
C96_63	748,518.2	3,963,549.2	1,346.0	36.58	0	-90
C96_64	748,552.1	3,963,641.2	1,346.0	15.24	220	-45
C96_65	748,532.2	3,963,616.1	1,348.0	18.79	0	-90
C96_66	748,522.6	3,963,603.9	1,349.0	24.38	0	-90
C96_67	748,512.3	3,963,590.9	1,350.0	32.00	0	-90
C96_68	748,517.5	3,963,646.7	1,345.0	21.34	220	-60
C96_69	748,499.2	3,963,623.0	1,350.0	28.96	220	-60
C96_70	748,479.8	3,963,598.7	1,352.0	32.00	0	-90
C96_71	748,506.3	3,963,678.1	1,349.0	91.44	0	-90
C96_72	748,488.6	3,963,658.3	1,347.0	30.48	220	-45
C96_73	748,472.6	3,963,642.0	1,350.0	39.62	220	-60
C96_74	748,449.8	3,963,659.9	1,350.0	42.67	220	-45
C96_75	748,441.3	3,963,647.5	1,354.0	24.38	0	-90
C96_76	748,431.7	3,963,636.3	1,354.0	30.48	0	-90
C96_77	748,437.8	3,963,691.0	1,351.0	19.81	0	-90
C96_78	748,426.6	3,963,677.2	1,351.0	18.29	220	-45
C96_79	748,859.7	3,963,342.5	1,321.0	24.38	220	-45
C96_80	748,913.7	3,963,314.3	1,321.0	28.96	220	-45
C96_81	748,914.5	3,963,361.8	1,322.0	15.24	0	-90
C96_82	748,921.8	3,963,369.1	1,324.0	12.19	0	-90
CBG_01	748,838.3	3,963,252.8	1,328.0	91.44	210	-50
CBG_02	748,652.7	3,963,384.3	1,340.0	97.54	210	-50
CBG_03	748,272.2	3,963,603.5	1,361.0	108.20	210	-50
CMW_02	748,899.4	3,963,496.8	1,330.0	182.88	0	-90
CMW_03	748,762.3	3,963,304.7	1,333.0	182.88	0	-90
CNW_16_11	748,039.0	3,963,990.0	1,357.0	54.86	0	-90
CNW_16_12	748,119.0	3,963,989.0	1,354.0	54.86	0	-90
CNW_16_13	748,065.0	3,964,117.0	1,358.0	85.34	0	-90
CNW_16_14	748,066.0	3,964,060.0	1,356.0	85.34	0	-90
CNW_16_15	748,074.0	3,964,046.0	1,361.0	85.34	0	-90
CNW_16_16	748,103.0	3,964,039.0	1,359.0	85.34	0	-90
CNW_16_17	748,150.0	3,964,043.0	1,358.0	91.44	0	-90
CNW_16_19	748,235.0	3,964,148.0	1,349.0	85.34	0	-90
CNW_16_21	748,360.0	3,964,021.0	1,350.0	60.96	0	-90
CNW_16_22	748,503.0	3,964,030.0	1,342.0	45.72	0	-90
CNW_16_23	748,146.0	3,963,881.0	1,356.0	54.86	0	-90
CNW_16_24	748,280.0	3,963,797.0	1,350.0	60.96	0	-90
CNW_16_25	748,358.0	3,963,723.0	1,347.0	60.96	0	-90
CNW_16_26	748,438.0	3,963,672.0	1,339.0	60.96	0	-90
CNW_16_28	747,827.0	3,964,277.0	1,391.0	88.39	0	-90
CNW_16_29	747,994.0	3,964,223.0	1,367.0	85.34	0	-90
CNW_16_30	748,155.0	3,964,231.0	1,350.0	85.34	0	-90
CNW_16_31	747,825.0	3,964,140.0	1,377.0	79.25	0	-90
CNW_16_32	747,869.0	3,964,105.0	1,369.0	85.34	0	-90
CNW_16_32N	747,872.0	3,964,171.0	1,369.0	85.34	0	-90
CNW_16_33	747,932.0	3,964,139.0	1,362.0	94.49	0	-90
CNW_16_34	747,995.0	3,964,155.0	1,360.0	91.44	0	-90
CNW_16_35	748,120.0	3,964,152.0	1,356.0	91.44	0	-90
CNW_16_36	748,349.0	3,964,153.0	1,354.0	45.72	0	-90
CNW_16_37	748,422.0	3,964,144.0	1,348.0	45.72	0	-90
CNW_16_39	748,445.0	3,964,015.0	1,346.0	60.96	0	-90
CNW_16_40	748,634.0	3,964,027.0	1,340.0	45.72	0	-90
CNW_16_5	748,008.0	3,964,049.0	1,370.0	91.44	0	-90
CNW_16_6	747,933.0	3,964,018.0	1,373.0	91.44	0	-45
CNW_16_6A	747,928.0	3,964,015.0	1,375.0	60.96	80	-90
CNW_16_7	747,974.0	3,963,992.0	1,368.0	76.20	0	-90
CNW_16_8	748,001.0	3,964,005.0	1,372.0	85.34	0	-90
CP_01	748,445.5	3,963,655.9	1,351.0	15.24	0	-90



Drill hole	Easting (m)	Northing (m)	Elevation (m)	Depth (m)	Azimuth (°)	Dip (°)
CP_02	748,488.9	3,963,642.1	1,350.0	15.24	0	90
CP_03	748,495.2	3,963,630.7	1,350.0	15.24	0	-90
CP_04	748,524.6	3,963,616.3	1,348.0	15.24	0	-90
CP_05	748,552.4	3,963,603.4	1,346.0	15.24	0	-90
CP_06	748,580.1	3,963,593.6	1,343.0	15.24	0	-90
CP_07	748,432.9	3,963,622.7	1,354.0	30.48	0	-90
CP_08	748,457.7	3,963,611.2	1,353.0	30.48	0	-90
CP_09	748,487.0	3,963,598.4	1,352.0	30.48	0	-90
CP_10	748,514.8	3,963,587.0	1,349.0	30.48	0	-90
CP_11	748,545.7	3,963,574.3	1,346.0	30.48	0	-90
CP_12	748,571.9	3,963,562.9	1,344.0	30.48	0	-90
CP_13	748,627.6	3,963,540.2	1,340.0	30.48	0	-90
CP_14	748,648.9	3,963,438.6	1,338.0	15.24	0	-90
CP_15	748,696.8	3,963,417.2	1,338.0	15.24	0	-90
CP_16	748,876.6	3,963,367.8	1,321.0	15.24	0	-90
CP_17	748,866.8	3,963,341.6	1,321.0	15.24	0	-90
CP_18	748,847.3	3,963,380.6	1,323.0	15.24	0	-90
CP_19	748,834.2	3,963,358.9	1,321.0	15.24	0	-90
CP_20	748,823.7	3,963,402.8	1,328.0	15.24	0	-90
CP_21	748,654.2	3,963,513.5	1,339.0	15.24	0	-90
CP_22	748,679.2	3,963,492.9	1,338.0	15.24	0	-90
CP_23	748,705.9	3,963,467.8	1,335.0	15.24	0	-90
CP_24	748,731.0	3,963,445.7	1,334.0	15.24	0	-90
CP_25	748,710.0	3,963,432.8	1,336.0	15.24	0	-90
CP_26	748,818.3	3,963,330.9	1,329.0	30.48	0	-90
CP_27	748,849.2	3,963,316.6	1,328.0	30.48	0	-90
CP_28	748,875.5	3,963,303.7	1,326.0	30.48	0	-90
CP_29	748,793.4	3,963,350.0	1,330.0	30.48	0	-90
CYC_1	748,770.0	3,963,376.6	1,332.0	76.20	215	-50
CYC_10	748,519.5	3,963,543.9	1,347.0	76.20	215	-50
CYC_11	748,500.3	3,963,515.8	1,348.0	76.20	215	-50
CYC_12	748,484.5	3,963,493.9	1,349.0	76.20	215	-50
CYC_13	748,153.0	3,964,041.0	1,368.0	91.44	0	-90
CYC_14	748,014.0	3,964,051.0	1,369.0	91.44	0	-90
CYC_15	748,068.0	3,964,117.0	1,366.0	91.44	0	-90
CYC_16	748,978.3	3,963,278.1	1,320.0	30.48	215	-50
CYC_17	748,979.8	3,963,280.6	1,320.0	15.24	0	-90
CYC_18	748,989.0	3,963,294.6	1,317.0	30.48	215	-50
CYC_19	748,991.4	3,963,297.4	1,317.0	15.24	0	-90
CYC_2	748,789.1	3,963,405.6	1,330.0	76.20	215	-50
CYC_20	748,998.1	3,963,306.2	1,319.0	30.48	35	-50
CYC_21	748,955.8	3,963,343.3	1,322.0	30.48	215	-50
CYC_22	748,957.2	3,963,345.5	1,322.0	15.24	0	-90
CYC_23	748,963.5	3,963,358.8	1,325.0	15.24	0	-90
CYC_24	748,917.6	3,963,346.3	1,322.0	18.29	0	-90
CYC_25	748,926.9	3,963,358.8	1,322.0	15.24	0	-90
CYC_26	748,936.8	3,963,375.0	1,324.0	30.48	215	-50
CYC_27	748,939.4	3,963,378.1	1,324.0	21.34	0	-90
CYC_28	748,875.5	3,963,423.4	1,327.0	15.24	0	-90
CYC_29	748,864.2	3,963,412.3	1,327.0	15.24	0	-90
CYC_3	748,800.8	3,963,423.4	1,329.0	76.20	215	-50
CYC_30	748,854.2	3,963,402.2	1,327.0	15.24	0	-90
CYC_31	748,800.8	3,963,423.7	1,329.0	15.24	0	-90
CYC_32	748,805.5	3,963,429.3	1,329.0	15.24	215	-50
CYC_4	748,884.1	3,963,297.9	1,326.0	76.20	215	-50
CYC_5	748,910.3	3,963,335.7	1,322.0	76.20	215	-50
CYC_6	748,921.9	3,963,352.5	1,322.0	67.06	215	-50
CYC_7	748,829.1	3,963,452.8	1,339.0	76.20	215	-50
CYC_8	748,610.0	3,963,422.6	1,345.0	76.20	215	-50
CYC_9	748,644.2	3,963,476.8	1,340.0	76.20	215	-50
CY_1	748,859.9	3,963,422.8	1,327.0	76.20	0	-90
CY_10	748,395.3	3,964,084.6	1,355.0	60.96	0	-90
CY_11	748,058.0	3,963,963.0	1,371.0	60.96	0	-90
CY_12	747,845.4	3,963,981.2	1,384.0	60.96	0	-90
CY_13	748,025.0	3,963,862.0	1,372.0	53.34	0	-90
CY_14	748,196.0	3,963,739.0	1,365.0	60.96	0	-90
CY_15	748,349.2	3,963,578.0	1,358.0	76.20	0	-90
CY_16	748,461.7	3,963,491.6	1,351.0	71.63	0	-90
CY_17	748,571.2	3,963,406.7	1,345.0	60.96	0	-90
CY_2	748,742.4	3,963,625.9	1,347.0	76.20	0	-90

Drill hole	Easting (m)	Northing (m)	Elevation (m)	Depth (m)	Azimuth (°)	Dip (°)
CY_3	748,060.0	3,963,957.0	1,347.0	106.68	0	-90
CY_4	748,358.0	3,964,018.0	1,355.0	112.78	0	-90
CY_5	748,230.0	3,964,287.0	1,363.0	76.20	0	-90
CY_7	748,734.0	3,963,894.2	1,340.0	70.10	0	-90
CY_8	748,771.0	3,963,269.5	1,330.0	76.20	0	-90
CY_9	748,064.0	3,964,064.0	1,371.0	76.20	0	-90
C_01	748,731.7	3,963,541.9	1,335.0	15.24	0	-90
C_02	748,715.5	3,963,513.6	1,334.0	15.24	0	-90
C_03	748,698.4	3,963,486.2	1,335.0	15.24	0	-90
C_04	748,684.0	3,963,457.1	1,336.0	15.24	0	-90
C_05	748,667.1	3,963,440.7	1,336.0	15.24	0	-90
C_06	748,779.3	3,963,470.4	1,334.0	15.24	0	-90
C_07	748,824.6	3,963,424.8	1,327.0	15.24	0	-90
C_08	748,808.6	3,963,397.8	1,327.0	15.24	0	-90
C_09	748,791.4	3,963,372.8	1,332.0	15.24	0	-90
C_10	748,762.4	3,963,443.3	1,331.0	15.24	0	-90
C_11	748,742.4	3,963,420.1	1,333.0	15.24	0	-90
C_12	748,726.1	3,963,394.6	1,334.0	15.24	0	-90
C_13	748,650.7	3,963,410.3	1,340.0	15.24	0	-90
C_14	748,581.7	3,963,444.1	1,345.0	15.24	0	-90
C_15	748,599.9	3,963,476.2	1,342.0	15.24	0	-90
DDH_04_01	748,883.1	3,963,324.4	1,320.0	10.36	0	-90
DDH_04_01A	748,882.1	3,963,327.4	1,320.0	18.29	0	-90
DDH_04_02	748,848.1	3,963,331.4	1,321.0	39.01	60	-64
DDH_04_03	748,821.1	3,963,391.4	1,328.0	13.11	0	-90
DDH_04_04	748,717.1	3,963,265.4	1,336.0	21.34	0	-90
DDH_04_05	748,661.1	3,963,517.4	1,339.0	23.16	0	-90
DDH_04_06	748,551.1	3,963,541.4	1,347.0	16.46	0	-90
DDH_04_07	748,459.1	3,963,611.4	1,353.0	30.48	0	-90
DDH_04_08	747,946.1	3,964,028.4	1,381.0	30.48	0	-90
NP97_03	748,681.8	3,963,520.6	1,337.0	41.15	90	-45
NP97_04	748,668.4	3,963,491.0	1,338.0	46.77	90	-45
NP97_05	748,644.1	3,963,491.7	1,340.0	76.20	90	-45
NP97_07	747,908.9	3,964,012.4	1,383.0	91.44	90	-60
NP97_08	747,883.4	3,964,044.2	1,382.0	115.82	0	-60
NP97_10	748,481.3	3,963,701.1	1,348.0	170.69	90	-60
NP97_12	748,508.3	3,964,030.8	1,351.0	91.44	70	-60
NP97_13	748,657.2	3,963,583.3	1,339.0	109.73	90	-45
OE_01	748,866.1	3,963,957.5	1,337.0	121.92	225	-45
OE_02	748,882.4	3,963,886.6	1,336.0	60.96	0	-90
OE_03	748,864.9	3,963,802.3	1,337.0	121.92	315	-45
OE_04	748,551.0	3,963,982.9	1,351.0	121.92	135	-45
OE_05	748,571.4	3,963,768.7	1,351.0	121.92	45	-45
OE_06	748,979.5	3,963,291.6	1,316.0	121.92	225	-45
QM83_12	748,731.7	3,963,541.9	1,335.0	23.77	0	-90
320			Total	14,906.83		
			Average	46.58		



## Appendix 2a – Stealth deposit drill hole listing & collar surveys

The following listing gives name and collar details of the drill holes within the Stealth model area.

Drill hole	Easting (m)	Northing (m)	Elevation (m)	Depth (m)	Azimuth (°)	Dip (°)
CBG_08	747,541.8	3,962,856.4	1,432.0	121.92	235	-50
FH95_01	747,827.2	3,962,789.9	1,448.0	167.64	0	-90
FH95_02	747,713.1	3,962,729.3	1,421.0	164.59	40	-45
FH95_03	747,817.8	3,962,689.6	1,448.0	213.36	0	-90
FH95_04	747,816.6	3,962,692.4	1,448.0	201.17	40	-45
FH95_05	747,712.6	3,962,729.7	1,421.0	182.88	0	-90
GB91_18	747,351.2	3,962,906.2	1,443.0	115.82	55	-60
GB91_19	747,295.6	3,963,017.0	1,471.0	140.21	55	-75
GB91_20	747,154.3	3,963,143.1	1,472.0	150.88	55	-60
GB91_21	747,157.0	3,963,241.8	1,454.0	91.44	55	-60
GBR_01	747,281.6	3,963,009.6	1,472.0	182.88	220	-60
GBR_02	747,235.0	3,963,066.3	1,476.0	182.88	60	-60
GBR_03	747,155.3	3,963,273.5	1,458.0	182.88	60	-60
GBR_04	747,386.4	3,962,918.2	1,441.0	73.15	75	-60
GBR_05	747,350.3	3,962,949.1	1,452.0	91.44	75	-58.5
GBR_06	747,421.1	3,962,916.7	1,440.0	91.44	75	-58
GBR_07	747,387.5	3,962,960.8	1,452.0	48.77	75	-60
GBR_08	747,454.1	3,962,907.9	1,439.0	42.67	75	-60
GBR_09	747,322.1	3,963,024.0	1,465.0	54.86	85	-60
GBR_10	747,290.4	3,963,020.0	1,471.0	146.30	25	-60
GBR_11	747,436.0	3,962,883.0	1,441.0	60.96	87	-58
GBR_12	747,310.6	3,963,124.2	1,449.0	121.92	75	-60
GBR_13	747,498.7	3,962,893.4	1,436.0	54.86	35	-60
GBR_14	747,494.0	3,962,887.9	1,435.0	60.96	0	-90
GBR_15	747,344.8	3,963,005.3	1,467.0	60.96	74	-60
GBR_16	747,540.3	3,962,874.0	1,434.0	68.58	30	-60
GBR_17	747,448.9	3,962,931.6	1,444.0	91.44	45	-60
GBR_18	747,411.9	3,962,940.9	1,445.0	73.15	45	-60
GBR_19	747,370.6	3,962,986.4	1,461.0	60.96	50	-60
GBR_20	747,342.0	3,962,978.8	1,461.0	109.73	55	-60
GBR_21	747,478.2	3,962,899.5	1,437.0	91.44	45	-60
GBR_22	747,286.8	3,963,018.8	1,472.0	146.30	25	-75
GBR_23	747,476.6	3,962,858.3	1,441.0	184.40	0	-90
GBR_24	747,520.9	3,962,921.6	1,445.0	111.25	40	-75
GBR_25	747,046.2	3,962,958.8	1,479.0	182.88	55	-50
GBR_28	747,149.8	3,963,133.3	1,473.0	182.88	40	-76.5
GBR_29	747,569.7	3,962,856.4	1,432.0	176.78	40	-60
GBR_30	747,555.3	3,962,903.2	1,442.0	91.44	30	-60
GBR_31	747,498.0	3,962,928.6	1,444.0	79.25	50	-60
GBR_32	747,521.7	3,962,918.6	1,442.0	106.68	220	-51
GBR_33	747,263.2	3,963,041.1	1,475.0	121.92	32	-60
GBR_34	747,296.6	3,963,040.0	1,465.0	79.25	37	-60
GBR_35	747,403.1	3,962,964.3	1,454.0	60.96	80	-60
GBR_36	747,314.4	3,962,993.3	1,467.0	121.92	57	-60
GBR_37	747,446.7	3,962,898.8	1,438.0	121.92	48	-60
GBR_38	747,538.4	3,962,871.0	1,433.0	123.44	30	-70
GBR_39	747,356.0	3,962,983.2	1,461.0	91.44	50	-60
GBR_40	747,313.2	3,962,971.5	1,461.0	121.92	50	-60
GBR_42	747,592.2	3,962,888.6	1,440.0	92.96	40	-58
GBR_43	747,090.2	3,962,898.3	1,460.0	152.40	60	-75
GBR_44	747,567.4	3,962,853.4	1,431.0	121.92	30	-79
GBR_45	747,421.1	3,962,914.6	1,440.0	121.92	0	-90
GBR_58	747,436.3	3,962,882.0	1,441.0	103.63	0	-90
GBR_59	747,359.0	3,962,909.3	1,443.0	91.44	0	-90
GBR_60	747,350.0	3,962,948.4	1,451.0	134.11	0	-90
GBR_61	747,533.1	3,962,861.6	1,433.0	91.44	215	-82
GBR_62	747,493.5	3,962,888.7	1,435.0	60.96	215	-64
GBR_70	747,406.0	3,962,891.9	1,443.0	115.82	0	-90
GBR_71	747,550.9	3,962,972.8	1,460.0	152.40	0	-90
GB_02	747,137.2	3,962,911.6	1,456.0	182.88	0	-90
GB_16	747,381.2	3,963,300.8	1,457.0	109.73	0	-90
NP97_01	747,433.4	3,962,886.5	1,441.0	152.40	90	-60
NP97_02	747,256.2	3,963,003.2	1,467.0	170.69	90	-50
S96_01	747,361.6	3,963,040.1	1,459.0	60.96	225	-45
S96_02	747,567.2	3,962,954.7	1,459.0	128.02	225	-50

S96_03	747,395.1	3,902,975.9	1,450.0	53.34	0	-00
S96_04	747,465.7	3,962,882.8	1,438.0	121.92	45	-59
S96_05	747,503.7	3,962,925.6	1,444.0	100.73	0	90
S96_06	747,382.3	3,962,927.5	1,443.0	85.34	45	-60
S96_07	747,329.3	3,962,946.1	1,451.0	115.82	45	-60
S96_08	747,522.2	3,962,862.7	1,434.0	97.54	45	-70
S96_09	747,609.3	3,962,850.0	1,430.0	100.58	45	-60
T_06	747,939.6	3,962,738.7	1,421.0	113.69	22	-60
T_07	747,936.7	3,962,731.1	1,420.0	36.58	205	-60
T_08	747,158.5	3,963,298.4	1,459.0	97.54	185	-60
T_10	747,155.7	3,963,268.7	1,458.0	60.96	0	-90
T_11	747,351.3	3,963,004.2	1,466.0	152.40	0	-90
T_12	747,375.4	3,963,010.2	1,465.0	152.40	0	-90
T_13	747,919.3	3,962,787.0	1,438.0	147.83	0	-90
T_29	747,359.9	3,963,008.4	1,466.0	178.31	0	-90
80		Total	9,274.43			
		Average	115.93			