ASX RELEASE

18 September 2014

CLOSE SPACED DRILLING RESULTS AT WILUNA EXCEED EXPECTATIONS

Close spaced drilling at the Wiluna Project has delivered:

- **Continuous high grade mineralisation at greater than 1000ppm U_3O_8 identified in three of the four Wiluna deposits;**
- **Mining operability of all deposits and confidence in the resource and geological model confirmed;**
- **Combined with positive disequilibrium results, further resource evaluation to be undertaken.**

Toro Energy Limited's (**ASX:TOE**) 2014 close spaced drilling campaign at the Centipede, Millipede, Lake Maitland and Lake Way deposits has revealed continuous mineralization within the deposits above the Company's previously stated expectations.

Combined with recent announcements of high grade intersections in July and positive disequilibrium in September 2014, these continuous mineralisation results provide a significant platform for further resource development work.

In three of the four deposits, zones of continuous mineralisation with consistent grades of over 1,000 ppm U_3O_8, mostly one to two metres thick were found (see Figures 1-4). This is the key characteristic needed to confirm mining operability, including the ability to deliver the proposed high grade operating strategy in the Project economic model.

These results continue to strongly support the amenability of the deposits to surface mining and enhance the confidence in the resource and geological model.

An area 100 m long and 100 m wide was selected on each of the four deposits for 5 x 5 m close spaced drilling, to enable Toro to study the actual distribution of mineralisation to a detail and scale equivalent to individual mining blocks. This year's campaign was the largest undertaken since consolidation of the six deposits that make up the Wiluna Project. A total of 1,639 holes were drilled for 16,375 m in the first four of the six Wiluna deposits, of which 71 holes for 644 m were sonic core, the remaining being aircore. A small proportion of the drilling was for the purpose of geotechnical studies related to pit wall design and investigations of the run-of-mine pad and processing plant foundations.

"Drilling campaigns undertaken in both 2013 and 2014 have now confirmed the amenability of the deposits to surface mining at Wiluna" Toro Managing Director Dr Vanessa Guthrie said today.

"We have significantly enhanced our geological data and understanding of the uranium mineralization to enable Toro to revise our resources initially and move towards a reserve assessment for the Wiluna Project when the definitive feasibility study is completed".

"Following the recent announcement of positive disequilibrium results from the 2013 drilling campaign, Toro has commenced an assessment of the ratio of geochemical assay U_3O_8 v gamma derived eU_3O_8 values from the 2014 drilling campaign. This involves a thorough review of all Project data to determine the extent of disequilibrium and its relevance to the entire regional resource. This work is expected to be completed during the fourth quarter of 2014."

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Toro Energy is a uranium development and exploration stage mining company based in Perth, Western Australia.

Toro's flagship asset is the 100% owned Wiluna Uranium Project, consisting of six calcrete hosted uranium deposits. The project is located 30 kilometres southwest of Wiluna in Central Western Australia. The Centipede and Lake Way deposits have received full government approval for mining providing the Wiluna Project with the opportunity to be Western Australia's first uranium mine.

Toro also owns a highly prospective suits of exploration properties highlighted by Toro's own discovery at the Theseus Project. The Company also owns uranium assets in the Northern Territory and in Namibia, Africa.

Toro is also pursuing growth opportunities through accretive uranium project acquisitions.

www.toroenergy.com.au

TOE - A member of the All Ordinaries Index

MINING BLOCK EVALUATION AREAS[1]

Figure 1 Centipede Deposit

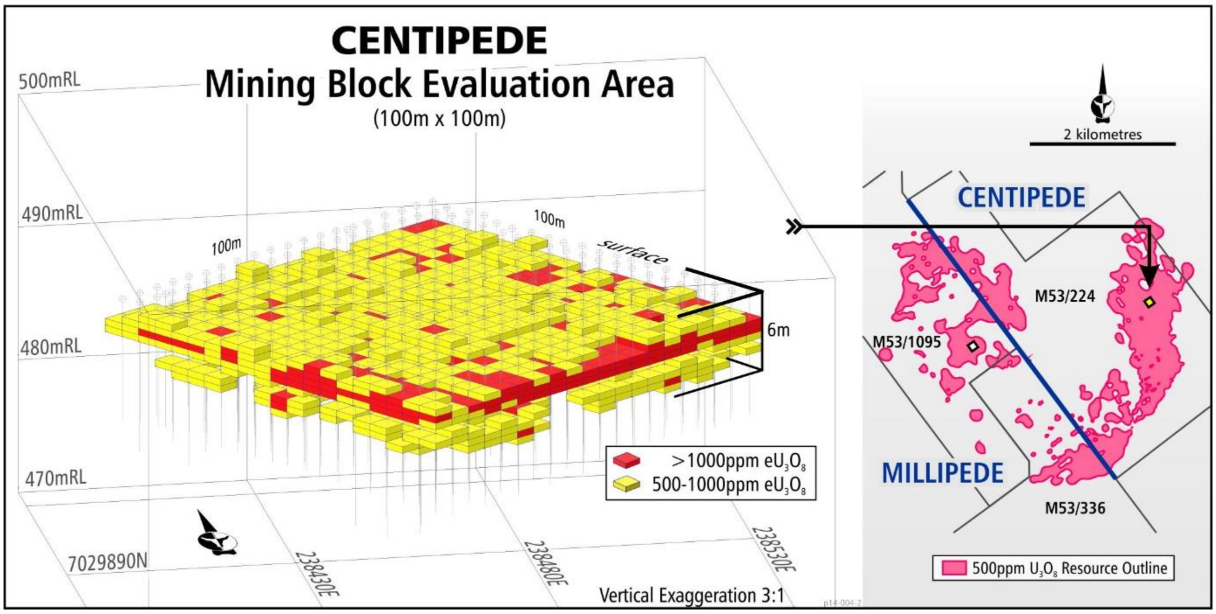
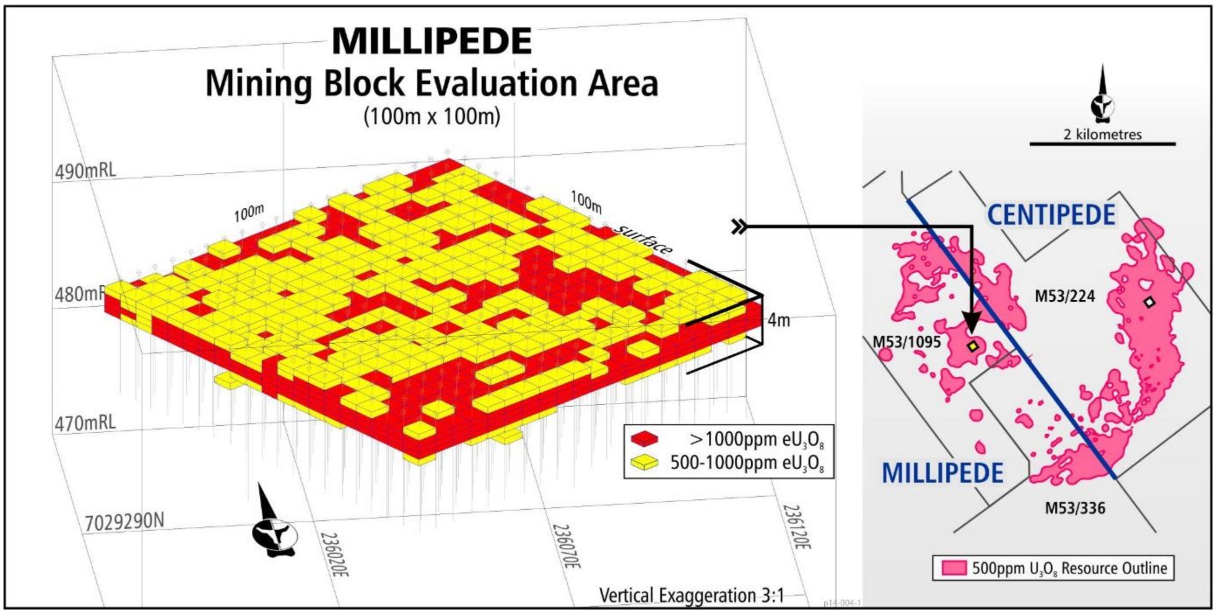


Figure 2 Millipede Deposit



1 *Pursuant to the Company's announcement on 2nd September 2014, a factor of 1.2 has been applied to the resource evaluation mining blocks (estimated from Ordinary Kriging) allowing for the estimated average positive disequilibrium described in that announcement. Details of the estimation technique used for the resource evaluation mining blocks are described in the accompanying JORC table.*

Figure 3 Lake Maitland Deposit

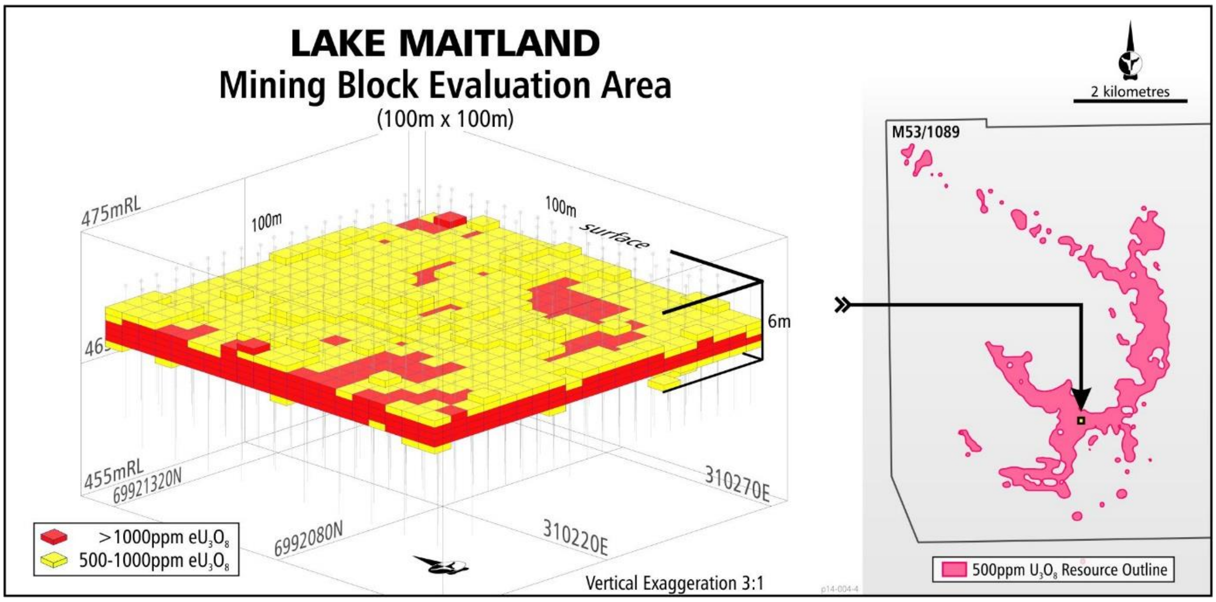
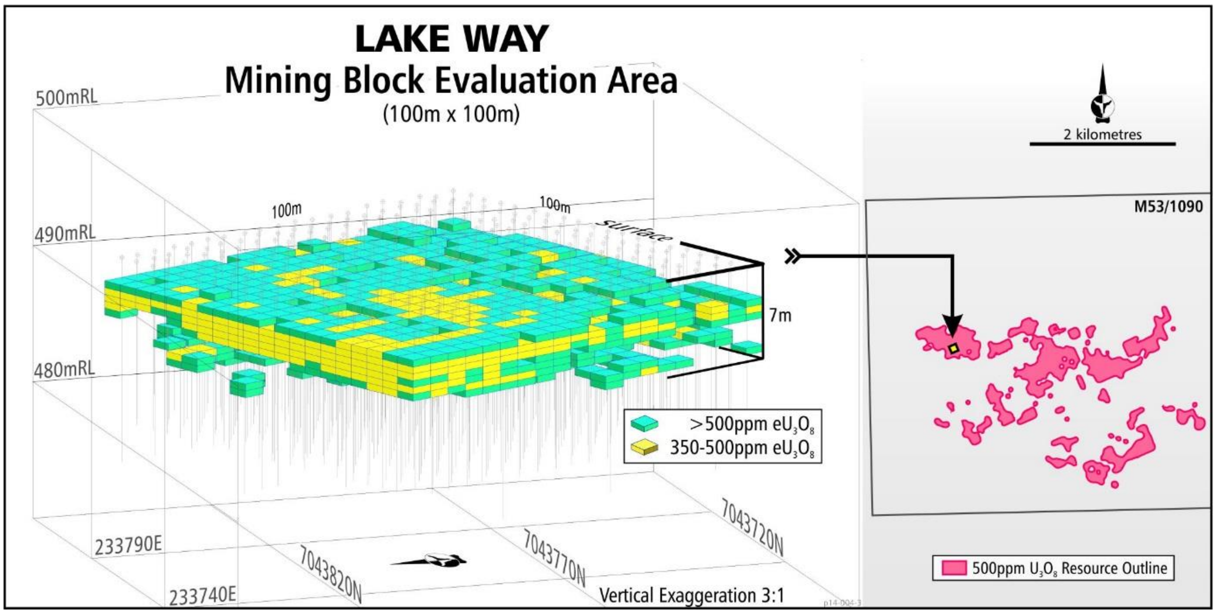


Figure 4 Lake Way Deposit



Wiluna Uranium Project Resource Table[2,3]

The Wiluna Uranium Project - JORC 2012											
		Measured		Indicated		Total Measured or Indicated		Inferred		Total	
Deposit	Measure	200 ppm	500 ppm	200 ppm	500 ppm	200 ppm	500 ppm	200 ppm	500 ppm	200 ppm	500 ppm
Centipede	Mt's	2.9	1.2	7.5	3.1	10.4	4.3	-	-	10.4	4.3
	Grade ppm	551	872	572	943	566	923	-	-	566	923
	Mlb's U_3O_8	3.5	2.3	9.5	6.5	13.0	8.8	-	-	13.0	8.8
Lake Way	Mt's	-	-	10.3	4.2	10.3	4.2	-	-	10.3	4.2
	Grade ppm	-	-	545	883	545	883	-	-	545	883
	Mlb's U_3O_8	-	-	12.3	8.2	12.3	8.2	-	-	12.3	8.2
Millipede	Mt's	-	-	4.5	1.6	4.5	1.6	1.9	0.4	6.4	1.9
	Grade ppm	-	-	530	956	530	956	382	887	486	943
	Mlb's U_3O_8	-	-	5.3	3.3	5.3	3.3	1.6	0.7	6.9	4.0
Lake Maitland	Mt's	-	-	19.9	7.5	19.9	7.5	-	-	19.9	7.5
	Grade ppm	-	-	555	956	555	956	-	-	555	956
	Mlb's U_3O_8	-	-	24.3	15.7	24.3	15.7	-	-	24.3	15.7
Sub-total	***Mt's***	***2.9***	***1.2***	***42.2***	***16.3***	***45.1***	***17.6***	***1.9***	***0.4***	***47.0***	***17.9***
	Grade ppm	***551***	***872***	***553***	***935***	***553***	***930***	***382***	***887***	***546***	***930***
	Mlb's U_3O_8	***3.5***	***2.3***	***51.4***	***33.7***	***55.0***	***36.0***	***1.6***	***0.7***	***56.6***	***36.7***
Dawson Hinkler	Mt's	-	-	8.4	0.9	8.4	0.9	5.2	0.3	13.6	1.1
	Grade ppm	-	-	336	596	336	596	282	628	315	603
	Mlb's U_3O_8	-	-	6.2	1.1	6.2	1.1	3.2	0.4	9.4	1.5
Nowthanna	Mt's	-	-	-	-	-	-	11.9	2.3	11.9	2.3
	Grade ppm	-	-	-	-	-	-	399	794	399	794
	Mlb's U_3O_8	-	-	-	-	-	-	10.5	4.0	10.5	4.0
Total Regional Resource	***Mt's***	**2.9**	**1.2**	**50.6**	**17.2**	**53.5**	**18.4**	**19.0**	**2.9**	**72.5**	**21.3**
	Grade ppm	**551**	**872**	**517**	**918**	**519**	**915**	**365**	**791**	**479**	**898**
	Mlb's U_3O_8	**3.5**	**2.3**	**57.7**	**34.8**	**61.2**	**37.1**	**15.3**	**5.1**	**76.5**	**42.2**

[2] *Refer to Competent Persons' Statement in this report. It can be confirmed that there has been no material change to resources of the Wiluna Project since the last reporting of the Wiluna Project's resources on the 20 November 2013.*

[3] *Tonnes and pounds are quoted to one decimal place which may cause rounding errors when tabulating.*

COMPETENT / QUALIFIED PERSONS' STATEMENTS

The information presented here that relates to mining block model evaluations and reconciliations for the four 100 m x 100 m evaluation areas at Centipede, Millipede, Lake Way and Lake Maitland is based on information compiled by Dr Greg Shirtliff and Mr Sebastian Kneer of Toro Energy Limited and Mr Daniel Guibal of SRK Consulting (Australasia) Pty Ltd. The review of the mining operability for the 100 m x 100 m-evaluation areas was conducted by independent mining engineers, Mr Grant Calderwood of GDC Services and Mr Carl Murray of SRK Consulting (Australasia) Pty Ltd. Mr Guibal takes overall responsibility for the resource estimates of the individual evaluation areas and Dr Shirtliff takes responsibility for the integrity of the data supplied for the estimations. Dr Shirtliff and Mr Murray are Members of the Australasian Institute of Mining and Metallurgy (AusIMM), Mr Guibal is a Fellow of the AusIMM and Mr Kneer is a Member of the Australian Institute of Geoscientists (AIG) and they have sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity they are undertaking to qualify as Competent Persons as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code 2012)'. The Competent Persons consent to the inclusion in this release of the matters based on the information in the form and context in which it appears.

It is important to note that there has been no material change to the resources of the Wiluna Project since the last reporting of the Wiluna Project's resources on the 20th November 2013. As such the competent/qualified persons statement for stated resources on the Wiluna Project remains as follows:

The information presented here that relates to Mineral Resources of the Centipede, Millipede, Lake Way, Lake Maitland, Dawson Hinkler and Nowthanna deposits is based on information compiled by Dr Greg Shirtliff of Toro Energy Limited (with the aid of Mega Uranium Limited geologists Mr Stewart Parker and Mr Robin Cox in the case of Lake Maitland) and Mr Robin Simpson and Mr Daniel Guibal of SRK Consulting (Australasia) Pty Ltd. Mr Guibal takes overall responsibility for the Resource Estimate, and Dr Shirtliff takes responsibility for the integrity of the data supplied for the estimation. Dr Shirtliff is a Member of the Australasian Institute of Mining and Metallurgy (AusIMM), Mr Guibal is a Fellow of the AusIMM and Mr Simpson is a Member of the Australian Institute of Geoscientists (AIG) and they have sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity they are undertaking to qualify as Competent Persons as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code 2012)'. The Competent Persons consent to the inclusion in this release of the matters based on the information in the form and context in which it appears.

JORC Code, 2012 Edition – Table 1 report – Wiluna Uranium Project – Toro Energy Limited

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	• U_3O_8 values are calculated from U values derived from both geochemistry and down-hole gamma radiation measurements. • **Geochemistry (Lake Maitland excluded) –** Toro's geochemical samples on all of the Wiluna deposits except Lake Maitland, represent 0.5m half core lengths (prior to 2013) or full core lengths (2013 and planned into the future) of 100mm sonic drill core. Full core samples provide an 8-10kg sample to the lab, half core samples are half this weight approximately. After crushing the lab splits a 2.5 kg sub-sample for milling (pulverizing) to 90% passing 75micron, before taking an aliquot for U analysis by 4 acid digest ICPMS (prior to 2013) or fusion-ICPMS (2013 and into the future). • In the case of half core samples field duplicates of the core are taken to ensure sample representivity, these field duplicates are the other half of the core that has been sampled. In the case of full core samples, duplicates are taken at the first sample split at the lab, directly after the initial crush, these duplicates are taken with a rotary splitter after pushing the sample back through the crusher after the initial split. It should be noted that due to the size of the sample supplied to the lab, the initial crushing is a two-step process, a primary crush to 10mm and a secondary crush to 3mm. Both these duplicates are taken at a rate of 1 in 20 or 5% of all non-standard samples. Differences in U concentrations between the duplicates and their corresponding samples are used to produce a mean standard sampling error. • Lab duplicates are taken at every stage of the sub-sampling process prior to analysis at the rate of 1 in 20. • Geochemical samples are taken through the ore zones as determined by hand-held scintillometers and if available at the time of sampling, down-hole gamma measurements. The half metre intervals are

Criteria	JORC Code explanation	Commentary
		determined from marking up half metre intervals down the full length of the core from the surface. This is completed at the rig so that any drilling issues can be observed and the geologist can have direct communication 'on the spot' with the driller. To gain geochemical and mineralogical information of waste material or for metallurgical purposes etc, often the entire hole is sampled for geochemistry and a larger suite of elements are analysed for, some having to employ different analytical techniques. • Depth corrections are made to geochemistry samples where appropriate, these are based on comparing the down-hole geochemistry to the down-hole gamma U values and assuming the down-hole depth as measured by the gamma probe during probing is correct. Winch cable stretch is not considered an issue in the Wiluna drilling due to the shallow depth of almost all drilling (maximum depth of approximately 25m). • **Gamma derived eU_3O_8 (Lake Maitland excluded) –** Toro uses Auslog natural gamma probes, either in-house or from external contractors, to measure down-hole gamma radiation on all of the Wiluna deposits, inclusive of Dawson Hinkler but exclusive of Lake Maitland,. Measurements are made every 2 cm with a logging speed of 3.5m per minute. • The gamma probes are used on all holes, which include sonic holes also used for geochemical sampling and air core holes drilled specifically for gamma probe measurements. Sonic core holes (100 mm core) are usually 150mm in diameter and air core holes are usually 100mm in diameter. Approximately 95% of all holes are aircore. • Prior to the drilling program all gamma probes are calibrated at the Adelaide Calibration Model pits in Adelaide, South Australia. During probing operations every 10th hole is logged twice as a duplicate log. Selected holes across the deposits are used as reference holes for relogging to detect drift in the instrument during each program. In 2013 over 50% of all holes drilled at Dawson Hinkler were re-logged with a different probe (from the same contractor) over 3 months after they were drilled to confirm results (results were confirmed). • As protection from hole collapse and to protect the probe, all logging is done inside 40mm or 50mm PVC pipe (unless larger diameter has been used for water bores) with an average wall thickness of 1.9 mm.

Criteria	JORC Code explanation	Commentary
		• Gamma measurements are converted to equivalent U_3O_8 values (eU_3O_8) by an algorithm that takes into account the probe and crystal used, density, hole diameter, ground water where applicable and PVC pipe thickness. • Down-hole gamma probe data is also deconvolved to more accurately reflect what would be expected in nature for down-hole response (gamma curves). • All gamma data is compared with geochemistry data both via down-hole comparisons and overall populations bivariate analysis, and distribution analysis to check for potential error or disequilibrium. To adequately compare with geochemistry gamma probe data is composited into half metre composites at the same intervals represented by the corresponding geochemical samples. • **Geochemistry (Lake Maitland only) –** Mega's geochemical samples on the Lake Maitland deposits represent 0.25 m full core lengths of 83 mm diamond drill core (PQ3). Weights of the geochemical samples range from 2-5 kg approximately. Intervals are determined during core mark-up and identified with plastic core blocks. Samples are dried at 110 °C before weighing and then crushing. After crushing a sub-sample is split using a rotary splitter for milling (pulverizing) to 90% passing 75 micron, before taking an aliquot for U analysis by 4 acid digest ICPMS. All samples with ICPMS results for U above 500 ppm were then re-analysed by fused disc XRF so that all U_3O_8 values from the extensive 2011 drilling program used in the estimation were from fused disc -XRF if at or above 500 ppm or 4 acid digest ICPMS if below 500 ppm. • Due to full core sampling no duplicates are needed to measure in-field sampling error. Duplicates are instead taken at the first sample split at the lab, directly after the initial crush, these duplicates are taken with a rotary splitter after pushing the sample back through the crusher after the initial split at a rate of 1 in 20 or 5% of all non- standard samples. Differences in U concentrations between the duplicates and their corresponding samples are used to produce a mean standard sampling error (results from 2011 are below 10% error). • Lab duplicates are taken at every stage of the sub-sampling process prior to analysis at the rate of 1 in 20. • Geochemical samples are taken through the entire length of each drill hole. The 0.25 m intervals are determined from marking up 0.25 m intervals down the full length of the core from the surface.

Criteria	JORC Code explanation	Commentary
		• Other elements analysed include Ba, Th, Al, Ca, Fe, K, Mg, Mn, S, Sr, Ti and V. • Depth corrections are made to geochemistry samples where appropriate, these are based on comparing the down-hole geochemistry to the down-hole gamma U values and assuming the down-hole depth as measured by the gamma probe during probing is correct. Winch cable stretch is not considered an issue at Lake Maitland drilling due to the shallow depth of (3-9 m on average).No depth corrections were deemed necessary in the most recent and extensive drilling program (2011). • **Gamma derived eU_3O_8 (Lake Maitland only) –** Mega uses a 33 mm Auslog natural gamma probe (S691) 'in-house', to measure down-hole gamma radiation. Measurements are made every 1 or 2 cm with a logging speed of approximately 2 m per minute. • The gamma probes are used on all drill holes, diamond, sonic and aircore. • Prior to the drilling program all gamma probes are calibrated at the Adelaide Calibration Model pits in Adelaide, South Australia. During probing operations selected holes are logged twice as a duplicate log. Some selected holes across the deposits are used as reference holes for re-logging to detect drift in the instrument during each program. • Probing is done as close as practicable after drilling. • Gamma measurements are converted to equivalent U_3O_8 values (eU_3O_8) by an algorithm that takes into account the probe and crystal used, density, hole diameter, ground water where applicable and PVC pipe thickness. • Down-hole gamma probe data is also de-convolved to more accurately reflect what would be expected in nature for down-hole response (gamma curves). • All gamma data is compared with geochemistry data both via down-hole comparisons and overall populations in bivariate analysis, and distribution analysis to check for potential error or disequilibrium. To adequately compare with geochemistry gamma probe data is composited into 0.25 m composites at the same intervals represented by the corresponding geochemical samples.

Criteria	JORC Code explanation	Commentary
		Significant differences between gamma derived eU_3O_8 and geochemical U_3O_8 have been noted in 2011 and historically. Disequilibrium analysis by an independent consultant group (On Site Technology Pty. Ltd.) found a global positive disequilibrium across the entire deposit of 1.18 (average). This factor that was confirmed by the comparison of assays to eU values has been applied to all eU_3O_8 used in the estimation.
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	**All Wiluna deposits excluding Lake Maitland** • Both sonic and aircore drilling techniques are utilized on the Wiluna Project. • The sonic drilling utilizes a 100mm core barrel (inside diameter) with outside casing where needed, producing a 150mm hole diameter and 100mm core. Depending on the ground conditions and thus quality of core being produced, core is retrieved from the 3m barrel in either 1 to 3m length, 1m at a time. Upon exiting the barrel, core is transferred into tubular plastic bags that fit the core before being placed in core trays. • Aircore drilling is conventional with a 72mm bit producing an approximate 100mm diameter hole. **Lake Maitland only** • Diamond, sonic, auger core and air core drilling techniques have all been utilized on the Lake Maitland deposit. • The sonic drilling utilizes a 100mm core barrel (inside diameter) with outside casing where needed, producing a 150mm hole diameter and 100mm core. Depending on the ground conditions and thus quality of core being produced, core is retrieved from the 3m barrel in either 1 to 3m length, 1m at a time. Upon exiting the barrel, core is transferred into tubular plastic bags that fit the core before being placed in core trays. On occasions where the sonic core was being used for density measurements a hard plastic (clear) cylinder that fits the core was used instead to ensure lasting core integrity. • Aircore drilling is conventional with a 72mm bit producing an approximate 100mm diameter hole.

Criteria	JORC Code explanation	Commentary
		Diamond drilling is PQ3, which utilizes an 83.18 mm core barrel (inside diameter) and produces an 83 mm diameter core with an approximate 123 mm diameter hole.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	**All Wiluna deposits excluding Lake Maitland** • Chip sample recoveries are not recorded as the chips are not used for any systematic analysis of uranium concentrations. • Sonic core recoveries are estimated based on a combination of measurement, observation of drilling, the driller's direction, observations made on quality of sample during geological logging and sample weight comparisons to average weights and rock type. It should be noted that precise core recovery estimation on sonic drillcore in the Wiluna deposits is inherently difficult due to expansion and contraction of soft sediments during drilling and during recovery of core from the barrel. • Core loss is minimized by 'casing as we drill' through all ore zones or any zone where the geological information is critical such as for geotechnical purposes. • There is no correlation between estimated core loss and grade • Grade in geochemical samples is also checked against composited gamma derived grades (see above), which acts as another check on errors in the geochemistry that may (or may not) be due to core recovery. **Lake Maitland only** • Sonic core recoveries are estimated based on a combination of measurement, observation of drilling, the driller's direction, observations made on quality of sample during geological logging and sample weight comparisons to average weights and rock type. It should be noted that precise core recovery estimation on sonic drillcore at Lake Maitland is inherently difficult due to expansion and contraction of soft sediments during drilling and during recovery of core from the barrel. • Historically, chip sample recoveries have not been recorded in the database. • Diamond core recoveries have been determined by conventional techniques of identification of lost core by driller and geologist at the rig

Criteria	JORC Code explanation	Commentary
		and during core mark up and measure. Core trays are also weighed without and then with core to estimate core recovery based on assumed SG for particular lithology. • During sonic core drilling core loss is minimized by 'casing as we drill' through all ore zones or any zone where the geological information is critical such as for geotechnical purposes. • To date Toro cannot find any correlation between estimated core loss and grade in the Lake Maitland data. • Grade in geochemical samples is also checked against composited gamma derived grades (see above), which acts as another check on errors in the geochemistry that may (or may not) be due to core recovery.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Geology is not used in the resource estimation process, the reasons for this are explained in more detail below, however, basically the deposit has been found to be correlated more to groundwater and depth from the surface than to any geological unit. Thus the geological logging is adequate for resource estimation. • Current geological logging (all Toro, 2013 onwards at Dawson Hinkler) is considered to be adequate for the stage of mine planning that Toro is currently at on the Wiluna Project. Further work is considered necessary to amalgamate or align historical geology logs and geology to current. • Current logging is both qualitative (subjective geological opinion of rock type and colour and in the case of Lake Maitland, also by limited mineral identification by spectral analysis) and quantitative (recording specific depth intervals and percentages of grain sizes, or in the case of Lake Maitland inclusive of limited quantification of mineralogy by spectral analysis via Hy-logger). Core photographs are taken for each individual metre (prior to 2013) and half metre (2013) after core has been split down the middle for logging and so as to see sedimentological features for logging (avoiding clay smear on outer surface of core made by drill rods). In the case of Lake Maitland, core photographs have been taken for the entire 2011 drilling program,

Criteria	JORC Code explanation	Commentary
		which consists of a total of 201 holes and is spread across the entirety of the deposit. • All drilling intersections have been logged geologically • Toro has not costeaned at Dawson Hinkler.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.*	• As described above, geochemical samples represent 0.5m half core lengths (prior to 2013) or full core lengths (2013 and planned into the future) of 100mm sonic drill core. Aircore chips were not sampled for geochemistry. At Lake Maitland geochemical samples represent 0.25 m full core lengths of 100mm sonic drill core or 83mm diamond core.
	• *For all sample types, the nature, quality and appropriateness of the sample preparation technique.*	• Sample preparation has been described above under 'sampling techniques, it is considered that all sub-sampling and lab preparations are consistent with other laboratories in Australia and overseas and are satisfactory for the intended purpose.
	• *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.*	• Lab duplicates are taken by the lab to test their own sub-sampling techniques, for full core geochemical samples the lab duplicate taken at the first split after the initial crush (sampled with a rotary splitter) is used by Toro to calculate the sampling error.
	• *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.*	• Total sampling errors calculated from half core field duplicates typically range from ±10-20%. Total sampling errors for the first split at the lab in case of full core sampling typically range from ±1-5%.
	• *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• The laboratory used for Toro's geochemical analysis bases all crushing grain sizes and subsequent sub-sampling weights on being inside accepted Gy safety lines for sample representivity. These grains sizes and sub-sample weights have been described above under 'sampling techniques'.

Criteria	JORC Code explanation	Commentary
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	**All Wiluna deposits excluding Lake Maitland** • Prior to 2013 a four acid digest followed by ICPMS was employed for analysis for geochemistry on the other Wiluna deposits – this was assumed to be an almost total rock digest technique although with recognition that highly resistant minerals are sometimes not entirely digested. In 2012 a test was done to compare four acid digest/ICPMS with sodium peroxide fusion followed by ICPMS with fused glass XRF. Analysis of a number of standards suggested that the Fusion/ICPMS was the most accurate. So in 2013, fusion/ICPMS has been used as the bases for all U analyses, however on a number of samples four acid digest/ICPMS and fused glass XRF are still used for comparative purposes. Performance against standards is excellent. • Historical geochemistry data is almost entirely XRF. • Down-hole gamma tools are used as explained above. All tools are Auslog natural gamma probes calibrated at the Adelaide Calibration Model pits in Adelaide, South Australia. • Certified matrix matched standards are used to check analyses at the lab at a rate of 5% or 1 in 20 samples. • Coarse quartz sand is used as blanks and are used at a rate of 5% or 1 in 20 samples as well as being strategically placed in front of and behind samples expected to have high concentrations of U so that thresholds for potential cross-contamination within preparations can be obtained. • Duplicates are used as already explained in detail above. • Limited laboratory checks have been made – in 2013 these represented approximately 3% of all samples.

Criteria	JORC Code explanation	Commentary
		Lake Maitland only • In the extensive 2011 diamond drilling program a four acid digest followed by ICPMS was employed for analysis for U geochemistry (ALS laboratories, Perth)– this was assumed to be an almost total rock digest technique although with recognition that highly resistant minerals are sometimes not entirely digested. Due to these potential issue and the fact that ICPMS has in earlier times had issues dealing with high U concentrations due to dilution factors (etc), the Mega geologists decided to re-analyse all samples with ICPMS results for U of greater than 500 ppm utilizing the XRF technique at the same laboratory (ALS, Perth), regarded by Mega geologists as a better whole rock technique. Performance against standards is acceptable. • Historical geochemistry data is almost entirely XRF. • Down-hole gamma tools are used as explained above. All tools are Auslog natural gamma probes calibrated at the Adelaide Calibration Model pits in Adelaide, South Australia. • “Off the shelf’ OREAS U standards are used to check analyses at the lab at a rate of 2% or 1 in 50 samples. • Coarse quartz sand is used as blanks and are used at a rate of 2% or 1 in 50 samples. • Lab duplicates are used as already explained in detail above, from the primary crush stage and every other sub-sampling stage. Limited laboratory checks have been made – from the most recent drilling (2011) a total of 138 samples were re-analysed for U by 4 acid digest ICPMS by a different commercial laboratory (Genalysis, Perth). The samples were chosen as representative of the following U_3O_8 concentrations – 10% between 100 and 200 ppm U_3O_8, 40% from between 200 and 500 ppm U_3O_8, and 50% from above 500 ppm U_3O_8. Differences between the labs were satisfactory, the largest being approximately 5% on average higher values from the XRF derived

Criteria	JORC Code explanation	Commentary
		U_3O_8 by ALS over the ICPMS U_3O_8 by Genalysis, this was taken into consideration during estimations.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• Limited interlab geochemistry analytical checks are completed for each drilling campaign, the last interlab check represented 3% of all the geochemical samples. Toro has a calibrated (at the Adelaide Calibration Model pits in Adelaide, South Australia) Auslog gamma probe to check the probing results achieved by external contractors. • Hole twinning has not been practiced on the Dawson Hinkler deposit by Toro thus far, rather infill drilling between historical holes. At Lake Maitland, a limited number of holes have been twinned - these include twinned holes drilled by both sonic and diamond core methods. A large proportion (approximately 10%) of the holes at Lake Way have been twinned to compare historical data. • All primary data (gamma log las files, geochemical sample lists, final collar files, geological logs, core photographs, electronic geochemical results, drillers plods, probing plods, deconvolved gamma files, gamma gamma density logs, disequilibrium analysis results etc) are stored on the company server in the appropriate drive and folders. Any hardcopy data, such as official geochemistry results or any paper copy geological logs, are kept in hardcopy in folders and archives as well as being scanned and kept on the company server in the appropriate drives and folders. • Data entry procedures are described in some detail below in section 3 under 'data integrity'. • To date, there has been no significant adjustments made to geochemical assay U_3O_8 data (or to any other elements). Slight adjustments are made to some geochemical assay data to account for depth corrections if an interval error is discovered, this is rare and always restricted to the near surface above mineralized zones.

Criteria	JORC Code explanation	Commentary
		Secular Disequilibrium and associated adjustments to gamma derived eU_3O_8 • Current practice on all drilling programs is to send the processed sample pulp from the laboratory to the Australian Nuclear Science and Technology Organisation (ANSTO) to test for secular disequilibrium across all deposits drilled. • Based on the findings from a disequilibrium analysis by On Site Technologies Pty Ltd in 2011 all gamma data used in the estimation for Lake Maitland has been multiplied by 1.18, the average positive disequilibrium found across the deposit. It is important to note that this has **not been applied to the eU_3O_8 data within the database, it has only been applied to data during the estimation process.** • Adjustments have also been made at Dawson Hinkler based on consistent differences between geochemistry and gamma derived uranium values. All gamma data within the region covered by the 2013 drilling program (which represents a single domain in the resource estimation) has been multiplied by a factor of 1.2 according to the consistent difference found between geochemistry and gamma, further explanation follows - The 2013 drilling was targeted at a single domain within the Dawson Hinkler deposit. The results from the 2013 drilling show a marked difference of some 20% (conservative approximation) between geochemistry and gamma suggesting a positive disequilibrium. QAQC of geochemistry (see above) confirmed the geochemistry results from the 2013 drilling. Re-logging over 50% of the 2013 drill holes with a different probe (same make and model) from an external contractor confirmed the gamma results from the recent drilling. Examination of historical drill data within the same domain revealed a similar difference between gamma and geochemistry. Examination of historical drill data from outside the domain within the rest of the deposit revealed an even greater difference between geochemistry and gamma derived eU_3O_8 values (geochemistry greater than gamma). As a result it was concluded that gamma derived eU_3O_8 values are consistently under-estimating U_3O_8 in the ground and so a factor needed to be applied to the gamma derived values. However, to be conservative, only data within the region where the recent 2013 drilling could confirm this underestimation was multiplied by the factor, and so historical results was not relied upon. Therefore, the factor

Criteria	JORC Code explanation	Commentary
		applied was that found within the domain drilled only (and not the greater factor found outside) and that factor was 1.2, to represent the 20% greater geochemistry derived values over the gamma derived values. • For the mining block model evaluation areas in this ASX release a factor of 1.2 was applied to the results of the block model (after estimation) to account for the systematic discrepancy between geochemical and gamma derived data seen in the sonic drill hole analytical results. The 1.2 factor is conservative in comparison to the actual discrepancy observed, however it is based on the average positive disequilibrium ratio according to the results of a recent study of secular disequilibrium by ANSTO on 2013 pulverised sonic core samples.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• All drill hole collars are pegged to the planned collar location using a differential GPS (DGPS) with base station (currently an Austech ProMark500 and ProFlex500). At the end of the drilling campaigns all collars a picked up using the same DGPS equipment for the final collar locations that are entered into the database. Accuracy of the DGPS is approximately to 100mm in the vertical and 50mm on the horizontal. • Due to all drill holes being shallow (maximum depth of 25m) and vertical no down-hole surveying is required. • The grid system used on the Wiluna Project is Geocentric Datum of Australia (GDA) 94, zone 51. • Topographic control is largely achieved by the DGPS with base station. As stated above, all Toro drill holes are accurate to approximately 100mm on the vertical. At Dawson Hinkler and Lake Maitland all drill holes have been 'pinned' to a topographic surface created from current drill hole collars surveyed in a with a DGPS and base station.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and*	• No exploration results, resource drilling only • The data spacing and distribution has been considered appropriate for the Mineral Resource estimation procedures and classifications applied by the external consultant doing the resource and is based

Criteria	JORC Code explanation	Commentary
	classifications applied.	mainly on variography and continuity shown in the statistical analysis of the data. See below in resource section for further information.
	• *Whether sample compositing has been applied.*	• Centipede/Millipede: Measured resources drilled at 25-35m x 25-35m. Indicated Resources 50m x 50m to 100 m x 100 m drill spacing, with good cover of sonic drilling. Inferred Resources: all other holes within mineralization envelope, greater than 100 x 100m. • Lake Way: all Indicated (75m x 75m drilling, with good sonic drilling cover). • Dawson Hinkler: No Measured resource; Indicated resources 100 x 100 m with some limited 100 m x 200 m drill spacing; Inferred resources greater than 100 x 200 m drill spacing. • Lake Maitland: No Measured resource, drilling grids on average of 100m x 100 m and in some places as close as 5 m x 5 m. • At the Wiluna deposits (excluding Lake Maitland) sample compositing to 0.5m composites has been applied to the 2cm interval eU3O8 data to match the 0.5m geochemical core samples. At Lake Maitland, compositing to 0.25 m composites has been applied to the 1 and 2 cm interval eU3O8 data to match the 0.25 m geochemical core samples.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Sampling is non-subjective (non-biased) down-hole sampling from the surface, either at 1 cm or 2cm intervals in the case of gamma probe data or 0.5m samples in the case of geochemistry. Historical geochemistry represents a similar non-bias down-hole process. The sampling orientation employed provides no bias to the groundwater related distribution of mineralization. • No bias suspected, ore lenses are horizontal and drilling is vertical, cutting mineralization at an approximate right angle (90 degrees).

Criteria	JORC Code explanation	Commentary
Sample security	• *The measures taken to ensure sample security.*	**All Wiluna deposits excluding Lake Maitland** • Sampling of drill core for geochemistry is achieved in the field directly after drilling at the drill site. All samples are bagged firstly in plastic and then again in calico (double bagged). A unique non-descript identifier number is used to number each sample that bares no relation to the deposit or the drill hole. All sample details are entered into a fixed format file ready for later import into the database. Samples are immediately transported by utility to the field camp where they are weighed before being packed into steal 44 gallon drums with lock-down lids and tested for radiation for transport classification. The drums are then fitted on timber pallets and transported to the local transport dock at Wiluna for delivery to Perth. Approximate time between sampling and transport to the laboratory is 4 weeks. • Sampling of gamma derived measurements is achieved by a single contractor using a gamma probe (see sampling techniques above). Raw gamma probe data is converted into a las file and sent to a Perth based office on a daily basis by email. This data is then packaged and sent to the Toro Energy Database Manager, who sends it to the analyst (consultant) for calculation of U concentrations and de-convolution. **Lake Maitland Deposit only** • Core length is measured by drillers and blocks are put in at the end of runs. The core is then picked up by the geologist at the end of hole and taken to the core shed where it is divided into 25cm whole samples and allocated a sample ID tag, this is done by the geologist and field assistant. The core is then logged and core loss is recorded. Core, in the core trays, is then stacked on to pallets (approximately 3 holes per pallet). For sample security, steel lids are used on the top row of trays before the entire pallet is plastic wrapped and steel strapped. Core was then picked up at site and delivered to ALS Perth, where it underwent spectral logging, weighing and assay. • Additionally, upon transfer of the database from Mega to Toro for estimation, all data was converted to raw text files and delivered directly to SRK for the data review prior to estimation so as to avoid

Criteria	JORC Code explanation	Commentary
		any loss of information by converting files into different database formats (Toro and Mega use different databases and database structures).
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• An internal review of geochemical sampling techniques in 2012 lead to a change in practice from non-selective half-core sampling to full core sampling so as to reduce total sampling error. This recommendation was followed in 2013 and has satisfactorily reduced sampling error to below ±10%. • A review by Toro geologists of the Mega drill core sampling techniques (both for geochemistry and gamma measurements [gamma gamma for density and gamma for eU_3O_8 calculations) for the 2011 drilling program found no errors that would affect the resource estimate in any significant way. The spectral analysis based geological model, which has been used to assign density in the block model was found to be highly predictive across the deposit with a limited amount of drill holes, however given the nature of the deposit as shown in a review of multi-element geochemistry (by Toro geologists) and Toro's experience with all of the similar style Wiluna deposits, the model is considered by Toro to be a reasonable interpretation of Lake Maitland geology and in fact in most circumstances a more accurate representation of the geology and geological relationships. • SRK reviewed the database that was to be used for the resource estimation and excluded any errors from the estimation. The number of exclusions was considered too small to have affected the estimation.

Section 2 Reporting of Exploration Results

IMPORTANT: Section 2 has been included here for ASX listing rule purposes only; no exploration conducted by Toro Energy on the Wiluna Uranium Project is reported in this ASX release. The information presented here does not relate to any new or additional resources (or discoveries) from those reported previously (refer to ASX release 20th November, 2013).

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	• The tenements for which the reported results relate to are those tenements holding the resources drilled, which include mining leases M53/1095 (Millipede resource), M53/224 (Centipede resource) and M53/1089 (Lake Maitland resource) and the Exploration lease E53/1132 (Lake Way resource). All resources have been publically declared in the ASX release of 20th November 2013. • All tenements are located in the North East Yilgarn region of Western Australia, just over 710 km NE of Perth and at the northern margins of the Norseman-Wiluna greenstone belt of the Eastern Goldfields. • E53/1132 is entirely owned by Nova Energy Pty. Ltd. a wholly owned subsidiary of Toro Energy Limited. It is not subject to interest, royalties or mortgages to other parties. • M53/1095 is entirely owned by Nova Energy Pty. Ltd. a wholly owned subsidiary of Toro Energy Limited. Toro owns all rights to uranium and MPI Nickel owns non-uranium rights. MPI Nickel have royalty obligations to Outokumpu for gold and nickel only. • M53/224 is entirely owned by Nova Energy Pty. Ltd. a wholly owned subsidiary of Toro Energy Limited. Toro owns all rights to uranium and Kimba resources owns non-uranium rights. • M53/1089 is entirely owned Redport Exploration Pty. Ltd., a wholly owned subsidiary of Toro Energy Limited. • All deposits, as part of Toro's Wiluna Project, are subject to Toro's current negotiations for a mining agreement with the traditional owners. A small area on M53/1095 is subject to a Department of Indigenous Affairs (DIA) listed site, however, there are no DIA sites affecting the area drilled or any part of the Millipede resource as stated at the 200 ppm eU_3O_8 cut-off. • Steps are currently being undertaken by Toro Energy for environmental approval of the Millipede and Lake Maitland resources; Federal and state environmental approval has been granted for the deposits of Centipede and Lake Way.

Criteria	JORC Code explanation	Commentary
	• *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• All stated tenements are in good standing with all government requirements and expenditure.

Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• Most of the uranium deposits of the Wiluna Uranium Project were discovered by Esso Exploration and Production Australia and its various joint venture partners from 176-1979 through regional RAB drilling over radiometric anomalies (government geophysics). Lake Maitland was discovered by Australis Mining NL in 1972. Exploration occurred between this time and 1982 with evaluation of the deposits using mainly RAB and RC drilling but some auger and diamond drilling was also completed. Most mineralised areas were drilled out on 100m centres and the surrounding areas on 200m centres.
		• The grade and thickness of the uranium mineralisation was determined from radiometric logging of all holes. Some chemical assays were also completed and disequilibrium studies carried out.
		• Since that initial exploration and definition of uranium resources various companies have had ownership of the deposits but little further work was completed until 1999 when Acclaim Uranium NL undertook further work at Centipede by gamma logging over 300 of the previous holes as well as drilling a further 120 aircore drill holes. Much of the Lake Way deposit was locked away until 2013 by a Department of Indigenous Affairs (DIA) site covering some 75% of the entire deposit.
		• Nova Energy gained ownership of the Centipede project and undertook various work programmes in 2006 and 2007 including:
		  • Compilation of historical data into a database
		  • Drilling of over 400 aircore drill holes with associated downhole gamma logging and sample assaying
		  • Gamma logging of approximately 100 historical holes where data had been lost
		  • Two large exploration costeans completed with a Wirtgen 2200 continuous miner
		  • Various baseline studies including groundwater, environmental and radiological studies
		  • Acquisition of satellite imagery

Criteria	JORC Code explanation	Commentary
		• Metallurgical studies • Project scoping study Significant work completed by Toro Energy on the Millipede deposit has included: • Detailed airborne magnetic, radiometric and digital terrain model surveys over the project area in 2010 • A resource estimation update of all of the Wiluna uranium deposits by SRK consulting in 2011 • Resource estimation update of the Centipede and Millipede resources by SRK Consulting in 2012 taking into account new density information • First phase 3-D geological modelling of all of the Wiluna Project's deposits in 2012, including Millipede • First phase 3-D ore shell modelling of all of the Wiluna Project's deposits in 2012. • Aircore and sonic core resource drilling in 2013 • A resource estimation update on Millipede, along with all other deposits, in 2013. Significant work completed by Toro Energy on the Lake Way deposit has included: • Sonic and aircore drilling in 2009 and 2010. • Detailed digital terrain model surveys over the project area in 2010 • A resource estimation update of all of the Wiluna uranium deposits by SRK consulting in 2011 • First phase 3-D geological modelling of all of the Wiluna Project's deposits in 2012,

Criteria	JORC Code explanation	Commentary
		• First phase 3-D ore shell modelling of all of the Wiluna Project's deposits in 2012. • Aircore and sonic core resource drilling in 2013 • A resource estimation update in 2013. Significant work completed by Redport Exploration on the Lake Maitland deposit has included: • Infill aircore drilling program in 2005; • Sonic drilling in 2008; • Resource estimation in 2009; • Diamond drilling program in 2011; • Mining study in 2011; • Secular disequilibrium analysis from diamond core pulp in 2012-13. • Toro Energy re-estimated the Lake Maitland resource in 2013.
Geology	• *Deposit type, geological setting and style of mineralisation.*	The uranium deposits of Toro's Wiluna Uranium Project can all be classified as calcrete associated surficial uranium deposits. • **Regional Geology -** The Wiluna Uranium Project is situated in the northeast of the Archean Yilgarn Block close to the Capricorn Orogen, the structural zone formed when the Yilgarn Block and the Pilbara Block joined some 1830-1780 million years ago. The basement rocks at Wiluna are part of the Eastern Goldfields Terrane (2.74 - 2.63 Ga), a succession of greenstone belts geographically enclosed by younger granitoid (gneiss-migmatite-granite, banded gneiss, sinuous gneiss and granitic plutons) that makes up the entire eastern Yilgarn Block and representative of an extensional tectonic regime with brief periods of compression. • The Wiluna deposits themselves are hosted within recent to Holocene sedimentation that sit in the upper reaches of a large southeast to south flowing drainage system that began forming in

Criteria	JORC Code explanation	Commentary
		the Mesozoic within Permian glacial formed tunnel valleys (Broekert and Sandford, 2005). Satellite radiometric images clearly show this drainage system, now a dry largely ephemeral system of salt lakes. • **Local Geology** - Locally, the underlying basement geology is similar for most deposits. Excluding Dawson Hinkler and Lake Maitland, all deposits are underlain by a north to northwest striking metafelsic and intermediate volcanic unit amongst a relatively wide zone of shearing. A thin extension of the greenstones that dominate further to the north and west, are also present beneath the eastern most margins. Greenstones dominate beneath Lake Maitland, however, these are associated with a shear zone to the east of those beneath Wiluna, although in parallel with. At the surface, little of the basement rocks are exposed. The deposits are associated with, although not restricted to calcrete at the current water table within stream and marginal lacustrine sediments deposited around the Holocene, but probably as far back as the Miocene. • The location of uranium mineralisation is controlled by current and palaeo-drainage systems and groundwater regimes and the associated hydro-geochemical conditions. • **Mineralisation** - The principal ore mineral is the uranium vanadate, Carnotite ($K_2[UO_2]_2[VO_4]2.3H_2O$). Carnotite has been found as micro to crypto-crystalline coatings on bedding planes in sediments, in the interstices between sand and silt grains, in voids and fissures within calcrete, dolomitic calcrete, and calcareous silcrete, as well as small concentrations (or ‘blotches’) in silty clay and clay horizons. • The main economic concentration of Carnotite, that targeted for mining, is restricted to a zone some 1-12 metres below the surface that seems to be related to the current water table. The zone is thus not lithologically specific, rather forming a wide flat and

Criteria	JORC Code explanation	Commentary
		relatively continuous lens inhabiting calcrete, silcrete, sandy silts and clays. The calcrete zone is also definitively related to the water table, although its specific relationship with the deposition of the Carnotite remains complex and somewhat unexplained.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• It should be noted that this ASX release does not present results from exploration drilling, rather resource drilling, specifically grade control style drilling grids of 5x5m spacing. • A table is presented below of all drill hole collars and their particulars. All drill holes from the 2014 drilling program for which this ASX announcement applies, were vertical and drilled between 9-12 m deep, except for a single sonic hole of 14 m depth. A total of 1,639 holes were drilled for 16,375 m in the first four of the six Wiluna deposits, of which 71 holes for 644 m were sonic core, the remaining being aircore. A small proportion of the drilling was for the purpose of geotechnical studies related to pit wall design and investigations of the run-of-mine pad and processing plant foundations.
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• There are no exploration results presented in this ASX release, rather block models created from estimations (using ordinary kriging) in Isatis using results from grade control drilling of the resource. See section 3 of JORC table below for further details relating to the data presented in this ASX release.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true*	• There are no exploration results presented in this ASX release, rather block models created from estimations (using ordinary kriging) in Isatis using results from grade control drilling of the resource. See section 3 of JORC table below for further details relating to the data presented in this ASX release.

Criteria	JORC Code explanation	Commentary
	width not known').	• The mineralization lenses of all of the Wiluna Uranium deposits are horizontal in nature. Thus, given that all drill holes are vertical from the surface, and hence perpendicular to mineralization, all stated mineralization intercept thicknesses represent the TRUE thickness of the mineralization lens at the specified cutoff grade.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to, a plan view of drill hole collar locations and appropriate sectional views.*	• All appropriate maps have been included with this ASX release. It should be noted that the drilling has occurred on a 5 x 5 m drill spacing within a 100 x 100 m grid, as shown in the figures attached and in the location within an already JORC compliant resource as shown in the figures attached.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• There are no exploration results presented in this ASX release, rather block models created from estimations (using ordinary kriging) in Isatis using results from grade control drilling of the resource. See section 3 of JORC table below for further details relating to the data presented in this ASX release.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• There are no exploration results presented in this ASX release, rather block models created from estimations (using ordinary kriging) in Isatis using results from grade control drilling of the resource. See section 3 of JORC table below for further details relating to the data presented in this ASX release.
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• There are no exploration results presented in this ASX release, rather block models created from estimations (using ordinary kriging) in Isatis using results from grade control drilling of the resource. See section 3 of JORC table below for further details relating to the data presented in this ASX release. • As this is essentially an infill drilling program with a grade control scaled drilling pattern and not an exploration program, there are no possible extensions to mineralization that can be highlighted as a result of this drilling. No exploration is planned from the basis of this work.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	**All Wiluna deposits excluding Lake Maitland** • Logging and sampling data is entered into a template with fixed formatting and fixed lithological choices (selected from fixed drop-down lists) by the geologist responsible for logging each hole. The template is formatted so that it can be imported directly into a DataShed database. All importing and exporting into and from the database is achieved by a single point of entry/exit responsible for the database (database manager), access for such tasks is restricted to the database manager. All files are transferred from the field to the database manager using a secure commercial based DropBox folder system with automatic back-up and error correction functions. Data files for resource estimation are transferred in a single zip file to the resource consultant, direct from the database manager. • All geological interval and gamma data is validated via a systematic check of down-hole gamma to down-hole scintillometer readings (made for each lithological unit) for every hole (both sonic and aircore). A secondary check on actual lithology logging is made by examining core and chip photographs cross-referenced to the geological logs. All historical data is validated in Isatis against the same data used in previous estimations. **Lake Maitland Only** • All geological logging and sampling is entered into a Toughbook laptop with an offline aQuire data entry program, which contains fixed lithological codes, carry over sample ID's, fixed core lengths and recorded core loss intervals. The program does not allow errors such as overlaps, or sample miss match. At the end of each day (whether for gamma data from probing or geological logging) all data is extracted and sent to the Perth office where it is automatically entered

Criteria	JORC Code explanation	Commentary
		to the sequel server database. This can only be accessed by the externally based database manager, Dusan Dammer of Advanced Data Care Pty. Ltd. or the Mega geologist in charge of Lake Maitland. • All data has undergone a thorough 2 week long validation and integrity check by SRK in consultation with Toro Energy prior to data preparation for resource estimation, including all U_3O_8 and eU_3O_8 values, density values, lithology and lithology models (Vector files etc) and geospatial information (drill hole collars etc).
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	• The competent person responsible for the resource estimate, Daniel Guibal, has not had a visit to site. It is considered that a site visit is not necessary given Mr Guibal's experience with Toro's Wiluna uranium deposits, some 6 years, including numerous estimations, as well as experience elsewhere with calcrete associated surficial uranium deposits.
Geological interpretation	• *The use of geology in guiding and controlling Mineral Resource estimation.* • *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.*	• The geological model is not used in the resource estimate since it has been found that mineralization is not necessarily correlated to any particular rock type, despite being often associated with carbonate or carbonated sediments. The mineralization has been found to be associated with the water table and so is more correlated to depth from the surface than any given lithology, maintaining grade across different lithologies. Thus the geological model for estimation is a simple mineralization envelope based on a concentration of U that represents that concentration where the background population of U ends and the U mineralization exists (in a classic bimodal distribution). In the Wiluna deposits this is 70 ppm U_3O_8 for the Centipede and Millipede deposits and 80 ppm U_3O_8 for the Lake Way, Dawson Hinkler and Nowthanna deposits. At Lake Maitland, this has been determined to be 100 ppm U_3O_8. • Examination of 3D LeapFrog models of different grade shells of the resource give a high level of confidence to the above interpretation of a ground water controlled deposit. • No geological data used in estimation, all data used is based on U values from de-convolved gamma derived equivalents and

Criteria	JORC Code explanation	Commentary
	• *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	geochemistry. U geochemistry is mostly 4 acid digest ICPMS, and fused disc XRF or peroxide fusion digest with ICPMS finish. A large number of cored drill holes (diamond and sonic) have been used to test the validity of the gamma measurements (via geochemistry) – for example all of the 2011 drilling at Lake Maitland, some 201 diamond holes. Where there is geochemistry data available it is given priority over gamma derived equivalents in the resource estimation. Prior to estimation all de-convolved gamma derived data has been multiplied by 1.18 at Lake Maitland and 1.2 in a single domain at Dawson Hinkler (described above) according to the average positive disequilibrium found by independent research and differences between geochemical analysis and down-hole gamma measurements (see above for further details). • The advantage of using a mineralization envelope based on U concentrations only (both chemistry and de-convolved gamma derived equivalents) is that there are few assumptions made. Domains are based on data variability and so in effect, real changes in the behaviour of the data and data distribution. There is no forcing statistical predictions into domains based on lithology that is not necessarily correlated spatially at all times. • A minimum of 5% of all drill holes are required to test the validity of gamma and to introduce into the estimation except in the case of the mine block evaluation areas where 2.5% has been accepted (due to the mine block evaluation study not contributing to any update of the total resource). • Density values used in the resource estimates at Lake Way, Centipede, Millipede, Dawson Hinkler and Nowthanna are single values representing average densities for the entire mineralization envelope. At Lake Maitland density values used in the resource estimate are derived from gamma gamma probe measurements calibrated to real wet and dry density measurements of reference sonic hole cores. The densities are averaged to the different main lithologies in the geological model and applied to the block model according to the boundaries of each lithological unit (acting as density domains). Further information below under ‘bulk density’. • A different geological interpretation, if used in the resource estimate, may affect the results of the resource estimate slightly, however, since geology is not used in estimations a change in geological

Criteria	JORC Code explanation	Commentary
		interpretations would make no difference. • Grade Continuity can be affected by numerous factors, including drilling density which varies from 5m x 5m to 100m x 200m,, nugget effect, itself linked to the type of measurement (geochemical data are more variable than radiometric deconvolved radiometric data), uncertainties on the data themselves due to calibration problems or/and disequilibrium for the radiometric values, sampling/assaying issues for the geochemical measurements (controlled by QA/QC), and geological continuity, which is reasonably established at Wiluna and Lake Maitland. Geology has been controlled by recent to Quaternary sediment deposition with overprinting calcretisation being controlled by the ground water flow.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The Wiluna deposits are surficial with a vertical thickness of a few meters at most. Occasionally deeper (15 to 25m below surface) mineralization exists, but its continuity is not proved, because of the lack of deep drilling
Estimation and modeling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*	• Except in the case of the mining block evaluations, the estimation technique is Uniform Conditioning followed by Localised Uniform Conditioning using the specialised geostatistical software, Isatis. The various steps of the estimation are the following: (1) Use of combined radiometric and geochemical data, with priority given to geochemistry. As discussed above the 2013 gamma data in the westernmost zone of Dawson Hinkler was corrected by a 1.2 factor to account for a systematic discrepancy between geochemical and gamma derived data and at Lake Maitland, a correction factor of 1.18 has been applied to take into account the average secular disequilibrium as found from research (see above). . (2) Creation of a mineralisation envelope using Leapfrog 3D at the cut-offs detailed above were created prior to factoring of the 2013 data. (3) Compositing to 0.5m. (4) Domaining by zones of reasonably consistent grade, or in the case of Lake Maitland, essentially by the strike orientation: NS, NE and NW

Criteria	JORC Code explanation	Commentary
		(5) Top-cuts used at the various deposits include 5000 ppm, 4500 ppm, 2000 ppm, 700 ppm and 500 ppm as well as no top-cut at all depending on the various domains. It has been found that the top-cut has very little impact on mean grade (less than 1%) and variance. No top-cuts at all applied to Lake Maitland and Lake Way. (6) Block model based on 30m x 30m x 0.5m panels for Centipede, Millipede and Lake Way, 50m x 100m x 0.5m for Nowthanna, 200m x 100m x 0.5m for Dawson-Hinkler and 50m x 50m x 0.5m panels for Lake Maitland. The panel sizes are chosen from the average drilling density. (7) Ordinary Kriging estimation of panels, after neighbourhood analysis to optimise quality of kriging. (8) Validation of Kriging results through statistics and swath plots (9) Uniform conditioning (UC) for 10m x 10m x 0.5m Selective Mining Units (SMU), which is a realistic assumption for a future operation where grade control using radiometric information will be possible. (10) Localised Uniform Conditioning: creation of a 10m x 10m x 0.5m block model based on the results of UC at Centipede, Millipede, Lake Way, Dawson Hinkler and Lake Maitland. (11) The tonnage are estimated using a constant dry density as detailed elsewhere in this table. **Mining Block Evaluation Areas Only** The four mining block evaluation areas of 100m x 100m each were created in Lake Way, Centipede, Millipede and Lake Maitland respectively. They were drilled at a systematic 5 m x 5m grid, using air core and down hole gamma logging. Each area was chosen to target: higher grade areas of the resource where the statistical frequency of values is low and the statistical variance is normally high; grades that were close to the proposed mill feed grade for the first ten years of mining; areas of Indicated resource to test the Indicated classification in the resource; and geological diversity. • In the mining block evaluation areas, estimation technique is by Ordinary Kriging using the specialised geostatistical software, Isatis. The various steps of the estimation are the following:

Criteria	JORC Code explanation	Commentary
		(1) Use of radiometric data only. A factor of 1.2 was applied to the results of the block model (after estimation) to account for the systematic discrepancy between geochemical and gamma derived data seen in the sonic drill hole analytical results. The 1.2 factor is conservative in comparison to the actual discrepancy observed, however it is based on the average positive disequilibrium ratio according to the results of a recent study of secular disequilibrium by ANSTO on 2013 pulverised sonic core samples. (2) Creation of a mineralisation envelope using Leapfrog 3D at the cut-offs detailed above. (3) Compositing to 0.5m. (4) No domaining applied (5) No top-cuts applied. (6) Block model based on 5m x 5m x 0.5m panels. The panel sizes are chosen from the average drilling density. (7) Ordinary Kriging estimation of panels, after neighbourhood analysis to optimise quality of kriging. (8) Validation of Kriging results through statistics and swath plots (9) The tonnage are estimated using a constant dry density as detailed elsewhere in this table.
	• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*	• Previous resource estimates (prepared for a number of years by SRK and Mr Daniel Guibal) are available and are considered in all current estimations.
	• *The assumptions made regarding recovery of by-products.*	• No by-products are assumed to be recovered nor are any planned to be recovered.
	• *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).*	• Currently there are no geostatistical estimations made on deleterious elements, however, such elements have been included in the analysis

Criteria	JORC Code explanation	Commentary
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* • • *Any assumptions behind modelling of selective mining units.* • *Any assumptions about correlation between variables.* • *Description of how the geological interpretation was used to control the resource estimates.* • *Discussion of basis for using or not using grade cutting or capping.* • *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	of drill core samples in 2013 and so such estimations will be able to be accomplished in the future as more coverage across the deposits is achieved. Current analysis of drill core geochemistry and Metallurgical samples strongly suggests there are no significant economic issues related to deleterious elements. • See above • See above • No assumptions • See above – no geological control in any of the 2012 JORC compliant resources. • See above • See above
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages are dry tonnages
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• Grade-tonnage curve are provided for a range of cut-offs. Optimal cut-off will be determined from the mining studies.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• The Lake Maitland deposit will be incorporated into Toro Energy's greater Wiluna Project, which includes the Centipede, Millipede, Lake Way, Dawson Hinkler and Nowthanna deposits. The proposed mining methods, metallurgy/processing and environmental management/factors will be the same as those publically outlined by Toro for the Wiluna Project. • Mining technique has been tested successfully on site, the main points follow. • Shallow strip mining to 15m maximum depth (approximately 8 m at Maitland) using a combination of a Vermeer surface miner, loader and articulated trucks. • 25-50cm benches

Criteria	JORC Code explanation	Commentary
		• De-watering of pits for process water • In-pit tailings disposal below natural ground surface in lined pits, progressive compartmental mining, tailings and rehabilitation • Current - strip 3.8:1, using 250ppm cut-off • Up to a 14 year life of mine, regional resources increase to 20+ years dependent on future approvals • 5 years at Centipede followed by Millipede, Lake Maitland, Lake Way and Dawson Hinkler.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	• Laboratory scale pilot plant has been successfully trialled that includes all of the currently proposed process from crushing/grinding to product – actual product produced. Every part of the processing circuit has been tested and/or had research associated with it. Main factors follow. • Alkaline tank leach with direct precipitation. • Target production is 780 tpa U_3O_8 • Processing 1.3 Mtpa at a head grade of 716ppm U_3O_8 • Processing plant is planned to be located on the Centipede deposit related tenements.
Environmen-tal factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• Two of the Wiluna deposits have been approved for mining by the West Australian EPA as part of the Wiluna Uranium Project and thus the project has gone through the Environmental Review and Management Programme process (The ERMP and all of the associated documents can be found on the Toro Energy website at http://www.toroenergy.com.au/sustainability/health-safety/environmental-review-and-management-programme-ermp/ Main factors follow. • Shallow open pit mining • In-pit tailings disposal below natural ground surface in lined pits, progressive compartmental mining, tailings and rehabilitation – no tailings disposal planned for Dawson Hinkler deposit site. • Tailings integrity modelled for 10,000 years • Mining footprint returned as close as possible to natural land surface level • No standing landforms remain post closure

Criteria	JORC Code explanation	Commentary
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	**All Wiluna deposits excluding Lake Maitland** • Density has been averaged so that a single density is applied to across the block model. • Density derived by consensus from surrounding deposits for Dawson Hinkler. **Lake Maitland only** • Density determined by calibrated gamma gamma probe measurements down drill holes from across the entirety of the deposit (predominantly the 2011 drilling campaigns). Gamma gamma probe calibrated directly with reference sonic core holes whereby both dry and wet density measurements were obtained. Gamma gamma measurements were found to be matching wet density and so all measurements were re-calibrated to a dry density using both the wet and dry density determinations on the sonic core. Density was then averaged over geological units (determined as explained above) so that each geological domain within the block model had a single average dry density.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	• The classification is based on the consideration of drill spacing, existence of geochemical data in such numbers that the radiometric data are well supported and finally the quality of the estimation as measured by kriging slope of regression. • Lake Way: all Indicated (75m x 75m drilling, with good sonic drilling cover). • Dawson Hinkler: No Measured resource; Indicated resources 100 x 100 m with some limited 100 m x 200 m drill spacing; Inferred resources greater than 100 x 200 m drill spacing. • Lake Maitland: No Measured resource, drilling grids on average of 100m x 100 m and in some places as close as 5 m x 5 m.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• There has been no audit of the resources reporting material change within this ASX release, other than internal Toro assessment and geological interpretation.

Criteria	JORC Code explanation	Commentary
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.*	• As mentioned, the classification is partly based on the quality of kriging. In addition, since 2009, various drilling campaigns took place at Wiluna in particular and there has been a good consistency of the estimates. • There is clearly more uncertainty at the individual panel level. Other factors having an impact on the estimation are: Disequilibrium; current measurements (2011) suggest that a significant positive disequilibrium exists at Lake Maitland. This has been established at 1.186 by consultant On Site Technologies and confirmed by further Golder Associates analysis of downhole gamma work compared with laboratory analysis of diamond core. Results from secular disequilibrium analysis by ANSTO of pulverised core from 2013 suggests a positive disequilibrium of at least 1.2 (average) exists at Millipede, Lake Way and Dawson Hinkler. This is considered conservative given observed differences between down-hole gamma and geochemistry.
	• *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• • The relationship between radiometric values and geochemical data can be variable at the local scale. • The assaying methods, as there are indications that XRF tends to overestimate grades by about 5% (by comparison to 4 acid digest ICPMS). • The cut-off grades; due to the estimation method (UC), the high cut-off grades (over 500 ppm) which depend on the modelling of the tail of the grade distributions are more uncertain at local level • No production statistics available – not an operating mine

Section 4 Estimation and Reporting of Ore Reserves

NOT APPLICABLE – NO RESERVES REPORTED

Section 5 Estimation and Reporting of Diamonds and Other Gemstones

NOT APPLICABLE – URANIUM ONLY

Drill Hole Table

All holes drilled vertical - 90 degrees to surface – hole depth is end of hole – holes not in order, grouped to deposit

Hole_ID	E	N	RL	Type	Depth (m)	Hole_ID	E	N	RL	Type	Depth (m)
WAC1546	310176.1	6992127	471.17	AC	12	WAC1599	310226	6992107	471.08	AC	9
WAC1547	310176	6992117	471.11	AC	12	WAC1600	310225.9	6992117	471.11	AC	9
WAC1548	310176	6992107	471.12	AC	12	WAC1601	310226.3	6992127	471.04	AC	9
WAC1549	310175.9	6992097	471.17	AC	12	WAC1602	310236.1	6992127	471.03	AC	9
WAC1550	310175.7	6992078	471.13	AC	12	WAC1603	310236.2	6992117	471.07	AC	9
WAC1551	310175.8	6992067	471.13	AC	12	WAC1604	310236.1	6992107	471.04	AC	9
WAC1552	310175.6	6992057	471.17	AC	12	WAC1605	310236.1	6992097	471.04	AC	9
WAC1553	310175.6	6992047	471.14	AC	12	WAC1606	310236	6992087	471.1	AC	9
WAC1554	310175.5	6992037	471.10	AC	12	WAC1607	310235.9	6992077	471.09	AC	9
WAC1555	310185.8	6992037	471.12	AC	12	WAC1608	310235.9	6992067	471.09	AC	9
WAC1556	310185.9	6992047	471.13	AC	12	WAC1609	310235.9	6992057	471.06	AC	9
WAC1557	310186	6992057	471.17	AC	12	WAC1610	310235.9	6992047	471.09	AC	9
WAC1558	310186	6992067	471.15	AC	12	WAC1611	310236.2	6992037	471.13	AC	9
WAC1559	310186	6992077	471.07	AC	12	WAC1612	310246.2	6992037	471.1	AC	9
WAC1560	310185.9	6992087	471.12	AC	12	WAC1613	310246	6992047	471.07	AC	9
WAC1561	310186.1	6992097	471.12	AC	12	WAC1614	310246	6992057	471.04	AC	9
WAC1562	310186.2	6992107	471.13	AC	12	WAC1615	310246	6992067	471.06	AC	9
WAC1563	310186	6992117	471.15	AC	12	WAC1616	310246	6992077	471.01	AC	9
WAC1564	310186	6992127	471.11	AC	12	WAC1617	310246.1	6992087	471.04	AC	9
WAC1565	310196	6992127	471.13	AC	12	WAC1618	310246	6992107	471.05	AC	9
WAC1566	310195.8	6992117	471.10	AC	9	WAC1619	310245.9	6992117	471.03	AC	9
WAC1567	310195.9	6992097	471.13	AC	9	WAC1620	310245.9	6992127	471.01	AC	9
WAC1568	310195.8	6992087	471.10	AC	9	WAC1621	310256.1	6992127	471.07	AC	9
WAC1569	310195.7	6992077	471.11	AC	9	WAC1622	310256	6992117	471.02	AC	9
WAC1570	310195.6	6992067	471.14	AC	9	WAC1623	310256	6992107	471.07	AC	9
WAC1571	310195.7	6992052	471.12	AC	9	WAC1624	310255.9	6992097	471.09	AC	9
WAC1572	310196	6992042	471.12	AC	9	WAC1625	310255.8	6992087	471.02	AC	9
WAC1573	310205.7	6992037	471.13	AC	9	WAC1626	310255.8	6992077	471.04	AC	9
WAC1574	310206	6992047	471.15	AC	9	WAC1627	310255.9	6992067	471.02	AC	9
WAC1575	310205.9	6992057	471.16	AC	9	WAC1628	310255.8	6992057	471.04	AC	9
WAC1576	310206	6992067	471.13	AC	9	WAC1629	310255.8	6992047	470.98	AC	9
WAC1577	310206.1	6992077	471.10	AC	9	WAC1630	310256	6992037	471.09	AC	9
WAC1578	310206	6992087	471.11	AC	9	WAC1631	310265.8	6992037	471.05	AC	9
WAC1579	310206.2	6992097	471.11	AC	9	WAC1632	310265.9	6992047	471.04	AC	9
WAC1580	310206.3	6992107	471.15	AC	9	WAC1633	310265.9	6992067	471.04	AC	9
WAC1581	310206.2	6992117	471.10	AC	9	WAC1634	310265.9	6992077	471.06	AC	9
WAC1582	310206.2	6992127	471.10	AC	9	WAC1635	310265.9	6992087	470.98	AC	9
WAC1583	310216.2	6992127	471.08	AC	9	WAC1636	310265.9	6992097	471.06	AC	9
WAC1584	310216	6992117	471.04	AC	9	WAC1637	310265.9	6992107	471.02	AC	9
WAC1585	310215.9	6992107	471.05	AC	9	WAC1638	310265.9	6992117	470.97	AC	9
WAC1586	310215.7	6992097	471.06	AC	9	WAC1639	310266	6992127	471.02	AC	9
WAC1587	310215.8	6992082	471.10	AC	9	WAC1640	310180.5	6992132	471.08	AC	9
WAC1588	310215.7	6992072	471.08	AC	9	WAC1641	310180.7	6992122	471.07	AC	9
WAC1589	310215.6	6992062	471.07	AC	9	WAC1642	310180.8	6992112	471.1	AC	9
WAC1590	310215.8	6992052	471.10	AC	9	WAC1643	310180.8	6992102	471.12	AC	9
WAC1591	310215.9	6992042	471.07	AC	9	WAC1644	310180.8	6992092	471.09	AC	9
WAC1592	310226	6992037	471.14	AC	9	WAC1645	310180.9	6992082	471.08	AC	9
WAC1593	310226.2	6992047	471.14	AC	9	WAC1646	310180.8	6992072	471.19	AC	9
WAC1594	310226	6992057	471.16	AC	9	WAC1647	310180.8	6992062	471.16	AC	9
WAC1595	310225.9	6992067	471.06	AC	9	WAC1648	310180.7	6992052	471.16	AC	9
WAC1596	310226	6992077	471.11	AC	9	WAC1649	310180.7	6992042	471.15	AC	9
WAC1597	310226.1	6992087	471.08	AC	9	WAC1650	310191.1	6992042	471.15	AC	9
WAC1598	310225.9	6992097	471.07	AC	9	WAC1651	310191.1	6992052	471.09	AC	9
WAC1652	310191.1	6992062	471.11	AC	9						

WAC1653	310191	6992072	471.10	AC	9	WAC1716	310240.6	6992062	471.05	AC	9
WAC1654	310191	6992082	471.14	AC	9	WAC1719	310251.3	6992042	471.08	AC	9
WAC1655	310191	6992092	471.13	AC	9	WAC1720	310251.1	6992052	471.01	AC	9
WAC1656	310191	6992102	471.14	AC	9	WAC1721	310251	6992062	471.03	AC	9
WAC1657	310191.1	6992112	471.13	AC	9	WAC1722	310250.9	6992072	471.00	AC	9
WAC1658	310191.1	6992122	471.15	AC	9	WAC1723	310250.9	6992082	471.05	AC	9
WAC1659	310191.2	6992132	471.14	AC	9	WAC1724	310251	6992092	471.05	AC	9
WAC1660	310200.9	6992132	471.12	AC	9	WAC1725	310250.8	6992102	471.04	AC	9
WAC1661	310200.9	6992122	471.11	AC	9	WAC1726	310251.1	6992112	471.05	AC	9
WAC1662	310200.8	6992112	471.10	AC	9	WAC1727	310251.1	6992122	471.01	AC	9
WAC1663	310200.9	6992102	471.11	AC	9	WAC1728	310251	6992132	471.03	AC	9
WAC1664	310200.8	6992092	471.08	AC	9	WAC1729	310261.1	6992132	470.99	AC	9
WAC1665	310200.9	6992082	471.09	AC	9	WAC1730	310261	6992122	470.92	AC	9
WAC1666	310200.8	6992072	471.11	AC	9	WAC1731	310260.9	6992112	470.94	AC	9
WAC1667	310200.8	6992062	471.12	AC	9	WAC1732	310260.8	6992102	471.00	AC	9
WAC1668	310200.8	6992052	471.14	AC	9	WAC1733	310260.9	6992092	471.08	AC	9
WAC1669	310200.9	6992042	471.14	AC	9	WAC1734	310261	6992082	471.11	AC	9
WAC1670	310210.9	6992042	471.09	AC	9	WAC1735	310261	6992072	471.05	AC	9
WAC1671	310211.1	6992052	471.12	AC	9	WAC1736	310260.9	6992062	471.03	AC	9
WAC1672	310211	6992062	471.09	AC	9	WAC1737	310260.9	6992052	471.08	AC	9
WAC1673	310211	6992072	471.12	AC	9	WAC1738	310260.8	6992042	470.95	AC	9
WAC1674	310211.1	6992082	471.08	AC	9	WAC1739	310270.9	6992042	471.00	AC	9
WAC1675	310211.1	6992092	471.09	AC	9	WAC1740	310271	6992052	471.05	AC	9
WAC1676	310211.1	6992102	471.08	AC	9	WAC1741	310271	6992062	470.98	AC	9
WAC1677	310211	6992112	471.09	AC	9	WAC1742	310270.9	6992072	471.00	AC	9
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WAC1705	310231.2	6992102	471.08	AC	9	WAC1761	310190.9	6992047	471.15	AC	9
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WAC1707	310231.1	6992122	471.04	AC	9	WAC1763	310190.7	6992067	471.08	AC	9
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WAC1777	310210.7	6992057	471.11	AC	9
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WAC1914	310256.1	6992052	471.04	AC	9
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WAC1923	310266.3	6992092	471.03	AC	9
WAC1924	310246.1	6992092	471.04	AC	9
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WAC1941	310265.9	6992042	471.06	AC	9
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WS0133	310195.9	6992062	471.12	SON	10
WS0134	310175.7	6992087	471.11	SON	10
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WS0136	310195.9	6992107	471.09	SON	10
WS0137	310235.9	6992072	471.04	SON	10
WS0138	310246.1	6992097	471.04	SON	10
WS0139	310270.8	6992107	470.95	SON	10
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WS0141	310215.9	6992087	471.02	SON	10
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WAC0472	233763.1	7043769	492.30	AC	12
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WAC0484	233745.5	7043772	492.21	AC	12
WAC0485	233736.3	7043768	492.19	AC	12
WAC0486	233727.3	7043775	492.23	AC	12
WAC0487	233737	7043779	492.14	AC	12
WAC0488	233746.2	7043783	492.22	AC	12
WAC0489	233755.3	7043787	492.30	AC	12
WAC0490	233764.5	7043791	492.23	AC	12
WAC0491	233774.1	7043795	492.22	AC	12
WAC0492	233782.9	7043799	492.21	AC	12
WAC0493	233792	7043803	492.22	AC	15
WAC0494	233801.6	7043807	492.17	AC	12
WAC0495	233797.1	7043816	492.27	AC	12
WAC0496	233787.9	7043812	492.31	AC	12
WAC0497	233778.7	7043808	492.24	AC	12
WAC0498	233769.8	7043804	492.28	AC	12
WAC0499	233760.4	7043800	492.31	AC	12
WAC0500	233751.4	7043796	492.27	AC	12
WAC0501	233742	7043792	492.33	AC	12
WAC0502	233728.3	7043787	492.09	AC	12
WAC0503	233719.7	7043794	492.15	AC	12
WAC0504	233729.2	7043798	492.31	AC	12
WAC0505	233738.4	7043802	492.27	AC	12
WAC0506	233747.5	7043805	492.31	AC	12
WAC0507	233756.8	7043809	492.21	AC	12
WAC0508	233766	7043813	492.33	AC	12
WAC0509	233775.2	7043817	492.31	AC	15
WAC0510	233784.3	7043821	492.17	AC	15
WAC0511	233793.4	7043825	492.20	AC	12
WAC0512	233789.3	7043834	492.15	AC	12
WAC0513	233780.3	7043830	492.13	AC	12
WAC0514	233770.9	7043827	492.26	AC	12
WAC0515	233752.8	7043819	492.28	AC	12
WAC0516	233743.6	7043815	492.28	AC	12
WAC0517	233734.3	7043811	492.22	AC	12
WAC0518	233725.2	7043807	492.27	AC	12
WAC0519	233716	7043803	492.22	AC	12
WAC0520	233711.8	7043812	492.31	AC	12
WAC0521	233716.5	7043814	492.28	AC	12
WAC0522	233734.9	7043822	492.31	AC	12
WAC0523	233744.3	7043826	492.25	AC	12
WAC0524	233767.1	7043836	492.22	AC	12
WAC0525	233776.6	7043840	492.25	AC	12
WAC0526	233812.4	7043768	492.15	AC	15
WAC0527	233802.9	7043764	492.21	AC	12
WAC0528	233794	7043760	492.24	AC	12
WAC0529	233784.7	7043756	492.27	AC	15
WAC0530	233775.4	7043752	492.22	AC	12
WAC0531	233765.9	7043748	492.25	AC	12

WAC0532	233756.9	7043744	492.23	AC	12	WAC0588	233742	7043754	492.30	AC	12
WAC0533	233738.6	7043736	492.27	AC	15	WAC0589	233751.2	7043758	492.29	AC	12
WAC0534	233757.5	7043756	492.34	AC	12	WAC0590	233760.1	7043762	492.30	AC	12
WAC0535	233766.9	7043760	492.27	AC	12	WAC0591	233769.3	7043766	492.28	AC	12
WAC0536	233776.2	7043764	492.18	AC	12	WAC0592	233778.6	7043770	492.26	AC	15
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WAC0538	233794.2	7043771	492.30	AC	12	WAC0594	233797.2	7043778	492.22	AC	12
WAC0539	233803.5	7043775	492.29	AC	12	WAC0595	233806.2	7043781	492.46	AC	12
WAC0540	233804.5	7043786	492.27	AC	12	WAC0596	233807.1	7043793	492.22	AC	15
WAC0541	233795.6	7043783	492.34	AC	12	WAC0597	233798.2	7043789	492.24	AC	12
WAC0542	233786.2	7043778	492.27	AC	12	WAC0598	233788.7	7043785	492.24	AC	12
WAC0543	233777.3	7043775	492.26	AC	12	WAC0599	233779.5	7043781	492.26	AC	12
WAC0544	233768.1	7043771	492.28	AC	12	WAC0600	233770.3	7043777	492.30	AC	12
WAC0545	233758.6	7043767	492.28	AC	12	WAC0601	233761	7043773	492.27	AC	12
WAC0546	233749.8	7043763	492.30	AC	12	WAC0602	233752.3	7043769	492.15	AC	12
WAC0547	233740.2	7043759	492.20	AC	12	WAC0603	233742.6	7043765	492.27	AC	12
WAC0548	233731.2	7043755	492.30	AC	12	WAC0604	233733.5	7043762	492.18	AC	12
WAC0549	233726.4	7043764	492.27	AC	15	WAC0605	233724.9	7043769	492.25	AC	12
WAC0550	233740.4	7043770	492.19	AC	12	WAC0606	233734	7043773	492.24	AC	12
WAC0551	233749.8	7043774	492.22	AC	12	WAC0607	233743.3	7043776	492.25	AC	12
WAC0552	233759.2	7043778	492.21	AC	12	WAC0608	233752.2	7043780	492.27	AC	12
WAC0553	233772.5	7043784	492.23	AC	12	WAC0609	233761.5	7043784	492.31	AC	12
WAC0554	233781.6	7043787	492.20	AC	12	WAC0610	233771.2	7043788	492.27	AC	12
WAC0555	233790.7	7043791	492.22	AC	12	WAC0611	233780	7043792	492.20	AC	12
WAC0556	233800.4	7043795	492.23	AC	15	WAC0612	233793.6	7043798	492.26	AC	12
WAC0557	233786.2	7043844	492.17	AC	12	WAC0613	233802.7	7043802	492.25	AC	12
WAC0558	233772.2	7043838	492.24	AC	12	WAC0614	233799.4	7043811	492.27	AC	15
WAC0559	233763.2	7043834	492.26	AC	12	WAC0615	233790.2	7043807	492.25	AC	12
WAC0560	233758.4	7043832	492.32	AC	12	WAC0616	233781.1	7043803	492.28	AC	12
WAC0561	233753.7	7043830	492.30	AC	15	WAC0617	233771.9	7043800	492.28	AC	12
WAC0562	233749	7043828	492.31	AC	12	WAC0618	233762.5	7043796	492.24	AC	12
WAC0563	233740.2	7043824	492.33	AC	12	WAC0619	233753.2	7043791	492.31	AC	12
WAC0564	233730.6	7043820	492.31	AC	12	WAC0620	233744.2	7043788	492.26	AC	12
WAC0565	233721.5	7043816	492.32	AC	8	WAC0621	233735	7043784	492.14	AC	12
WAC0566	233707.7	7043810	492.27	AC	12	WAC0622	233725.7	7043780	492.24	AC	12
WAC0567	233710.9	7043801	492.30	AC	12	WAC0623	233717.3	7043787	492.15	AC	12
WAC0568	233720.1	7043805	492.27	AC	12	WAC0624	233726.3	7043791	492.27	AC	12
WAC0569	233729.3	7043809	492.24	AC	12	WAC0625	233735.8	7043795	492.31	AC	12
WAC0570	233738.6	7043813	492.30	AC	12	WAC0626	233744.5	7043799	492.27	AC	12
WAC0571	233748	7043817	492.32	AC	15	WAC0627	233753.8	7043803	492.28	AC	12
WAC0572	233757.5	7043821	492.26	AC	12	WAC0628	233763.1	7043807	492.29	AC	12
WAC0573	233761.8	7043822	492.27	AC	12	WAC0629	233772.2	7043811	492.27	AC	12
WAC0574	233766.3	7043824	492.25	AC	12	WAC0630	233781.5	7043815	492.23	AC	15
WAC0575	233775.5	7043828	492.20	AC	12	WAC0631	233790.8	7043818	492.27	AC	12
WAC0576	233784.7	7043832	492.20	AC	12	WAC0632	233792.3	7043830	492.19	AC	12
WAC0577	233815.2	7043774	492.23	AC	15	WAC0633	233782.2	7043826	492.29	AC	12
WAC0578	233806.1	7043770	492.31	AC	12	WAC0634	233787	7043828	492.23	AC	12
WAC0579	233796	7043767	492.16	AC	15	WAC0635	233777.1	7043824	492.26	AC	15
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WAC0581	233778.3	7043759	492.31	AC	15	WAC0637	233759.2	7043816	492.27	AC	12
WAC0582	233769.1	7043755	492.30	AC	15	WAC0638	233750.5	7043812	492.29	AC	12
WAC0583	233759.8	7043751	492.29	AC	12	WAC0639	233740.8	7043808	492.27	AC	12
WAC0584	233750.3	7043747	492.27	AC	15	WAC0640	233731.8	7043804	492.21	AC	12
WAC0585	233741.5	7043743	492.20	AC	12	WAC0641	233722.3	7043800	492.22	AC	12
WAC0586	233736.6	7043741	492.18	AC	12	WAC0642	233713.5	7043796	492.16	AC	12
WAC0587	233733.5	7043750	492.26	AC	12	WAC0643	233708.7	7043806	492.25	AC	12

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WAC0646	233736.8	7043817	492.29	AC	12	WAC0702	238417.9	7029852	491.56	AC	9
WAC0647	233746.2	7043821	492.25	AC	12	WAC0703	238426.2	7029858	491.57	AC	9
WAC0648	233755.2	7043825	492.26	AC	12	WAC0704	238434.1	7029864	491.63	AC	9
WAC0649	233764.8	7043829	492.28	AC	12	WAC0705	238442.2	7029870	491.56	AC	9
WAC0650	233773.7	7043833	492.28	AC	12	WAC0706	238458.6	7029881	491.56	AC	12
WAC0651	233783	7043837	492.25	AC	12	WAC0707	238466.5	7029886	491.57	AC	9
WAC0652	233779.4	7043846	492.29	AC	12	WAC0708	238474.9	7029893	491.57	AC	9
WAC0653	233770	7043842	492.30	AC	12	WAC0709	238483.4	7029899	491.60	AC	9
WAC0654	233760.9	7043838	492.29	AC	12	WAC0710	238491	7029904	491.53	AC	9
WAC0655	233751.8	7043834	492.29	AC	15	WAC0711	238497.4	7029896	491.51	AC	9
WAC0656	233742.5	7043830	492.28	AC	12	WAC0712	238489.3	7029890	491.69	AC	12
WAC0657	233733	7043826	492.30	AC	12	WAC0713	238481.6	7029885	491.66	AC	9
WAC0658	233724	7043823	492.28	AC	12	WAC0714	238472.9	7029878	491.58	AC	9
WAC0659	233714.7	7043819	492.29	AC	12	WAC0715	238465	7029873	491.60	AC	9
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WAC0661	233719.1	7043782	492.21	AC	12	WAC0717	238448.7	7029862	491.59	AC	9
WAC0662	238394.9	7029885	491.55	AC	12	WAC0718	238440	7029856	491.53	AC	9
WAC0663	238403.3	7029891	491.58	AC	12	WAC0719	238432.1	7029850	491.47	AC	9
WAC0664	238411.6	7029897	491.50	AC	12	WAC0720	238423.9	7029844	491.53	AC	9
WAC0665	238419.5	7029902	491.61	AC	12	WAC0721	238429.4	7029836	491.52	AC	9
WAC0666	238427.8	7029908	491.73	AC	12	WAC0722	238437.2	7029842	491.55	AC	9
WAC0667	238436.1	7029914	491.71	AC	12	WAC0723	238445.6	7029848	491.62	AC	9
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WAC0669	238451.9	7029925	491.58	AC	12	WAC0725	238462.1	7029859	491.64	AC	9
WAC0670	238460.4	7029931	491.69	AC	12	WAC0726	238470.2	7029865	491.67	AC	9
WAC0671	238468.1	7029937	491.68	AC	12	WAC0727	238478.4	7029870	491.66	AC	9
WAC0672	238474.8	7029929	491.60	AC	12	WAC0728	238486.7	7029876	491.69	AC	9
WAC0673	238466.5	7029923	491.67	AC	12	WAC0729	238494.8	7029882	491.72	AC	9
WAC0674	238458.4	7029917	491.68	AC	12	WAC0730	238502.9	7029888	491.64	AC	9
WAC0675	238449.8	7029911	491.78	AC	12	WAC0731	238509	7029880	491.72	AC	9
WAC0676	238441.8	7029906	491.68	AC	12	WAC0732	238500.6	7029874	491.79	AC	9
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WAC0678	238425.2	7029895	491.56	AC	12	WAC0734	238484.2	7029862	491.76	AC	9
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WAC0680	238409	7029883	491.50	AC	12	WAC0736	238468.1	7029851	491.62	AC	9
WAC0681	238400.7	7029877	491.46	AC	9	WAC0737	238459.7	7029845	491.58	AC	9
WAC0682	238406.1	7029869	491.47	AC	9	WAC0738	238451.6	7029839	491.52	AC	9
WAC0683	238414.6	7029875	491.51	AC	9	WAC0739	238443.5	7029834	491.56	AC	9
WAC0684	238422.6	7029880	491.57	AC	9	WAC0740	238435.3	7029828	491.52	AC	9
WAC0685	238431	7029886	491.62	AC	9	WAC0741	238440.8	7029820	491.51	AC	9
WAC0686	238439.2	7029892	491.62	AC	9	WAC0742	238449.2	7029826	491.54	AC	9
WAC0687	238447.4	7029897	491.69	AC	9	WAC0743	238457.4	7029831	491.52	AC	9
WAC0688	238455.3	7029903	491.68	AC	9	WAC0744	238465.3	7029837	491.52	AC	9
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WAC0695	238461.6	7029895	491.59	AC	9	WAC0751	238520.5	7029863	491.65	AC	9
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WAC0697	238444.9	7029884	491.60	AC	9	WAC0753	238503.9	7029852	491.79	AC	9
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WAC0828	236074.9	7029243	491.83	AC	9
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WAC0836	236048.3	7029298	491.86	AC	9
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WAC0841	236056.7	7029304	491.84	AC	9
WAC0842	236062.5	7029296	491.89	AC	12
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WAC0870	238482.9	7029855	491.76	AC	9	WAC0926	238432.3	7029893	491.64	AC	9
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WAC0872	238499.2	7029867	491.70	AC	9	WAC0928	238448.5	7029905	491.71	AC	9
WAC0873	238507.5	7029873	491.77	AC	9	WAC0929	238456.7	7029910	491.75	AC	9
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WAC0879	238452.9	7029846	491.63	AC	9	WAC0935	238435	7029907	491.67	AC	9
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WAC0881	238436.4	7029834	491.56	AC	9	WAC0937	238418.5	7029895	491.54	AC	9
WAC0882	238428.5	7029829	491.48	AC	9	WAC0938	238410.4	7029890	491.56	AC	9
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WAC0887	238455.2	7029860	491.58	AC	9	WAC0943	238455.9	7029824	491.59	AC	9
WAC0888	238463.2	7029866	491.69	AC	9	WAC0944	238464.4	7029830	491.59	AC	9
WAC0889	238471.7	7029872	491.61	AC	12	WAC0945	238472.2	7029836	491.62	AC	9
WAC0890	238479.5	7029877	491.65	AC	9	WAC0946	238466.9	7029844	491.60	AC	9
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WAC0896	238466.1	7029880	491.56	AC	9	WAC0952	238461.5	7029816	491.57	AC	9
WAC0897	238457.7	7029874	491.58	AC	9	WAC0953	238469.7	7029822	491.63	AC	9
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WAC0899	238441.5	7029863	491.51	AC	9	WAC0955	238458.8	7029838	491.58	AC	9
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WAC1185	236020.9	7029285	491.89	AC	9
WAC1186	236026.7	7029277	491.88	AC	9
WAC1187	236032.5	7029268	491.88	AC	9
WAC1188	236038.3	7029260	491.88	AC	9
WAC1189	236044	7029252	491.87	AC	9
WAC1190	236049.8	7029244	491.87	AC	9
WAC1191	236055.6	7029236	491.87	AC	9
WAC1192	236061.2	7029227	491.88	AC	9
WAC1193	236069.4	7029233	491.84	AC	9
WAC1194	236063.6	7029241	491.85	AC	9
WAC1195	236057.8	7029250	491.83	AC	9
WAC1196	236052.2	7029258	491.86	AC	12
WAC1197	236030.2	7029255	491.88	AC	9
WAC1198	236046.3	7029266	491.89	AC	9
WAC1199	236040.6	7029274	491.87	AC	9
WAC1200	236034.9	7029282	491.87	AC	9
WAC1201	236029.2	7029291	491.89	AC	9
WAC1202	236023.5	7029299	491.90	AC	9
WAC1203	236018.1	7029307	491.86	AC	9

WAC1204	236026.1	7029313	491.91	AC	9	WAC1260	238419.9	7029884	491.62	AC	9
WAC1205	236031.8	7029305	491.93	AC	9	WAC1261	238411.6	7029879	491.55	AC	9
WAC1206	236037.3	7029296	491.86	AC	9	WAC1262	238403.5	7029873	491.59	AC	12
WAC1207	236043.2	7029288	491.84	AC	9	WAC1263	238409.1	7029864	491.48	AC	9
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WAC1209	236054.6	7029272	491.90	AC	9	WAC1265	238425.3	7029876	491.49	AC	9
WAC1210	236060.3	7029264	491.89	AC	9	WAC1266	238433.8	7029882	491.62	AC	9
WAC1211	236066.2	7029255	491.80	AC	9	WAC1267	238442	7029888	491.72	AC	9
WAC1212	236072	7029247	491.88	AC	9	WAC1268	238450.2	7029893	491.72	AC	9
WAC1213	236077.7	7029239	491.86	AC	9	WAC1269	238458.6	7029899	491.62	AC	9
WAC1214	236085.8	7029245	491.77	AC	9	WAC1270	238466.9	7029905	491.67	AC	9
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WAC1216	236074.5	7029261	491.76	AC	9	WAC1272	238481.8	7029916	491.58	AC	9
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WAC1354	233785.3	7043805	492.36	AC	12
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WAC1356	233767.3	7043798	492.32	AC	12
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WAC1359	233739.6	7043786	492.36	AC	12
WAC1360	233730.3	7043782	492.32	AC	12
WAC1361	233721.2	7043778	492.37	AC	12
WAC1362	233736.9	7043752	492.40	AC	12
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WAC1371	233811	7043783	492.39	AC	12
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WAC1380	233729.3	7043760	492.43	AC	12
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WAC1402	233755.9	7043798	492.40	AC	12
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WAC1407	233789.1	7043823	492.38	AC	12
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WAC1415	233715.6	7043792	492.22	AC	12
WAC1416	233713.6	7043807	492.45	AC	12
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WAC1424	233774.7	7043844	492.42	AC	12
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WAC1427	233747	7043832	492.45	AC	12

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WAC1441	233786.4	7043817	492.41	AC	12	WAC1497	236075.9	7029232	491.86	AC	9
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WAC1471	236011.5	7029272	491.88	AC	9	WAC1527	236049.8	7029322	491.88	AC	9
WAC1472	236017.3	7029264	491.88	AC	9	WAC1528	236055	7029315	491.87	AC	9
WAC1473	236023	7029256	491.87	AC	9	WAC1529	236060.7	7029306	491.89	AC	9
WAC1474	236028.7	7029248	491.90	AC	9	WAC1530	236066.5	7029298	491.88	AC	9
WAC1475	236034.5	7029239	491.87	AC	9	WAC1531	236072.1	7029290	491.88	AC	10
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WAC1479	236060.1	7029221	491.90	AC	9	WAC1535	236094.8	7029257	491.88	AC	9
WAC1480	236054.3	7029229	491.90	AC	9	WAC1536	236100.4	7029249	491.88	AC	9
WAC1481	236048.6	7029237	491.90	AC	9	WAC1537	236103.8	7029263	491.87	AC	9
WAC1482	236042.9	7029245	491.89	AC	9	WAC1538	236098.1	7029271	491.90	AC	9
WAC1483	236037.2	7029253	491.87	AC	9	WAC1539	236092.3	7029280	491.88	AC	9
WAC1484	236031.5	7029262	491.88	AC	9	WAC1540	236086.4	7029288	491.93	AC	9

WAC1541	236080.6	7029296	491.87	AC	9
WAC1542	236074.8	7029304	491.91	AC	9
WAC1543	236069.2	7029312	491.88	AC	9
WAC1544	236063.4	7029320	491.90	AC	9
WAC1545	236057.7	7029329	491.91	AC	9
WS0079	233698.9	7043817	492.26	SON	10
WS0080	233725.9	7043818	492.23	SON	10
WS0081	233760.1	7043827	492.23	SON	10
WS0082	233783.6	7043848	492.19	SON	10
WS0083	233745.8	7043745	492.29	SON	10
WS0084	233782.1	7043749	492.25	SON	10
WS0085	233813	7043779	492.24	SON	10
WS0086	233768.4	7043782	492.24	SON	10
WS0087	233733	7043788	492.29	SON	10
WS0088	233789.4	7043796	492.29	SON	10
WS0089	238467.6	7029930	491.61	SON	10
WS0090	238432	7029911	491.69	SON	10
WS0091	238404.8	7029880	491.48	SON	10
WS0092	238424.9	7029851	491.51	SON	10
WS0093	238450.8	7029876	491.60	SON	10
WS0094	238465.6	7029898	491.63	SON	10
WS0095	238485.2	7029887	491.68	SON	10
WS0096	238469.2	7029858	491.57	SON	10
WS0097	238516.3	7029860	491.72	SON	10
WS0098	238442.5	7029809	491.48	SON	11
WS0099	235984.9	7029284	491.84	SON	10
WS0100	236020.6	7029242	491.87	SON	10
WS0101	236026.7	7029216	491.86	SON	10
WS0102	236068.1	7029226	491.81	SON	10
WS0103	236109.1	7029255	491.87	SON	10
WS0104	236082.5	7029267	491.90	SON	10
WS0105	236060.1	7029281	491.84	SON	10
WS0106	236026.4	7029295	491.87	SON	10
WS0107	236071.8	7029308	491.87	SON	10
WS0108	236051	7029251	491.88	SON	10
WS0109	236018.7	7029271	491.84	SON	10
WS0110	236001	7029252	491.89	SON	14
WS0129	236049.2	7029226	491.88	SON	10
WS0130	238446.8	7029921	491.57	SON	13
WS0148	238400.4	7029884	491.48	SON	10