TopTung Limited
ABN 12 118 788 846
Level 8, 46 Edward Street, Brisbane QLD 4000
PO Box 15505, City East, Brisbane QLD 4002
Australia
Tel: 0404 837 410 - Tel: 0419 702 616
info@toptung.com.au - www.toptung.com.au

ASX ANNOUNCEMENT
(ASX: TTW)

6 August 2018

ACQUISITION OF ADVANCED HIGH GRADE NICKEL-COPPER SULPHIDE PROJECTS IN CANADA

TopTung Limited ("TTW:" or "the Company") is pleased to announce the 100% acquisition of Australian Company Zeus Minerals Ltd, an **Advanced Nickel-Copper Sulphide** focused explorer with two principal project areas that encompass three highly prospective sub-projects located within the mining friendly jurisdiction of Quebec, Canada.

- The project areas contain a number of drill proven **Massive Ni-Cu Sulphide** occurrences with substantial Cobalt and Platinum Group Elements (PGE) credits.
- TopTung Limited has received firm commitments from GTT Ventures in an oversubscribed $500,000 placement at $0.035.
- TTW Board further strengthened by proposed appointment of Mr Marnus Bothma as Non-Executive Director, Mr Bothma is the Managing Director of Zeus Minerals Ltd and brings with him significant technical knowledge of the Project area.

Key Commercial Terms:

TopTung will acquire will acquire Zeus Minerals Ltd under a Share Sale and Purchase Agreement. The vendors of Zeus have given representations, warranties and indemnities in favour of TopTung which are considered customary for a transaction of this nature.

The purchase price is:

- A non-refundable cash deposit of $50,000, which will be paid out of existing cash reserves, which will enable the Company to conduct 30 days due diligence at its absolute discretion.
- $1,250,000 share consideration, payable by the issue of 35,714,286 fully paid ordinary shares at a deemed issue price of $0.035 each to the Zeus vendors (in their respective proportions), who are not related parties to the Company.

Completion of the acquisition is subject to the following conditions:

- Satisfaction or waiver of the conditions to an agreement under which Zeus Minerals is acquiring companies which hold the projects set out above, so that that acquisition completes at the same time as TTW acquires Zeus Minerals.
- ASX confirming that the acquisition does not trigger the requirements of Chapter 11 of the Listing Rules.
- TTW completing due diligence on the Company to its sole satisfaction within 30 days.

- TTW obtaining all required regulatory approvals to completion, including but not limited to obtaining all required approvals under the Listing Rules.

- There being no Material Adverse Change in the business, financial or trading position, or assets, liabilities or profitability or prospects of Zeus Minerals, or any event reasonably likely to result in such a material adverse change.

- There is no material breach, and there are no facts or circumstances that may reasonably be expected to lead to a material breach, of any warranties before Completion..

TopTung will seek shareholder approval to conduct the placement and to issue the consideration shares. The notice of meeting to approve this transaction will be dispatched in the coming weeks.

Project summary:

All projects are hosted in the **Belleterre-Angliers Greenstone Belt (BAGB)** in the Témiscamingue area, south-western Québec, Canada.

The project areas contain a number of drill proven **Ni-Cu (± Co ± PGEs) high grade massive sulphide mineralised zones** intersected by shallow drilling (Figure 1) as well as hosting the historic **Lorraine Cu-Ni Mine.**

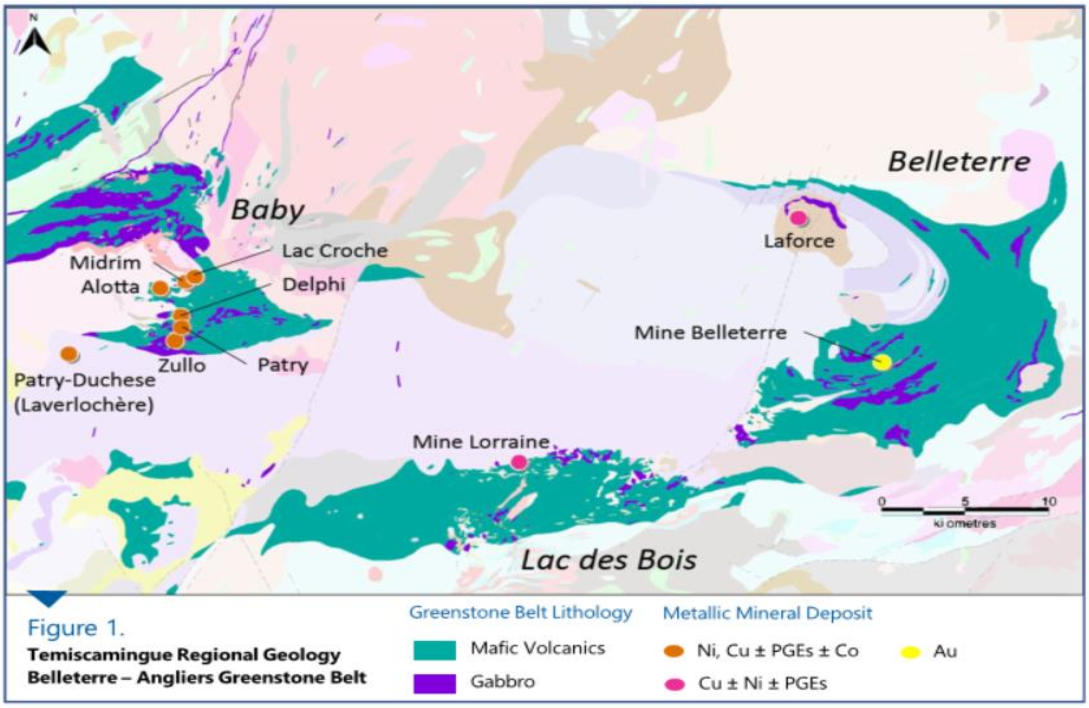


Figure 1: Geology of the Belleterre-Angliers Greenstone Belt showing the location of the Ni-Cu sulphide and gold occurrences. NOTE Laverlochère also features porphyry-related molybdenumand copper sulphide mineralisation.

The Belleterre-Angliers Greenstone Belt (BAGB) and the greater Abitibi Greenstone belt is considered highly fertile and hosts numerous significant deposits including:

- The Belleterre Gold Mine (Figure 1), which produced just under **1 Moz** of gold from 2.17 Mt of ore at an average grade of **10.73g/t gold** between 1936 and 1958.

- **The 2nd largest Nickel reserve in the world, 5th largest Nickel Sulphide discovery ever** and 8th largest Cobalt reserve in the world lies 150km northeast of the project area - Dumont Ni-Co project (RNC Minerals TSX:RNX).

- The Lorraine Ni-Cu Sulphide Mine, which historically produced 14.28 million pounds of Copper and 6.34 million pounds of Nickel lies within the project area

- Lorraine Mine production records for one Gabbro Sill (~600kt of ore) shows that over **AUD $100,000,000** of metal was extracted in less than 24 months**.**

- Gabbro sills of the BAGB host numerous Ni-Cu Sulphide occurrences . The Geoffrey Anomaly, which forms as a deep, flat lying electromagnetic conductor, measuring 4km x 1km is interpreted as the feeder to a swarm of such mineralised Gabbroic Sills.

Significant Shallow Intercepts Include:

- **Hole BT – 01 – 32**

  48.05m @ 3.05% NiEq with 0.09% Co from 54.25m

  - 13.1m @ 1.59% Ni, 1.03% Cu and 0.22% Co from 54.25m
  - 29.3m @ 1.87% Ni, 2.16% Cu and 0.10% Co from 73m

- **Hole BT-01-19**

  26.50m @ 3.05% NiEq with 1.37g/t Pd and 0.09% Co from 36.80m

  - 22.20m @ 1.88% Ni, 2.04% Cu, 1.47g/t Pd and 0.10% Co from 36.80m

- **Hole BT-01-36**

  1.95m @ 5.50% NiEq with 0.10% Co from 51.55m

  - 1.45m @ 6.2% Ni and 2.91% Cu and 0.10% Co from 51.55m

- **Hole BT-01-33**

  12.80m @ 3.54% NiEq with 1.72g/t Pd and 0.11% Co from 59.90m

  - 7.55m @ 2.76% Ni, 1.31% Cu and 1.82 g/t Pd and 0.13% Co from 64m

- **Hole BT-01-17**

  3.90m @ 3.04% NiEq with 1.27g/t Pd and 0.14% Co from 40.40m

- **Hole BT-01-18**

  3.35m @ 3.96% NiEq with 0.95gt Pd and 2.18g/t Pd from 25m

  - 1.0m @ 20.53% Cu, 1.55g/t Pt and 5.5g/t Pd from 25m

- **Hole BT-01-07**

  24.60m @ 2.44% NiEq with 1.61g/t Pd from 53.40m

  - 13.10m @ 1.89% Ni, 2.24% Cu and 1.61 g/t Pd from 53.40m
  - 4.80m @ 2.31% Ni, 1.57% Cu and 1.52 g/t Pd and 0.10% Co from 73.20m

- **Hole BT-01-35**

  12.70m @ 3.18% NiEq with 1.52g/t Pd and 0.11% Co from 73.65m

  - 10.60m @ 2.20% Ni, 1.73% Cu and 1.68 g/t Pd and 0.12% Co from 73.65m

- **Hole BT-01-05**

  25m @ 1.42% NiEq from 50m

  - 9.67m @ 1.61% Ni, 1.71% Cu and 1.21g/t Pd from 50.75

- **Hole BT-01-15**

  3m @ 3.97% Cu from 79m

  - 0.60m @ 18.65% Cu and 2.72g/t Pd from 79m

Placement:

In conjunction with the proposed acquisition, TopTung will undertake a placement to raise $500,000 through the issue of fully paid ordinary shares at an issue price of $0.035 per share (**Placement**). TopTung has been informed by its corporate advisor GTT Ventures that the placement has been oversubscribed and has received a firm commitment for the full placement amount.

Board Changes

Subject to shareholder approval and the completion of the Share Sale and Purchase Agreement, the company intends to appoint Mr Marnus Bothma as a non-executive director of the Company. The appointment will be made in accordance with the standard terms for such appointment and will be on the same terms as the other non-executive directors of the com pany.

Mr Bothma holds a masters degree in Geology from the University of Wollongong. Mr Bothma is experienced in early to mid stage exploration having conducted numerous technical programmes in Australia, Canada and Korea.

Mr Bothma has significant experience in multi-commodity project management and acquisition.

Mr Bothma has direct experience in magmatic Cu-Ni sulphide mineralisation within the Belleterre-Angliers Greenstone Belt, Canada, having conducted preliminary project acquisitions and project exploration management including overseeing geophysical surveys, field reconnaissance programmes and drilling programmes.

Further Advanced Acquisitions:

- The Company will continue to pursue other advanced acquisitions that have a strategic fit for the Company and provide updates on any further acquisitions as required by ASX listing rules.

- The Company has a clear focus bringing long term wealth to its shareholders through acquiring and exploring highly prospective advanced projects, that can subsequently lead to mining activities.

- The Company remains well positioned with ~$4mil in cash (post completion) to drill its highly prospective advanced projects and continue its search for other complimentary advanced projects.

The Company remains committed to advancing its Torrington Project and specifically the topaz related research in collaboration with the UNSW.

Project Potential

Nickel-Copper Sulphide Exploration Projects

The Company owns 100% exploration rights over three project areas covering 63.5km² within the Belleterre-Angliers Greenstone Belt, Quebec, Canada, as set out in Table 1 to this announcement. The project areas include:

- Baby Projects: Alotta/Delphi/Patry/Zullo

- Laverlochere Project

- Lac Des Bois Project: Lorraine

Drill Proven Ni-Cu Sulphide Mineralisation

The project areas contain a number of drilled **Massive Ni-Cu Sulphide mineralised zones** with significant shallow intercepts including as listed above

A Historical Producing Mine

The Lorraine Mine hosted within Zeus Minerals tenement package was a **Cu-Ni sulphide mine**. Production totaled **14.28 million pounds of Copper and 6.34 Million Pounds of Nickel** @ 1.57% Cu, 0.62% Ni, 6.86 g/t Ag and 0.67 g/t Au

Zeus recognises the potential for plunge extensions to the massive sulphide Cu-Ni-Co-Pd bodies at the former mine workings which ceased operations in 1968. There is also potential to locate additional mineralisation within the immediate mine area particularly beneath the previously mined ore body.

Drill Ready Targets

- 24 EM targets identified by Falconbridge in 2001 programme targeting multiple shallow 2-5 Mt deposits.
- Additional targets have been identified from a 2018 aerial magnetic survey.
- The existing deposits are interpreted to be structurally controlled with approximately **6.5km of mineralisation controlling structures**, being interpreted from the magnetic data.
- The Company will expedite drilling to estimate a mineral resource in accordance with the JORC (2012 Edition) Guidelines.
- Zues Minerals has prepared drilling applications for a diamond core programme at the Alotta and Patry Projects.
- The planned drill targets are accessible with bitumen roads and established service tracks leading to the targets areas.
- The Company has acquired an extensive technical database with over 5,000m of diamond drill core available, 4-channel MEGATEM survey data, high definition aerial magnetic and geochemical surveys.
- The extensive areas of mafic lavas and sills together with the large volumes of gabbroic intrusions - which host the sulphide mineralisation in the BAGB indicates **potential to develop further drill targets**.

Well Located to Infrastructure

- Exceptional rail and road infrastructure located nearby with a major freeway abutting the projects.
- A number of Ni, Cu, PGE and Co **processing facilities with toll milling capacity** occur within trucking distance.
- Located 520km north of Toronto and in close proximity to a township, electricity and water.

Further Technical Information

*The nickel equivalent (NiEq) values have been determined as outlined in Appendix 1.

Summary drill hole intersections highlighted in this announcement are given in full in Appendix 2.

The Competent Persons declaration is given in Appendix 3.

JORC Code 2012 Table 1, Sections 1 and 2 for the Baby and Lac Des Bois Projects are given in Appendices 4 and 5.

Collar and survey data for the drill holes are given in Appendix 6.

Mineralisation:

Magmatic Nickel-Copper Sulphide

The Belleterre-Angliers Greenstone Belt (BAGB) hosts numerous Ni-Cu-PGE sulphide occurrences associated with gabbroic bodies, including the past-producing Lorraine Mine (600,000 tonnes @ 0.62% Ni and 1.08% Cu: Huffman et al., 1993), which is captured by the Company's Lac des Bois Project. Other important known mineralised occurrences captured by the Company in its Baby Project, include Alotta, and Delphi-Patry-Zullo. The properties lie along the north-eastern extension of a well-defined Nickel-Copper-PGM-rich metallotec that also hosts orebodies at Temagami Copper, Kaniche, and the Sudbury Igneous Complex.

The nickel-copper deposits are of two distinct types: those associated with gabbroic sills and those associated with generally small plugs and stocks that range compositionally from dunite to gabbro (Card and Poulsen, 1998). Both are described as synvolcanic (Barnes et al., 1993). **The advanced Ni-Cu assets of Zeus Minerals are all the first type: namely magmatic Ni-Cu sulphide associated with gabbroic sills.**

A characteristic of the Ni-Cu mineralised bodies in the BAGB is the relatively small volume of gabbro in comparison to the volume of sulphides. Huffman et al. (1993) suggest the mineralised gabbro bodies acted as feeder conduits to overlying basalt flows as suggested by their identical major and trace element geochemistry, and similar degrees of alteration and metamorphism. Huffman et al. (1993) suggests this would have allowed for the movement of large amounts of magma through these conduits before being erupted, resulting in a large magma: sulphide ratio, or high R-factor, which explains both the excellent Ni-Cu-PGE tenors of the sulphides and the large volumes of sulphide relative to the observed volumes of gabbro.

When considered in conjunction with the large volume of mafic lavas and sills in the BAGB, the the potential for discoveries is excellent.

Baby Projects

The Baby Project, which includes the Alotta, Delphi-Patry-Zullo, and Laverlochère Projects, covers prospective gabbroic sills preserved at or near the southern and western margin of the Baby Segment.

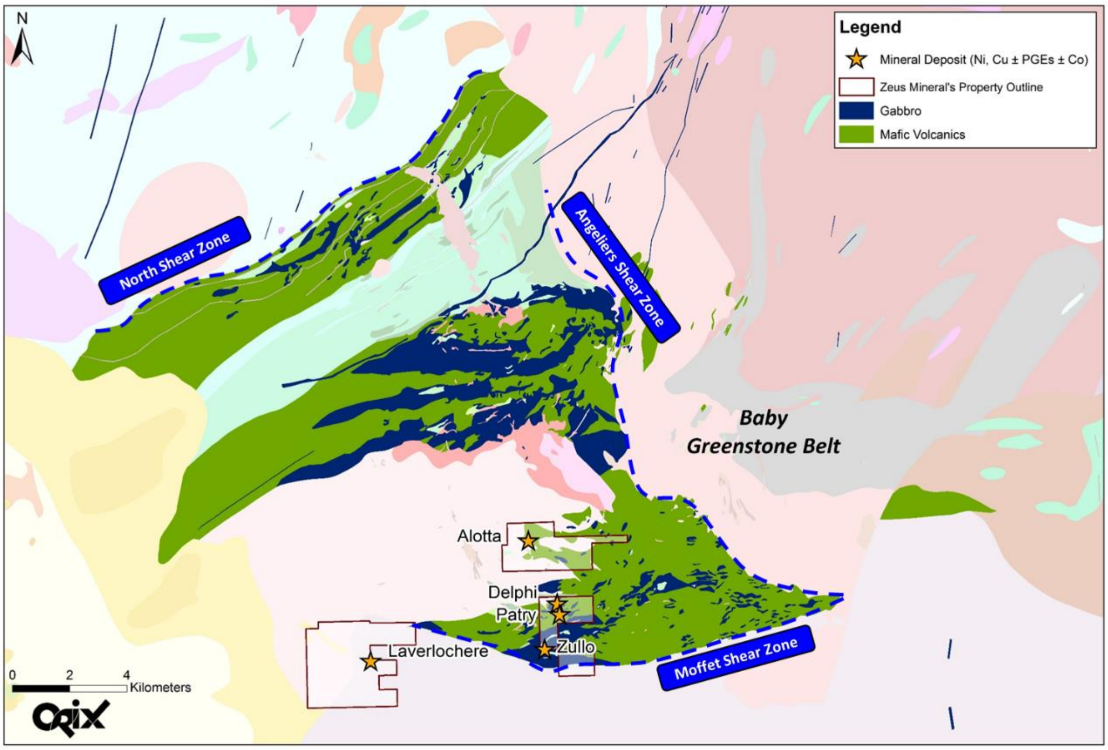


Figure 2: Baby Project: Geology with Project locations with Ni-Cu (Alotta, Delphi, Patry and Zullo) and Cu-Mo (Laverlochère) mineralisationsearch

Significant amounts of historical exploration on the Projects has been completed by listed explorers including Aurora Platinum Corp (TSX: ARP-V), FNX Mining (TSX: FNX-T) and Fieldex Exploration (TSX: FLX-V). The works include: extensive diamond drilling (over 5,000m of core available); airborne electromagnetic ("EM") and magnetic surveys, geochemical soil and rock chip sampling; and ground IP surveys and EM surveys.

Alotta

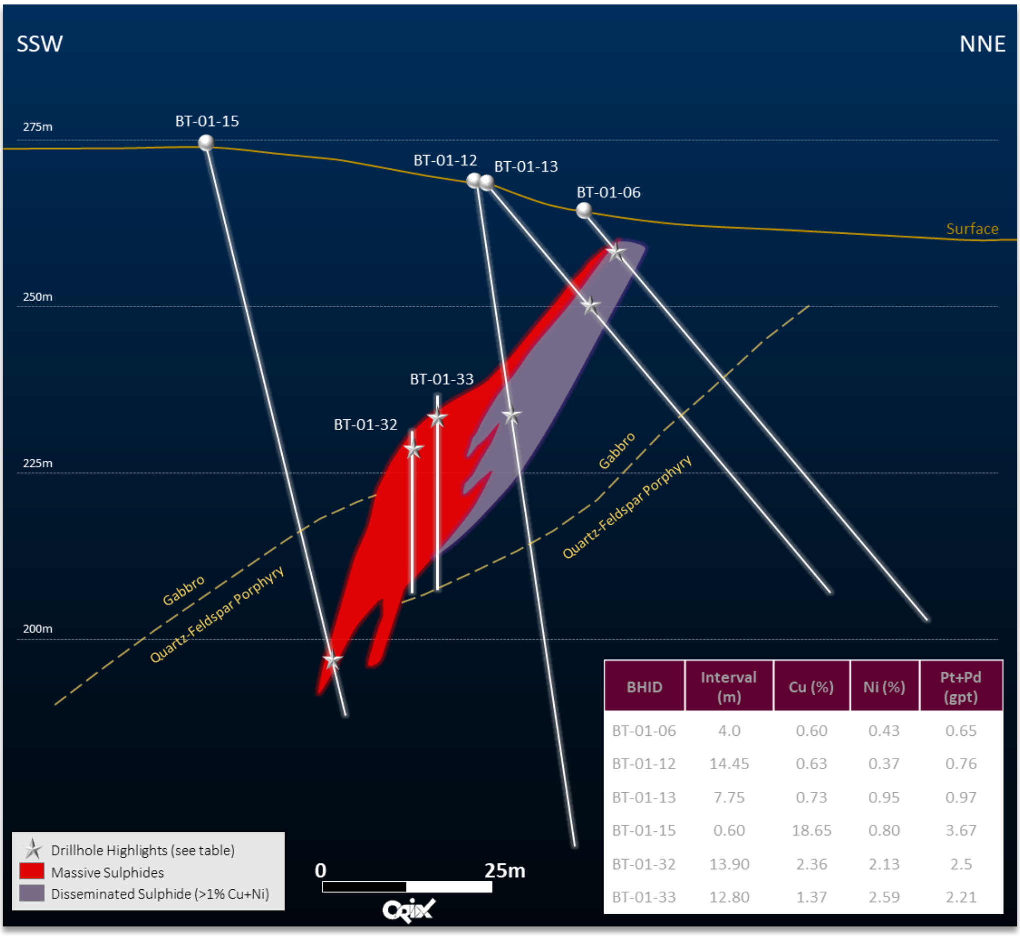
Project Review

The Alotta project comprises 12 claims for 461.07ha in a single contiguous claim block (Figure 4). The property contains the significant drill indicated Cu-Ni sulphide mineralisation of Alotta.

The property is accessible from the town of Ville-Marie northeast along Highway 391and then east along Highway 382 for 10km. Forest service tracks link the project to the highway.

Geology and Mineralisation

The Alotta Gabbro is the best preserved and exposed of the gabbro bodies within the Baby Group. The unit is differentiated into crude, texturally distinct magmatic layers with significant blebby to massive sulphide mineralisation hosted by a medium-grained, sub-ophitic textured gabbro. The Ni-Cu-PGE mineralisation is located on the central southern shore of Petit Lac Long. The south shore of the lake is approximately coincident with the lower contact of the differentiated gabbro body which trends northwest and whose north contact dips at approximately 45° to the south-west. The gabbro appears to form a sill-like body, about 250 m thick, pinching out to the southeast and with a plunge in the order of 15° at 290° (Figure 3).



BHID	Interval (m)	Cu (%)	Ni (%)	Pt+Pd (gpt)
BT-01-06	4.0	0.60	0.43	0.65
BT-01-12	14.45	0.63	0.37	0.76
BT-01-13	7.75	0.73	0.95	0.97
BT-01-15	0.60	18.65	0.80	3.67
BT-01-32	13.90	2.36	2.13	2.5
BT-01-33	12.80	1.37	2.59	2.21

Figure 3: Ni and Cu sulphide mineralised lens at Alotta, cross section 12+12.5w Looking 290˚ (10m clipping)

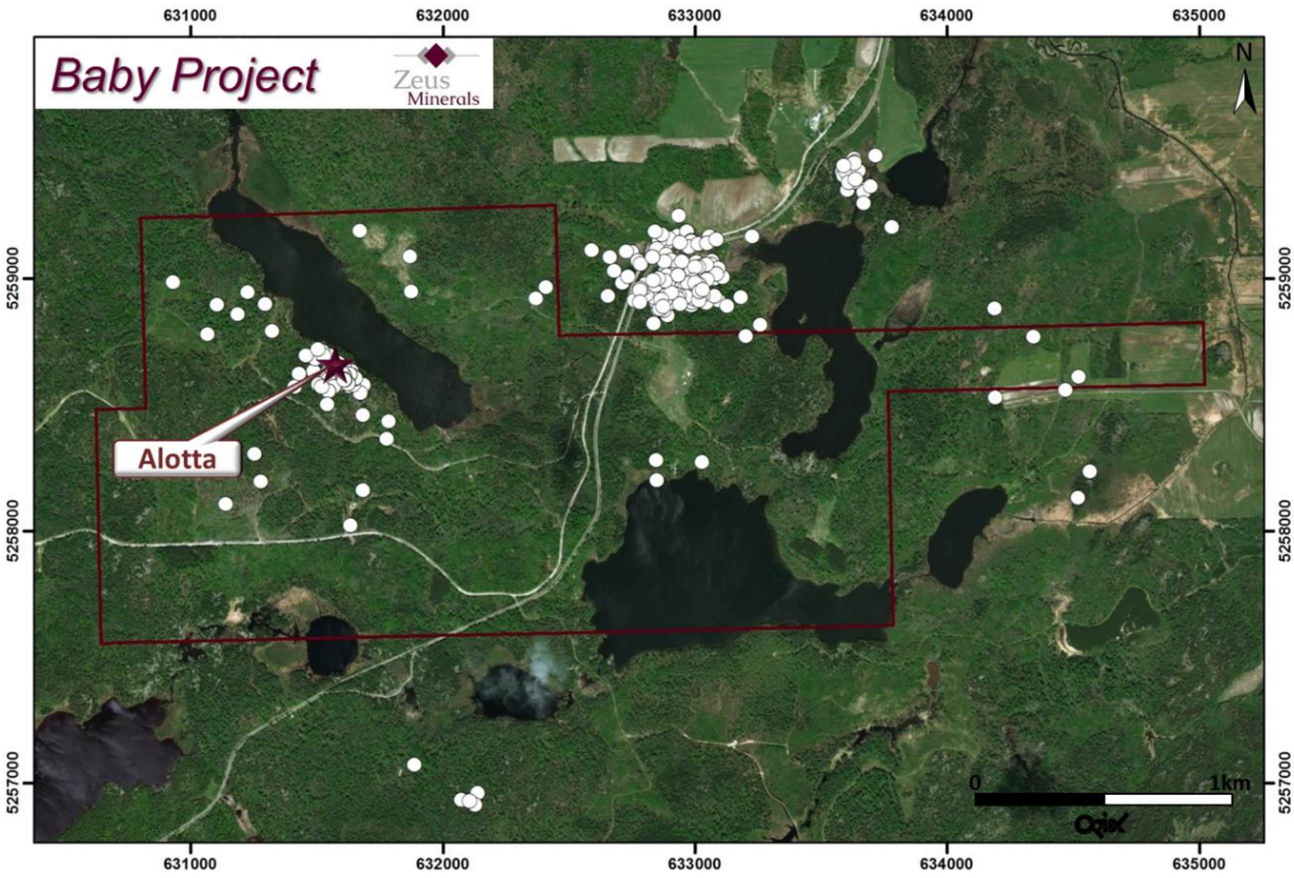


Figure 4: Alotta mineralisation - Drill hole locations.

Previous Exploration

Work in 1988 by the Ministry of Energy and natural resources of Québec (or MERN) precursor, the MRNQ, identified massive Ni-Cu sulphide mineralisation immediately south of Petit Lac Long (Winter, 2003). The Alotta showing, which included the area just described, was first drilled in the late 1980's with intersections of up to **35 metres averaging 1.76% copper and 1.55% nickel**. Up to 4.24 grams per tonne platinum over 0.9 metres has also been reported at Alotta. (Aurora, 2001).

Between 2000 and 2003, Aurora Platinum Corp ("Aurora") released encouraging results from the exploration of its Belleterre project, which confirmed the presence of mineralisation and established the presence of a **body of Ni-Cu sulphide mineralisation at Alotta**. The Company's Belleterre project included the Alotta, Delphi, Patry, and Zullo Projects.

During the period, the company completed mapping and geochemistry surveys as well as airborne and ground geophysical surveys, excavation of several trenches, over 120 diamond drill holes, and petrology studies.

Aurora's first drill holes completed at Alotta in the fall of 2000 yielded significant grades of nickel and copper at shallow depths (25 – 75m) in 15 of the 35 holes drilled (for a total of 4,040 metres).

Highlights include:

- **21 metres grading 2.0% Ni, 2.14% Cu, 0.11% Co, 0.5g/t Pt and 1.5g/t Pd.**
- **13.9 metres grading 2.13% Ni, 2.36% Cu, 0.10% Co, 0.7g/t Pt and 1.8g/t Pd.**
- **1.0 metre grading 20.53% Cu, 1.55g/t Pt and 5.5g/t Pd.**

In November 2000, a helicopter-borne electromagnetic (EM) and magnetic survey was carried out by AeroQuest Limited over the Midrim Property, using an AeroTEM six channel time domain EM system and a high sensitivity caesium vapour magnetometer. A total of 1191.1 line-kilometres were flown at 50, 100 and 200-metre line spacings (Figure 5). The survey shows that the magnetite-rich gabbroic host rocks to the Alotta mineralisation and other known projects in the Belleterre Property are more extensive than depicted on published government maps. Known mineralisation was identified by the airborne survey, with several new and significant buried conductors delineated in the airborne survey representing good drill targets.

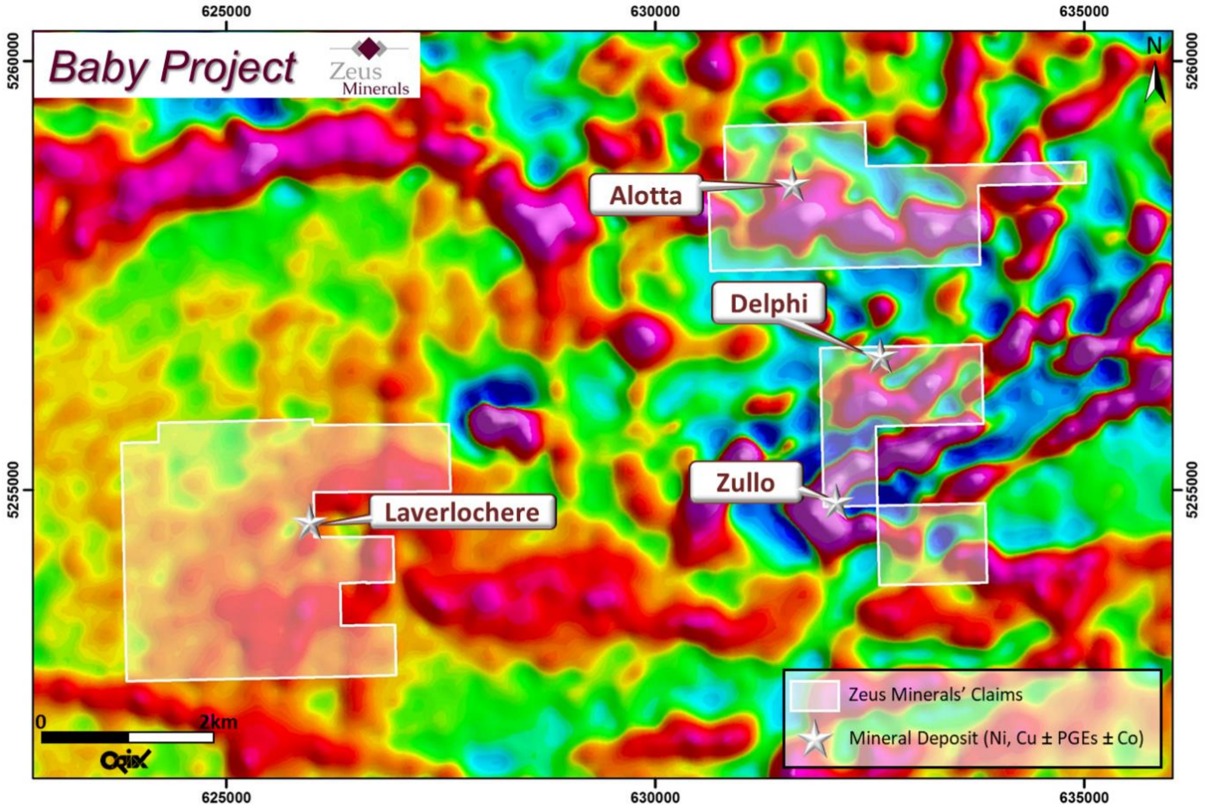


Figure 5: Baby – Airborne Magnetic Survey 1VD

At Alotta, Time-Domain Spectral Induced Polarization and magnetometer surveys were completed over 24 lines at 50 and 100-metre line spacings with 25-metre stations for the IP survey and 12.5-metre stations for the magnetic survey. Total survey coverage was 26.974 kilometres (IP) and 29.175 kilometres (magnetics). **The survey showed that the main Alotta zone is associated with strong chargeabilities with low resistivities and moderate magnetics. Nine high priority chargeability and/or magnetic targets were defined.**

At Alotta North, 14 lines using the same parameters were surveyed for total coverage of 12.75 kilometres (IP) and 12.425 kilometres (magnetics). **Five high priority chargeability and/or magnetic targets were defined.**

Delphi-Patry-Zullo Projects

Project Review

The Delphi-Patry-Zullo project unites three of the Belleterre showings into a single project because of their proximity to each other. The Project comprises six claims for 384.54ha in two claim blocks each containing three claims. Delphi and Patry lie in one claim block; Zullo lies in the other (Figures 5 and 6). Each of the two claim blocks contains significant drill indicated Cu-Ni sulphide mineralisation. The Patry project is located about 3 km south of the Alotta deposit.

The property is accessible from the town of Ville-Marie northeast along Highway 391 and then east along Highway 382 for 10km. Forest service tracks link the project to the highway.

Geology and Mineralisation

Three main rock units exist within the Delphi-Patry-Zullo area: a basal sequence of massive to pillowed basalt at least 900 m thick, which is overlain by quartz-feldspar porphyry-derived sediments/volcaniclastics that range from thinly bedded tuffs to coarse agglomeratic/conglomeratic types. These units form north-dipping east-northeast trending homoclinal sequence located on the south limb of a synform (Winter, 2003).

Five gabbro sill-like bodies have been identified within the area with three of them occurring within the basal basalt. The fourth gabbro body was intruded at the contact between the mafic volcanics and the overlying quartz-feldspar porphyry derived sediments/volcaniclastics with the fifth gabbro forming the core of the west plunging synform in the northern part of the area.

Ni-Cu-PGM sulphide mineralisation has been identified both in outcrop and in drill core at both the Delphi and Patry Projects. Both projects are associated with interpreted west-northwest trending axial planar structures produced by the D1 deformation and are accompanied by intense chlorite and carbonate alteration.

Like at Alotta, the mineralisation in the Delphi-Patry-Zullo area consists of pyrrhotite, chalcopyrite, pyrite, and pentlandite. The mineralisation varies from massive to semi-massive to blebby, to disseminated to foliation-controlled stringers (Winter, 2003).

At Delphi, Ni-Cu-PGM mineralisation is located within an axial planar shear and has probably been remobilised. Borehole geophysics suggests an offhole conductor just above drill hole 42 at the base of the gabbro sill. This target remains to be evaluated. In the Patry showing, massive sulphide as well as stringer and disseminated to blebby Ni-Cu-PGM mineralisation is associated with an axial plane parallel shear and the keel of a small syncline occupied by a small west-plunging gabbro sill trending approximately 280°.

On the Delphi-Patry grid, a 650 m wide west-northwest trending structural corridor has been identified. The corridor is centred on the Patry project and includes the Delphi project and its associated structures to the north and parallel structures to the south. It defined on magnetic imagery by a pronounced magnetic low which crosscuts all the major magnetic units.

The lithologies present at Zullo are very similar to those at the Delphi-Patry area with the oldest units being massive to pillowed basalts with interflow cherts and siltstones. Facing directions determined from pillow lavas support the structure as being a synclinal antiform with a northwest-trending axial plane and plunge. These have been intruded by a sill or sills of differentiated gabbro that ranges in composition from gabbro to leucogabbro. The gabbro sill or sills have a total thickness of about 700 metres. All units are cut by late quartz-feldspar porphyry dykes which trend west-northwesterly and appear to have been introduced along axial plane parallel shears.

The mineralisation at Zullo occurs as chalcopyrite associated with a quartz vein in volcanics and is probably associated with an axial plane parallel shear.

Previous Exploration

Two holes were drilled at Patry to test mineralisation beneath the small gossan outcrops. The Patry drilling was designed to test the down-dip extension of disseminated to blebby sulphides (pyrite-pyrrhotite-chalcopyrite-pentlandite) in a strongly chloritized and carbonatised gabbro and an associated shear zone. Hole BT-01-36 intersected 1.45 metres of massive pyrrhotite, pentlandite and chalcopyrite from 51.55 to 53.00 metres within the shear zone. **The zone of massive sulphide assayed at 6.2% Ni, 2.91% Cu, 0.10% Co, 0.28 g/t Pt and 0.45 g/t Pd. A second hole BT-01-40, drilled parallel to BT-01-36 and 30 metres to the west, intersected 19 metres of mineralisation averaging 1.38% combined Ni-Cu from 79.30 to 98.45 metres. The mineralisation in these two holes is a continuous zone plunging about 40º at 290º.**

Time-Domain Spectral Induced Polarization and magnetometer surveys were completed across most areas. At Delphi, 11 lines were surveyed with a total coverage of 16.425 kilometres (IP) and 18.475 kilometres (magnetics). **Seven high priority chargeability and/or magnetic targets were defined; two of these corresponded well with the Alotta model.** Also, at Delphi, borehole IP indicated an off-hole conductive zone at the bottom of BT-01-42, below the Delphi surface showing. At Patry, borehole geophysics indicated that the mineralisation in drill holes BT-01-36 and BT-01-40 was connected and that the mineralisation was trending about 290º and plunging in the same direction. **The 2001 MEGATEM® II EM and magnetic survey identified a total of 17 priority I and II conductors associated with northwest-southeast structures.**

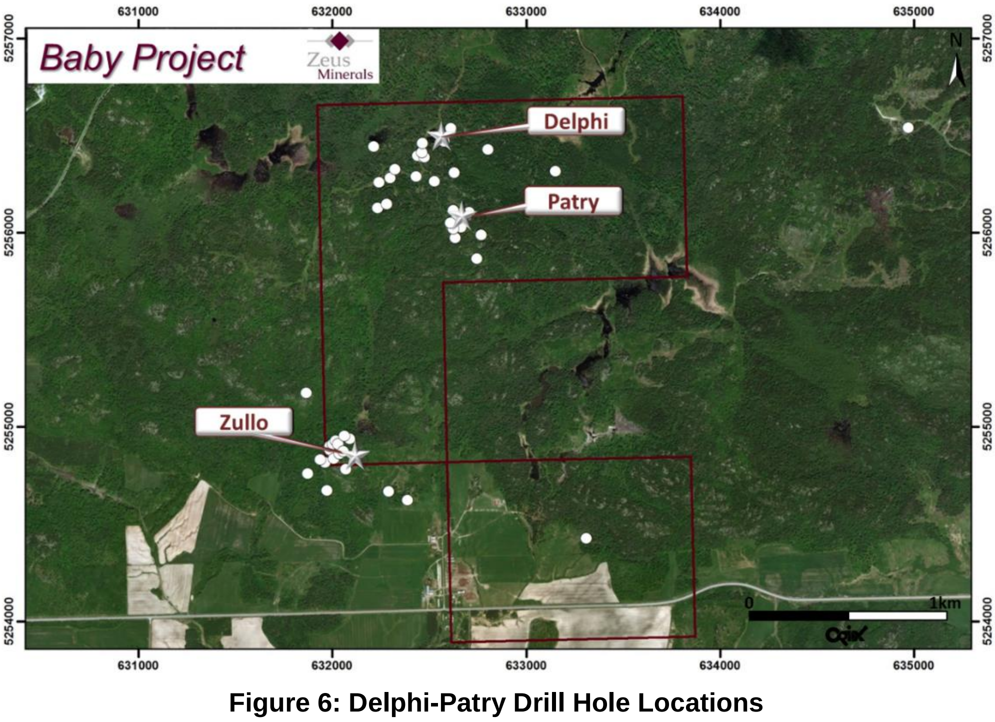


Figure 6: Delphi-Patry Drill Hole Locations

Laverlochère Project

Project Review

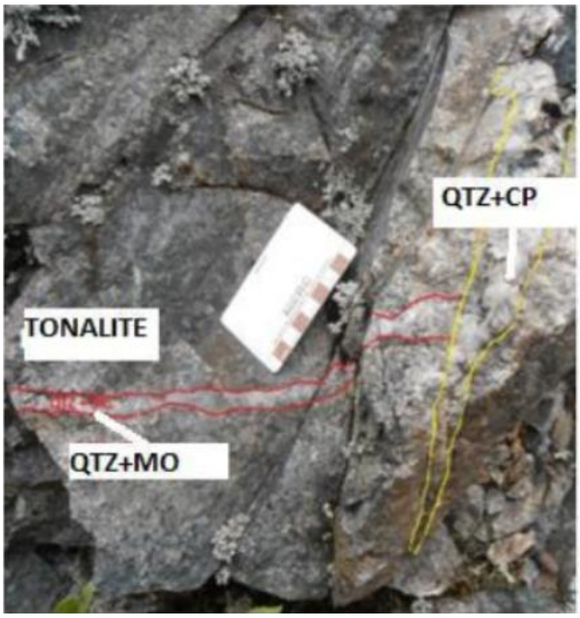
The Laverlochère property is located approximately 100 km south of Rouyn-Noranda near the village of St Isidore of Laverlochère. Laverlochère township, which lies on the project eastern boundary, is located 15 km northeast of Ville-Marie (Figure 2).

This property has 19 claims and covers an area of approximately 902 hectares. The property is accessible by the main road 391 Lorrainville.

Geology and Mineralisation

Four major rock packages are recognised at Laverlochère, which from oldest to youngest, are volcaniclastic sediments, porphyry andesite, breccias, and conglomerates. Gabbro sills and younger tonalite rocks intrude and cut the stratigraphy. The quartz-feldspar porphyry-derived sediments/volcaniclastics include tuffs interbedded with sandstones and polymictic conglomerates and are like those described on the Alotta and the Delphi-Patry-Zullo Projects. Conformable porphyritic andesite lies over the volcaniclastics.

Sediments of the Baby Group overlie andesite, and are, in turn, overlain unconformably by conglomerates of the Huronian Cobalt group. The conglomerates are polymictic, rounded, very poorly sorted with clasts that can reach up to 2 meters in diameter. The clasts include granite, and porphyritic lavas thought to correspond to tillites of the basal Gowganda Formation of the Cobalt group of the Huronian Supergroup (Debicki, 1990). The Huronian is a major glacial period (Eyles and Young, 1994).



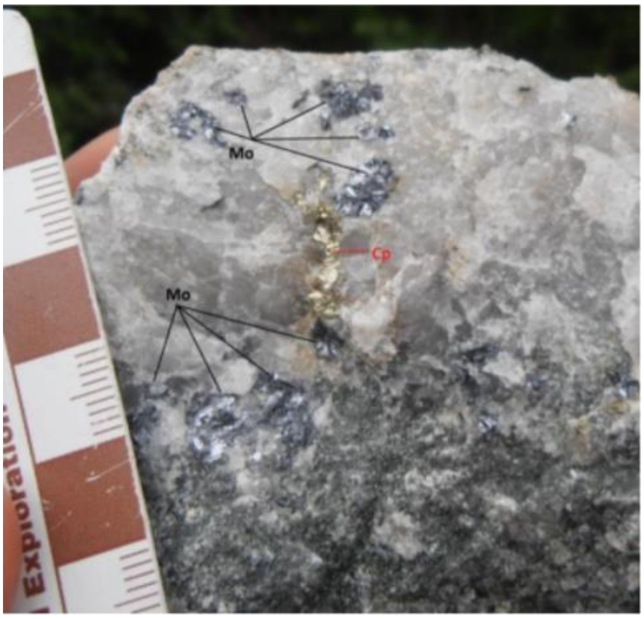


Figure 7: Quartz-molybdenite ± chalcopyrite vein (underlined in red) intersected by a vein of quartz-chalcopyrite (underlined in yellow). Dissemination of molybdenite and chalcopyrite in the vein of quartz. Molybdenite is also present in the vein selvages.

Lac Des Bois Project

Project Review

The Lac des Bois property comprises 90 claims in a single contiguous claim block for an area (Figure 8). The property contains the old Cu-Ni sulphide deposit of the Lorraine Mine and several other mineralised Ni-Cu, PGE or gold occurrences. It surrounds Globex's Lac Kelly deposit, which is excised from within the claim block and which contains a resource of 1.4Mt at a combined grade of 1.4% Cu/Ni (Globex Mining, 2017).

The property is accessible from the town of Ville-Marie via the regional secondary 382 road to Latulipe. From Latulipe, the Lac des Bois concession gravel road leads north to the western part of the property. Access within the property is through 4WD trails.

Mineralisation

Four types of mineral deposits or occurrences have been identified on the Lorraine project (Figure 8; Moreau, 2017):

- Magmatic Ni-Cu-Co-Au-PGE deposit like the former Lorraine Mine, the Blondeau showing and the encapsulated Lac Kelly deposit.
- Vein-type intrusion-related gold deposits in vein quartz hosted by gabbro at Lorraine and Blondeau.
- Orogenic, structurally controlled, gold deposits like the Lac au Renard Ouest Cu-Au showing.
- Zn-Cu volcanogenic semi-massive to massive sulphides (Cu, Zn, Ag, Co) deposit like the Roy showing found on the property.

Both the Roy and Lac au Renard Ouest showings remain underexplored.

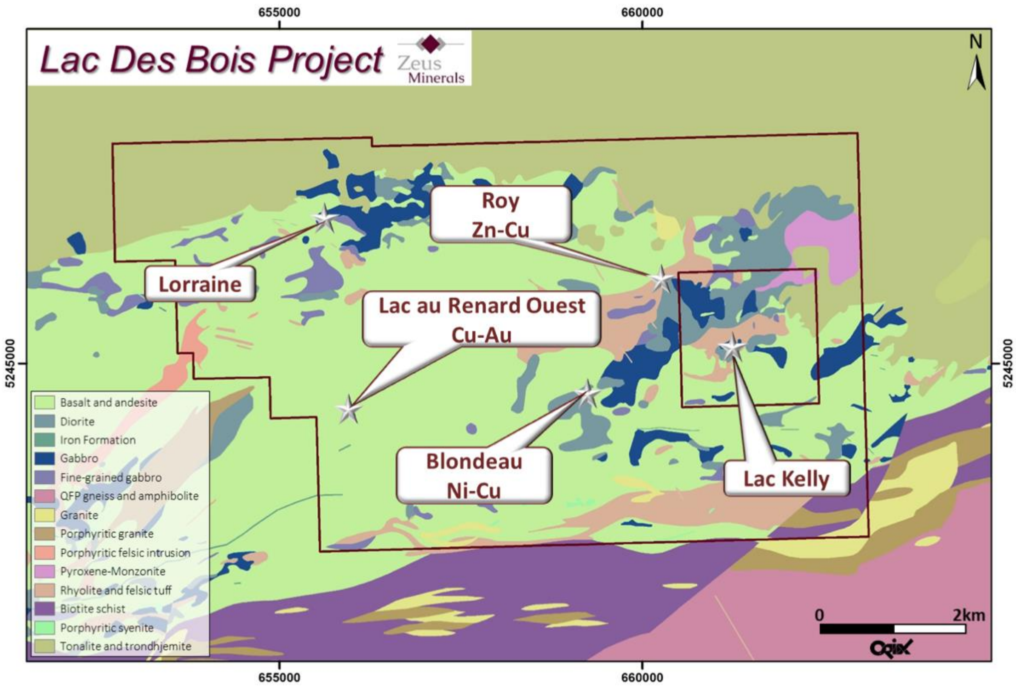


Figure 8: Advanced Projects - Lac desBois

Lorraine Ni-Cu Deposit

Mineralisation

The Cu-Ni sulphide deposit of the Lorraine Mine is associated with the contact between a syn-volcanic gabbro and tholeiitic mafic lavas in the Lac des Bois section of the BAGB (Hinzer and Dunbar, 1988).

Production at the Lorraine Mine came from a single elongate sulphide lens found along the sheared gabbro-volcanic contact (Hinterland, 2004). The lens exhibits a mineralogical zonation characterised by a central massive sulphide zone rich in pyrrhotite and pentlandite surrounded by a chalcopyrite-rich disseminated sulphide zone. Magmatic segregation followed by hydrothermal remobilisation has resulted in the development of a Ni-Co dominated core enriched with Pd surrounded by a Cu dominated envelope enriched with Au-Ag-Pt. Thus, the disseminated sulphides are rich in Cu, Au, Ag, Pt and Zn in contrast the massive sulphides are rich in Ni, Co and Pd (Moreau, 2017).

The chalcopyrite is observed to fill fractures in the pyrrhotite, magnetite and the silicate minerals, and petrographic studies show evidence of deformation, including deformation twins, wavy extinction, granoblastic textures, and foliation of the sulphides.

The overall model formation of the Lorraine Mine sulphide involves three steps a) formation of a Ni-Cu sulphide body depleted in Os-Ir-Ru-Rh; b) deformation of the sulphide lens resulting in the migration of chalcopyrite to the margins of the body to form the disseminated sulphides and leaving a core of massive sulphide rich in pyrrhotite and pentlandite; c) local redistribution of Pd and Pt by a low temperature fluid. There are two ways in which the first step- formation of a Ni-Cu sulphide body depleted in Os-Ir-Ru-Rh- could have occurred either the Lorraine Mine sulphides represent a fractionated Cu-rich igneous sulphide liquid, or they represent hydrothermal sulphides. In both cases, the possibility exists that there are Os-Ir-Ru-Rh rich sulphides as yet undiscovered in the area (Barnes et al., 1993).

Gold is the most important target at Lorraine (Hinterland, 2004). Two types of mineralisation are sought:

1. Vein-type intrusion-related gold deposits in vein quartz hosted by gabbro
2. Orogenic, structurally controlled, gold deposits

Numerous gold values up to a maximum of 13.8 g/t were obtained from samples of disseminated chalcopyrite mineralisation in altered gabbro at Lorraine. Grab samples taken on the property have reported up to 28 g/t Au Hinterland Metals (2004) state that the old mine records reference structural, vein-type gold mineralisation on the sixth level that was never followed up:

Elsewhere in the BAGB, structurally-controlled gold mineralisation is generally associated with deformed massive to stringer sulphide horizons. Free gold is commonly hosted in quartz-carbonate veins.

Previous Exploration

Exploration activity in this area dates to the 1930’s (Retty, 1931). Since that time three spikes of exploration activity have resulted in a relatively active, but discontinuous, exploration history in this region The first major spike took place in the early to mid-50’s. During the period 1953-57, the Lac Kelly Cu-Ni deposit (5.5 km east-southeast of the Lorraine Mine) was recognised and drilled to the 1,100 feet depth (335m) in two intensive drilling campaigns. Also, at that time, the Blondeau Ni-Cu zone (4.0 km southeast of the Lorraine Mine) was discovered and drilled, and the Roy zone (4.5 km east of Lorraine Mine) was drilled.

The second spike occurred from the mid-1960's to the early 1970's during a period of high base metals prices. The Lorraine mine was discovered, developed, and mined during this period. The Mine Lorraine discovery resulted in renewed exploration activity across the region.

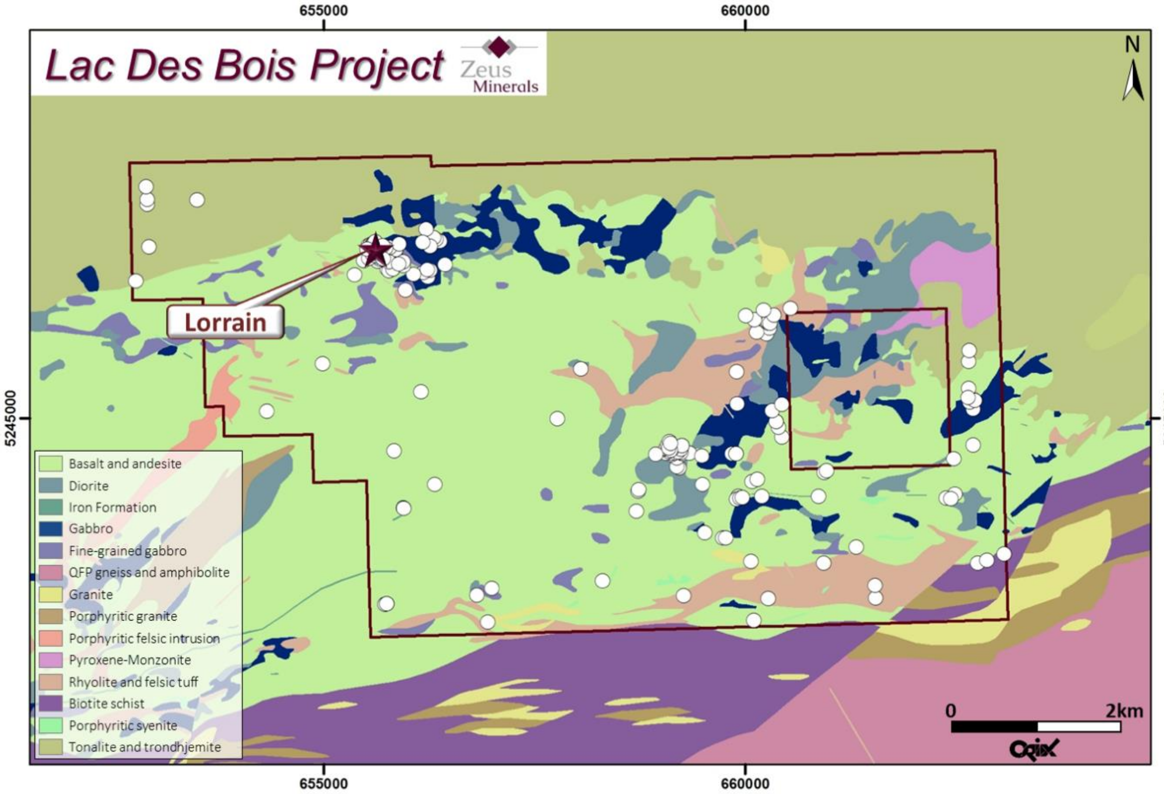


Figure 9: Lac des Bois Drill Hole Locations

Surface sampling has substantiated Cu-Ni mineralisation throughout the property. In almost all cases the anomalous geochemistry is directly associated with sulphide mineralisation hosted within gabbroic rocks and associated with mafic volcanics. Peak values of 2% Cu and 0.2% Ni was returned from a strongly silicified gabbro containing up to 10% pyrite and pyrrhotite.

The base metal mineralisation at Lorraine is associated with a strong IP anomaly which follows the mafic volcanic-gabbro contact. Major magnetic highs which are conformable with the stratigraphy coincide with known surface sulphide mineralisation. Magnetic disturbances north of Lorraine may be attributed to the target magnetite-bearing gabbro.

In late 2015, Eagle Geophysics Ltd. was commissioned by Greg Ltd. to fly a helicopter-borne gradient magnetic survey over the Loraine property. The survey covered a total of 527.1 line-kilometres (Figure 10). A Very Low Frequency (VLF) electromagnetic receiver was also installed for the benefit of the survey.

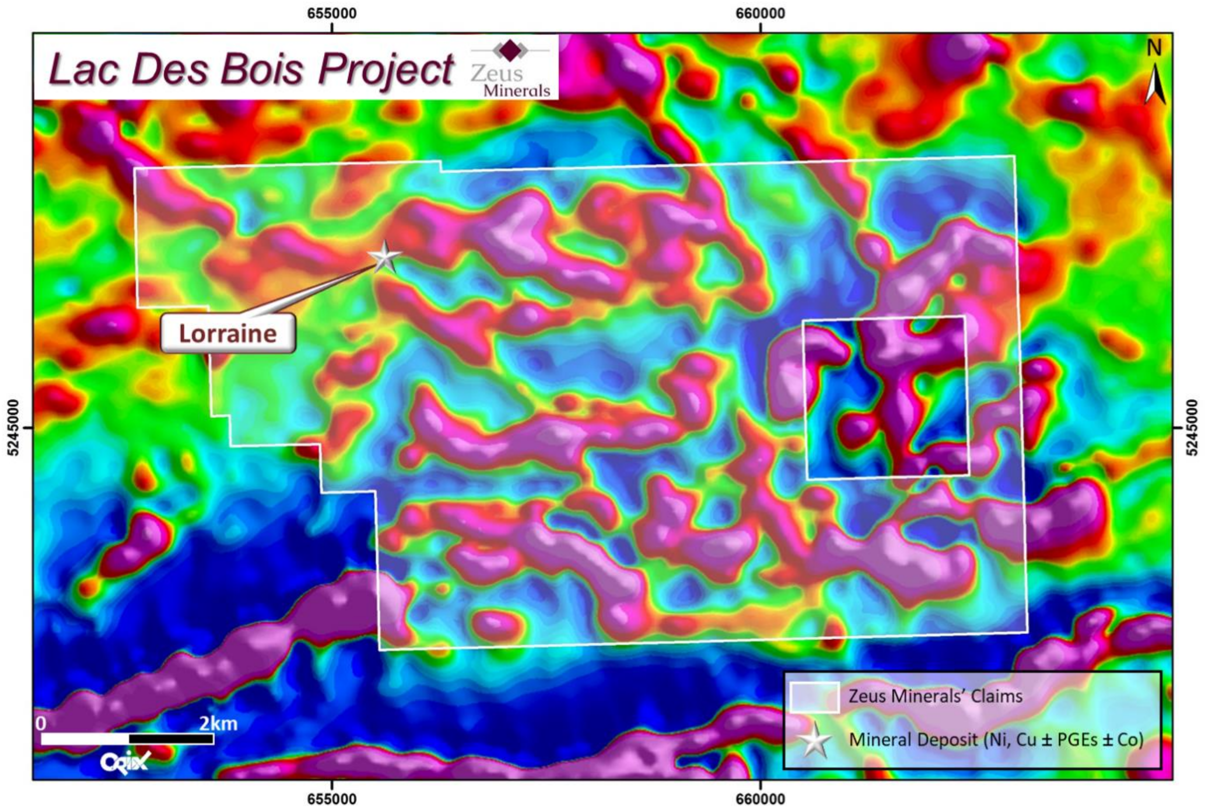


Figure 10: Lac Des Bois – Airborne Magnetic Survey 1VD

The high-resolution survey results along with reconnaissance and detailed field work including geological mapping and sampling close to the former Mine Lorraine workings were included in a comprehensive structural study of the property.

The study produced the following results:

- Structural studies suggest a major NW-trending structural corridor encompassing all major showings and the former Mine Lorraine.
- Geophysics is congruent with the structural studies.
- The interpretation of structural and geophysics maps suggests additional exploration targets to be tested.

TTW recognises the potential for plunge extensions to the massive sulphide Ni-Co-Pd bodies at the former mine workings. They have also recognised the potential for disseminated Cu-Au-Ag-Pt mineralisation in the wall rock surrounding the former mine workings. The author agrees with the remnant potential in the property including structural repeats within the same gabbroic sill and extensions to known mineralisation.

The available geological reports, including project specific technical reports and research papers, reviewed TTW, support the potential claims for significant mineralisation, particularly beneath the existing workings.

Zeus Portfolio Asset Conclusion

The mineral asset portfolio held by Zeus presents several assets with varying degrees of advancement and previous exploration activities.

The important volume of mafic lavas and sills in the Belleterre-Angliers Greenstone Belt suggests that the potential for discoveries is excellent. The Company proposes to narrow the target areas with follow-up detailed mapping and with soil geochemistry and/or geophysics, where appropriate. The Company believes that these primary objectives are reasonable and achievable.

The planned exploration is appropriate as the drill-ready targets are mostly already identified. **Work currently underway is focussed on delineating extensions to known ore zones, which potentially may eventually lead to a mining operation.**

The Company, together with its technical consultants, will compile the legacy data and review it for each asset, including the development of a structural framework and targeting protocol for each deposit-type. Completion of this task will rank and prioritise targets for the Company so developing a systematic, cost efficient and effective exploration process at every stage. This process create additional targets and allow the Company to prioritise them prior to the commitment to further capital.

As presented, the exploration philosophy and programmemes proposed by Zeus are technically sound and based on the information provided to date, the project development milestones are achievable.

TTW believes that, soundly based geochemical, geological and structural targeting, use of geophysics where appropriate, and with a commitment to drilling under cover and at depth has the potential to delineate further mineral resources.

I, Jonathan King, BSc (Hons.), MAIG, confirm that I am the Competent Person for the Report and;

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).

- I am a Competent Person as defined by the JORC Code 2012 Edition, having five years experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.

- I am a member in good standing of the Australian Institute of Geoscientists (AIG).

- I have reviewed the Report to which this Consent Statement applies.

I am a consultant working for:

Dreamlife Holdings Pty Ltd

Table 1 - Claim Schedule

Property	NTS Sheet	Type of Title	Title No	Status	Date of Registration	Expiry Date	Due Date	Area (Ha)
Alotta	NTS 31M06	CDC	1131116	Active	February 25, 2005	July 2, 2018	May 1, 2018	40.4
	NTS 31M06	CDC	1131117	Active	February 25, 2005	July 2, 2018	May 1, 2018	58.19
	NTS 31M06	CDC	1131118	Active	February 25, 2005	July 2, 2018	May 1, 2018	58.19
	NTS 31M06	CDC	1131119	Active	February 25, 2005	July 2, 2018	May 1, 2018	58.19
	NTS 31M06	CDC	1131120	Active	February 25, 2005	July 2, 2018	May 1, 2018	58.19
	NTS 31M06	CDC	1131127	Active	February 25, 2005	July 2, 2018	May 1, 2018	32.74
	NTS 31M06	CDC	1131128	Active	February 25, 2005	July 2, 2018	May 1, 2018	47.78
	NTS 31M06	CDC	1131129	Active	February 25, 2005	July 2, 2018	May 1, 2018	45.89
	NTS 31M06	CDC	1131130	Active	February 25, 2005	July 2, 2018	May 1, 2018	15.73
	NTS 31M06	CDC	1131131	Active	February 25, 2005	July 2, 2018	May 1, 2018	15.46
	NTS 31M06	CDC	1131132	Active	February 25, 2005	July 2, 2018	May 1, 2018	15.09
	NTS 31M06	CDC	1131133	Active	February 25, 2005	July 2, 2018	May 1, 2018	15.22
Delphi/ Patry	NTS 31M06	CDC	1131092	Active	February 25, 2005	July 2, 2018	May 1, 2018	58.21
	NTS 31M06	CDC	1131093	Active	February 25, 2005	July 2, 2018	May 1, 2018	58.21
	NTS 31M06	CDC	1131094	Active	February 25, 2005	July 2, 2018	May 1, 2018	58.21
Zullo	NTS 31M06	CDC	2462712	Active	Sept 19, 2016	Sept 18, 2018	July 18, 2018	58.23
	NTS 31M06	CDC	2462713	Active	Sept 19, 2016	Sept 18, 2018	July 18, 2018	58.23
	NTS 31M06	CDC	2466858	Active	October 21, 2016	October 20, 2018	August 19, 2018	58.22
Lorraine	NTS 31M07	CDC	2406736	Active	June 18, 2014	June 17, 2018	April 16, 2018	58.33
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	NTS 31M07	CDC	2460443	Active	August 31, 2016	August 30, 2018	June 29, 2018	58.32
	NTS 31M07	CDC	2460444	Active	August 31, 2016	August 30, 2018	June 29, 2018	58.31
	NTS 31M07	CDC	2411844	Active	September 15, 2014	Sept 14, 2018	July 14, 2018	58.34
	NTS 31M07	CDC	2363761	Active	September 18, 2012	Sept 17, 2018	July 17, 2018	74.53
	NTS 31M07	CDC	2415020	Active	October 23, 2014	October 22, 2018	August 21, 2018	37.2
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	NTS 31M07	CDC	2415022	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.35
	NTS 31M07	CDC	2415023	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.35
	NTS 31M07	CDC	2415024	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.35
	NTS 31M07	CDC	2415025	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.35
	NTS 31M07	CDC	2415026	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.35
	NTS 31M07	CDC	2415027	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.35
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	NTS 31M07	CDC	2415032	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.34
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	NTS 31M07	CDC	2415037	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.33
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	NTS 31M07	CDC	2415041	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.33
	NTS 31M07	CDC	2415042	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.32
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	NTS 31M07	CDC	2415054	Active	October 23, 2014	October 22, 2018	August 21, 2018	58.31
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	NTS 31M07	CDC	2415239	Active	October 28, 2014	October 27, 2018	August 26, 2018	58.36
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	NTS 31M07	CDC	2415243	Active	October 28, 2014	October 27, 2018	August 26, 2018	58.36
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	NTS 31M07	CDC	2415245	Active	October 28, 2014	October 27, 2018	August 26, 2018	58.36

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	NTS 31M07	CDC	2415247	Active	October 28, 2014	October 27, 2018	August 26, 2018	58.36
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	NTS 31M07	CDC	2369440	Active	November 6, 2012	November 5, 2018	Sept 4, 2018	42.48
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	NTS 31M07	CDC	2402024	Active	March 21, 2014	March 20, 2020	January 18, 2020	23.9
	NTS 31M07	CDC	2402025	Active	March 21, 2014	March 20, 2020	January 18, 2020	42.47
	NTS 31M07	CDC	2402026	Active	March 21, 2014	March 20, 2020	January 18, 2020	72.8

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Appendix 1: Use of Metal Equivalence Calculations

The composited value of the polymetallic (Ni-Cu-PGM-Au) mineralisation within Zeus's portfolio is presented as percentage nickel equivalents (NiEq%). The Lac Kelly deposit, located 5.5km from the Company's historic Lorraine Mine, has been the beneficiary of comprehensive metallurgical study. The deposit is considered as an analogue to the mineralisation style being sought by Zeus: Lac Kelly sits in the same greenstone belt, in the same package of rocks, host the same style of mineralisation in the same rock types, and includes the same suite of metals. The Lac Kelly (and the Lorraine Mine) indicate excellent metallurgical recoveries of the target metals. The Company posits that the mineralogy and geological setting of the Lac Kelly deposit offer an excellent indication of the expected recoveries across the deposit type, and thus qualify use of reporting on a metal equivalent basis. The metallurgical recoveries for the Lac Kelly deposit were adopted for use in the NiEq% calculations; these are: Ni (86%), Cu (96%), Co (92%); PGM + Au (80%). Metallurgical test work by Zeus is proposed to commence after the listing of the company and completion of the maiden drill campaign and is expected to underpin these assumptions.

NiEq% = (Ni%*86%) + (Cu%*0.492*96%) + (Co%*6.454*92%) + (Pt ppm*0.067*80%) + (Pd ppm*0.073*80%). Metal prices used are: Cu US$6,786/t, Ni US$13,789/t, Co US$88,999/t, PGM US$930/oz, (reference infomine.com spot prices quoted on 11-05-2018).

Note 1: A Report on the Kelly Lake Project (prepared for Loubel Exploration Inc.). J.D. Charlton, 11 February 2001

It is the company's opinion that the metallurgical studies will confirm that all the elements included in the above metal equivalents calculation have a reasonable potential to be recovered and sold.

Appendix 2: Alotta-Delphi Diamond Drilling Results

Hole	NAD83Z17_E	NAD83Z17_N	from	to	sample	Ni_Per	Cu_Per	Pd_gpt	Pt_ppb	Co_Per
AB46-02-01	633582	5255888	22.4	22.9	96071	0.0126	380	0.009	5	0.0051
AB46-02-01			22.9	24.5	96072	0.0071	132	0.008	5	0.0032
AB46-02-01			24.5	26	96073	0.0141	203	0.007	5	0.0042
AB46-02-01			44.9	45.4	96074	0.002	3.8	0.002	5	0.0006
AB46-02-01			63	64.5	96075	0.009	16.6	0.005	5	0.0027
AB46-02-01			64.5	66	96076	0.0084	41.6	0.006	5	0.0034
AB46-02-01			88.5	89.8	96077	0.0081	109	0.005	5	0.0032
AB46-02-01			89.8	91	96078	0.0065	46.8	0.002	5	0.0024
AB46-02-01			91	92.3	96079	0.0064	56.9	0.002	5	0.0024
AB46-02-01			92.3	93.5	96080	0.0086	18.6	0.001	5	0.0029
AB46-02-01			93.5	95	96081	0.0096	52.1	0.003	5	0.0031
AB46-02-01			113	114.5	96082	0.0102	56.5	0.002	5	0.0031
AB46-02-01			114.5	115	96083	0.0095	7.8	0.003	5	0.0025
AB46-02-01			115	116.5	96084	0.0175	10.8	0.004	5	0.0041
AB46-02-01			120.5	122.2	96085	0.0195	5.1	0.003	5	0.004
AB46-02-01			122.2	123.6	96086	0.0549	52.1	0.006	5	0.0081
AB46-02-01			177.5	179	96087	0.0549	52.8	0.005	5	0.0076
AB46-02-01			179	180	96088	0.0548	44.9	0.005	5	0.0088
AB46-02-01			180	181.7	96089	0.0212	39.7	0.007	5	0.0051
AB46-02-01			181.7	182.8	96090	0.0074	258	0.001	5	0.0047
AB46-02-01			182.8	184	96091	0.011	1080	0.001	5	0.007
AB46-02-01			184	185	96092	0.0102	140	0.004	5	0.0036
AB46-02-01			185	186.5	96093	0.0094	125	0.004	5	0.0035
AB46-02-01			193.1	194.7	96094	0.011	126	0.004	5	0.0037
AB46-02-02	633262	5256074	7	8.6	96110	0.0015	13.2	0.023	5	0.0009
AB46-02-02			15.5	17	96111	0.0045	43.9	0.018	5	0.0039
AB46-02-02			17	18.4	96112	0.0033	20	0.009	5	0.0031
AB46-02-02			18.4	19.2	96113	0.0015	46.5	0.012	5	0.0016
AB46-02-02			19.2	20.6	96114	0.0033	37.2	0.007	5	0.003
AB46-02-02			20.6	22	96117	0.0039	44.8	0.002	5	0.004
AB46-02-02			22	23.5	96118	0.004	69.4	0.002	5	0.005
AB46-02-02			23.5	25	96119	0.0033	144	0.001	5	0.0048
AB46-02-02			25	26.5	96120	0.0038	65.8	0.001	5	0.0048
AB46-02-02			26.5	28	96121	0.0035	101	0.001	5	0.0043
AB46-02-02			28	29.5	96122	0.0034	68.2	0.0005	5	0.0046
AB46-02-02			29.5	30.5	96123	0.0035	66.3	0.002	5	0.0047
AB46-02-02			30.5	32	96115	0.0031	65.2	0.007	5	0.0046
AB46-02-02			32	33.5	96124	0.004	99.4	0.002	5	0.0048
AB46-02-02			33.5	35	96125	0.0033	132	0.002	5	0.0052
AB46-02-02			35	36.5	96126	0.0027	66	0.002	5	0.0045
AB46-02-02			36.5	38	96127	0.0033	166	0.001	5	0.0052
AB46-02-02			57.4	59	96116	0.0011	7.8	0.01	5	0.0007
AB46-02-02			69.5	71	96128	0.0058	211	0.001	5	0.0047
AB46-02-02			71	72.5	96129	0.0058	186	0.002	5	0.0044

AB46-02-02			72.5	74	96130	0.006	97.1	0.002	5	0.0045
AB46-02-02			74	75.5	96131	0.0064	91.3	0.0005	5	0.0046
AB46-02-02			75.5	77	96132	0.0065	153	0.0005	5	0.0046
AB46-02-02			77	78.5	96133	0.0071	101	0.0005	5	0.0043
AB46-02-02			78.5	80	96134	0.0064	186	0.0005	5	0.0044
AB46-02-02			80	81.4	96135	0.0074	188	0.0005	5	0.0047
AB46-02-02			81.4	82.9	96136	0.0013	18.4	0.0005	5	0.0008
AB46-02-02			107.3	108.7	96137	0.0082	61	0.004	5	0.0039
AB46-02-02			114.5	116	96138	0.0087	62.9	0.003	5	0.0041
AB46-02-02			116	117.5	96139	0.0096	83.2	0.002	5	0.0043
AB46-02-02			124.7	126	96140	0.0096	60.8	0.003	5	0.0043
AB46-02-02			130.6	132.1	96141	0.0132	93	0.004	5	0.0047
AB46-02-02			136	137.5	96142	0.0104	51.8	0.004	5	0.0038
AB46-02-02			145.5	147	96143	0.0093	65.1	0.003	5	0.0035
AB46-02-02			150.5	152	96144	0.0124	21.1	0.004	5	0.0039
AB46-02-03	633582	5255888	22.65	23	96507	0.0067	110	0.008	5	0.0035
AB46-02-03			25	26	96506	0.013	103	0.007	5	0.0043
AB46-02-03			26	27.3	96505	0.0095	164	0.007	5	0.0041
AB46-02-03			27.64	28.52	96504	0.0149	202	0.008	5	0.0057
AB46-02-03			28.52	29.88	96503	0.0132	280	0.008	5	0.0068
AB46-02-03			62.32	63.31	96508	0.0046	127	0.005	5	0.0033
AB46-02-03			63.31	64.31	96509	0.0052	85.1	0.002	18	0.0043
AB46-02-03			96.99	98.41	96522	0.0083	71.4	0.015	11	0.0038
AB46-02-03			110.55	111.55	96523	0.0108	50.9	0.005	5	0.004
AB46-02-03			113.67	114.81	96524	0.0111	30.6	0.004	5	0.0036
AB46-02-03			114.81	115.4	96525	0.0102	44.2	0.004	5	0.0034
AB46-02-03			117.9	118.8	96501	0.0077	19.2	0.003	5	0.0024
AB46-02-03			118.8	119.65	96502	0.0083	20.6	0.003	5	0.0027
AB46-02-03			127.37	127.91	96527	0.0262	47.4	0.004	5	0.0052
AB46-02-03			127.91	128.91	96526	0.0755	29.1	0.004	5	0.0103
AB46-02-03			205.86	207.31	96528	0.0659	70.9	0.004	5	0.0099
AB46-02-03			207.31	208.7	96510	0.0498	50.7	0.0005	5	0.0075
AB46-02-03			208.7	209.99	96511	0.0228	61.1	0.009	13	0.005
AB46-02-03			209.99	210.85	96512	0.013	116	0.0005	16	0.0042
AB46-02-03			210.85	212	96513	0.01	321	0.0005	15	0.0064
AB46-02-03			212	213.48	96514	0.0109	336	0.0005	5	0.0068
AB46-02-03			213.48	214.72	96515	0.0094	291	0.0005	5	0.0055
AB46-02-03			214.72	216.03	96516	0.0033	259	0.0005	16	0.0019
AB46-02-03			216.03	217.03	96517	0.0131	139	0.009	5	0.0047
AB46-02-03			217.03	218.47	96518	0.0121	124	0.013	5	0.0043
AB46-02-03			218.47	219.89	96519	0.013	123	0.012	5	0.0047
AB46-02-03			219.89	221.35	96520	0.0122	106	0.012	5	0.0043
AB46-02-03			221.35	222.67	96521	0.0111	105	0.017	5	0.0037
BT-01-05	631628.6	5258579.9	47.5	48	13580	0.025	0.014	0.003	5	0.012
BT-01-05			48	49	13581	0.026	0.013	0.014	11	0.02
BT-01-05			49	50	13582	0.018	0.015	0.005	5	0.02
BT-01-05			50	50.75	13583	0.059	1.09	0.287	225	0.017

BT-01-05			50.75	51.75	13584	2.55	2.41	1.65	262	0.097
BT-01-05			51.75	52.75	13585	2.6	1.94	1.424	430	0.076
BT-01-05			52.75	53.75	13586	2.59	1.44	0.994	59	0.119
BT-01-05			53.75	54.75	13587	1.27	1.48	1.266	129	0.093
BT-01-05			54.75	55.55	13588	0.765	2.11	0.98	290	0.042
BT-01-05			55.55	56	13589	0.243	0.371	0.341	106	0.019
BT-01-05			56	57	13590	0.212	1.89	0.558	175	0.01
BT-01-05			57	58	13591	0.108	0.207	0.175	57	0.015
BT-01-05			58	59	13592	2.57	2.49	2.494	446	0.077
BT-01-05			59	59.9	13593	2.38	2.28	3.008	864	0.082
BT-01-05			59.9	60.15	13594	0.378	0.938	0.612	183	0.028
BT-01-05			60.15	60.42	13595	2.7	2.01	2.498	394	0.093
BT-01-05			60.42	62	13596	0.39	1.01	0.537	154	0.033
BT-01-05			62	63	13597	0.311	0.536	0.407	114	0.03
BT-01-05			63	64	13598	0.133	0.262	0.187	68	0.015
BT-01-05			64	65	13599	0.168	0.282	0.208	69	0.017
BT-01-05			65	66	13600	0.176	0.304	0.259	82	0.024
BT-01-05			66	67	13601	0.218	0.393	0.251	78	0.017
BT-01-05			67	68	13602	0.23	0.405	0.244	80	0.02
BT-01-05			68	69	13603	0.286	0.583	0.424	128	0.024
BT-01-05			69	70	13604	0.215	0.42	0.29	94	0.023
BT-01-05			70	71	13605	0.139	0.246	0.167	52	0.018
BT-01-05			71	72	13606	0.189	0.318	0.241	77	0.018
BT-01-05			72	72.75	13607	0.124	0.212	0.139	46	0.014
BT-01-05			72.75	73.65	13608	0.068	0.099	0.067	24	0.013
BT-01-05			73.65	74.65	13609	0.044	0.088	0.049	10	0.014
BT-01-05			74.65	75	13610	3.03	3.74	0.898	270	0.036
BT-01-05			75	76	13611	0.032	0.055	0.03	5	0.012
BT-01-05			76	77	13612	0.015	0.018	0.007	5	0.01
BT-01-06	631638.3	5258632	4	5	13551	0.014	0.01	0.006	5	0.012
BT-01-06			5	6	13552	0.011	0.005	0.002	5	0.012
BT-01-06			6	7	13553	0.065	0.147	0.115	40	0.025
BT-01-06			7	7.9	13554	0.404	0.534	0.492	173	0.034
BT-01-06			7.9	9	13555	0.605	0.73	0.647	222	0.048
BT-01-06			9	10	13556	0.355	0.592	0.451	149	0.036
BT-01-06			10	11	13557	0.342	0.552	0.352	132	0.034
BT-01-06			11	12	13558	0.207	0.309	0.227	77	0.03
BT-01-06			12	13	13559	0.16	0.211	0.163	53	0.023
BT-01-06			13	14	13560	0.123	0.145	0.134	44	0.023
BT-01-06			14	15	13561	0.131	0.171	0.139	48	0.022
BT-01-06			15	16	13562	0.156	0.216	0.162	69	0.022
BT-01-06			16	17	13563	0.139	0.192	0.134	48	0.021
BT-01-06			17	18	13564	0.082	0.11	0.061	21	0.02
BT-01-06			18	19	13565	0.133	0.169	0.11	40	0.02
BT-01-06			19	20	13566	0.168	0.282	0.17	58	0.023
BT-01-06			20	21	13567	0.245	0.439	0.333	122	0.025
BT-01-06			21	22	13568	0.161	0.278	0.213	79	0.024

BT-01-06			22	23	13569	0.141	0.205	0.144	49	0.022
BT-01-06			23	24	13570	0.151	0.236	0.105	39	0.024
BT-01-06			24	25	13571	0.127	0.197	0.085	31	0.022
BT-01-06			25	26	13572	0.193	0.38	0.1	59	0.023
BT-01-06			26	26.65	13573	0.135	0.172	0.226	77	0.019
BT-01-06			26.65	27.65	13574	0.124	0.163	0.133	48	0.02
BT-01-06			27.65	28.8	13575	0.126	0.161	0.196	77	0.018
BT-01-06			28.8	29.8	13576	0.047	0.039	0.05	25	0.017
BT-01-06			29.8	30.8	13577	0.037	0.026	0.051	45	0.016
BT-01-06			30.8	31.8	13578	0.035	0.06	0.041	18	0.011
BT-01-06			31.8	32.5	13579	0.018	0.013	0.047	18	0.01
BT-01-07	631628.4	5258579.5	51	52	13613	0.024	0.01	0.005	5	0.015
BT-01-07			52	53	13614	0.176	0.473	0.288	69	0.018
BT-01-07			53	53.4	13615	0.067	0.078	0.061	36	0.015
BT-01-07			53.4	54	13616	1.64	9.8	3.002	340	0.071
BT-01-07			54	55	13617	2.75	2.51	1.762	120	0.075
BT-01-07			55	56	13618	2.8	1.52	1.636	127	0.069
BT-01-07			56	57	13619	2.95	2.17	1.732	145	0.072
BT-01-07			57	58	13620	2.88	2.43	1.834	178	0.075
BT-01-07			58	59	13621	2.69	2.22	2.188	346	0.07
BT-01-07			59	60	13622	2.83	1.85	2.114	500	0.074
BT-01-07			60	60.65	13623	2.53	1.3	2.124	698	0.108
BT-01-07			60.65	62	13624	0.444	2.53	1.186	536	0.04
BT-01-07			62	63	13625	0.875	2.37	1.464	700	0.046
BT-01-07			63	64	13626	1.31	1.83	1.608	400	0.072
BT-01-07			64	65	13627	1.29	0.853	1.03	208	0.078
BT-01-07			65	66.5	13628	0.805	0.962	0.646	206	0.051
BT-01-07			66.5	68	13629	0.044	0.093	0.071	18	0.015
BT-01-07			68	69	13630	0.013	0.016	0.008	5	0.01
BT-01-07			69	70	13631	0.04	0.591	0.413	683	0.016
BT-01-07			70	71	13632	0.042	0.307	0.287	99	0.021
BT-01-07			71	72	13633	0.055	0.744	0.557	237	0.019
BT-01-07			72	73.2	13634	0.016	0.053	0.017	5	0.014
BT-01-07			73.2	74	13635	2.1	2.39	1.948	990	0.096
BT-01-07			74	75	13636	2.94	0.919	1.428	268	0.104
BT-01-07			75	76	13637	2.52	1.8	1.624	214	0.141
BT-01-07			76	77.3	13638	2.76	1.17	1.752	220	0.093
BT-01-07			77.3	78	13639	0.53	2.01	0.586	212	0.055
BT-01-07			78	79	13640	0.065	0.121	0.122	33	0.02
BT-01-07			79	80	13641	0.066	0.283	0.294	130	0.023
BT-01-08	631628.1	5258578.7	91.65	93.7	13642	0.022	0.024	0.014	5	0.013
BT-01-08			93.7	95	13643	0.016	0.012	0.01	19	0.01
BT-01-09	631601.9	5258581.9	72	72.65	13683	0.124	0.159	0.111	48	0.019
BT-01-09			72.65	73.55	13684	0.309	0.425	0.26	98	0.032
BT-01-09			73.55	75	13685	0.098	0.064	0.097	50	0.01
BT-01-10	631602	5258582.5	51.15	52	13687	0.248	0.342	0.247	94	0.03
BT-01-10			52	53	13688	0.313	0.469	0.367	138	0.03

BT-01-10			53	54	13689	0.22	0.322	0.231	85	0.019
BT-01-10			54	55	13690	0.084	0.14	0.101	39	0.013
BT-01-10			55	56	13691	0.087	0.162	0.1	61	0.014
BT-01-10			56	57	13692	0.038	0.03	0.031	12	0.01
BT-01-10			57	58	13693	0.097	0.157	0.091	39	0.017
BT-01-10			58	59	13694	0.091	0.104	0.086	40	0.01
BT-01-10			64.15	64.6	13695	0.212	0.327	0.229	94	0.023
BT-01-10			67.9	69	13696	0.074	0.053	0.044	22	0.015
BT-01-10			69	70	13697	0.126	0.161	0.112	44	0.012
BT-01-10			70	71	13698	0.172	0.247	0.192	64	0.019
BT-01-10			71	72.3	13699	0.218	0.403	0.252	107	0.024
BT-01-10			72.3	73.45	13700	0.989	4.12	0.718	175	0.19
BT-01-10			73.45	74.55	13701	0.348	0.606	0.517	157	0.021
BT-01-10			74.55	76	13702	0.312	0.489	0.376	120	0.031
BT-01-10			76	77	13703	0.401	0.538	0.415	130	0.019
BT-01-10			77	78.35	13704	0.362	0.609	0.501	149	0.023
BT-01-10			78.35	79.6	13705	0.131	0.176	0.145	52	0.023
BT-01-10			79.6	80.6	13706	0.007	0.01	0.006	5	0.01
BT-01-10			80.6	81.55	13707	0.012	0.01	0.008	5	0.01
BT-01-10			81.55	83	13708	0.161	0.307	0.121	40	0.027
BT-01-10			83	84	13709	0.135	0.235	0.173	59	0.014
BT-01-10			84	85	13710	0.043	0.042	0.034	12	0.005
BT-01-11	631620.2	5258625.5	11.25	12.25	13644	0.034	0.011	0.004	5	0.017
BT-01-11			12.25	13.25	13645	0.039	0.022	0.005	5	0.016
BT-01-11			13.25	14.4	13646	0.042	0.019	0.003	5	0.01
BT-01-11			14.4	15.35	13647	0.107	0.109	0.126	53	0.021
BT-01-11			15.35	16.9	13648	0.63	0.998	0.668	270	0.032
BT-01-11			16.9	18	13649	0.6	0.992	0.482	208	0.031
BT-01-11			18	19.7	13650	0.402	0.622	0.546	192	0.027
BT-01-11			19.7	20.5	13651	0.315	0.866	0.43	140	0.024
BT-01-11			20.5	20.75	13652	2.92	0.233	1.308	153	0.105
BT-01-11			20.75	22	13653	0.348	0.598	0.535	173	0.029
BT-01-11			22	23	13654	0.6	0.966	0.556	196	0.041
BT-01-11			23	24	13655	0.62	0.944	0.704	268	0.061
BT-01-11			24	25	13656	0.401	0.849	0.388	158	0.036
BT-01-11			25	26.35	13657	1.34	0.456	0.63	322	0.106
BT-01-11			26.35	27	13658	0.244	1.16	0.704	157	0.029
BT-01-11			27	28	13659	0.271	0.424	0.355	135	0.023
BT-01-11			28	29	13660	0.288	0.951	0.623	197	0.03
BT-01-11			29	30	13661	0.31	0.73	0.361	97	0.033
BT-01-11			30	31	13662	0.317	0.477	0.395	120	0.028
BT-01-11			31	32	13663	0.217	0.397	0.306	92	0.018
BT-01-11			32	33	13664	0.256	0.425	0.234	84	0.027
BT-01-11			33	34	13665	0.297	0.635	0.334	120	0.035
BT-01-11			34	35	13666	0.251	0.456	0.267	99	0.034
BT-01-11			35	36	13667	0.304	0.499	0.255	93	0.029
BT-01-11			36	37	13668	0.241	0.397	0.316	111	0.023

BT-01-11			37	38	13669	0.19	0.296	0.266	97	0.024
BT-01-11			38	39	13670	0.138	0.217	0.136	48	0.022
BT-01-11			39	40	13671	0.223	0.435	0.28	99	0.027
BT-01-11			40	41	13672	0.342	0.501	0.489	154	0.024
BT-01-11			41	42.35	13673	0.137	0.18	0.115	44	0.01
BT-01-11			42.35	44	13674	0.017	0.025	0.018	10	0.01
BT-01-11			44	45	13675	0.01	0.01	0.004	5	0.015
BT-01-11			45	46.25	13676	0.01	0.01	0.006	16	0.01
BT-01-11			46.25	47.25	13677	0.099	0.113	0.103	41	0.01
BT-01-11			47.25	48.25	13678	0.112	0.144	0.118	47	0.016
BT-01-11			48.25	49.25	13679	0.058	0.056	0.047	26	0.013
BT-01-11			49.25	50.2	13680	0.096	0.116	0.145	45	0.011
BT-01-11			50.2	50.45	13681	0.861	2.74	1.392	113	0.023
BT-01-11			50.45	51.5	13682	0.016	0.02	0.01	10	0.01
BT-01-12	631630.9	5258619.3	25	26	13711	0.189	0.255	0.18	72	0.011
BT-01-12			26	27.2	13712	0.154	1.75	1.638	167	0.02
BT-01-12			27.2	27.8	13713	2.42	3.33	2.218	392	0.091
BT-01-12			27.8	28.55	13714	3.06	1.21	1.648	268	0.117
BT-01-12			28.55	29.25	13715	0.931	1.82	1.412	650	0.046
BT-01-12			29.25	30	13716	0.397	0.671	0.682	250	0.018
BT-01-12			30	31	13717	0.326	0.454	0.445	157	0.02
BT-01-12			31	32	13718	0.262	0.442	0.48	176	0.019
BT-01-12			32	33	13719	0.345	0.534	0.496	173	0.025
BT-01-12			33	34	13720	0.313	0.468	0.392	133	0.019
BT-01-12			34	35	13721	0.302	0.804	0.494	166	0.026
BT-01-12			35	36	13722	0.316	0.476	0.474	166	0.017
BT-01-12			36	37	13723	0.356	0.475	0.49	167	0.016
BT-01-12			37	38	13724	0.344	0.533	0.438	180	0.015
BT-01-12			38	39	13725	0.373	0.553	0.542	181	0.021
BT-01-12			39	40	13726	0.376	0.642	0.624	200	0.014
BT-01-12			40	41	13727	0.34	0.505	0.492	180	0.015
BT-01-12			41	42	13728	0.313	0.546	0.414	149	0.013
BT-01-12			42	43	13729	0.349	0.518	0.458	162	0.012
BT-01-12			43	44	13730	0.249	0.378	0.304	107	0.013
BT-01-12			44	45	13731	0.267	0.43	0.358	115	0.014
BT-01-12			45	46	13732	0.277	0.4	0.407	129	0.019
BT-01-12			46	47	13733	0.291	0.412	0.369	135	0.018
BT-01-12			47	48	13734	0.3	0.399	0.352	124	0.023
BT-01-12			48	49	13735	0.096	0.131	0.1	37	0.015
BT-01-12			49	50	13736	0.047	0.033	0.022	11	0.011
BT-01-12			50	51	13737	0.101	0.164	0.108	46	0.021
BT-01-12			51	52	13738	0.192	0.255	0.186	71	0.019
BT-01-12			52	53	13739	0.144	0.179	0.173	68	0.017
BT-01-12			53	54	13740	0.096	0.111	0.148	46	0.01
BT-01-13	631631.3	5258620.3	18	19	13741	0.05	0.024	0.015	5	0.007
BT-01-13			19	20.25	13742	0.1	0.215	0.229	36	0.005
BT-01-13			20.25	20.85	13743	2.54	0.791	1.264	180	0.043

BT-01-13			20.85	21.7	13744	2.96	0.86	1.17	310	0.067
BT-01-13			21.7	23	13745	0.363	0.77	0.488	162	0.017
BT-01-13			23	24	13746	0.302	0.715	0.57	236	0.019
BT-01-13			24	25	13747	0.5	0.92	0.718	218	0.038
BT-01-13			25	26	13748	0.341	0.634	0.806	238	0.028
BT-01-13			26	27	13749	0.375	0.63	0.482	185	0.031
BT-01-13			27	28	13750	0.258	0.528	0.593	179	0.023
BT-01-13			28	29	13751	0.189	0.326	0.431	250	0.016
BT-01-13			29	30	13752	0.185	0.311	0.425	134	0.015
BT-01-13			30	31	13753	0.118	0.202	0.231	67	0.012
BT-01-13			31	32	13754	0.226	0.328	0.603	181	0.012
BT-01-13			32	33	13755	0.165	0.271	0.298	99	0.015
BT-01-13			33	34	13756	0.175	0.298	0.348	115	0.022
BT-01-13			34	35	13757	0.153	0.251	0.282	99	0.013
BT-01-13			35	36	13758	0.16	0.247	0.292	92	0.023
BT-01-13			36	37	13759	0.131	0.203	0.219	71	0.02
BT-01-13			37	38	13760	0.165	0.279	0.258	87	0.015
BT-01-13			38	39	13761	0.096	0.148	0.179	55	0.011
BT-01-13			39	40	13762	0.231	0.393	0.428	133	0.011
BT-01-13			40	41	13763	0.327	0.644	0.541	146	0.02
BT-01-13			41	42	13764	0.408	0.783	0.65	210	0.019
BT-01-13			42	43	13765	0.294	0.47	0.507	148	0.017
BT-01-13			43	44	13766	0.064	0.095	0.132	43	0.017
BT-01-13			44	45	13767	0.024	0.03	0.02	5	0.01
BT-01-14	631642.6	5258615.4	19.8	21	13768	0.393	0.687	0.572	206	0.027
BT-01-14			21	22	13769	0.357	0.603	0.566	200	0.021
BT-01-14			22	23	13770	0.373	0.74	0.856	243	0.023
BT-01-14			23	24	13771	0.403	0.773	0.626	248	0.02
BT-01-14			24	25	13772	0.399	0.686	0.934	316	0.02
BT-01-14			25	26	13773	0.345	0.621	0.89	284	0.022
BT-01-14			26	27	13774	0.314	0.565	0.464	168	0.031
BT-01-14			27	28	13775	0.285	0.511	0.75	237	0.02
BT-01-14			28	29	13776	0.264	0.431	0.649	195	0.016
BT-01-14			29	30	13777	0.134	0.214	0.322	97	0.01
BT-01-14			30	31	13778	0.172	0.282	0.394	124	0.013
BT-01-14			31	32	13779	0.175	0.295	0.423	116	0.005
BT-01-14			32	33	13780	0.155	0.236	0.321	92	0.005
BT-01-14			33	34	13781	0.174	0.283	0.452	132	0.014
BT-01-14			34	35	13782	0.182	0.258	0.394	120	0.005
BT-01-14			35	36	13783	0.052	0.042	0.045	5	0.005
BT-01-14			36	37	13784	0.056	0.075	0.076	21	0.005
BT-01-14			37	38	13785	0.03	0.044	0.038	15	0.005
BT-01-14			38	39	13786	0.076	0.325	0.297	113	0.005
BT-01-15	631615.8	5258582.1	77.8	79	13787	0.014	0.116	0.025	1124	0.005
BT-01-15			79	79.6	13788	0.796	18.65	2.722	944	0.028
BT-01-15			79.6	81	13789	0.031	0.425	0.076	20	0.005
BT-01-15			81	82	13790	0.005	0.146	0.018	5	0.005

BT-01-15			86.15	87	13791	0.01	0.052	0.0005	5	0.005
BT-01-15			87	87.9	13792	0.059	0.05	0.029	5	0.013
BT-01-17	631651.2	5258604.3	35.35	36	13793	0.138	0.408	0.329	92	0.041
BT-01-17			36	37	13794	0.248	0.628	0.464	183	0.027
BT-01-17			37	38	13795	0.08	0.111	0.074	38	0.014
BT-01-17			38	39	13796	0.081	0.114	0.097	38	0.015
BT-01-17			39	40.4	13797	0.129	0.287	0.217	105	0.018
BT-01-17			40.4	41	13798	0.411	5.3	1.268	384	0.146
BT-01-17			41	42	13799	2.26	1.12	1.368	220	0.127
BT-01-17			42	43.55	13800	1.92	0.709	1.236	133	0.162
BT-01-17			43.55	44.3	13801	0.902	1.29	1.236	644	0.091
BT-01-17			44.3	45.6	13802	0.021	0.402	0.246	95	0.005
BT-01-17			45.6	47	13803	0.01	0.053	0.021	5	0.005
BT-01-17			47	48	13804	0.005	0.01	0.0005	5	0.005
BT-01-17			48	49	13805	0.005	0.01	0.0005	5	0.005
BT-01-17			49	50	13806	0.01	0.024	0.0005	5	0.01
BT-01-17			50	51	13807	0.005	0.01	0.0005	5	0.005
BT-01-17			51	52	13808	0.069	0.247	0.564	80	0.003
BT-01-17			52	53	13809	0.005	0.005	0.0005	5	0.005
BT-01-17			53	54.5	13810	0.005	0.005	0.0005	5	0.014
BT-01-17			54.5	55.1	13811	2.22	1.82	2.26	96	0.071
BT-01-17			55.1	56	13812	0.016	0.042	0.039	5	0.005
BT-01-17			58	59	13813	0.01	0.01	0.0005	5	0.012
BT-01-17			59	60	13814	0.005	0.01	0.0005	5	0.005
BT-01-17			60	61	13815	0.005	0.005	0.0005	5	0.012
BT-01-17			61	62	13816	0.005	0.005	0.0005	5	0.013
BT-01-18	631651.5	5258605.8	23.8	25	13817	0.025	0.137	0.119	5	0.012
BT-01-18			25	26	13818	0.751	20.53	5.514	1554	0.063
BT-01-18			26	27	13819	0.01	0.137	0.033	5	0.021
BT-01-18			27	27.8	13820	0.01	1.63	0.544	195	0.02
BT-01-18			27.8	28.35	13821	0.7	1.25	2.422	2714	0.132
BT-01-18			28.35	29.5	13822	0.195	0.686	0.527	283	0.03
BT-01-18			29.5	31	13823	0.236	0.422	0.571	198	0.036
BT-01-18			31	32	13824	0.214	0.342	0.456	143	0.029
BT-01-18			32	33	13825	0.149	0.233	0.299	94	0.036
BT-01-18			33	34	13826	0.245	0.43	0.445	159	0.04
BT-01-18			34	35	13827	0.246	0.404	0.443	156	0.028
BT-01-18			35	36	13828	0.205	0.308	0.396	136	0.032
BT-01-18			36	37	13829	0.047	0.037	0.018	5	0.015
BT-01-19	631615.3	5258623.1	35.8	36.8	13830	0.033	0.248	0.484	280	0.02
BT-01-19			36.8	38	13831	1.88	4.98	2.77	146	0.142
BT-01-19			38	39	13832	2.18	2.12	2.364	2646	0.116
BT-01-19			39	40	13833	2.91	1.38	1.106	210	0.105
BT-01-19			40	41	13834	2.35	1.6	2.11	1198	0.092
BT-01-19			41	42	13835	2.27	1.91	0.942	364	0.099
BT-01-19			42	43	13836	2.32	2.03	1.554	292	0.106
BT-01-19			43	44	13837	2.22	1.94	1.47	708	0.096

BT-01-19			44	45	13838	2.32	1.78	1.888	488	0.099
BT-01-19			45	46	13839	2.35	1.86	1.87	156	0.096
BT-01-19			46	47.23	13840	2.98	0.787	0.75	28	0.124
BT-01-19			47.23	48	13841	0.618	0.703	1.158	222	0.045
BT-01-19			48	49.1	13842	0.208	0.572	0.624	158	0.027
BT-01-19			49.1	50	13843	1.81	3.35	1.728	175	0.124
BT-01-19			50	51	13844	2.29	1.66	1.682	63	0.104
BT-01-19			51	52	13845	2.63	2.66	2.22	238	0.095
BT-01-19			52	53	13846	2.64	2.69	1.406	72	0.1
BT-01-19			53	54	13847	2.3	1.42	0.838	21	0.118
BT-01-19			54	55	13848	1.22	3.31	1.802	380	0.214
BT-01-19			55	56	13849	2.07	0.602	0.916	428	0.156
BT-01-19			56	57.25	13850	0.983	4.07	1.394	992	0.137
BT-01-19			57.25	57.8	13851	0.16	3.12	1.822	982	0.082
BT-01-19			57.8	59	13852	0.023	0.317	0.249	131	0.011
BT-01-19			73.25	74.25	13853	0.028	0.036	0.011	5	0.005
BT-01-19			74.25	75.25	13854	2.43	2.12	1.57	972	0.111
BT-01-19			75.25	76.55	13855	2.36	1.52	1.5	188	0.125
BT-01-19			76.55	77.55	13856	0.064	0.249	0.25	30	0.013
BT-01-20	631592.4	5258618.3	48	49	13862	0.256	0.403	0.359	93	0.012
BT-01-20			49	50	13863	0.32	0.53	0.426	116	0.033
BT-01-20			50	51	13864	0.311	0.584	0.467	131	0.03
BT-01-20			51	52.4	13865	0.228	0.343	0.372	102	0.019
BT-01-20			52.4	54.15	13866	0.102	0.028	0.011	5	0.019
BT-01-23	631585	5258665.6	43.2	44.2	13867	0.175	0.221	0.246	89	0.016
BT-01-23			44.2	45.2	13868	0.127	0.156	0.15	43	0.017
BT-01-23			45.2	46.2	13869	0.126	0.156	0.125	34	0.014
BT-01-23			46.2	47.2	13870	0.185	0.245	0.182	50	0.019
BT-01-23			47.2	48.2	13871	0.131	0.177	0.165	46	0.017
BT-01-27	631682.7	5258159.7	73	74.23	13857	0.015	0.017	0.012	22	0.005
BT-01-27			76.55	77.4	13858	0.016	0.021	0.005	5	0.005
BT-01-27			77.95	78.6	13859	0.015	0.017	0.003	5	0.017
BT-01-27			82.72	84.18	13860	0.025	0.018	0.008	5	0.023
BT-01-29	631276.8	5258195.5	47.57	48	22601	0.005	0.005	0.0005	5	0.005
BT-01-29			51.05	51.65	22602	0.005	0.005	0.0005	5	0.005
BT-01-29			61.52	63	22603	0.005	0.005	0.0005	5	0.005
BT-01-29			79.18	80.97	22604	0.005	0.005	0.001	5	0.005
BT-01-29			80.97	81.86	22605	0.017	0.03	0.0005	5	0.01
BT-01-29			81.86	83.18	22606	0.013	0.005	0.0005	5	0.005
BT-01-29			83.18	84.85	22607	0.016	0.015	0.0005	5	0.005
BT-01-29			86.2	87.65	22608	0.017	0.016	0.0005	5	0.005
BT-01-29			87.65	89.2	22609	0.026	0.015	0.0005	5	0.005
BT-01-29			89.2	89.8	22610	0.028	0.019	0.002	5	0.005
BT-01-29			89.8	90.5	22611	0.02	0.02	0.0005	5	0.005
BT-01-29			90.5	91.65	22612	0.01	0.005	0.0005	5	0.005
BT-01-29			91.65	93	22613	0.005	0.01	0.0005	5	0.005
BT-01-29			93	94.55	22614	0.005	0.005	0.0005	5	0.005

BT-01-29			94.55	95.8	22615	0.005	0.005	0.0005	5	0.005
BT-01-29			95.8	97.45	22616	0.005	0.005	0.0005	5	0.005
BT-01-29			97.45	98.85	22617	0.005	0.005	0.0005	5	0.005
BT-01-29			98.85	100.3	22618	0.005	0.01	0.0005	5	0.005
BT-01-30	631137.6	5258106.2	128.65	129.8	22970	0.005	0.021	0.001	5	0.005
BT-01-32	631592.2	5258625.7	36.65	38	13872	0.146	0.168	0.151	53	0.021
BT-01-32			38	39	13873	0.273	0.432	0.299	114	0.026
BT-01-32			39	40	13874	0.102	0.12	0.13	33	0.023
BT-01-32			40	41	13875	0.109	0.158	0.118	39	0.015
BT-01-32			41	41.4	13876	0.425	0.292	0.213	42	0.036
BT-01-32			53	54.25	13877	0.051	0.089	0.061	20	0.004
BT-01-32			54.25	55.4	13878	1.83	1.8	2.004	478	0.072
BT-01-32			55.4	56	13879	2.75	1.52	1.958	306	0.103
BT-01-32			56	57	13880	0.465	0.579	0.629	195	0.035
BT-01-32			57	58	13881	0.409	1.03	0.906	254	0.033
BT-01-32			58	59	13882	1.09	0.991	7.962	2860	0.038
BT-01-32			59	60.75	13883	0.593	1.21	0.896	166	0.034
BT-01-32			60.75	62	13884	2.72	0.494	1.204	110	0.19
BT-01-32			62	63	13885	3.18	0.106	1.71	63	0.146
BT-01-32			63	64	13886	2.06	1.62	1.368	39	0.304
BT-01-32			64	65	13887	1.53	1.91	1.21	101	0.364
BT-01-32			65	66	13888	0.24	0.622	1.584	56	0.257
BT-01-32			66	67.35	13889	2.75	0.519	1.642	57	0.119
BT-01-32			67.35	68.35	13890	0.311	0.546	0.423	103	0.026
BT-01-32			68.35	69.35	13891	0.063	0.05	0.043	13	0.015
BT-01-32			69.35	70.35	13892	0.036	0.023	0.015	5	0.016
BT-01-32			70.35	71.35	13893	0.027	0.018	0.01	5	0.017
BT-01-32			71.35	72.15	13894	0.049	0.258	0.108	34	0.014
BT-01-32			72.15	73	13895	2.26	1.74	1.514	322	0.105
BT-01-32			73	74	13896	2.66	4.06	2.58	358	0.098
BT-01-32			74	75	13897	2.81	1.8	1.326	220	0.107
BT-01-32			75	76	13898	2.7	1.85	1.842	392	0.113
BT-01-32			76	77	13899	2.68	2.49	1.948	432	0.105
BT-01-32			77	78	13900	3.24	2.57	1.354	266	0.121
BT-01-32			78	79	13901	3.08	1.73	2.056	330	0.119
BT-01-32			79	80.55	13902	2.79	1.23	1.616	346	0.182
BT-01-32			80.55	81.65	13903	0.565	2.63	1.19	578	0.053
BT-01-32			81.65	82.65	13904	1.74	3.23	2.624	1314	0.084
BT-01-32			82.65	83.65	13905	2.28	1.72	3.688	2750	0.151
BT-01-32			83.65	84.35	13906	1.98	3.13	2.462	2666	0.162
BT-01-32			84.35	85.35	13907	0.115	1.88	0.302	228	0.021
BT-01-32			85.35	86.05	13908	0.067	4.72	0.738	486	0.004
BT-01-32			86.05	87.65	13909	0.023	0.331	0.077	20	0.018
BT-01-32			91.3	92.3	13910	0.017	0.024	0.014	5	0.01
BT-01-32			92.3	93.3	13911	2.55	3.54	1.894	786	0.082
BT-01-32			93.3	94.3	13912	3.1	3.52	1.646	198	0.104
BT-01-32			94.3	95.3	13913	1.47	2.11	0.864	356	0.053

BT-01-32			95.3	96.3	13914	2.14	9.12	2.512	116	0.08
BT-01-32			96.3	97.1	13915	2.9	2.6	1.98	416	0.097
BT-01-32			97.1	98	13918	3	1.62	1.864	116	0.123
BT-01-32			98	99	13919	3.09	1.92	2.098	1070	0.119
BT-01-32			99	100.2	13920	2.82	3.88	2.686	2078	0.109
BT-01-32			100.2	101	13921	3.1	1.67	1.95	416	0.128
BT-01-32			101	101.5	13922	2.76	1.02	1.78	120	0.067
BT-01-32			101.5	102.3	13916	2.4	1.51	2.084	202	0.126
BT-01-32			102.3	103.3	13917	0.143	0.725	0.685	242	0.011
BT-01-33	631591.3	5258625.9	45	46	13923	0.305	0.462	0.278	102	0.029
BT-01-33			46	47	13924	0.151	0.264	0.162	60	0.015
BT-01-33			47	48	13925	0.081	0.11	0.071	27	0.011
BT-01-33			48	49	13926	0.046	0.03	0.015	5	0.014
BT-01-33			49	50	13927	0.089	0.088	0.072	28	0.016
BT-01-33			50	51	13928	0.254	0.361	0.269	97	0.027
BT-01-33			51	52	13929	0.246	0.439	0.375	147	0.02
BT-01-33			52	53	13930	0.185	0.395	0.312	106	0.023
BT-01-33			53	54	13931	0.132	0.226	0.186	65	0.018
BT-01-33			54	55	13932	0.085	0.116	0.087	32	0.012
BT-01-33			55	56	13933	0.128	0.186	0.164	66	0.015
BT-01-33			56	57	13934	0.111	0.125	0.095	40	0.023
BT-01-33			57	58	13935	0.041	0.036	0.018	5	0.012
BT-01-33			58	59	13936	0.035	0.03	0.019	5	0.01
BT-01-33			59	59.9	13937	0.039	0.169	0.071	14	0.021
BT-01-33			59.9	61	13938	2.62	2.46	2.526	722	0.093
BT-01-33			61	62	13939	2.49	1.28	1.334	446	0.08
BT-01-33			62	63	13940	2.77	1.3	1.952	1082	0.099
BT-01-33			63	64	13941	2.66	0.65	1.534	308	0.071
BT-01-33			64	65	13942	3.63	1.11	1.574	272	0.159
BT-01-33			65	66	13943	3.11	1.13	1.438	412	0.114
BT-01-33			66	67	13944	2.93	1.34	1.82	950	0.115
BT-01-33			67	68	13945	2.87	1.8	2.52	330	0.144
BT-01-33			68	69	13946	3.25	1.44	2.312	364	0.136
BT-01-33			69	70.15	13947	3.12	1.64	1.994	162	0.145
BT-01-33			70.15	71.55	13948	1.05	0.847	1.284	137	0.105
BT-01-33			71.55	72.7	13949	0.223	0.904	0.653	279	0.029
BT-01-33			72.7	73.75	13950	0.09	0.243	0.173	71	0.015
BT-01-33			103.2	104.25	13951	0.057	0.3	0.107	572	0.017
BT-01-33			104.25	105.2	13952	3.06	2.54	2.256	520	0.162
BT-01-33			105.2	106	13953	0.12	0.247	0.245	44	0.024
BT-01-35	631569.7	5258629.9	67.65	68.65	13954	0.249	0.354	0.243	103	0.023
BT-01-35			68.65	69.65	13955	0.392	0.565	0.368	150	0.05
BT-01-35			69.65	70.75	13956	0.277	0.411	0.293	110	0.027
BT-01-35			70.75	71.75	13957	0.241	0.316	0.268	100	0.031
BT-01-35			71.75	72.8	13958	0.19	0.263	0.196	78	0.028
BT-01-35			72.8	73.65	13959	0.102	0.121	0.063	24	0.023
BT-01-35			73.65	74.65	13960	2.83	1.85	2.25	264	0.118

BT-01-35			74.65	75.65	13961	2.96	1.64	2.042	664	0.121
BT-01-35			75.65	76.5	13962	2.53	1.2	1.894	1330	0.08
BT-01-35			76.5	77.2	13963	2.76	0.699	1.622	67	0.088
BT-01-35			77.2	78.2	13964	2.77	0.871	1.684	58	0.111
BT-01-35			78.2	79.4	13965	2.55	1.28	1.864	90	0.181
BT-01-35			79.4	80.4	13966	0.764	3.16	1.144	116	0.047
BT-01-35			80.4	81.4	13967	0.87	3.23	1.076	77	0.052
BT-01-35			81.4	82.4	13968	1.08	3.94	1.164	52	0.265
BT-01-35			82.4	83.4	13969	2.64	0.189	1.662	48	0.125
BT-01-35			83.4	84.25	13970	2.62	0.453	2.168	81	0.119
BT-01-35			84.25	85	13971	0.931	0.684	0.9	137	0.089
BT-01-35			85	86.35	13972	0.325	1.21	0.632	485	0.039
BT-01-35			91.5	92.5	13973	0.047	0.077	0.093	24	0.014
BT-01-35			92.5	93.5	13974	0.083	6.43	1.214	430	0.027
BT-01-35			93.5	94.5	13975	0.017	0.217	0.064	29	0.019
BT-01-35			102.75	103.75	13976	0.064	0.326	0.29	180	0.039
BT-01-35			103.75	104.5	13977	2.74	0.964	2.38	728	0.068
BT-01-35			104.5	105.5	13978	0.071	0.037	0.046	16	0.012
BT-01-35			119.5	120.2	13979	0.05	0.015	0.2	89	0.02
BT-01-35			120.2	121.1	13980	1.97	3.31	0.95	458	0.137
BT-01-35			121.1	121.9	13981	2.76	2.86	1.296	86	0.131
BT-01-35			121.9	122.9	13982	0.027	0.025	0.02	14	0.012
BT-01-36	632663.03	5256028.7	29.5	30.4	22651	0.01	0.02	0.01	10	0.01
BT-01-36			30.4	31	22652	0.005	0.02	0.006	5	0.005
BT-01-36			31	32	22653	0.005	0.01	0.008	5	0.005
BT-01-36			32	33.2	22654	0.01	0.005	0.006	5	0.005
BT-01-36			33.2	34	22655	0.01	0.005	0.008	5	0.005
BT-01-36			34	34.9	22656	0.01	0.005	0.01	5	0.005
BT-01-36			34.9	35.8	22657	0.005	0.02	0.008	5	0.005
BT-01-36			35.8	36.7	22658	0.005	0.01	0.007	5	0.005
BT-01-36			36.7	37.7	22659	0.005	0.01	0.008	14	0.005
BT-01-36			37.7	39	22660	0.01	0.005	0.004	5	0.005
BT-01-36			39	40	22661	0.005	0.01	0.004	5	0.005
BT-01-36			40	41	22662	0.005	0.005	0.004	5	0.005
BT-01-36			41	42	22663	0.01	0.01	0.007	5	0.005
BT-01-36			42	43	22664	0.01	0.005	0.0005	5	0.005
BT-01-36			43	44	22665	0.01	0.01	0.0005	5	0.005
BT-01-36			44	45	22666	0.01	0.005	0.0005	14	0.005
BT-01-36			45	46	22667	0.01	0.01	0.0005	5	0.005
BT-01-36			46	47	22668	0.01	0.005	0.0005	11	0.005
BT-01-36			47	48	22669	0.01	0.005	0.0005	10	0.005
BT-01-36			48	49	22670	0.01	0.005	0.0005	5	0.005
BT-01-36			49	50.1	22671	0.005	0.005	0.0005	14	0.005
BT-01-36			50.1	51.15	22672	0.01	0.005	0.0005	19	0.005
BT-01-36			51.15	51.55	22673	0.03	0.07	0.0005	16	0.005
BT-01-36			51.55	52.2	22674	9.73	2.31	0.048	72	0.005
BT-01-36			52.2	52.7	22675	4.16	4.54	0.76	176	0.09

BT-01-36			52.7	53	22676	2.03	1.49	0.828	900	0.16
BT-01-36			53	53.5	22677	0.27	0.37	0.207	91	0.02
BT-01-36			53.5	55	22678	0.06	0.05	0.014	19	0.02
BT-01-36			55	56	22679	0.21	0.3	0.106	61	0.005
BT-01-36			56	57	22680	0.16	0.22	0.145	72	0.02
BT-01-36			57	58	22681	0.12	0.16	0.134	37	0.01
BT-01-36			58	59	22682	0.09	0.16	0.094	29	0.01
BT-01-36			59	60	22683	0.03	0.02	0.003	5	0.005
BT-01-36			60	61	22684	0.04	0.03	0.01	14	0.005
BT-01-36			61	62.2	22685	0.03	0.07	0.012	24	0.005
BT-01-36			62.2	63.5	22686	0.02	0.005	0.0005	5	0.005
BT-01-36			68.7	70	22687	0.02	0.01	0.0005	5	0.005
BT-01-36			105.1	106.6	22688	0.02	0.005	0.0005	11	0.005
BT-01-36			106.6	107.6	22689	0.02	0.005	0.0005	5	0.005
BT-01-36			122	123	22690	0.02	0.01	0.006	5	0.01
BT-01-36			123	124	22691	0.01	0.005	0.005	10	0.01
BT-01-36			124	125	22692	0.02	0.03	0.007	13	0.01
BT-01-36			125	126.2	22693	0.02	0.02	0.008	5	0.02
BT-01-37	632662.45	5256027.97	79.1	79.9	22694	0.02	0.005	0.007	5	0.01
BT-01-37			79.9	80.65	22695	0.02	0.02	0.005	11	0.005
BT-01-37			80.65	81.5	22696	0.01	0.005	0.0005	5	0.005
BT-01-37			81.5	82.4	22697	0.005	0.005	0.0005	5	0.005
BT-01-37			82.4	82.7	22698	0.03	0.04	0.007	11	0.005
BT-01-37			82.7	83.9	22699	0.01	0.005	0.004	5	0.01
BT-01-37			83.9	85	22700	0.06	0.005	0.003	5	0.01
BT-01-37			85	86	22701	0.07	0.04	0.067	36	0.01
BT-01-37			86	87	22702	0.04	0.02	0.022	23	0.005
BT-01-37			87	88	22703	0.02	0.005	0.008	5	0.005
BT-01-37			88	88.8	22704	0.01	0.005	0.009	5	0.005
BT-01-37			88.8	89.8	22705	0.04	0.005	0.08	32	0.005
BT-01-37			89.8	90.5	22706	0.36	0.41	0.381	138	0.01
BT-01-37			90.5	91.3	22707	0.23	0.16	0.131	41	0.02
BT-01-37			91.3	92.7	22708	0.04	0.02	0.014	5	0.02
BT-01-37			92.7	93.9	22709	0.02	0.005	0.002	5	0.005
BT-01-37			93.9	95	22710	0.01	0.005	0.0005	5	0.005
BT-01-37			95	96	22711	0.01	0.005	0.002	5	0.005
BT-01-37			96	97	22712	0.04	0.03	0.059	24	0.005
BT-01-37			97	98	22713	0.08	0.09	0.054	21	0.005
BT-01-37			98	99	22714	0.24	0.23	0.184	49	0.005
BT-01-37			99	100	22715	0.02	0.005	0.002	5	0.02
BT-01-37			100	101	22716	0.02	0.005	0.006	5	0.005
BT-01-37			101	102	22717	0.01	0.005	0.006	5	0.01
BT-01-37			102	103	22718	0.01	0.005	0.003	5	0.005
BT-01-37			103	104	22740	0.005	0.005	0.003	5	0.005
BT-01-38	632633.41	5255972.77	10.7	11.7	22741	0.07	0.005	0.002	5	0.005
BT-01-38			21.5	23	22742	0.08	0.005	0.0005	5	0.005
BT-01-38			23	24	22743	0.08	0.005	0.002	5	0.005

BT-01-38			24	25.3	22744	0.08	0.005	0.001	5	0.005
BT-01-38			40.5	42	22745	0.06	0.005	0.006	5	0.005
BT-01-38			42	43.5	22746	0.07	0.005	0.015	10	0.005
BT-01-38			43.5	45	22747	0.06	0.005	0.002	5	0.01
BT-01-38			45	46.5	22748	0.06	0.005	0.003	5	0.01
BT-01-38			46.5	48	22749	0.06	0.005	0.002	21	0.01
BT-01-38			48	49.2	22750	0.06	0.005	0.004	5	0.005
BT-01-38			68.6	70.1	22751	0.01	0.005	0.005	5	0.005
BT-01-38			70.1	71.5	22752	0.02	0.005	0.0005	5	0.005
BT-01-38			76	77	22753	0.02	0.005	0.006	5	0.01
BT-01-38			77	78.2	22754	0.02	0.005	0.006	23	0.01
BT-01-38			89.8	91.3	22755	0.01	0.005	0.004	5	0.01
BT-01-38			91.3	92.4	22756	0.02	0.005	0.009	5	0.005
BT-01-38			92.4	93.5	22757	0.01	0.02	0.006	5	0.01
BT-01-38			93.5	94.7	22758	0.02	0.03	0.007	11	0.01
BT-01-38			99	100	22759	0.06	0.005	0.0005	5	0.01
BT-01-38			100	101	22760	0.06	0.005	0.004	25	0.01
BT-01-38			101	102.5	22761	0.06	0.005	0.004	5	0.01
BT-01-38			102.5	104	22762	0.07	0.005	0.006	5	0.01
BT-01-38			107.5	109	22763	0.08	0.005	0.004	14	0.005
BT-01-38			122.8	124.15	22764	0.07	0.005	0.004	13	0.01
BT-01-38			124.15	125.2	22765	0.07	0.005	0.002	15	0.02
BT-01-38			125.2	126.7	22766	0.08	0.005	0.002	5	0.01
BT-01-38			126.7	128.2	22767	0.07	0.005	0.003	10	0.01
BT-01-38			128.2	129.7	22768	0.07	0.005	0.007	5	0.01
BT-01-38			129.7	131	22769	0.08	0.005	0.009	11	0.01
BT-01-38			131	132.5	22770	0.08	0.005	0.009	5	0.01
BT-01-38			132.5	134	22771	0.03	0.005	0.0005	5	0.01
BT-01-38			134	135.5	22772	0.02	0.005	0.006	5	0.01
BT-01-38			135.5	137	22773	0.03	0.005	0.006	12	0.005
BT-01-38			137	138.5	22774	0.02	0.005	0.0005	5	0.01
BT-01-38			138.5	140	22775	0.02	0.005	0.0005	12	0.01
BT-01-38			140	141.5	22776	0.03	0.02	0.011	5	0.01
BT-01-38			141.5	143	22777	0.04	0.005	0.031	29	0.01
BT-01-38			143	144.4	22778	0.01	0.005	0.004	12	0.01
BT-01-39	632768.48	5255989.32	23	24.2	22719	0.01	0.005	0.001	5	0.01
BT-01-39			28.4	29.5	22720	0.01	0.02	0.004	5	0.005
BT-01-39			29.5	30.5	22721	0.01	0.02	0.003	10	0.005
BT-01-39			67.9	68.8	22722	0.02	0.005	0.007	5	0.005
BT-01-39			71.7	72.1	22723	0.02	0.005	0.006	5	0.005
BT-01-39			72.1	72.9	22724	0.03	0.005	0.004	5	0.005
BT-01-39			72.9	73.3	22725	0.02	0.02	0.002	5	0.005
BT-01-39			92.5	93.5	22726	0.06	0.005	0.001	5	0.01
BT-01-39			93.5	94.5	22727	0.06	0.005	0.0005	5	0.005
BT-01-39			94.5	95.5	22728	0.06	0.005	0.003	5	0.005
BT-01-39			95.5	96.5	22729	0.06	0.005	0.004	5	0.01
BT-01-39			105.3	106.8	22730	0.07	0.005	0.001	5	0.005

BT-01-39			106.8	108.3	22731	0.07	0.005	0.002	5	0.005
BT-01-39			108.3	109.8	22732	0.08	0.005	0.002	5	0.005
BT-01-39			109.8	111.3	22733	0.08	0.005	0.002	5	0.005
BT-01-39			117.3	118.5	22734	0.02	0.005	0.01	14	0.01
BT-01-39			118.5	119.5	22735	0.05	0.005	0.003	5	0.01
BT-01-39			119.5	120.5	22736	0.05	0.02	0.002	5	0.005
BT-01-39			136.6	137.8	22737	0.005	0.02	0.013	11	0.005
BT-01-39			137.8	138.8	22738	0.005	0.01	0.01	5	0.005
BT-01-39			138.8	139.9	22739	0.005	0.005	0.007	5	0.005
BT-01-40	632622.84	5256019.99	5	6.4	22779	0.02	0.005	0.0005	5	0.005
BT-01-40			31.2	32.1	22780	0.05	0.005	0.003	5	0.01
BT-01-40			32.1	32.85	22781	0.04	0.005	0.001	5	0.005
BT-01-40			32.85	33.9	22782	0.02	0.005	0.002	5	0.01
BT-01-40			33.9	34.6	22783	0.01	0.005	0.0005	5	0.01
BT-01-40			39.9	41	22784	0.03	0.005	0.003	12	0.005
BT-01-40			41	42	22785	0.03	0.005	0.003	10	0.01
BT-01-40			42	43	22786	0.02	0.005	0.003	5	0.01
BT-01-40			44.7	46	22787	0.03	0.005	0.0005	5	0.005
BT-01-40			46	47	22788	0.03	0.005	0.003	5	0.01
BT-01-40			47	48.5	22789	0.02	0.005	0.002	5	0.01
BT-01-40			48.5	50	22790	0.02	0.005	0.004	5	0.01
BT-01-40			50	51.2	22791	0.02	0.005	0.003	11	0.02
BT-01-40			56.7	58.2	22792	0.02	0.005	0.002	12	0.01
BT-01-40			76.4	77.4	22793	0.1	0.09	0.018	5	0.01
BT-01-40			77.4	78.2	22794	0.2	0.31	0.223	76	0.02
BT-01-40			78.2	79.2	22795	0.21	0.29	0.22	69	0.02
BT-01-40			79.2	80	22796	0.3	1.64	0.31	172	0.02
BT-01-40			80	81	22797	0.45	0.54	0.451	129	0.03
BT-01-40			81	82	22798	0.24	0.41	0.305	95	0.03
BT-01-40			82	83	22799	0.21	1.04	0.147	92	0.02
BT-01-40			83	84.1	22800	0.39	0.46	0.282	99	0.02
BT-01-40			84.1	85	22801	0.39	1.51	0.356	162	0.03
BT-01-40			85	86	22802	0.65	0.65	0.458	153	0.03
BT-01-40			86	87	22803	0.48	1.11	0.385	144	0.04
BT-01-40			87	88	22804	0.61	0.64	0.414	139	0.03
BT-01-40			88	88.9	22805	0.6	0.74	0.41	165	0.06
BT-01-40			88.9	89.9	22806	0.61	0.81	0.427	165	0.05
BT-01-40			89.9	90.9	22807	0.64	0.63	0.493	169	0.05
BT-01-40			90.9	92	22808	1.2	1.97	0.634	287	0.05
BT-01-40			92	93	22809	0.63	0.92	0.399	160	0.08
BT-01-40			93	94	22810	0.42	0.6	0.261	110	0.05
BT-01-40			94	95	22811	0.55	0.32	0.42	107	0.02
BT-01-40			95	95.9	22812	0.43	1.04	0.25	133	0.03
BT-01-40			95.9	96.7	22813	0.44	0.63	0.323	135	0.05
BT-01-40			96.7	97.4	22814	0.15	0.14	0.104	30	0.04
BT-01-40			97.4	98.45	22815	0.36	0.36	0.29	91	0.01
BT-01-40			98.45	99.05	22816	0.04	0.01	0.005	5	0.03

BT-01-40			99.05	99.9	22817	0.03	0.005	0.008	5	0.005
BT-01-40			99.9	101.1	22818	0.02	0.005	0.004	5	0.005
BT-01-40			101.1	102.2	22819	0.02	0.005	0.006	5	0.01
BT-01-40			120.2	121.2	22820	0.02	0.02	0.006	5	0.005
BT-01-40			124	124.9	22821	0.02	0.005	0.002	10	0.01
BT-01-41	632323.43	5256324.81	4.4	5.9	22899	0.005	0.005	0.006	5	0.005
BT-01-41			5.9	7.4	22900	0.005	0.005	0.0005	5	0.005
BT-01-41			7.4	8.3	22901	0.019	0.05	0.001	5	0.005
BT-01-41			8.3	9.7	22902	0.005	0.005	0.0005	5	0.005
BT-01-41			9.7	11	22903	0.005	0.005	0.0005	5	0.005
BT-01-41			11	12.5	22904	0.005	0.005	0.0005	5	0.005
BT-01-41			12.5	14	22905	0.005	0.005	0.0005	5	0.005
BT-01-41			14	15	22906	0.005	0.005	0.0005	0	0.005
BT-01-41			15	16	22907	0.005	0.005	0.0005	0	0.005
BT-01-41			16	17.2	22908	0.005	0.005	0.0005	5	0.005
BT-01-41			17.2	18.6	22909	0.005	0.005	0.0005	5	0.005
BT-01-41			18.6	20.1	22910	0.005	0.013	0.0005	5	0.005
BT-01-41			20.1	21.6	22911	0.005	0.005	0.001	5	0.005
BT-01-41			21.6	22.6	22912	0.005	0.018	0.0005	5	0.005
BT-01-41			22.6	23.3	22913	0.005	0.018	0.0005	5	0.005
BT-01-41			23.3	24.5	22914	0.005	0.043	0.0005	5	0.005
BT-01-41			24.5	25.8	22915	0.005	0.014	0.0005	5	0.005
BT-01-41			25.8	26.6	22916	0.005	0.005	0.0005	5	0.005
BT-01-41			26.6	27.65	22917	0.034	0.07	0.023	5	0.005
BT-01-41			27.65	28.6	22918	0.005	0.045	0.003	5	0.005
BT-01-41			58.7	59.7	22919	0.005	0.013	0.003	5	0.005
BT-01-41			59.7	60.4	22920	0.005	0.005	0.0005	5	0.005
BT-01-41			60.4	61.4	22921	0.005	0.011	0.002	5	0.005
BT-01-41			90.7	92	22922	0.01	0.016	0.0005	5	0.005
BT-01-41			92	92.7	22923	0.005	0.005	0.0005	5	0.005
BT-01-41			144	145.3	22924	0.005	0.012	0.001	5	0.005
BT-01-41			145.3	145.9	22925	0.005	0.005	0.012	12	0.005
BT-01-42	632432.54	5256289.46	10	11	22860	0.028	0.005	0.003	5	0.005
BT-01-42			11	12	22861	0.029	0.005	0.001	5	0.005
BT-01-42			12	13	22862	0.005	0.005	0.002	5	0.011
BT-01-42			13	14	22863	0.005	0.005	0.0005	5	0.005
BT-01-42			14	15	22864	0.024	0.005	0.002	5	0.005
BT-01-42			15	16	22865	0.025	0.005	0.007	15	0.011
BT-01-42			68.6	69.1	22866	0.025	0.005	0.006	5	0.005
BT-01-42			98	99	22867	0.017	0.005	0.002	5	0.01
BT-01-42			107	108.5	22868	0.01	0.005	0.002	5	0.005
BT-01-42			116.5	117.5	22869	0.019	0.005	0.001	5	0.005
BT-01-42			117.5	117.8	22870	0.015	0.005	0.0005	5	0.005
BT-01-42			117.8	118.8	22871	0.015	0.005	0.001	5	0.005
BT-01-42			138.9	139.3	22872	0.02	0.115	0.001	5	0.005
BT-01-42			140.7	141.7	22873	0.016	0.021	0.0005	5	0.005
BT-01-42			141.7	142.7	22874	0.017	0.034	0.0005	5	0.01

BT-01-42			142.7	144	22875	0.016	0.032	0.0005	5	0.014
BT-01-42			144	145	22876	0.017	0.029	0.001	5	0.013
BT-01-42			145	146	22877	0.018	0.055	0.0005	5	0.01
BT-01-42			146	147	22878	0.019	0.06	0.001	5	0.005
BT-01-42			151	152.5	22879	0.035	0.02	0.006	5	0.012
BT-01-42			176.1	177.1	22880	0.061	0.038	0.012	18	0.005
BT-01-42			177.1	178.1	22881	0.06	0.036	0.01	5	0.013
BT-01-42			178.1	179.1	22882	0.057	0.024	0.018	12	0.013
BT-01-42			179.1	180.1	22883	0.063	0.066	0.008	5	0.014
BT-01-42			180.1	181.15	22884	0.045	0.014	0.004	15	0.014
BT-01-42			187.4	188.3	22885	0.017	0.005	0.005	5	0.011
BT-01-42			188.3	189	22886	0.027	0.014	0.002	12	0.005
BT-01-42			189	190	22887	0.014	0.005	0.0005	5	0.005
BT-01-42			191	192	22888	0.017	0.019	0.0005	5	0.005
BT-01-42			194.7	195.1	22889	0.018	0.005	0.001	10	0.005
BT-01-43	632525.24	5256263.35	72.7	74	22890	0.029	0.005	0.005	18	0.005
BT-01-43			74	75.2	22891	0.023	0.005	0.003	5	0.005
BT-01-43			84.1	85.6	22892	0.026	0.005	0.004	5	0.012
BT-01-43			140.5	141.4	22893	0.033	0.005	0.002	5	0.01
BT-01-43			141.4	142.3	22894	0.027	0.005	0.006	5	0.012
BT-01-43			146	147	22895	0.026	0.013	0.016	5	0.012
BT-01-43			147	148	22896	0.005	0.01	0.018	5	0.015
BT-01-43			148	149	22897	0.005	0.011	0.006	5	0.005
BT-01-43			149	150	22898	0.005	0.01	0.005	5	0.005
BT-01-47	632628.64	5256308.88	88.1	89.3	22926	0.012	0.019	0.003	5	0.005
BT-01-47			94	95	22927	0.01	0.005	0.006	5	0.005
BT-01-47			95	96.5	22928	0.014	0.005	0.004	5	0.005
BT-01-47			96.5	98	22929	0.01	0.011	0.003	5	0.005
BT-01-47			98	99.5	22930	0.01	0.005	0.005	5	0.005
BT-01-47			99.5	100.5	22931	0.012	0.005	0.01	16	0.005
BT-01-47			100.5	102	22932	0.005	0.005	0.011	18	0.005
BT-01-47			102	103	22933	0.005	0.012	0.006	12	0.005
BT-01-47			126.6	128.1	22934	0.005	0.005	0.008	13	0.005
BT-01-47			128.1	129.6	22935	0.005	0.005	0.017	14	0.005
BT-01-47			129.6	131.1	22936	0.005	0.01	0.007	10	0.005
BT-01-47			131.1	132.6	22937	0.005	0.005	0.005	17	0.005
BT-01-47			134.2	135.7	22938	0.005	0.005	0.007	5	0.005
BT-01-47			135.7	137.2	22939	0.005	0.005	0.008	20	0.005
BT-01-47			137.2	138.7	22940	0.005	0.005	0.009	19	0.005
BT-01-47			138.7	140.2	22941	0.005	0.005	0.012	16	0.005
BT-01-47			140.2	141.2	22942	0.005	0.013	0.01	25	0.005
BT-01-47			141.2	142.2	22943	0.005	0.013	0.011	19	0.005
BT-01-48	632610.81	5256535.87	10.4	11.9	22944	0.005	0.005	0.0005	5	0.005
BT-01-48			11.9	13.4	22945	0.005	0.005	0.0005	5	0.005
BT-01-48			13.4	14.9	22946	0.005	0.005	0.0005	5	0.01
BT-01-48			14.9	16.4	22947	0.005	0.005	0.002	5	0.01
BT-01-48			19	20	22948	0.005	0.01	0.0005	5	0.005

BT-01-48			21.45	22.3	22949	0.005	0.005	0.001	11	0.011
BT-01-48			30.6	32.1	22950	0.005	0.011	0.0005	5	0.01
BT-01-48			37.5	38.3	22951	0.005	0.005	0.0005	5	0.005
BT-01-48			43.4	44	22952	0.005	0.005	0.001	5	0.005
BT-01-48			45.7	46.7	22953	0.005	0.015	0.0005	5	0.005
BT-01-48			60.5	61.8	22954	0.005	0.005	0.001	5	0.005
BT-01-48			61.8	63	22955	0.01	0.005	0.002	5	0.01
BT-01-48			66.1	66.8	22956	0.005	0.005	0.0005	5	0.005
BT-01-48			66.8	67.65	22957	0.005	0.005	0.0005	5	0.005
BT-01-48			67.65	68.2	22958	0.005	0.005	0.0005	5	0.005
BT-01-48			73.5	75	22959	0.005	0.005	0.0005	5	0.005
BT-01-48			75	76.5	22960	0.005	0.005	0.0005	5	0.005
BT-01-48			76.5	78	22961	0.005	0.005	0.0005	5	0.005
BT-01-48			78	79.1	22962	0.017	0.005	0.0005	5	0.005
BT-01-48			86.9	87.9	22963	0.017	0.005	0.0005	5	0.005
BT-01-48			87.9	89	22964	0.017	0.005	0.0005	13	0.005
BT-01-48			95.2	96.2	22965	0.013	0.005	0.0005	5	0.005
BT-01-48			96.2	97.2	22966	0.015	0.005	0.0005	5	0.005
BT-01-48			97.2	98.2	22967	0.014	0.005	0.0005	5	0.005
BT-01-48			98.2	99.25	22968	0.013	0.005	0.0005	5	0.01
BT-01-48			124.1	124.5	22969	0.013	0.013	0.0005	5	0.005
BT-01-49	632609.16	5256050.72	8	9	22822	0.02	0.005	0.005	5	0.005
BT-01-49			17	18	22823	0.02	0.005	0.009	11	0.01
BT-01-49			18	19.1	22824	0.02	0.005	0.006	5	0.01
BT-01-49			48.7	50	22825	0.06	0.04	0.037	13	0.01
BT-01-49			50	51.5	22826	0.06	0.02	0.016	5	0.02
BT-01-49			51.5	53	22827	0.05	0.03	0.025	12	0.01
BT-01-49			53	54.5	22828	0.05	0.02	0.016	5	0.02
BT-01-49			54.5	56	22829	0.05	0.01	0.02	13	0.01
BT-01-49			56	57.5	22830	0.07	0.04	0.038	17	0.01
BT-01-49			57.5	59	22831	0.05	0.02	0.032	22	0.01
BT-01-49			59	60.5	22832	0.07	0.07	0.038	21	0.02
BT-01-49			60.5	62	22833	0.05	0.02	0.024	17	0.01
BT-01-49			62	63.5	22834	0.05	0.03	0.025	5	0.01
BT-01-49			63.5	65	22835	0.05	0.02	0.022	5	0.01
BT-01-49			65	66.5	22836	0.08	0.07	0.039	5	0.01
BT-01-49			66.5	68	22837	0.07	0.05	0.031	5	0.01
BT-01-49			68	69.5	22838	0.06	0.03	0.015	5	0.01
BT-01-49			69.5	71	22839	0.07	0.07	0.024	5	0.01
BT-01-49			71	72	22840	0.07	0.05	0.016	5	0.02
BT-01-49			72	73.5	22841	0.06	0.03	0.026	5	0.02
BT-01-49			73.5	75	22842	0.083	0.066	0.02	15	0.01
BT-01-49			75	76.5	22843	0.07	0.042	0.023	5	0.012
BT-01-49			76.5	77.65	22844	0.074	0.048	0.014	5	0.012
BT-01-49			77.65	78.9	22845	0.005	0.005	0.001	5	0.005
BT-01-49			78.9	80.3	22846	0.068	0.026	0.006	5	0.013
BT-01-49			80.3	81.7	22847	0.068	0.018	0.007	5	0.013

BT-01-49			81.7	82.7	22848	0.031	0.005	0.003	5	0.009
BT-01-49			82.7	83.7	22849	0.01	0.005	0.001	5	0.005
BT-01-49			83.7	84.8	22850	0.017	0.005	0.0005	5	0.005
BT-01-49			84.8	86.3	22851	0.033	0.005	0.001	5	0.005
BT-01-49			97.9	99.4	22852	0.031	0.005	0.003	5	0.011
BT-01-49			102	103	22853	0.037	0.005	0.001	11	0.013
BT-01-49			103	104	22854	0.032	0.018	0.002	5	0.013
BT-01-49			105.8	106.7	22855	0.041	0.017	0.002	5	0.013
BT-01-49			116.6	117.8	22856	0.072	0.005	0.002	5	0.013
BT-01-49			138	139.5	22857	0.07	0.005	0.003	5	0.013
BT-01-49			139.5	140.5	22858	0.068	0.005	0.004	5	0.015
BT-01-49			140.5	141.5	22859	0.07	0.005	0.006	5	0.012
BT-02-51	631509	5258670	77.6	78.6	50201	0.16	0.22	0.164	45	0.02
BT-02-51			78.6	79.6	50202	0.13	0.24	0.159	55	0.02
BT-02-51			79.6	80.6	50203	0.07	0.06	0.076	5	0.02
BT-02-51			80.6	81.6	50204	0.13	0.22	0.118	27	0.02
BT-02-51			81.6	82.6	50205	0.07	0.08	0.066	5	0.02
BT-02-51			82.6	83.6	50206	0.09	0.09	0.081	5	0.02
BT-02-51			83.6	84.6	50207	0.09	0.1	0.088	16	0.02
BT-02-51			84.6	85.6	50208	0.06	0.07	0.069	5	0.01
BT-02-51			85.6	86.3	50209	0.02	0.01	0.012	5	0.01
BT-02-52	631522	5258735	11	12	50210	0.09	0.13	0.06	5	0.02
BT-02-52			12	13	50211	0.13	0.16	0.086	32	0.02
BT-02-52			13	14	50212	0.07	0.09	0.058	16	0.01
BT-02-57	631541	5258694	40.1	40.9	50213	0.005	0.005	0.0005	5	0.005
BT-02-57			40.9	41.9	50214	0.15	0.22	0.161	37	0.02
BT-02-57			41.9	43.1	50215	0.13	0.18	0.085	23	0.01
BT-02-57			43.1	44.1	50216	0.005	0.005	0.0005	5	0.005
BT-02-57			44.1	45.1	50217	0.005	0.005	0.0005	5	0.005
BT-02-57			45.1	46.5	50218	0.08	0.13	0.103	13	0.01
BT-02-57			46.5	47	50219	0.1	1.88	0.442	162	0.05
BT-02-57			47	48.3	50220	0.09	0.08	0.038	5	0.01
BT-02-57			48.3	48.7	50221	1.32	2.38	0.823	155	0.1
BT-02-57			48.7	50.1	50222	0.03	0.05	0.002	5	0.005
BT-02-57			50.1	51.15	50223	0.02	0.03	0.0005	5	0.005
BT-02-58	631683	5258445	16	17	50224	0.03	0.02	0.007	5	0.005
BT-02-58			17	18	50225	0.12	0.22	0.16	48	0.01
BT-02-58			18	19	50226	0.15	0.26	0.192	63	0.02
BT-02-58			19	20	50227	0.04	0.03	0.0005	5	0.005
BT-02-58			20	21	50228	0.07	0.04	0.049	12	0.01
BT-02-58			21	22	50229	0.06	0.05	0.029	5	0.01
BT-02-58			22	23	50230	0.12	0.16	0.18	38	0.01
BT-02-58			23	24	50231	0.09	0.16	0.085	28	0.01
BT-02-58			24	25	50232	0.06	0.07	0.044	16	0.01
BT-02-58			25	26	50233	0.08	0.12	0.07	13	0.01
BT-02-61	632658	5256136	8	9.5	96283	0.008	0.0094	0.016	16	0.0049
BT-02-61			14	15.5	96284	0.007	0.0101	0.011	17	0.0051

BT-02-61			26	27.5	96285	0.0078	0.0121	0.01	11	0.0049
BT-02-61			33.5	35	96286	0.0106	0.0069	0.009	5	0.0049
BT-02-61			39	40.5	96287	0.0108	0.0063	0.009	5	0.0059
BT-02-61			40.5	41.5	96288	0.0104	0.0074	0.009	5	0.0056
BT-02-61			44.5	46	96289	0.0098	0.0057	0.009	5	0.0047
BT-02-61			46	47.1	96290	0.01	0.0167	0.008	5	0.0064
BT-02-61			47.1	48.1	96291	0.011	0.006	0.009	5	0.0038
BT-02-61			48.1	49.6	96292	0.0118	0.0114	0.009	5	0.0055
BT-02-61			49.6	51	96293	0.0148	0.013	0.02	49	0.0057
BT-02-61			51	52.5	96294	0.0102	0.0216	0.008	5	0.0077
BT-02-61			52.5	54	96295	0.011	0.0133	0.008	5	0.0061
BT-02-61			54	55.5	96296	0.012	0.0098	0.009	11	0.0054
BT-02-61			55.5	56.5	96297	0.0114	0.0085	0.009	5	0.0061
BT-02-61			56.5	58	96298	0.0136	0.0071	0.009	5	0.0057
BT-02-61			58	59	96299	0.0126	0.0066	0.01	5	0.0052
BT-02-61			59	59.8	96300	0.0126	0.0053	0.009	5	0.0041
BT-02-61			59.8	61	88001	0.013	0.0084	0.009	14	0.0049
BT-02-61			61	62	88002	0.0136	0.0045	0.01	14	0.0052
BT-02-61			62	63.5	88003	0.0132	0.0237	0.009	14	0.0087
BT-02-61			63.5	65	88004	0.0128	0.0111	0.009	17	0.0056
BT-02-61			65	66.3	88005	0.0162	0.0132	0.009	16	0.0067
BT-02-61			66.3	67.5	88006	0.014	0.0078	0.009	11	0.0066
BT-02-61			67.5	68.6	88007	0.008	0.0013	0.006	5	0.0033
BT-02-61			68.6	70.1	88008	0.0156	0.0046	0.01	15	0.0066
BT-02-61			70.1	71	88009	0.015	0.0035	0.01	14	0.0054
BT-02-61			75.7	77.5	88010	0.0094	0.0055	0.006	11	0.005
BT-02-61			77.5	79	88011	0.0118	0.0059	0.009	14	0.0054
BT-02-61			79	80.5	88012	0.0104	0.0054	0.008	16	0.0045
BT-02-61			80.5	82	88013	0.0114	0.0034	0.009	16	0.0049
BT-02-61			82	83.5	88014	0.0124	0.0066	0.01	12	0.0056
BT-02-61			83.5	85.5	88015	0.0138	0.0054	0.009	14	0.0064
BT-02-61			85.5	86.3	88016	0.0036	0.0001	0.002	5	0.0012
BT-02-61			86.3	87.8	88017	0.0142	0.0061	0.009	13	0.0055
BT-02-61			87.8	89.6	88018	0.015	0.0045	0.01	15	0.0061
BT-02-61			89.6	90.8	88019	0.0032	0.0002	0.003	12	0.0011
BT-02-61			90.8	92.1	88020	0.0118	0.0039	0.01	19	0.0049
BT-02-61			92.1	93.5	88021	0.0032	0.0001	0.0005	5	0.0005
BT-02-61			93.5	95	88022	0.0296	0.0025	0.007	13	0.0067
BT-02-61			95	96.6	88023	0.031	0.0031	0.008	14	0.0072
BT-02-61			96.6	98.2	88024	0.0324	0.008	0.008	15	0.0072
BT-02-61			98.2	99.6	88025	0.0286	0.0026	0.009	17	0.0065
BT-02-61			99.6	100.1	88026	0.0154	0.0001	0.005	11	0.003
BT-02-61			100.1	101.5	88027	0.0312	0.0001	0.008	13	0.0067
BT-02-61			101.5	102.5	88028	0.0128	0.0062	0.01	15	0.0059
BT-02-61			102.5	104	88029	0.0272	0.0044	0.009	14	0.0066
BT-02-61			104	105.8	88030	0.0348	0.0048	0.008	5	0.0075
BT-02-61			105.8	107.5	88031	0.0194	0.0042	0.009	15	0.0058

BT-02-61			107.5	109	88032	0.036	0.021	0.029	14	0.007
BT-02-61			109	110.5	88033	0.0588	0.0211	0.032	18	0.0077
BT-02-61			110.5	112	88034	0.0916	0.033	0.056	20	0.009
BT-02-61			112	113.5	88035	0.14	0.128	0.126	44	0.015
BT-02-61			113.5	115	88036	0.164	0.198	0.128	39	0.015
BT-02-61			115	116.5	88037	0.0938	0.0985	0.083	33	0.0084
BT-02-61			116.5	118	88038	0.146	0.179	0.186	63	0.0111
BT-02-61			118	118.5	88039	0.297	0.403	0.245	88	0.0174
BT-02-61			118.5	119.5	88040	0.154	0.196	0.136	51	0.016
BT-02-61			119.5	120.7	88041	0.196	0.22	0.159	66	0.019
BT-02-61			120.7	121.7	88042	0.192	0.162	0.175	66	0.017
BT-02-61			121.7	123.3	88043	0.014	0.014	0.005	5	0.006
BT-02-61			123.3	124.8	88044	0.289	0.195	0.325	70	0.0179
BT-02-61			124.8	126.3	88045	0.086	0.204	0.108	55	0.01
BT-02-61			126.3	127.5	88046	0.112	0.408	0.117	61	0.011
BT-02-61			127.5	128.5	88047	0.958	1.26	0.944	468	0.053
BT-02-61			128.5	129.5	88048	0.726	6.772	0.765	236	0.039
BT-02-61			129.5	130.5	88049	0.406	0.674	0.468	203	0.036
BT-02-61			130.5	131.5	88050	0.352	0.548	0.399	157	0.031
BT-02-61			131.5	132.5	88051	0.364	0.46	0.432	163	0.027
BT-02-61			132.5	133.5	88052	0.444	0.738	0.563	254	0.033
BT-02-61			133.5	134.5	88053	0.418	0.788	0.347	147	0.025
BT-02-61			134.5	135.5	88054	0.314	0.4	0.316	118	0.022
BT-02-61			135.5	136.5	88055	0.122	0.152	0.162	63	0.012
BT-02-61			136.5	137.5	88056	0.174	0.184	0.188	63	0.016
BT-02-61			137.5	138.5	88057	0.159	0.136	0.132	54	0.0121
BT-02-61			138.5	139.5	88058	0.0768	0.0697	0.06	42	0.0097
BT-02-61			139.5	140.4	88059	0.193	0.265	0.274	139	0.0123
BT-02-61			140.4	141.4	88060	0.0536	0.0831	0.09	45	0.0063
BT-02-61			141.4	142.4	88061	0.0116	0.0102	0.011	5	0.0045
BT-02-61			142.4	143.4	88062	0.0114	0.0073	0.008	5	0.0051
BT-02-61			143.4	145	88063	0.01	0.0052	0.01	5	0.0044
BT-02-61			145	146.5	88064	0.0096	0.0055	0.008	5	0.0048
BT-02-61			146.5	148	88065	0.0108	0.0053	0.01	5	0.0046
BT-02-61			148	149.3	88066	0.0128	0.0068	0.006	5	0.0052
BT-02-61			149.3	150.6	88067	0.013	0.0088	0.007	5	0.0057
BT-02-61			150.6	152	88068	0.011	0.0058	0.009	15	0.0053
BT-02-62	632633	5256156	6.5	8	88373	0.0325	0.0024	0.007	5	0.0051
BT-02-62			8	9.5	88374	0.0293	0.0029	0.008	5	0.0054
BT-02-62			9.5	11	88375	0.0122	0.0027	0.009	5	0.0053
BT-02-62			11	12.5	88376	0.0132	0.0073	0.01	5	0.0046
BT-02-62			12.5	14	88377	0.0128	0.0076	0.009	5	0.0045
BT-02-62			14	15.5	88378	0.0111	0.0085	0.01	5	0.0042
BT-02-62			15.5	17	88379	0.0118	0.0092	0.01	5	0.0045
BT-02-62			17	18.5	88380	0.0107	0.0098	0.008	5	0.0059
BT-02-62			18.5	20	88381	0.0124	0.0087	0.008	5	0.004
BT-02-62			20	21.5	88382	0.0104	0.0095	0.01	5	0.0041

BT-02-62			21.5	23	88383	0.0106	0.0086	0.009	5	0.0034
BT-02-62			23	24.5	88384	0.0104	0.0061	0.012	5	0.0042
BT-02-62			24.5	26	88385	0.0114	0.0103	0.01	11	0.0042
BT-02-62			26	27.5	88386	0.0111	0.0093	0.009	5	0.0042
BT-02-62			27.5	29	88387	0.0114	0.008	0.009	5	0.0041
BT-02-62			29	30.5	88388	0.0125	0.0091	0.01	5	0.0044
BT-02-62			30.5	32	88389	0.0129	0.0084	0.009	5	0.0037
BT-02-62			39	40.5	88390	0.0113	0.0074	0.009	5	0.0036
BT-02-62			40.5	42	88391	0.0105	0.0099	0.009	5	0.0036
BT-02-62			42	43.5	88392	0.0108	0.0171	0.01	11	0.0036
BT-02-62			43.5	45	88393	0.0114	0.0082	0.01	5	0.0034
BT-02-62			45	46.5	88394	0.0111	0.0105	0.008	5	0.0034
BT-02-62			46.5	48	88395	0.0125	0.0099	0.009	5	0.0034
BT-02-62			48	49.5	88396	0.0126	0.0141	0.01	5	0.0034
BT-02-62			49.5	50.7	88397	0.0117	0.0088	0.009	5	0.0032
BT-02-62			50.7	51.8	88398	0.0134	0.0143	0.009	5	0.0039
BT-02-62			51.8	54	88399	0.0106	0.0038	0.008	5	0.0029
BT-02-62			54	55.8	88400	0.0116	0.007	0.008	5	0.0036
BT-02-62			55.8	57.6	88401	0.0107	0.0063	0.009	5	0.0032
BT-02-62			57.6	59	88402	0.0109	0.006	0.01	5	0.0036
BT-02-62			59	60.5	88403	0.0097	0.006	0.009	5	0.0032
BT-02-62			60.5	61.8	88404	0.0111	0.0095	0.009	5	0.0035
BT-02-62			61.8	63.3	88405	0.013	0.01	0.014	5	0.004
BT-02-62			63.3	64.8	88406	0.0121	0.0277	0.01	5	0.0036
BT-02-62			64.8	66.3	88407	0.0099	0.0058	0.01	5	0.0036
BT-02-62			70.9	72.1	88408	0.0156	0.0052	0.01	5	0.0049
BT-02-62			72.1	72.9	88409	0.0067	0.0102	0.01	5	0.0038
BT-02-62			72.9	74	88410	0.0092	0.0077	0.009	5	0.0036
BT-02-62			74	75.5	88411	0.0102	0.009	0.009	5	0.0039
BT-02-62			75.5	77	88412	0.0122	0.0082	0.01	5	0.0035
BT-02-62			77	78.5	88413	0.0123	0.0109	0.009	5	0.0043
BT-02-62			78.5	80	88414	0.0115	0.0055	0.01	5	0.0037
BT-02-62			80	81.5	88415	0.0116	0.0068	0.008	5	0.0033
BT-02-62			81.5	83	88416	0.0099	0.0072	0.01	5	0.0034
BT-02-62			83	84.5	88417	0.011	0.0081	0.008	5	0.0044
BT-02-62			84.5	86	88418	0.0106	0.0096	0.009	5	0.004
BT-02-62			86	87.5	88419	0.011	0.0094	0.008	5	0.0048
BT-02-62			87.5	89	88420	0.0109	0.008	0.01	5	0.0038
BT-02-62			89	90.5	88421	0.0106	0.0069	0.009	5	0.0034
BT-02-62			90.5	92	88422	0.011	0.0079	0.01	5	0.0035
BT-02-62			92	93.5	88423	0.0102	0.008	0.009	5	0.0042
BT-02-62			93.5	95	88424	0.0113	0.0081	0.009	5	0.0038
BT-02-62			95	96	88425	0.011	0.0084	0.01	5	0.004
BT-02-62			96	97	88426	0.0107	0.0073	0.011	5	0.0035
BT-02-62			97	98.5	88427	0.0115	0.0063	0.009	5	0.0034
BT-02-62			98.5	99.7	88428	0.0114	0.0051	0.009	14	0.0036
BT-02-62			99.7	100.1	88429	0.0106	0.0402	0.009	5	0.0071

BT-02-62			100.1	101.1	88430	0.0128	0.0061	0.01	5	0.0037
BT-02-62			101.1	102.5	88431	0.0128	0.0076	0.01	5	0.0039
BT-02-62			102.5	104	88432	0.0108	0.0082	0.011	5	0.004
BT-02-62			104	105.5	88433	0.0101	0.0109	0.009	5	0.004
BT-02-62			105.5	107	88434	0.0115	0.0065	0.01	5	0.0035
BT-02-62			107	108.5	88435	0.0104	0.0278	0.01	5	0.0049
BT-02-62			108.5	110	88436	0.0103	0.007	0.014	13	0.0039
BT-02-62			110	111.5	88437	0.0111	0.008	0.01	5	0.0042
BT-02-62			111.5	112.6	88438	0.0113	0.0099	0.01	5	0.0044
BT-02-62			112.6	113.9	88439	0.0137	0.0103	0.009	5	0.0048
BT-02-62			113.9	115.2	88440	0.0129	0.0098	0.01	5	0.0071
BT-02-62			115.2	117.5	88441	0.0123	0.0069	0.01	5	0.0039
BT-02-62			117.5	119	88442	0.0119	0.0066	0.01	5	0.0037
BT-02-62			119	120.5	88443	0.0103	0.0159	0.017	23	0.0045
BT-02-62			120.5	122	88444	0.0115	0.0077	0.009	5	0.0038
BT-02-62			122	123.9	88445	0.0103	0.0045	0.009	5	0.0035
BT-02-62			123.9	125.7	88446	0.0118	0.0112	0.009	10	0.0044
BT-02-62			125.7	127.4	88447	0.0148	0.0041	0.009	11	0.004
BT-02-62			127.4	129.3	88448	0.0274	0.0114	0.007	5	0.0045
BT-02-62			129.3	131.1	88449	0.0301	0.004	0.008	12	0.0046
BT-02-62			131.1	132.7	88450	0.015	0.0056	0.008	5	0.0038
BT-02-62			132.7	134.3	88451	0.014	0.0112	0.009	15	0.0044
BT-02-62			134.3	135.8	88452	0.0436	0.0052	0.004	11	0.0053
BT-02-62			135.8	136.9	88453	0.0358	0.0183	0.024	13	0.006
BT-02-62			136.9	137.4	88454	0.0111	0.0185	0.004	5	0.003
BT-02-62			137.4	138.5	88455	0.0374	0.0202	0.009	5	0.0047
BT-02-62			138.5	139.6	88456	0.0359	0.0226	0.012	13	0.0048
BT-02-62			139.6	140.2	88457	0.0589	0.0461	0.024	16	0.0054
BT-02-62			140.2	141.5	88458	0.0561	0.0185	0.035	24	0.0066
BT-02-62			141.5	143	88459	0.0409	0.0113	0.015	5	0.0047
BT-02-62			143	144.5	88460	0.0343	0.0205	0.01	14	0.0047
BT-02-62			144.5	146	88461	0.0436	0.0256	0.002	5	0.006
BT-02-62			146	147	88462	0.0422	0.007	0.002	11	0.006
BT-02-62			147	148	88463	0.0318	0.0084	0.0005	5	0.0048
BT-02-62			148	149	88464	0.026	0.0179	0.007	5	0.0043
BT-02-62			149	149.7	88465	0.0041	0.0082	0.001	10	0.0011
BT-02-62			149.7	150.4	88466	0.153	0.34	0.164	54	0.0108
BT-02-62			150.4	151.3	88467	0.0901	0.167	0.157	42	0.0101
BT-02-62			151.3	152.3	88468	0.0705	0.197	0.168	54	0.0124
BT-02-62			152.3	153.3	88469	0.0523	0.199	0.169	51	0.0115
BT-02-62			153.3	154.3	88470	0.109	0.163	0.132	44	0.0097
BT-02-62			154.3	155.3	88471	0.0994	0.186	0.159	53	0.0128
BT-02-62			155.3	156.3	88472	0.0602	0.19	0.165	55	0.0117
BT-02-62			156.3	157.3	88473	0.162	0.282	0.239	79	0.0139
BT-02-62			157.3	158.3	88474	0.0479	0.0232	0.032	11	0.0054
BT-02-62			158.3	159.3	88475	0.127	0.191	0.16	55	0.011
BT-02-62			159.3	160.3	88476	0.0695	0.0932	0.062	22	0.0062

BT-02-62			160.3	161.3	88477	0.036	0.0297	0.026	12	0.0048
BT-02-62			161.3	162.3	88478	0.0692	0.117	0.101	21	0.0075
BT-02-62			162.3	163.3	88479	0.0827	0.0897	0.075	20	0.0077
BT-02-62			163.3	164.3	88480	0.0529	0.0373	0.037	5	0.0055
BT-02-62			164.3	165.5	88481	0.066	0.0825	0.071	13	0.0077
BT-02-62			165.5	166.7	88482	0.0841	0.113	0.091	27	0.0071
BT-02-62			166.7	167.8	88483	0.0547	0.0706	0.062	12	0.0061
BT-02-62			167.8	168.8	88484	0.0355	0.0152	0.018	5	0.0052
BT-02-62			168.8	169.8	88485	0.0353	0.0146	0.009	5	0.0052
BT-02-62			169.8	170.8	88486	0.0364	0.131	0.099	36	0.0065
BT-02-62			170.8	171.8	88487	0.114	0.166	0.235	64	0.0098
BT-02-62			171.8	172.8	88488	0.036	0.0574	0.072	20	0.0049
BT-02-62			172.8	173.8	88489	0.0472	0.0697	0.057	16	0.0075
BT-02-62			173.8	174.8	88490	0.0319	0.0288	0.03	5	0.005
BT-02-62			174.8	175.8	88491	0.0418	0.0183	0.02	5	0.0045
BT-02-62			175.8	176.8	88492	0.0611	0.0791	0.073	28	0.0074
BT-02-62			176.8	177.6	88493	0.127	0.246	0.182	61	0.0136
BT-02-62			177.6	178.6	88494	0.0506	0.0498	0.053	11	0.0069
BT-02-62			178.6	179.6	88495	0.0353	0.029	0.044	17	0.0058
BT-02-62			179.6	180.8	88496	0.0401	0.0345	0.039	11	0.0066
BT-02-62			180.8	182	88497	0.0431	0.038	0.048	19	0.0065
BT-02-63	632605	5256167	14.7	16.1	98903	0.0072	0.0087	0.007	11	0.0041
BT-02-63			34.5	36	98904	0.0111	0.0093	0.009	12	0.0037
BT-02-63			36	36.6	98905	0.0039	0.0041	0.007	5	0.0016
BT-02-63			36.6	37	98906	0.0128	0.434	0.008	5	0.0048
BT-02-63			45	46	98907	0.0079	0.0101	0.008	5	0.0038
BT-02-63			50	50.7	98908	0.0045	0.0017	0.008	5	0.0011
BT-02-63			63.4	63.9	98909	0.0052	0.0057	0.006	5	0.0012
BT-02-63			72	72.6	98910	0.0112	0.0142	0.008	5	0.0035
BT-02-63			73.5	74.6	98911	0.0116	0.0154	0.009	5	0.0043
BT-02-63			74.6	75.1	98912	0.0098	0.117	0.008	5	0.0029
BT-02-63			94.4	95.3	98913	0.0102	0.0435	0.009	5	0.0049
BT-02-63			95.3	96	98914	0.011	0.066	0.008	5	0.0037
BT-02-63			102.5	103.5	98915	0.0082	0.0343	0.01	5	0.0043
BT-02-63			103.5	104.4	98916	0.0085	0.0234	0.009	5	0.0051
BT-02-63			118.5	119	98917	0.011	0.0172	0.006	5	0.0053
BT-02-63			177	178	98918	0.0104	0.0101	0.009	5	0.0033
BT-02-63			178	179	98919	0.0101	0.0103	0.008	5	0.0032
BT-02-63			180.5	182	98920	0.014	0.0159	0.012	5	0.0036
BT-02-63			182	183.5	98921	0.015	0.002	0.01	5	0.0036
BT-02-63			183.5	185	98922	0.0135	0.0221	0.011	11	0.0042
BT-02-63			185	186.5	98923	0.0131	0.0018	0.009	5	0.0046
BT-02-63			186.5	188	98924	0.0169	0.0053	0.011	5	0.0055
BT-02-63			188	189.5	98925	0.0134	0.004	0.007	5	0.004
BT-02-63			189.5	191	98926	0.0145	0.0046	0.009	12	0.0035
BT-02-63			191	192.5	98927	0.0231	0.0049	0.011	5	0.0038
BT-02-63			192.5	194	98928	0.0119	0.0058	0.008	5	0.0034

BT-02-63			194	194.9	98929	0.0054	0.001	0.004	5	0.0017
BT-02-63			194.9	196.1	98930	0.0124	0.0058	0.01	10	0.004
BT-02-63			196.1	197.3	98931	0.0119	0.0046	0.01	15	0.0047
BT-02-63			197.3	199	98932	0.0132	0.0108	0.012	5	0.004
BT-02-63			199	199.7	98933	0.0125	0.0278	0.009	5	0.0044
BT-02-63			199.7	200.1	98934	0.0201	1.06	0.008	5	0.0111
BT-02-63			200.1	201	98935	0.0158	0.0131	0.009	12	0.0044
BT-02-63			201	202	98936	0.034	0.0331	0.027	5	0.0044
BT-02-63			202	203	98937	0.0744	0.113	0.087	25	0.0075
BT-02-63			203	204	98938	0.0821	0.101	0.085	19	0.0092
BT-02-63			204	204.4	98939	0.139	0.117	0.097	33	0.0105
BT-02-63			204.4	204.7	98940	0.0651	0.0044	0.014	5	0.0036
BT-02-63			204.7	205	98941	0.167	0.18	0.157	41	0.0095
BT-02-63			205	205.6	98942	0.041	0.0057	0.032	12	0.0025
BT-02-63			205.6	206.5	98943	0.252	0.524	0.269	79	0.0144
BT-02-63			206.5	207.5	98944	0.0357	0.0326	0.025	5	0.004
BT-02-63			207.5	208	98945	0.0329	0.0402	0.021	5	0.0034
BT-02-63			208	209	98946	0.0551	0.1	0.031	5	0.0072
BT-02-63			209	210	98947	0.109	0.17	0.103	37	0.0096
BT-02-63			210	210.95	98948	0.0888	0.0836	0.072	23	0.008
BT-02-63			210.95	211.1	98949	0.0566	0.0523	0.061	16	0.0027
BT-02-63			211.1	212	98950	0.644	2.87	0.585	192	0.0202
BT-02-63			212	213	98951	0.288	0.564	0.24	98	0.0163
BT-02-63			213	214	98952	0.016	0.0134	0.014	5	0.0019
BT-02-63			215	216	98953	0.228	0.649	0.339	150	0.0241
BT-02-63			216	217	98954	0.36	0.591	0.499	168	0.0201
BT-02-63			217	218	98955	0.123	0.245	0.109	50	0.0077
BT-02-63			218	219	98956	0.0394	0.0248	0.067	37	0.0046
BT-02-63			219	220	98957	0.0526	0.009	0.025	13	0.0063
BT-02-63			220	221	98958	0.0168	0.011	0.011	14	0.0035
BT-02-63			221	222	98959	0.0151	0.0039	0.012	11	0.0033
BT-02-63			222	222.8	98960	0.0104	0.0043	0.006	5	0.0046
BT-02-63			222.8	224	98961	0.0102	0.002	0.009	5	0.0037
BT-02-63			224	225	98962	0.009	0.0064	0.01	5	0.0038
BT-02-64	632436	5256211	37.2	38.6	88298	0.0083	0.0047	0.009	13	0.0042
BT-02-64			38.6	39.2	88299	0.0059	0.0011	0.007	5	0.0032
BT-02-64			39.2	40.7	88300	0.0048	0.0092	0.008	5	0.0033
BT-02-64			57.9	58.9	88301	0.0073	0.0071	0.008	5	0.0032
BT-02-64			63.5	65.1	88302	0.0054	0.0091	0.009	5	0.0031
BT-02-64			65.1	66.5	88303	0.0245	0.0049	0.004	5	0.0041
BT-02-64			66.5	68	88304	0.0214	0.0088	0.005	5	0.0039
BT-02-64			70.5	72	88305	0.007	0.0092	0.008	11	0.003
BT-02-64			72	73	88306	0.0152	0.0234	0.006	5	0.0039
BT-02-64			73	74.5	88307	0.0072	0.0071	0.009	5	0.0034
BT-02-64			74.5	76	88308	0.0074	0.0091	0.01	5	0.0036
BT-02-64			76	77.5	88309	0.0067	0.0104	0.008	5	0.0033
BT-02-64			77.5	79	88310	0.0071	0.0122	0.009	5	0.0032

BT-02-64			79	80.5	88311	0.0053	0.007	0.009	5	0.0027
BT-02-64			80.5	82.2	88312	0.0052	0.0093	0.009	14	0.0029
BT-02-64			82.2	83.8	88313	0.0207	0.0057	0.002	5	0.0041
BT-02-64			83.8	84.8	88314	0.0205	0.0252	0.004	5	0.005
BT-02-64			84.8	85.8	88315	0.0066	0.0101	0.008	10	0.0035
BT-02-64			85.8	87	88316	0.0052	0.0077	0.009	15	0.0028
BT-02-64			87	88.4	88317	0.0063	0.0087	0.008	5	0.0028
BT-02-64			88.4	90	88318	0.0112	0.0075	0.0005	5	0.0032
BT-02-64			90	91.5	88319	0.0189	0.0075	0.0005	5	0.0038
BT-02-64			91.5	93	88320	0.0176	0.0041	0.0005	11	0.0034
BT-02-64			93	94.5	88321	0.0266	0.0107	0.0005	13	0.0043
BT-02-64			94.5	96	88322	0.0277	0.0014	0.0005	13	0.0045
BT-02-64			96	97.5	88323	0.0279	0.0072	0.0005	10	0.0045
BT-02-64			97.5	99	88324	0.0241	0.0072	0.0005	5	0.0037
BT-02-64			99	100.5	88325	0.0184	0.0066	0.0005	5	0.0037
BT-02-64			100.5	102	88326	0.0225	0.0088	0.0005	5	0.0041
BT-02-64			102	103.5	88327	0.0221	0.0076	0.004	5	0.0043
BT-02-64			103.5	105	88328	0.0248	0.0047	0.0005	5	0.0045
BT-02-64			105	106.5	88329	0.0439	0.0199	0.0005	5	0.0085
BT-02-64			106.5	108	88330	0.0382	0.0179	0.0005	5	0.0062
BT-02-64			108	109	88331	0.0397	0.0068	0.0005	5	0.0058
BT-02-64			109	110	88332	0.0354	0.0445	0.025	14	0.0043
BT-02-64			110	111	88333	0.0265	0.0159	0.007	5	0.0059
BT-02-64			111	112.1	88334	0.136	0.163	0.14	40	0.0084
BT-02-64			112.1	113.3	88335	0.115	0.131	0.125	39	0.0085
BT-02-64			113.3	114.4	88336	0.0699	0.0274	0.034	17	0.0075
BT-02-64			114.4	115.1	88337	0.0756	0.117	0.057	31	0.0145
BT-02-64			115.1	115.9	88338	0.0716	0.0547	0.047	5	0.0066
BT-02-64			115.9	116.7	88339	0.0765	0.0597	0.062	13	0.0065
BT-02-64			116.7	117.9	88340	0.0031	0.0096	0.0005	5	0.001
BT-02-64			117.9	119	88341	0.0099	0.0184	0.0005	5	0.0036
BT-02-64			119	120	88342	0.0975	0.0873	0.082	16	0.0082
BT-02-64			120	121.4	88343	0.106	0.0958	0.0005	5	0.0094
BT-02-64			121.4	122.8	88344	0.016	0.0068	0.071	11	0.0015
BT-02-64			122.8	124	88345	0.108	0.0679	0.108	22	0.0091
BT-02-64			124	125	88346	0.0982	0.114	0.087	16	0.0088
BT-02-64			125	126	88347	0.0828	0.116	0.029	5	0.0111
BT-02-64			126	127	88348	0.0503	0.0137	0.009	5	0.007
BT-02-64			127	128	88349	0.0468	0.0104	0.138	38	0.0053
BT-02-64			128	129	88350	0.121	0.166	0.09	17	0.0098
BT-02-64			129	130	88351	0.0648	0.0279	0.049	5	0.0068
BT-02-64			130	131	88352	0.0535	0.0186	0.023	5	0.0061
BT-02-64			131	132	88353	0.0558	0.0167	0.019	5	0.0065
BT-02-64			132	133	88354	0.054	0.025	0.019	5	0.0068
BT-02-64			133	134	88355	0.0032	0.0049	0.0005	5	0.0011
BT-02-64			134	135.5	88356	0.0013	0.0008	0.0005	5	0.0005
BT-02-64			135.5	136.5	88357	0.0105	0.0145	0.008	5	0.0009

BT-02-64			136.5	136.7	88358	1.4	1.66	0.925	206	0.0536
BT-02-64			136.7	137.3	88359	0.0632	0.0073	0.021	5	0.004
BT-02-64			137.3	138.2	88360	0.0553	0.0224	0.028	5	0.0054
BT-02-64			138.2	139.2	88361	0.0516	0.025	0.02	5	0.0054
BT-02-64			139.2	140.2	88362	0.0549	0.0208	0.024	5	0.0055
BT-02-64			140.2	141.2	88363	0.0497	0.008	0.015	5	0.0056
BT-02-64			141.2	142.2	88364	0.0531	0.0128	0.027	5	0.0057
BT-02-64			142.2	143.2	88365	0.055	0.0189	0.022	5	0.0064
BT-02-64			143.2	144.2	88366	0.0568	0.0425	0.033	5	0.0069
BT-02-64			144.2	145.4	88367	0.0558	0.0394	0.038	5	0.0069
BT-02-64			145.4	146.4	88368	0.0591	0.0394	0.032	5	0.0072
BT-02-64			146.4	147.4	88369	0.057	0.0269	0.029	5	0.0068
BT-02-64			147.4	148.4	88370	0.0695	0.0777	0.054	5	0.0065
BT-02-64			148.4	149.3	88371	0.0019	0.0015	0.0005	5	0.0006
BT-02-64			149.3	150	88372	0.0418	0.0346	0.033	5	0.005
BT-02-65	632328	5256198	7	8.7	88234	0.0085	0.0186	0.015	5	0.0032
BT-02-65			8.7	10.2	88235	0.011	0.0248	0.012	12	0.004
BT-02-65			10.2	10.7	88236	0.0361	0.203	0.042	13	0.0078
BT-02-65			10.7	11.8	88237	0.0533	0.279	0.073	25	0.0067
BT-02-65			11.8	13.3	88238	0.018	0.0289	0.032	5	0.0038
BT-02-65			18.5	20	88239	0.0337	0.0492	0.049	5	0.0039
BT-02-65			20	21.2	88240	0.0715	0.0809	0.109	18	0.0059
BT-02-65			21.2	22.6	88241	0.0381	0.0092	0.023	5	0.0047
BT-02-65			22.6	23.7	88242	0.0533	0.0509	0.067	19	0.005
BT-02-65			23.7	25.2	88243	0.0123	0.0093	0.005	5	0.0027
BT-02-65			25.2	26.7	88244	0.0215	0.0218	0.003	5	0.0033
BT-02-65			26.7	27.5	88245	0.0483	0.0638	0.073	17	0.0042
BT-02-65			27.5	29.3	88246	0.0239	0.0157	0.014	5	0.0039
BT-02-65			29.3	30.8	88247	0.025	0.0094	0.009	5	0.004
BT-02-65			30.8	32	88248	0.0426	0.034	0.121	46	0.0043
BT-02-65			32	32.8	88249	0.0706	0.0876	0.119	37	0.0073
BT-02-65			32.8	33.8	88250	0.0164	0.0156	0.012	5	0.0031
BT-02-65			48.7	50.3	88251	0.0426	0.0359	0.008	5	0.0056
BT-02-65			50.3	51.8	88252	0.0277	0.0119	0.005	5	0.0045
BT-02-65			51.8	53.4	88253	0.0016	0.0012	0.0005	5	0.0008
BT-02-65			53.4	54.9	88254	0.0299	0.0052	0.0005	5	0.005
BT-02-65			54.9	56.3	88255	0.0315	0.0145	0.0005	5	0.0047
BT-02-65			56.3	57.8	88256	0.0011	0.0012	0.0005	5	0.0007
BT-02-65			57.8	59.3	88257	0.0209	0.0084	0.0005	5	0.0038
BT-02-65			59.3	60.4	88258	0.0226	0.012	0.0005	5	0.0037
BT-02-65			60.4	61.1	88259	0.0179	0.0118	0.0005	5	0.0043
BT-02-65			61.1	62.6	88260	0.0126	0.007	0.0005	5	0.0034
BT-02-65			62.6	64.1	88261	0.0184	0.0074	0.0005	5	0.0046
BT-02-65			64.1	65.6	88262	0.0248	0.0123	0.003	5	0.0042
BT-02-65			65.6	67	88263	0.0197	0.0156	0.003	5	0.0036
BT-02-65			67	68.5	88264	0.0205	0.028	0.017	5	0.0033
BT-02-65			68.5	69.4	88265	0.0494	0.0732	0.062	13	0.0052

BT-02-65			69.4	70.9	88266	0.011	0.0129	0.02	5	0.0037
BT-02-65			73.5	74.5	88267	0.01	0.0319	0.033	5	0.0038
BT-02-65			88.5	90.1	88268	0.0073	0.0061	0.008	5	0.0032
BT-02-65			90.1	91.5	88269	0.0199	0.0011	0.005	5	0.0038
BT-02-65			121	122.5	88270	0.0068	0.0093	0.01	5	0.0043
BT-02-65			122.5	124	88271	0.0054	0.0173	0.009	5	0.0027
BT-02-65			128	129.6	88272	0.0044	0.01	0.01	5	0.003
BT-02-65			129.6	130.7	88273	0.0048	0.0071	0.009	5	0.0035
BT-02-65			130.7	132.1	88274	0.0049	0.0033	0.002	5	0.0018
BT-02-65			132.1	133.5	88275	0.0056	0.0091	0.009	5	0.0033
BT-02-65			133.5	135	88276	0.0044	0.0085	0.009	5	0.0031
BT-02-65			135	136.5	88277	0.0043	0.0058	0.008	5	0.003
BT-02-65			136.5	138	88278	0.0055	0.0084	0.008	5	0.0031
BT-02-65			138	139.5	88279	0.0071	0.008	0.008	5	0.0031
BT-02-65			139.5	141	88280	0.0175	0.0035	0.006	5	0.0066
BT-02-65			141	142.5	88281	0.0224	0.0042	0.006	5	0.0078
BT-02-65			142.5	144	88282	0.0253	0.0101	0.008	5	0.0075
BT-02-65			144	145.5	88283	0.0204	0.0041	0.009	5	0.0046
BT-02-65			145.5	147	88284	0.0185	0.0086	0.009	5	0.0051
BT-02-65			147	148	88285	0.0174	0.0062	0.009	11	0.0048
BT-02-65			148	149.1	88286	0.0085	0.0038	0.008	5	0.0042
BT-02-65			149.1	150.4	88287	0.0014	0.0034	0.0005	5	0.0006
BT-02-65			150.4	150.8	88288	0.0016	0.0035	0.0005	5	0.0064
BT-02-65			150.8	152.3	88289	0.0025	0.0039	0.002	5	0.0012
BT-02-65			152.3	153.5	88290	0.0077	0.0068	0.009	5	0.0028
BT-02-65			167	168.2	88291	0.0115	0.0073	0.01	12	0.0037
BT-02-65			168.2	169.5	88292	0.0013	0.0038	0.0005	5	0.0008
BT-02-65			169.5	170.3	88293	0.0091	0.0061	0.0005	5	0.0039
BT-02-65			170.3	171.2	88294	0.0067	0.0039	0.004	5	0.003
BT-02-65			171.2	172.7	88295	0.0089	0.0076	0.003	5	0.0036
BT-02-65			177.7	178.9	88296	0.0063	0.0068	0.002	5	0.003
BT-02-65			178.9	180.5	88297	0.0088	0.0048	0.009	14	0.0032
BT-02-66	632216	5256251	21.3	22.8	88150	0.03	0.0042	0.002	5	0.0061
BT-02-66			22.8	24	88151	0.014	0.0049	0.002	5	0.0025
BT-02-66			24	25.7	88152	0.0314	0.0052	0.0005	5	0.0078
BT-02-66			25.7	26.4	88153	0.0094	0.0033	0.0005	5	0.0016
BT-02-66			26.4	28	88154	0.0334	0.0019	0.0005	5	0.0065
BT-02-66			35	36.5	88155	0.0334	0.004	0.0005	5	0.0073
BT-02-66			41.5	43	88156	0.0352	0.0049	0.0005	5	0.0075
BT-02-66			45	46.5	88157	0.0336	0.0094	0.0005	5	0.007
BT-02-66			46.5	47.5	88158	0.023	0.0139	0.0005	5	0.0068
BT-02-66			47.5	48.5	88159	0.0292	0.0041	0.0005	5	0.0075
BT-02-66			48.5	49.5	88160	0.0294	0.0049	0.0005	5	0.0075
BT-02-66			49.5	51	88161	0.025	0.0057	0.0005	5	0.0071
BT-02-66			56.3	57.8	88162	0.0184	0.0107	0.002	5	0.0043
BT-02-66			57.8	58.7	88163	0.0968	0.205	0.177	47	0.0108
BT-02-66			58.7	60.3	88164	0.0136	0.01	0.002	5	0.0044

BT-02-66			60.3	62	88165	0.015	0.0055	0.002	5	0.0043
BT-02-66			62	63.5	88166	0.014	0.0131	0.002	5	0.0046
BT-02-66			63.5	64.5	88167	0.121	0.16	0.226	62	0.0083
BT-02-66			64.5	65.5	88168	0.056	0.0698	0.128	31	0.0054
BT-02-66			65.5	66.5	88169	0.169	0.182	0.242	48	0.0102
BT-02-66			66.5	68	88170	0.0644	0.0334	0.045	10	0.0079
BT-02-66			68	69.5	88171	0.0458	0.0143	0.021	5	0.0075
BT-02-66			69.5	71	88172	0.043	0.0233	0.026	5	0.0074
BT-02-66			71	72.5	88173	0.0542	0.0044	0.002	5	0.0088
BT-02-66			72.5	74	88174	0.047	0.0024	0.0005	5	0.0077
BT-02-66			74	75.5	88175	0.0434	0.0038	0.0005	5	0.0073
BT-02-66			75.5	77	88176	0.0448	0.005	0.0005	5	0.0074
BT-02-66			82.5	83	88177	0.0318	0.0264	0.008	5	0.005
BT-02-66			83	84.5	88178	0.0238	0.0272	0.017	16	0.0052
BT-02-66			84.5	86	88179	0.027	0.0397	0.021	14	0.0056
BT-02-66			86	86.8	88180	0.0318	0.0081	0.002	5	0.0045
BT-02-66			86.8	88.3	88181	0.0264	0.0229	0.007	5	0.0063
BT-02-66			95	96.5	88182	0.0302	0.0095	0.015	5	0.0059
BT-02-66			102	103.5	88183	0.033	0.0071	0.001	5	0.006
BT-02-66			103.5	105	88184	0.0324	0.0124	0.006	5	0.0065
BT-02-66			110	111.5	88185	0.045	0.0056	0.0005	5	0.0071
BT-02-66			111.5	113	88186	0.034	0.0099	0.002	5	0.0057
BT-02-66			113	114.1	88187	0.0312	0.0066	0.0005	5	0.0053
BT-02-66			114.1	114.8	88188	0.0424	0.0052	0.0005	5	0.0068
BT-02-66			114.8	116	88189	0.0214	0.0076	0.002	5	0.0046
BT-02-66			116	117.5	88190	0.0216	0.0067	0.0005	5	0.0047
BT-02-66			117.5	119	88191	0.0214	0.0067	0.0005	5	0.0048
BT-02-66			119	120.5	88192	0.0218	0.0082	0.002	5	0.0049
BT-02-66			120.5	121.5	88193	0.0224	0.0065	0.0005	5	0.0053
BT-02-66			121.5	122.5	88194	0.0292	0.0148	0.017	14	0.0052
BT-02-66			122.5	123.5	88195	0.0994	0.0976	0.109	29	0.0117
BT-02-66			123.5	124.4	88196	0.0232	0.0106	0.003	5	0.0055
BT-02-66			124.4	125.1	88197	0.0048	0.0019	0.003	5	0.0023
BT-02-66			125.1	126.2	88198	0.019	0.007	0.002	5	0.0048
BT-02-66			126.2	127.2	88199	0.0178	0.009	0.0005	5	0.0048
BT-02-66			127.2	128.2	88200	0.034	0.0094	0.0005	5	0.0071
BT-02-66			128.2	128.7	88201	0.0836	0.078	0.005	5	0.0101
BT-02-66			128.7	129.8	88202	0.0242	0.0137	0.002	5	0.0045
BT-02-66			129.8	130.8	88203	0.0266	0.0115	0.0005	5	0.0046
BT-02-66			130.8	131.8	88204	0.0216	0.017	0.004	5	0.0041
BT-02-66			131.8	132.8	88205	0.0298	0.0333	0.024	14	0.0045
BT-02-66			132.8	133.8	88206	0.105	0.0808	0.093	21	0.0093
BT-02-66			133.8	134.8	88207	0.117	0.131	0.117	27	0.0104
BT-02-66			134.8	135.8	88208	0.138	0.179	0.138	31	0.0116
BT-02-66			135.8	136.8	88209	0.106	0.113	0.091	15	0.009
BT-02-66			136.8	137.8	88210	0.213	0.28	0.213	54	0.0138
BT-02-66			137.8	138.8	88211	0.213	0.281	0.257	62	0.0132

BT-02-66			138.8	139.8	88212	0.184	0.283	0.184	55	0.0117
BT-02-66			139.8	140.8	88213	0.275	0.21	0.354	86	0.0172
BT-02-66			140.8	141.8	88214	0.269	0.364	0.343	89	0.0175
BT-02-66			141.8	142.7	88215	0.199	0.408	0.287	66	0.0139
BT-02-66			142.7	143.6	88216	0.347	0.277	0.475	133	0.0246
BT-02-66			143.6	144.6	88217	0.101	0.106	0.104	21	0.0077
BT-02-66			144.6	145.6	88218	0.16	0.204	0.183	44	0.0108
BT-02-66			145.6	146.4	88219	0.0628	0.0666	0.064	16	0.0066
BT-02-66			146.4	147.4	88220	0.0086	0.0145	0.015	5	0.003
BT-02-66			147.4	148.9	88221	0.005	0.0113	0.012	5	0.0031
BT-02-66			151	152.2	88222	0.0048	0.0041	0.004	5	0.0019
BT-02-66			152.2	153.7	88223	0.0082	0.0079	0.01	11	0.0036
BT-02-66			156.7	158.2	88224	0.0042	0.01	0.011	5	0.0037
BT-02-66			158.2	159	88225	0.0094	0.0066	0.01	12	0.0045
BT-02-66			159	160.3	88226	0.0054	0.0113	0.011	12	0.0037
BT-02-66			160.3	161.8	88227	0.0046	0.0086	0.011	11	0.0032
BT-02-66			164.7	166.2	88228	0.0054	0.0092	0.013	14	0.0047
BT-02-66			166.2	167.5	88229	0.0056	0.0089	0.011	13	0.005
BT-02-66			173	174.5	88230	0.0112	0.0082	0.01	11	0.0056
BT-02-66			174.5	176.3	88231	0.0068	0.0073	0.009	5	0.0043
BT-02-66			176.3	177.8	88232	0.0062	0.0072	0.011	13	0.0042
BT-02-66			177.8	179.3	88233	0.0308	0.0082	0.011	5	0.004
BT-02-67	631520	5258500	48	49.5	98790	0.0145	0.0036	0.009	5	0.0059
BT-02-67			54.5	56	98791	0.0098	0.0027	0.008	5	0.0051
BT-02-67			61	62.5	98792	0.011	0.003	0.008	5	0.0052
BT-02-67			67.5	69	98793	0.004	0.003	0.006	5	0.0038
BT-02-67			74	75.5	98794	0.005	0.0027	0.009	5	0.0052
BT-02-67			80.5	81.6	98795	0.0058	0.0034	0.007	5	0.0058
BT-02-67			92	93.5	98796	0.0067	0.0026	0.008	5	0.0056
BT-02-67			98.5	100	98797	0.0117	0.0028	0.007	5	0.0049
BT-02-67			105	106.5	98798	0.0119	0.0028	0.005	5	0.0052
BT-02-67			111.5	113	98799	0.0084	0.0032	0.005	5	0.0066
BT-02-67			118	119.5	98800	0.0093	0.0034	0.006	5	0.0077
BT-02-67			125.4	126.6	98801	0.0084	0.0035	0.006	5	0.0073
BT-02-67			129.5	131	98802	0.0117	0.0035	0.005	5	0.0079
BT-02-67			136	137.5	98803	0.008	0.0036	0.004	5	0.0078
BT-02-67			142.5	144	98804	0.0072	0.0048	0.002	5	0.0126
BT-02-67			149	150.5	98805	0.0074	0.0053	0.002	5	0.0152
BT-02-67			155.5	157	98806	0.0038	0.004	0.002	5	0.013
BT-02-67			162	163.5	98807	0.0076	0.0044	0.002	5	0.013
BT-02-67			168.5	170	98808	0.0079	0.0047	0.0005	5	0.0151
BT-02-67			175	176.5	98809	0.0063	0.0036	0.0005	5	0.0088
BT-02-67			181.5	183	98810	0.0083	0.0049	0.0005	5	0.0144
BT-02-67			189.7	191.2	98811	0.0072	0.0045	0.0005	5	0.0157
BT-02-67			191.2	192.7	98812	0.0068	0.0059	0.0005	5	0.021
BT-02-67			192.7	193.9	98813	0.0083	0.0044	0.0005	5	0.0143
BT-02-67			198	199	98814	0.009	0.0037	0.002	5	0.0147

BT-02-67			204	205.5	98815	0.0071	0.0041	0.003	5	0.0178
BT-02-67			210.5	212	98816	0.0186	0.0044	0.003	5	0.021
BT-02-67			217	218.5	98817	0.008	0.0041	0.003	5	0.0201
BT-02-67			225	226.5	98818	0.0095	0.0046	0.007	5	0.0192
BT-02-67			226.5	228	98819	0.0067	0.0043	0.004	5	0.0213
BT-02-67			228	229.5	98820	0.0093	0.0046	0.004	5	0.0206
BT-02-67			229.5	231	98821	0.0093	0.0039	0.002	5	0.0195
BT-02-67			231	232.5	98822	0.0291	0.0041	0.004	5	0.0213
BT-02-67			232.5	234	98823	0.0501	0.005	0.003	5	0.0382
BT-02-67			234	235.5	98824	0.0549	0.0042	0.006	5	0.0329
BT-02-67			235.5	237	98825	0.125	0.0063	0.036	14	0.0602
BT-02-67			237	238.5	98826	0.102	0.0042	0.051	14	0.0516
BT-02-67			238.5	240	98827	0.167	0.0066	0.05	13	0.0828
BT-02-67			240	241.5	98828	0.0951	0.0043	0.089	29	0.0815
BT-02-67			241.5	243	98829	0.185	0.007	0.086	31	0.0766
BT-02-67			243	244	98830	0.0874	0.0053	0.136	40	0.0448
BT-02-67			244	245	98831	0.013	0.0036	0.057	24	0.011
BT-02-67			245	246	98832	0.0176	0.0021	0.106	36	0.0048
BT-02-67			246	247	98833	0.0142	0.0037	0.068	23	0.0085
BT-02-67			247	248.5	98834	0.0123	0.0014	0.013	5	0.0022
BT-02-67			248.5	249.4	98835	0.0079	0.0007	0.003	5	0.0014
BT-02-67			249.4	250.3	98836	0.0018	0.0007	0.005	5	0.0012
BT-02-67			250.3	251.5	98837	0.0351	0.0005	0.003	5	0.001
BT-02-67			251.5	252.5	98838	0.0012	0.0009	0.0005	5	0.0009
BT-02-67			267	268	98839	0.0009	0.0006	0.0005	5	0.002
BT-02-67			277	278	98840	0.0377	0.0025	0.0005	5	0.0101
BT-02-67			283	284.5	98841	0.0067	0.0018	0.0005	5	0.0066
BT-02-67			288	289	98842	0.005	0.0013	0.0005	5	0.0011
BT-02-68	632691	5256192	6	7.3	88085	0.0128	0.0054	0.012	15	0.0059
BT-02-68			7.3	8.5	88086	0.033	0.0069	0.008	10	0.0066
BT-02-68			10.4	11.9	88087	0.0361	0.0063	0.014	21	0.0063
BT-02-68			11.9	12.7	88088	0.0185	0.0081	0.002	14	0.0066
BT-02-68			12.7	13.5	88089	0.0321	0.0021	0.011	17	0.0062
BT-02-68			13.5	14.1	88090	0.0151	0.0148	0.002	5	0.0049
BT-02-68			25.5	27	88091	0.0086	0.0075	0.012	15	0.0046
BT-02-68			27	28.5	88092	0.0033	0.0165	0.022	31	0.004
BT-02-68			45.5	47	88093	0.009	0.011	0.014	19	0.0064
BT-02-68			47	48.5	88094	0.0084	0.0089	0.011	23	0.0057
BT-02-68			60.5	62	88095	0.0165	0.014	0.013	17	0.0069
BT-02-68			62	63.5	88096	0.0089	0.0058	0.012	23	0.0055
BT-02-68			80	81	88097	0.004	0.0138	0.034	37	0.0059
BT-02-68			84.5	86	88098	0.0025	0.0163	0.003	29	0.0067
BT-02-68			105.5	106.8	88099	0.0218	0.0041	0.01	17	0.0071
BT-02-68			106.8	108.3	88100	0.0179	0.0081	0.004	16	0.0056
BT-02-68			114.5	116	88101	0.0228	0.003	0.004	14	0.0064
BT-02-68			172	173.5	88102	0.0195	0.0078	0.013	15	0.0067
BT-02-68			173.5	174.7	88103	0.0262	0.0067	0.009	24	0.0079

BT-02-68			174.7	176.2	88104	0.0226	0.0063	0.011	21	0.0068
BT-02-68			179.8	180.5	88105	0.0081	0.0231	0.009	18	0.0055
BT-02-68			187.5	189	88106	0.0082	0.0056	0.014	29	0.0054
BT-02-68			189	189.5	88107	0.0081	0.154	0.011	24	0.0051
BT-02-68			189.5	191	88108	0.0077	0.0098	0.01	23	0.0054
BT-02-68			191	192	88109	0.0111	0.0361	0.013	26	0.0064
BT-02-68			192	193.5	88110	0.0113	0.0157	0.017	30	0.0076
BT-02-68			193.5	195	88111	0.0099	0.0047	0.013	13	0.006
BT-02-68			195	196.5	88112	0.0147	0.0095	0.014	14	0.0066
BT-02-68			196.5	198	88113	0.0112	0.0066	0.013	14	0.0068
BT-02-68			198	199.5	88114	0.0099	0.0062	0.014	15	0.0063
BT-02-68			199.5	200.5	88115	0.113	0.188	0.079	17	0.0124
BT-02-68			200.5	201.5	88116	0.0556	0.0494	0.043	12	0.0082
BT-02-68			201.5	202.5	88117	0.0644	0.0495	0.067	18	0.0076
BT-02-68			202.5	203.3	88118	0.0568	0.174	0.094	25	0.0053
BT-02-68			203.3	204.2	88119	0.0912	0.0822	0.163	42	0.0106
BT-02-68			204.2	205.2	88120	0.0758	0.068	0.154	36	0.0086
BT-02-68			205.2	205.5	88121	0.004	0.0047	0.0005	5	0.002
BT-02-68			205.5	206.2	88122	0.133	0.165	0.266	78	0.0114
BT-02-68			206.2	207.1	88123	0.12	0.204	0.413	120	0.0157
BT-02-68			207.1	208.1	88124	0.109	0.194	0.335	104	0.0152
BT-02-68			208.1	209.6	88125	0.0076	0.0076	0.0005	5	0.0039
BT-02-68			209.6	210.2	88126	0.244	0.696	1.78	475	0.0252
BT-02-68			210.2	211.4	88127	0.0022	0.0242	0.06	12	0.0036
BT-02-68			211.4	212.4	88128	0.233	1.62	1.3	538	0.0277
BT-02-68			212.4	213.4	88129	0.438	1.72	0.835	395	0.0337
BT-02-68			213.4	214.4	88130	0.218	0.492	0.722	292	0.0215
BT-02-68			214.4	215.4	88131	0.0223	0.0268	0.031	21	0.0067
BT-02-68			215.4	216.8	88132	0.0308	0.0422	0.077	41	0.0071
BT-02-68			216.8	217.3	88133	0.0353	0.0052	0.018	11	0.006
BT-02-68			217.3	218.6	88134	0.0324	0.0062	0.014	5	0.008
BT-02-68			218.6	220.1	88135	0.0394	0.0074	0.026	15	0.0083
BT-02-68			220.1	221.4	88136	0.0241	0.0083	0.02	17	0.0072
BT-02-68			221.4	222.9	88137	0.0154	0.0044	0.016	17	0.0067
BT-02-68			222.9	224.1	88138	0.0428	0.0043	0.008	11	0.0079
BT-02-68			224.1	225.1	88139	0.0155	0.0112	0.0005	5	0.0044
BT-02-68			225.1	226.1	88140	0.0093	0.0289	0.015	17	0.0068
BT-02-68			226.1	227	88141	0.0442	0.0064	0.007	11	0.0076
BT-02-68			227	228.1	88142	0.002	0.0035	0.0005	5	0.0018
BT-02-68			228.1	228.6	88143	0.006	0.0339	0.016	20	0.0072
BT-02-68			228.6	230.2	88144	0.0097	0.0023	0.0005	5	0.0029
BT-02-68			230.2	231.5	88145	0.0336	0.0044	0.004	5	0.0058
BT-02-68			231.5	233	88146	0.0298	0.0022	0.007	5	0.008
BT-02-68			241.5	243	88147	0.0131	0.0058	0.012	16	0.0055
BT-02-68			243	244.5	88148	0.0223	0.0069	0.009	15	0.0067
BT-02-68			244.5	246	88149	0.0204	0.0064	0.011	16	0.0065
BT-02-69	631520	5258500	18	19.5	98751	0.006	0.011	0.0005	11	0.0045

BT-02-69			24.5	26	98752	0.0053	0.0121	0.001	12	0.0041
BT-02-69			31	32.5	98753	0.006	0.0088	0.0005	20	0.0042
BT-02-69			37.5	39	98754	0.0058	0.01	0.012	5	0.0041
BT-02-69			44	45.5	98755	0.0062	0.0103	0.011	5	0.0042
BT-02-69			50.5	52	98756	0.007	0.0072	0.012	5	0.0044
BT-02-69			57	58.5	98757	0.0064	0.0053	0.012	12	0.0037
BT-02-69			63.5	65	98758	0.0067	0.0095	0.011	12	0.0042
BT-02-69			70	71.5	98759	0.0076	0.0074	0.011	12	0.004
BT-02-69			76.7	77.6	98760	0.0086	0.0056	0.008	5	0.0023
BT-02-69			84	85.5	98761	0.0054	0.0087	0.008	5	0.0037
BT-02-69			90.5	92	98762	0.0069	0.0091	0.009	5	0.0043
BT-02-69			97	98.5	98763	0.0092	0.0078	0.008	5	0.005
BT-02-69			103.5	105	98764	0.0084	0.0075	0.007	5	0.0046
BT-02-69			110	111.5	98765	0.0119	0.0068	0.002	5	0.0052
BT-02-69			116.5	118	98766	0.0121	0.008	0.002	5	0.0053
BT-02-69			123	124.5	98767	0.0127	0.0077	0.001	5	0.0057
BT-02-69			129.5	131	98768	0.0121	0.0058	0.003	5	0.0052
BT-02-69			136	137.5	98769	0.0136	0.006	0.0005	5	0.0054
BT-02-69			141.2	141.9	98770	0.0022	0.0133	0.008	11	0.0019
BT-02-69			141.9	142.6	98771	0.0136	0.0086	0.002	5	0.0056
BT-02-69			147.5	149	98772	0.0147	0.0066	0.001	5	0.0059
BT-02-69			153	154.5	98773	0.0198	0.0051	0.002	5	0.0067
BT-02-69			159.5	161	98774	0.019	0.0089	0.003	10	0.0053
BT-02-69			166	167.5	98775	0.0321	0.0136	0.001	5	0.0073
BT-02-69			167.5	168.5	98776	0.0285	0.006	0.003	5	0.0067
BT-02-69			171	172.5	98777	0.0578	0.0524	0.096	41	0.0082
BT-02-69			175.5	177	98778	0.0245	0.0072	0.0005	5	0.0051
BT-02-69			177	178.5	98779	0.0268	0.0081	0.0005	5	0.0063
BT-02-69			178.5	180	98780	0.025	0.008	0.0005	5	0.0059
BT-02-69			180	181	98781	0.0213	0.0092	0.0005	5	0.0056
BT-02-69			181	182	98782	0.105	0.217	0.286	114	0.0122
BT-02-69			182	183	98783	0.0024	0.0036	0.0005	5	0.0015
BT-02-69			185.5	186	98784	0.001	0.0016	0.0005	5	0.0016
BT-02-69			196.7	197.7	98785	0.0157	0.0127	0.006	13	0.0063
BT-02-69			204.7	205.4	98786	0.0071	0.007	0.0005	15	0.0037
BT-02-69			209.6	210.2	98787	0.0146	0.0077	0.0005	5	0.0052
BT-02-69			217.5	219	98788	0.0018	0.0006	0.0005	5	0.0019
BT-02-69			219	220	98789	0.0018	0.0004	0.0005	5	0.0019
BT-02-70	631475	5258360	27.1	27.5	98843	0.0025	0.0011	0.002	5	0.0011
BT-02-70			39.2	39.5	98844	0.002	0.0004	0.002	5	0.0011
BT-02-70			111.1	112.1	98845	0.0024	0.0033	0.002	5	0.005
BT-02-70			155.8	156.8	98846	0.003	0.0003	0.002	5	0.0013
BT-02-70			156.8	158.3	98847	0.0219	0.0066	0.004	5	0.0041
BT-02-70			158.3	159.8	98848	0.022	0.0093	0.003	5	0.004
BT-02-70			159.8	161.3	98849	0.0263	0.0391	0.008	5	0.0057
BT-02-70			161.3	162.8	98850	0.0203	0.0193	0.004	5	0.0045
BT-02-70			162.8	164.3	98851	0.0444	0.0984	0.026	12	0.0054

BT-02-70			164.3	165.8	98852	0.028	0.0356	0.01	5	0.0041
BT-02-70			165.8	167.3	98853	0.0269	0.0441	0.01	5	0.0043
BT-02-70			171	172.5	98854	0.0222	0.0116	0.002	5	0.0049
BT-02-70			177	178.5	98855	0.0232	0.0089	0.002	5	0.0046
BT-02-70			180	181	98856	0.0362	0.0739	0.041	12	0.0049
BT-02-70			185.5	187	98857	0.0168	0.0114	0.002	5	0.0043
BT-02-70			195	196.5	98858	0.0194	0.0077	0.002	5	0.0053
BT-02-70			199.7	201	98859	0.0258	0.0097	0.004	5	0.0057
BT-02-70			206	207	98860	0.0192	0.0018	0.002	5	0.0034
BT-02-70			209.8	211.2	98861	0.0191	0.0068	0.002	5	0.0038
BT-02-70			215	216	98862	0.0276	0.0105	0.005	5	0.0046
BT-02-70			220	221	98863	0.0112	0.0129	0.007	5	0.0024
BT-02-70			221	222	98864	0.0076	0.0096	0.003	5	0.0024
BT-02-70			222	223	98865	0.0159	0.0309	0.009	5	0.0034
BT-02-70			223	224	98866	0.0185	0.0172	0.012	5	0.0031
BT-02-70			224	225	98867	0.0139	0.021	0.01	5	0.0028
BT-02-70			225	226.1	98868	0.0052	0.0028	0.002	5	0.0018
BT-02-70			226.1	227.1	98869	0.0024	0.001	0.002	5	0.0013
BT-02-70			235.4	236.4	98870	0.0019	0.0085	0.0005	5	0.0012
BT-02-70			236.4	237	98871	0.0176	0.0169	0.006	5	0.0039
BT-02-70			237	238	98872	0.0254	0.023	0.021	5	0.0041
BT-02-70			238	239	98873	0.0276	0.0476	0.024	5	0.0042
BT-02-70			239	240	98874	0.0378	0.0673	0.041	14	0.0042
BT-02-70			240	241	98875	0.0192	0.0012	0.005	5	0.0058
BT-02-70			241	242	98876	0.0179	0.0255	0.004	5	0.0046
BT-02-70			242	243	98877	0.0167	0.0088	0.003	5	0.0042
BT-02-70			243	244	98878	0.01	0.0101	0.002	5	0.0048
BT-02-70			244	245	98879	0.0111	0.004	0.0005	5	0.0034
BT-02-70			245	246	98880	0.0137	0.0097	0.0005	5	0.0045
BT-02-70			251.5	252.5	98881	0.0121	0.0052	0.0005	5	0.0036
BT-02-70			256	257	98882	0.016	0.0051	0.0005	5	0.0048
BT-02-70			262.5	263.5	98883	0.017	0.0091	0.0005	5	0.0042
BT-02-70			268.6	269.1	98884	0.0104	0.0065	0.0005	5	0.0029
BT-02-70			269.9	271	98885	0.0169	0.0152	0.0005	5	0.0039
BT-02-70			272	272.5	98886	0.015	0.0092	0.002	5	0.0043
BT-02-70			277.5	278.5	98887	0.0155	0.0075	0.004	5	0.0038
BT-02-70			283	284.5	98888	0.0187	0.0047	0.009	5	0.0034
BT-02-70			285	285.5	98889	0.0132	0.0164	0.0005	5	0.0051
BT-02-70			293.3	294.1	98890	0.0213	0.005	0.002	5	0.0036
BT-02-70			294.1	295	98891	0.0068	0.0062	0.004	5	0.0021
BT-02-70			296.5	297	98892	0.0063	0.0038	0.002	5	0.0017
BT-02-70			297	297.8	98893	0.0208	0.0058	0.002	5	0.0037
BT-02-70			297.8	298.5	98894	0.0199	0.0067	0.002	5	0.0039
BT-02-70			298.5	298.7	98895	0.0973	0.269	0.181	51	0.0084
BT-02-70			298.7	300	98896	0.0196	0.0096	0.006	5	0.004
BT-02-70			315.6	315.8	98897	0.0037	0.0018	0.0005	5	0.0007
BT-02-70			320.1	320.5	98898	0.0061	0.0013	0.003	5	0.0019

BT-02-70			334.25	334.7	98899	0.007	0.0013	0.002	5	0.0024
BT-02-70			341	342	98900	0.0017	0.0335	0.0005	5	0.0006
BT-02-70			347.3	347.85	98901	0.0019	0.0045	0.002	5	0.0019
BT-02-70			354.5	355	98902	0.0019	0.0005	0.0005	5	0.0005
MR-01-49	632409.1	5258965.1	113	114	22388	0.004	0.003	0.0001	5	0.006
MR-01-49			114	115	22389	0.02	0.023	0.0027	5	0.011
MR-01-49			115	116	22390	0.01	0.005	0.0005	5	0.013
MR-01-49			116	117.2	22391	0.005	0.005	0.0004	5	0.005
MR-01-49			123	124	22392	0.013	0.005	0.0002	5	0.005

Appendix 3: Competent Person's Consent Form

Competent Person's Consent Form

I, Jonathan King, BSc (Hons.), MAIG, confirm that I am the Competent Person for the Report and;

- I have read and understood the requirements of the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code, 2012 Edition).
- I am a Competent Person as defined by the JORC Code 2012 Edition, having five years experience that is relevant to the style of mineralisation and type of deposit described in the Report, and to the activity for which I am accepting responsibility.
- I am a member in good standing of the Australian Institute of Geoscientists (AIG).
- I have reviewed the Report to which this Consent Statement applies.

I am a consultantt working for:

Dreamlife Holdings Pty Ltd

Appendix 4: JORC Code, 2012 Edition- Section 1- Baby Project

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Comments
Sampling techniques	*Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*	*Aurora Platinum Inc:* *For the various diamond drill programmes, all the core is logged and zones of mineralization are sampled, with most sample lengths being 1.0 m. However, as geological conditions dictate shorter sample lengths are taken and some longer ones up to 1.5 m are also taken. The core is split longitudinally with a diamond saw with one-half being taken as the sample. The remaining half of the core is stored at the office/core storage facility in Laverlochère and remains available to Zeus to relog/use.* *No handheld instruments were used to support logging the core*
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	*Every 40th drill core sample was quartered with one-quarter of the sample being sent to a second lab for check analysis.*
	Aspects of the determination of mineralisation that are Material to the Public Report.In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	*As outlined above standard diamond drilling and sampling practices were exercised in all drilling campaigns.*
Drilling techniques	*Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	*Only NQ-sized diamond drilling has been performed across all the Projects that comprise the Baby Project*
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.*	*Sample recovery was assessed visually and recorded onto a logging sheet.*
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	*Samples are assumed to be representative as no reference is made to sample recovery/coreloss on any log*
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	*No relationship between sample recovery and grade has been established.*
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	*All samples were geologically logged to the level of detail required to support a Mineral Resource Estimation.*
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.	*The logging conducted is qualitative. Limited core photos are available for some of the core drilled across the property.*

Criteria	JORC Code explanation	Comments
	The total length and percentage of the relevant intersections logged.	All drill holes have been logged in full.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	Core was mostly half sawn, except where a check sample was taken, in which case one half was quartered and submitted to a separate laboratory.
	If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.	Only diamond drilling
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	Samples are dried if necessary and crushed to 90% passing minus 10 mesh at XRAL's sample preparation facility. Crusher rejects are stored at the laboratory and a subsample of approximately 300 g is riffled and pulverized to 90% passing minus 200 mesh.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	In addition to the laboratory's internal analysis of accuracy and precision, 5% of the pulps are retained and sent to a second lab for analysis of precision. As a further check, every 40th drill core sample is quartered with one-quarter of the sample being sent to a second lab for analysis.
	Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.	Every 40th drill core sample was quartered with one-quarter of the sample being sent to a second lab for analysis. No field duplicates were taken.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	The sample sizes are considered to be appropriate to correctly represent the sought-after mineralisation styles.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	Gold, platinum and palladium were analysed by Fire Assay with a DCP finish. A gravimetric assay is done for gold values greater than 1000 ppb. Silver, copper, nickel and cobalt are determined by an atomic absorption finish after total digestion of the sample. The used techniques are considered appropriate for the mineralisation styles encountered.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No tools of this nature were utilised.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	In addition to the laboratory's internal analysis of accuracy and precision, 5% of the pulps are retained and sent to a second lab for analysis of precision. As a further check, every 40th drill core sample is quartered with one-quarter of the sample being sent to a second lab for analysis.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	No verification of significant intercepts has been conducted.
	The use of twinned holes.	No twinning of drill holes has been conducted.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	It is unknown how the primary data was initially captured. Historical reports with detailed geological logging and sampling have been captured by Zeus.
	Discuss any adjustment to assay data.	No adjustments were made to the raw assay data presented in this report.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral	Drill hole collar locations were recorded using a handheld GPS or differential GPS. No downhole surveys are reported on any logs

Criteria	JORC Code explanation	Comments
	Resource estimation.	
	Specification of the grid system used.	*NAD83 - Zone 17 coordinates are utilised.*
	Quality and adequacy of topographic control.	*Elevation information utilised for the drilling was from the GPS.*
Data spacing and distribution	*Data spacing for reporting of Exploration Results.*	*The completed drill holes were not formulated or grid controlled, but rather placed where most suitable with access.*
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	*The data spacing and distribution of drilling programmes are sufficient to establish a degree of geological and grade continuity appropriate for the estimation of a Mineral Resource, but lack of downhole surveys restrict use in resource estimations.*
	Whether sample compositing has been applied.	*No sample compositing has been applied to drill samples.*
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	*The orientation of the drill holes to date is appropriate in regards to the orientation of the 3D modelled mineralisation.*
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	*Some drilling is likely to report widths that are generally thicker than the true width of mineralisation. There are no known biases caused by the orientation of the drill holes.*
Sample security	*The measures taken to ensure sample security.*	*Aurora personnel transport the samples to Les Laboratoires XRAL (a division of the SGS Group), Rouyn-Noranda, Quebec.*
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	*No audits or reviews have been conducted to date.*

Appendix 4: JORC Code, 2012 Edition- Section 2- Baby Project

Section 2 Reporting of Exploration Results

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	· Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Baby Project is located 600km northwest of Montreal and 25km northeast of Villa Marie in the Témiscamingue area, south-western Québec, Canada. The designated claim package of Zeus Minerals includes 4 sub-projects in two project areas that collectively contain 127 claim blocks totalling approximately 6351 hectares. Zeus has a legally binding share sale agreement with the sole shareholder of Zeus Minerals Corp BC 1122652 and Zeus Olympus Sub Corp BC 1128488 (companies incorporated in British Columbia, Canada) whereby Zeus will acquire 100% of the issued capital of both Companies.
	· The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	The claims are registered and granted.
Exploration done by other parties	· Acknowledgment and appraisal of exploration by other parties.	Aurora Platinum Inc was the first company to perform systematic exploration and prospecting across the Baby Project area.
Geology	· Deposit type, geological setting and style of mineralisation.	Zeus is focused on the exploration for Ni-Cu-PGM-bearing gabbro bodies which intrude a sequence of mafic volcanic rocks at or near the contact with overlying felsic volcaniclastic sedimentary rocks in the Belleterre-Angliers Greenstone Belt. The mineralisation occurs as disseminated to massive sulphides near the base of the gabbro bodies and as remobilised sulphides along shears. The company is also exploring Porphyry-related Cu-Mo mineralisation associated with quartz veins in a tonalite intrusive at its Laverlochere property.
Drill hole Information	· A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:	The drill holes reported in this report have been reported using ~1% NIEq minimum reporting grade.
	o easting and northing of the drill hole collar	Coordinates are reported in NAD83-Zone 17.
	o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar	RL is NAD83
	o dip and azimuth of the hole	Dip is the inclination of the hole from horizontal (i.e. a hole drilled vertically down from the surface is -90 ^{o}). Azimuth is reported in degrees as the direction towards which the hole is drilled. The dip and azimuths have only been recorded at the collar. These varied from hole to hole, as the target was often a moderately-dipping, and plunging lens locally reworked by subsequent shearing. Drilling was positioned and oriented to suit the anticipated geometry of the ore body.

Criteria	JORC Code explanation	Commentary
	o down hole length and interception depth	*Down hole length of the hole is the distance from the surface to the end of the hole, as measured along the drill trace. Interception depth is the distance down the hole as measured along the drill trace. Intersection width is the downhole distance of an intersection as measured along the drill trace. These varied from hole to hole, and dependent on the purpose of the hole – no set depth, grid controlled drilling performed.*
	o hole length.	*Hole length is the distance from the surface to the end of the hole, as measured along the drill trace. These varied per hole based on the objective.*
	· If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	*All results relating to the drill sections provided have been stated including "No significant intercepts".*
Data aggregation methods	*· In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.*	*All reported assays have been length weighted.*
	· Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	*For the various diamond drill programmes, all the core is logged and zones of mineralization are sampled, with most sample lengths being 1.0 m. However, as geological conditions dictate shorter sample lengths are taken and some longer ones up to 1.5 m are also taken. No aggregate results have been reported.*
	· The assumptions used for any reporting of metal equivalent values should be clearly stated.	*NiEq% = (Ni%*86%) + (Cu%*0.492*96%) + (Co%*6.454*92%) + (Pt ppm*0.067*80%) + (Pd ppm*0.073*80%).* *Metal prices used are: Cu US$6,786/t, Ni US$13,789/t, Co US$88,999/t, PGM US$930/oz, (reference infomine.com spot prices quoted on 11-05-2018).* *The metallurgical recoveries for the Lac Kelly deposit used; these are: Ni (86%), Cu (96%), Co (92%); PGM + Au (80%).* *The Lac Kelly deposit has been the beneficiary of comprehensive metallurgical study. It sits in the same greenstone belt, in the same package of rocks, host the same style of mineralisation in the same rock types, and includes the same suite of metals.* *The Company posits that the mineralogy and geological setting of the Lac Kelly deposit offer an excellent indication of the expected recoveries across the deposit type, and thus qualify use of reporting on a metal equivalent basis.*
Relationship between mineralisation widths and intercept lengths	*· These relationships are particularly important in the reporting of Exploration Results.*	*It is probable that some mineralisation widths have been reported as thicker than the actual width of mineralisation given the modelled geometry of lens is moderately dipping and plunging.*
	· If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	*The geometry of the mineralisation is confined to a lens 60 metres in length with a maximum width of 15 metres. The lens dips south at approximately 58° and plunges west at 15º.*
	· If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	*All drill results within this report are downhole intervals only. True width is not known and will be calculated from further drilling and when the geometry is confirmed.*

Criteria	JORC Code explanation	Commentary
Diagrams	*· Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	*A plan view and drill sections where relevant have been provided in this report.*
Balanced reporting	*· Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	*Sampling only occurred where mineralisation or a zone of geological interest was encountered All results from this sampling have been reported.*
Other substantive exploration data	*· Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	*The other material exploration data inclusive of various types of geophysical survey information has been documented in this report. Mostly general in nature and provides support as to the mineral prospectivity remaining in the ground and as such is not considered as material.*
Further work	*· The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).*	*A detailed exploration budget is included in this report which focuses towards the defined mineralised targets, further exploration drilling, resource estimation and metallurgical studies.*
	· Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	*Exploration targeting based on the current drilling results has been completed and a suitably designed drilling programme has been approved to commence after the listing of the company.*

Appendix 5: JORC Code, 2012 Edition- Section 1- Lac des Bois Project

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.	Much of the legacy data associated with the project is in the early stages of compilation. The reported results come mainly from historical exploration reports, research papers or a recent 43-101 technical report prepared for the property.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Not reported
	Aspects of the determination of mineralisation that are Material to the Public Report.In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	No sampling was performed by the author. The author was able to verify part of the historical work. The trails, old mine working zones (Mine Lorraine) and mineralized outcrops were observed, attesting the exploration work done in the past. The author currently has no reason to suspect that the work reported on the property was in fact not done.
Drilling techniques	Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	Between 1952 and 2005, 168 diamond holes for an advance of 17,242m were drilled. This information is presently being compiled.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	Logs captured on paper. Sampling method not reported.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	Not reported
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Not reported
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	Geologically logged, much of the drilling was in support of resource work. This information is still being acquired, compiled and assessed.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.	The bulk of the drilling was quantitative and used in resource estimation at the Lorraine or Blondeau Projects The scattered diamond holes were mostly qualitative.
	The total length and percentage of the relevant intersections logged.	Holes logged through their development length, but not necessarily sampled.

Criteria	JORC Code explanation	Commentary
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.*	*Not reported*
	If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.	*Only diamond drilling performed*
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	*Not reported o*
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	*Not reported*
	Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.	*Not reported*
	Whether sample sizes are appropriate to the grain size of the material being sampled.	*Not reported*
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	*Unknown*
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	*Not available at the time the work was completed*
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	*Not reported*
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.*	*Peer review by subsequent explorers – satisified*
	The use of twinned holes.	*Not reported*
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	*Paper logs for all details*
	Discuss any adjustment to assay data.	*Not reported*
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	*Established local grids used to control exploration, including drilling*
	Specification of the grid system used.	*Not reported*

Criteria	JORC Code explanation	Commentary
	Quality and adequacy of topographic control.	Not reported
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Limited grid-based exploration, mostly uncontrolled prospecting
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	No drilling at this time, the historical is still being compiled and further remarks will be made in subsequent announcements by the company after the compilation and review is complete.
	Whether sample compositing has been applied.	Not reported
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	Not reported.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	Not reported
Sample security	The measures taken to ensure sample security.	Not reported
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	No audits identified

Appendix 5: JORC Code, 2012 Edition- Section 2- Lac des Bois Project

Section 2 Reporting of Exploration Results

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	· Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Lac des Bois Project is located 600km northwest of Montreal and 50km east-southeast of Villa Marie in the Témiscamingue area, south-western Québec, Canada. The designated claim package of Zeus Minerals includes 4 Projects in two project areas that collectively contain 127 claim blocks totalling approximately 6351 hectares. Zeus has a legally binding share sale agreement with the sole shareholder of Zeus Minerals Corp BC 1122652 and Zeus Olympus Sub Corp BC 1128488 (companies incorporated in British Columbia, Canada) whereby Zeus will acquire 100% of the issued capital of both Companies.
	· The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	No issues or impediments
Exploration done by other parties	· Acknowledgment and appraisal of exploration by other parties.	Several TSX-listed companies have reviewed the asset, including Aurora Platinum Inc and Greg Exploration inc..
Geology	· Deposit type, geological setting and style of mineralisation.	Production at the Lorraine Mine came from a single elongate sulphide lens found along the sheared gabbro-volcanic contact. The lens exhibits a mineralogical zonation characterised by a central massive sulphide zone rich in pyrrhotite and pentlandite surrounded by a chalcopyrite-rich disseminated sulphide zone. Potential VMS mineralisation, including Zn-Cu was identified at the Roy showing, and some significant gold mineralisation is known to exist in the gabbro and is hosted within quartz-carbonate veins in metavolcanic rocks.i
Drill hole Information	· A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:	The historical drilling data is still being compiled into a workable format. The company will release the findings after the results of the compilation are reviewed.
	o easting and northing of the drill hole collar	Not reported
	o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar	No RL specific information was sourced.

Criteria	JORC Code explanation	Commentary
	o dip and azimuth of the hole	*Holes are variable in dip and azimuth*
	o down hole length and interception depth	*Not reported*
	o hole length.	*Reported on logs, still be captured digitally*
	· If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	*Careful compilation of the data is warranted, as progressive summaries of work completed has seen a blurring of the information and by whom. This needs to be rectified before commencing exploration.*
Data aggregation methods	*· In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.*	*Unknown what reporting protocols were used*
	· Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	*Unknown*
	· The assumptions used for any reporting of metal equivalent values should be clearly stated.	*Unknown*
Relationship between mineralisation widths and intercept lengths	*· These relationships are particularly important in the reporting of Exploration Results.*	*Unknown*
	· If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	*Drill orientation appropriate for target, though may be refined upon further study*
	· If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	*Drill orientation is appropriate.*

Criteria	JORC Code explanation	Commentary
Diagrams	· Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Historical data is still being compiled
Balanced reporting	· Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	The project is limited by the availability of public domain information given the relative age of the project and the then voluntary reporting obligations on companies. The author included as much information as he could find from multiple sources in the public domain in a best effort to provide balanced reporting.
Other substantive exploration data	· Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	Geochemical information has been culled from whatever public domain reports could be found. This information mostly reported peak values, but where ranges of values were reported they are adopted for the report. The reader must consider this in their assessment of the results.
Further work	· The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Compilation of a cohesive digital database including all historical drilling, surface sampling, mapping, and geophysical information. Detailed geological mapping. Review the structural setting for Ni-Cu and gold mineralisation prior to drilling.
	· Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	The company will update the market with the results of the data compilation as it progresses.

APPENDIX 6: Drill hole collar and survey data files

Drill Collar Data – Coordinate System UTM Datum NAD83 Z17

Hole Number	mE	mN	Elevation (m)	Depth (m)
BT-01-01	631670.9	5258544.3	282.1	147
BT-01-02	631678.4	5258561.4	276.7	100
BT-01-03	631684.6	5258578.8	271.4	101
BT-01-04	631671.5	5258544.5	282.1	149
BT-01-05	631628.6	5258579.9	274	105
BT-01-06	631638.3	5258632	263.6	80
BT-01-07	631628.4	5258579.5	274	105
BT-01-08	631628.1	5258578.7	273.9	137
BT-01-09	631601.9	5258581.9	274.7	130
BT-01-10	631602	5258582.5	274.8	110
BT-01-11	631620.2	5258625.5	267.7	101
BT-01-12	631630.9	5258619.3	267.9	100
BT-01-13	631631.3	5258620.3	267.9	80
BT-01-14	631642.6	5258615.4	266.4	102
BT-01-15	631615.8	5258582.1	274.2	101
BT-01-16	631643.6	5258577.8	272.5	101
BT-01-17	631651.2	5258604.3	267.5	90
BT-01-18	631651.5	5258605.8	267.4	80
BT-01-19	631615.3	5258623.1	268.1	101
BT-01-20	631592.4	5258618.3	275.3	120
BT-01-21	631605.6	5258650.3	268.3	101
BT-01-22	631605.2	5258651.8	268.6	101
BT-01-23	631585	5258665.6	272.9	101
BT-01-24	631225.1	5258945.2	270.3	105
BT-01-25	631104.3	5258895.5	270.3	100
BT-01-26	631785.3	5258434.7	259.1	150
BT-01-27	631682.7	5258159.7	270.1	150
BT-01-28	631631.6	5258022.4	267.1	119
BT-01-29	631276.8	5258195.5	276.2	150
BT-01-30	631137.6	5258106.2	270.1	149
BT-01-31	631410.9	5258570	272.2	154
BT-01-32	631592.2	5258625.7	275	122
BT-01-33	631591.3	5258625.9	275.4	120
BT-01-34	631588.6	5258614.4	275.4	128
BT-01-35	631569.7	5258629.9	277.6	150
BT-01-36	632663.03	5256028.7	289.59	130
BT-01-37	632662.45	5256027.97	289.16	150
BT-01-38	632633.41	5255972.77	288.81	148
BT-01-39	632768.48	5255989.32	287.87	150
BT-01-40	632622.84	5256019.99	290.02	125
BT-01-41	632323.43	5256324.81	276.23	149
BT-01-42	632432.54	5256289.46	280.16	200
BT-01-43	632525.24	5256263.35	281.04	150
BT-01-47	632628.64	5256308.88	283.62	150
BT-01-48	632610.81	5256535.87	281.79	150

BT-01-49	632609.16	5256050.72	286.99	150
BT-02-50	631543	5258625	265	151
BT-02-51	631509	5258670	265	150
BT-02-52	631522	5258735	265	125
BT-02-53	631618	5258474	265	200
BT-02-54	631669	5258474	265	150
BT-02-55	631683	5258160	265	140
BT-02-56	631208	5258984	265	100
BT-02-57	631541	5258694	265	100
BT-02-58	631683	5258445	265	125
BT-02-61	632658	5256136	287	152
BT-02-62	632633	5256156	287	182
BT-02-63	632605	5256167	287	225
BT-02-64	632436	5256211	287	150
BT-02-65	632328	5256198	287	182
BT-02-66	632216	5256251	287	182
BT-02-67	631520	5258500	265	321
BT-02-68	632691	5256192	287	275
BT-02-69	631520	5258500	265	238
BT-02-70	631475	5258360	265	378

Drill Collar Azimuth – Dip – Downhole Survey Data

Hole Number	Survey Depth	Azimuth	Dip
BT-01-01	0	20	-59
BT-01-01	100	20	-57
BT-01-01	147	20	-54
BT-01-02	0	22	-60
BT-01-02	100	22	-52
BT-01-03	0	23	-60
BT-01-03	100	23	-57
BT-01-04	0	42	-50
BT-01-04	100	42	-49
BT-01-04	149	42	-47
BT-01-05	0	22	-44
BT-01-05	100	22	-44
BT-01-06	0	22	-50
BT-01-06	79.7	22	-48
BT-01-07	0	22	-60
BT-01-07	100	22	-53
BT-01-08	0	360	-90
BT-01-08	100	360	-90
BT-01-08	137	360	-90
BT-01-09	0	16	-70
BT-01-09	130	16	-69
BT-01-10	0	15	-50

BT-01-10	100	15	-48
BT-01-11	0	16	-60
BT-01-11	100	16	-58
BT-01-12	0	20	-80
BT-01-12	100	20	-83
BT-01-13	0	23	-50
BT-01-13	80	23	-50
BT-01-14	0	17	-52
BT-01-14	100	17	-48
BT-01-15	0	21	-74
BT-01-15	100	21	-78
BT-01-16	0	14	-76
BT-01-16	100	14	-71
BT-01-17	0	360	-90
BT-01-18	0	13	-50
BT-01-18	80	13	-47
BT-01-19	0	110	-50
BT-01-19	101	110	-50
BT-01-20	0	22	-50
BT-01-20	120	22	-49
BT-01-21	0	52	-50
BT-01-21	101	52	-48
BT-01-22	0	20	-50
BT-01-22	100	20	-49
BT-01-23	0	29	-50
BT-01-23	101	29	-46
BT-01-24	0	20	-50
BT-01-24	105	20	-48
BT-01-25	0	20	-50
BT-01-26	0	21	-50
BT-01-26	150	21	-53
BT-01-27	0	20	-50
BT-01-28	0	20	-44
BT-01-28	119	20	-48
BT-01-29	0	20	-50
BT-01-30	0	20	-50
BT-01-31	0	110	-50
BT-01-31	150	110	-48
BT-01-32	0	103	-51
BT-01-32	122	103	-47
BT-01-33	0	103	-62
BT-01-34	0	107	-50
BT-01-34	128	107	-46
BT-01-35	0	101	-50
BT-01-36	0	25	-50
BT-01-36	130	25	-48.5
BT-01-37	0	25	-70
BT-01-37	150	25	-71
BT-01-38	0	25	-50
BT-01-38	145	25	-49

BT-01-39	0	355	-50
BT-01-39	150	355	-45
BT-01-40	0	28	-50
BT-01-40	125	28	-44
BT-01-41	0	360	-50
BT-01-41	149	360	-49
BT-01-42	0	14	-50
BT-01-42	200	14	-39.5
BT-01-43	0	360	-50
BT-01-43	150	360	-49
BT-01-47	0	360	-50
BT-01-47	150	360	-49
BT-01-48	0	360	-50
BT-01-48	150	360	-45.5
BT-01-49	0	28	-62
BT-01-49	150	28	-61
BT-02-50	0	106	-50
BT-02-50	150	106	-48
BT-02-51	0	90	-50
BT-02-51	150	90	-46
BT-02-52	0	90	-50
BT-02-52	125	90	-52
BT-02-53	0	90	-50
BT-02-53	100	90	-48
BT-02-53	200	90	-48
BT-02-54	0	90	-50
BT-02-55	0	90	-50
BT-02-56	0	90	-50
BT-02-57	0	20	-50
BT-02-57	100	20	-50
BT-02-58	0	100	-50
BT-02-58	125	100	-48
BT-02-61	0	210	-60
BT-02-61	50	208.2	-56.7
BT-02-61	100	205.1	-53.4
BT-02-61	152	208	-52.3
BT-02-62	0	210	-60
BT-02-62	50	208.3	-57.4
BT-02-62	101	206.4	-54.3
BT-02-62	152	207.8	-52.2
BT-02-63	0	210	-60
BT-02-63	50	210.4	-59.5
BT-02-63	101	208.5	-56.9
BT-02-63	152	210.8	-56.9
BT-02-63	200	207.4	-55.9
BT-02-63	225	204.5	-55.8
BT-02-64	0	180	-50
BT-02-64	50	180.4	-46.3
BT-02-64	101	179.1	-43.9
BT-02-64	150	181.1	-42.6

BT-02-65	0	180	-50
BT-02-65	50	181.6	-49
BT-02-65	101	184.5	-48.7
BT-02-65	152	190.4	-49.4
BT-02-65	182	189.1	-49.8
BT-02-66	0	180	-50
BT-02-66	60	182.2	-51.6
BT-02-66	120	184.6	-51.1
BT-02-66	182	186.2	-50.3
BT-02-67	0	5	-85
BT-02-67	51	10.8	-84.9
BT-02-67	100	8.1	-85.1
BT-02-67	150	10.3	-85
BT-02-67	200	12.1	-84.7
BT-02-67	250	10.1	-84.8
BT-02-67	300	10.9	-84.6
BT-02-67	321	13.3	-84.5
BT-02-68	0	210	-50
BT-02-68	50	210.8	-46.8
BT-02-68	101	214.6	-45.6
BT-02-68	152	209	-45.9
BT-02-68	200	208.3	-44.8
BT-02-68	275	206	-42.7
BT-02-69	0	20	-70
BT-02-69	54	16.4	-70.2
BT-02-69	100	16.5	-69.8
BT-02-69	150	16	-69.8
BT-02-69	201	17.1	-69.7
BT-02-69	238	19.3	-69.1
BT-02-70	0	20	-60
BT-02-70	50	18.9	-59.7
BT-02-70	100	19.7	-58.9
BT-02-70	150	20.9	-57.7
BT-02-70	200	25.7	-57.5
BT-02-70	250	21.3	-57.3
BT-02-70	300	22.9	-57.3
BT-02-70	350	23.7	-56.9