14 March 2018

STRANDLINE
resources limited

Significant new mineral sands intersections at the Sudi project

Assays reveal thick intervals of heavy mineral sands along the 8km anomaly defined at Sudi, which is in joint venture with Rio Tinto

HIGHLIGHTS

- **Strandline has discovered significant mineral sands with the first phase of air core drilling at the Sudi Project in Southern Tanzania**
- **The drilling has outlined mineral sands anomalies with indications of high-value assemblage along 8km of strike**
- **Assays reveal thick intervals of Total Heavy Mineral (THM) from surface. Significant results include:**
  - 25.5m @ 3.4% THM, including 12m @ 4.1% THM from surface (17SDAC5030)
  - 9m @ 3.8% THM from surface (17SDAC5326)
  - 9m @ 3.4% THM from surface (17SDAC5006)
  - 10.5m @ 3.0% THM from surface (17SDAC5093)
  - 7.5m @ 3.1% THM from surface (17SDAC5327)
  - 6m @ 3.1% THM from 6m (17SDAC5020).
  - 6m @ 3.9% THM from 16.5m (17SDAC5348)
- **Mineral assemblage testwork from composite samples confirms a high unit value assemblage averaging 11.5% zircon, 4.7% rutile and 64.4% ilmenite; one composite contained 17.8% zircon**
- **Joint Venture is now planning its next phase of drilling across priority targets at Sudi and other areas of interest in Southern Tanzania**

Strandline Resources (**ASX: STA**) is pleased to announce that it has discovered significant mineral sands intersections at its Sudi Project, which forms part of the joint venture (JV) area with Rio Tinto Mining & Exploration Limited (**Rio Tinto**) in Southern Tanzania.

Assays from the first phase of air core drilling at Sudi, which is located 30km by sealed road from the port infrastructure of Mtwara, also show that the discovery has a high-value assemblage, particularly zircon and titanium.

Under the terms of the JV, Rio Tinto is funding the exploration programme, which is being conducted by Strandline (see ASX releases dated 26 April 2017 and 26 June 2017).

Drilling of the Sudi tenements formed part of the JV's regional screening programme across four project areas along 200km of coast extending north from the Tanzania-Mozambique boarder (which include the

Miteja, Kiswere, Mtwara and Sudi prospects). The regional programme comprised 366 AC drill holes totalling 6134m. Results from the other project areas will be interpreted over the coming months.

Strandline Managing Director Luke Graham said the Sudi discovery shows strong potential to add substantial value to the Company's rapidly growing mineral sands asset base.

"It is already clear that Sudi is an exciting discovery with high-value mineral sands content" Mr Graham said.

"Sudi will add further value to our pipeline of mineral sands assets, which already include the Fungoni project development, where we have completed the Definitive Feasibility Study and have a binding offtake agreement in place, and the large-scale Tanga South (Tajiri) JORC mineral resource, where we recently doubled the Resource to 147 million tonnes at 3.1 per cent Total Heavy Minerals.

"All these projects have growth potential and provide a strong foundation on which Strandline will build a world-class mineral sands business with quality products, geographic diversification, development optionality and scalability."

"At the same time, we are assessing funding and development options for our large-scale Coburn mineral sands project in WA, which is ideally positioned to capitalise on rising prices for its minerals."

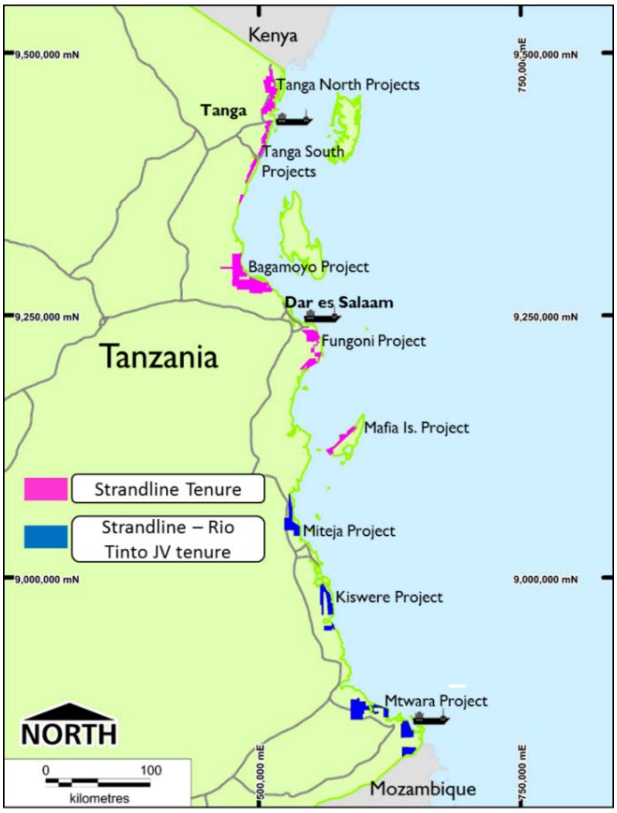

Figure 1 - Strandline holds a strategic tenement package located along 350 km of the Tanzanian coastline

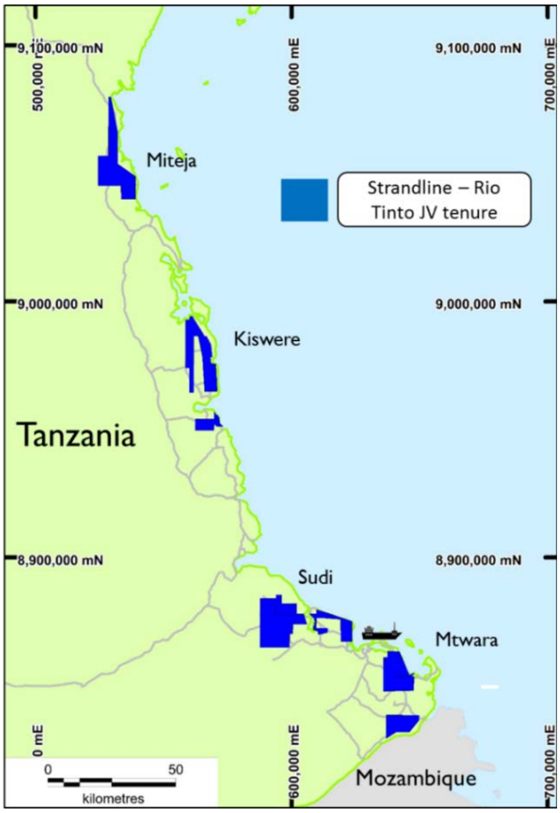

Figure 2 – Rio Tinto JV encompasses some of the Company's southern tenements including the Miteja, Kiswere, Sudi and Mtwara prospects

INTRODUCTION – SUDI PROJECT

Strandline, has successfully completed its first season of air core drilling in Southern Tanzania in joint venture with Rio Tinto. This announcement specifically relates to exploration results from the Sudi Project located 35km north of the port city of Mtwara (refer Figure 2).

The drill program was designed to target topographic and radiometric features and comprised a total of 178 holes for 3,109 metres. THM results have been received with results greater that 3% THM provided in Table 1 below.

Table 1 Significant drill results (>3% THM) from the Sudi AC drill programs

HOLE_ID	Prospect	UTM E (WGS84)	UTM N (WGS84)	DIP	AZIM	EOH (m)	FROM (m)	TO (m)	INTERVAL (m)	THM (%)	SLIME (%)
17SDAC5006	Trackside	598398	8874837	-90	360	12	0	9	9	3.4	26.8
17SDAC5020	Sudi Terrace	599907	8875721	-90	360	13.5	6	12	6	3.1	24.1
17SDAC5030	Sudi Terrace	598829	8876879	-90	360	36	0	25.5	25.5	3.4	10.6
						Including	0	12	12	4.1	13.1
						including	16.5	25.5	9	3.2	7.8
17SDAC5093	Sudi Terrace	601577	8874109	-90	360	24	0	10.5	10.5	3.0	17.7
17SDAC5325	Trackside	597946	8875121	-90	360	12	0	10.5	10.5	2.9	37.0
17SDAC5326	Trackside	598109	8875243	-90	360	30	0	9	9	3.8	33.7
17SDAC5327	Trackside	598283	8875359	-90	360	19.5	0	7.5	7.5	3.1	34.2
17SDAC5334	Sudi Terrace	599352	8876255	-90	360	36	21	25.5	4.5	3.5	3.9
17SDAC5348	Sudi Terrace	601025	8874614	-90	360	27	16.5	22.5	6	3.9	20.7

The drill program encountered thick intervals of higher grade mineralised sand (between 2 and 4% THM) and widespread lower grade mineralisation (between 1 and 2% THM). The initial drill lines were spaced approximately 3 to 4km apart with holes at 400m centres, comprising 108 holes for 1,614 metres. At the conclusion of the first pass of drilling a second pass was implemented targeting an 8km long zone of mineralisation reducing the line spacing down to 800m with 200m hole centres. This required an additional 70 holes for 1495 metres of AC drilling.

The THM results from the drill program have confirmed the presence of strongly anomalous THM along the target zone with down holes thickness of mineralisation varying from 6 to 25 metres. The width of the higher grade THM mineralisation is interpreted to range from 100 to 800 metres but further infill drilling is required to more accurately define this metric. The higher grade zones of THM are located within a very broad 500 to 1500 meters wide haloe of lower grade mineralisation that has been delineated along 8km of strike.

Refer to Figure 3 for the location of the prospects and zones of mineralisation.

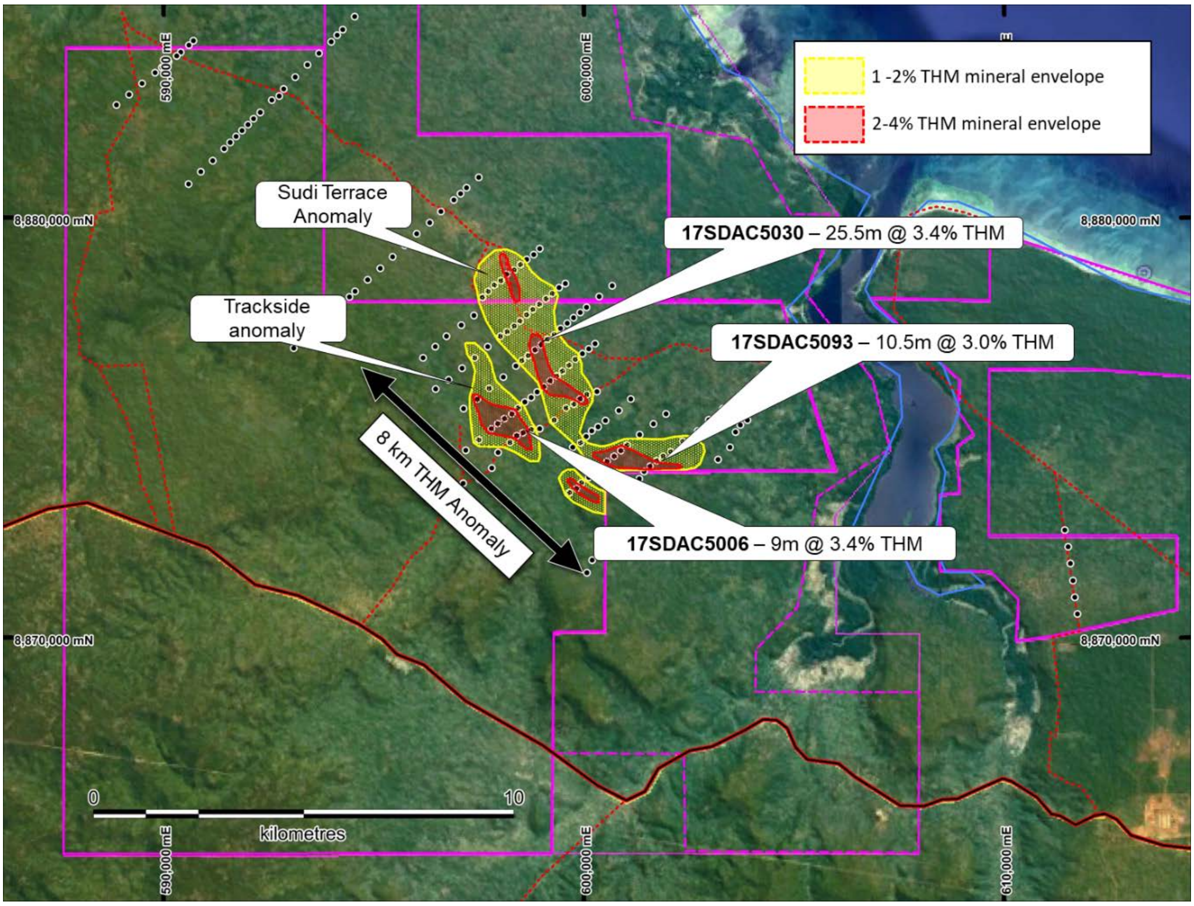

Figure 1. Sudi Project drill hole collars and locations of the Trackside and Terrace anomalies

Mineral assemblage testwork was completed from five drill hole composite samples across the mineralisation with a summary of the results presented in Table 2. The laboratory results revealed a high unit-value mineral assemblage averaging 16.2% combined zircon and rutile (11.5% and 4.7% respectively) and 64.4% ilmenite (which includes 21.1% altered ilmenite and 43.3% ilmenite species). Refer to Figure 3 for a microscopic view of the heavy mineral from hole 17SDAC5093. The images shows quite abundant elongate crystals of zircon.

Table 2 All of the Mineral Assemblage data from mineralised holes from the Sudi AC drill program

HOLE_ID	Composite	UTM E (WGS84)	UTM N (WGS84)	DIP	AZIM	EOH (m)	FROM (m)	TO (m)	THM (% of sand)	Altered Ilmenite (%)	Ilmenite (%)	Zircon (%)	Rutile (%)
17SDAC5006	5006_007	598398	8874837	-90	360	12	0	12	2.8	20.4	54.5	8.7	3.52
17SDAC5020	5020upper	599907	8875721	-90	360	14	0	12	3	19.8	46.4	12.7	5
17SDAC5030	5030upper	598829	8876879	-90	360	36	0	12	4.1	21.1	48.3	11.4	5.3
17SDAC5030	5030lower	598829	8876879	-90	360	36	12	36	2.2	22.7	33.9	9.16	4.81
17SDAC5093	5093upper	601577	8874109	-90	360	24	0	12	2.9	19.9	43	17.8	5
Altered Ilmenite: $TiO_2 \geq 55\%$ and $< 70\%$							**Averages**		**2.9**	**21.1**	**43.3**	**11.5**	**4.7**

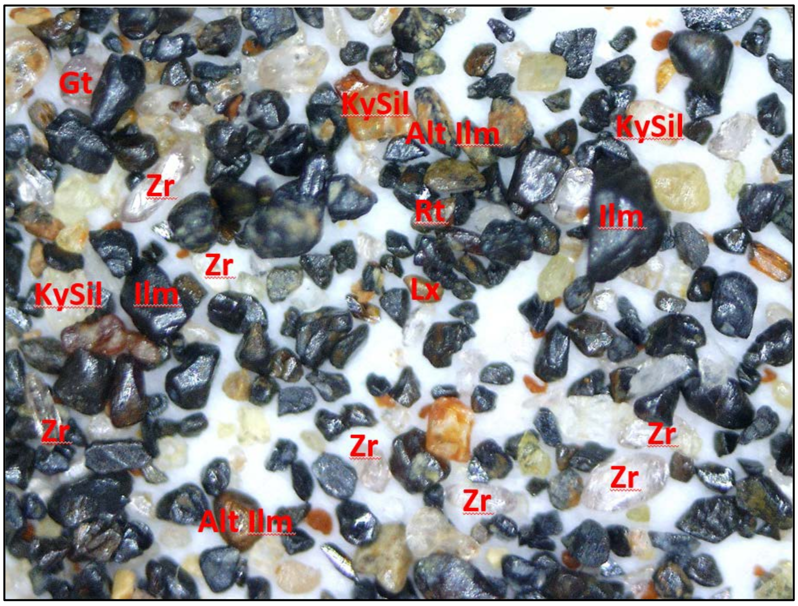

Figure 2. Microsope view of the heavy mineral concentrate from composite 5093upper with readily observed zircon (17% of the VHM). Field is view is 4.5mm

SUMMARY OF JOINT VENTURE – SOUTHERN TANZANIA

As announced on 26 April and 26 June 2017, Strandline entered into an Earn-in and Joint Venture (JV) Agreement with Rio Tinto in connection with the Company's suite of heavy mineral sands tenements located in the southern region of Tanzania. Reconnaissance air core drilling progressed strongly during the second half of 2017 across a number of priority target areas at Sudi, Kiswere, Miteja and Madimba tenements.

The Agreement with Rio Tinto is worth up to US$10.75 million (~A$14.5 million) consisting of a two-stage earn-in plus cash payments. The Stage 1 earn-in commenced in June 2017 with Rio Tinto having the option to sole fund US$5 million of exploration within 3.5 years to earn a 51% interest in the joint venture. Stage 2 involves an option to incur a further US$4 million expenditure within 2 years to earn an aggregated 75% interest.

The JV has enabled Strandline to accelerate exploration activities on the Project Area, with Rio Tinto contributing expertise and funding, whilst enabling the Company to concurrently progress its exciting northern projects (Fungoni, Tanga South and Bagamoyo) and to pursue additional strategic exploration and development initiatives including advancing the large-scale Coburn in West Australia.

ABOUT STRANDLINE

Strandline Resources Limited (**ASX: STA**) is an emerging heavy mineral sands (**HMS**) developer with a growing portfolio of 100%-owned development assets located in Western Australia and within the world's major zircon and titanium producing corridor in South East Africa. Strandline's strategy is to develop and operate quality, high margin, expandable mining assets with market differentiation and global relevance.

Strandline's project portfolio comprises development optionality, geographic diversity and scalability. This includes two zircon-rich, 'development ready' projects, the Fungoni Project in Tanzania and the large Coburn Project in Western Australia, as well as a series of titanium dominated exploration targets spread along 350km of highly prospective Tanzanian coastline, including the advanced Tanga South Project and Bagamoyo Project.

The Company's focus is to continue its aggressive exploration and development strategy and execute its multi-tiered and staged growth plans to maximise shareholder value.

TANZANIA MINERAL SANDS COMPETENT PERSON'S STATEMENTS

The information in this report that relates to Exploration Results is based on, and fairly represents, information and supporting documentation prepared by Mr Brendan Cummins, a permanent employee of Strandline. Mr Cummins is a member of the Australian Institute of Geoscientists and he has sufficient experience which is relevant to the style of mineralisation and type of deposits under consideration and to the activity which has been undertaken to qualify as Competent Persons as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Cummins consent to the inclusion in this release of the matters based on the information in the form and context in which they appear. Mr Cummins is a shareholder of Strandline Resources.

FORWARD LOOKING STATEMENTS

This report contains certain forward looking statements. Forward looking statements are only predictions and are subject to risks, uncertainties and assumptions which are outside of the control of Strandline. These risks, uncertainties and assumptions include commodity prices, currency fluctuations, economic and financial market conditions, environmental risks and legislative, fiscal or regulatory developments, political risks, project delay, approvals and cost estimates. Actual values, results or events may be materially different to those contained in this announcement. Given these uncertainties, readers are cautioned not to place reliance on forward looking statements. Any forward looking statements in this announcement reflect the views of Strandline only at the date of this announcement. Subject to any continuing obligations under applicable laws and ASX Listing Rules, Strandline does not undertake any obligation to update or revise any information or any of the forward looking statements in this announcement to reflect changes in events, conditions or circumstances on which any forward looking statements is based.

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Appendix 1 – JORC Code, 2012 Edition – Table 1

Appendix 1

JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	• Aircore drilling was used to obtain samples at 1.5m intervals • Each 1.5m sample was homogenized within the sample bag by rotating the sample bag • A sample of sand, approx. 20gm, is scooped from the sample bag for visual THM% estimation and logging. The same sample mass is used for every pan sample for visual THM% estimation • The standard sized sample is to ensure calibration is maintained for consistency in visual estimation • A sample ledger is kept at the drill rig for recording sample intervals and sample mass, and photographs are taken of samples for each hole to cross-reference with logging • The large 1.5m Aircore drill samples have an average mass of about 8kg and were split down to approximately 500gm by a leveled 3 tier riffle splitter for exportation to the processing laboratory in Australia • The laboratory sample was dried, de-slimed (removal of -45µm fraction) and then had oversize (+1mm fraction) removed. Approximately 100gm of sample was then split to use for heavy liquid separation using TBE to determine total heavy mineral (THM %) content of the sand
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Aircore drilling with inner tubes for sample return was used • Aircore is considered a standard industry technique for HMS mineralization. Aircore drilling is a form of reverse circulation drilling where the sample is collected at the face and returned inside the inner tube • Aircore drill rods used were 3m long • NQ diameter (76mm) drill bits and rods were used • All drill holes were vertical

Criteria	JORC Code explanation	Commentary
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• Drill sample recovery is monitored by measuring and recording the total mass of each 1.5m sample at the drill rig with a standard spring balance • While initially collaring the hole, limited sample recovery can occur in the initial 0.0m to 1.5m sample interval owing to sample and air loss into the surrounding loose soil • The initial 0.0m to 1.5m sample interval is drilled very slowly in order to achieve optimum sample recovery • The entire 1.5m sample is collected at the drill rig in large numbered plastic bags for dispatch to the field based initial split preparation facility • At the end of each drill rod, the drill string is cleaned by blowing down with air to remove any clay and silt potentially built up in the sample pipes • The twin-tube aircore drilling technique is known to provide high quality samples from the face/bottom of the drill hole • Wet and moist samples are placed into large plastic basins to air/sun dry in the field prior to splitting
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• The 1.5m aircore samples were each qualitatively logged onto paper field sheets prior to digital entry into a Microsoft Excel spreadsheet • The aircore samples were logged for lithology, colour, grainsize, rounding, sorting, estimated THM%, estimated Slimes% and any relevant comments - such as slope, vegetation, or cultural activity • Every drillhole was logged in full • Logging is undertaken with reference to a Drilling Guideline with codes prescribed and guidance on description to ensure consistent and systematic data collection
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field*	• The entire 1.5m drill sample collected at the source was dispatched to a field sample preparation facility to split with a 3 tier riffle splitter to reduce sample size for exportation • The water table depth was noted in all geological logs if intersected • Samples with aggregates of soil, clay or grits are gently hit with a rubber mallet in the plastic bag to break them down so the sample with flow easily through the splitter chutes • A total of 450 to 650gm of each sample was inserted into calico sample bags and exported to Diamantina Laboratories in Perth for THM analysis

Criteria	JORC Code explanation	Commentary
	duplicate/second-half sampling. • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Employees undertaking the splitting are closely monitored by a geologist to ensure sampling quality is maintained • Almost all of the samples are sand, silty sand, sandy silt, clayey sand or sandy clay and this sample preparation method is considered appropriate • The sample sizes were deemed suitable to reliably capture THM, slime, and oversize characteristics, based on industry experience of the geologists involved and consultation with laboratory staff • Field duplicates of the samples were completed at a frequency of 1 per 25 primary samples. These are alternated with the Standard Reference Material. • Standard Reference Material samples are inserted into the sample stream in the field at a frequency of 1 per 50 samples
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	• The wet panning at the drill site provides an estimate of the THM% which is sufficient for the purpose of determining approximate concentrations of THM in the first instance Aircore sample: • The individual 1.5m aircore sub-samples (approx. 1000gm) were assayed by Diamantina Laboratories in Perth, Western Australia, which is considered the Primary laboratory • The aircore samples were first screened for removal and determination of Slimes (-45µm) and Oversize (+1mm), then the sample was analysed for total heavy mineral (-1mm to +45µm) content by heavy liquid separation • The laboratory used TBE as the heavy liquid medium – with density range between 2.92 and 2.96 g/ml • This is an industry standard technique • Field duplicates of the samples were collected at a frequency of 1 per 25 primary samples • Diamantina Laboratories completed its own internal QA/QC checks that included laboratory repeats every 10th sample prior to the results being released and the use or standard reference material • Analysis of QA/QC samples show the laboratory data to be of acceptable accuracy and precision • The adopted QA/QC protocols are acceptable for this stage test work • Test work has been undertaken at a Secondary laboratory (Western Geolabs) to check the veracity of the Primary laboratory data

Criteria	JORC Code explanation	Commentary
		• No issues have been identified and the THM data is consider of high quality Mineral Composites Assemblage and characterisation samples were submitted Process Mineralogical Laboratories, in British Columbia, Canada. The method of analysis was a Scanning Electron Microscope (Tescan Vega 3) fitted with an Energy Dispersive Spectrometer (SEM-EDS) and equipped with Tescan Integrated Mineral Analyser (TIMA) and Oxford INCA Feature software capable of searching and quantifying the elemental composition of a statistically representative number of Ti-species including rutile, ilmenite, Ti-magnetite, pseudo-rutile and leucoxene. Mineral assemblage and Characterisation comprise: • Composite samples were supplied to PML • PML then reduced the mass with a micro riffle splitter to approximately 2-5gm for preparation of a polished section • Total oxide geochemistry on a grain-by-grain basis • Mineral species determination by chemical analysis • Mineral species mass % calculated from the grain spherical volume (derived from exposed grain surface area) multiplied by the mineral density • Approximately 2000-3000 grain counts, sizing and probing for mineral chemistry analysis for each sample • Titanium deportment for each titanium species • Zircon – total oxide mineral geochemistry for zircon analysis • The laboratory undertook duplicate and standard reference material analysis • A split was sent to MS analytical in BC, Canada for XRF analysis using method WRX-Zr3 to determine Zr that is used as a check against the SEM derived Zr value
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.*	• All results are checked by the Chief Geologist • The company Chief Geologist makes periodic visits to the laboratory to observe sample processing • A process of laboratory data validation using mass balance is undertaken to identify entry errors or questionable data

Criteria	JORC Code explanation	Commentary
	• *Discuss any adjustment to assay data.*	• Field and laboratory duplicate data pairs (THM/oversize/slime) of each batch are plotted to identify potential quality control issues • Standard Reference Material sample results are checked from each sample batch to ensure they are within tolerance (<2SD) and that there is no bias • The field and laboratory data has been updated into a master spreadsheet which is appropriate for this stage in the programme. Data validation criteria are included to check for overlapping sample intervals, end of hole match between 'Lithology', 'Sample', 'Survey' files, duplicate sample numbers and other common errors • No twin holes were drilled in the programme • No adjustments are made to the primary assay data
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• Down hole surveys for shallow aircore holes are not required • A handheld GPS was used to identify the positions of the drill holes in the field. The handheld GPS has an accuracy of +/- 10m in the horizontal • The datum used is WGS84 and coordinates are projected as UTM zone 37S • The drillhole collar elevation was collected from a detailed Digital Terrain Model collected in 2016 • The accuracy of the locations is sufficient for this stage of exploration
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Regional drill designs typically started with drill lines located 3 to 5km apart with drill holes 400m apart along the lines • The infill drilling at Sudi was reduced to 80 x 200 and is till considered quite broad. • Each aircore drill sample is a single 1.5m sample of sand intersected down the hole • No sample compositing techniques were used. The samples were taken at the completion of 1.5m intervals. • Compositing of samples was undertaken on HM concentrates for mineral assemblage determination. Composite samples were gathered from 5 holes across the higher grade drill holes taking quite broad zones of mineralization that included high and low grade HM material.

Criteria	JORC Code explanation	Commentary
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• The aircore drilling was generally oriented perpendicular to the strike of the dominant topographic or radiometric anomalies. • The strike of the mineralization is typically sub-parallel to the contemporary coastline • Drill holes were vertical and the nature of the mineralisation is relatively horizontal • The orientation of the drilling is considered appropriate for testing the lateral and vertical extent of mineralization without any bias
Sample security	• *The measures taken to ensure sample security.*	• Aircore samples remained in the custody of Company representatives while they were transported from the field to Dar es Salaam for final packaging and securing for airlifting to Australia. • Tanzania has strict guidelines in relation to the process of exporting mineral samples from the country. • The samples were inspected by Tanzanian Government officials from MEM and TRA who took sub samples composites for analysis. Once they were inspected the drums holding the samples were sealed. MEM and TRA require sample analysis for royalty payment calculation prior to issuing an exportation license and allowing the samples to be dispatched. • The samples were then sent using a commercial transport company (Deugro) to Perth and delivered directly to the laboratory after quarantine inspection and heat treatement for the samples < 3m depth • The laboratory inspected the packages and did not report tampering of the samples
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• Internal reviews were undertaken

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.*	• The exploration work was completed on tenements that are 100% owned by the Company in Tanzania or are able to be acquired for 100% ownership • The drill samples were taken from tenements PL 9969/2014 and PL 11131/2016. • The tenements have not exceeded 4 years but PL 9969 will require a renewal for an additional 3 years in July 2018. At least 50% of the area will also need to be surrendered. • Traditional landowners and village Chiefs of the affected villages and farms were consulted supportive of the drilling program
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• Historic exploration work was completed by Tanganyika Gold in 1998 and 1999. The Company has obtained the hardcopy reports and maps in relation to this Tanganyika and OmegaCorp information • The historic data comprises surface sampling and mapping • There has been very little to none modern based exploration for mineral sands in southern Tanzania
Geology	• *Deposit type, geological setting and style of mineralisation.*	• Two types of heavy mineral placer style deposits are possible in Tanzania 1. Thin but high grade strandlines which may be related to marine or fluvial influences 2. Large but lower grade deposits related to windblown sands • The coastline of Tanzania is not well known for massive dunal systems such as those developed in Mozambique, however some dunes are known to occur and cannot be discounted as an exploration model. Palaeo strandlines are more likely and will be related to fossil shorelines or terraces in a marine or fluvial setting. In Tanzania three terraces have been documented and include the Mtoni terrace (1-5m ASL), Tanga (20-40m ASL) and Sakura Terrace (40 to 60m ASL). Strandline mineral sand accumulations related to massive storm events are thought to be preserved at these terraces above the current sea level.

Criteria	JORC Code explanation	Commentary
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* o *easting and northing of the drill hole collar* o *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* o *dip and azimuth of the hole* o *down hole length and interception depth* o *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• The drill hole data are reported in Appendix 2.
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Length weighted intervals are reported in this release • Significant results are reported > 3% THM. • Completed down hole averages are reported in Appendix 2
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	• The nature of the mineralisation is broadly horizontal, thus vertical aircore holes are thought to represent close to true thicknesses of the mineralisation • Downhole widths are reported
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• Figures and plans are displayed in the main text of the Release
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• All material results have been reported and tabulated in Appendices 2.

Criteria	JORC Code explanation	Commentary
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Mineral assemblage work for the Sudi project has been completed and presented in this release. • Detailed airborne geophysical surveys have also been completed over the prospective target horizons across tenements PL 9969 and 11131. The surveys were flown by Geotech between August and September 2016. • The survey was flown using: Principal geophysical sensors included three geometrics high-sensitivity cesium magnetometers, fluxgate reference magnetometer, three RSI ARGS RSX-5 spectrometers and a RMS DAARC500 Adaptive Aeromagnetic Real Time Compensator – three magnetometers input with gradiometer capability. Ancillary equipment included a GPS navigation system and a radar altimeter • The survey was flown at a nominal height of 30m in a 45°-225° orientation with 100m spaced lines and 1000m spaced tielines. • A Schmitt Industries AR300 laser altimeter was used which has an altitude range 0.5 to 300m and accuracy ±5cm • The topographic data was gridded and elevation 1m accurate contours generated. The data was used to identify breaks in slope – nick points along the broadly coastal parallel sequence of small hills • Thorium was also used to identify areas of potential elevated zircon content. However not all of the Thorium anomalies were related to heavy mineral sands with several anomalies related to Th enrichment in clay horizons.
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Additional Aircore drilling is planned for the 2018 field season commencing after the wet season. • A bulk sample comprising 400 kg has been collected and will be used to assess process recoveries and potential final product specification for the Sudi mineralization.

Appendix 2 – Downhole Drill Intersects

Appendix 2 – Downhole Drill Intersects

HOLE_ID	UTM E (WGS84)	UTM N (WGS84)	RI	DIP	AZim	EOH (m)	FROM (m)	TO (m)	Interval (m)	THM (%)	SLIME (%)	OVERSIZE (%)
17SDAC5000	596788	8873499	130	-90	360	16.5	0	16.5	16.5	0.7	40	5
17SDAC5001	597128	8873699	126	-90	360	6	0	6	6	0.7	32	15
17SDAC5002	597505	8873790	118	-90	360	4.5	0	4.5	4.5	0.7	32	24
17SDAC5003	597804	8874060	108	-90	360	9	0	9	9	0.8	31	8
17SDAC5004	597958	8874434	97	-90	360	24	0	24	24	0.5	44	15
17SDAC5005	598238	8874670	91	-90	360	4.5	0	4.5	4.5	1.2	40	25
17SDAC5006	598398	8874837	94	-90	360	12	0	12	12	2.9	30	6
17SDAC5007	598547	8874907	99	-90	360	13.5	0	13.5	13.5	2.2	32	6
17SDAC5008	598750	8874986	100	-90	360	30	0	30	30	1.3	15	8
17SDAC5009	598949	8875001	96	-90	360	16.5	0	16.5	16.5	0.8	17	22
17SDAC5010	603888	8875202	39	-90	360	6	0	6	6	1.1	33	18
17SDAC5011	603719	8875087	45	-90	360	6	0	6	6	1.3	27	18
17SDAC5012	603605	8874920	50	-90	360	6	0	6	6	2.0	23	8
17SDAC5013	603471	8874558	50	-90	360	9	0	9	9	1.0	37	6
17SDAC5014	603192	8874263	55	-90	360	12	0	12	12	1.3	27	7
17SDAC5015	600331	8872213	76	-90	360	30	0	30	30	0.5	92	2
17SDAC5016	600192	8871867	82	-90	360	15	0	15	15	0.2	42	8
17SDAC5017	600066	8871572	85	-90	360	9	0	9	9	0.4	26	13
17SDAC5018	599292	8875208	82	-90	360	12	0	12	12	1.6	22	12
17SDAC5019	599575	8875495	80	-90	360	16.5	0	16.5	16.5	1.6	25	4
17SDAC5020	599907	8875721	70	-90	360	13.5	0	13.5	13.5	2.7	21	9
17SDAC5021	600306	8875889	70	-90	360	12	0	12	12	0.8	26	12
17SDAC5022	599439	8877384	55	-90	360	16.5	0	16.5	16.5	1.4	10	17
17SDAC5023	599603	8877510	49	-90	360	3	0	3	3	1.2	13	12
17SDAC5024	599752	8877641	46	-90	360	6	0	6	6	1.4	15	16
17SDAC5025	599909	8877771	44	-90	360	6	0	6	6	0.9	19	20
17SDAC5026	600060	8877894	40	-90	360	6	0	6	6	1.0	25	13
17SDAC5027	600365	8878152	37	-90	360	24	0	24	24	0.3	26	27
17SDAC5028	600674	8878403	35	-90	360	9	0	9	9	0.8	15	14
17SDAC5029	599135	8877130	63	-90	360	15	0	15	15	1.3	15	16
17SDAC5030	598829	8876879	83	-90	360	36	0	36	36	2.8	11	10
17SDAC5031	598672	8876746	92	-90	360	30	0	30	30	1.5	11	6
17SDAC5032	598524	8876624	96	-90	360	18	0	18	18	1.4	15	4
17SDAC5033	596908	8880450	82	-90	360	16.5	0	16.5	16.5	1.4	14	5
17SDAC5034	597203	8880735	62	-90	360	6	0	6	6	1.1	19	7
17SDAC5035	597494	8880988	53	-90	360	12	0	12	12	0.6	25	15
17SDAC5036	596593	8880170	91	-90	360	10.5	0	10.5	10.5	0.9	21	8
17SDAC5037	596327	8879911	94	-90	360	30	0	30	30	1.0	15	12
17SDAC5038	596025	8879644	104	-90	360	16.5	0	16.5	16.5	0.7	21	5
17SDAC5039	595739	8879368	113	-90	360	16.5	0	16.5	16.5	1.7	17	6
17SDAC5040	595448	8879098	123	-90	360	16.5	0	16.5	16.5	1.3	26	5
17SDAC5041	595156	8878819	132	-90	360	16.5	0	16.5	16.5	1.0	24	5

HOLE_ID	UTM E (WGS84)	UTM N (WGS84)	Rl	DIP	AZim	EOH (m)	FROM (m)	TO (m)	Interval (m)	THM (%)	SLIME (%)	OVERSIZE (%)
17SDAC5042	594855	8878550	137	-90	360	16.5	0	16.5	16.5	1.0	27	7
17SDAC5043	594557	8878271	139	-90	360	12	0	12	12	1.1	36	12
17SDAC5044	598984	8876996	71	-90	360	30	0	30	30	1.5	8	6
17SDAC5045	594421	8878143	141	-90	360	10.5	0	10.5	10.5	1.0	36	11
17SDAC5046	594272	8878005	149	-90	360	12	0	12	12	1.3	39	10
17SDAC5047	594125	8877881	148	-90	360	24	0	24	24	1.0	29	15
17SDAC5048	593978	8877736	156	-90	360	3	0	3	3	1.1	41	13
17SDAC5049	593843	8877606	163	-90	360	6	0	6	6	1.2	51	8
17SDAC5050	593685	8877464	168	-90	360	9	0	9	9	1.3	42	14
17SDAC5051	593390	8877191	177	-90	360	9	0	9	9	1.1	47	10
17SDAC5052	593094	8876919	187	-90	360	15	0	15	15	0.8	34	22
17SDAC5053	592574	8882823	94	-90	360	10.5	0	10.5	10.5	1.0	25	14
17SDAC5054	592298	8882535	102	-90	360	9	0	9	9	0.9	28	19
17SDAC5055	592140	8882386	112	-90	360	12	0	12	12	1.2	28	13
17SDAC5056	591864	8882103	130	-90	360	12	0	12	12	0.7	28	17
17SDAC5057	591722	8881956	137	-90	360	30	0	30	30	1.0	25	7
17SDAC5058	592011	8882243	142	-90	360	16.5	0	16.5	16.5	1.3	20	11
17SDAC5059	591579	8881819	321	-90	360	12	0	12	12	1.1	20	23
17SDAC5060	591442	8881671	322	-90	360	16.5	0	16.5	16.5	0.8	24	20
17SDAC5061	591164	8881382	331	-90	360	9	0	9	9	0.7	26	17
17SDAC5062	590887	8881123	166	-90	360	16.5	0	16.5	16.5	0.8	19	20
17SDAC5063	590596	8880832	182	-90	360	16.5	0	16.5	16.5	0.9	20	18
17SDAC5064	592857	8883089	115	-90	360	16.5	0	16.5	16.5	1.1	31	12
17SDAC5065	593134	8883371	114	-90	360	10.5	0	10.5	10.5	0.7	21	16
17SDAC5066	593419	8883667	109	-90	360	10.5	0	10.5	10.5	0.5	25	17
17SDAC5067	593698	8883937	104	-90	360	3	0	3	3	0.7	21	6
17SDAC5068	593983	8884210	93	-90	360	3	0	3	3	0.8	22	18
17SDAC5069	594125	8884374	89	-90	360	4.5	0	4.5	4.5	1.4	35	3
17SDAC5070	594259	8884502	89	-90	360	1.5	0	1.5	1.5	1.2	15	8
17SDAC5071	594541	8884815	84	-90	360	1.5	0	1.5	1.5	0.9	17	21
17SDAC5072	590708	8884242	96	-90	360	7.5	0	7.5	7.5	0.7	33	28
17SDAC5073	590598	8884137	97	-90	360	10.5	0	10.5	10.5	1.0	23	25
17SDAC5074	590409	8883967	100	-90	360	9	0	9	9	0.7	25	26
17SDAC5075	590305	8883874	104	-90	360	3	0	3	3	0.5	17	34
17SDAC5076	590113	8883739	109	-90	360	27	0	27	27	1.2	21	17
17SDAC5077	589954	8883607	120	-90	360	16.5	0	16.5	16.5	1.0	22	20
17SDAC5078	589800	8883477	132	-90	360	16.5	0	16.5	16.5	1.2	23	18
17SDAC5079	589485	8883220	145	-90	360	16.5	0	16.5	16.5	0.6	19	25
17SDAC5080	589181	8882959	156	-90	360	24	0	24	24	0.6	17	24
17SDAC5081	588874	8882709	174	-90	360	16.5	0	16.5	16.5	0.7	19	26
17SDAC5082	597715	8878276	92	-90	360	30	0	30	30	1.2	9	9
17SDAC5083	597873	8878423	80	-90	360	18	0	18	18	1.2	12	9
17SDAC5084	598029	8878530	75	-90	360	30	0	30	30	1.6	10	7

HOLE_ID	UTM E (WGS84)	UTM N (WGS84)	Rl	DIP	AZim	EOH (m)	FROM (m)	TO (m)	Interval (m)	THM (%)	SLIME (%)	OVERSIZE (%)
17SDAC5085	598163	8878683	72	-90	360	18	0	18	18	1.7	8	10
17SDAC5086	598339	8878775	64	-90	360	16.5	0	16.5	16.5	1.1	9	11
17SDAC5087	598487	8878910	59	-90	360	24	0	24	24	1.0	9	11
17SDAC5088	598641	8879035	46	-90	360	16.5	0	16.5	16.5	1.0	19	8
17SDAC5089	598804	8879148	45	-90	360	16.5	0	16.5	16.5	0.7	8	18
17SDAC5090	598949	8879285	41	-90	360	6	0	6	6	0.4	21	33
17SDAC5091	599295	8877235	57	-90	360	10.5	0	10.5	10.5	1.4	13	15
17SDAC5092	601429	8873980	67	-90	360	16.5	0	16.5	16.5	1.3	21	16
17SDAC5093	601577	8874109	77	-90	360	24	0	24	24	1.7	29	13
17SDAC5094	601735	8874237	66	-90	360	16.5	0	16.5	16.5	1.3	26	11
17SDAC5095	601885	8874346	62	-90	360	16.5	0	16.5	16.5	0.9	27	12
17SDAC5096	601319	8873808	72	-90	360	9	0	9	9	1.5	16	5
17SDAC5097	592748	8882925	84	-90	360	30	0	30	30	0.9	25	15
17SDAC5098	597060	8880595	73	-90	360	25.5	0	25.5	25.5	0.5	16	25
17SDAC5099	593979	8877732	153	-90	360	30	0	30	30	0.9	29	11
17SDAC5100	597583	8878134	94	-90	360	30	0	30	30	0.5	11	15
17SDAC5101	599763	8875587	68	-90	360	18	0	18	18	1.0	21	24
17SDAC5102	600071	8875812	66	-90	360	27	0	27	27	1.0	17	24
17SDAC5103	611442	8872590	34	-90	360	12	0	12	12	0.1	31	30
17SDAC5104	611523	8872189	30	-90	360	9	0	9	9	0.2	24	36
17SDAC5105	611571	8871788	34	-90	360	24	0	24	24	0.1	40	15
17SDAC5106	611631	8871388	43	-90	360	9	0	9	9	0.4	25	23
17SDAC5107	611682	8870989	53	-90	360	15	0	15	15	0.4	25	17
17SDAC5108	611743	8870591	69	-90	360	16.5	0	16.5	16.5	0.3	18	6
17SDAC5296	597133	8875475	88	-90	360	12	0	12	12	0.6	39	18
17SDAC5297	597458	8875707	78	-90	360	19.5	0	19.5	19.5	0.6	49	18
17SDAC5298	597746	8875969	99	-90	360	22.5	0	22.5	22.5	1.1	16	9
17SDAC5299	598080	8876226	87	-90	360	19.5	0	19.5	19.5	0.9	12	5
17SDAC5300	598385	8876494	95	-90	360	19.5	0	19.5	19.5	0.8	14	16
17SDAC5301	597099	8876444	120	-90	360	19.5	0	19.5	19.5	0.7	14	27
17SDAC5302	597403	8876689	123	-90	360	30	0	30	30	1.1	18	6
17SDAC5303	597712	8876959	108	-90	360	24	0	24	24	0.7	18	4
17SDAC5304	598014	8877206	113	-90	360	19.5	0	19.5	19.5	0.6	13	33
17SDAC5305	598170	8877312	112	-90	360	19.5	0	19.5	19.5	1.2	14	7
17SDAC5306	598335	8877441	87	-90	360	24	0	24	24	1.6	13	7
17SDAC5307	598479	8877566	81	-90	360	24	0	24	24	1.5	10	11
17SDAC5308	598636	8877712	79	-90	360	30	0	30	30	1.0	10	7
17SDAC5309	598781	8877835	81	-90	360	19.5	0	19.5	19.5	1.7	8	10
17SDAC5310	598939	8877965	78	-90	360	19.5	0	19.5	19.5	1.2	11	16
17SDAC5311	599096	8878096	78	-90	360	19.5	0	19.5	19.5	0.9	17	13
17SDAC5312	599252	8878216	75	-90	360	19.5	0	19.5	19.5	1.2	17	15
17SDAC5313	599411	8878358	76	-90	360	30	0	30	30	0.7	11	11
17SDAC5314	599556	8878454	73	-90	360	19.5	0	19.5	19.5	0.7	20	16

HOLE_ID	UTM E (WGS84)	UTM N (WGS84)	Rl	DIP	AZim	EOH (m)	FROM (m)	TO (m)	Interval (m)	THM (%)	SLIME (%)	OVERSIZE (%)
17SDAC5315	596783	8876168	89	-90	360	6	0	6	6	1.3	33	10
17SDAC5316	596472	8875949	105	-90	360	19.5	0	19.5	19.5	0.7	29	19
17SDAC5317	597385	8877698	82	-90	360	19.5	0	19.5	19.5	0.3	12	47
17SDAC5318	597085	8877466	91	-90	360	19.5	0	19.5	19.5	0.6	21	11
17SDAC5319	596727	8877200	108	-90	360	30	0	30	30	0.9	15	11
17SDAC5320	596467	8876955	114	-90	360	19.5	0	19.5	19.5	0.8	27	7
17SDAC5321	596172	8876687	128	-90	360	19.5	0	19.5	19.5	0.9	34	5
17SDAC5322	597192	8874488	143	-90	360	12	0	12	12	0.6	33	21
17SDAC5323	597496	8874737	128	-90	360	19.5	0	19.5	19.5	1.2	38	8
17SDAC5324	597794	8874997	84	-90	360	10.5	0	10.5	10.5	1.9	37	11
17SDAC5325	597946	8875121	80	-90	360	12	0	12	12	2.7	37	8
17SDAC5326	598109	8875243	80	-90	360	30	0	30	30	1.5	52	15
17SDAC5327	598283	8875359	94	-90	360	19.5	0	19.5	19.5	1.5	56	7
17SDAC5328	600118	8876906	50	-90	360	9	0	9	9	0.6	22	38
17SDAC5329	600262	8877030	49	-90	360	33	0	33	33	0.8	18	19
17SDAC5330	599963	8876789	59	-90	360	19.5	0	19.5	19.5	1.1	15	21
17SDAC5331	599799	8876654	71	-90	360	19.5	0	19.5	19.5	1.6	12	13
17SDAC5332	599649	8876513	79	-90	360	19.5	0	19.5	19.5	1.2	19	17
17SDAC5333	599483	8876368	89	-90	360	19.5	0	19.5	19.5	1.0	22	22
17SDAC5334	599352	8876255	106	-90	360	36	0	36	36	2.0	15	10
17SDAC5335	599193	8876146	112	-90	360	24	0	24	24	2.0	16	12
17SDAC5336	599048	8876001	118	-90	360	21	0	21	21	2.1	14	9
17SDAC5337	598883	8875878	84	-90	360	19.5	0	19.5	19.5	0.9	13	21
17SDAC5338	598743	8875746	82	-90	360	19.5	0	19.5	19.5	0.6	13	5
17SDAC5339	598591	8875636	90	-90	360	19.5	0	19.5	19.5	0.8	15	36
17SDAC5340	598435	8875495	101	-90	360	19.5	0	19.5	19.5	1.3	43	10
17SDAC5341	603307	8875477	68	-90	360	19.5	0	19.5	19.5	0.8	23	28
17SDAC5342	602973	8875211	80	-90	360	30	0	30	30	1.1	22	12
17SDAC5343	602703	8874950	83	-90	360	19.5	0	19.5	19.5	1.0	26	14
17SDAC5344	602350	8874697	82	-90	360	19.5	0	19.5	19.5	1.4	26	11
17SDAC5345	601950	8875357	48	-90	360	19.5	0	19.5	19.5	0.7	28	12
17SDAC5346	601649	8875117	55	-90	360	30	0	30	30	1.0	23	17
17SDAC5347	601329	8874862	63	-90	360	24	0	24	24	0.9	28	12
17SDAC5348	601025	8874614	77	-90	360	27	0	27	27	1.7	25	15
17SDAC5349	600872	8874476	86	-90	360	21	0	21	21	1.7	20	23
17SDAC5350	600718	8874348	96	-90	360	19.5	0	19.5	19.5	2.2	18	7
17SDAC5351	600547	8874220	102	-90	360	21	0	21	21	2.0	17	6
17SDAC5352	600418	8874083	70	-90	360	19.5	0	19.5	19.5	0.9	13	9
17SDAC5353	600262	8873976	69	-90	360	24	0	24	24	0.9	19	8
17SDAC5354	600116	8873842	77	-90	360	19.5	0	19.5	19.5	0.9	13	6
17SDAC5355	599938	8873709	92	-90	360	30	0	30	30	1.0	19	18
17SDAC5356	599819	8873578	100	-90	360	19.5	0	19.5	19.5	1.3	19	13
17SDAC5357	599658	8873481	98	-90	360	19.5	0	19.5	19.5	1.3	20	10

HOLE_ID	UTM E (WGS84)	UTM N (WGS84)	Rl	DIP	AZim	EOH (m)	FROM (m)	TO (m)	Interval (m)	THM (%)	SLIME (%)	OVERSIZE (%)
17SDAC5358	601111	8875711	70	-90	360	30	0	30	30	1.3	15	12
17SDAC5359	600829	8875436	65	-90	360	19.5	0	19.5	19.5	0.4	46	9
17SDAC5360	600510	8875199	40	-90	360	19.5	0	19.5	19.5	0.8	32	9
17SDAC5361	600340	8875049	51	-90	360	19.5	0	19.5	19.5	1.0	26	13
17SDAC5362	600189	8874946	61	-90	360	19.5	0	19.5	19.5	0.7	22	15
17SDAC5363	600051	8874819	67	-90	360	19.5	0	19.5	19.5	1.1	15	8
17SDAC5364	599923	8874668	78	-90	360	19.5	0	19.5	19.5	1.3	19	6
17SDAC5365	599732	8874556	87	-90	360	19.5	0	19.5	19.5	1.0	23	8
17SDAC5366	602066	8874452	87	-90	360	19.5	0	19.5	19.5	0.9	22	12