

# SPECTACULAR EXPLORATION RESULTS SET UP JUNDEE FOR +10-YEAR LIFE

Jundee Goldfield emerging as one of the greatest gold fields in Australia with multiple new discoveries in a 35km radius of the mine

## KEY POINTS

- ▶ Northern Star has made multiple new gold discoveries at and around its Jundee gold mine in WA where the total endowment has reached 10Moz
- ▶ These discoveries are characterised by extremely high-grades and extend over significant dimensions of up to 2km each
- ▶ They include the Zodiac discovery 800m to the East of the Jundee mine, new significant results include 0.5m at 765gpt
- ▶ Mineralisation at Zodiac has been defined over 2km and remains open in all directions
- ▶ Northern Star is now drilling what will be one of the deepest holes in Australian gold history; this hole is targeting two additional seismic reflectors below Zodiac, which has already returned grades up to 765gpt
- ▶ Zodiac and these two additional reflectors all have potential to extend up-plunge to the surface and are therefore considered to have significant upside
- ▶ Sensational deeper results down-plunge from the main Jundee Dolerite still to follow up on (past production 3.4Moz at 10gpt); results include:
  - 0.4m @ 611gpt, 0.3m @ 380gpt and 0.4m @ 142gpt (true width)
- ▶ The Armada trend, located 400m west of Jundee, has grown to 2.5km strike; recent results include:
  - 14m @ 7.7gpt, 10m @ 7.7gpt and 6.8m @ 8.2gpt (true width)
- ▶ Within the Armada trend, drilling has significantly extended the Revelation/Nexus portion with recent results including:
  - 0.4m @ 305gpt, 0.3m @ 295gpt and 1m @ 88.1gpt (true width)
- ▶ At the Gateway 5100 lode, drilling has returned spectacular results close to surface, including:
  - 1.2m @ 957gpt, 6.9m @ 49gpt and 11m @ 21.1gpt (true width)
- ▶ Significant surface discovery at Ramone, 35km south of Jundee mine; Ramone already has potential to be an open pit mine with mineralisation outlined over 400m strike so far; results include:
  - 14m @ 8.0gpt, 13m @ 8.5gpt and 18.5m @ 6.2gpt (true width)
- ▶ In light of this combined exploration success, Northern Star expects Jundee's current Reserves of 1.4Moz to grow substantially as drilling continues
- ▶ To accelerate this growth in Jundee's Reserves, the FY2018 group exploration budget has been increased by A\$10M to A\$45M

### ASX ANNOUNCEMENT 20 February 2018

Australian Securities  
Exchange Code: NST

#### Board of Directors

Mr Bill Beament  
*Executive Chairman*

Mr Chris Rowe  
*Non-Executive Director*

Mr Peter O'Connor  
*Non-Executive Director*

Mr John Fitzgerald  
*Non-Executive Director*

Ms Shirley In'tVeld  
*Non-Executive Director*

Mr David Flanagan  
*Non-Executive Director*

#### Issued Capital

Shares 603.2 million  
Options 0.8 million  
Performance Rights 10 million

Current Share Price A\$6.10

Market Capitalisation  
A\$3.7 billion

Cash, Bullion & Investments  
31 Dec 2017 - A\$433.1 million

#### Projects

Paulsens Mine  
Kanowna Belle Mine  
Kundana Mine  
Kundana Mines (51% of EKJV)  
Jundee Mine  
Central Tanami (25% of JV)  
Western Tanami

#### Listed Investments

ASX: VXR, DAU, RND, TBR, ALY, EAR  
TSX-V: SGI

► **Kalgoorlie operations;**

- **Kundana (NST 100%): Millennium mine infill and definition drilling achieved strong results including: 1.8m @ 80.4gpt, 1.6m @ 73.2gpt and 2.2m @ 29.4gpt (true width)**
- **Significant exploration success at Barker's and Strzelecki veins extends their mineralisation interpretation down-plunge by 200m and 400m respectively**
- **Kundana EJKV (NST 51%): in-mine extensional drilling across Rubicon-Hornet-Pegasus lodes has significantly expanded the mineralised systems in the hanging wall. Results include: 4.5m @ 17.7gpt, 5.3m @ 6.7gpt and 10.0m @ 9.9gpt (true width)**
- **Deepest mineralised intercept to date at EKJV, 1km below surface, of 2.95m @ 13gpt**
- **Pode has been significantly extended both down dip and to the north with spectacular results including 3.1m @ 1184gpt, 3.4m @ 19.2gpt and 2.1m @ 28.7gpt (true width)**
- **Significant drill results achieved in Resource extension drilling at Kanowna Belle throughout all current mining blocks, A through to E**
- **Kanowna's Velvet lode continues to substantially grow with significant result including:**
  - 31.3m @ 21.7gpt, 15.8m @ 9.5gpt and 5.5m @ 17.8gpt (true width)
- **Drilling below current Kanowna underground workings is underway, early results are very encouraging with significant results including:**
  - 9.4m @ 8.0gpt, 10.0m @ 15.0gpt and 7.2m @ 8.4gpt (down hole width)
- **Significant strike extensions at Paradigm from the Resource boundary, results include:**
  - 0.3m @ 427gpt, 0.4m @ 260.5gpt and 4.3m @ 19.5gpt (true width)

Northern Star Resources Limited (ASX: NST) is pleased to announce a series of spectacular exploration results which show that it is set to establish a 10-year life at its 10Moz endowed Jundee Gold Project in WA.

The results include new discoveries with huge potential and extensions to recent discoveries.

Collectively, this outstanding exploration success points to a substantial increase in Jundee's current 1.4Moz Reserve.

In light of these results and their enormous potential, Northern Star has increased its total FY2018 exploration budget by A\$10 million to A\$45 million. This is aimed at accelerating the drilling programs which will enable the recent discoveries to be brought into the Reserve category.

Northern Star Executive Chairman Bill Beament said the results would change the way the 10Moz gold endowed Jundee Gold Field was viewed.

"With production of 7Moz over the past 22 years, Jundee has been an exceptional mine by any measure," Mr Beament said.

"But these results show the Jundee Gold Field is now emerging as one of the greatest gold fields in Australia.

"The Zodiac discovery is a game-changer of enormous proportions. The 765gpt intersection from the seismic reflector at Zodiac is nothing short of spectacular, particularly when the huge potential along strike is considered, and we are yet to intersect the second reflector.

"The 2.5km long Armada trend also continues to grow and we are extending the known mineralisation in a host of places in and around the mine.

"At the same time, the regional potential of the Jundee Gold Field is becoming clearer with the Ramone discovery demonstrating the wider upside.

"We are now very confident that we will grow Jundee's 1.4Moz Reserve base significantly, adding years to its mine life."

Northern Star has also enjoyed significant ongoing exploration success at its Kalgoorlie operations, where Resource drilling continues to extend the known mineralisation in numerous places.

“We have long-stated that Kalgoorlie is a Tier-One asset and these results support our view,” Mr Beament said.

“We are well on track to establishing both Jundee and Kalgoorlie as 300,000ozpa producers with long lives and low costs.

“And given that this is being driven from organic sources, our growth will flow without damaging our sector-leading financial returns.”

## **EXPLORATION OVERVIEW**

### **Jundee Mine**

In-mine Resource and exploration drilling continue to expand the known extent of all the major mining areas at Jundee while growing the new Armada trend and highlighting potential of the new Zodiac discovery to the south of the main production areas.

In-mine underground drilling in the upper levels of Gateway has defined high grade extensions to the 5100 Lode system along strike (Figure 1). The potential northern extension of this area is currently being drill tested from the surface with the program expected to be completed by the end of the current quarter.

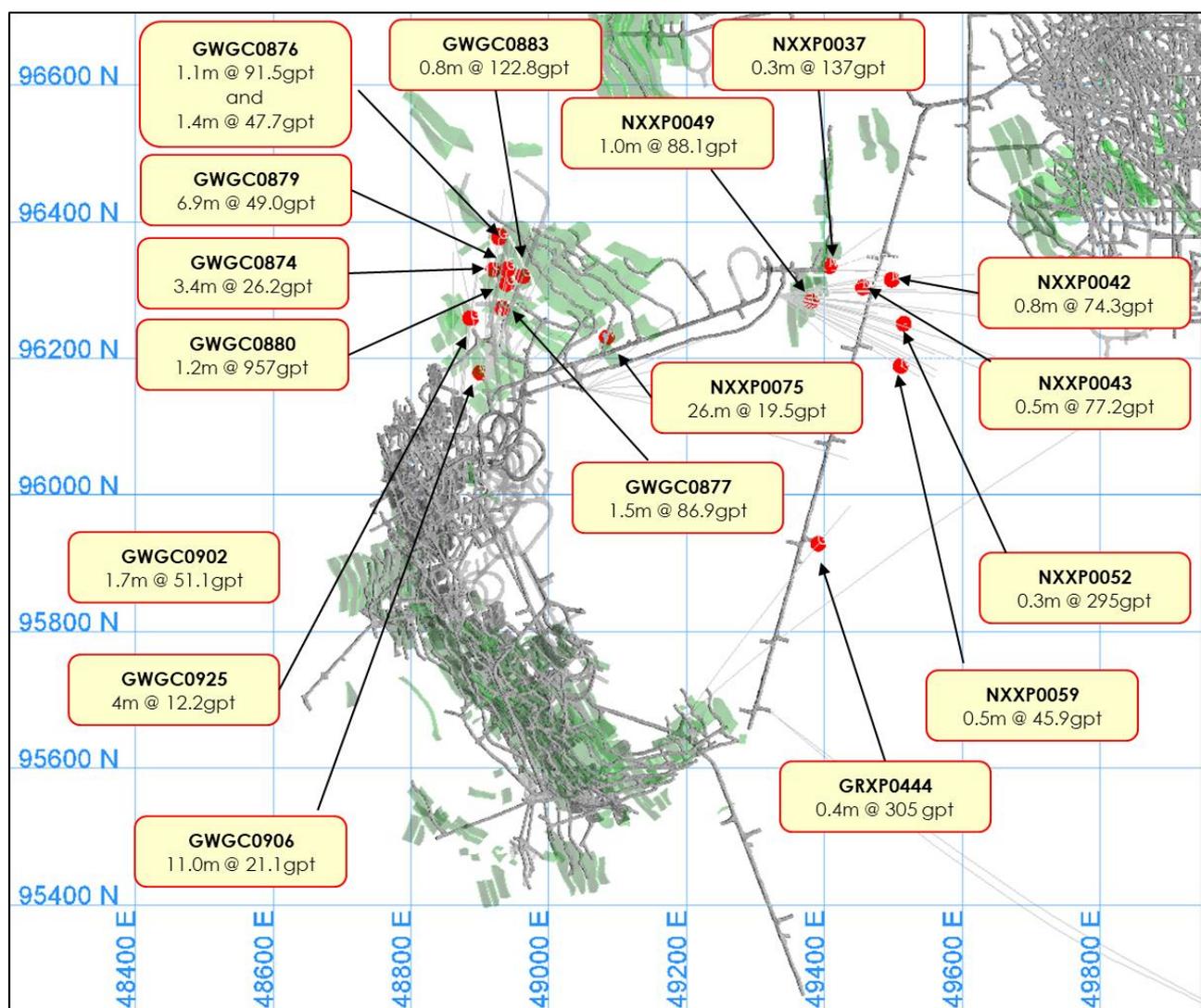


Figure 1 – Jundee Mine - Plan view Gateway-Gringotts-Nexus area with significant intersections

Adjacent to the Gateway-Gringotts area, the new Armada-Nexus-Revelation system is a major mineralised corridor in the hanging wall of the main Jundee sequence spanning some 2-3km in length. Initial extensional drilling into the Nexus-Revelation trend (Figure 1) has intersected typical high-grade Jundee mineralisation, including NXXP0059 - 0.3m at 295gpt.

With the initial underground access level into Armada completed, close spaced drilling in the initial production areas has generated strong results (Figure 2) across wide structures in the Armada trend.

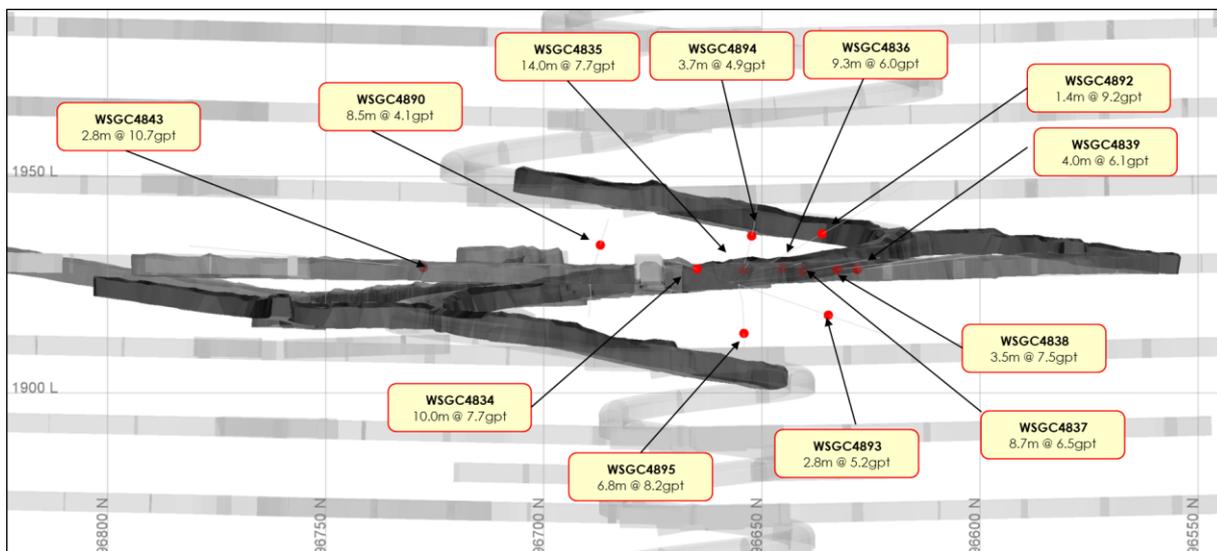


Figure 2 – Long section of central Armada development with significant intersections, planned future development shown in light colour

The entire Armada system remains open in all directions with extensional drilling in progress from the northern end of the 39Level drill drive testing the areas north of the existing Resource. In addition, testing of the entire Armada mineralised trend below the level of the existing 39Level drill drive is planned on completion of additional drilling platforms with considerable potential still to be tested.

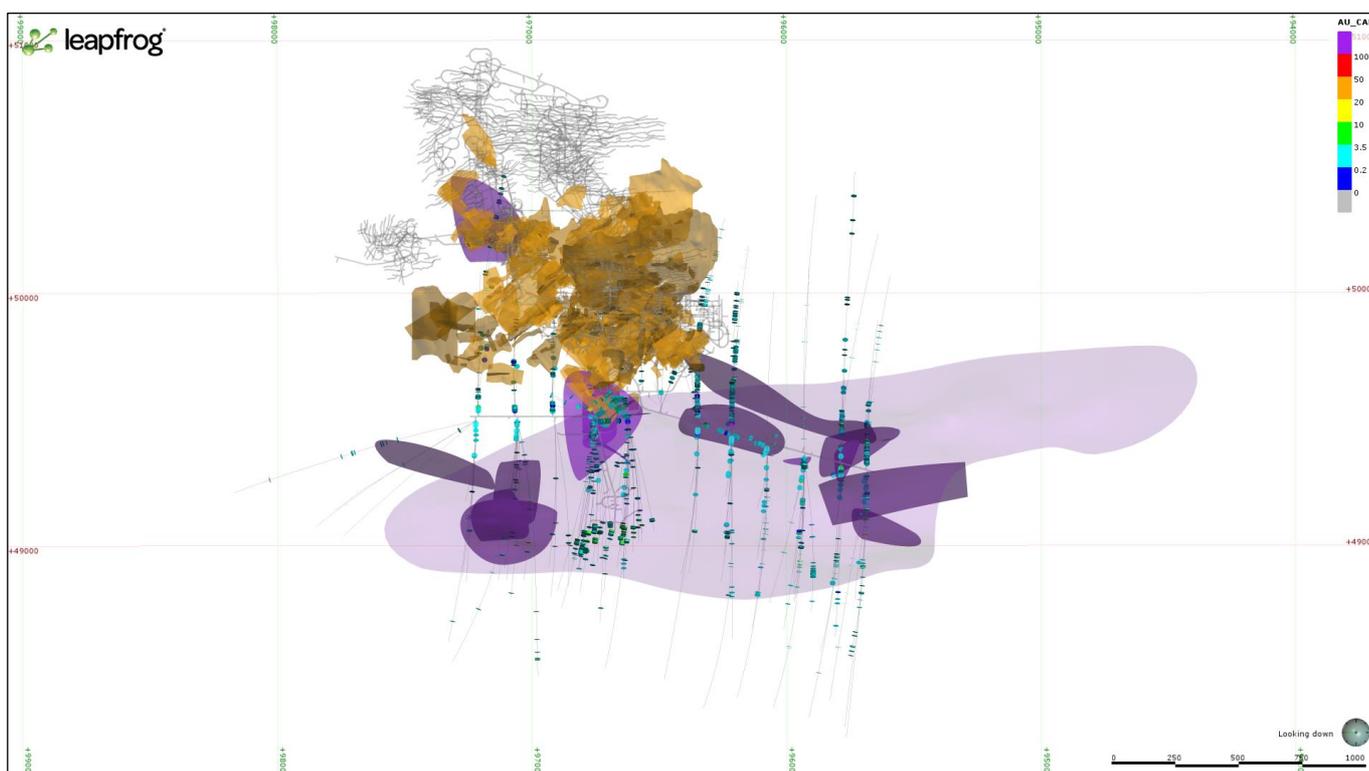


Figure 3 – Plan view – Jundee 39Level DDR drill traces with coloured discs highlighting MZ intersections. Dark purple shapes highlight new target areas from drilling to date (ex-Armada) imposed on Armada trend (pale purple shape). Westside-Barton area shown in gold.

The wide spaced exploratory drilling program from the 39Level drill drive at the base of the mine continues to progressively explore beyond the existing Jundee mine system with significant success. Post the Armada discovery, the initial fan drilling program is nearing completion with numerous high-grade intersections (see Table x) located up to 400m below the existing mine development at Westside and Barton (Figure 3). These targets highlight potential extensions to the part of the mine with historical production of 3.4Moz at ~10gpt.

## Zodiac

In August, Northern Star announced a major new discovery from the first diamond drill hole into a new target area generated from the 3D seismic program at Jundee. The Zodiac mineralisation is positioned in the footwall of the Jundee Mine, some 800m east of the existing mining infrastructure in the Gateway-Gringotts area.

An initial, very broad-spaced, diamond drilling program, from both surface and underground positions, has successfully outlined a new significant mineralised trend centred around the Stirling Fault located to the south of the main Jundee mining area.

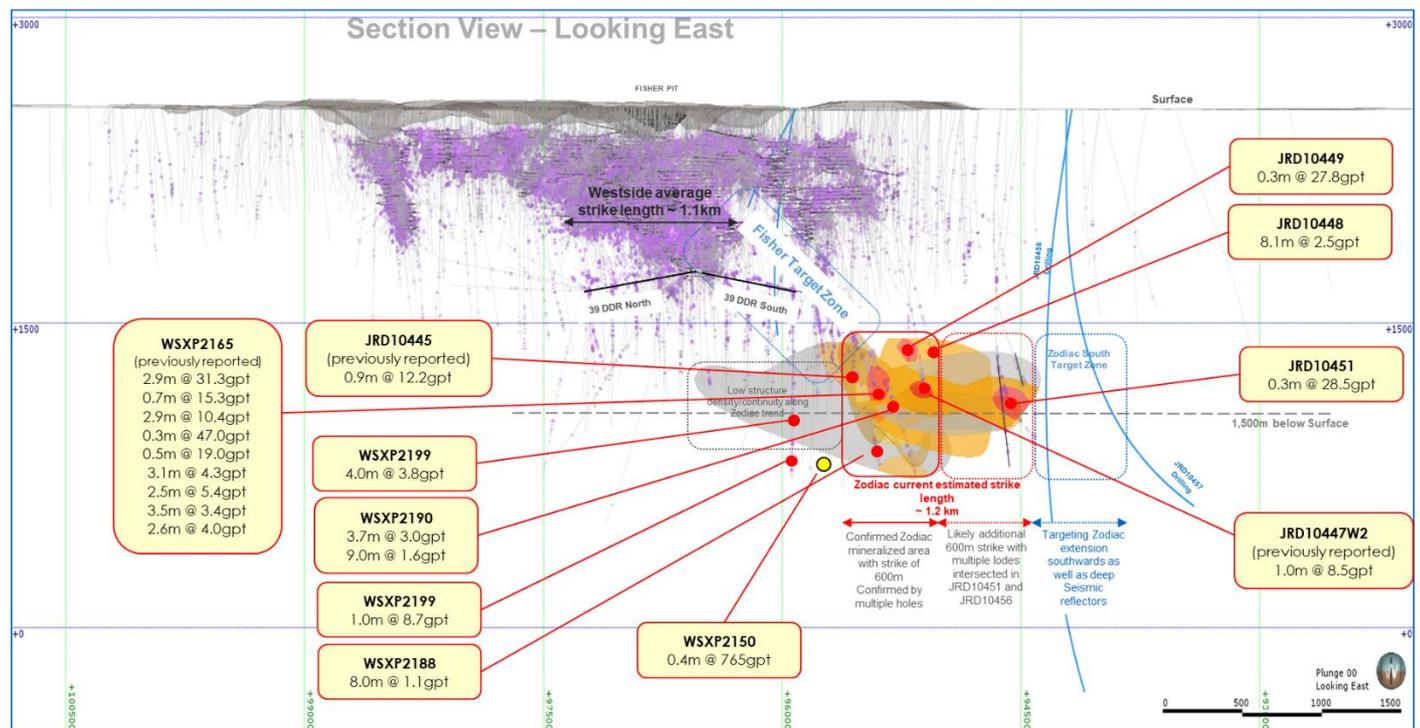


Figure 4 -Jundee Mine long section highlighting the extent of the Zodiac trend defined to date

The Zodiac system, represented by a broad zone with multiple mineralised intercepts, has been traced over a strike length of approximately 2km to date, remaining open in all directions (Figure 5). With exploration of this major new structural corridor still at a very early stage, the strength and intensity of mineralisation observed within the Zodiac system mirrors the early exploration drilling results in the major Barton-Westside and Armada systems with the Jundee area.

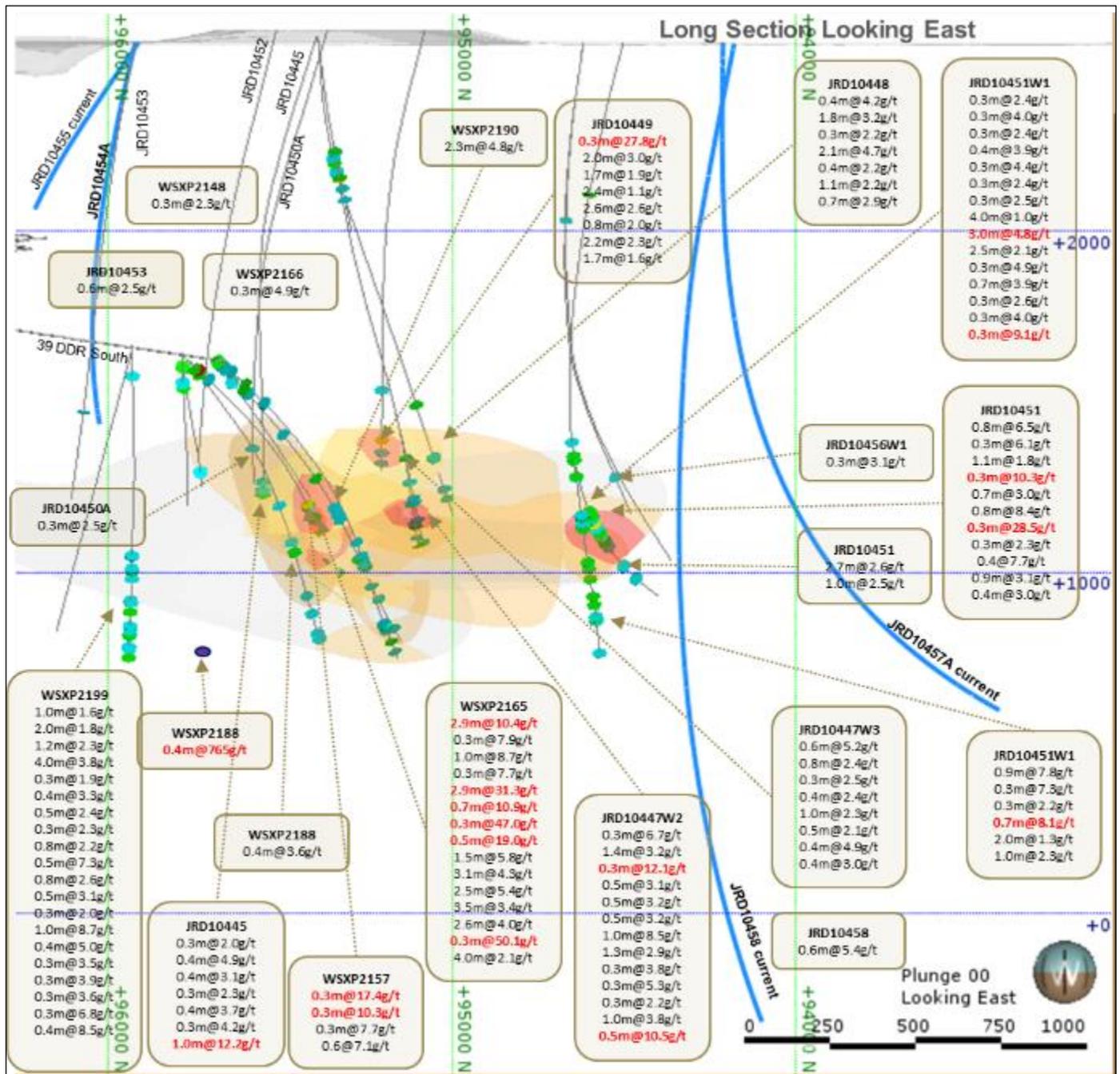


Figure 5 – Close-up long section of Zodiac target area with selected drill intersections

Zodiac represents the first of several target horizons identified from ongoing interpretation of the 3D seismic study. Two deep, step out diamond drill holes (up to 3,100m) are currently in progress targeting both southern extensions to the Zodiac trend and a package of potential targets deeper into the footwall of the recognised Jundee sequence.

Early visual indications have revealed both holes have intersected Zodiac style mineralisation at anticipated target positions with at least two additional zones of extensive veining and alteration intersected beneath the Zodiac mineralisation in the deeper drill hole. Both holes are expected to be completed in early March.

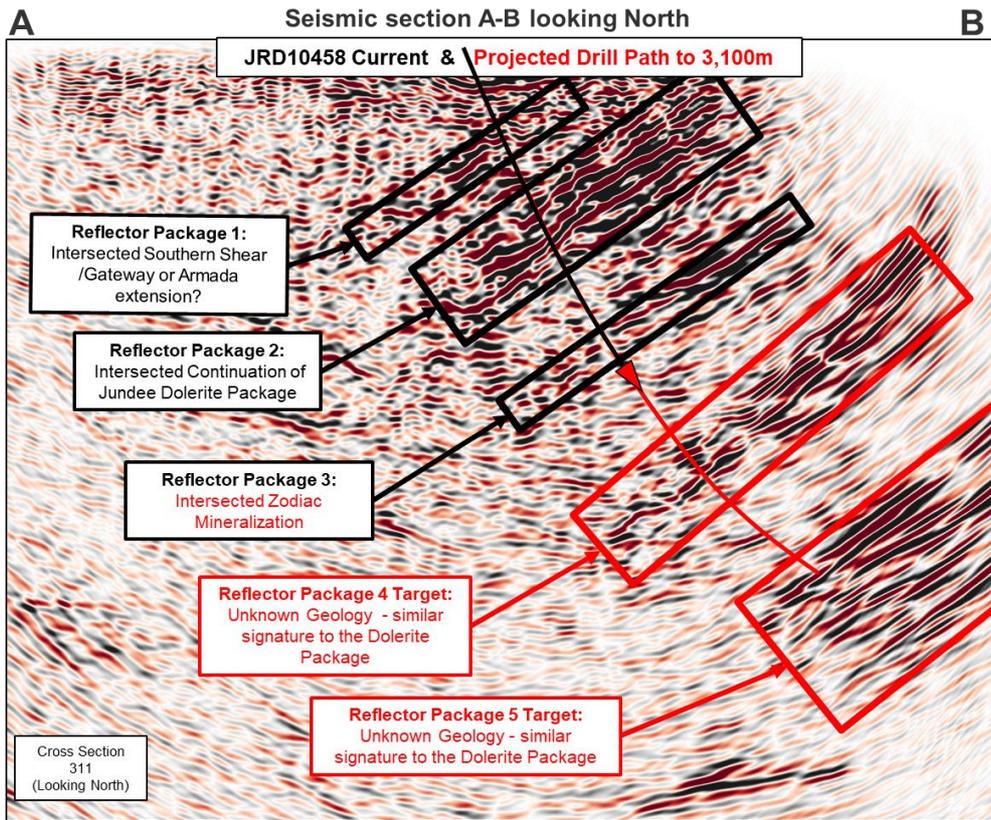


Figure 6 – Schematic 3D seismic section through Zodiac target area highlighting stacked targets

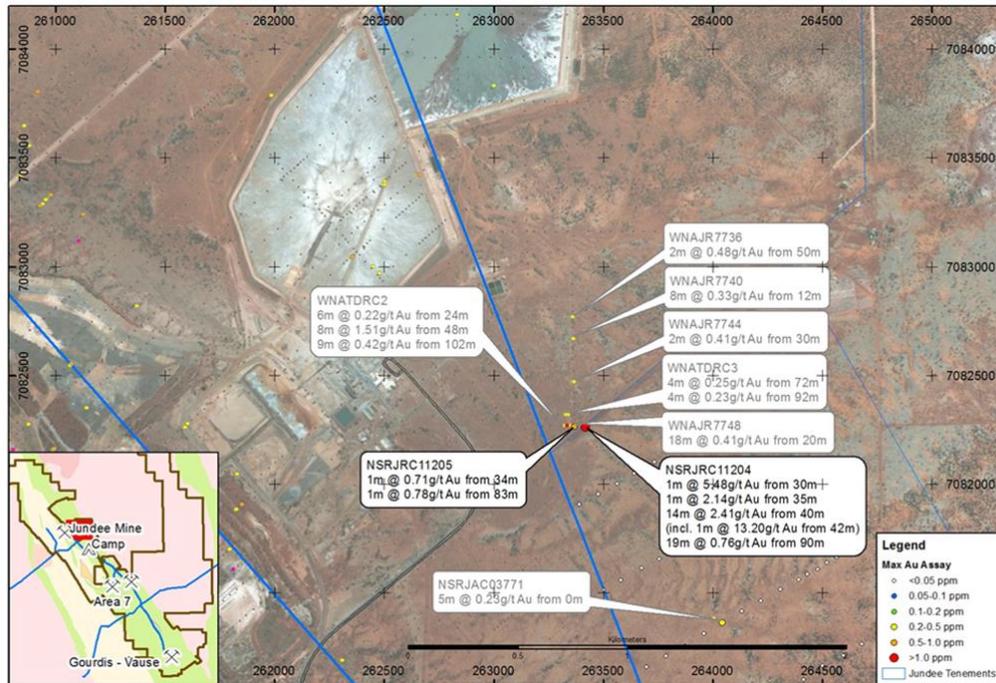


Figure 7 – Plover Bore South - Plan view of surface aircore drilling results

In addition, early reconnaissance RC drilling targeting the conceptual up dip projection of the Zodiac mineralisation has successfully intersected significant near surface mineralisation (NSRJRC11204 – 14.0m at 2.41gpt from 40m and 19m at 0.76gpt from 90m) at the Plover Bore South prospect in an area adjacent to existing surface infrastructure (Figure 7).

These results highlight the exceptional future exploration potential of the Jundee Mine opening an extensive exploration target area south and east of the Mine area.

## Regional Exploration

Across the broader Jundee region, extensive aircore drilling programs continue testing new targets generated from the geological remapping of the Jundee province in 2016.

In the Gourdis-Vause region, located 25km south of Jundee Mine area, RC drilling of an early aircore anomaly (29m @ 4.7gpt gold from surface - ASX announcement dated 7 November 2016) has intersected a significant new discovery at the Ramone prospect.

RC and diamond drilling results to date (Figure 8) have outlined a broad mineralised zone over a strike length of approximately 400m, including:

- NSRJRC11245 – 17.2m at 8.5 gpt from 38m;
- NSRJRC11249 – 22.4m at 3.4 gpt from 127m;
- NSRJRC11250 – 24.4m at 6.2 gpt from 28m; and
- NSRJRC11263 – 27.1m at 2.6 gpt from 17m. (all true width)

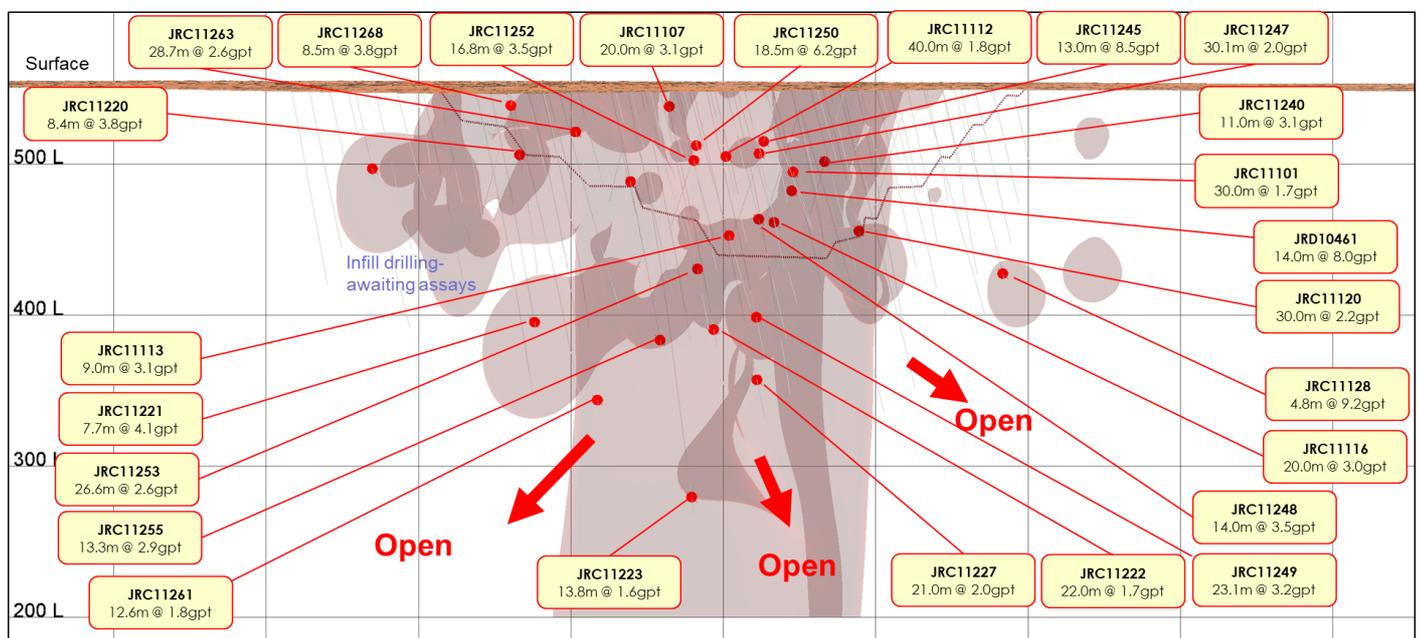


Figure 8 – Long section of Ramone prospect showing significant drill intersections with schematic mineralisation distribution

Resource definition drilling is in progress over the central area of the Ramone prospect (assays pending) with preliminary open pit Resource estimate expected to be completed in the June Quarter. Exploration of the Ramone system along strike and at depth is continuing with the mineralisation remaining open in all directions.

Elsewhere, regional aircore and RC drilling defined significant new anomalies at Gourdis West (3.3m at 3.1gpt from 114m) while north of Jundee, new significant targets were identified at Magic Dragon (5m at 2.5gpt from 20m) and Demon (5m at 1.18gpt from 30m) highlighting the considerable potential within the Jundee tenements for future discoveries (Figure 9).

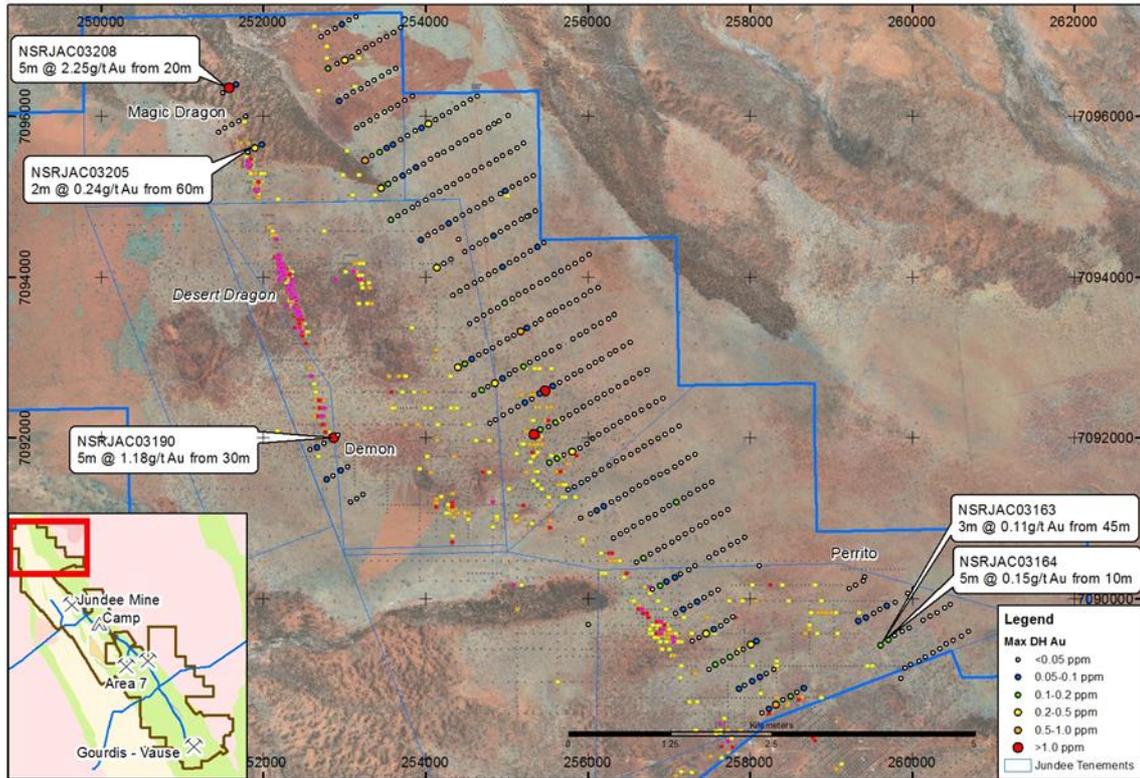


Figure 9 – Desert Dragon area aircore drill hole location plan with significant anomalies

## Kalgoorlie Gold Operations

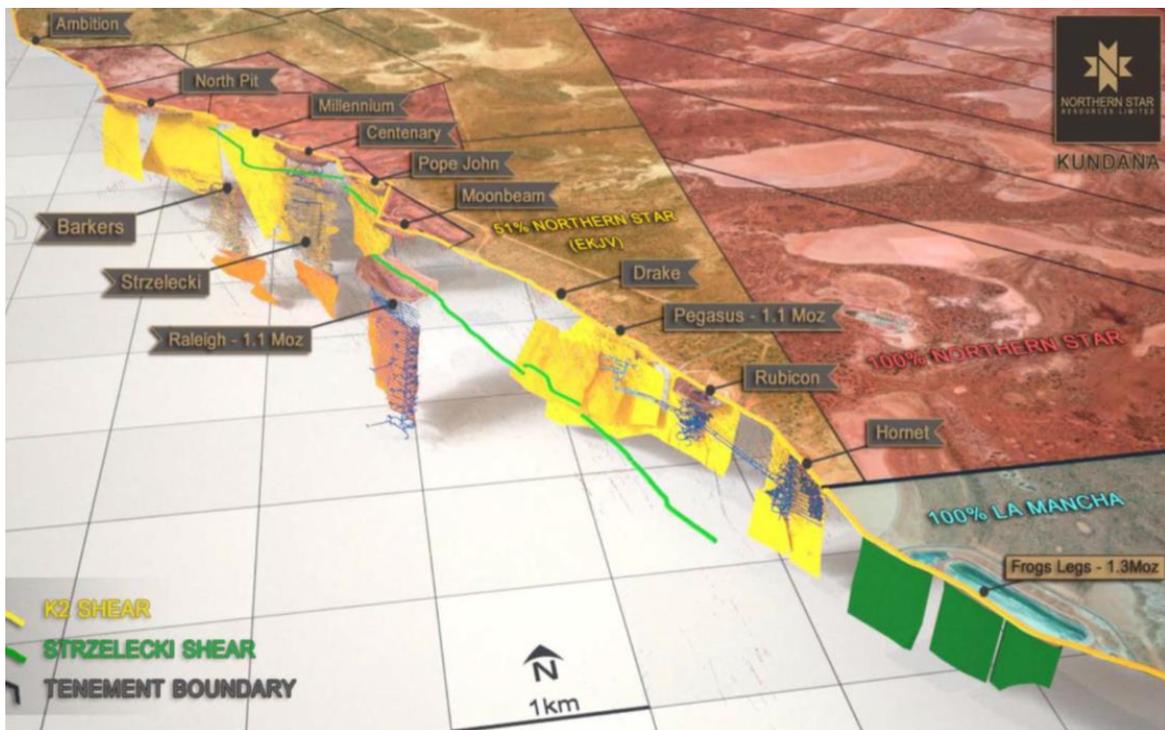


Figure 10 – Kundana and EKJV Operations Location Plan

## Kundana (NST 100%)

The 100% owned Kundana area is where Northern Star will achieve a large proportion of its overall Group production growth from FY2018 onwards.

At the new Millennium Mine, infill and definition diamond drilling underground achieved strong results (Figure 11) with mining widths increasing to the northern end.

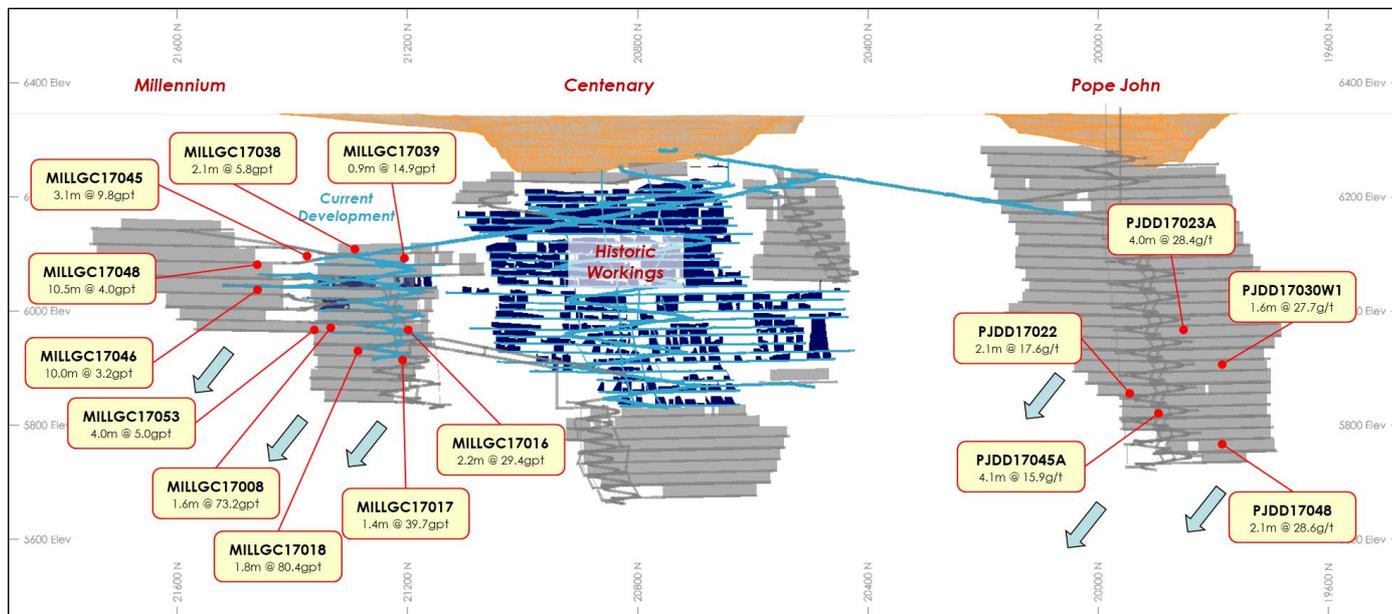


Figure 11 – Long Section of the Millennium-Centenary-Pope John complex with Millennium drilling results and previously reported Pope John drilling intersections.

At the adjacent Barker's Mine, the extensional drilling on the footwall Helga's Lode structure extended the mineralisation up-dip with excellent results typical of the Barker's Mine. Access to this area is only a short distance from the newly refurbished Barker's Mine portal providing an early production option.

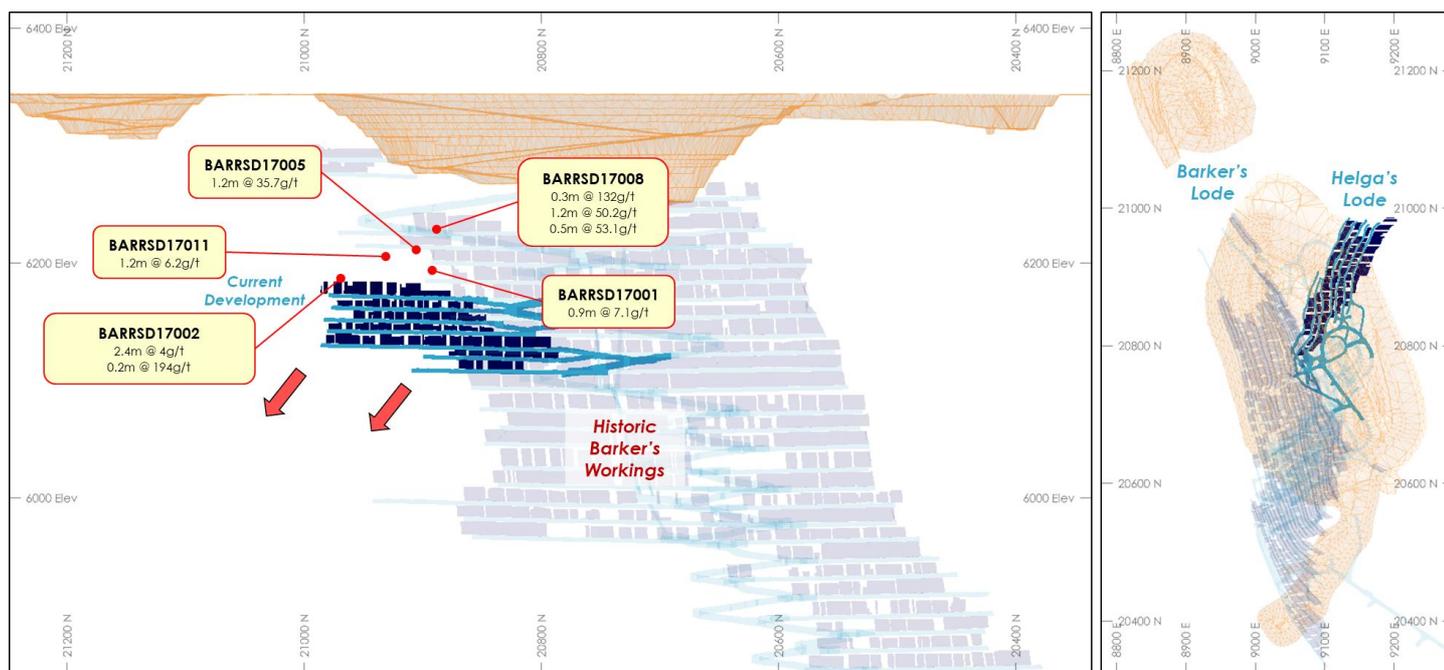


Figure 12 – Plan and long section view of Helga's Vein structure and significant drilling results at the Barker's Mine

In addition, surface deep diamond drilling successfully located extensions to the Barker's and Strzelecki Vein structures at depth below the current mining infrastructure. The successful intersection of both the Barker's Vein (200m down dip) and Strzelecki Vein (470m down dip) in hole BKDD17049A indicates the potential for significant future extensions to these very high-grade structures (Figure 13).

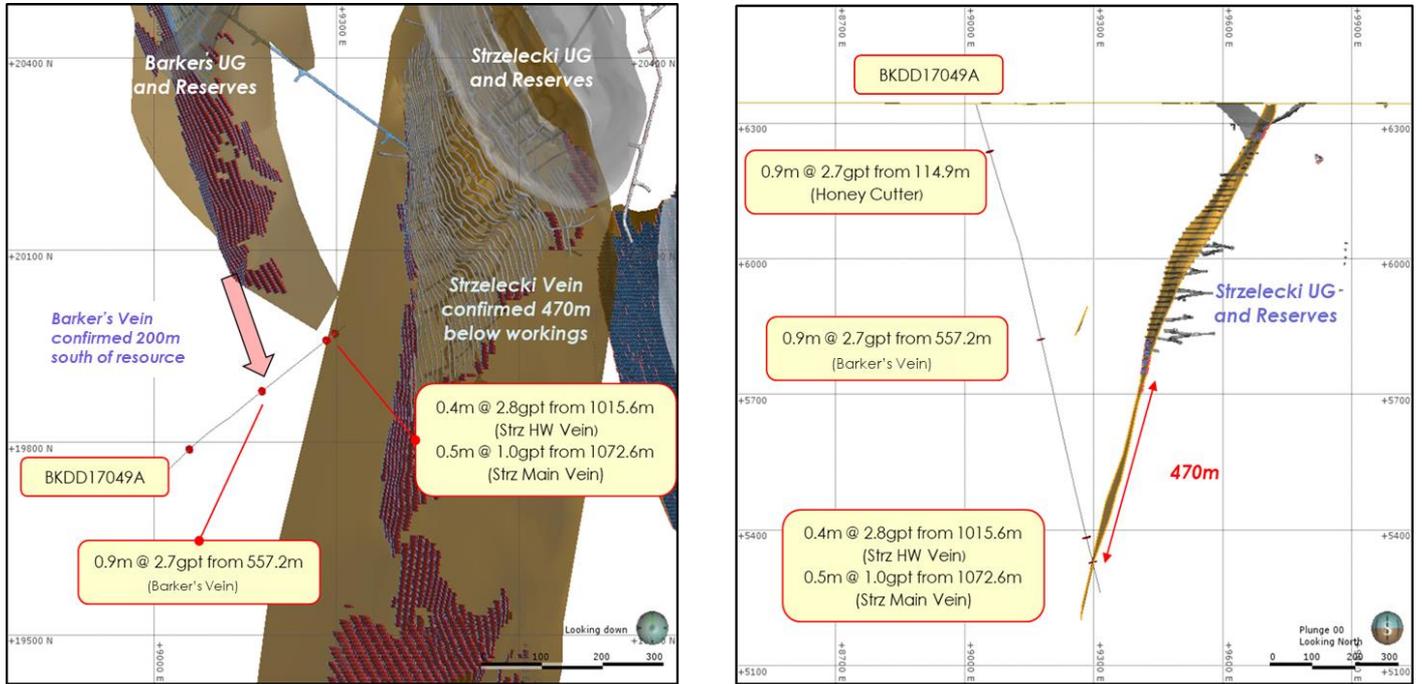


Figure 13 – Plan and cross-sectional view of drilling results beneath Barker's and Strzelecki mines highlighting depth potential of both systems

## Kundana EKJV (NST 51%)

In-mine extensional underground diamond drilling across the Rubicon-Hornet-Pegasus mining complex has significantly expanded the footprint of the mineralised systems in the hanging wall of the main K2 structure.

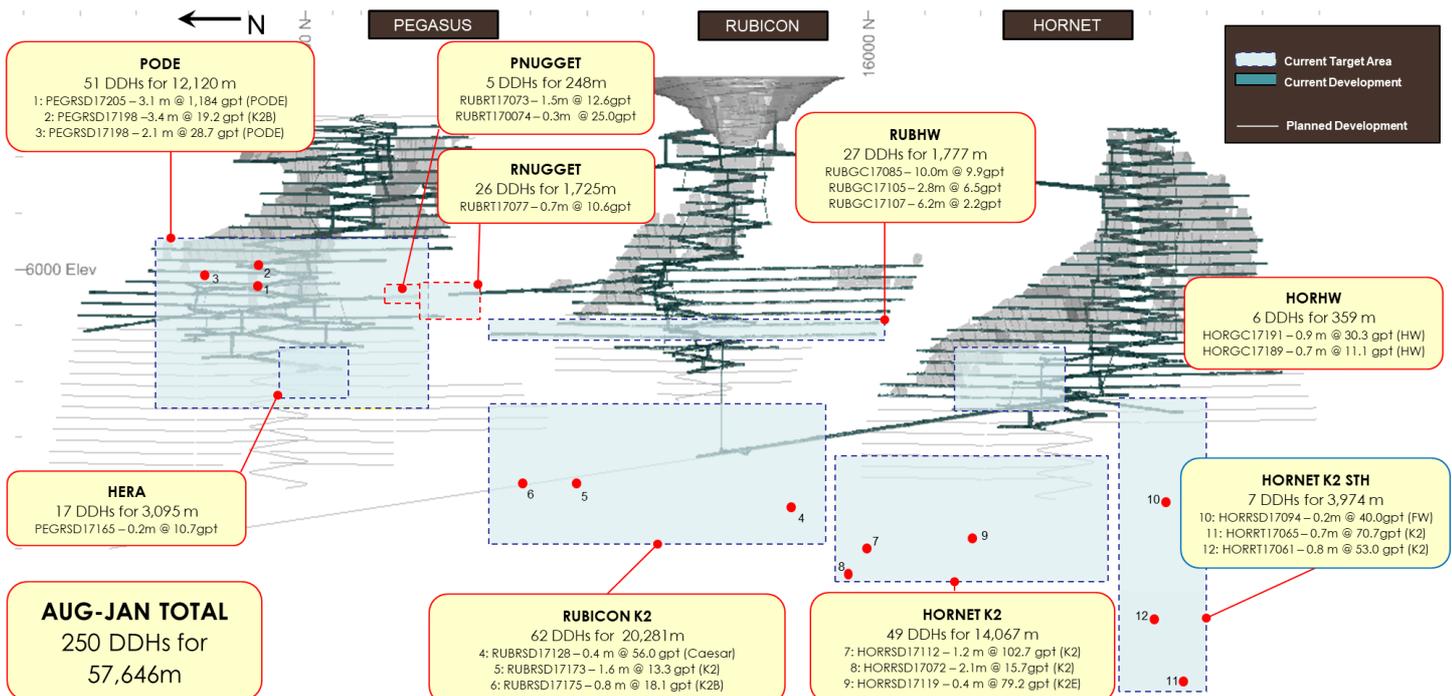


Figure 14 – Long section view of EKJV Rubicon-Hornet-Pegasus mining complex with significant drill hole intersections

At Hornet, exploratory drilling from the new Link Drill Drive successfully outlined depth extensions to the K2 structure and adjacent hanging wall mineralisation (Figure 14). HORRT17061, one of the most southern and deepest holes in the planned Hornet extension drilling, intersected the Hornet K2 structure recording 2.95m(Tw) @13.03gpt gold at over 1,000m below surface. Infill drilling adjacent to the current Hornet mining areas revealed multiple high-grade structures in the hanging wall to the K2 structure leading to the potential for bulk mining in some areas.

Drilling at Rubicon from the new Link Drill Drive also continued to outline depth extensions to the K2 structure and adjacent hanging wall mineralisation while infill drilling in the Rubicon South area identified a new hanging wall system (RUBHW) at the base of the current development.

At Pegasus, extensional drilling has concentrated on hanging wall positions ahead of the development of the Link Drill Drive beneath Pegasus. The Poda zone, associated with the K2B structure, has been significantly extended both down dip and northwards with spectacular high-grade intersections including PEGRSD17205 – 3.1m at 1,184 gpt, PEGRSD17198 – 3.4m at 19.2 gpt and PEGRSD17205 – 2.1m @ 28.7 gpt (figure 14). In addition, new sub-parallel hanging wall zones were discovered at depth (Hera) and Pegasus South (Nugget) outside the existing Resource inventory.

## Kanowna Belle

Following the significant increase in the Resource and Reserve inventory at Kanowna, in-mine expansion drilling has targeted Resource extensions within the A, B, C and D block mining areas with considerable success (Figure 15).

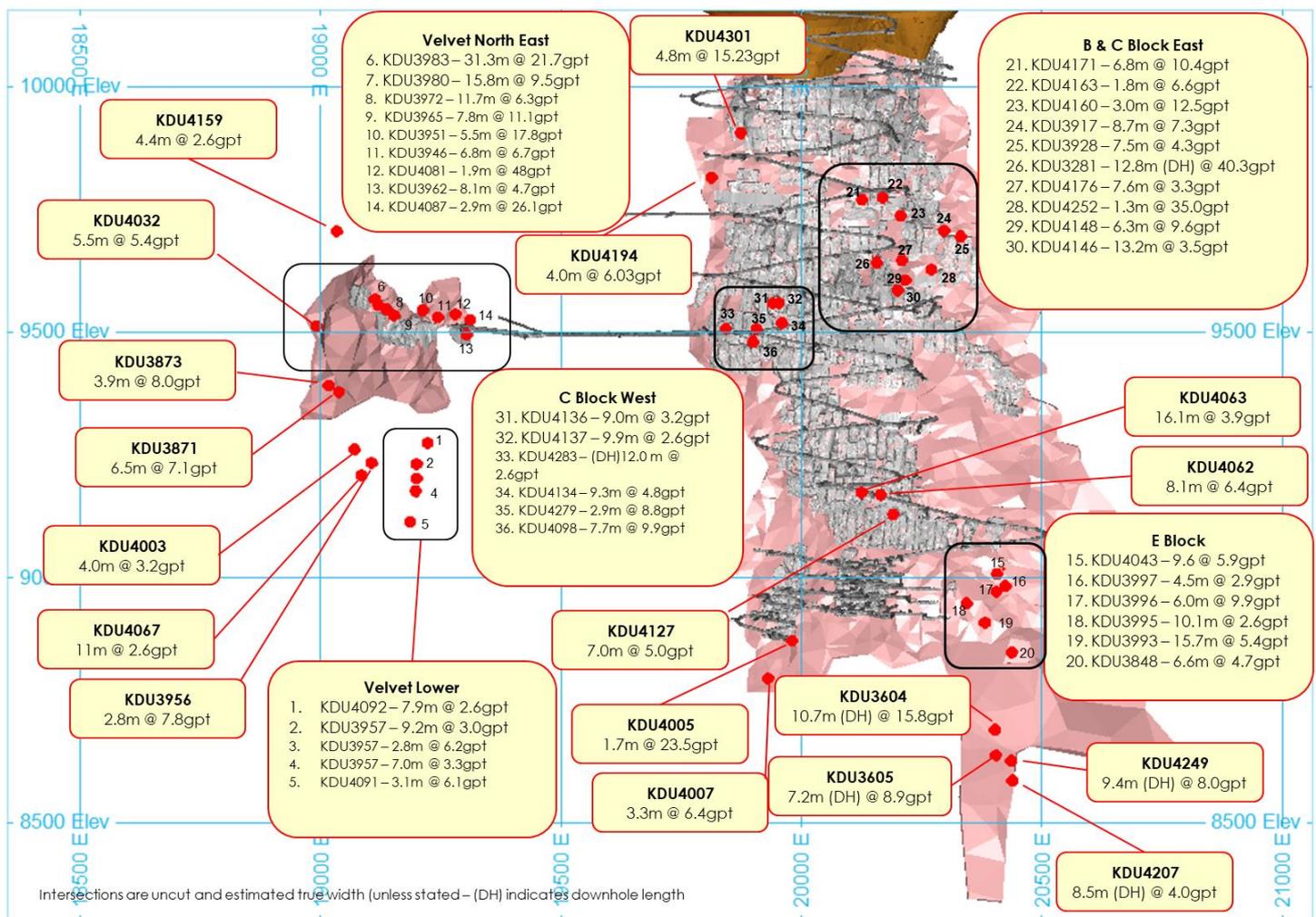


Figure 15 – Long section view Kanowna Belle Mine with significant drill hole intersections

New mineralised positions have been located along both the eastern and western margins of C Block with stronger mineralisation also defined in the hanging wall positions across A and B Blocks.

Extensional drilling has recommenced at depth from the 9245-drill drive with early results indicating the development of a new lode structure (KDU4207 – 8.5m at 4.0gpt (dh)) in the hanging wall of the controlling Fitzroy Fault.

At Velvet, recent diamond drilling continues to expand the mineralisation footprint with both parallel zones adjacent to the main production area (Velvet NE) and deeper down plunge extensions (Velvet Lower) outlined.

## **Carbine**

In the Carbine area, located 50km north of the Kundana operations, exploration and pre-development activities continue to highlight the strong potential for Paradigm and the adjacent Carbine deposit, to play an important role in the Company's growth strategy.

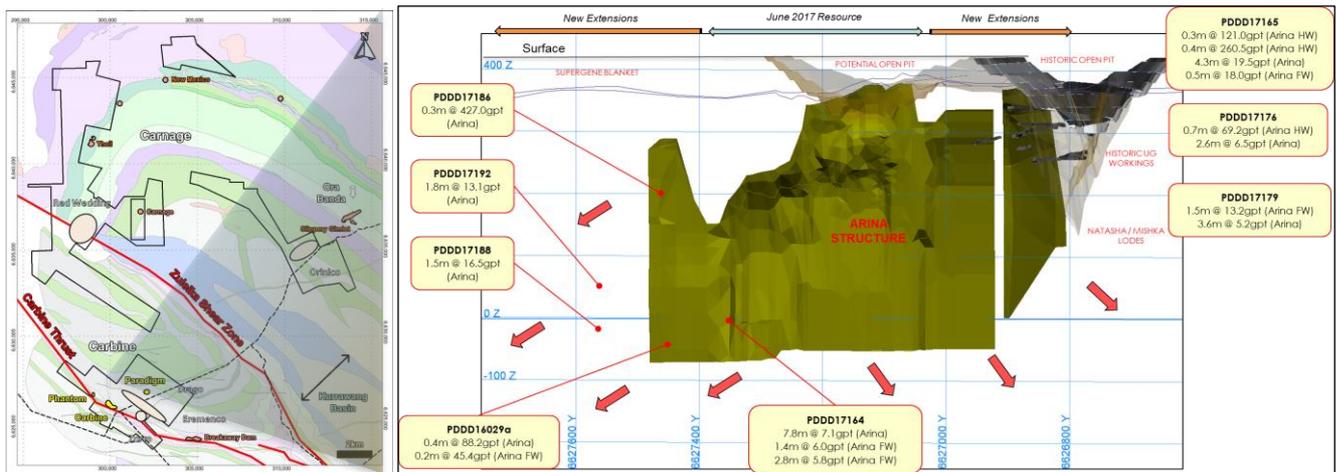


Figure 16 – Paradigm location plan and long section view (looking NE) of drill hole intersection in the Arina structure

At Paradigm, extensional drilling along the central Arina structural corridor delivered further high-grade intersections together with strong mineralisation in both the footwall and hanging wall positions. The Paradigm mineralisation extends over a 1.0km strike length and remains open in all directions (Figure 16).

Pre-development activities have commenced at Paradigm with dewatering of the existing open pit completed and the commencement of an open pit ore Reserve definition drilling program.

## **Paulsens**

Underground diamond drilling at Paulsens concentrated on exploration drilling targeting the Voyager 2 West and Voyager 2 North offset from several drill platforms with modest results. Excavation of the new 660DDR was completed and a single rig commenced drilling in December targeting the Southern Gabbro break area where surface diamond drilling has intersected zones of quartz-sulphide veining along an interpreted structural break in the Mine Gabbro unit.

In conjunction with the underground drilling, re-interpretation of existing 2D seismic data revealed new information over the broader Paulsens area. Drilling has been temporarily suspended pending the undertaking of a new 3D seismic survey anticipated for completion in the June Quarter.

Yours faithfully



**BILL BEAMENT**  
Executive Chairman  
**Northern Star Resources Limited**

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**Competent Persons Statements**

The information in this announcement that relates to exploration results, data quality, geological interpretations for the Company's Project areas is based on information compiled by Michael Mulrone, a Competent Person who is a Member of the Australasian Institute of Mining and Metallurgy and a full-time employee of Northern Star Resources Limited. Mr Mulrone has sufficient experience that is relevant to the styles of mineralisation and type of deposits under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves" for the Company's Project areas. Mr Mulrone consents to the inclusion in this announcement of the matters based on this information in the form and context in which it appears.

**Forward Looking Statements**

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## APPENDIX A – DRILL RESULTS

Table 1 - Jundee Significant Intersections

JUNDEE SIGNIFICANT INTERSECTIONS - ARMADA											
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
WSGC4816A	49588	96540	1912	2	266	509.9	461.6	464.9	3.2	2.6	2.1
WSGC4817	49589	96540	1912	8	263	486.0	444.2	446.3	2.1	1.9	1.8
WSGC4834	49142	96657	1925	4	277	79.0	42.6	43.7	1.1	3.8	0.7
WSGC4835	49142	96657	1926	4	266	74.0	<b>37.2</b>	<b>52.7</b>	<b>15.4</b>	<b>7.7</b>	<b>14.0</b>
						and	55.6	56.6	1.0	6.1	0.7
						and	57.3	59.6	2.3	5.5	2.1
WSGC4835	49142	96657	1926	4	266	74.0	59.9	63.2	3.3	3.0	1.9
WSGC4836	49142	96657	1926	5	252	55.0	<b>33.6</b>	<b>43.3</b>	<b>9.7</b>	<b>6.0</b>	<b>9.3</b>
WSGC4837	49142	96657	1926	4	244	83.2	<b>33.0</b>	<b>42.9</b>	<b>9.9</b>	<b>6.5</b>	<b>8.7</b>
WSGC4838	49142	96657	1926	4	232	86.1	<b>35.8</b>	<b>40.1</b>	<b>4.3</b>	<b>7.5</b>	<b>3.5</b>
WSGC4839	49142	96657	1926	4	224	86.0	<b>37.0</b>	<b>42.4</b>	<b>5.4</b>	<b>6.1</b>	<b>4.0</b>
						and	41.6	42.2	0.5	16.5	0.4
						and	58.5	58.9	0.4	3.9	0.3
WSGC4843	49145	96692	1925	4	311	134.6	<b>52.9</b>	<b>55.9</b>	<b>2.9</b>	<b>10.7</b>	<b>2.8</b>
WSGC4890	49145	96689	1926	14	262	58.6	<b>29.2</b>	<b>38.4</b>	<b>9.2</b>	<b>4.1</b>	<b>8.5</b>
WSGC4891	49145	96689	1925	-7	269	and	44.6	45.5	1.0	3.9	0.8
						and	49.2	49.5	0.3	7.0	0.3
						and	69.0	58.5	0.6	4.2	0.5
WSGC4892	49142	96655	1926	20	228	67.0	62.9	64.3	1.4	5.6	1.0
WSGC4893	49142	96655	1925	-9	243	85.1	46.4	51.7	5.3	5.2	2.8
WSGC4894	49142	96655	1926	16	265	and	59.3	59.7	0.4	5.6	0.3
						and	34.9	40.1	5.2	4.9	3.7
						and	57.3	58.8	1.6	1.2	1.5
WSGC4895	49142	96655	1925	-11	266	84.3	<b>57.2</b>	<b>64.2</b>	<b>7.0</b>	<b>8.2</b>	<b>6.8</b>
WSGC4895	49142	96655	1925	-11	266	and	67.9	69.0	1.2	2.2	0.9
WSGC4895	49142	96655	1925	-11	266	and	74.0	74.7	0.7	4.0	0.4
WSGC4895	49142	96655	1925	-11	266	and	77.4	80.0	2.6	2.8	2.3

JUNDEE SIGNIFICANT INTERSECTIONS - 39 DDR DEEP EXPLORATION												
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)	
GRXP0139	49078	95732	2146	-63	73	1500.0	386.4	389.5	3.1	7.5	1.5	
GRXP0139					Including	1500.0	386.4	386.7	0.3	19.4	0.3	
WSXP2138	49322	95685	1621	-65	90	510.1	<b>202.0</b>	<b>204.7</b>	<b>2.7</b>	<b>11.5</b>	<b>1.9</b>	
WSGC3655	49602	96747	1915	-82	28	229.0	<b>212.7</b>	<b>213.1</b>	<b>0.4</b>	<b>611.0</b>	<b>0.4</b>	
WSGC3656	49602	96739	1915	-86	233	248.0	236.8	237.4	0.7	32.2	0.5	
WSGC4782	49488	96761	1724	22	267	570.0	<b>466.8</b>	<b>477.3</b>	<b>10.5</b>	<b>6.9</b>	<b>7.0</b>	
WSXP1464	49612	96653	1913	-77	309	349.8	251.1	252.4	1.3	65.6	0.3	
WSXP1464	49612	96653	1913	-77	309	and	<b>256.0</b>	<b>256.5</b>	<b>0.6</b>	<b>62.4</b>	<b>0.4</b>	
WSXP1514	49596	96544	1911	-46	355	369.0	304.6	306.0	1.4	16.3	1.0	
WSXP1515	49595	96544	1911	-47	3	358.8	317.6	318.4	0.8	36.7	0.5	
WSXP1516	49595	96544	1911	-49	332	380.7	379.0	379.7	0.6	10.7	0.4	
WSXP1518	49596	96543	1911	-2	90	347.0	296.1	296.4	0.3	49.0	0.2	
WSXP1629	49715	96416	1924	-74	79	296.0	182.0	183.0	1.0	20.6	0.9	
WSXP1797	49732	96548	1789	-25	302	381.0	332.6	333.5	0.9	17.5	0.4	
WSXP1868	49507	96349	1719	-25	81	316.0	36.0	37.0	1.0	51.0	0.3	
WSXP1875	49506	96349	1719	-85	89	550.1	117.3	119.0	1.7	5.6	0.5	
WSXP1915	49535	96772	1721	-45	90	372.0	<b>67.3</b>	<b>68.4</b>	<b>1.1</b>	<b>28.2</b>	<b>1.0</b>	
WSXP1917	49534	96771	1720	-83	88	488.9	65.2	65.5	0.3	15.8	0.3	
WSXP1926	49469	96214	1699	-85	90	and	85.6	88.6	3.0	9.4	2.0	
						and	550.2	<b>147.7</b>	<b>148.0</b>	<b>0.3</b>	<b>380.0</b>	<b>0.3</b>
						and	93.9	70.6	71.0	0.4	56.8	0.3
WSXP1946	49535	96771	1721	-34	97	88.1	56.7	57.0	0.3	93.8	0.2	
WSXP1947	49535	96771	1720	-51	118	88.1	56.7	57.0	0.3	93.8	0.2	
WSXP1953	49506	96623	1739	-26	54	165.0	<b>132.1</b>	<b>133.3</b>	<b>1.2</b>	<b>40.5</b>	<b>0.8</b>	
WSXP1955	49505	96623	1739	-49	41	152.6	<b>124.8</b>	<b>125.3</b>	<b>0.5</b>	<b>142.0</b>	<b>0.4</b>	
WSXP1959	49506	96623	1739	-32	62	and	118.9	119.3	0.4	54.8	0.3	
						and	<b>26.2</b>	<b>30.1</b>	<b>3.9</b>	<b>14.4</b>	<b>1.4</b>	
						and	55.6	56.0	0.4	12.9	0.4	
WSXP1961	49506	96623	1739	-48	56	180.0	<b>119.6</b>	<b>119.9</b>	<b>0.3</b>	<b>154.0</b>	<b>0.3</b>	
WSXP1962	49506	96623	1739	-34	52	437.8	<b>107.6</b>	<b>107.9</b>	<b>0.3</b>	<b>103.0</b>	<b>0.3</b>	
WSXP1985	49506	96622	1739	-28	80	419.9	61.2	62.2	1.0	10.9	0.7	
WSXP2000	49345	95933	1657	-85	270	450.1	196.0	199.4	3.4	11.5	1.5	
WSXP2021	49489	96761	1722	20	270	and	216.5	221.5	5.0	3.8	2.3	
						and	48.6	48.9	0.3	24.0	0.3	
						and	49.5	50.7	1.3	14.2	1.1	
WSXP2025	49489	96761	1721	-65	260	600.0	100.0	100.3	0.3	19.6	0.3	
WSXP2034	49489	96761	1722	13	270	593.2	<b>53.3</b>	<b>54.8</b>	<b>1.5</b>	<b>24.5</b>	<b>1.3</b>	
WSXP2080	49276	95686	1619	-15	270	1062.5	241.0	242.0	1.0	25.8	0.3	
WSXP2095	49489	96761	1722	6	273	690.0	60.0	64.3	4.3	11.2	1.0	
WSXP2100	49306	95787	1636	2	270	999.1	350.2	351.9	1.6	8.3	1.1	
WSXP2104	49306	95787	1635	-85	270	883.8	84.0	84.7	0.7	20.6	0.5	
JRCD9114W2	49164	96509	2563	-75	85	1330.0	1051.0	1051.8	0.8	20.1	0.5	
JRD9603W1	49132	96238	2558	-68	80	1315.0	1203.6	1204.0	0.4	11.8	0.4	



## JUNDEE SIGNIFICANT INTERSECTIONS - GATEWAY

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
GWGC0864	48908	96171	2312	-11	349	300.0	238.4	238.7	0.3	2.8	0.3
GWGC0869	48909	96171	2312	-19	359	238.0	174.0	174.5	0.4	3.4	0.4
GWGC0870	48910	96171	2311	-33	2	228.9	<b>136.4</b>	<b>138.1</b>	<b>1.7</b>	<b>28.1</b>	<b>1.6</b>
GWGC0871	48909	96171	2312	-12	0	254.9	195.0	196.0	1.0	3.1	0.6
GWGC0874	48909	96171	2312	-22	2	220.1	<b>146.9</b>	<b>151.0</b>	<b>4.2</b>	<b>26.2</b>	<b>3.4</b>
GWGC0875	48909	96171	2312	-8	5	260.0	204.0	204.5	0.4	5.7	0.3
						and	217.4	219.8	2.4	11.0	1.7
GWGC0876	48909	96171	2311	-4	5	280.0	<b>207.2</b>	<b>208.4</b>	<b>1.2</b>	<b>91.5</b>	<b>1.1</b>
						and	<b>210.4</b>	<b>212.0</b>	<b>1.6</b>	<b>47.7</b>	<b>1.4</b>
						and	<b>224.3</b>	<b>226.6</b>	<b>2.3</b>	<b>27.3</b>	<b>1.4</b>
GWGC0877	48909	96171	2310	-34	12	190.0	<b>128.2</b>	<b>130.2</b>	<b>2.0</b>	<b>86.9</b>	<b>1.5</b>
GWGC0878	48910	96172	2311	-24	10	205.0	<b>137.6</b>	<b>140.0</b>	<b>2.4</b>	<b>33.4</b>	<b>2.0</b>
GWGC0879	48910	96171	2312	-9	9	246.9	<b>161.4</b>	<b>168.5</b>	<b>7.1</b>	<b>49.0</b>	<b>6.9</b>
						and	<b>188.9</b>	<b>190.8</b>	<b>1.9</b>	<b>12.9</b>	<b>1.7</b>
GWGC0880	48910	96171	2311	-16	10	220.0	<b>147.1</b>	<b>148.7</b>	<b>1.6</b>	<b>95.5</b>	<b>1.2</b>
GWGC0883	48909	96171	2311	-10	17	219.1	<b>160.0</b>	<b>161.1</b>	<b>1.1</b>	<b>122.8</b>	<b>0.8</b>
GWGC0901	48868	96072	2197	5	359	285.0	224.0	224.8	0.8	0.2	0.6
GWGC0902	48868	96072	2197	6	3	260.0	<b>188.0</b>	<b>190.2</b>	<b>2.2</b>	<b>51.1</b>	<b>1.7</b>
GWGC0903	48868	96072	2197	-2	3	200.1	120.6	125.2	4.6	4.8	0.3
GWGC0906	48869	96072	2197	5	16	210.0	<b>106.4</b>	<b>120.0</b>	<b>13.6</b>	<b>21.1</b>	<b>11.0</b>
GWGC0907	48871	96069	2197	7	28	204.9	99.1	100.1	1.0	2.4	0.5
GWGC0909	48871	96068	2196	3	38	126.1	84.5	88.0	3.5	6.4	3.1
GWGC0913	48910	96171	2311	-61	11	178.1	<b>93.6</b>	<b>94.9</b>	<b>1.3</b>	<b>27.8</b>	<b>1.2</b>
GWGC0925	48868	96072	2197	9	6	263.7	156.4	156.8	0.4	9.0	0.3
GWGC0925	48868	96072	2197	9	6	263.7	<b>188.7</b>	<b>193.0</b>	<b>4.3</b>	<b>12.2</b>	<b>4.0</b>
NXXP0062	49052	96155	2316	14	50	185.0	128.8	132.7	3.9	6.1	1.7
NXXP0065	49053	96154	2315	12	66	200.0	132.0	134.0	2.0	6.2	1.6
						and	139.8	141.3	1.4	4.7	1.0
NXXP0067	49053	96154	2315	2	75	125.0	84.2	85.0	0.8	5.2	0.6
NXXP0068	49053	96154	2315	8	86	189.6	116.4	117.2	0.8	1.5	0.3
NXXP0071	49053	96154	2315	-8	98	115.0	70.6	71.2	0.7	9.5	0.5
NXXP0075	49045	96177	2314	-9	33	95.0	<b>64.6</b>	<b>67.4</b>	<b>2.8</b>	<b>19.5</b>	<b>2.6</b>
						and	67.9	68.2	0.3	14.5	0.3
NXXP0076	49046	96177	2314	-12	54	80.0	63.2	65.4	2.1	6.9	1.5
NXXP0079	49053	96154	2315	-9	104	403.2	69.6	71.3	1.7	14.3	1.3

## JUNDEE SIGNIFICANT INTERSECTIONS - NEXUS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
GRXP0444	49199	95675	2283	-10	36	399.6	258.0	259.5	1.5	1.9	1.2
						and	<b>324.0</b>	<b>325.0</b>	<b>1.0</b>	<b>305.0</b>	<b>0.4</b>
GRXP0445	49198	95675	2283	0	48	885.0	272.0	273.0	1.0	8.7	0.7
NXXP0052	49335	96293	2353	8	104	191.0	<b>185.7</b>	<b>186.2</b>	<b>0.5</b>	<b>295.0</b>	<b>0.3</b>
NXXP0049	49335	96293	2353	-5	102	146.0	<b>46.0</b>	<b>47.7</b>	<b>1.7</b>	<b>88.1</b>	<b>1.0</b>
NXXP0059	49335	96292	2353	7	123	238.0	<b>204.5</b>	<b>205.3</b>	<b>0.8</b>	<b>45.9</b>	<b>0.5</b>
NXXP0037	49403	96329	2356	16	53	105.0	<b>5.9</b>	<b>6.2</b>	<b>0.3</b>	<b>137.0</b>	<b>0.3</b>
NXXP0040	49403	96329	2354	-35	91	75.1	39.1	39.4	0.3	57.2	0.3
NXXP0043	49336	96293	2353	3	85	149.0	<b>120.4</b>	<b>121.1</b>	<b>0.8</b>	<b>77.2</b>	<b>0.5</b>
NXXP0048	49336	96293	2353	9	96	226.0	151.4	152.6	1.1	16.9	0.8
NXXP0042	49335	96293	2353	17	81	300.0	<b>171.7</b>	<b>172.5</b>	<b>0.8</b>	<b>74.3</b>	<b>0.8</b>

## JUNDEE SIGNIFICANT INTERSECTIONS - ZODIAC

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
JRD10448	49282	95391	2570	-55	96	1911.6	449.5	449.8	0.3	2.1	0.3
						and	469.9	470.2	0.3	5.2	0.3
						and	498.1	499.0	0.9	3.2	0.8
						and	512.0	513.4	1.4	2.5	1.2
						and	1458.5	1458.9	0.4	4.2	0.4
						and	<b>1656.0</b>	<b>1664.1</b>	<b>8.1</b>	<b>2.5</b>	<b>8.1</b>
						and	1668.0	1668.4	0.4	2.2	0.4
						and	1777.6	1778.6	1.1	2.2	1.1
						and	1811.1	1812.0	0.9	2.9	0.7
JRD10449	50265	95205	2590	-55	69	2064.6	151.6	151.6	0.3	27.8	0.3
JRD10450A	50650	95581	2588	-60	55	1594.8			NSI		
JRD10451	50106	94547	2551	-61	66	2308.0	1855.0	1855.3	0.3	28.5	0.3
						and	2066.0	2068.7	2.7	2.6	2.7
						and	2157.4	2158.5	1.0	2.5	1.0
JRD10451W1	49023	94503	2552	-61	62	2241.1	1387.4	1387.7	0.3	2.4	0.3
						and	1441.5	1441.8	0.3	4.0	0.3
						and	1445.4	1445.7	0.3	2.4	0.3
						and	1461.3	1461.9	0.6	3.9	0.4
						and	1524.1	1524.7	0.6	4.4	0.3
						and	1527.2	1527.6	0.4	2.4	0.3
						and	1528.7	1529.0	0.3	2.5	0.4
						and	1678.8	1683.8	5.0	1.0	4.0
						and	<b>1685.2</b>	<b>1688.6</b>	<b>3.4</b>	<b>4.8</b>	<b>3.0</b>
						and	1711.5	1714.5	3.0	2.1	2.5
						and	1735.9	1736.3	0.4	4.9	0.3
						and	1865.5	1866.7	1.2	3.9	0.7
						and	1935.5	1935.8	0.3	9.1	0.3
						and	2003.5	2004.6	1.1	7.8	0.9
						and	2039.5	2039.9	0.3	7.3	0.3
						and	2091.9	2092.7	0.8	8.1	0.7
JRD10452	50097	95512	2588	-61	61	1387.2			NSI		
JRD10453	50301	95923	2553	-72	89	1399.2	1131.3	1131.9	0.6	2.5	0.6
JRD10456	49454	94619	2551	-60	75	2000.0	596.1	596.4	0.3	2.6	0.3
WSXP2166	49321	95682	1621	-34	127	1277.7	1103.3	1103.7	0.3	1.1	0.3



## JUNDEE SIGNIFICANT INTERSECTIONS - ZODIAC

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
WSXP2188	49348	95785	1637	-32	123	and	1225.8	1226.1	0.3	2.4	0.3
						1310.5	948.0	949.0	1.0	3.6	0.4
						and	1124.9	1125.2	0.3	1.4	0.3
						and	1191.9	1202.0	10.1	1.1	8.0
						and	1272.6	1272.9	0.3	3.1	0.3
WSXP2190	49322	95683	1621	-29	130	and	1274.8	1275.2	0.4	2.4	0.3
						and	1298.7	1299.1	0.4	2.4	0.4
						1311.5	956.4	958.8	2.4	1.9	2.1
						and	<b>982.8</b>	<b>987.4</b>	<b>4.6</b>	<b>3.0</b>	<b>3.7</b>
						and	<b>1179.3</b>	<b>1190.5</b>	<b>11.2</b>	<b>1.6</b>	<b>9.0</b>
WSXP2199	49390	95932	1658	-40	90	and	1195.1	1195.7	0.6	3.3	0.4
						and	1200.1	1200.4	0.3	3.7	0.3
						and	1249.9	1250.3	0.4	4.2	0.4
						and	1285.3	1286.0	0.7	2.0	0.6
						1300.0	<b>941.5</b>	<b>947.3</b>	<b>5.8</b>	<b>3.8</b>	<b>4.0</b>
						and	1061.0	1062.0	1.0	3.3	0.4
						and	1067.4	1068.0	0.6	2.4	0.5
						and	1070.7	1071.1	0.4	2.3	0.3
						and	1071.4	1072.5	1.1	2.2	0.8
						and	1108.5	1109.0	0.5	7.3	0.5
WSXP2150	49348	95786	1636	-65	50.4	and	1162.4	1163.3	0.8	2.6	0.8
						and	1175.3	1176.0	0.8	3.1	0.5
						and	1181.9	1182.3	0.3	2.0	0.3
						and	1196.9	1198.1	1.1	8.7	1.0
						and	1198.5	1199.0	0.5	5.0	0.4
						and	1201.0	1201.3	0.3	3.5	0.3
						and	1202.0	1202.3	0.3	3.9	0.3
						and	1202.7	1203.0	0.3	3.6	0.3
						and	1203.3	1203.6	0.3	6.8	0.3
						and	1204.2	1204.6	0.4	8.5	0.4
1300.0	<b>913.8</b>	<b>914.3</b>	<b>0.5</b>	<b>765.0</b>	<b>0.4</b>						

## JUNDEE SIGNIFICANT INTERSECTIONS - REGIONAL

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
NSRJAC03190	252866	7092000	535	-90	0	50.0	30.0	35.0	5.0	1.2	3.5
NSRJAC03208	251576	7096352	535	-90	0	50.0	20.0	25.0	5.0	2.3	3.5
NSRJRC11154	278436	7058846	535	-60	45	50.0	26.0	29.0	3.0	2.5	2.0
NSRJRC11156	278328	7058735	535	-60	45	180.0	178.0	180.0	2.0	4.9	1.5
NSRJRC11160	277974	7059229	535	-60	45	180.0	77.0	80.0	3.0	1.8	2.0
NSRJRC11161	277926	7059173	535	-60	45	180.0	114.0	119.0	5.0	3.1	3.5
NSRJRC11204	263417	7082263	535	-60	270	120.0	<b>40.0</b>	<b>56.0</b>	<b>16.0</b>	<b>1.8</b>	<b>12.0</b>
						and	92.0	120.0	28.0	0.5	20.0

## RAMONE SIGNIFICANT INTERSECTIONS

Drill Hole #	Easting (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
NSRJRC11101	285531	7060596	554	-61	140	90.0	1.0	30.0	29.0	0.9	20.0
						and	<b>40.0</b>	<b>90.0</b>	<b>50.0</b>	<b>1.7</b>	<b>30.0</b>
						Including	<b>61.0</b>	<b>71.0</b>	<b>10.0</b>	<b>6.0</b>	<b>7.0</b>
NSRJRC11101	285531	7060596	554	-60	150	120.0	118.0	120.0	2.0	1.9	0.8
NSRJRC11102	285293	7060322	554	-60	150	30.0	22.0	24.0	2.0	2.2	0.8
NSRJRC11103	285280	7060343	554	-60	150	102.0	<b>3.0</b>	<b>43.0</b>	<b>40.0</b>	<b>1.7</b>	<b>16.0</b>
NSRJRC11104	285267	7060365	554	-60	150	126.0	18.0	39.0	21.0	1.3	8.4
NSRJRC11105	285392	7060546	554	-60	150	and	66.0	78.0	12.0	3.1	4.8
						and	174.0	114.0	10.0	1.7	7.0
						and	142.0	152.0	10.0	2.4	8.0
NSRJRC11107	285460	7060527	554	-60	150	and	168.0	173.0	5.0	0.5	5.0
						102.0	<b>2.0</b>	<b>30.0</b>	<b>28.0</b>	<b>3.1</b>	<b>20.0</b>
NSRJRC11108	285310	7060390	554	-60	150	and	35.0	38.0	3.0	1.3	2.0
						120.0	39.0	43.0	4.0	1.2	1.6
NSRJRC11109	285297	7060412	554	-60	150	and	<b>47.0</b>	<b>91.0</b>	<b>44.0</b>	<b>1.5</b>	<b>17.6</b>
						156.0	48.0	51.0	3.0	4.2	1.2
						and	73.0	79.0	6.0	2.7	2.4
						and	106.0	108.0	2.0	1.4	0.8
						and	<b>121.0</b>	<b>156.0</b>	<b>35.0</b>	<b>1.5</b>	<b>14.0</b>
NSRJRC11110	285514	7060530	554	-60	151	60.0			NSI		
NSRJRC11111	285503	7060552	554	-60	150	90.0	8.0	17.0	9.0	1.5	7.2
NSRJRC11112	285491	7060574	554	-60	150	120.0	<b>24.0</b>	<b>81.0</b>	<b>59.0</b>	<b>1.8</b>	<b>40.0</b>
NSRJRC11113	285341	7060437	554	-60	150	and	100.0	116.0	16.0	0.4	14.0
						174.0	78.0	90.0	12.0	1.5	8.0
							<b>104.0</b>	<b>118.0</b>	<b>14.0</b>	<b>3.1</b>	<b>9.0</b>
NSRJRC11115	285409	7060418	554	-60	150	90.0	1.0	14.0	13.0	1.7	10.0
NSRJRC11116	285384	7060462	554	-60	150	and	20.0	35.0	15.0	1.0	11.0
						168.0	<b>82.0</b>	<b>115.0</b>	<b>33.0</b>	<b>3.0</b>	<b>20.0</b>
						and	127.0	129.0	2.0	3.4	1.5
						and	135.0	144.0	9.0	2.0	5.4
NSRJRC11118	285454	7060443	554	-60	150	and	162.0	164.0	2.0	2.4	1.2
						90.0	1.0	32.0	31.0	0.8	12.4
						and	14.0	22.0	8.0	2.1	4.8
NSRJRC11119	285577	7060624	554	-60	150	120.0	<b>15.0</b>	<b>80.0</b>	<b>65.0</b>	<b>1.4</b>	<b>39.0</b>
NSRJRC11120	285565	7060646	554	-60	150	150.0	35.0	41.0	6.0	0.7	4.0
						and	49.0	66.0	17.0	0.5	11.0
						and	<b>72.0</b>	<b>123.0</b>	<b>51.0</b>	<b>2.2</b>	<b>30.0</b>
NSRJRC11121	285643	7060606	554	-60	150	66.0			NSI		
NSRJRC11122	285496	7060468	554	-60	150	90.0	<b>2.0</b>	<b>12.0</b>	<b>10.0</b>	<b>4.0</b>	<b>6.0</b>
NSRJRC11123	285484	7060490	554	-60	150	120.0	84.0	87.0	3.0	5.0	1.8
						and	92.0	94.0	2.0	3.3	1.2



## RAMONE SIGNIFICANT INTERSECTIONS

Drill Hole #	Eastings (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
NSRJRC11124	285472	7060512	554	-60	150	156.0	40.0	42.0	2.0	8.7	1.2
NSRJRC11126	285676	7060653	554	-60	150	90.0			NSI		
NSRJRC11127	285525	7060516	554	-60	150	120.0	48.0	49.0	1.0	6.3	0.6
NSRJRC11128	285651	7060693	554	-60	150	150.0	<b>139.0</b>	<b>147.0</b>	<b>8.0</b>	<b>9.2</b>	<b>4.8</b>
NSRJRC11212	285271	7060451	554	-60	150	123.0	59.0	68.0	9.0	1.0	7.0
NSRJRC11213	285260	7060474	554	-60	150	184.0	<b>45.0</b>	<b>73.0</b>	<b>28.0</b>	<b>2.6</b>	<b>16.8</b>
						Including	<b>55.0</b>	<b>69.0</b>	<b>14.0</b>	<b>4.9</b>	<b>8.4</b>
NSRJRC11215	285325	7060454	554	-60	150	102.0			NSI		
NSRJRC11216	285312	7060475	554	-60	150	126.0	18.0	27.0	9.0	1.7	6.3
NSRJRC11217	285301	7060494	554	-60	150	156.0	52.0	56.0	4.0	2.1	2.8
						and	96.0	100.0	4.0	1.4	2.8
						and	127.0	147.0	20.0	1.4	14.0
NSRJRC11219	285370	7060479	554	-60	150	144.0	16.0	33.0	17.0	1.6	11.9
NSRJRC11220	285357	7060502	554	-60	150	138.0	<b>50.0</b>	<b>62.0</b>	<b>12.0</b>	<b>3.8</b>	<b>8.4</b>
						and	<b>94.0</b>	<b>110.0</b>	<b>16.0</b>	<b>2.1</b>	<b>11.2</b>
						and	120.0	121.0	1.0	4.1	0.7
NSRJRC11221	285346	7060522	554	-60	150	186.0	<b>173.0</b>	<b>184.0</b>	<b>11.0</b>	<b>4.0</b>	<b>7.7</b>
NSRJRC11222	285461	7060622	535	-60	150	234.0	50.0	66.0	16.0	0.3	9.6
						and	95.0	125.0	30.0	0.5	18.0
						and	141.0	142.0	1.0	5.6	0.7
						and	<b>154.0</b>	<b>195.0</b>	<b>41.0</b>	<b>1.7</b>	<b>22.0</b>
NSRJRC11223	285436	7060665	554	-60	150	324.0	35.0	46.0	11.0	1.9	6.6
						and	<b>292.0</b>	<b>315.0</b>	<b>23.0</b>	<b>1.6</b>	<b>13.8</b>
NSRJRC11224	285505	7060644	554	-60	150	120.0			NSI		
NSRJRC11225	285505	7060644	554	-60	150	234.0	42.0	51.0	9.0	1.2	6.3
						and	108.0	110.0	2.0	3.7	1.4
						and	156.0	168.0	12.0	1.1	8.4
						and	187.0	192.0	5.0	2.8	3.5
NSRJRC11226	285493	7060665	554	-60	150	84.0			NSI		
NSRJRC11227	285479	7060688	554	-60	150	324.0	48.0	49.0	1.0	6.3	0.7
						and	168.0	169.0	1.0	3.0	0.7
						and	<b>212.0</b>	<b>242.0</b>	<b>30.0</b>	<b>2.0</b>	<b>21.0</b>
NSRJRC11232	285655	7060640	554	-60	150	85.0	10.0	14.0	4.0	4.6	2.8
NSRJRC11233	285643	7060662	554	-60	150	140.0	64.0	66.0	2.0	1.6	1.4
						and	83.0	87.0	4.0	6.2	2.8
						and	116.0	118.0	2.0	1.2	1.4
NSRJRC11234	285630	7060684	554	-60	150	180.0			NSI		
NSRJRC11235	285624	7060594	554	-60	330	100.0	29.0	38.0	9.0	1.8	4.5
						and	95.0	98.0	3.0	1.6	1.5
NSRJRC11236	285612	7060615	554	-60	150	85.0	<b>3.0</b>	<b>22.0</b>	<b>19.0</b>	<b>2.4</b>	<b>13.3</b>
NSRJRC11237	285599	7060637	554	-60	150	140.0			NSI		
NSRJRC11238	285587	7060659	554	-60	150	180.0	30.0	31.0	1.0	2.7	0.7
						and	57.0	59.0	2.0	3.6	1.4
						and	65.0	69.0	4.0	1.7	2.8
NSRJRC11239	285574	7060680	554	-60	150	230.0	89.0	92.0	3.0	1.3	2.1
						and	95.0	98.0	3.0	2.2	2.1
						and	168.0	169.0	1.0	6.5	0.7
						and	173.0	174.0	1.0	4.1	0.7
NSRJRC11240	285581	7060569	554	-60	330	100.0	21.0	26.0	5.0	1.3	2.5
						and	30.0	33.0	3.0	5.7	1.5
						and	<b>42.0</b>	<b>64.0</b>	<b>22.0</b>	<b>3.1</b>	<b>11.0</b>
NSRJRC11241	285569	7060590	554	-60	150	90.0	4.0	6.0	2.0	1.2	1.4
						and	11.0	14.0	3.0	3.4	2.1
						and	40.0	42.0	2.0	3.4	1.4
NSRJRC11242	285556	7060612	554	-60	150	140.0	<b>26.0</b>	<b>54.0</b>	<b>28.0</b>	<b>1.8</b>	<b>19.6</b>
						and	62.0	75.0	13.0	1.8	9.1
						and	79.0	82.0	3.0	1.7	2.1
						and	109.0	114.0	5.0	2.5	3.5
NSRJRC11243	285544	7060634	554	-60	150	190.0	23.0	27.0	4.0	6.4	2.8
						and	56.0	63.0	7.0	1.2	4.9
						and	79.0	81.0	2.0	2.9	1.4
						and	<b>94.0</b>	<b>101.0</b>	<b>7.0</b>	<b>4.2</b>	<b>4.9</b>
						and	<b>129.0</b>	<b>132.0</b>	<b>3.0</b>	<b>9.8</b>	<b>2.1</b>
NSRJRC11244	285531	7060655	554	-60	150	240.0	60.0	63.0	3.0	1.4	2.1
						and	75.0	76.0	1.0	3.8	0.7
						and	86.0	90.0	4.0	2.2	2.8
						and	114.0	116.0	2.0	4.6	1.4
						and	127.0	136.0	9.0	2.9	6.3
						and	138.0	144.0	6.0	1.2	4.2
						and	173.0	180.0	7.0	1.5	4.9
						and	220.0	224.0	4.0	1.5	2.8
NSRJRC11245	285538	7060544	554	-60	330	120.0	16.0	18.0	2.0	1.2	1.0
						and	35.0	36.0	1.0	3.5	0.5
						and	<b>38.0</b>	<b>64.0</b>	<b>26.0</b>	<b>8.5</b>	<b>13.0</b>
						Including	<b>43.0</b>	<b>46.0</b>	<b>3.0</b>	<b>51.7</b>	<b>1.5</b>
						and	66.0	73.0	7.0	2.7	3.5
						and	92.0	95.0	3.0	1.2	1.5
NSRJRC11246	285525	7060565	554	-60	150	90.0	1.0	6.0	5.0	1.9	3.5
						and	17.0	21.0	4.0	1.4	2.8
						and	25.0	30.0	5.0	2.0	3.5
						and	64.0	66.0	2.0	4.0	1.4
NSRJRC11247	285513	7060587	554	-60	150	140.0	27.0	31.0	4.0	1.1	2.8
						and	<b>33.0</b>	<b>76.0</b>	<b>43.0</b>	<b>2.0</b>	<b>30.1</b>
NSRJRC11248	285500	7060609	554	-60	150	190.0	68.0	71.0	3.0	1.4	2.1
						and	<b>87.0</b>	<b>107.0</b>	<b>20.0</b>	<b>3.5</b>	<b>14.0</b>
						and	121.0	138.0	17.0	1.6	11.9
						and	173.0	174.0	1.0	2.5	0.7
NSRJRC11249	285488	7060630	554	-60	150	240.0	<b>144.0</b>	<b>177.0</b>	<b>33.0</b>	<b>3.2</b>	<b>23.1</b>
						Including	170.0	173.0	3.0	13.9	1.5
						and	188.0	190.0	2.0	1.6	1.4
						and	204.0	210.0	6.0	1.2	4.2
NSRJRC11250	285494	7060519	554	-60	330	110.0	<b>28.0</b>	<b>65.0</b>	<b>37.0</b>	<b>6.2</b>	<b>18.5</b>
						Including	<b>43.0</b>	<b>46.0</b>	<b>3.0</b>	<b>39.0</b>	<b>1.5</b>
NSRJRC11251	285482	7060540	554	-60	150	90.0	1.0	14.0	13.0	1.7	9.1
						and	20.0	30.0	10.0	1.0	7.0

## RAMONE SIGNIFICANT INTERSECTIONS

Drill Hole #	Eastings (MGA)	Northing (MGA)	Collar RL (MGA)	Dip (degrees)	Azimuth (MGA)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
						and	32.0	34.0	2.0	1.9	1.4
						and	44.0	46.0	2.0	1.3	1.4
NSRJRC11252	285469	7060562	554	-60	150	140.0	40.0	46.0	6.0	1.2	4.2
						and	<b>48.0</b>	<b>72.0</b>	<b>24.0</b>	<b>3.5</b>	<b>16.8</b>
						and	74.0	83.0	9.0	1.6	6.3
						and	<b>85.0</b>	<b>91.0</b>	<b>6.0</b>	<b>5.0</b>	<b>4.2</b>
						and	131.0	132.0	1.0	3.5	0.7
NSRJRC11258	285426	7060537	554	-60	150	140.0	22.0	24.0	2.0	2.0	1.4
						and	56.0	64.0	8.0	2.4	5.6
						and	<b>66.0</b>	<b>85.0</b>	<b>19.0</b>	<b>2.5</b>	<b>13.3</b>
						and	90.0	95.0	5.0	1.4	3.5
						and	114.0	117.0	3.0	2.6	2.1
						and	120.0	126.0	6.0	1.6	4.2
						and	136.0	140.0	4.0	2.1	2.8
NSRJRC11261	285380	7060568	554	-60	150	240.0	<b>222.0</b>	<b>240.0</b>	<b>18.0</b>	<b>1.8</b>	<b>12.6</b>
NSRJRC11263	285395	7060490	554	-60	150	90.0	<b>17.0</b>	<b>58.0</b>	<b>41.0</b>	<b>2.6</b>	<b>28.7</b>
						Including	<b>26.0</b>	<b>42.0</b>	<b>16.0</b>	<b>4.8</b>	<b>11.2</b>
NSRJRC11253	285457	7060584	554	-60	150	and	<b>59.0</b>	<b>60.0</b>	<b>1.0</b>	<b>34.6</b>	<b>0.7</b>
						and	93.0	104.0	11.0	1.2	7.7
						and	<b>111.0</b>	<b>149.0</b>	<b>38.0</b>	<b>2.6</b>	<b>26.6</b>
						and	152.0	155.0	3.0	1.9	2.1
						and	168.0	171.0	3.0	2.4	2.1
						and	175.0	178.0	3.0	1.2	2.1
NSRJRC11254	285444	7060605	554	-60	150	240.0	76.0	78.0	2.0	1.8	1.4
						and	173.0	193.0	20.0	1.3	14.0
						and	227.0	229.0	2.0	6.3	1.4
NSRJRC11255	285423	7060593	554	-60	150	240.0	175.0	177.0	2.0	3.6	1.4
						and	<b>183.0</b>	<b>202.0</b>	<b>19.0</b>	<b>2.9</b>	<b>13.3</b>
						and	205.0	209.0	4.0	1.6	2.8
						and	237.0	239.0	2.0	3.7	1.4
NSRJRC11256	285451	7060494	554	-60	150	50.0			NSI		
NSRJRC11257	285438	7060516	554	-60	150	90.0	<b>9.0</b>	<b>31.0</b>	<b>22.0</b>	<b>2.4</b>	<b>15.4</b>
						and	50.0	55.0	5.0	5.8	3.5
						and	66.0	67.0	1.0	6.8	0.7
						and	89.0	90.0	1.0	5.5	0.7
NSRJRC11264	285383	7060512	554	-60	150	140.0	21.0	23.0	2.0	1.0	1.4
						and	33.0	38.0	5.0	4.4	3.5
						and	<b>60.0</b>	<b>77.0</b>	<b>17.0</b>	<b>2.0</b>	<b>11.9</b>
						and	85.0	87.0	2.0	2.1	1.4
						and	98.0	101.0	3.0	1.3	2.1
NSRJRC11265	285370	7060534	554	-60	150	190.0	92.0	95.0	3.0	1.8	2.1
						and	97.0	102.0	5.0	1.6	3.5
						and	112.0	115.0	3.0	1.7	2.1
						and	123.0	124.0	1.0	4.8	0.7
						and	147.0	153.0	6.0	2.1	4.2
						and	167.0	171.0	4.0	1.2	2.8
NSRJRC11266	285358	7060555	554	-60	150	240.0	206.0	220.0	14.0	1.0	9.8
NSRJRC11267	285336	7060543	554	-60	150	240.0	144.0	145.0	1.0	2.3	0.7
						and	219.0	222.0	3.0	1.8	2.1
						and	228.0	236.0	8.0	1.4	5.6
NSRJRC11268	285365	7060444	554	-60	330	100.0	13.0	30.0	17.0	3.8	8.5
						and	61.0	66.0	5.0	1.5	2.5
NSRJRD10460	285456	7060532	554	-60	150	105.4	11.0	24.0	13.0	2.3	9.1
						Including	20.5	21.0	0.5	26.2	0.4
						and	28.5	35.5	7.0	2.6	4.9
						and	46.1	46.7	0.6	11.7	0.4
NSRJRD10461	285527	7060608	554	-60	150	150.6	40.0	42.5	2.5	1.5	1.8
						and	67.4	68.3	0.9	6.7	0.6
						and	<b>72.0</b>	<b>92.0</b>	<b>20.0</b>	<b>8.0</b>	<b>14.0</b>
						Including	<b>86.6</b>	<b>88.8</b>	<b>2.2</b>	<b>31.5</b>	<b>1.5</b>
						and	99.4	101.4	2.0	11.6	1.4
						and	108.8	109.1	0.3	6.4	0.2
						and	121.5	123.5	2.0	2.0	1.4
						and	132.5	134.0	1.5	1.3	1.1
NSRJRD10462	285551	7060670	554	-60	150	235.0	38.4	39.0	0.6	2.5	0.4
						and	86.2	<b>104.5</b>	<b>18.4</b>	<b>2.1</b>	<b>12.8</b>
						Including	99.7	100.0	0.3	35.6	0.2
						and	124.8	125.3	0.6	3.4	0.4
						and	141.3	144.5	3.2	4.2	2.2
						and	166.3	166.9	0.6	18.8	0.4
						and	233.0	234.0	1.0	2.0	0.7



Table 2 - EKJV Significant Intersections

EKJV SIGNIFICANT INTERSECTIONS - HORNET																	
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)						
HORGC17039	9815	15693	5770	29	288	31.1	9.4	10.0	0.6	11.0	0.4						
						and	12.8	13.8	1.0	5.7	0.7						
						and	23.0	24.0	1.0	5.7	0.7						
						and	30.6	31.1	0.4	5.6	0.3						
HORGC17040	9813	15707	5767	-30	310	20.0	3.0	6.0	3.0	2.5	2.0						
HORGC17041	9814	15717	5770	28	287	33.0	1.1	2.4	1.3	8.2	1.2						
HORGC17042	9815	15722	5768	-10	309	20.1	<b>1.0</b>	<b>6.6</b>	<b>5.6</b>	<b>17.7</b>	<b>4.5</b>						
						HORGC17043	9815	15746	5770	29	257	33.0	<b>1.0</b>	<b>7.1</b>	<b>6.1</b>	<b>6.7</b>	<b>5.3</b>
HORGC17045	9812	15754	5768	-14	292	22.0	<b>0.0</b>	<b>7.0</b>	<b>7.0</b>	<b>4.5</b>	<b>6.3</b>						
						HORGC17046	9812	15761	5771	28	304	45.0	<b>5.0</b>	<b>8.3</b>	<b>3.3</b>	<b>20.7</b>	<b>2.6</b>
						and	and	and	<b>9.7</b>	<b>11.9</b>	<b>2.2</b>	<b>15.2</b>	<b>1.7</b>				
						and	and	and	17.4	17.9	0.5	6.5	0.4				
HORGC17047	9809	15771	5768	-30	281	26.1	<b>2.0</b>	<b>6.5</b>	<b>4.5</b>	<b>6.1</b>	<b>3.7</b>						
						and	8.3	9.2	0.9	12.1	0.8						
						and	10.0	10.3	0.3	11.1	0.3						
						HORGC17048	9807	15782	5769	-15	293	20.4	1.3	2.0	0.7	21.0	0.7
HORGC17049	9802	15799	5771	28	279	17.7	12.9	13.5	0.6	2.5	0.5						
						HORGC17050	9802	15803	5769	-37	284	19.0	9.0	10.0	1.0	4.5	0.7
						HORGC17051	9801	15817	5770	-4	307	45.2	4.0	6.0	2.0	4.1	1.7
						and	and	and	8.9	9.3	0.4	5.2	0.3				
HORGC17052	9799	15830	5772	30	310	20.5	4.3	4.6	0.3	8.1	0.2						
						HORGC17053	9802	15845	5772	7	310	23.3			NSI		
						HORGC17054	9800	15864	5773	24	302	45.4			NSI		
						HORGC17055	9800	15879	5772	3	304	33.4			NSI		
HORGC17056	9799	15900	5774	24	315	18.1			NSI								
HORGC17067	9801	15917	5773	0	311	21.3	2.7	3.8	1.1	3.1	0.9						
HORGC17073	9799	15935	5773	-4	322	24.5			NSI								
HORGC17074	9801	15948	5773	-6	322	27.2	0.0	1.4	1.4	3.9	0.9						
HORGC17075	9802	15964	5773	-3	327	and	17.0	19.5	2.5	4.4	1.6						
						and	30.1	0.0	0.6	0.6	5.4	0.4					
						and	3.9	6.7	2.9	2.6	1.7						
						HORGC17076	9804	15982	5773	-7	323	27.0	2.5	5.5	3.0	3.4	2.0
HORGC17077	9802	15964	5772	-38	316	41.1	0.0	3.2	3.2	9.3	1.7						
HORGC17078	9804	15981	5772	-38	315	and	12.0	13.0	1.0	5.2	0.5						
						and	38.9	0.0	2.0	2.0	4.2	1.8					
						and	5.0	6.0	1.0	4.9	0.9						
						HORGC17188	9800	15765	5747	7	273	57.1	0.0	3.7	3.7	3.1	3.3
HORGC17189	9796	15781	5748	23	246	and	15.7	16.7	1.0	8.1	0.7						
						and	35.6	36.0	0.4	6.8	0.4						
						and	0.0	1.7	1.7	4.2	1.7						
						and	11.1	11.8	0.8	11.1	0.7						
HORGC17191	9794	15798	5748	3	272	and	6.2	6.5	0.4	13.7	0.3						
						and	9.6	10.5	0.9	2.9	0.8						
						and	<b>12.6</b>	<b>13.6</b>	<b>1.0</b>	<b>30.3</b>	<b>0.9</b>						
						and	40.6	41.1	0.5	13.9	0.5						
HORGC17193	9792	15837	5749	1	290	33.1	10.9	12.1	1.2	2.2	1.1						
HORGC18001	9811	15794	5789	6	310	18.1	11.5	12.1	0.6	22.1	0.5						
HORGC18002	9812	15783	5789	2	315	16.3	0.0	2.7	2.7	5.7	2.0						
HORGC18003	9815	15774	5789	5	295	and	8.7	9.5	0.8	3.7	0.7						
						and	23.9	3.2	5.2	2.0	15.4	1.8					
						and	8.4	8.8	0.5	8.0	0.4						
						HORGC18003	9815	15774	5789	5	295	19.0	19.0	19.8	0.8	4.1	0.7
HORGC18004	9819	15762	5789	1	298	24.2	0.0	4.8	4.8	4.2	4.4						
HORRSD17067	9624	16089	5696	-24	73	and	6.6	7.5	0.9	4.8	0.8						
						and	8.7	10.6	1.9	3.9	1.8						
						and	16.3	17.0	0.7	16.5	0.6						
						HORRSD17067	9624	16089	5696	-24	73	168.0	84.6	85.9	1.3	6.2	1.1
HORRSD17068	9624	16089	5696	-32	88	168.0	<b>69.7</b>	<b>75.3</b>	<b>5.6</b>	<b>5.8</b>	<b>5.0</b>						
HORRSD17070	9624	16090	5696	-53	79	201.0	158.7	159.3	0.6	5.8	0.4						
HORRSD17071	9624	16088	5696	-55	116	227.4	79.7	81.2	1.5	2.1	1.0						
HORRSD17072	9624	16089	5696	-67	97	and	<b>172.0</b>	<b>172.4</b>	<b>0.4</b>	<b>81.3</b>	<b>0.3</b>						
						and	<b>172.4</b>	<b>180.5</b>	<b>14.4</b>	<b>4.4</b>	<b>7.7</b>						
						and	191.0	192.8	1.8	3.6	1.1						
						HORRSD17072	9624	16089	5696	-67	97	260.8	217.7	218.5	0.8	3.5	0.4
HORRSD17081	9626	15710	5752	-51	54	246.0	216.9	217.3	0.4	3.5	0.3						
HORRSD17082	9626	15710	5752	-60	52	276.1	68.7	69.6	0.9	3.2	0.8						
HORRSD17083	9624	15725	5752	-46	68	and	258.6	259.9	1.3	1.9	1.0						
						HORRSD17084	9624	15726	5752	-53	56	248.4	199.9	200.7	0.8	2.4	0.5
						and	and	and	238.5	239.5	1.0	3.8	0.7				
						and	and	and	243.0	243.9	0.9	2.8	0.6				
HORRSD17085	9624	15727	5752	-65	44	387.0	102.0	102.4	0.4	3.6	0.2						
HORRSD17086	9632	15902	5727	27	77	237.5	215.8	216.1	0.4	6.1	0.3						
HORRSD17087	9632	15903	5727	26	66	254.7	176.0	176.8	0.8	9.5	0.6						
HORRSD17088	9632	15903	5727	6	61	and	188.7	190.7	2.0	5.0	1.5						
						and	and	and	213.9	214.2	0.3	34.2	0.2				
						and	and	and	228.8	229.1	0.3	13.6	0.3				
						HORRSD17088	9632	15903	5727	6	61	335.8	176.7	177.1	0.4	6.3	0.3
HORRSD17089	9632	15903	5727	24	57	290.6	175.1	177.3	2.2	3.3	1.2						
HORRSD17090	9632	15903	5727	17	55	and	and	and	2.2	3.3	1.2						
						and	and	and	248.1	249.4	1.3	11.4	0.8				
						and	and	and	254.0	254.4	0.4	5.4	0.3				
						and	and	and	281.5	282.2	0.7	3.8	0.5				
HORRSD17091	9632	15903	5727	10	54	248.9	213.8	214.3	0.6	6.4	0.5						
HORRSD17092	9618	15521	5751	-68	88	and	214.7	218.0	3.3	6.7	2.5						
HORRSD17092	9618	15521	5751	-68	88	462.0	416.3	417.6	1.3	12.6	0.6						
						and	420.3	421.6	1.3	4.8	0.6						



## EKJV SIGNIFICANT INTERSECTIONS - HORNET

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
						and	425.2	426.1	0.9	5.7	0.4
						and	428.0	428.4	0.4	15.6	0.1
HORRSD17093	9618	15521	5751	-71	86	555.0	38.1	38.7	0.6	2.5	0.5
HORRSD17094	9619	15456	5743	-52	99	317.8	306.5	306.8	0.3	40.0	0.2
HORRSD17095	9619	15456	5743	-59	98	353.0	46.0	47.0	1.0	2.2	0.9
HORRSD17095	9619	15454	5743	-59	98	353.0	316.7	317.5	0.8	9.5	0.8
HORRSD17108	9632	15902	5729	-11	57	203.8	130.5	130.8	0.3	4.7	0.3
						and	133.9	134.8	0.9	10.8	0.8
						and	151.3	152.0	0.7	7.3	0.6
						and	160.9	161.3	0.4	31.4	0.3
						and	195.0	196.0	1.0	4.6	0.6
HORRSD17109	9632	15902	5726	-28	109	180.0	76.5	77.0	0.5	60.3	0.3
						and	133.0	133.8	0.8	6.0	0.5
						and	139.0	140.5	1.5	5.0	1.0
						and	159.0	160.0	1.0	2.7	2.0
						and	167.4	168.4	0.9	5.7	0.7
						and	176.3	176.7	0.4	8.0	0.2
HORRSD17110	9632	15902	5726	-62	81	236.4	67.3	67.6	0.3	6.8	0.2
						and	220.0	221.6	1.6	2.5	0.8
HORRSD17111	9632	15903	5726	-65	82	292.1	209.0	209.6	0.6	20.5	0.3
HORRSD17112	Including					362.9	<b>322.2</b>	<b>325.5</b>	<b>3.3</b>	<b>102.7</b>	<b>1.2</b>
HORRSD17114	9624	15725	5752	-62	73	304.3				NSI	
HORRSD17115	9624	15727	5752	-59	58	275.8	262.9	266.4	3.5	14.4	1.3
						and	266.0	266.7	0.7	6.4	0.3
HORRSD17116	9625	15727	5752	-57	43	297.0	102.1	102.5	0.4	25.2	0.2
						and	281.7	282.2	0.6	4.9	0.2
HORRSD17117	9624	15727	5752	-56	32	375.0	115.9	118.1	2.2	4.1	0.5
						and	327.6	328.0	0.4	13.5	0.1
						and	332.0	333.0	1.0	3.2	0.3
HORRSD17118	9624	15727	5752	-61	36	395.4	107.5	108.7	1.2	9.1	0.3
							357.1	359.7	2.6	6.8	2.6
							360.7	363.0	2.3	4.3	2.3
HORRSD17119	9624	15727	5752	-61	47	339.0	100.0	102.9	2.9	2.8	1.1
HORRSD17119	9624	15727	5752	-61	47	and	<b>311.1</b>	<b>311.7</b>	<b>0.6</b>	<b>79.2</b>	<b>0.4</b>
HORRT17023	9624	16090	5696	-44	104	188.6	139.9	142.7	2.8	1.7	2.2
HORRT17024	9624	16090	5696	-62	87	239.9	179.5	183.0	3.5	2.6	1.4
HORRT17025	9624	16090	5696	-68	67	325.0	254.1	254.7	0.6	6.6	0.3
HORRT17026	9624	16090	5696	-71	98	356.9	347.6	348.1	0.5	42.5	0.3
HORRT17036	9632	15905	5725	-67	47	350.9	289.2	290.3	1.1	5.7	0.2
HORRT17061	9614	15602	5762	-72	51	605.6	<b>563.8</b>	<b>571.3</b>	<b>7.5</b>	<b>13.0</b>	<b>3.0</b>
						and	<b>571.9</b>	<b>574.0</b>	<b>2.1</b>	<b>53.0</b>	<b>0.8</b>
						and	601.3	602.2	0.9	22.4	0.1
HORRT17063	9620	15443	5742	-70	114	689.9	66.4	67.0	0.6	9.2	0.5
						and	605.0	614.0	9.0	4.2	4.0
						and	617.0	618.0	1.0	3.0	0.8
						and	624.1	625.0	1.0	3.1	0.7
HORRT17064	9620	15443	5742	-61	137	603.1	121.0	122.0	1.0	13.2	1.0
HORRT17065	9620	15443	5742	-69	131	698.8	15.0	15.6	0.6	2.4	0.5
						and	165.3	165.6	0.3	12.4	0.2
						and	165.3	165.6	0.3	12.4	0.2
						and	630.2	631.8	1.7	2.8	0.8
						and	<b>664.3</b>	<b>666.1</b>	<b>1.8</b>	<b>70.7</b>	<b>0.7</b>
HORRT17066	9620	15454	5742	-76	90	521.6			NSI		

## EKJV SIGNIFICANT INTERSECTIONS - RUBICON

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
RUBGC17084	9844	16369	5919	38	264	29.4	6.7	7.1	0.4	14.4	0.4
						and	17.7	18.7	1.0	20.1	0.9
RUBGC17085	9844	16391	5920	42	267	32.3	<b>0.3</b>	<b>12.0</b>	<b>11.7</b>	<b>9.9</b>	<b>10.0</b>
						and	15.0	16.0	1.0	3.6	0.9
RUBGC17086	9844	16397	5917	-24	263	32.1	<b>0.0</b>	<b>9.0</b>	<b>9.0</b>	<b>3.5</b>	<b>7.6</b>
						and	18.0	19.0	1.0	7.2	1.0
						and	<b>25.2</b>	<b>29.1</b>	<b>3.9</b>	<b>6.3</b>	<b>3.9</b>
RUBGC17087	9832	16475	5918	-53	256	20.6	1.3	2.4	1.1	4.7	1.1
RUBGC17088	9832	16476	5921	37	259	20.6	1.1	1.5	0.4	5.2	0.4
						and	2.7	3.5	0.8	4.1	0.7
RUBGC17089	9828	16503	5922	43	263	20.3	0.0	1.5	1.5	3.6	1.5
						and	3.9	4.3	0.5	4.3	0.5
RUBGC17090	9857	16304	5919	38	255	23.3			NSI		
RUBGC17091	9862	16286	5919	36	252	35.4			NSI		
RUBGC17092	9866	16254	5918	9	282	26.6			NSI		
RUBGC17093	9865	16228	5920	34	273	26.5	14.6	15.0	0.4	11.4	0.4
RUBGC17094	9853	16180	5919	-25	270	23.6			NSI		
RUBGC17095	9851	16162	5920	-3	244	20.1			NSI		
RUBGC17096	9852	16087	5923	35	260	29.5			NSI		
RUBGC17099	9854	16017	5921	-17	261	33.0			NSI		
RUBGC17100	9853	15988	5924	29	268	30.8			NSI		
RUBGC17104	9848	16338	5899	35	262	17.5	5.4	9.1	3.7	2.4	3.1
RUBGC17105	9843	16358	5897	1	261	29.7	3.3	6.2	2.9	6.5	2.8
RUBGC17106	9843	16358	5900	40	277	29.4	1.7	3.7	2.0	2.4	1.8
RUBGC17107	9841	16386	5898	2	271	29.7	0.4	8.1	7.7	2.2	6.2
						and	15.2	18.8	3.6	2.6	2.8
RUBGC17110	9859	16280	5897	-10	249	30.1	28.2	28.7	0.5	17.1	0.5
RUBGC17111	9858	16211	5900	28	280	35.9	6.4	6.7	0.3	3.6	0.3
						and	25.8	26.3	0.5	3.8	0.5
RUBGC17115	9845	16066	5901	-3	255	24.0	4.7	5.2	0.5	13.6	0.5
RUBGC17116	9847	16039	5902	-11	262	33.1	31.7	32.1	0.4	7.9	0.3
RUBRT17058	9734	16611	5959	-68	274	50.9	24.5	25.4	0.9	4.3	0.6
						and	30.1	31.1	1.0	5.2	0.6
RUBGC17217	9855	16275	5877	1	254	32.0	0.7	1.9	1.2	2.7	1.2
						and	19.7	20.4	0.7	12.5	0.7



## EKJV SIGNIFICANT INTERSECTIONS - RUBICON

Drill Hole #	Eastings (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
RUBGC17218	9845	16208	5880	27	261	31.0	2.5	3.8	1.3	3.3	1.3
						and	21.0	22.0	1.0	2.4	1.0
						and	24.9	25.2	0.3	10.1	0.3
						and	30.5	31.0	0.5	6.0	0.4
RUBGC17219	9840	16088	5880	-11	252	26.0	2.0	3.3	1.3	4.6	1.1
RUBGC17220	9842	16050	5881	-9	254	42.0	7.4	8.1	0.6	11.4	0.6
						and	41.4	42.0	0.6	2.8	0.5
RUBRS17123	9624	16092	5696	-9	6	425.7	148.0	149.0	1.0	4.6	0.8
						and	160.9	162.5	1.7	7.5	1.4
						and	165.5	166.0	0.6	4.3	0.5
RUBRS17124	9624	16092	5697	-14	16	254.8	148.7	151.0	2.3	2.8	2.0
						and	202.2	202.6	0.4	4.3	0.3
						and	245.3	246.2	1.0	10.2	0.7
RUBRS17125	9624	16092	5697	-18	52	227.9	68.0	69.0	1.0	6.0	0.7
						and	119.3	119.8	0.5	8.6	0.3
						and	126.1	128.3	2.2	3.9	1.4
						and	181.6	182.2	0.6	7.1	0.5
RUBRS17126	9624	16092	5697	-38	46	267.0	199.2	201.1	1.9	3.3	1.2
RUBRS17127	9624	16092	5697	-49	47	296.8	211.2	213.0	1.8	3.9	1.1
RUBRS17128	9624	16092	5696	-51	7	371.5	91.5	92.1	0.6	6.1	0.5
						and	100.5	101.0	0.5	56.0	0.4
						and	175.7	176.0	0.4	10.9	0.3
RUBRS17129	9624	16092	5696	-58	11	358.7	100.2	102.0	1.8	12.5	1.7
						and	249.0	251.0	2.0	3.2	2.0
RUBRS17130	9624	16092	5696	-57	30	398.9	102.0	103.3	1.3	5.7	0.3
						and	105.6	107.2	1.6	26.6	0.1
						and	242.0	242.5	0.6	10.4	0.4
						and	320.1	321.6	1.5	3.2	1.0
RUBRS17131	9624	16092	5697	-58	27	503.9	111.0	114.3	3.3	3.3	3.3
						and	353.0	354.2	1.2	3.2	1.2
						and	359.8	361.1	1.3	4.1	1.0
						and	361.6	362.2	0.6	2.6	0.5
						and	401.6	401.9	0.3	27.8	0.2
						and	454.2	454.8	0.6	6.9	0.4
RUBRS17132	9624	16092	5697	-62	28	392.0	106.2	108.7	2.5	3.8	2.5
						and	112.6	113.2	0.6	7.3	0.5
						and	338.4	338.7	0.3	5.1	0.2
RUBRS17134	9624	16092	5697	-67	31	161.1	106.7	107.6	0.8	15.7	0.6
RUBRS17153	9619	16257	5672	-9	54	212.1	187.5	189.0	1.5	2.9	1.2
						and	196.5	197.7	1.2	9.8	0.5
RUBRS17154	9619	16256	5670	-24	82	209.9	154.1	154.6	0.5	3.6	0.4
RUBRS17159	9619	16256	5670	-17	30	322.0	251.8	252.5	0.8	3.4	0.5
RUBRS17172	9620	16257	5670	1	30	354.2	164.7	165.2	0.5	3.0	0.5
						and	289.9	291.4	1.5	4.5	1.0
						and	293.0	293.6	0.6	4.6	0.5
						and	302.7	303.4	0.7	6.6	0.6
						and	313.0	313.8	0.9	3.9	0.8
						and	316.8	317.7	0.9	5.9	0.7
RUBRS17173	9619	16258	5673	-3	26	348.1	311.5	312.0	0.5	21.9	0.3
						and	317.6	322.0	4.5	13.3	1.6
RUBRS17173						Including	319.9	321.1	1.1	42.7	0.4
RUBRS17174	9619	16256	5670	1	353	428.0	371.2	371.6	0.4	5.6	0.3
RUBRS17175	9619	16256	5670	-2	349	467.1	355.9	356.6	0.7	4.1	0.7
						and	420.7	421.5	0.8	18.1	0.8
						and	444.7	445.3	0.6	6.6	0.5
RUBRS17176	9618	16259	5672	-4	25	398.9	334.3	335.0	0.7	4.5	0.4
						and	337.9	340.3	2.4	7.0	1.3
RUBRT17058	9734	16611	5959	-68	274	50.9	35.8	37.9	2.1	4.7	1.2
RUBRT17059	9735	16641	5957	-68	271	42.0	10.8	12.1	1.3	2.4	0.8
RUBRT17060	9741	16642	5957	-18	84	36.0	9.4	10.1	0.7	15.6	0.6
RUBRT17061	9738	16656	5956	-89	357	42.0	12.7	13.8	1.1	5.5	1.0
RUBRT17062	9742	16656	5959	16	95	48.0	11.4	13.9	2.6	3.6	2.3
RUBRT17064	9742	16670	5956	-7	92	26.1	2.2	4.0	1.8	3.2	0.9
RUBRT17065	9740	16686	5955	-84	29	33.0	25.5	30.9	5.4	3.5	4.3
RUBRT17067	9742	16715	5954	-88	62	30.0	4.9	8.2	3.4	2.7	3.0
						and	14.6	15.6	1.0	18.6	0.3
RUBRT17068	9744	16715	5956	25	96	33.0	11.6	12.3	0.6	3.8	0.4
RUBRT17069	9742	16670	5956	26	91	41.9	1.1	3.3	2.2	5.4	1.7
						and	9.4	9.7	0.4	18.8	0.4
RUBRT17070	9743	16678	5957	10	67	32.9	20.5	21.3	0.8	7.8	0.5
RUBRT17071	9743	16700	5959	38	93	41.9	29.6	30.0	0.4	4.9	0.3
						and	41.2	41.9	0.7	5.2	0.3
RUBRT17072	9743	16700	5959	26	30	50.6	37.9	40.0	2.1	6.3	1.0
RUBRT17073	9734	16624	5958	-49	275	78.0	52.5	56.0	3.6	12.6	1.5
RUBRT17074	9735	16655	5956	-47	277	72.0	62.6	63.3	0.7	25.0	0.3
RUBRT17077	9739	16716	5954	-30	306	117.0	94.3	95.0	0.8	10.6	0.7
RUBRT17079	9739	16716	5954	-29	290	147.0			NSI		
RUBRT17082	9734	16611	5959	-40	266	96.2	52.9	56.1	3.1	3.4	2.8
RUBRT17083	9736	16670	5956	-32	274	140.5	54.0	55.1	1.1	2.6	0.9
RUBRT17118	9624	16092	5696	-26	47	251.8	194.4	195.7	1.3	2.9	1.0
RUBRT17119	9624	16092	5696	-41	9	323.8	98.9	99.4	0.5	5.7	0.4
						and	99.8	100.1	0.3	6.1	0.3
						and	101.5	104.4	2.9	6.7	2.8
RUBRT17120	9624	16092	5697	-51	29	335.8	303.2	305.5	2.3	4.2	0.7
RUBRT17121	9624	16092	5697	-63	34	443.9	104.0	108.0	4.0	10.4	1.2
						and	368.4	370.7	2.3	3.6	2.0
						and	377.4	378.0	0.6	4.5	0.4
						and	390.4	391.0	0.6	14.8	0.3
RUBRT17122	9623	16092	5696	-56	21	435.0	116.2	119.2	3.1	1.3	2.8
RUBRT17135	9620	16257	5670	-20	63	221.8	165.2	165.8	0.6	9.2	0.5
						and	168.5	169.7	1.1	5.2	1.0
						and	206.5	206.8	0.3	77.9	0.2
						and	207.6	209.2	1.6	39.0	0.1
RUBRT17136	9619	16256	5671	-38	50	248.8	189.8	190.2	0.5	2.3	0.4
RUBRT17137	9619	16256	5671	-53	45	302.9	80.4	81.5	1.0	6.6	0.5
RUBRT17138	9619	16256	5671	-61	40	362.8	123.7	124.0	0.4	19.6	0.3



## EKJV SIGNIFICANT INTERSECTIONS - RUBICON

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
RUBRT17140	9619	16258	5671	-38	32	320.8	315.9	316.2	0.3	11.0	0.3
RUBRT17142	9620	16257	5670	-61	357	468.5	101.0	102.0	1.0	4.9	1.0
						and	424.5	425.0	0.5	2.5	0.5
RUBRT17143	9620	16257	5670	-13	358	351.5	103.0	104.0	1.0	3.5	0.4
						and	297.1	299.7	2.6	6.2	1.2
						and	297.5	298.3	0.8	14.8	0.4

## EKJV SIGNIFICANT INTERSECTIONS - PEGASUS

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
PEGGC17135	9809	17278	5936	0	263	18.1	2.0	3.0	1.0	8.5	1.0
						and	6.4	7.8	1.4	11.7	1.4
PEGGC17149	9813	17193	5913	11	274	22.0	13.9	14.6	0.6	2.1	0.6
PEGGC17150	9813	17205	5913	8	260	26.0	14.3	16.0	1.7	11.6	1.7
PEGGC17151	9811	17221	5914	7	266	24.0	0.0	0.9	0.9	16.0	0.9
						and	4.8	5.3	0.5	2.2	0.5
						and	13.1	13.6	0.5	29.1	0.5
PEGPH17230	9827	16917	6169	-34	286	99.2	17.5	18.5	1.0	4.9	0.6
PEGPH17232	9744	16932	6110	-32	68	72.5	0.8	3.3	2.5	2.1	2.5
						and	4.0	4.6	0.6	18.2	0.5
PEGRSD17154	9717	17133	5881	-51	347	180.0	114.0	115.0	1.0	2.5	0.9
						and	133.0	135.0	2.0	4.6	1.4
PEGRSD17155	9717	17133	5881	-63	323	176.9	32.7	34.7	2.0	4.2	0.5
						and	129.4	130.4	1.0	3.2	0.6
PEGRSD17156	9717	17133	5881	-61	1	150.0	102.3	104.0	1.7	2.9	1.2
						and	106.9	107.2	0.3	41.9	0.2
PEGRSD17157	9716	17132	5881	-81	327	137.8	93.6	95.2	1.6	9.4	0.4
PEGRSD17158	9716	17132	5881	-74	272	149.8	30.1	30.4	0.3	40.8	0.2
						and	109.1	111.1	2.1	6.9	1.0
PEGRSD17160	9718	17126	5881	-81	162	128.8	<b>83.4</b>	<b>83.7</b>	<b>0.3</b>	<b>138.0</b>	<b>0.3</b>
PEGRSD17162	9727	17143	5882	-20	33	160.1	91.0	92.2	1.3	21.3	0.7
						and	94.1	94.8	0.8	4.6	0.7
						and	<b>115.6</b>	<b>123.8</b>	<b>8.2</b>	<b>10.2</b>	<b>3.6</b>
PEGRSD17164	9728	17135	5882	-15	154	207.3	<b>102.0</b>	<b>106.7</b>	<b>4.7</b>	<b>7.1</b>	<b>4.0</b>
						and	<b>113.9</b>	<b>118.0</b>	<b>4.1</b>	<b>6.2</b>	<b>3.5</b>
						and	<b>126.4</b>	<b>128.6</b>	<b>2.2</b>	<b>42.9</b>	<b>1.5</b>
						and	<b>179.1</b>	<b>180.9</b>	<b>1.8</b>	<b>42.1</b>	<b>1.2</b>
PEGRSD17165	9731	16943	6066	13	207	56.4	21.5	22.4	0.9	7.1	0.5
						and	27.0	27.3	0.3	10.7	0.2
PEGRSD17166	9732	16494	6067	-1	242	243.3	19.3	20.4	1.0	4.2	0.7
						and	31.0	33.1	2.1	8.1	1.5
						and	47.3	48.1	0.7	6.5	0.5
PEGRSD17167	9729	16945	6064	-19	233	185.0	59.0	64.1	5.1	2.9	3.5
PEGRSD17168	9729	16946	6065	-36	247	237.0	131.9	132.7	0.8	4.7	0.3
						and	163.0	164.0	1.0	4.2	0.3
						and	173.0	177.1	4.1	7.6	1.5
PEGRSD17169	9731	16943	6065	-38	258	260.7	105.8	106.6	0.8	3.6	0.6
						and	146.1	147.1	1.0	2.7	0.7
						and	155.7	156.6	0.9	4.8	0.6
						and	158.9	159.5	0.6	25.5	0.4
						and	175.9	176.9	1.0	2.1	0.7
PEGRSD17170	9732	16951	6067	17	325	133.0	52.0	53.0	1.0	6.2	0.7
PEGRSD17171	9735	16951	6064	-21	307	118.0	68.7	69.7	1.0	3.1	0.7
PEGRSD17172	9735	16951	6064	-35	296	147.0	60.0	61.0	1.0	6.3	0.7
						and	103.6	104.4	0.8	4.4	0.6
						and	105.2	105.5	0.3	6.9	0.2
						and	107.9	108.8	1.0	2.7	0.7
PEGRSD17173	9735	16951	6064	-40	291	184.0	62.7	63.1	0.4	3.2	0.3
PEGRSD17175	9733	16951	6066	1	314	123.1	108.8	110.4	1.6	4.2	1.2
PEGRSD17176	9733	16951	6066	-25	291	156.1	<b>118.4</b>	<b>123.0</b>	<b>4.6</b>	<b>7.4</b>	<b>3.5</b>
PEGRSD17177	9733	16951	6066	-35	280	185.8	167.0	173.0	6.0	2.0	4.0
PEGRSD17178	9733	16952	6066	-12	334	171.0	112.6	113.5	0.9	5.3	0.7
						and	115.7	116.6	0.9	5.2	0.7
PEGRSD17179	9732	16952	6065	-28	324	191.9	98.9	100.0	1.1	3.4	0.4
						and	109.0	109.9	0.9	4.9	0.4
						and	113.3	114.2	0.9	2.6	0.7
PEGRSD17180	9732	16952	6065	-36	316	233.9	185.5	189.3	3.7	3.1	3.0
						and	210.0	210.8	0.8	6.6	0.6
PEGRSD17182	9732	16952	6065	-18	336	255.3	57.9	58.5	0.6	2.2	0.4
PEGRSD17183	9733	16952	6065	-30	327	240.0	171.9	175.1	3.3	3.5	1.6
PEGRSD17184	9767	17120	6004	1	326	351.0			NSI		
PEGRSD17185	9767	17121	6004	0	328	369.4			NSI		
PEGRSD17186	9767	17120	6005	-3	289	303.4	152.0	152.9	1.0	2.1	1.0
						and	161.0	162.0	1.0	7.3	1.0
						and	163.1	164.0	1.0	3.2	0.9
						and	277.6	281.6	4.1	2.0	1.2
PEGRSD17187	9767	17120	6004	-4	292	329.6	295.6	297.3	1.7	2.0	1.3
						and	299.3	299.7	0.4	3.6	0.3
						and	303.1	303.8	0.7	2.3	0.5
PEGRSD17188	9767	17120	6005	-4	276	273.4	266.0	268.9	2.9	2.8	2.8
PEGRSD17191	9767	17120	6003	-10	272	308.6	238.0	239.0	1.0	14.4	0.8
						and	243.8	244.5	0.7	9.6	0.5
						and	<b>245.7</b>	<b>249.6</b>	<b>3.9</b>	<b>5.8</b>	<b>3.5</b>
PEGRSD17192	9767	17120	6003	-11	309	342.4	283.2	285.2	2.0	9.7	1.6
PEGRSD17194	9767	17120	6005	-21	261	315.1	33.0	33.3	0.3	4.7	0.3
						and	105.0	109.0	4.0	4.1	3.0
PEGRSD17195	9767	17120	6005	-21	254	294.2	216.0	217.0	1.0	2.7	1.0
						and	246.0	251.0	5.0	2.7	4.6
PEGRSD17196	9780	17109	6043	-15	282	237.0	68.0	73.7	5.7	14.9	5.2
						and	177.0	177.6	0.6	2.7	0.6
						and	208.6	212.5	3.9	2.5	1.4
PEGRSD17197	9780	17109	6043	-12	262	237.0	56.2	57.0	0.8	9.5	0.8

## EKJV SIGNIFICANT INTERSECTIONS - PEGASUS

Drill Hole #	Eastings (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
						66.5	68.1	1.7	2.8	1.6	
						and	156.3	156.6	0.3	16.5	0.3
						and	220.2	222.8	2.5	3.6	2.5
PEGRSD17198	9780	17109	6043	-11	297	264.4	<b>66.2</b>	<b>71.1</b>	<b>4.9</b>	<b>19.2</b>	<b>3.4</b>
						and	<b>231.0</b>	<b>233.4</b>	<b>2.5</b>	<b>28.7</b>	<b>2.1</b>
PEGRSD17199	9780	17109	6043	-9	284	234.4	57.5	59.3	1.8	5.5	1.0
PEGRSD17200	9780	17109	6043	-4	275	255.3	160.0	163.8	3.8	3.8	0.9
						and	163.4	163.8	0.4	11.1	0.3
PEGRSD17201	9780	17109	6043	-1	284	225.3	49.4	51.4	2.0	4.0	1.2
						and	156.4	158.4	2.0	3.5	1.5
PEGRSD17202	9779	17109	6043	-2	288	297.2	58.2	58.7	0.5	3.0	0.5
						and	124.9	126.0	1.1	11.8	1.0
						and	130.0	130.5	0.5	3.3	0.5
						and	246.0	247.5	1.5	6.1	1.4
						and	251.0	251.5	0.5	4.7	0.5
PEGRSD17203	9780	17110	6043	2	295	246.4	169.4	172.4	3.0	3.5	2.8
						and	177.5	178.0	0.5	2.5	0.5
PEGRSD17204	9779	17109	6043	9	253	213.3	53.8	54.2	0.4	7.9	0.4
						and	126.0	126.7	0.7	2.3	0.7
						and	130.9	132.0	1.1	3.5	1.0
						and	138.5	142.7	4.2	7.6	4.0
PEGRSD17205	9780	17110	6044	10	274	290.1	46.0	48.5	2.6	2.4	2.0
						and	180.4	182.0	1.6	2.3	1.4
						and	<b>187.7</b>	<b>190.9</b>	<b>3.2</b>	<b>1183.6</b>	<b>3.1</b>
PEGRSD17205						Including	<b>187.7</b>	<b>188.1</b>	<b>0.4</b>	<b>616.0</b>	<b>0.4</b>
PEGRSD17205						Including	<b>188.1</b>	<b>188.4</b>	<b>0.3</b>	<b>3260.0</b>	<b>0.3</b>
PEGRSD17205						Including	<b>189.3</b>	<b>189.8</b>	<b>0.5</b>	<b>330.0</b>	<b>0.5</b>
PEGRSD17205						Including	<b>189.8</b>	<b>190.1</b>	<b>0.3</b>	<b>6300.0</b>	<b>0.3</b>
PEGRSD17205						Including	<b>190.1</b>	<b>190.4</b>	<b>0.3</b>	<b>1060.0</b>	<b>0.3</b>
						and	284.0	285.0	1.0	2.8	0.8
PEGRSD17206	9780	17110	6044	8	309	252.3	201.0	202.4	1.4	2.3	0.8
						and	210.0	210.3	0.4	6.6	0.3
						and	214.9	216.5	1.6	4.4	1.3
PEGRSD17207	9780	17110	6045	28	298	176.7	125.7	127.5	1.8	3.4	1.7
PEGRSD17208	9780	17110	6044	23	307	185.7	111.2	111.7	0.5	10.0	0.3
						and	155.0	156.0	1.0	14.6	0.7
PEGRSD17209	9780	17110	6044	19	319	231.1	191.2	192.7	1.5	10.3	1.0
PEGRSD17210	9781	17111	6044	17	325	243.0	205.0	205.6	0.6	4.1	0.1
						and	212.0	216.2	4.2	14.7	0.5
PEGRSD17211	9781	17111	6044	16	332	258.1	250.7	251.2	0.5	6.6	0.3
PEGRSD17212	9781	17111	6045	23	331	241.0	220.7	221.9	1.2	6.5	1.0
PEGRSD17213	9781	17111	6045	21	336	263.7	12.4	12.8	0.4	4.1	0.3
						and	213.9	214.5	0.6	11.0	0.3
PEGRSD17216	9781	17111	6046	37	337	212.8	182.0	183.7	1.7	8.0	0.6
						and	<b>190.6</b>	<b>198.4</b>	<b>7.8</b>	<b>5.4</b>	<b>4.0</b>
PEGRSD18007	9695	17050	5916	-79	292	201.0	49.2	50.9	1.7	3.2	1.7
PEGRSD18008	9695	17050	5916	-67	334	233.8	118.6	118.9	0.3	2.0	0.1
PEGRT17121	9742	16815	5950	12	244	21.0	7.4	13.2	5.8	2.1	5.3



**Table 3 - Kundana Significant Intersections**

KUNDANA SIGNIFICANT INTERSECTIONS - HELGA'S											
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
BARRSD17001	9121	20914	6243	-46	116	93.1	65.9	67.2	1.3	7.1	0.9
BARRSD17002	9121	20914	6241	-31	51	129.9	105.2	108.6	3.4	4.0	2.4
						and	<b>116.2</b>	<b>116.5</b>	<b>0.3</b>	<b>194.0</b>	<b>0.2</b>
BARRSD17003	9122	20913	6241	-26	118	93.0	69.0	69.3	0.3	3.8	0.2
BARRSD17004	9121	20914	6241	-20	56	147.0			NSI		
BARRSD17005	9121	20914	6243	-24	94	93.1	<b>77.8</b>	<b>79.5</b>	<b>1.8</b>	<b>35.7</b>	<b>1.2</b>
BARRSD17006	9121	20914	6243	-11	83	149.4			NSI		
BARRSD17007	9121	20914	6241	-5	39	174.0			NSI		
BARRSD17008	9121	20912	6243	-8	104	123.0	<b>97.5</b>	<b>97.9</b>	<b>0.4</b>	<b>132.0</b>	<b>0.3</b>
						and	<b>105.1</b>	<b>106.9</b>	<b>1.7</b>	<b>50.2</b>	<b>1.2</b>
						and	<b>110.8</b>	<b>111.4</b>	<b>0.6</b>	<b>53.1</b>	<b>0.5</b>
BARRSD17009	9121	20914	6241	2	49	168.4			NSI		
BARRSD17010	9121	20913	6243	15	94	201.0	169.6	171.0	1.5	1.8	1.1
BARRSD17011	9121	20914	6241	-23	48	105.0	89.4	91.1	1.7	6.2	1.2
BARRSD17012	9139	20845	6251	-56	139	68.0	42.6	43.9	1.3	1.8	
BARRSD17013	9139	20846	6251	-26	97	69.1	43.7	44.5	0.8	2.4	0.6
BARRSD17014	9139	20845	6251	-25	131	83.7	38.1	39.0	1.0	8.7	0.8
BARRSD17015	9137	20845	6251	-76	133	83.2	54.0	54.3	0.3	12.1	0.3
BARRSD17016	9139	20846	6252	-4	137	93.0			NSI		
BARRSD17017	9139	20846	6252	-1	91	99.1	68.8	69.1	0.3	2.1	0.3
BARRSD17018	9139	20846	6252	4	72	155.0			NSI		
BARRSD17019	9139	20846	6253	14	87	108.0			NSI		
BARRSD17020	9139	20846	6253	12	75	105.0			NSI		

KUNDANA SIGNIFICANT INTERSECTIONS - MILLENNIUM											
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
MILLGC17001	9607	21300	6053	-28	30	108.7	88.8	90.0	1.2	11.8	0.8
MILLGC17002	9607	21300	6053	-36	40	93.0	69.4	70.4	1.0	16.4	0.7
MILLGC17003	9607	21300	6053	-47	36	101.2	78.9	79.2	0.3	7.6	0.2
MILLGC17004	9607	21300	6053	-49	23	132.0	<b>113.1</b>	<b>114.4</b>	<b>1.3</b>	<b>47.3</b>	<b>0.8</b>
MILLGC17005	9607	21300	6053	-64	23	150.3	<b>118.5</b>	<b>121.0</b>	<b>2.5</b>	<b>42.4</b>	<b>1.7</b>
MILLGC17006	9609	21299	6052	-45	61	74.6	63.6	65.2	1.7	4.2	1.1
MILLGC17007	9608	21299	6053	-56	49	98.6	76.9	78.4	1.5	13.7	1.0
MILLGC17008	9608	21299	6053	-66	47	104.8	<b>92.0</b>	<b>93.9</b>	<b>1.9</b>	<b>73.2</b>	<b>1.6</b>
MILLGC17009	9608	21299	6053	-59	71	94.2	75.4	76.2	0.9	19.8	0.6
MILLGC17010	9608	21298	6053	-69	77	110.7	92.9	95.4	2.5	1.3	1.7
MILLGC17011	9608	21298	6053	-44	90	83.8	65.5	66.0	0.5	4.6	0.4
MILLGC17012	9608	21286	6053	-35	118	113.5	<b>91.4</b>	<b>92.7</b>	<b>1.3</b>	<b>20.4</b>	<b>1.1</b>
						and	<b>93.1</b>	<b>93.6</b>	<b>0.5</b>	<b>119.0</b>	<b>0.4</b>
MILLGC17013	9608	21286	6053	-40	102	95.2	74.3	75.8	1.6	11.5	1.3
MILLGC17014	9608	21286	6052	-50	111	106.3	90.3	93.4	3.1	2.8	2.1
MILLGC17015	9608	21287	6053	-57	91	98.5	82.0	84.7	2.7	6.9	2.0
MILLGC17016	9608	21286	6052	-57	117	120.1	<b>105.6</b>	<b>109.4</b>	<b>3.8</b>	<b>29.4</b>	<b>2.2</b>
MILLGC17017	9633	21183	6033	-59	20	146.7	<b>124.6</b>	<b>126.3</b>	<b>1.7</b>	<b>39.7</b>	<b>1.4</b>
MILLGC17018	9633	21183	6032	-66	30	140.8	<b>114.9</b>	<b>116.3</b>	<b>1.4</b>	<b>80.4</b>	<b>1.4</b>
MILLGC17019	9633	21183	6032	-61	36	125.8	<b>101.4</b>	<b>102.7</b>	<b>1.3</b>	<b>56.6</b>	<b>0.9</b>
MILLGC17020	9633	21183	6032	-50	40	107.8	<b>88.0</b>	<b>89.0</b>	<b>1.0</b>	<b>31.1</b>	<b>0.7</b>
MILLGC17021	9639	21175	6032	-65	49	111.0	93.7	96.6	2.9	3.7	2.0
MILLGC17022A	9639	21175	6032	-75	69	125.9	112.2	113.1	1.0	4.6	0.7
MILLGC17023	9641	21172	6032	-60	80	93.0	78.7	79.3	0.5	16.9	0.4
MILLGC17024	9641	21172	6032	-55	110	98.8	81.8	84.0	2.3	1.9	1.6
MILLGC17025A	9641	21171	6033	-63	120	121.6	101.7	102.8	1.1	2.9	0.8
						and	103.1	104.3	1.2	3.0	0.8
MILLGC17027	9641	21170	6032	-64	132	146.2	135.9	136.9	1.0	6.5	0.7
MILLGC17029	9642	21172	6032	-74	103	128.9	102.1	102.4	0.3	7.5	0.2
MILLGC17031	9608	21299	6055	19	36	116.1	93.3	95.0	1.8	11.0	1.2
MILLGC17032	9608	21298	6055	26	54	90.0	77.3	78.0	0.7	21.0	0.5
MILLGC17033	9656	21279	6099	10	29	56.9	41.9	42.6	0.7	3.2	0.5
MILLGC17034	9656	21278	6099	23	55	48.0	32.5	38.0	5.5	9.0	4.1
MILLGC17035	9657	21275	6099	22	94	50.9	38.2	39.0	0.8	6.1	0.6
MILLGC17036	9657	21274	6098	10	119	53.8	44.9	46.2	1.3	13.6	0.9
MILLGC17037	9655	21273	6095	10	138	86.9	78.5	80.6	2.1	2.4	1.6
MILLGC17038	9610	21326	6098	6	60	78.0	65.0	68.2	3.1	5.8	2.1
MILLGC17039	9654	21273	6095	0	129	61.7	52.9	53.8	0.9	14.9	0.9
MILLGC17040	9610	21326	6095	0	34	102.0	91.2	92.0	0.8	12.6	0.8
MILLGC17041	9657	21275	6100	27	119	72.0	57.5	60.5	3.0	7.2	2.1
MILLGC17042	9657	21278	6100	42	69	65.7	51.2	52.7	1.6	5.5	1.1
MILLGC17043	9608	21316	6096	22	78	87.0	77.4	78.0	0.5	3.5	0.4
MILLGC17044	9610	21326	6095	9	46	101.6	76.2	76.5	0.4	13.0	0.3
MILLGC17045	9597	21354	6091	5	31	125.0	<b>107.8</b>	<b>110.9</b>	<b>3.1</b>	<b>9.8</b>	<b>3.1</b>
MILLGC17046	9597	21354	6091	4	20	149.0	131.9	137.0	5.1	3.2	3.6
MILLGC17047	9597	21354	6090	-7	11	185.0	150.0	154.4	4.4	2.7	1.9
						and	158.3	160.3	2.0	3.5	1.4
MILLGC17048	9597	21354	6090	-23	4	221.1	168.0	183.0	15.0	4.0	2.8
MILLGC17049	9597	21354	6090	-32	18	144.2	121.6	124.6	3.0	4.8	2.1
MILLGC17050	9600	21323	6014	4	27	109.4	86.3	87.9	1.6	1.9	1.6
MILLGC17051	9600	21323	6014	-12	19	119.7	101.1	104.9	3.8	4.7	2.7
MILLGC17052A	9600	21323	6013	-24	19	116.5	96.3	101.9	5.6	1.4	3.9
MILLGC17053	9600	21323	6013	-27	11	140.8	<b>124.2</b>	<b>129.7</b>	<b>5.4</b>	<b>5.0</b>	<b>4.0</b>
MILLGC17054	9600	21322	6013	-38	17	121.8	105.5	106.9	1.4	6.2	1.0
MILLGC17055	9600	21322	6012	-44	29	110.7	84.4	85.9	1.5	4.0	1.1
MILLGC17056	9600	21322	6012	-49	21	126.3	108.0	109.0	1.1	12.8	0.8
MILLRVD001	9627	21085	6124	-24	73	150.0	131.6	132.1	0.5	2.1	0.4
MILLRVD002	9627	21085	6124	-28	87	130.3	116.9	117.3	0.4	11.8	0.3
MILLRVD003	9627	21085	6124	-14	62	134.4	114.2	115.6	1.5	2.0	1.3
						and	111.4	112.1	0.7	2.2	0.6
MILLRVD005	9627	21085	6124	-27	40	133.2	111.3	112.0	0.7	6.5	0.6
MILLRVD006	9627	21086	6124	-26	53	132.0	119.3	120.2	0.9	4.8	0.7



## KUNDANA SIGNIFICANT INTERSECTIONS - MILLENNIUM

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
MILLRVD007	9627	21085	6125	-17	50	134.6	115.0	115.7	0.7	14.1	0.6
MILLRVD008	9627	21086	6124	-32	44	155.7	131.4	132.2	0.8	10.1	0.7
MILLRVD009	9614	21184	6112	-14	73	140.0	94.5	96.5	2.1	5.5	1.7
MILLRVD010	9614	21183	6110	-47	60	134.6	114.5	115.4	1.0	17.7	0.8
MILLRVD011	9614	21184	6110	-41	41	143.8	<b>124.7</b>	<b>127.6</b>	<b>2.9</b>	<b>11.3</b>	<b>2.3</b>
MILLRVD012	9614	21183	6110	-54	58	149.9	130.4	132.0	1.6	8.7	1.3
MILLRVD013	9614	21183	6110	-58	58	164.7	<b>142.2</b>	<b>143.9</b>	<b>1.7</b>	<b>15.5</b>	<b>1.4</b>
MILLRVD014	9614	21183	6110	-67	74	191.9	159.8	161.0	1.3	3.1	0.9
MILLRVD015	9614	21183	6110	-61	78	156.0	141.9	144.0	2.1	1.5	1.7
MILLRVD016	9614	21183	6110	-54	91	146.9			NSI		
MILLRVD017	9614	21183	6110	-49	103	152.9	127.0	127.8	0.8	2.9	0.6
MILLRVD018	9614	21183	6110	-45	83	128.7	110.1	110.7	0.6	2.5	0.4
MILLRVD019	9614	21183	6110	-36	87	119.5	99.7	100.3	0.5	5.6	0.4
MILLRVD020	9627	21085	6124	-35	28	147.0	121.7	122.6	0.8	0.8	0.7
MILLRVD021	9627	21085	6124	-37	42	141.0			NSI		

## KUNDANA SIGNIFICANT INTERSECTIONS - REGIONAL

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
BKDD17049A	330994	6600197	343	-67	17	1144.1	114.9	115.8	0.9	2.7	0.6
						and	1015.6	1016.0	0.4	2.8	0.3
						and	1072.6	1073.0	0.4	1.0	0.3

Table 4 - Kanowna Significant Intersections

## KANOWNA SIGNIFICANT INTERSECTIONS - A BLOCK

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU3023	20337	49904	10145	53	258	132	26.6	27.1	0.5	16.2	0.3
KDU4011	19963	49903	9993	37	14	51	0.0	2.0	2.0	2.7	0.7
						and	9.0	15.0	6.0	2.1	2.2
						and	29.5	33.0	3.5	3.1	1.3
KDU4053	19985	49898	9992	36	336	56	33.0	42.0	9.0	3.9	3.1
KDU4054	19985	49898	9991	28	357	51	19.0	24.0	5.0	2.6	2.7
						and	<b>41.7</b>	<b>50.5</b>	<b>8.8</b>	<b>4.4</b>	<b>4.7</b>
KDU4179	20168	50013	10068	37	171	62	19.4	21.9	2.6	3.7	2.4
KDU4181	20194	50013	10066	33	194	32	<b>20.7</b>	<b>25.8</b>	<b>5.1</b>	<b>9.5</b>	<b>5.1</b>
KDU4182	20194	50013	10064	4	162	49	26.0	33.0	7.0	3.4	5.6
						and	44.0	48.9	4.9	3.3	2.3
KDU4209	19902	49928	9991	12	211	53	25.7	26.3	0.6	2.0	0.5
KDU4210	19902	49928	9991	-6	210	198			NSI		
KDU4212	19909	49924	9991	-4	195	59			NSI		
KDU4216	19941	49919	10015	5	194	64	<b>8.6</b>	<b>13.0</b>	<b>4.5</b>	<b>10.0</b>	<b>3.9</b>
						and	16.7	19.0	2.3	8.5	2.0
						and	24.0	25.9	1.9	11.5	1.7
KDU4217A	19915	49925	10019	0	198	35	8.9	13.6	4.7	7.2	3.8
						and	25.0	26.7	1.7	3.7	1.4
KDU4218A	19915	49926	10021	31	200	75	8.8	14.0	5.2	2.7	5.0
KDU4220	19888	49938	10023	-6	207	62			NSI		
KDU4221	19878	49942	10026	21	204	74			NSI		
KDU4301	19879	49947	10026	14	333	36	<b>4.0</b>	<b>15.0</b>	<b>11.0</b>	<b>15.2</b>	<b>4.8</b>
KDU4302	19879	49947	10024	-44	330	27	21.0	23.4	2.4	5.1	1.0
KDU4103	20164	50038	10113	-19	175	53	27.0	32.3	5.3	4.0	3.3

## KANOWNA SIGNIFICANT INTERSECTIONS - B BLOCK

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU4188	19853	49994	9962	-3	192	74	48.8	53.8	5.0	1.3	4.1
KDU4189	19840	50001	9962	-1	194	69	46.0	49.0	3.0	1.5	2.6
						and	54.0	57.0	3.0	4.6	2.6
KDU4160	20146	49857	9906	0	154	270	50.0	51.7	1.7	4.1	0.8
						and	79.0	86.2	7.2	2.2	3.6
						and	109.0	110.6	1.6	6.1	0.8
						and	<b>138.7</b>	<b>143.1</b>	<b>4.4</b>	<b>12.5</b>	<b>3.0</b>
KDU4166	20145	49857	9906	-4	178	54	26.2	28.7	2.6	3.1	1.9
KDU4167	20144	49857	9905	-24	204	71	40.0	45.1	5.1	2.9	2.5
KDU4169	20143	49857	9906	-11	222	57	10.0	16.0	6.0	3.4	5.6
						and	21.3	24.8	3.5	3.4	3.0
KDU4170	20145	49856	9909	41	186	47	19.3	22.0	2.7	7.0	2.3
KDU4171	20144	49857	9907	14	220	48	<b>22.0</b>	<b>31.8</b>	<b>13.0</b>	<b>6.1</b>	<b>11.2</b>
KDU4172	20144	49857	9908	36	227	47	16.5	24.0	7.5	1.4	6.8
KDU4184	19879	49975	9963	21	161	75	31.4	32.7	1.3	11.1	1.2
KDU4185	19877	49975	9963	14	198	128	28.9	31.0	2.1	3.3	2.0
KDU4186	19875	49976	9963	24	222	51	33.3	34.4	1.2	1.1	1.0
KDU4190	19840	50001	9963	17	194	70	45.6	49.3	3.7	1.2	3.6
KDU4192	19820	50007	9964	19	189	67	45.2	45.8	0.6		
KDU4194	19820	50008	9962	-20	185	90	58.8	62.1	3.3	0.9	2.1
						and	<b>68.7</b>	<b>75.0</b>	<b>6.3</b>	<b>6.0</b>	<b>4.0</b>
KDU3197	20230	49935	9924	5	195	406	<b>109.0</b>	<b>111.9</b>	<b>2.9</b>	<b>10.5</b>	<b>2.8</b>
KDU3197	20230	49935	9924	5	195	and	122.0	123.1	1.1	6.1	1.0
KDU3198	20230	49935	9924	10	193	399	<b>81.0</b>	<b>86.0</b>	<b>5.0</b>	<b>7.6</b>	<b>4.9</b>
						and	<b>94.0</b>	<b>99.0</b>	<b>5.0</b>	<b>5.3</b>	<b>4.9</b>
KDU3199	20230	49934	9924	4	189	439	92.5	95.0	2.5	2.5	2.2
						and	102.0	104.0	2.0	10.1	1.8



## KANOWNA SIGNIFICANT INTERSECTIONS - B BLOCK

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
						and	105.0	111.0	6.0	2.3	5.4
						and	119.8	122.8	3.1	4.0	2.7
KDU3200	20230	49935	9924	10	185	465	91.0	93.4	2.4	6.9	2.1
						and	97.8	102.0	4.2	3.4	3.7
						and	119.0	127.0	8.0	2.2	7.0
KDU3244	20231	49935	9925	16	194	429	116.7	117.5	0.8	4.7	0.7
						and	277.0	279.0	2.0	10.8	1.5
KDU3246	20232	49935	9925	10	190	449	93.0	94.0	1.0	11.6	1.0
						and	<b>114.0</b>	<b>119.0</b>	<b>5.0</b>	<b>6.0</b>	<b>4.8</b>
KDU4187A	19853	49994	9964	32	188	61			NSI		
KDU4193	19820	50008	9962	-33	183	121	78.6	79.1	0.5		
KDU4196	19820	50008	9962	-28	193	97	72.9	76.0	3.1	1.8	1.6
KDU4163	20149	49856	9907	19	151	61	41.0	42.0	1.0	30.6	0.3
						and	41.0	46.9	5.9	6.6	1.8
KDU4164	20149	49857	9908	36	147	58	24.0	36.0	12.0	2.2	3.1
KDU4165	20149	49857	9910	55	157	55	15.0	17.7	2.7	3.3	0.8
KDU4168	20144	49857	9906	-4	204	51	17.0	25.7	8.7	2.0	7.9
						and	33.8	35.0	1.3	3.7	0.0

## KANOWNA SIGNIFICANT INTERSECTIONS - C BLOCK

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU3917	20323	49889	9859	-8	200	119	<b>63.5</b>	<b>74.0</b>	<b>10.5</b>	<b>7.3</b>	<b>8.7</b>
						and	<b>85.0</b>	<b>90.0</b>	<b>5.0</b>	<b>6.3</b>	<b>4.3</b>
						and	93.0	96.0	3.0	3.4	2.6
KDU3918	20323	49889	9859	-6	196	185	70.0	76.0	6.0	2.8	5.2
						and	80.0	87.0	7.0	2.6	5.9
						and	106.8	108.7	2.0	5.3	1.0
						and	<b>117.4</b>	<b>127.0</b>	<b>9.6</b>	<b>3.9</b>	<b>8.1</b>
						and	132.0	139.0	7.0	3.1	5.2
						and	142.0	147.0	5.0	2.8	3.7
KDU3928	20323	49889	9859	-14	173	110	<b>65.0</b>	<b>75.9</b>	<b>10.9</b>	<b>4.3</b>	<b>7.5</b>
						and	78.0	82.8	4.8	3.1	4.0
						and	<b>83.7</b>	<b>93.3</b>	<b>9.7</b>	<b>4.1</b>	<b>5.2</b>
KDU4045	19912	49836	9741	-23	184	35	26.6	27.4	0.9	2.5	0.5
KDU4074	20039	49859	9801	13	188	183	50.7	56.7	6.1	3.4	5.7
						and	85.0	89.0	4.0	3.4	3.4
						and	111.9	118.0	6.2	2.3	4.9
KDU4093	19801	49816	9655	24	236	99	22.1	23.2	1.1	2.0	0.8
KDU4094	19801	49816	9655	38	210	87	61.8	62.1	0.3	21.1	0.2
KDU4095	19880	49786	9653	20	195	141	35.6	48.0	12.4	1.4	12.1
						and	101.4	103.0	1.6	16.5	0.8
KDU4096	19907	49780	9652	11	196	122	62.9	65.7	2.9	6.0	2.7
						and	<b>81.0</b>	<b>97.0</b>	<b>16.0</b>	<b>6.4</b>	<b>13.0</b>
						Including	<b>89.1</b>	<b>92.5</b>	<b>3.4</b>	<b>21.7</b>	<b>2.4</b>
KDU4097	19931	49777	9651	5	0	84	<b>16.7</b>	<b>25.4</b>	<b>8.7</b>	<b>11.2</b>	<b>7.7</b>
						and	63.0	69.0	6.0	2.7	5.3
						and	<b>71.3</b>	<b>75.0</b>	<b>3.8</b>	<b>7.4</b>	<b>3.3</b>
KDU4104	19814	49844	9715	-15	177	171	21.8	30.0	8.2	2.8	5.6
						and	87.0	89.8	2.8	3.3	1.9
KDU4105	19834	49836	9716	23	213	90	16.2	20.0	3.8	2.8	3.5
						and	23.0	29.0	6.0	2.4	5.6
						and	<b>59.2</b>	<b>61.5</b>	<b>2.3</b>	<b>2.3</b>	<b>2.2</b>
KDU4106	19830	49837	9717	19	192	101	15.3	21.0	5.7	3.6	5.6
						and	32.0	33.9	1.9	4.5	1.9
						and	58.1	62.5	4.4	1.7	4.3
KDU4107	19861	49826	9715	11	214	93	<b>21.5</b>	<b>29.0</b>	<b>7.5</b>	<b>3.2</b>	<b>6.6</b>
						and	35.4	41.0	5.6	2.7	4.8
						and	59.1	61.9	2.8	2.7	2.4
KDU4108	19861	49826	9716	10	196	91	21.0	25.0	4.0	2.9	3.7
						and	35.0	39.6	4.6	2.9	4.2
KDU4109	19860	49827	9716	19	202	88	20.6	22.5	1.9	3.3	1.8
						and	30.0	35.7	5.7	3.0	4.4
KDU4110	19873	49822	9715	17	189	90	<b>30.0</b>	<b>41.0</b>	<b>11.0</b>	<b>2.5</b>	<b>10.6</b>
						and	62.0	63.4	1.4	7.9	1.3
KDU4111	19883	49820	9715	14	192	100	39.0	46.6	7.6	2.4	7.4
						and	67.0	70.0	3.0	2.0	1.5
KDU4114	19843	49862	9777	30	233	42	20.8	24.0	3.2	2.8	2.6
KDU4115	19842	49861	9774	-11	217	56	23.8	28.1	4.3	5.2	2.9
KDU4116	19843	49862	9777	45	200	132	19.2	24.0	4.8	1.5	4.6
						and	36.7	44.0	7.3	1.7	7.1
KDU4117	19888	49779	9786	-26	7	22	7.0	10.0	3.0	4.0	3.0
KDU4118	19871	49788	9783	-29	35	20	17.0	19.6	2.6	2.1	2.4
KDU4129	20187	49609	9306	17	168	72	<b>51.8</b>	<b>61.8</b>	<b>10.0</b>	<b>3.4</b>	<b>7.7</b>
						and	69.4	71.8	2.4	3.8	2.0
KDU4133	19954	49797	9682	-8	164	106	<b>65.5</b>	<b>82.4</b>	<b>16.9</b>	<b>3.5</b>	<b>12.2</b>
						and	92.4	95.1	2.7	5.1	1.9
						and	<b>101.7</b>	<b>105.0</b>	<b>3.4</b>	<b>13.3</b>	<b>2.7</b>
KDU4134	19954	49797	9682	-7	175	89	<b>61.0</b>	<b>73.0</b>	<b>12.0</b>	<b>4.8</b>	<b>9.3</b>
KDU4135	19954	49796	9682	-9	184	88	<b>61.0</b>	<b>75.0</b>	<b>14.0</b>	<b>3.4</b>	<b>10.6</b>
KDU4136	19954	49797	9683	29	195	62	<b>48.0</b>	<b>57.0</b>	<b>9.0</b>	<b>3.2</b>	<b>9.0</b>
KDU4137	19954	49797	9684	32	179	81	<b>45.0</b>	<b>55.0</b>	<b>10.0</b>	<b>2.6</b>	<b>9.9</b>
KDU4138	19954	49797	9684	31	170	270	<b>45.0</b>	<b>55.0</b>	<b>10.0</b>	<b>2.1</b>	<b>9.4</b>
						and	62.0	69.4	7.4	2.2	7.0
						and	84.4	88.0	3.6	2.6	1.7
						and	109.0	117.0	8.0	2.7	4.6
						and	134.5	137.9	3.4	2.7	1.9
						and	175.0	179.0	4.0	3.2	2.2
						and	<b>246.0</b>	<b>247.5</b>	<b>1.5</b>	<b>24.9</b>	<b>0.9</b>
KDU4143	20168	49799	9737	10	188	80	51.0	59.2	8.2	2.2	7.7
						and	50.0	55.7	5.7	2.3	5.2
KDU4145	20168	49799	9737	2	177	80	52.3	57.2	4.9	3.7	4.2



## KANOWNA SIGNIFICANT INTERSECTIONS - C BLOCK

Drill Hole #	Eastings (Mine Grid)	Northing (Mine Grid)	Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU4146	20197	49796	9737	4	174	78	42.1	57.3	15.2	3.5	13.2
KDU4148	20216	49794	9738	39	177	260	20.5	27.0	6.5	9.6	6.3
						and	38.9	41.0	2.1	4.8	2.0
						and	47.3	50.0	2.7	3.5	2.6
						and	63.6	66.0	2.5	4.0	2.4
						and	70.0	71.1	1.1	8.2	0.6
						and	137.0	139.0	2.0	6.3	1.0
						and	235.0	237.4	2.4	28.5	1.2
KDU4252	20265	49795	9770	17	172	93	36.9	39.0	2.1	2.0	1.9
						and	46.0	47.5	1.5	35.0	1.3
KDU4253	20227	49802	9770	16	142	80	12.2	17.0	4.8	5.3	3.4
						and	31.0	32.5	1.5	2.8	0.8
						and	37.3	38.0	0.7	19.3	0.4
						and	41.0	47.0	6.0	5.1	3.4
						and	64.0	64.5	0.5	246.0	Unknown
KDU4283	19879	49787	9652	9	201	126	55.0	61.5	6.5	2.7	6.0
						and	63.0	65.3	2.3	4.0	2.1
						and	96.0	108.0	12.0	2.6	Unknown
KDU4292	19818	49833	9617	20	215	94	80.6	83.0	2.4	2.7	1.2
KDU4098	19931	49777	9651	-6	199	237	18.1	27.7	9.6	9.9	7.7
						and	54.0	68.0	14.0	1.9	11.2
						and	65.2	67.3	2.1	4.9	1.6
						and	76.0	78.2	2.2	3.7	1.7
						and	87.0	93.0	6.0	11.8	4.0
						and	103.0	112.0	9.0	5.1	5.0
KDU4174	20267	49794	9769	-10	184	122	103.9	104.8	0.9	86.1	Unknown
KDU4176	20227	49802	9771	29	194	297	8.9	16.6	7.8	2.3	7.7
						and	38.4	43.0	4.6	3.2	4.6
						and	71.0	80.0	9.0	3.3	7.6
KDU4069	19867	49879	9804	23	203	80	28.2	30.0	1.8	3.8	1.8
						and	32.0	37.2	5.2	2.3	5.0
						and	73.6	74.3	0.7	8.6	0.7
KDU4070	19867	49880	9802	-5	201	75	33.0	44.0	11.0	3.0	8.9
						and	47.0	52.1	5.1	2.4	4.1
KDU4071	19942	49860	9802	-5	180	150	48.7	56.0	7.3	3.8	5.8
						and	70.0	72.4	2.4	4.7	1.9
						and	112.5	115.0	2.5	11.0	1.3
KDU4279	19906	49780	9652	9	179	183	60.4	69.0	8.6	3.5	8.2
						and	71.0	72.0	1.1	4.1	1.0
						and	85.5	86.5	1.0	4.2	1.0
						and	90.1	93.0	2.9	8.8	2.9
KDU4279	19906	49780	9652	9	179	183	146.0	147.0	1.0	6.0	0.5
KDU4232	20203	49798	9801	31	25	52	22.2	25.4	3.2	3.1	1.5
KDU4234	20203	49798	9799	-23	54	33	12.0	17.0	5.0	7.7	3.9
KDU4235	20203	49798	9801	18	63	52	35.4	46.4	11.0	3.2	3.7
KDU4233	20203	49798	9801	13	54	38	19.2	19.9	0.8	4.8	0.4
						and	25.0	26.0	1.0	5.5	0.5
KDU4236	20195	49828	9799	-29	171	66	30.0	32.8	2.8	11.3	1.3
KDU4254	20245	49798	9769	-14	205	58	48.9	53.3	4.4	2.7	3.4
						and	56.9	58.0	1.1	3.4	0.9

## KANOWNA SIGNIFICANT INTERSECTIONS - D BLOCK

Drill Hole #	Eastings (Mine Grid)	Northing (Mine Grid)	Drill Hole Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	End of Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU4021	20170	49736	9548	-23	171	160	118.0	128.8	10.8	1.9	6.0
KDU4022	20170	49736	9548	-17	168	154	111.0	120.4	9.4	3.0	5.8
KDU4199	20488	49688	9540	-2	194	140	25.6	29.0	3.4	2.3	2.9
KDU4200	20490	49688	9539	-3	186	147	79.0	83.0	4.0	2.3	3.6
KDU4215	20490	49688	9540	-14	161	187	42.0	45.2	3.2	2.4	1.9
KDU4199	20488	49688	9540	-2	194	140	32.0	33.2	1.2	4.4	1.0
KDU4215	20490	49688	9540	-14	161	187	93.0	98.0	5.0	1.9	2.9
KDU4199	20488	49688	9540	-2	194	140	99.9	101.4	1.6	5.1	1.5
						and	106.6	108.0	1.5	1.9	1.4
KDU4015	20168	49736	9549	-4	212	160	93.2	97.0	3.9	9.9	2.9
KDU4017	20168	49736	9548	-19	191	180	109.0	115.9	6.9	3.2	4.5
KDU4018	20169	49736	9548	-14	186	121	100.0	109.3	9.3	3.6	6.6
KDU4019	20169	49736	9549	-5	180	108	89.0	91.7	2.7	3.6	2.1
KDU4020A	20169	49736	9548	-18	178	130	113.0	118.0	5.0	2.9	3.2
KDU4023	20170	49736	9548	-15	158	140	66.6	68.7	2.1	3.6	0.8
						and	91.5	94.0	2.6	2.1	1.2
						and	119.2	130.3	11.1	3.4	6.3
KDU3467	20193	49490	9210	37	75	63	32.0	35.0	3.0	3.7	0.8
KDU4063	20149	49660	9315	19	193	115	91.0	107.6	16.6	3.9	16.1
KDU4198	20488	49688	9540	-2	204	50	38.5	45.1	6.6	1.3	3.3
KDU4062	20149	49660	9315	16	171	123	98.0	107.0	9.0	3.1	7.8
						and	110.8	120.8	10.0	6.4	8.1
						Including	118.0	120.0	2.0	20.5	1.4
KDU4089	20149	49660	9315	16	210	117	79.3	82.0	2.7	2.5	2.6
KDU4112	20024	49736	9332	23	165	129	27.0	28.0	1.0	13.3	0.5
KDU4113	20024	49736	9332	21	185	107	90.0	91.0	1.0	4.7	0.5
KDU4120	20039	49727	9331	19	213	169	92.4	98.0	5.6	3.7	5.6
KDU4127	20187	49609	9303	-20	174	79	16.5	31.0	14.5	5.0	7.0
						and	41.5	45.6	4.1	3.3	2.0
						and	66.0	69.4	3.4	2.3	1.6
KDU4128	20187	49609	9304	-8	171	79	20.6	23.0	2.4	2.4	1.4
						and	61.0	63.0	2.0	3.7	1.2
KDU4130	20188	49609	9307	34	154	76	10.8	14.0	3.2	2.7	1.8
						and	54.1	65.0	10.9	2.6	7.5
KDU3271	20186	49609	9305	23	130	167	25.5	28.0	2.6	4.7	1.3



## KANOWNA SIGNIFICANT INTERSECTIONS - LOWES EXTENSION

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Drill Hole Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	End of Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU3605	20396	49123	9215	-86	145	579	<b>317.0</b>	<b>325.0</b>	<b>8.0</b>	<b>8.9</b>	7.9
KDU3605	20396	49123	9215	-86	145	579	494.9	505.3	10.4	3.6	4.8
KDU3604	20396	49126	9215	-87	37	501	<b>270.9</b>	<b>281.6</b>	<b>10.7</b>	<b>15.8</b>	Unknown
						Including	280.9	276.4	4.4	12.9	Unknown
						Including	278.0	281.6	3.6	29.2	Unknown
						and	301.0	305.6	4.7	3.0	Unknown
KDU4205	20328	49017	9197	-47	63	665	522.0	524.0	2.0	2.0	1.4
KDU4206	20328	49017	9197	-60	61	594	61.3	63.0	1.7	3.7	0.8
						and	201.0	205.0	3.0	2.4	1.5
						and	390.6	398.0	7.5	1.7	3.6
KDU4207	20327	49017	9197	-72	75	616	89.0	96.0	7.0	1.8	3.5
						and	<b>355.9</b>	<b>364.4</b>	<b>8.5</b>	<b>4.0</b>	Unknown
						and	564.0	565.2	1.2	1.5	0.7
KDU4249	20327	49018	9197	-65	44	498	<b>351.0</b>	<b>360.4</b>	<b>9.4</b>	<b>8.0</b>	<b>5.0</b>
						and	450.0	453.2	3.2	1.4	2.3
						and	450.0	453.2	3.2	1.4	2.3

## KANOWNA SIGNIFICANT INTERSECTIONS - E BLOCK

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Drill Hole Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	End of Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU3847	20397	49127	9216	-44	15	320	278.0	283.5	5.5	3.6	4.8
KDU3848	20397	49127	9216	-35	7	315	<b>264.1</b>	<b>271.0</b>	<b>7.0</b>	<b>4.7</b>	<b>6.6</b>
KDU3849	20398	49127	9216	-50	4	325	90.0	93.0	3.0	5.4	2.8
						and	278.0	288.0	10.0	1.6	9.2
KDU3850	20397	49127	9216	-48	350	303	279.0	281.0	2.0	11.3	1.8
KDU3851	20397	49127	9216	-41	353	321			NSI		
KDU3992	20424	49300	9240	-62	347	198	<b>143.0</b>	<b>153.0</b>	<b>10.0</b>	<b>4.5</b>	<b>8.4</b>
KDU3993	20424	49300	9240	-55	332	193	<b>147.0</b>	<b>165.1</b>	<b>18.1</b>	<b>5.4</b>	<b>15.7</b>
KDU3995	20424	49300	9240	-35	323	179	<b>153.0</b>	<b>164.6</b>	<b>11.6</b>	<b>2.6</b>	<b>10.1</b>
KDU3996	20424	49300	9242	-30	351	153	<b>132.0</b>	<b>138.0</b>	<b>6.0</b>	<b>9.9</b>	<b>6.0</b>
KDU3997	20424	49300	9242	-34	1	186	80.0	84.5	4.5	2.9	4.5
						and	136.0	137.3	1.3	2.9	1.2
KDU3998	20424	49300	9242	-21	343	178	134.1	136.1	2.0	2.4	2.0
						and	145.0	147.0	2.0	3.5	2.0
KDU3999	20424	49300	9242	-15	7	186	<b>124.9</b>	<b>133.0</b>	<b>8.1</b>	<b>3.9</b>	<b>7.6</b>
KDU4000	20424	49300	9242	-8	342	195	146.0	150.0	4.0	1.5	3.6
KDU4042	20425	49300	9241	-12	344	185	<b>139.4</b>	<b>150.0</b>	<b>10.7</b>	<b>4.6</b>	<b>10.0</b>
KDU4043	20425	49300	9240	-15	352	185	<b>136.1</b>	<b>146.0</b>	<b>9.9</b>	<b>5.9</b>	<b>9.6</b>
						and	<b>149.0</b>	<b>160.0</b>	<b>11.0</b>	<b>3.9</b>	<b>6.0</b>
KDU4044	20425	49300	9241	-11	358	183	<b>137.8</b>	<b>155.0</b>	<b>17.2</b>	<b>7.3</b>	<b>16.2</b>
						Including	<b>152.0</b>	<b>155.0</b>	<b>3.0</b>	<b>13.7</b>	<b>2.8</b>
KDU4005	19984	49547	9061	-27	183	410	<b>43.0</b>	<b>46.0</b>	<b>3.0</b>	<b>23.5</b>	<b>1.7</b>
KDU4006	19983	49547	9061	-36	198	244	<b>49.4</b>	<b>53.0</b>	<b>3.6</b>	<b>14.4</b>	<b>1.7</b>
KDU4007	19983	49548	9061	-31	203	162	<b>148.0</b>	<b>155.9</b>	<b>7.9</b>	<b>6.4</b>	<b>3.3</b>
KDU4010	19982	49548	9061	-32	221	400	50.6	51.4	0.8	20.3	0.4
						and	105.1	106.0	0.9	7.6	0.5
						and	134.0	140.0	6.0	2.5	3.2
						and	149.7	151.1	1.4	6.5	0.6
KDU4013	19984	49547	9061	-28	190	423	38.9	40.0	1.1	24.3	0.7
						and	43.3	46.3	3.0	34.7	1.8
KDU4005	19984	49547	9061	-27	183	410	132.0	143.0	11.0	2.2	6.1
KDU4008	19983	49548	9061	-31	209	480	29.0	33.0	4.0	5.7	2.2
						and	42.0	47.0	5.0	4.5	2.8
						and	120.0	123.0	3.0	3.3	1.7
						and	133.0	137.0	4.0	2.6	2.2
KDU4055	20028	49612	9095	-22	176	507	238.4	243.0	4.6	3.4	2.5
						and	249.0	250.6	1.6	7.4	0.9
KDU3989	20476	49287	9244	22	49	455	<b>114.3</b>	<b>116.0</b>	<b>1.7</b>	<b>27.9</b>	Unknown
						and	139.0	140.4	1.4	6.4	Unknown
KDU3990	20476	49287	9244	1	49	426	97.0	99.0	2.0	4.8	Unknown
						and	218.5	221.7	3.3	2.0	Unknown
						and	249.0	252.1	3.1	2.8	Unknown
KDU3991	20476	49287	9244	17	58	414	116.0	117.1	1.1	6.7	Unknown
KDU4052	20476	49287	9244	2	61	400	<b>218.9</b>	<b>226.0</b>	<b>7.1</b>	<b>3.1</b>	Unknown
						and	<b>229.0</b>	<b>238.0</b>	<b>9.0</b>	<b>3.4</b>	Unknown
						and	<b>267.0</b>	<b>276.0</b>	<b>9.0</b>	<b>3.2</b>	Unknown
						and	284.0	289.0	5.0	3.0	Unknown
KDU3281	20140	49667	9818	4	83	270	<b>12.8</b>	<b>25.6</b>	<b>12.8</b>	<b>40.3</b>	Unknown

## KANOWNA SIGNIFICANT INTERSECTIONS - VELVET

Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Drill Hole Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	End of Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU4032	19168	50288	9506	10	260	252	<b>175.6</b>	<b>182.0</b>	<b>6.4</b>	<b>5.4</b>	<b>5.5</b>
KDU4033	19169	50287	9505	4	237	210	119.0	126.0	7.0	1.0	6.8
KDU4034	19170	50287	9506	18	232	209			NSI		
KDU4035	19170	50286	9505	4	222	198			NSI		
KDU4125	19169	50287	9506	15	261	258	147.0	151.0	4.0	3.6	3.7
						and	155.5	162.6	7.1	1.8	6.6
KDU4126	19169	50287	9506	18	268	237	181.0	186.4	5.4	2.3	4.2
KDU4156	19171	50285	9504	-26	214	224			NSI		
KDU4237	19104	50226	9497	-2	266	131	45.0	49.0	4.0	1.3	3.2
						and	98.0	102.0	4.0	6.5	3.1
KDU4238	19105	50226	9496	-23	265	149	56.0	59.1	3.1	1.7	2.1
						and	70.1	75.4	5.3	1.3	3.5
						and	81.0	83.8	2.8	1.5	1.7
						and	106.5	108.9	2.4	11.1	1.4
KDU4240	19104	50226	9497	6	247	101	42.1	46.2	4.1	1.1	3.8
KDU4242	19105	50224	9497	-1	222	113	38.6	40.7	2.1	1.6	1.1



KANOWNA SIGNIFICANT INTERSECTIONS - VELVET												
Drill Hole #	Easting (Mine Grid)	Northing (Mine Grid)	Drill Hole Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	End of Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)	
KDU4244	19105	50224	9497	-1	204	and	46.0	47.2	1.2	2.4	1.2	
						111	36.0	40.2	4.2	3.0	3.7	
						and	43.7	49.7	6.0	2.3	5.3	
KDU4270	19186	50226	9488	-16	213	and	53.4	57.5	4.1	4.4	3.6	
						178	126.5	128.1	1.7	1.8	1.5	
						and	178	119.0	122.2	3.2	1.0	2.9
KDU4276	19186	50226	9488	-17	225	178	119.0	122.2	3.2	1.0	2.9	
KDU4277	19186	50226	9488	-8	217	167	113.7	115.0	1.3	3.3	1.2	
KDU4154	19170	50285	9504	-22	245	253			NSI			
KDU3874	19267	50071	9588	20	212	51	11.9	13.3	1.4	8.8	1.3	
KDU3875	19326	50124	9569	26	229	190	86.7	89.4	2.7	11.9	1.1	
KDU3877	19327	50123	9570	26	176	and	108.0	117.0	9.0	5.1	3.8	
						330	289.0	294.7	5.7	2.0	3.9	
						and	158	72.7	81.2	8.5	4.1	4.1
KDU3878	19246	50160	9614	26	167	and	113.0	118.0	5.0	4.3	2.5	
KDU3879	19326	50123	9571	37	229	and	165	112.3	115.0	2.7	2.6	2.4
						and	239	<b>113.0</b>	<b>117.0</b>	<b>4.0</b>	<b>9.5</b>	<b>3.4</b>
						and	156	56.0	56.9	0.9	1.3	0.9
KDU3880	19326	50123	9571	35	208	239	<b>113.0</b>	<b>117.0</b>	<b>4.0</b>	<b>9.5</b>	<b>3.4</b>	
KDU3881	19246	50160	9614	17	207	and	73.2	76.0	2.8	4.1	2.6	
						and	98.0	103.0	5.0	2.1	2.5	
						and	111.0	112.3	1.3	8.2	1.2	
						and	130.7	133.3	2.6	1.8	1.3	
KDU3884	19247	50160	9615	18	159	207	84.3	86.0	1.7	2.2	0.6	
KDU3885	19246	50160	9614	7	172	159	72.0	73.8	1.8	1.6	1.0	
KDU3945	19263	50076	9588	22	232	and	96.6	100.0	3.4	1.8	1.9	
						40	<b>13.0</b>	<b>16.9</b>	<b>3.9</b>	<b>6.5</b>	<b>3.8</b>	
						and	45	<b>16.0</b>	<b>23.6</b>	<b>7.6</b>	<b>6.7</b>	<b>6.8</b>
KDU3946	19257	50082	9590	35	235	45	<b>33.0</b>	<b>38.1</b>	<b>5.1</b>	<b>7.5</b>	<b>4.6</b>	
KDU3946	19257	50082	9590	35	235	45	<b>33.0</b>	<b>38.1</b>	<b>5.1</b>	<b>7.5</b>	<b>4.6</b>	
KDU3947	19257	50082	9590	50	238	50	<b>17.0</b>	<b>24.6</b>	<b>7.6</b>	<b>6.4</b>	<b>5.8</b>	
KDU3948	19246	50092	9588	22	227	and	<b>31.8</b>	<b>36.0</b>	<b>4.3</b>	<b>6.9</b>	<b>3.3</b>	
						37	<b>17.0</b>	<b>28.0</b>	<b>11.0</b>	<b>3.4</b>	<b>10.8</b>	
						and	41	<b>17.4</b>	<b>28.9</b>	<b>11.5</b>	<b>2.6</b>	<b>11.3</b>
KDU3949	19241	50096	9588	21	230	41	<b>17.4</b>	<b>28.9</b>	<b>11.5</b>	<b>2.6</b>	<b>11.3</b>	
KDU3951	19237	50101	9590	38	225	45	<b>38.4</b>	<b>44.6</b>	<b>6.3</b>	<b>17.8</b>	<b>5.5</b>	
KDU3959	19328	50123	9569	18	181	162			NSI			
KDU3961	19328	50123	9568	-1	182	175	130.5	130.9	0.4	6.4	0.2	
KDU3962	19327	50123	9569	2	195	156	<b>84.7</b>	<b>86.1</b>	<b>1.4</b>	<b>20.4</b>	<b>1.2</b>	
KDU3963	19328	50123	9568	-8	191	and	<b>114.4</b>	<b>124.0</b>	<b>9.6</b>	<b>4.7</b>	<b>8.1</b>	
						160	117.3	119.6	2.3	3.5	1.7	
						and	156	92.2	93.0	0.8	1.9	0.7
KDU3964	19327	50123	9568	-5	197	156	92.2	93.0	0.8	1.9	0.7	
KDU4078	19326	50123	9571	34	220	210	90.0	90.8	0.8	1.9	0.7	
						and	102.7	104.0	1.3	1.7	1.2	
						and	177	<b>84.0</b>	<b>86.0</b>	<b>2.0</b>	<b>48.0</b>	<b>1.9</b>
						and	174	93.0	94.7	1.7	6.6	1.7
KDU4081	19326	50123	9570	28	216	177	<b>84.0</b>	<b>86.0</b>	<b>2.0</b>	<b>48.0</b>	<b>1.9</b>	
KDU4082	19325	50123	9569	11	225	174	93.0	94.7	1.7	6.6	1.7	
KDU4084	19326	50123	9569	3	207	165	112.9	114.0	1.2	9.9	1.1	
KDU4085	19326	50123	9569	11	205	174	81.1	82.4	1.3	9.7	1.2	
						and	106.0	108.0	2.0	5.3	1.9	
						and	163.0	167.0	4.0	3.3	2.0	
						and	165	112.0	116.0	4.0	5.2	3.1
KDU4086	19326	50123	9569	14	188	and	121.0	123.7	2.7	2.1	2.1	
KDU4087	19326	50123	9569	21	187	174	<b>114.2</b>	<b>118.0</b>	<b>3.8</b>	<b>26.1</b>	<b>2.9</b>	
KDU4087	19326	50123	9569	21	187	174	<b>114.2</b>	<b>118.0</b>	<b>3.8</b>	<b>26.1</b>	<b>2.9</b>	
KDU4251	19262	50163	9613	-14	165	Including	<b>116.0</b>	<b>118.0</b>	<b>2.0</b>	<b>44.3</b>	<b>1.5</b>	
						210	119.4	120.9	1.5	6.6	0.5	
						and	162.0	169.0	7.0	5.6	2.6	
						and	276	90.0	92.6	2.6	5.8	2.5
KDU4041A	19328	50123	9570	19	216	and	<b>112.0</b>	<b>115.8</b>	<b>3.8</b>	<b>7.4</b>	<b>3.7</b>	
KDU4223	19306	50004	9589	-22	207	and	121	0.0	3.0	2.5	2.2	
						and	<b>7.9</b>	<b>11.4</b>	<b>3.5</b>	<b>45.9</b>	<b>2.6</b>	
						and	117.0	121.1	4.1	2.5	3.0	
KDU4224	19288	50017	9590	21	230	and	123	19.7	21.0	1.3	2.7	1.2
						and	93.9	95.0	1.1	3.2	1.1	
						and	115	7.4	8.1	0.8	15.6	0.7
KDU4226	19288	50017	9589	0	229	and	51.0	54.0	3.0	3.8	3.0	
						and	58.0	63.0	5.0	2.5	4.9	
						and	133	59.0	62.8	3.8	3.2	3.5
KDU4227	19288	50017	9590	31	223	and	68.5	70.3	1.9	5.9	1.7	
						and	73.0	76.0	3.0	2.3	2.8	
						and	144	<b>65.0</b>	<b>72.6</b>	<b>7.6</b>	<b>4.7</b>	<b>6.1</b>
KDU4228	19288	50017	9588	-27	231	144	<b>65.0</b>	<b>72.6</b>	<b>7.6</b>	<b>4.7</b>	<b>6.1</b>	
KDU4229	19259	50039	9588	-18	221	120	41.6	44.0	2.5	2.1	2.1	
KDU4246	19288	50017	9589	-9	226	and	95.0	99.0	4.0	3.2	3.4	
						and	112	0.0	1.0	1.0	1.7	0.9
						and	<b>55.4</b>	<b>66.6</b>	<b>11.2</b>	<b>3.7</b>	<b>10.5</b>	
						and	84.0	86.0	2.0	4.3	1.9	
						and	210	176.7	187.0	10.4	3.2	3.9
						and	360	76.0	80.1	4.1	5.2	3.5
KDU3954	19326	50123	9570	25	222	and	301.1	304.0	2.9	6.6	2.8	
KDU3968	19172	50188	9587	25	223	60	21.0	27.7	6.7	1.9	6.4	
KDU3871	19168	50289	9505	-30	232	291	<b>183.0</b>	<b>190.0</b>	<b>7.0</b>	<b>7.1</b>	<b>6.5</b>	
KDU3873	19168	50289	9505	-27	242	282	<b>159.0</b>	<b>164.0</b>	<b>5.0</b>	<b>8.0</b>	<b>3.9</b>	
KDU3955A	19168	50289	9505	-42	215	and	<b>183.9</b>	<b>193.0</b>	<b>9.1</b>	<b>2.8</b>	<b>7.1</b>	
						381	271.0	278.0	7.0	2.6	4.3	
						and	380	<b>360.0</b>	<b>365.0</b>	<b>5.0</b>	<b>7.8</b>	<b>2.8</b>
KDU3956	19169	50288	9504	-32	190	380	<b>360.0</b>	<b>365.0</b>	<b>5.0</b>	<b>7.8</b>	<b>2.8</b>	
KDU3957	19175	50279	9504	-28	173	483	<b>361.0</b>	<b>374.8</b>	<b>13.8</b>	<b>3.0</b>	<b>9.2</b>	
						and	385.0	392.0	7.1	4.1	2.7	
						and	405.2	412.0	6.8	6.2	2.8	
						and	<b>434.0</b>	<b>451.0</b>	<b>17.0</b>	<b>3.3</b>	<b>7.0</b>	
KDU3958	19169	50288	9504	-40	186	495			NSI			
KDU4001	19169	50287	9505	-41	231	345			NSI			
KDU4002	19169	50287	9504	-39	207	400			NSI			
KDU4003	19169	50287	9504	-30	196	398	340.0	346.0	6.0	3.2	4.0	
KDU4004	19169	50287	9504	-23	188	420	208.9	212.0	3.1	3.2	1.7	
KDU4067	19171	50284	9504	-42	197	and	219.2	222.0	2.8	8.3	1.8	
						and	507	<b>327.2</b>	<b>330.1</b>	<b>2.9</b>	<b>14.4</b>	<b>1.8</b>
						and	<b>336.0</b>	<b>354.0</b>	<b>18.0</b>	<b>2.6</b>	<b>11.0</b>	
KDU4067	19171	50284	9504	-42	197	and	<b>336.0</b>	<b>354.0</b>	<b>18.0</b>	<b>2.6</b>	<b>11.0</b>	
KDU4091	19175	50279	9504	-34	175	617	485.2	492.9	7.8	6.1	3.1	
KDU4155	19171	50285	9504	-19	231	185	135.5	136.0	0.6	11.9	0.5	
						and	141.1	143.0	1.9	2.7	1.7	
						and	150.4	154.0	3.6	2.6	3.2	



KANOWNA SIGNIFICANT INTERSECTIONS - VELVET											
Drill Hole #	Eastings (Mine Grid)	Northing (Mine Grid)	Drill Hole Collar RL (Mine Grid)	Dip (degrees)	Azimuth (degrees, Mine Grid)	End of Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
KDU4157	19175	50279	9504	-36	184	486	426.0	428.0	2.0	10.7	1.0
						and	459.0	464.0	5.0	2.1	2.6
						and	473.0	476.0	3.0	2.3	1.6
						and	479.5	481.4	1.9	3.0	1.0
KDU4092	19175	50279	9504	-26	170	377	327.2	330.1	2.9	14.4	1.2
						and	<b>337.5</b>	<b>356.0</b>	<b>18.5</b>	<b>2.6</b>	<b>7.9</b>
						Including	337.5	347.0	9.5	3.7	4.0
KDU3707	19370	50254	9555	8	273	432	348.8	354.7	5.8	2.7	5.1
KDU3708	19371	50254	9556	11	282	474	363.3	367.4	4.1	3.6	2.4
KDU3712	19371	50254	9556	29	274	396	327.3	332.0	4.7	5.0	3.0
KDU3965	19178	50184	9585	-4	228	60	<b>29.0</b>	<b>37.0</b>	<b>8.0</b>	<b>11.1</b>	<b>7.8</b>
KDU3967	19178	50184	9587	16	223	60	26.8	28.0	1.3	5.1	1.2
KDU3969	19171	50188	9585	-16	225	64	<b>28.4</b>	<b>37.4</b>	<b>9.0</b>	<b>6.4</b>	<b>8.0</b>
						and	52.0	54.0	2.0	8.8	1.8
KDU3970	19171	50188	9585	-9	229	55	<b>27.5</b>	<b>33.9</b>	<b>6.4</b>	<b>10.1</b>	<b>6.0</b>
KDU3971	19161	50196	9585	-8	225	51	<b>29.0</b>	<b>49.8</b>	<b>20.8</b>	<b>3.3</b>	<b>19.6</b>
KDU3972	19161	50196	9587	10	226	55	<b>25.4</b>	<b>37.1</b>	<b>11.7</b>	<b>6.3</b>	<b>11.7</b>
KDU3973	19161	50196	9587	19	220	51	46.3	48.0	1.7	9.0	1.7
KDU3974	19162	50196	9588	39	222	60			NSI		
KDU3975	19154	50202	9585	-20	228	55	40.8	43.6	2.9	3.3	2.5
KDU3976	19155	50202	9587	33	234	60	27.0	32.2	5.2	4.9	4.8
KDU3977	19154	50202	9588	39	238	68	49.0	55.0	6.0	1.2	5.2
KDU3978	19143	50211	9585	-20	223	60	38.0	45.5	7.5	2.1	6.4
KDU3980	19143	50211	9587	21	222	65	<b>22.8</b>	<b>39.1</b>	<b>16.3</b>	<b>9.5</b>	<b>15.8</b>
						and	45.0	46.4	1.4	12.1	1.4
KDU3983	19128	50222	9589	39	227	72	<b>20.0</b>	<b>56.0</b>	<b>36.0</b>	<b>21.7</b>	<b>31.3</b>
						Including	<b>51.5</b>	<b>56.0</b>	<b>4.6</b>	<b>159.6</b>	<b>4.0</b>
KDU3985	19116	50231	9588	29	221	70	27.1	48.0	20.9	4.8	19.6
KDU3986	19128	50222	9589	47	221	77	23.3	24.9	1.6	3.9	1.2
						and	58.0	60.0	2.0	5.6	1.5
KDU4047	19214	50218	9616	13	255	141	88.2	91.0	2.9	5.3	2.5
						and	<b>108.8</b>	<b>113.0</b>	<b>4.2</b>	<b>5.7</b>	<b>3.7</b>
KDU4048	19213	50218	9616	16	264	150	103.1	105.0	1.9	3.8	1.6
KDU4049	19213	50218	9616	25	267	153	117.8	119.0	1.2	2.4	0.9
KDU4051	19214	50218	9616	26	248	126	86.0	88.4	2.4	2.3	2.2
						and	248	105.0	4.0	2.5	3.6
KDU4158	19370	50254	9558	40	283	425			NSI		
KDU4159	19370	50254	9557	27	283	498	348.0	350.0	2.0	3.6	1.3
						and	381.7	388.6	6.9	2.6	4.4

Table 5 - Paradigm Significant Intersections

PARADIGM SIGNIFICANT INTERSECTIONS											
Drill Hole #	Eastings (MGA grid)	Northing (MGA grid)	Collar RL (MGA)	Dip (degrees)	Azimuth (degrees, MGA grid)	Hole Depth (m)	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au (gpt) uncut	Est True Thickness (m)
PDDDD16029A	301828	6627255	424	-60	40	727	<b>518.9</b>	<b>519.3</b>	<b>0.5</b>	<b>88.2</b>	<b>0.4</b>
						and	585.1	585.4	0.3	45.4	0.2
PDDDD17123	301907	6627119	422	-60	51	350	241.5	242.8	1.3	3.9	1.0
PDDDD17125	301931	6627185	422	-60	76	393	323.6	326.5	2.9	1.6	2.3
PDDDD17127	302010	6627242	422	-60	76	180	90.0	91.0	1.0	13.8	0.8
PDDDD17130	301944	6627143	422	-65	73	340	260.0	261.4	1.4	4.0	1.1
PDDDD17132	301864	6627165	423	-62	76	441	182.2	182.5	0.3	5.1	0.2
PDDDD17135	301916	6627271	422	-60	76	273	185.0	186.0	1.0	11.0	0.5
						and	198.9	199.2	0.4	8.3	0.2
						and	252.1	252.8	0.7	4.3	0.3
PDDDD17136	301919	6627261	422	-66	76	300	140.5	141.0	0.5	11.1	0.2
						and	263.9	270.8	6.9	3.3	4.0
						and	288.5	289.1	0.6	7.8	0.2
PDDDD17137	3601848	6627242	423	-60	76	343			NSI		
PDDDD17163	301847	6627285	423	-60	76	355	207.0	207.3	0.3	6.7	0.2
PDDDD17164	301793	6627280	421	-62	75	679	<b>479.9</b>	<b>491.0</b>	<b>11.1</b>	<b>7.1</b>	<b>7.8</b>
						and	505.0	507.0	2.0	6.0	1.4
						and	509.0	513.0	4.0	5.8	2.8
PDDDD17165	302021	6627003	421	-60	74	250	<b>83.7</b>	<b>84.0</b>	<b>0.3</b>	<b>121.0</b>	<b>0.3</b>
						and	<b>97.9</b>	<b>98.4</b>	<b>0.5</b>	<b>260.5</b>	<b>0.4</b>
						and	<b>106.8</b>	<b>112.9</b>	<b>6.2</b>	<b>19.5</b>	<b>4.3</b>
						and	213.6	214.3	0.8	18.0	0.5
PDDDD17176	302007	6626979	419	-66	82	289	<b>235.1</b>	<b>236.5</b>	<b>1.4</b>	<b>69.2</b>	<b>0.7</b>
						and	246.0	249.7	3.7	6.5	2.6
PDDDD17178	302044	6626978	421	-60	88	284	65.4	65.8	0.4	3.7	0.3
						and	150.6	151.3	0.8	2.6	0.6
PDDDD17179	302174	6626922	419	-61	255	194	59.0	60.0	1.0	4.6	0.7
						and	<b>67.8</b>	<b>70.0</b>	<b>2.2</b>	<b>13.2</b>	<b>1.5</b>
						and	98.2	103.3	5.1	5.2	3.6
PDDDD17180	302218	6626933	419	-60	256	260	83.0	84.0	1.0	5.1	0.8
						and	106.6	107.3	0.7	3.0	0.6
PDDDD17181	302264	6626945	419	-60	256	350	126.0	127.0	1.0	4.1	0.8
						and	260.0	263.0	3.0	2.3	2.4
						and	311.9	314.0	2.1	1.9	1.7
PDDDD17182	302263	6626863	419	-55	256	271	103.1	104.5	1.4	1.4	0.7
PDDDD17184	301786	6627091	423	-50	45	570	498.0	501.4	3.4	2.2	7.6
						and	<b>508.0</b>	<b>510.0</b>	<b>2.0</b>	<b>3.2</b>	<b>6.4</b>
PDDDD17186	301798	6627377	424	-50	76	349	<b>333.0</b>	<b>333.5</b>	<b>0.5</b>	<b>427.0</b>	<b>0.3</b>
PDDDD17188	301692	6627294	412	-55	45	649	78.5	79.3	0.8	6.8	0.6
						and	209.8	210.5	0.7	6.9	0.6
						and	541.5	542.5	0.9	7.2	0.7
						and	<b>552.9</b>	<b>554.8</b>	<b>1.9</b>	<b>16.6</b>	<b>1.5</b>
PDDDD17192	301962	6627519	412	-60	77	670	112.8	113.1	0.3	14.3	0.2
						and	136.5	137.3	0.8	3.0	0.7
						and	373.7	374.3	0.5	3.0	0.4
						and	399.1	400.6	1.6	3.5	1.3
						and	<b>449.0</b>	<b>451.3</b>	<b>2.3</b>	<b>13.1</b>	<b>1.8</b>

## APPENDIX B – JORC CODE 2012 – TABLE 1 REPORTS

### Jundee (Ramone)

### JORC Code, 2012 Edition – Table 1 Report

### Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Sampling is by both diamond drilling (DD) and Reverse Circulation (RC) drilling completed by NSR. DD samples are HQ core with sample intervals defined by the geologist to honour geological boundaries ranging from 0.3 to 1.2m in length. RC samples are collected via rig-mounted static cone splitter with sample falling through inverted cone splitter, splitting the sample in 88%/9%/3% ratio. 9% split retained for 1m composites and 3% split retained for 4m composites. 1m samples are sent for further analysis if any 4m composites return a gold value > 0.1ppm or intervals containing alteration/mineralisation failed to return a significant composite assay result. NSR Resource definition drilling routinely collects 1m composites.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	DD core is aligned and measured by tape, comparing back to down hole core blocks consistent with industry practice. RC metre intervals are delineated with spray paint to determine metres drilled. Sample rejects are left on the sample pad to indicate metres drilled for the hole.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	Diamond drilling is completed to industry standard using varying sample lengths (0.3 to 1.2m) based on geological intervals, which are then crushed and pulverised to produce a ~200g pulp sub sample to use in the assay process. Diamond core samples are fire assayed (50g charge) and screen fire assayed for vis gold. Visible gold is occasionally encountered in core. RC sampling to industry standard at the time of drilling where ~4kg samples are pulverised to produce a ~200g pulp sample to utilise in the assay process. RC samples were fire assayed (50g charge).
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	RC drilling is carried out using a face sampling hammer and a 130mm diameter bit. Diamond drilling carried used HQ3 (triple tube) techniques in their entirety to deliver initial good quality oriented core for met/Geotech/geology work. Sampled sections were HQ3. Core is routinely orientated using the ORI-shot device.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	RC – Approximate recoveries are sometimes recorded as percentage ranges based on a visual and weight estimate of the sample. DD – Recoveries are recorded as a percentage calculated from measured core versus drilled intervals.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	Diamond drilling practice results in high core recovery due to the competent nature of the ground. RC drilling recovery is supervised on the rig and any recovery issues are recorded and rectified.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	There is no known relationship between sample recovery and grade, diamond drill sample recovery is very high.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	DD core and RC chip samples have been logged by qualified geologists to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies RC hole logging was carried out on a metre by metre basis and at the time of drilling.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Logging is Qualitative and Quantitative; all core is photographed wet. Visual estimates are made of sulphide, quartz and alteration as percentages.
	The total length and percentage of the relevant intersections logged.	100% of all DD and RC drilling is logged.

Criteria	JORC Code explanation	Commentary
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	DD core is halved with an Almonté diamond core saw. The core is quarter cut when metallurgical samples are required. Sample intervals are defined by a qualified geologist to honour geological boundaries. The left half is archived.  All mineralised zones are sampled plus associated visibly barren material in contact with mineralised zones.  Core is sampled on the width of the geological/mineralised structure with a minimum sample length of 0.3m and a maximum sample length of 1.2m. Total weight of each sample generally does not exceed 5kg.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	RC drilling uses a cyclone mounted inverted cone splitter.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	DD core is dried at 100°C to constant mass, all samples below approximately 4kg are totally pulverised in LM5's to nominally 90% passing a 75µm screen. The few samples generated above 4kg are crushed to <6mm and riffle split first prior to pulverisation.  RC samples are dried at 100°C to constant mass, all samples below approximately 3kg are totally pulverised in LM5's to nominally 85% passing a 75µm screen. Samples generated above 4kg are crushed to <6mm and cone split to nominal mass prior to pulverisation.  In 2012, Francois-Bongarcon (Agoratek International) conducted a heterogeneity studies, audit of site laboratory, and audit of plant samplers. Confirmed that the sampling protocol currently in use are appropriate to the mineralisation encountered and should provide representative results.  For RC samples, no formal heterogeneity study has been carried out or monographed. An informal analysis suggests that the sampling protocol currently in use are appropriate to the mineralisation encountered and should provide representative results.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Repeat analysis of pulp samples (all sample types) occurs at an incidence of 1 in 20 samples.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Field duplicates, (i.e. other half of cut core) are routinely assayed. NSR routinely collects field duplicates during RC drilling.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Sample sizes are considered appropriate.  No formal monograph study has been conducted on the RC primary sub sample split. Industry standard practice supports splitting of primary sub samples at particle sizes of <6mm and P <sub>80</sub> 75µm.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	For all drill samples, gold concentration was determined by fire assay using the lead collection technique with a 50-gram sample charge weight. MP-AES instrument finish was used to be considered as total gold.  Various multi-element suites are analysed using a four-acid digest with an AT/OES finish.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	Not applicable to this report.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	The QAQC protocols used include the following for all drill samples: <ul style="list-style-type: none"> <li>- Field QAQC protocols used for all drill samples include commercially prepared certified reference materials (CRM) inserted at an incidence of 1 in 30 samples. The CRM used is not identifiable to the laboratory with QAQC data is assessed on import to the database and reported monthly, quarterly and yearly.</li> <li>- NSR RC Resource definition drilling routinely inserts field blanks and monitor their performance.</li> <li>- Laboratory QAQC protocols used for all drill samples include repeat analysis of pulp samples occurs at an incidence of 1 in 20 samples and screen tests (percentage of pulverised sample passing a 75µm mesh) are undertaken on 1 in 40 samples.</li> <li>- The laboratories' own standards are loaded into the database and the laboratory reports its own QAQC data monthly.</li> <li>- In addition to the above, about 3% of diamond drill samples are sent to a check laboratory. Samples for check -assay are selected automatically from holes based on the following criteria: grade above 1 gpt or logged as a mineralised zone or is followed by feldspar flush or blank.</li> <li>- Failed standards are generally followed up by re-assaying a second 50g pulp sample of all samples in the fire above 0.1ppm by the same method at the primary laboratory.</li> </ul>

Criteria	JORC Code explanation	Commentary
		Both the accuracy component (CRM's and third-party checks) and the precision component (duplicates and repeats) of the QAQC protocols are thought to demonstrate acceptable levels of accuracy and precision.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	Significant intersections verified by corporate NSR personnel.
	The use of twinned holes.	There were purpose-drilled diamond core twinned holes to check selected RC holes, with strong correlation of geological and assay results.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Primary data is imported into SQL database using semi-automated or automated data entry with hard copies of core assays and surveys are stored at site. Visual checks are part of daily use of the data in Vulcan.
	Discuss any adjustment to assay data.	The first gold assay is almost always utilised for any Resource estimation except where evidence from re-assaying and/or check-assaying dictates. A systematic procedure utilising several re-assays and/or check assays is in place to determine when the final assay is changed from the first gold assay.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Collar positions are recorded using conventional survey methods based on Leica TS15 3" total stations and Trimble R10 GNSS instruments. The location of each station is referenced to state-wide network of Standard Survey Marks (SSM) established and coordinated by the Department of Land Administration (WA Government). Where regional drill hole positions are distant from the SSM network, the world wide Global Navigational Satellite System (GNSS) network is used.  Positional checks are carried out using a combination of existing known positions (usually based on prominent landmarks) and grid referenced information such as ortho-linear rectified photogrammetry based on the Map Gird of Australia MGA94.  Surface collar RL's have been validated utilising an airborne elevation survey by Arvista in October 2017. Multi shot cameras and gyro units were used for down-hole survey.
	Specification of the grid system used.	Collar coordinates are recorded in MGA94 Zone 51. The difference between magnetic north (MN) and true north (TN) is 1° 34' 30". The difference between true north (TN) and AMG84 Zone 51 (AMG GN) is 1° 02' 47". The difference between true north and GDA is zero.
	Quality and adequacy of topographic control.	Topographic control is from Digital Elevation Contours (DEM) 2017, 1m contour data and site surveyed pickups.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Exploration results in this report range from 25m x 25m drill hole spacing to 50m x 50m.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The data spacing and distribution is sufficient to establish geological and/or grade continuity appropriate for the Mineral Resource and classifications to be applied.
	Whether sample compositing has been applied.	Core is sampled to geology; sample compositing is not applied until the estimation stage. RC samples are taken as 1 m samples. For RC Resource definition drilling 1 m samples are routinely collected.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	The orientation of sampling is generally on a high angle to the main mineralisation trends as these are vertical to sub-vertical. Drill holes are drilled on a 60 degrees angle.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	The drill orientation to mineralised structures biases the number of samples per drill hole. It is not thought to make a material difference in the Resource estimation.
Sample security	The measures taken to ensure sample security.	All samples are selected, cut and bagged in tied numbered calico bags, grouped in larger tied plastic bags, and placed in large sample cages with a sample submission sheet. The cages are either sent to the site laboratory or are transported via freight truck to Perth, with consignment note and receipted by external and independent laboratory  All sample submissions are documented, and all assays are returned via email and hard copy.  Sample pulp splits from the site lab are stored at the Jundee mine site and those from Perth are stored at the Newburn and Malaga labs.  RC samples processed at SGS have had the bulk residue discarded and pulp packets sent to Jundee mine site for long term storage.

Criteria	JORC Code explanation	Commentary
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	Historical audits of all Jundee data were carried out by previous operators. In 2012, Francois-Bongarcon (Agoratek International) conducted a heterogeneity studies, audit of site laboratory, and audit of plant samplers. Both audits found the sampling techniques and data to be adequate. All recent NSR sample data has been extensively QAQC reviewed both internally and externally.

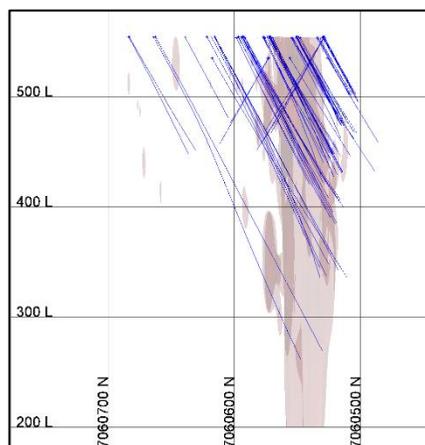
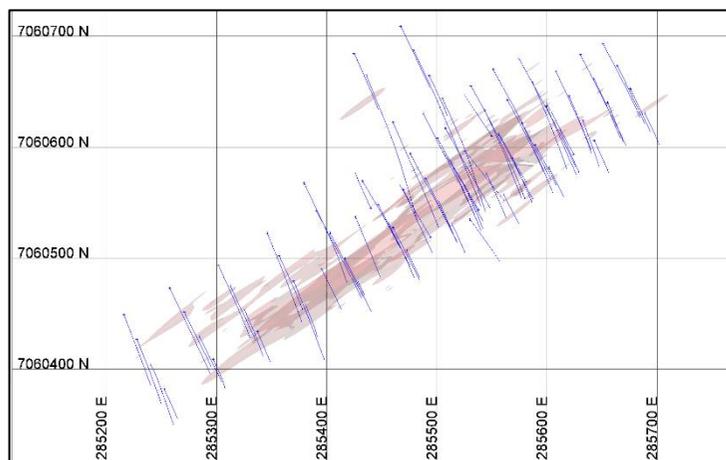
## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Jundee Project consists of 62 Mining Leases and 1 General Purpose Lease covering a total area of approximately 57,422.2 Ha. All are registered in the name of Northern Star Resources Limited. The Project also includes 23 Miscellaneous Licences, 3 Groundwater Licenses, a Pipeline License and the Jundee Pastoral Lease covering the bore fields, roads, airstrip, and gas pipeline. There are numerous access agreements in place including access rights over part of M53/193 which lies contiguous to, and beneath, the General Purpose Lease on which the Jundee processing plant is located. There are no heritage issues with the current operation. The majority of the Jundee leases are granted Mining Leases prior to 1994 (pre-Mabo) and as such Native Title negotiations are not required. During 2004, two agreements were struck between Ngaanyatjarra Council (now Central Desert Native Title Services (CDNTS)) and NYO, these agreements being the Wiluna Land Access Agreement 2004 and the Wiluna Claim Heritage Agreement 2004.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	All leases and licences to operate are granted and in the order for between 3 and 21 years.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	Not Applicable, all the exploration work has been completed by NSR.
Geology	Deposit type, geological setting and style of mineralisation.	Jundee is an Archean lode-gold mineralised deposit that is part of the Northern Yandal Greenstone belt. Gold mineralisation is controlled by a brittle fracture-system, is commonly fracture-centred, and is predominantly hosted in dolerite, basalt and felsic intrusive. Mineralisation can be disseminated or vein style host.
Drill hole information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>o easting and northing of the drill hole collar</li> <li>o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>o dip and azimuth of the hole</li> <li>o down hole length and interception depth</li> <li>o hole length.</li> </ul>	All relevant information is part of this release
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Not Applicable
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	Results are reported using a nominal 0.5 gpt Au cut-off and up to 2-meter internal waste.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	All the RC samples are 1m in length
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents are reported.
	These relationships are particularly important in the reporting of Exploration Results.	All the drill holes have been drilled on 60 degrees angle.

Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	Mineralisation structures are vertical to sub-vertical.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	It is interpreted that true width is approximately 50-70% of down hole intersections.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Diagrams from part of the main release.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	All results for this period are listed, including those labelled NSI (no significant intersection)
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	Preliminary metallurgy work shows recoveries above 95%.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Further extensional and definition drilling is planned for FY2018.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Plans and sections of the Ramone deposit are included in this report.

## RAMONE - REPRESENTATIVE PLANS & CROSS SECTIONS



## Jundee

### JORC Code, 2012 Edition – Table 1

#### Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	DD - Sampled sections are generally NQ2 or BQ. Core sample intervals are defined by the geologist to honour geological boundaries ranging from 0.3 to 1.2m in length.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Core is aligned and measured by tape, comparing back to downhole core blocks consistent with industry practice.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	Diamond drilling completed to industry standard using varying sample lengths (0.3 to 1.2m) based on geological intervals, which are then crushed and pulverised to produce a ~200g pulp sub sample to use in the assay process. Diamond core samples are fire assayed (30g charge). Visible gold is occasionally encountered in core.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Surface diamond drilling carried out by using both HQ2 or HQ3 or PQ2 (triple tube) and NQ2 (standard tube) techniques. Sampled sections are generally NQ2. Core is routinely orientated using the ORI-shot device.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	DD – Recoveries are recorded as a percentage calculated from measured core verses drilled intervals.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	Diamond drilling practice results in high core recovery due to the competent nature of the ground.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	There is no known relationship between sample recovery and grade, diamond drill sample recovery is very high.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	Core is logged by qualified Geologist to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Logging is Qualitative and Quantitative, and all core is photographed wet (some older core is pre-digital, photos not all reviewed). Visual estimates of sulphide, quartz and alteration as percentages.
	The total length and percentage of the relevant intersections logged.	100% of the drill core is logged.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	DD - Resource Definition Drilling uses NQ2: Core is half cut with an Almonté diamond core saw. Sample intervals are defined by a qualified geologist to honour geological boundaries. The left half is archived - Grade Control Drilling uses BQ: Whole core sampling is undertaken. Sample intervals are defined by a qualified geologist to honour geological boundaries. All mineralised zones are sampled, plus associated visibly barren material in contact with mineralised zones . Core is sampled on the width of the geological/mineralised structure in recognized ore zones. The minimum sample length is 0.3m while the maximum is 1.2m. Total weight of each sample generally does not exceed 5kg.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	Core results only being released in this case
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	Following drying at 100°C to constant mass, all samples below approximately 4kg are totally pulverised in LM5's to nominally 90% passing a 75µm screen. The very few samples generated above 4kg are crushed to <6mm and riffle split first prior to pulverisation.

Criteria	JORC Code explanation	Commentary
		In 2012, Francois-Bongarcon (Agoratek International) conducted a heterogeneity studies, audit of site laboratory, and audit of plant samplers. Confirmed that the sampling protocol currently in use are appropriate to the mineralisation encountered and should provide representative results.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Repeat analysis of pulp samples (for all sample types – diamond, RC, rock and soil) occurs at an incidence of 1 in 20 samples.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Field duplicates, i.e. other half of cut core, have not been routinely assayed.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Sample sizes are considered appropriate.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	For all drill core samples, gold concentration is determined by fire assay using the lead collection technique with a 30-gram sample charge weight. An AAS finish is used to be considered as total gold.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	Seismic is used for interpretations and drill planning
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	<p>The QAQC protocols used include the following for all drill samples:</p> <ul style="list-style-type: none"> <li>▪ The field QAQC protocols used include the following for all drill samples:                             <ul style="list-style-type: none"> <li>- Commercially prepared certified reference materials (CRM) are inserted at an incidence of 1 in 30 samples. The CRM used is not identifiable to the laboratory,</li> <li>- QAQC data is assessed on import to the database and reported monthly, quarterly and yearly.</li> </ul> </li> <li>▪ The laboratory QAQC protocols used include the following for all drill samples:                             <ul style="list-style-type: none"> <li>- Repeat analysis of pulp samples occurs at an incidence of 1 in 20 samples,</li> <li>- Screen tests (percentage of pulverised sample passing a 75µm mesh) are undertaken on 1 in 40 samples,</li> <li>- The laboratories' own standards are loaded into the database,</li> <li>- The laboratory reports its own QAQC data on a monthly basis.</li> <li>- In addition to the above, ~ 3% of samples are sent to a check laboratory. Samples for check -assay are selected automatically from holes, based on the following criteria: grade above 1gpt or logged as a mineralised zone or is followed by feldspar flush or blank.</li> </ul> </li> <li>▪ Failed standards are generally followed up by re-assaying a second 30g pulp sample of samples between the failed standard and the next sequenced standard by the same method at the primary laboratory. Re-assays are dependent on grade above 0.1ppm</li> </ul> <p>Both the accuracy component (CRM's and third-party checks) and the precision component (duplicates and repeats) of the QAQC protocols are thought to demonstrate acceptable levels of accuracy and precision.</p>
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	Significant intersections verified cy corporate NSR personnel
	The use of twinned holes.	There are no purpose drilled twinned holes.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Primary Data imported into SQL database using semi-automated or automated data entry. Hard copies of NSR and previous operators, core assays and surveys are stored at site. Visual checks are part of daily use of the data in Vulcan.
	Discuss any adjustment to assay data.	A systematic procedure utilising several re-assays and/or check assays is in place to determine when the final assay is changed from the first gold assay. Some minor adjustments have been made to overlapping data.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Collar positions are recorded using conventional survey methods based on Leica TS15 3" total stations and Trimble R10 GNSS instruments. The location of each station is referenced to state-wide network of Standard Survey Marks (SSM) established and coordinated by the Department of Land Administration (WA Government). Where regional drill hole positions are distant from the SSM network the world wide Global Navigational Satellite System (GNSS) network is used. Positional checks are carried out using a combination of existing known positions (usually based on prominent landmarks) and grid referenced information such as ortholinear rectified photogrammetry based on the Australian Map Grid 1984 (AMG84_51).

Criteria	JORC Code explanation	Commentary
		Collar coordinates are recorded in MGA94 or Local Jundee Grid (JUNL2) dependant on the location and orientation of ore-bodies. Cross checks were made on the survey control points and data in June 2005. Collar information is stored in both local coordinates and MGA94 coordinate in the drilling database. In-mine drill-hole collars are normally accurate to 10 cm. Multi shot cameras and gyro units were used for down-hole survey.
	Specification of the grid system used.	Collar coordinates are recorded in AMG84 Zone 51 (AMG GN) and Local Jundee Grid (JUNL2) dependant on the location and orientation of ore-bodies. The difference between Jundee mine grid (GN) and magnetic north (MN) as at 31 December 2011 is 39° 35' 00" and the difference between magnetic north (MN) and true north (TN) is 1° 34' 30". The difference between true north (TN) and AMG84 Zone 51 (AMG GN) is 1° 02' 47". The difference between true north and GDA is zero.
	Quality and adequacy of topographic control.	Topographic control is from Digital Elevation Contours (DEM) 2010, 1m contour data and site surveyed pit pickups.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	All Reserves are based on a maximum drill hole spacing of 40m x 40m and all Resources are based on a maximum of 80m x 80m.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Reserves are generally based on 20m x 20m drilling up to a maximum of 40m x 40m. Resources are generally based on 40m x 40m drilling up to a maximum of 80m x 80m. The data spacing and distribution is sufficient to establish geological and/or grade continuity appropriate for the Mineral Resource and classifications to be applied.
	Whether sample compositing has been applied.	Core is sampled to geology; sample compositing is not applied until the estimation stage.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	The orientation of sampling is generally perpendicular to the main mineralisation trends. The orientation achieves unbiased sampling of all possible mineralisation and the extent to which this is known.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	The drill orientation to mineralised structures biases the number of samples per drill hole. It is not thought to make a material difference in the Resource estimation. As the opportunity arises, better angled holes are infill drilled.
Sample security	The measures taken to ensure sample security.	All samples are selected, cut and bagged in tied numbered calico bags, grouped in larger tied plastic bags, and placed in large sample cages with a sample submission sheet. The cages are either sent to the site laboratory or are transported via freight truck to Perth, with consignment note and receipted by external and independent laboratory. All sample submissions are documented and all assays are returned via email. Sample pulp splits from the site lab are stored at the Jundee mine site and those from the Newburn Lab in Perth are stored at the Newburn Lab.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	In 2006, Maxwell conducted an audit of all Jundee data. In 2012, Francois-Bongarcon (Agoratek International) conducted a heterogeneity studies, audit of site laboratory, and audit of plant samplers. Both audits found the sampling techniques and data to be adequate. All recent NSR sample data has been extensively QAQC reviewed both internally and externally.

## Section 2 Reporting of Exploration Results

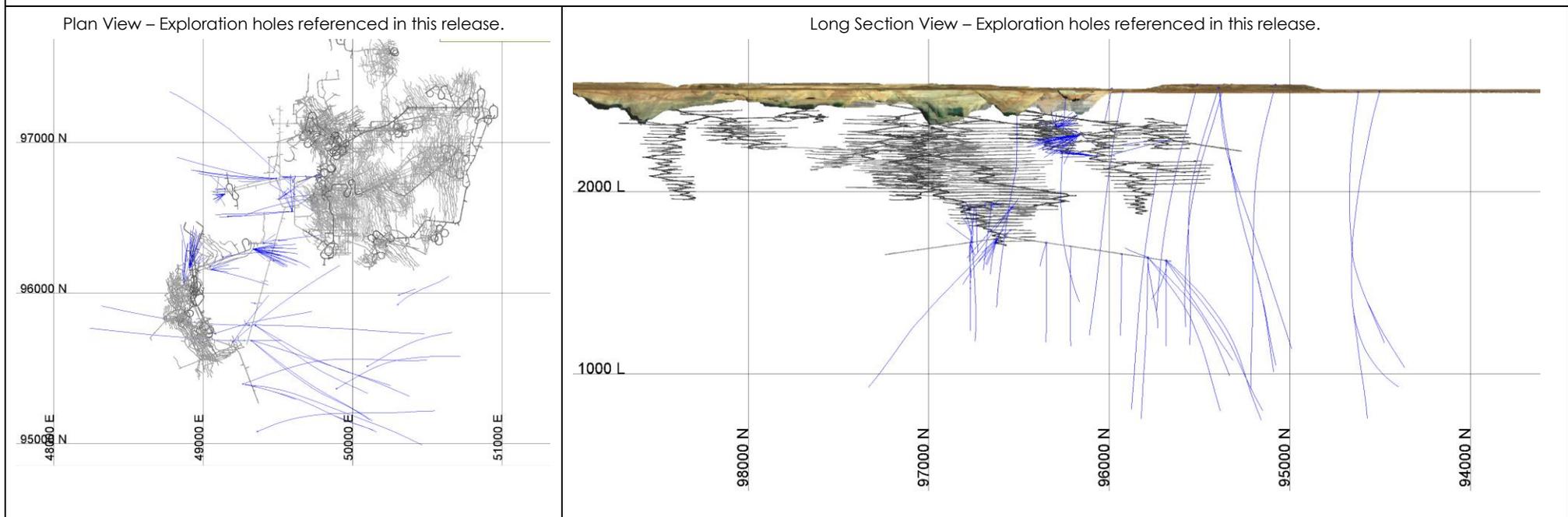
(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Jundee project consists of tenements comprising 62 mining leases and 1 general purpose lease, covering a total area of approximately 57,422.2 Ha. All are registered in the name of Northern Star Resources Limited. The project also includes 23 miscellaneous licences, 3 groundwater licenses, a pipeline license, and the Jundee Pastoral Lease. These cover the bore fields, roads, airstrip, and gas pipeline. There are numerous access agreements in place including access rights over part of Mark Creasy's mining lease 53/193 which lies contiguous to and beneath the general purpose lease on which the Jundee gold mine processing plant is located. There are no heritage issues with the current operation. The majority of the Jundee leases are granted Mining Leases prior to 1994 (pre Mabo) and as such Native Title negotiations are not required. During 2004, two agreements where

Criteria	JORC Code explanation	Commentary
		struck between Ngaanyatjarra Council (now Central Desert native Title Services (CDNTS)) and NYO, these agreements being the Wiluna Land Access Agreement 2004 and the Wiluna Claim Heritage Agreement 2004.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	All leases and licences to operate are granted and in the order for between 3 and 20 years.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	The Jundee/Nimary Deposits were discovered in the late 1980's/early 1990's after LAG and soil sampling by Mark Creasy (Jundee) and Hunter Resources (Nimary) identified large surface gold anomalies. The deposits were drilled out over the following years by Eagle Mining (which took over Hunter Resources), and Great Central Mines (which formed a joint venture with Creasy and later purchased his share). Open pit operations commenced in mid-1995, with the first gold poured in December 1995. Great Central Mines assumed full control of the field with its successful takeover of Eagle Mining in mid-1997. Great Central Mines was later taken over by Normandy in mid-2000, which in turn was taken over by Newmont in early-2002. NSR purchased the Jundee project in 2014
Geology	Deposit type, geological setting and style of mineralisation.	Jundee is an Archean lode-gold mineralised deposit that is part of the Northern Yandal Greenstone belt. Gold mineralisation is controlled by a brittle fracture-system, is commonly fracture-centred, and is predominantly hosted in dolerite and basalt. Mineralisation can be disseminated or vein style host.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>o easting and northing of the drill hole collar</li> <li>o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>o dip and azimuth of the hole</li> <li>o down hole length and interception depth</li> <li>o hole length.</li> </ul>	A table listing all holes relevant to this announcement is included in the release
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Exclusion of the drill information will not detract from the understanding of the report.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	Reported exploration results are uncut.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Short intervals are length weighted to create the final intersections.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents are reported.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results: <ul style="list-style-type: none"> <li>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> <li>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').</li> </ul>	Due to complex mineralisation geometry and varying intercept angles the true thickness is manually estimated on a hole by hole basis.  Downhole length and estimated true width is shown in the report tables.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Plan view and long section views of relevant drilling forms part of this release.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	The results released are considered representative of the results received to date.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results;	No other meaningful data to report.

Criteria	JORC Code explanation	Commentary
	bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Further extensional and definition drilling is planned for FY2018 from both underground and surface positions.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Representative diagrams are attached with this report.

## JUNDEE EXPLORATION RESULTS – PLAN & LONG SECTION



## Millennium - February 2018 JORC Code, 2012 Edition – Table 1 Report Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Sampling was completed using underground diamond drilling. Diamond core was transferred to core trays for logging and sampling. Whole core samples were nominated by the geologist and based upon geological and ore-zone boundaries, with the remaining sampled on metre intervals.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Diamond core was transferred to core trays for logging and sampling. Half core samples were nominated by the geologist from NQ2 diamond core with a minimum sample width of 30cm.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	DD drill core was cut in half using an automated core saw the mass of material collected will depend on the hole size and sampling interval.  Core samples were nominated by the geologist from the diamond core, generally being around one metre in length, but with sample widths ranging between approximately 0.3m and 1.0m as dictated by the geology. Sample lengths varied because drill core samples were allocated so as not to cross significant geological boundaries.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Underground drilling at Millennium utilised NQ2 (50.5mm) diameter core.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	For diamond drilling, the contractors adjust their rate of drilling and method if recovery issues arise.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Recovery is excellent for diamond core and no relationship between grade and recovery was observed.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	All diamond core is logged for regolith, lithology, veining, alteration, mineralisation and structure. Structural measurements of specific features are also taken through oriented zones.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	All logging is quantitative where possible and qualitative elsewhere. A photograph is taken of every core tray.
	The total length and percentage of the relevant intersections logged.	The average intersection length is 1.81m.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	Diamond core is cut using an automated core saw. In most cases, half the core is taken for sampling with the remaining half being stored for later reference. Whole core sampling was only utilised in areas where the Geology is well understood and there is less requirement to retain core for future reference.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	Not relevant.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The sample preparation is considered appropriate.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Grind checks are performed at both the crushing stage(3mm) and pulverising stage (75µm), requiring 90% of material to pass through the relevant size.  Duplicates, pulp duplicates and crush duplicates are also performed.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Sample preparation was conducted at Bureau Veritas Kalgoorlie.

Criteria	JORC Code explanation	Commentary
		The sample preparation process commencing with sorting, checking and drying at less than 110°C to prevent sulphide breakdown. Samples are jaw crushed to a nominal -6mm particle size. If the sample is greater than 3kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3kg (typically 1.5kg) at a nominal <3mm particle size. The entire crushed sample (if less than 3kg) or sub-sample is then pulverised to 90% passing 75µm, using a Labtechnics LM5 bowl pulveriser. 300g pulp subsamples are then taken with an aluminium or plastic scoop and stored in labelled pulp packets.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Grind checks are performed at both the crushing stage(3mm) and pulverising stage (75µm), requiring 90% of material to pass through the relevant size.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	A 40g fire assay charge is used with a lead flux in the furnace. The prill is totally digested by HCl and HNO <sub>3</sub> acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical tools were used to determine any element concentrations.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Certified reference materials (CRMs) are inserted into the sample sequence randomly at a rate of 1 per 20 samples to test the analysis process. Any values outside of 3 standard deviations are re-assayed with a new CRM. blanks are inserted into the sample sequence at a rate of 1 per 20 samples. This is random, except where high grade mineralisation is expected. Here, a Blank is inserted after the high-grade sample to test for contamination. Failures above 0.2gpt are followed up, and re-assayed. New pulps are prepared if failures remain. No field duplicates are submitted for diamond core. Umpire sampling programs are carried out on an ad-hoc basis. Regular audits of laboratory facilities are undertaken by Northern Star personnel.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	All significant intersections are verified by another Northern Star geologist during the drill hole validation process, and later by a Competent Person to be signed off.
	The use of twinned holes.	No twinned holes were drilled for this data set
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Geological logging is directly entered into an Acquire database. Assay files are received in csv format and loaded directly into the database by the project's responsible geologist with an Acquire importer object. Hardcopy and electronic copies of these are stored.
	Discuss any adjustment to assay data.	No adjustments are made to this assay data.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Underground diamond hole positions are marked before drilling by mine survey staff and the actual hole collar position located by mine survey staff once drilling is completed. During drilling, single-shot surveys are every 30m to ensure the hole remains close to design. This is performed using the Reflex Ez-Trac system. For UG holes multi-shot surveys are taken every 9m when retreating out of the hole.
	Specification of the grid system used.	Data is collected using both local mine grid (Kundana 10) and MGA 94 Zone 51 as appropriate.
	Quality and adequacy of topographic control.	The Differential GPS returns reliable elevation data which has been confirmed against a high resolution Digital Terrain Model survey performed by Arvista in 2015.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Drill hole spacing for these results were typically 20m x 20m to provide definition of economic ore shoots.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The data spacing and distribution is considered sufficient to support the Resource and Reserve estimates. Surrounding exploration drilling can be spaced up to 200m apart.
	Whether sample compositing has been applied.	Sample data is composited before grade estimation is undertaken. Average intersection grades are reported in ASX and corporate announcements.
	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	Most of the structures in the Kundana Project dip steeply (80°) to WSW. To target these orientations, the drill hole dips of 60-70° towards ~060° achieve high angle intersections on all structure.

Criteria	JORC Code explanation	Commentary
Orientation of data in relation to geological structure	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No sampling bias is considered to have been introduced by the drilling orientation.
Sample security	The measures taken to ensure sample security.	Prior to laboratory submission samples are stored by Northern Star Resources in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound, and tracked through their chain of custody and via audit trails.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	No audits or reviews have recently been conducted on sampling techniques.

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Millennium-Centenary Mine is located on Mining Lease M16/87, M16/72, M16/157, which is owned by Kundana Gold Pty Ltd, a wholly owned subsidiary of Northern Star Resources Limited. There are no private royalty agreements applicable to this tenement.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	No known impediments exist and the tenements are in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	All drilling and exploration of the Kundana project was conducted by previous owners of the tenements (including Pancontinental Gold, Aurion Gold, Placer Dome Inc, Barrick Gold) prior to the acquisition by Northern Star Resources.
Geology	Deposit type, geological setting and style of mineralisation.	The Kundana camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain.  K2-style mineralisation consists of narrow vein deposits hosted by shear zones located along steeply-dipping overturned lithological contacts. The K2 structure is present along the contact between a black shale unit (Centenary shale) and intermediate volcanics (Spargoville formation).  Early indications from the diamond drilling of this report indicate a late generation of shearing overprinting and largely focussed along the earlier K2 structure. At this stage, it is unclear if this later generation of shearing is associated with an additional mineralising event.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>o easting and northing of the drill hole collar</li> <li>o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>o dip and azimuth of the hole</li> <li>o down hole length and interception depth</li> <li>o hole length.</li> </ul>	All drill holes are listed in the appendix
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Exclusion of the drill information will not detract from the understanding of the report.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	All reported assay results have been length weighted to provide an intersection width. A maximum of 2m of barren material between mineralised samples has been permitted in the calculation of these widths.  Typically grades over 1.0gpt are considered significant, however, where low grades are intersected in areas of known mineralisation these will be reported. No top-cutting is applied when reporting intersection results.

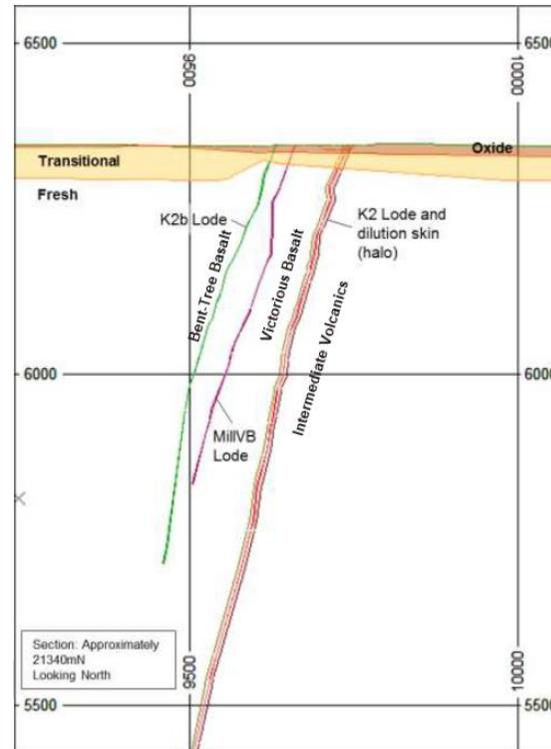
Criteria	JORC Code explanation	Commentary
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.##gpt including ##.#m @ ##.##gpt.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalent values have been used for the reporting of these exploration results.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results:	True widths have been calculated for intersections of the known ore zones based on existing knowledge of the nature of these structures.
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	The target structure is very planar and its orientation well constrained, allowing very reliable calculations of true widths. True widths have been calculated for all reported intersections.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	Both the downhole width and true width have been clearly specified when used.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Appropriate plans and section have been included in this report.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced avoiding misleading reporting of Exploration Results.	Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and 'From' and 'To' depths.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	No other material exploration data has been collected for this area.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Additional drilling is planned with the intention of extending known mineralisation laterally and at depth. Drilling will also be undertaken to improve confidence in previously identified mineralisation and to assist in the location of high grade shoots.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Appropriate diagrams accompany this release.

## MILLENNIUM – CENTENARY REPRESENTATIVE PLAN AND CROSS SECTION DIAGRAMS

Plan view of the Millennium-Centenary Resource and nearby infrastructure



Cross Section of the Millennium / Centenary Deposits



## Barker's Exploration Results - February 2018 JORC Code, 2012 Edition – Table 1 Report Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Sampling was completed using underground diamond drilling. Diamond core was transferred to core trays for logging and sampling. Whole core samples were nominated by the geologist and based upon geological and ore-zone boundaries, with the remaining sampled on metre intervals.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Diamond core was transferred to core trays for logging and sampling. Half core samples were nominated by the geologist from NQ2 diamond core with a minimum sample width of 30cm.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	Due to the high-nugget nature of mineralisation of Barker's-Helga's mineralisation, whole core sampling was employed to provide a more representative sample.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Underground drilling at Barker's utilised NQ2 (50.5mm) diameter core.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	For diamond drilling, the contractors adjust their rate of drilling and method if recovery issues arise.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Recovery is excellent for diamond core and no relationship between grade and recovery was observed
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	All diamond core is logged for regolith, lithology, veining, alteration, mineralisation and structure. Structural measurements of specific features are also taken through oriented zones.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	All logging is quantitative where possible and qualitative elsewhere. A photograph is taken of every core tray.
	The total length and percentage of the relevant intersections logged.	
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	Whole core sampling has been used for this drilling campaign.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	Not relevant.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The sample preparation is considered appropriate.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Umpire sampling is conducted regularly across Kalgoorlie Operations for all sample types.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Sample preparation was conducted at Bureau Veritas Kalgoorlie. The sample preparation process commencing with sorting, checking and drying at less than 110°C to prevent sulphide breakdown. Samples are jaw crushed to a nominal -6mm particle size. If the sample is greater than 3kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3kg (typically 1.5kg) at a nominal <3mm particle size. The entire crushed sample (if less than 3kg) or sub-sample is then pulverised to 90% passing

Criteria	JORC Code explanation	Commentary
		75µm, using a Labtechnics LM5 bowl pulveriser. 300g pulp subsamples are then taken with an aluminium or plastic scoop and stored in labelled pulp packets.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Grind checks are performed at both the crushing stage(3mm) and pulverising stage (75µm), requiring 90% of material to pass through the relevant size.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	A 40g fire assay charge is used with a lead flux in the furnace. The prill is totally digested by HCl and HNO <sub>3</sub> acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical tools were used to determine any element concentrations.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Certified reference materials (CRMs) are inserted into the sample sequence randomly at a rate of 1 per 20 samples to test the analysis process. Any values outside of 3 standard deviations are re-assayed with a new CRM. blanks are inserted into the sample sequence at a rate of 1 per 20 samples. This is random, except where high grade mineralisation is expected. Here, a Blank is inserted after the high-grade sample to test for contamination. Failures above 0.2gpt are followed up, and re-assayed. New pulps are prepared if failures remain. No field duplicates are submitted for diamond core. Umpire sampling programs are carried out on an ad-hoc basis. Regular audits of laboratory facilities are undertaken by Northern Star personnel.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	All significant intersections are verified by another Northern Star geologist during the drill hole validation process, and later by a Competent Person to be signed off.
	The use of twinned holes.	No twinned holes were drilled for this data set
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Geological logging is directly entered into an Acquire database. Assay files are received in csv format and loaded directly into the database by the project's responsible geologist with an Acquire importer object. Hardcopy and electronic copies of these are stored.
	Discuss any adjustment to assay data.	No adjustments are made to this assay data.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Underground diamond hole positions are marked before drilling by mine survey staff and the actual hole collar position located by mine survey staff once drilling is completed. During drilling, single-shot surveys are every 30m to ensure the hole remains close to design. This is performed using the Reflex Ez-Trac system. For UG holes multi-shot surveys are taken every 9m when retreating out of the hole.
	Specification of the grid system used.	Kundana mine grid known as K10 is used
	Quality and adequacy of topographic control.	The Differential GPS returns reliable elevation data which has been confirmed against a high resolution Digital Terrain Model survey performed by Arvista in 2015.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	For the Resource definition drilling, spacing for Barker's is 30m x 30m.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Resource definition drilling spacing was typically 40m x 40m, to allow the Resource to be upgraded to indicated. For the Barker's underground drilling, drill spacing was reduced to 30m x 30m due to the nuggetty nature of mineralisation. UG grade control drilling spacing is typically 20m x 20m to define high-grade ore shoots. Surrounding exploration drilling can be spaced up to 200m apart.
	Whether sample compositing has been applied.	No compositing has been applied to these exploration results, although composite intersections are reported.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	Most of the structures in the Kundana Project dip steeply (80°) to WSW. To target these orientations, the drill hole dips of 60-70° towards ~060° achieve high angle intersections on all structure.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No sampling bias is considered to have been introduced by the drilling orientation.

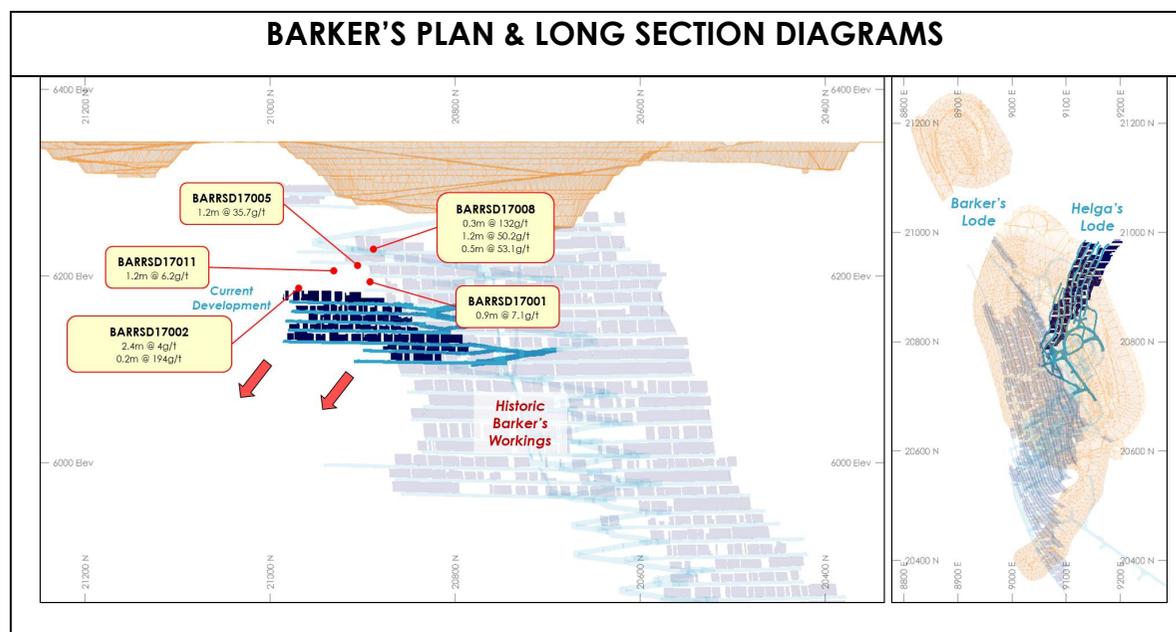
Criteria	JORC Code explanation	Commentary
Sample security	The measures taken to ensure sample security.	Prior to laboratory submission samples are stored by Northern Star Resources in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound, and tracked through their chain of custody and via audit trails.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	No audits or reviews have recently been conducted on sampling techniques.

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Barker's Mine is located on Mining Lease M16/72, which is owned by Kundana Gold Pty Ltd, a wholly owned subsidiary of Northern Star Resources Limited. There are no private royalty agreements applicable to this tenement.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	No known impediments exist and the tenements are in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	All drilling and exploration of the Kundana project was conducted by previous owners of the tenements (including Pancontinental Gold, Aurion Gold, Placer Dome Inc, Barrick Gold) prior to the acquisition by Northern Star Resources.
Geology	Deposit type, geological setting and style of mineralisation.	The Kundana camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain.  Barker's-style mineralisation consists of narrow vein deposits (0.20m to 1.0m thick) hosted by shear zones located along steeply-dipping overturned lithological contacts.  The footwall stratigraphy of Barker's consists of several different units of the Powder Sill Gabbro, a thick stratigraphy-parallel differentiated mafic intrusive. The volcanoclastic sedimentary rocks of the hanging-wall consist of a sequence of interbedded siltstones, feldspathic sandstones, feldspathic-lithic wackes and feldspathic-lithic rhyolites.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>o easting and northing of the drill hole collar</li> <li>o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>o dip and azimuth of the hole</li> <li>o down hole length and interception depth</li> <li>o hole length.</li> </ul>	All drill holes are listed in the appendix
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Exclusion of the drill information will not detract from the understanding of the report.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	All reported assay results have been length weighted to provide an intersection width. A maximum of 2m of barren material between mineralised samples has been permitted in the calculation of these widths. Typically grades over 1.0gpt are considered significant, however, where low grades are intersected in areas of known mineralisation these will be reported. No top-cutting is applied when reporting intersection results.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.##gpt including ##.#m @ ##.##gpt.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalent values have been used for the reporting of these exploration results.

Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results:	True widths have been calculated for intersections of the known ore zones based on existing knowledge of the nature of these structures.
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	Both the downhole width and true width have been clearly specified when used.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	Denoted in the drill results table where applicable.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Appropriate plans and section have been included in this report.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and 'From' and 'To' depths.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	No other material exploration data has been collected for this area.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Further work will continue in 2018/2019 to extend the Indicated Resource deeper by additional drilling and identify new mineralised shoots on the Barker's and Helga's lode system.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Appropriate diagrams accompany this release.



## Hornet-Rubicon-Pegasus-Raleigh – February 2018

### JORC Code, 2012 Edition – Table 1 Report

#### Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Sampling was completed using underground diamond drilling. Diamond core was transferred to core trays for logging and sampling. Whole core samples were nominated by the geologist and based upon geological and ore-zone boundaries, with the remaining sampled on metre intervals.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Diamond core was transferred to core trays for logging and sampling. Half core samples were nominated by the geologist from NQ2 diamond core with a minimum sample width of 30cm. Occasionally whole core sampling is employed where core recovered is overly fractured or for grade control purposes.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	DD drill core was cut in half using an automated core saw the mass of material collected will depend on the hole size and sampling interval.  Core samples were nominated by the geologist from the diamond core, generally being around one metre in length, but with sample widths ranging between approximately 20cm and 100cm as dictated by the geology. Sample lengths varied because drill core samples were allocated so as not to cross significant geological boundaries.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Underground drilling utilised NQ2 (50.5mm) diameter core.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	For diamond drilling the contractors adjust their rate of drilling and method if recovery issues arise.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Recovery was excellent for diamond core and no relationship between grade and recovery was observed.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	All diamond core is logged for regolith, lithology, veining, alteration, mineralisation and structure. Structural measurements of specific features are also taken through oriented zones.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	All logging is quantitative where possible and qualitative elsewhere. A photograph is taken of every core tray.
	The total length and percentage of the relevant intersections logged.	
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	Diamond core is cut using an automated core saw. In most cases, half the core is taken for sampling with the remaining half being stored for later reference. Whole core sampling was only utilised in areas where the Geology is well understood and there is less requirement to retain core for future reference.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	Not relevant.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The sampling types used are considered appropriate for the deposits.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Grind checks are performed at both the crushing stage(3mm) and pulverising stage (75µm), requiring 90% of material to pass through the relevant size.  Duplicates, pulp duplicates and crush duplicates are also performed.

Criteria	JORC Code explanation	Commentary
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Sample preparation was conducted at Bureau Veritas Kalgoorlie. The sample preparation process commencing with sorting, checking and drying at less than 110°C to prevent sulphide breakdown. Samples are jaw crushed to a nominal -6mm particle size. If the sample is greater than 3kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3kg (typically 1.5kg) at a nominal <3mm particle size. The entire crushed sample (if less than 3kg) or sub-sample is then pulverised to 90% passing 75µm, using a Labtechnics LM5 bowl pulveriser. 300g pulp subsamples are then taken with an aluminium or plastic scoop and stored in labelled pulp packets.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Grind checks are performed at both the crushing stage(3mm) and pulverising stage (75µm), requiring 90% of material to pass through the relevant size.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	A 40g Fire assay charge is used with a lead flux, dissolved in the furnace. The prill is totally digested by HCl and HNO3 acids before Atomic absorption spectroscopy (AAS) determination for gold analysis.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical tools were used to determine any element concentrations.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Certified reference materials (CRMs) are inserted into the sample sequence randomly at a rate of 1 per 20 samples to ensure correct calibration. Any values outside of 3 standard deviations are re-assayed with a new CRM. blanks are inserted into the sample sequence at a rate of 1 per 20 samples. The insertion points are selected at random, except where high grade mineralisation is expected. In these cases, a blank is inserted after the high-grade sample to test for contamination. Results greater than 0.2gpt is received are investigated, and re-assayed if appropriate. New pulps are prepared if anomalous results cannot be resolved. Field Duplicates are taken for all RC samples (1 in 20 sample). No Field duplicates are submitted for diamond core. Umpire sampling programs are undertaken on an ad-hoc basis.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	All significant intersections are verified by another Northern Star geologist during the drill hole validation process, and later by a Competent person to be signed off.
	The use of twinned holes.	No Twinned holes were drilled for this data set.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Geological logging is directly entered into an Acquire database. Assay files are received in csv format and loaded directly into the database by the project's responsible geologist with an Acquire importer object. Hardcopy and electronic copies of these are stored.
	Discuss any adjustment to assay data.	No adjustments are made to this assay data.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Underground diamond hole positions are marked before drilling by mine survey staff and the actual hole collar position located by mine survey staff once drilling is completed. During drilling, single-shot surveys are every 30m to ensure the hole remains close to design. This is performed using the Reflex Ez-Trac system. Upon hole completion, a Gyroscopic survey is conducted by a third-party surveying contractor, taking readings every 5m for improved accuracy. Direction measurements are collected relative to true north. For UG holes multi-shot surveys are taken every 9m when retreating out of the hole.
	Specification of the grid system used.	Data is collected using both local mine grid (Kundana 10) and MGA 94 Zone 51 as appropriate.
	Quality and adequacy of topographic control.	Quality topographic control has been achieved through Lidar data and survey pickups of holes over the last 15 years.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Drill hole spacing varies. Grade control drilling spacing is typically 20m x 20m to provide definition of economic ore shoots. Resource definition drilling spacing is typically 40m x 40m. This allows the Resource to be upgraded to indicated. Inferred Resources typically have a spacing of 80m x 80m. Some exploration holes are spaced up to 200m apart.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The data spacing and distribution is considered sufficient to support the Resource and Reserve estimates.

Criteria	JORC Code explanation	Commentary
	Whether sample compositing has been applied.	Sample data is composited before grade estimation is undertaken. Average intersection grades are reported in ASX and corporate announcements.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	Most of the structures in the Kundana camp dip steeply (80°) to WSW. The Poda structure has a much shallower dip in a similar direction, approximately 60°. To target these orientations the drill hole dips of 60-70° towards ~060° achieve high angle intersections on all structures. Drill holes with low intersection angles will be excluded from Resource estimation where more suitable data is available.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No sampling bias is considered to have been introduced by the drilling orientation.
Sample security	The measures taken to ensure sample security.	Prior to laboratory submission samples are stored by Northern Star Resources in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound, and tracked through their chain of custody and via audit trails.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	No audits or reviews have recently been conducted on sampling techniques.

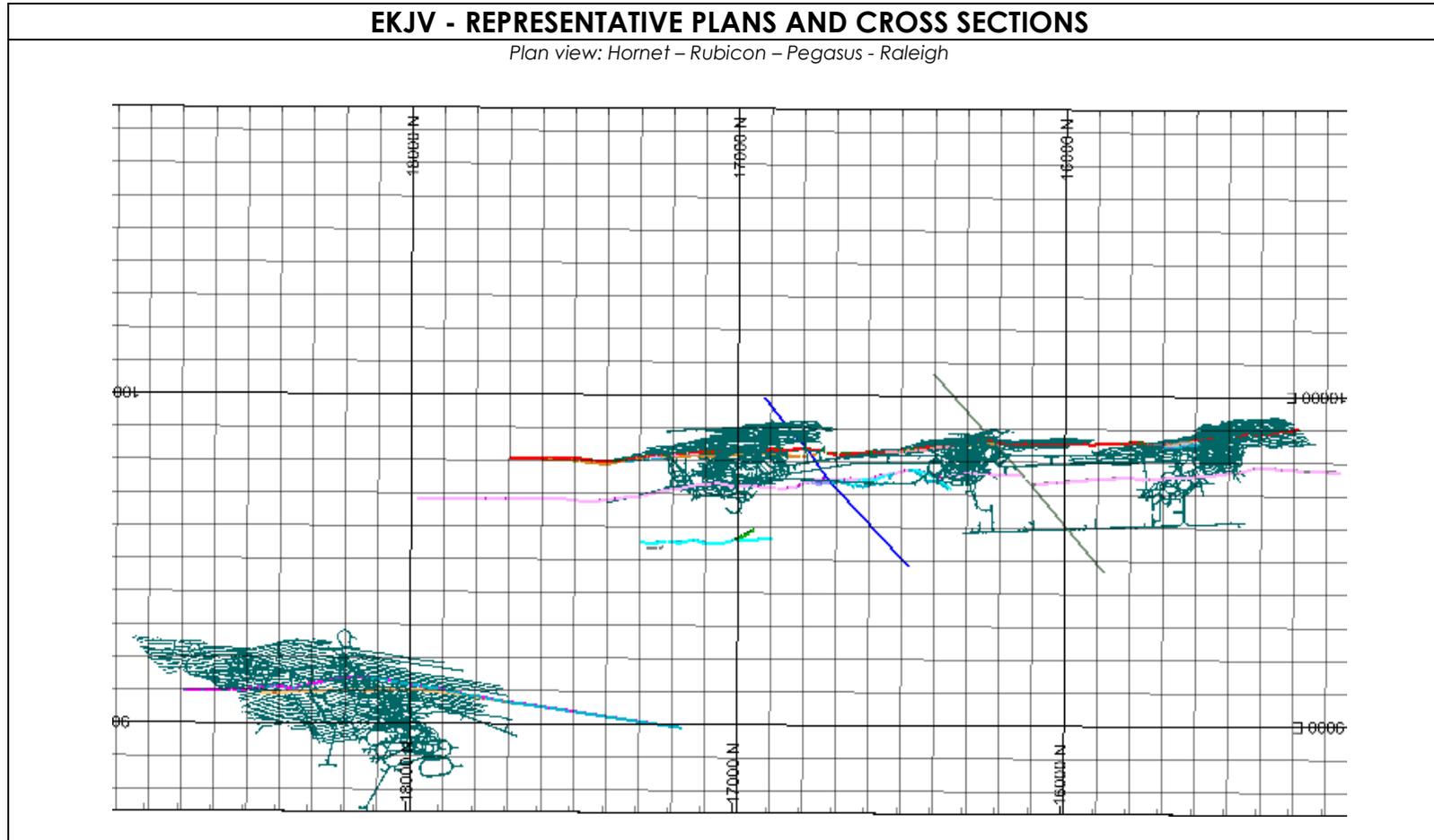
## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	All holes mentioned in this report are located within the M16/309 and M16/326 Mining leases and are held by The East Kundana Joint Venture (EKJV). The EKJV is majority owned and managed by Northern Star Resources Limited (51%). The minority holding in the EKJV is held by Tribune Resources Ltd (36.75%) and Rand Mining Ltd (12.25%). The tenement on which the Rubicon, Hornet and Pegasus deposits are hosted (M16/309) is subject to three royalty agreements. The agreements that are on M16/309 are the Kundana- Hornet Central Royalty, the Lake Grace Royalty and the Kundana Pope John Agreement No. 2602-13. The southern portion of Raleigh is located on M15/993, which is held by the East Kundana joint venture entities. The northern extent of Raleigh is located on M16/157 which is 100% owned by Northern Star Resources.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	No known impediments exist, and the tenements are in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	The first reference to the mineralisation style encountered at the Kundana project was the mines department report on the area produced by Dr. I. Martin (1987). He reviewed work completed in 1983 – 1984 by a company called Southern Resources, who identified two geochemical anomalies, creatively named Kundana #1 and Kundana #2. The Kundana #2 prospect was subdivided into a further two prospects, dubbed K2 and K2A. Between 1987 and 1997, limited work was completed. Between 1997 and 2006 Tern Resources (subsequently Rand Mining and Tribune Resources), and Gilt-edged mining focused on shallow open pit potential which was not considered viable for Pegasus, however the Rubicon open Pit was considered economic and production commenced in 2002. In 2011, Pegasus was highlighted by an operational review team and follow-up drilling was planned through 2012. This report is concerned solely with 2014 drilling that led on from this period.
Geology	Deposit type, geological setting and style of mineralisation.	The Kundana camp is situated within the Norseman-Wiluna Greenstone Belt, in an area dominated by the Zuleika shear zone, which separates the Coolgardie domain from the Ora Banda domain. K2-style mineralisation (Pegasus, Rubicon, Hornet) consists of narrow vein deposits hosted by shear zones located along steeply-dipping overturned lithological contacts. The K2 structure is present along the contact between a black shale unit (Centenary shale) and intermediate volcanoclastics (Spargoville formation). Minor mineralisation, termed K2B, also occurs further west, on the contact between the Victorious basalt and Bent Tree Basalt (both part of the regional upper Basalt Sequence). As well as additional mineralisation including the K2E and K2A veins, Polaris/Rubicon Breccia (Silicified and mineralised Shale) and several other HW lodes adjacent to the main K2 structure.

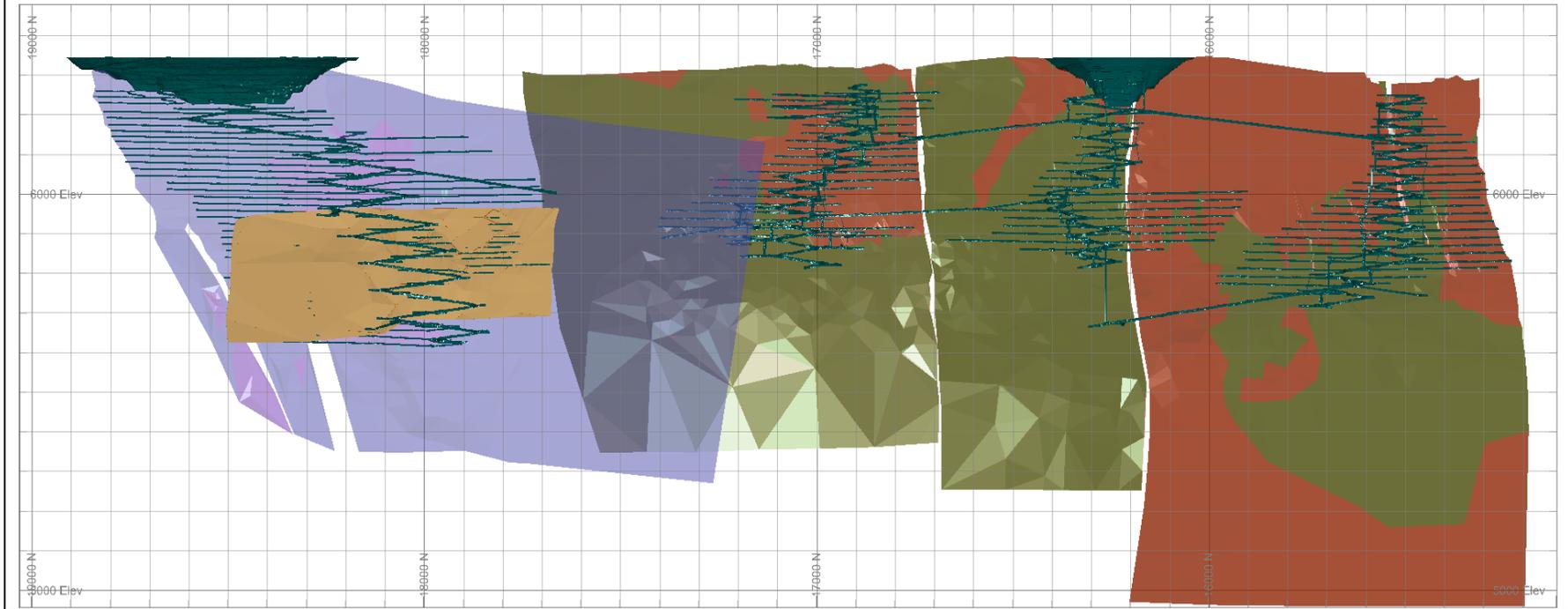
Criteria	JORC Code explanation	Commentary
		A 60° W dipping fault, offsets this contact and exists as a zone of vein-filled brecciated material hosting the Podes-style mineralisation at Pegasus and the Nugget lode at Rubicon. Ambition is interpreted similar in style to the north of Pegasus
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>o easting and northing of the drill hole collar</li> <li>o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>o dip and azimuth of the hole</li> <li>o down hole length and interception depth</li> <li>o hole length.</li> </ul>	All drill holes are listed in the appendix
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Exclusion of the drill information will not detract from the understanding of the report
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	All reported assay results have been length weighted to provide an intersection width. A maximum of 2m of barren material between mineralised samples has been permitted in the calculation of these widths. Typically grades over 1.0gpt are considered significant, however, where low grades are intersected in areas of known mineralisation these will be reported. No top-cutting is applied when reporting intersection results.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.##gpt including ##.#m @ ##.##gpt.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalent values have been used for the reporting of these exploration results.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results:	True widths have been calculated for intersections of the known ore zones, based on existing knowledge of the nature of these structures.
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	The target structure is very planar and its orientation well constrained, allowing very reliable calculations of true widths. True widths have been calculated for all reported intersections.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	Both the downhole width and true width have been clearly specified when used.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Appropriate plans and section have been included in the body of this report.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and 'From' and 'To' depths.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	No other recent material data has been collected.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	Additional drilling is planned with the intention of extending known mineralisation laterally and at depth. Drilling will also be undertaken to improve confidence in previously identified mineralisation and to assist in the location of high grade shoots.

Criteria	JORC Code explanation	Commentary
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Appropriate diagrams accompany this release.



## EKJV - REPRESENTATIVE PLANS AND CROSS SECTIONS

*Long Section: Hornet – Rubicon – Pegasus - Raleigh*



## Kanowna Belle (including Velvet) JORC Code, 2012 Edition – Table 1 Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	The deposit is sampled in majority by diamond drilling (DD) and reverse circulation (RC) drilling. Sample intervals are defined by the geologist to honour geological boundaries.  DD core was orientated, measured and then sampled by cutting the core in half longitudinally using an "Almonte" diamond saw. Cutting was along orientation lines, which are retained in the tray or where orientation lines are absent along cutting lines marked on the pieced core.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	Sample intervals are marked on the core by a geologist typically every 1m or to honour geological boundaries. Sample interval lengths vary from 0.3m to 1.3m (NQ). The same half of the core was selected for each sample interval, placed in numbered calico bags and submitted to the laboratory for analysis. The other half of the core was left in the core tray which was stamped for identification, stored and catalogued. A minor amount of infill or grade control drilling was submitted as whole core.  Due to the refractory nature of the mineralisation there is very little free, coarse gold. It is considered that the half core samples submitted for assay are representative of the ore being sampled.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	Assaying is by fire assay with a 40gm charge and AAS analysis for gold. All sampling data is entered onto logging sheets or a tablet computer and entered into the central Acquire database.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	DD core is mostly NQ with some BQ, HQ and LTK60. Depth of diamond tails are generally 20-30m. Where appropriate diamond core was orientated using a spear, Ballmark™, Ezimark™, or ACE multi electronic tool.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	DD core recovery factors are generally very high with in excess of 95% recovery. RC recovery was also recorded as good to very good. Historic DD core stored onsite shows excellent recovery.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	For DD, the contractors adjust the rate of drilling and method if recovery issues arise. All recovery is recorded by the drillers on core blocks. This is checked and compared to the measurements of the core by the geologist. Any issues are communicated back to the drilling contractor.  Some loss occurred when drilling through fault zones such as the Fitzroy Fault. Areas of potential lower recovery were generally known beforehand and controlled drilling techniques were employed to maximise recovery.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	There is no known relationship between recovery and grade.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	All DD core was logged by geologists with lithology, mineralisation, structure, alteration, veining and specific gravity recorded. Quantitative measures such as structural measurements, intensity of alteration, percentage of mineralisation, thickness of veins and veins per metre were also recorded. Geotechnical measurements on DD core include RQD, Recovery, and Fracture Frequency. For selected holes joint sets, infill, infill thickness and roughness were also geotechnically measured. Photographs are taken of each core tray when wet. All mineralised intersections are logged and sampled.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	Logging is qualitative and all core is photographed. Visual estimates are made for mineralisation percentages for core.
	The total length and percentage of the relevant intersections logged.	100% of the drill core is logged.
	If core, whether cut or sawn and whether quarter, half or all core taken.	DD core is sampled from sawn, half-core on intervals controlled by geological domaining represented by mineralisation, alteration and lithology. Most grade control holes were full core sampled. Mineralised intersections

Criteria	JORC Code explanation	Commentary
Sub-sampling techniques and sample preparation		are sampled with a maximum and minimum length of 1.3m and 0.3m, respecting lithological or alteration contacts. The down hole depth of all sample interval extents are recorded.
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	Exploration update consisting of core results only.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The sample preparation is considered appropriate.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Most holes have the majority of intervals sampled.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Quarter core sampling is sometimes undertaken as a check, however routine field duplicates are not performed on diamond core as these are not considered to be true duplicates.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	Grind checks are performed at both the crushing stage (3mm) and pulverising stage (75µm) requiring 90% of material to pass through the relevant size.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	All samples are prepared and assayed at commercial laboratories. Entire samples are crushed/pulverised to 95% minus 75µ, splitting off 200g and preparing a 40g charge for fire assay with an atomic absorption finish (FA/AA) for Au, LECO for S and inductively coupled plasma (ICP) for As and other multi-elements. Monthly QAQC reports are prepared to check for any bias or trends with conclusions discussed with the laboratory management.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical tools were used to determine any element concentrations.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Sampling and assaying QAQC procedures include: Periodical resubmission of samples to primary and secondary laboratories. Submittal of independent certified reference material. Sieve testing to check grind size. Sample recovery checks. Unannounced laboratory inspections. Standard control samples and blanks purchased from certified commercial suppliers are inserted at a ratio of 1:20. The standard control samples are changed on a 3-month rotation. The results are reviewed on a per batch basis and batches of samples are re-analysed if the result is greater than three standard deviations from the expected result. Any result outside of two standard deviations is flagged for investigation by a geologist and may also be re-assayed. Primary laboratory Bureau Veritas meets ISO 9001:2000.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	All significant intersections are verified by another Northern Star geologist during the drill hole validation process, and later by a Competent Person to be signed off.
	The use of twinned holes.	No twinned holes were drilled for this data set.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	All assay data adheres to Kanowna QAQC standards and is further validated by a qualified person before it can be used in the Resource estimation process. All data is stored in the site Acquire database. Assay files are received in csv and pdf format and are loaded directly into the database by the supervising geologist who then checks that the results have inserted correctly. Electronic copies of these are also kept.
	Discuss any adjustment to assay data.	Below detection limit assays are replaced with 0.005
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	All collar positions were surveyed. All recent DD holes were surveyed down hole by various methods including single shot down hole camera and in-rod non - magnetic survey tools. Holes are typically surveyed at 30m intervals down hole. Since the 1 <sup>st</sup> of June 2015, a true north seeking gyroscopic tool has been used to line up the rig and record a zero-meter survey.

Criteria	JORC Code explanation	Commentary
		Any poor surveys are re-surveyed and in some cases holes have been gyroscope surveyed for non-magnetic affected surveys. Drill hole collars are located by the underground mine surveyors using a laser system respective to the local mine grid and to the overall property in UTM or Australian grid coordinates
	Specification of the grid system used.	A local grid system (KBMine grid) is used. It is rotated anticlockwise 28.43 degrees to the MGA94 grid.
	Quality and adequacy of topographic control.	Topographic control is not relevant to the underground mine.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Drill hole spacing is nominally 40m x 40m down to a nominal 20m x 20m in the main zones of mineralisation at Kanowna. Secondary mineralised structures in the hanging wall and footwall are typically narrower and less consistent so have a nominal drill spacing of 15m x 15m. The spacing of 20x20m and 15x15m in conjunction with geological continuity and confidence is used to assign classifications of indicated in the resource estimation model. Samples have been composited to 1m, which is the dominant sample length, prior to estimation.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The data spacing is considered appropriate.
	Whether sample compositing has been applied.	No compositing has been applied to these exploration results, although composite intersections are reported.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	The majority of drilled data is perpendicular to the interpreted strike of the Kanowna orebodies where possible.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	Holes with orientations that are considered likely to introduce sampling bias are excluded from the estimation during the validation process.
Sample security	The measures taken to ensure sample security.	All core is kept within the site perimeter fence on the Mining Lease M27/103. Samples are dispatched and/or collected by an offsite delivery service on a regular basis. Each sample batch is accompanied with a <ul style="list-style-type: none"> <li>• Job number.</li> <li>• Number of samples.</li> <li>• Sample Numbers (including standards and duplicates).</li> <li>• Required analytical methods.</li> <li>• A job priority rating.</li> </ul> A chain of custody is demonstrated by both Company and Bureau Veritas in the delivery and receipt of sample materials. Any damage to or loss of samples within each batch (e.g. total loss, spillage or obvious contamination), is reported to the Company in the form of a list of samples affected and detailing the nature of the problem(s).
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	The last external audit was conducted in 2009 with the conclusion that industry best practice was being followed. Standards and procedures have remained largely unchanged since this time. A review of sampling techniques, assay results and data usage was conducted internally by the Companies' Principal Geologist during the model peer review process with no material issues.

## Section 2 Reporting of Exploration Results

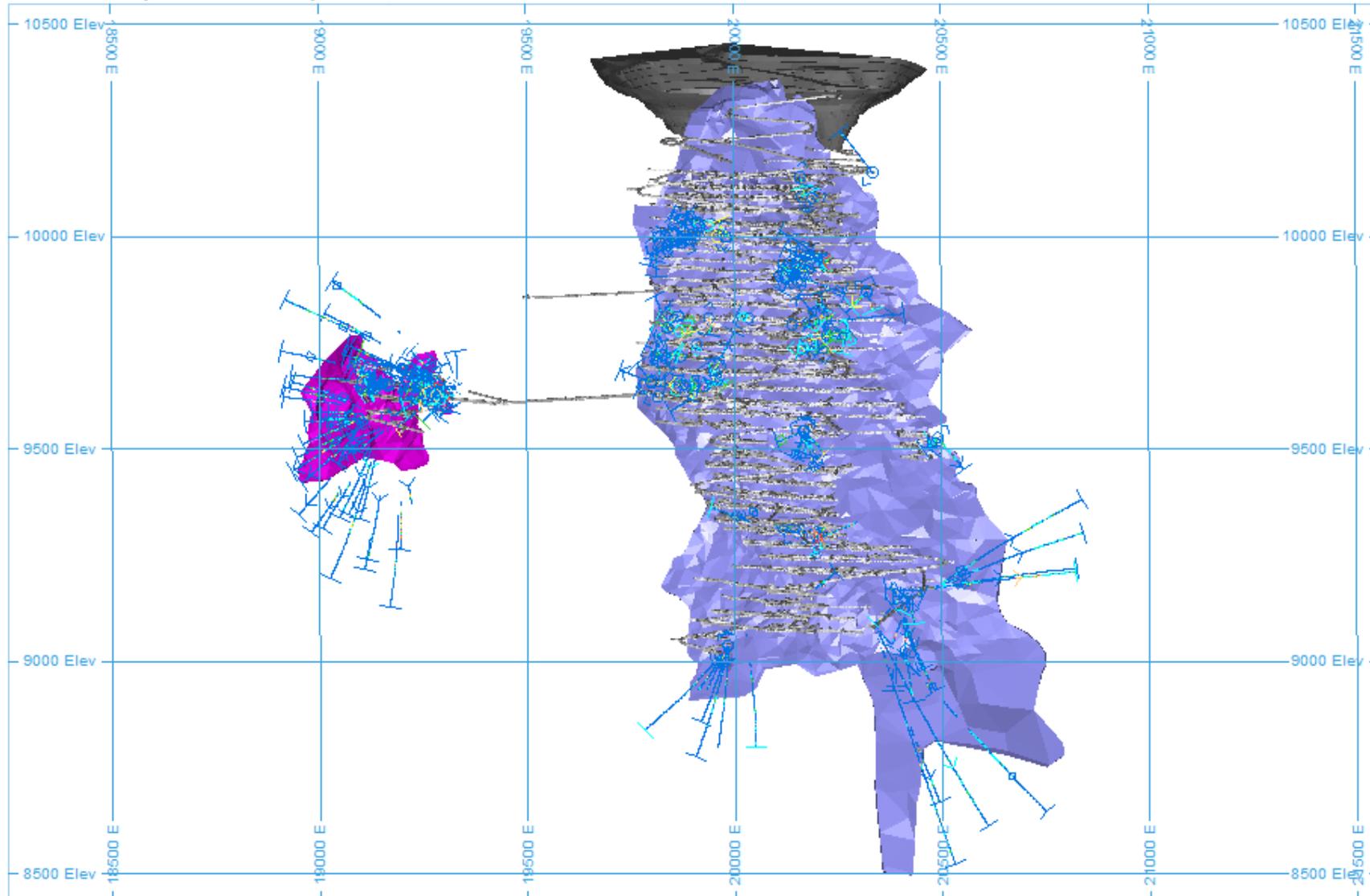
(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Kanowna Belle mine and associated infrastructure is located on Mining Leases M27/92 and M27/103. Mining lease M27/92 (972.65 ha) was granted on March 14 1988 and M27/103 (944.25 ha) was granted on January 12 1989. Both leases were granted for periods of 21 years after which they can be renewed for a further 21 years. The Mining Leases and most of the surrounding tenement holdings are 100% owned by Northern Star (Kanowna) Pty Limited, a wholly owned subsidiary of Northern Star Resources Limited. The mining tenements are either located on vacant crown land or on pastoral leases.  The leases containing the deposit are pre-1994 leases so are not subject to Native Title claims.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	No known impediments exist and the tenements are in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	Kanowna was discovered in 1989 by Delta Gold, open pit mining commenced between 1993 and 1998 resulting in a 220m deep pit. Underground operation began in 1998. In 2002, Delta Gold Limited and Goldfields Limited merged to form Aurion Gold Limited and Placer Dome Inc. (Placer Dome) subsequently acquired Aurion Gold Limited. In 2006 Barrick Gold Corporation acquired Placer Dome and in 2014 Northern Star acquired the operation from Barrick.  Exploration drilling is ongoing from underground to extend the known mineral Resources.
Geology	Deposit type, geological setting and style of mineralisation.	Kanowna Belle is located within the Kalgoorlie Terrane, one of a number of elongate, broadly NNW-SSE striking structural-stratigraphic late Archaean greenstone terranes of the Eastern Goldfields of Western Australia. The Kanowna Belle gold mine is located close to the centre of the NNW-SSE trending, greenstone-dominated Boorara Domain, the eastern most subdivision of the Kalgoorlie Terrane.  The Kanowna Belle deposit can be categorised as a refractory, Archean lode-gold type deposit. The orebody is comprised of several ore shoots, including the large Lowes Shoot, and several smaller lodes including Troy, Hilder, Hangingwall and Footwall shoots controlled by sets of structures of various orientations oblique to Lowes.  Lowes contains some 80% of known gold mineralisation and strikes ENE, dips steeply SSW and plunges steeply SW. Lowes Shoot has a strike length of 500m, width of 5m to 50m and down-plunge extent greater than 1,250m. The overall steep SE plunge is interpreted to reflect the intersection of D1 (ENE) and D2 (NW) structures.  Kanowna Belle is one of the only known refractory pyritic orebodies in the Yilgarn Craton. Gold in the Kanowna Belle deposit occurs mostly as fine-grained (<10 µm) inclusions in pyrite or as very fine-grained gold located in arsenic-rich growth zones in pyrite. Typical ore assemblages contain 0.5% S to 1.5% S and 40 ppm As.  The Kanowna Belle deposit is hosted by sedimentary volcanoclastic and conglomeratic rocks which are separated into hangingwall and footwall sequences by a major, steeply SSE dipping zone of structural disruption. This structure represents the product of at least three distinct stages of deformation, comprising the Fitzroy Mylonite, the Fitzroy Shear Zone and the Fitzroy Fault, which have produced clear structural overprinting relations. Importantly, this structure has localised emplacement of the Kanowna Belle porphyry which hosts at least 70% of known mineralisation. Localisation of high grade mineralisation and most intense alteration around the composite structure emphasises its importance for acting as the major plumbing system for fluids.  Formation of the Fitzroy Mylonite and Fitzroy Shear Zone are interpreted to have occurred during regional south-to-north D1 thrusting. A switch in far-field stress axes to the approximately ENE-WSW D2 orientation caused reactivation of the Fitzroy Shear Zone, resulting in sigmoidal folding of pre-existing structures and formation of a shallow lineation associated with sinistral transcurrent shearing. The Kanowna Belle porphyry cross-cuts fabrics associated with the D1 Fitzroy Mylonite and Fitzroy Shear Zone and is in turn overprinted by S2.
Drill hole information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>o easting and northing of the drill hole collar</li> <li>o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>o dip and azimuth of the hole</li> <li>o down hole length and interception depth</li> <li>o hole length.</li> </ul>	Full details for reported holes are part of this release.

Criteria	JORC Code explanation	Commentary
	If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Exclusion of the drill information will not detract from the understanding of the report.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	All reported assay results have been length weighted to provide an intersection width. A maximum of 2m of barren material between mineralised samples has been permitted in the calculation of these widths.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	No assay results have been top-cut for the purpose of this report. A lower cut-off of 1gpt has been used to identify significant results, although lower results are included where a known ore zone has been intercepted and the entire intercept is low grade.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalent values have been used for the reporting of these exploration results.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results:	True widths have been calculated for intersections of the known ore zones, based on existing knowledge of the nature of these structures.
	If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	Both the downhole width and true width have been clearly specified when used.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	Where mineralisation orientations are not known, downhole lengths are reported.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Appropriate plans and section have been included in this report.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and 'From' and 'To' depths.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	Nil.
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).	<u>KB Resource</u> : Further mine planning work is planned for the area of the Mineral Resource model. The down dip extension of the KB Mineral Resource will be drill tested from the 9245 Exploration drive. <u>Velvet</u> : Because of the difficulty in targeting the mineralisation from current development, an exploration decline has been completed to better asses the mineralisation.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Shown in the release.

## Overview diagrams

Long section: Looking north, drilling completed in Lowes and Velvet from Kanowna Belle with the main mineralisation domains.



## Carbine-Paradigm Exploration Results – February 2018 JORC Code, 2012 Edition – Table 1 Report Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.	Sampling was completed using a combination of surface Reverse circulation (RC) and Diamond Drilling (DD). DD samples are generally HQ2 core with sample intervals defined by the geologist to honour geological boundaries ranging from 0.2 to 1.0m in length.  RC samples are collected via rig-mounted static cone splitter with sample falling through a riffle splitter or inverted cone splitter, splitting the sample in 88%/9%/3% ratio. 9% split retained for 1m composites and 3% split retained for 4m composites.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	RC samples were split using a rig-mounted cone splitter on 1m intervals to obtain a sample for assay.  Diamond core was placed in core trays for logging and sampling. Half core samples were nominated by the geologist from diamond core with a minimum sample width of either 20cm (HQ) or 30cm (NQ2).
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	RC sampling was split using a rig mounted cone splitter to deliver a sample of approximately 3Kg  DD drill core was cut in half using an automated core saw, where the mass of material collected will vary on the hole diameter and sampling interval.  All samples were delivered to a commercial laboratory where they were dried, crushed to 95% passing 3mm if required, at this point large samples may be split using a rotary splitter, pulverisation to 95% passing 75µm, a 50g charge was selected for fire assay.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Both RC and Diamond Drilling techniques were used at the Paradigm project.  2017 drill holes have been HQ2 from surface.  Core was orientated using the Reflex ACT Core orientation system.  RC Drilling was completed using a 5.75" drill bit, downsized to 5.25" at depth.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	Moisture content and sample recovery is recorded for each RC sample.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	RC drilling contractors adjust their drilling approach to specific conditions to maximize sample recovery. No recovery issues were identified during the 2017 RC drilling. Recovery was poor at the very beginning of each hole, as is normal for this type of drilling in overburden.  For diamond drilling, the contractors adjust their rate of drilling and method if recovery issues arise. All recovery is recorded by the drillers on core blocks, some recovery issues were encountered in the regolith. This is checked and compared to the measurements of the core by the geological team. Any issues are communicated back to the drilling contractor.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	No relationship or bias has identified between grade and sample recovery.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.	All diamond core is logged for Regolith, Lithology, veining, alteration, mineralisation and structure. Structural measurements of specific features are also taken through oriented zones.  RC sample chips are logged in 1m intervals for the entire length of each hole. Regolith, lithology, alteration, veining and mineralisation are all recorded.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	All logging is quantitative where possible and qualitative elsewhere. A photograph is taken of every core tray.
	The total length and percentage of the relevant intersections logged.	In all instances, the entire drill hole is logged.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken.	Diamond core is cut using an automated core saw. In most cases, half the core is taken for sampling with the remaining half being stored for later reference.

Criteria	JORC Code explanation	Commentary
	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	All RC samples are split using a rig-mounted cone splitter to collect a 1m sample 3-4kg in size. All samples were intended and assumed to be dry, moisture content was recorded for every sample.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	Preparation of NSR samples was conducted at MinAnalytical preparation facilities, commencing with sorting, checking and drying at less than 110°C to prevent sulphide breakdown. Samples are jaw crushed to a nominal - 6mm particle size. If the sample is greater than 3kg a Boyd crusher with rotary splitter is used to reduce the sample size to less than 3kg (typically 1.5kg) at a nominal <3mm particle size.  The entire crushed sample (if less than 3kg) or sub-sample is then pulverized to 90% passing 75µm, using a Labtechnics LM5 bowl pulveriser. 300g Pulp subsamples are then taken with an aluminium scoop and stored in labelled pulp packets.  The sample preparation is considered appropriate for the deposit.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Procedures are utilised to guide the selection of sample material in the field. Standard procedures are used for all process within the laboratory. Grind checks are performed at both the crushing stage(3mm) and pulverising stage (75µm), requiring 90% of material to pass through the relevant size.
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate / second-half sampling.	Field duplicates were taken for RC samples on a ratio of 1 in 20.  Umpire sampling programs are carried out on an ad-hoc basis.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	The sample sizes are considered appropriate for the material being sampled.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.	A 40gm FIRE assay charge is used with a lead flux in the furnace. The prill is totally digested by HCl and HNO <sub>3</sub> acids before Atomic Absorption Spectroscopy (AAS) determination for gold analysis.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical tools were used to determine any element concentrations.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Certified reference materials (CRMs) are inserted into the sample sequence randomly at a rate of 1 per 20 samples to ensure correct calibration. Any values outside of 3 standard deviations are re-assayed with a new CRM.  blanks are inserted into the sample sequence at a rate of 1 per 20 samples. The insertion points are selected at random, except where high grade mineralisation is expected. In these cases, a Blank is inserted after the high-grade sample to test for contamination. Results greater than 0.2gpt if received are investigated, and re-assayed if appropriate. New pulps are prepared if anomalous results cannot be resolved.  Barren flushes are regularly inserted after anticipated high gold grades at the pulverising stage.  Field Duplicates are taken for all RC samples and submitted for analysis based on a range of primary assay results skewed towards anomalous gold grades. No Field duplicates are submitted for diamond core.  No bias has been established using these procedures.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel.	All significant intersections are verified by another Northern Star geologist during the drill hole validation process, and later by a Competent person to be signed off.
	The use of twinned holes.	No Twinned holes were drilled for this data set.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Geological logging is directly entered into an Acquire database. Assay files are received in csv format and loaded directly into the database by the project's responsible geologist with an Acquire importer object. Hardcopy and electronic copies of these are stored.
	Discuss any adjustment to assay data.	No adjustments are made to this assay data.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	A planned hole is pegged using a Differential GPS by the field assistants.  The final collar is picked up after hole completion by Cardno Survey with a Differential GPS in the MGA 94_51 grid.  During drilling single-shot surveys are every 30m to ensure the hole remains close to design. This is performed using the Reflex Ez-Trac system which measures the gravitational dip and magnetic azimuth results are uploaded directly from the Reflex software export into the Acquire database.
	Specification of the grid system used.	Collar coordinates are recorded in MGA94 Zone 51.

Criteria	JORC Code explanation	Commentary
	Quality and adequacy of topographic control.	The Differential GPS returns reliable elevation data which has been confirmed against a high resolution Digital Terrain Model survey performed by Arvista in 2015.
Data spacing and distribution	Data spacing for reporting of Exploration Results.	Drill hole spacing across the area varies from approximately 40m to 100m spacing.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Resource definition drilling spacing was typically 40m x 40m, to allow the Resource to be upgraded to indicated. Surrounding exploration drilling can be spaced up to 200m apart.
	Whether sample compositing has been applied.	Sample data is composited before grade estimation is undertaken.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	The orientation of the historically mined ore bodies is well known and suggests drilling direction is perpendicular to the orientation of mineralisation. The unexploited ore body has been extensively drilled, confirming a perpendicular drill direction.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No sampling bias is considered to have been introduced by the drilling orientation.
Sample security	The measures taken to ensure sample security.	Prior to laboratory submission samples are stored by Northern Star Resources in a secure yard. Once submitted to the laboratories they are stored in a secure fenced compound, and tracked through their chain of custody and via audit trails.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	No audits have been undertaken for the drill holes at this stage.

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	All drilling related to the Paradigm Prospect in this report are located within Mining Lease M16/548 which is owned by Kundana Gold Pty Ltd, a wholly owned subsidiary of Northern Star Resources. There are no private royalty agreements applicable to this tenement.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	No known impediments exist and the tenements are in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	The Carbine - Paradigm area has been explored since the late 1800's. Numerous companies, including BHP, Newcrest, Centaur Mining, Goldfields Exploration, Placer Dome and Barrick have been active in the area. The Paradigm deposit was discovered by Goldfields Exploration via aircore drilling in the late 1990's.
Geology	Deposit type, geological setting and style of mineralisation.	<p>The Carbine area is northern extension of the regionally significant Zuleika Shear Zone. The tenements are in the Norseman-Wiluna Archaean greenstone belt in the Eastern Goldfields province of the Yilgarn Craton, Western Australia.</p> <p>Gold mineralisation in the Zuleika Shear Zone and adjacent greenstone sequences occurs in all rock types, although historical and recent production is dominated by two predominant styles:</p> <p>Brittle D2 faults with laminated (multiple crack-seal) quartz veining containing gold and trace base metal sulphides (galena, sphalerite, chalcopyrite, scheelite).</p> <p>Brittle quartz vein stockwork developed within granophyric gabbro within the Powder Sill</p> <p>At the Paradigm deposit, gold is hosted in veins and disseminated sulphides associated with shearing along the large scale Lincancunbur fault and adjacent fine grained stratigraphic horizons</p>
Drill hole Information	<p>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:</p> <ul style="list-style-type: none"> <li>o easting and northing of the drill hole collar</li> <li>o elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> </ul>	All drill holes are listed in the Appendix

Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>o dip and azimuth of the hole</li> <li>o down hole length and interception depth</li> <li>o hole length.</li> </ul> <p>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</p>	Exclusion of the drill information will not detract from the understanding of the report.
Data aggregation methods	<p>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.</p> <p>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</p> <p>The assumptions used for any reporting of metal equivalent values should be clearly stated.</p>	<p>All reported assay results have been length weighted to provide an intersection width. A maximum of 2m of barren material between mineralised samples has been permitted in the calculation of these widths. Typically grades over 1.0gpt are considered significant, however, where low grades are intersected in areas of known mineralisation these will be reported. No top-cutting is applied when reporting intersection results.</p> <p>Where an intersection incorporates short lengths of high grade results these intersections will be reported in addition to the aggregate value. These will typically take the form of ##.#m @ ##.##gpt including ##.#m @ ##.##gpt.</p> <p>No metal equivalent values have been used for the reporting of these exploration results.</p>
Relationship between mineralisation widths and intercept lengths	<p>These relationships are particularly important in the reporting of Exploration Results:</p> <p>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</p> <p>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').</p>	<p>True widths have been calculated for intersections of the known ore zones, based on existing knowledge of the nature of these structures.</p> <p>Both the downhole width and true width have been clearly specified when used.</p> <p>Denoted in the drill results table where applicable.</p>
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Appropriate plans and section have been included in the body of this report.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced avoiding misleading reporting of Exploration Results.	Both high and low grades have been reported accurately, clearly identified with the drill hole attributes and 'From' and 'To' depths.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	No other material exploration data has been collected for this area.
Further work	<p>The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).</p> <p>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</p>	<p>Further drilling is planned to target extensions.</p> <p>Appropriate diagrams accompany this release.</p>

## PARADIGM DEPOSIT - REPRESENTATIVE PLAN AND CROSS SECTION

