



31 October 2022

**ASX:AUN**

## ABOUT AURUMIN

Aurumin Limited (ACN 639 427 099) is an Australian exploration company with advanced projects.

## AURUMIN BOARD

**Piers Lewis**

Non Executive Chairman

**Brad Valiukas**

Managing Director

**Shaun Day**

Non Executive Director

**Darren Holden**

Non Executive Director

## CAPITAL STRUCTURE

155.3 million shares

17.8 million listed options

34.5 million unlisted options

## PROJECTS

Central Sandstone

Mt Dimer

Mt Palmer

Johnson Range

Karramindie

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## CENTRAL SANDSTONE RESOURCE UPDATE

# SANDSTONE OPERATIONS RESOURCE INCREASED TO 946koz @ 1.5g/t Au (INCLUDES JOHNSON RANGE)

## COMBINED SHILLINGTON AND TWO MILE HILL OPEN PIT RESOURCES INCREASED TO 181koz @ 1.4g/t Au

## TWO MILE HILL UG RESOURCE INCREASED TO 574koz @ 1.6g/t Au

**Aurumin Limited (ASX: AUN)** ("Aurumin" or "the Company") is pleased to announce an updated **JORC-2012 compliant Mineral Resource Estimate (MRE)** for the Shillington and Two Mile Hill Deposits at its 100% owned Central Sandstone Gold Project.

The Central Sandstone Gold Project is located 12km south of the township of Sandstone, 550km northeast of Perth, and located on a sealed highway between the mining towns of Mt Magnet and Leinster in the East Murchison Mineral Field of Western Australia.

The MRE for the Two Mile Hill and Shillington deposits in the Central Sandstone Project has been updated, incorporating results from Aurumin's recently completed reverse circulation (RC) and diamond (DD) drilling campaign of nine RC holes at Shillington (1245m) and four DD holes at Two Mile Hill (2662m). Drilling was completed in July 2022, with final assay results received in September 2022.

### Aurumin's Managing Director, Brad Valiukas, commented:

*"We have been maintaining a dual focussed approach since acquiring the Central Sandstone Project, to both optimise existing resources and identify new resources. We continue to see the Two Mile Hill underground deposit as a key part of the project going forward, with the scale to potentially underpin future production, and this has focussed our optimisation efforts."*

*"This resource update is an important step in progressing the Project, and is in line with the potential identified when the Sandstone assets were acquired. The increase in grade to 1.6g/t for the Two Mile Hill Underground MRE, up from 1.1g/t, is a result of Aurumin's recent infill and extensional drilling, delivering improved data density, grades and geological understanding."*

*"This resource model at Two Mile Hill has generally tightened up the lateral extents, and there remain portions of the tonalite host to be tested with further potential upside. We will now undertake some scoping-level work on the deposit."*

*"The next drill programme at Sandstone will focus on the current geochemical and structural targets, with plans and PoWs currently being finalised, to further advance the new targets that we have. Soil sampling work continues to progress in the background, and we expect to release the first results from tenement E57/1140 during November."*

## UPDATED RESOURCE TABLE

The Shillington Mineral Resource has been reported at a cut-off grade of 0.5g/t Au and within 140m of natural ground surface. The Mineral Resource has been classified as containing both Indicated and Inferred material.

The Two Mile Hill Open Pit Resource is reported at a cut-off grade of 0.5g/t Au above 370m RL (or within 150m of the natural ground surface). The Two Mile Hill Underground Resource has been reported at a cut-off grade of 0.73g/t below 370m RL (150m below natural surface) to -40mRL (or to a depth of 560m below natural ground surface).

Table 1 – Updated Sandstone Operations Resources Table – with updates highlighted

| <b>Sandstone Operations Resources</b>  |                        |                           |                    |                        |                           |                    |                        |                           |                    |
|--|------------------------|---------------------------|--------------------|------------------------|---------------------------|--------------------|------------------------|---------------------------|--------------------|
| <b>Deposit</b>   | <b>Indicated</b>       |                           |                    | <b>Inferred</b>        |                           |                    | <b>Total</b>           |                           |                    |
|  | <b>Tonnes<br/>(kt)</b> | <b>Grade<br/>(g/t Au)</b> | <b>Au<br/>(oz)</b> | <b>Tonnes<br/>(kt)</b> | <b>Grade<br/>(g/t Au)</b> | <b>Au<br/>(oz)</b> | <b>Tonnes<br/>(kt)</b> | <b>Grade<br/>(g/t Au)</b> | <b>Au<br/>(oz)</b> |
| <b>Central Sandstone*</b>  |                        |                           |                    |                        |                           |                    |                        |                           |                    |
| <b>Sandstone Open Pit Deposits – Summary Mineral Resource Estimates (2012 JORC Code) at 0.5g/t cut-off</b>     |                        |                           |                    |                        |                           |                    |                        |                           |                    |
| Two Mile Hill  | 1738                   | 1.3                       | 71,700             | 378                    | 1.5                       | 18,200             | 2116                   | 1.3                       | 89,900             |
| Shillington  | 1300                   | 1.5                       | 60,800             | 613                    | 1.5                       | 29,800             | 1913                   | 1.5                       | 90,600             |
| Wirraminna   | 300                    | 1.3                       | 12,100             | 280                    | 1.1                       | 9,700              | 580                    | 1.2                       | 21,800             |
| Old Town Well  | 282                    | 1.0                       | 8,800              | 68                     | 0.6                       | 1,400              | 351                    | 0.9                       | 10,100             |
| Plum Pudding   | 384                    | 1.1                       | 13,100             | 35                     | 0.9                       | 1,000              | 419                    | 1.1                       | 14,100             |
| Eureka   | 340                    | 0.9                       | 9,700              | 221                    | 0.9                       | 6,500              | 561                    | 0.9                       | 16,200             |
| Twin Shafts  | 149                    | 1.0                       | 4,700              | 37                     | 0.7                       | 900                | 186                    | 0.9                       | 5,600              |
| Goat Farm  |                        |                           |                    | 398                    | 1.0                       | 13,200             | 398                    | 1.0                       | 13,200             |
| McIntyre   | 496                    | 1.2                       | 19,400             | 67                     | 0.9                       | 1,900              | 562                    | 1.2                       | 21,300             |
| Ridge  | 173                    | 1.2                       | 6,700              | 67                     | 1.9                       | 4,000              | 240                    | 1.4                       | 10,700             |
| McClaren   | 236                    | 1.4                       | 10,600             | 60                     | 1.7                       | 3,200              | 296                    | 1.5                       | 13,800             |
| <b>Open Pit Subtotal</b>   | <b>5,398</b>           | <b>1.3</b>                | <b>217,600</b>     | <b>2,223</b>           | <b>1.3</b>                | <b>89,800</b>      | <b>7622</b>            | <b>1.3</b>                | <b>307,400</b>     |
| <b>Sandstone Underground Deposits – Summary Mineral Resource Estimates (2012 JORC Code) at 0.73g/t cut-off</b> |                        |                           |                    |                        |                           |                    |                        |                           |                    |
| Two Mile Hill Underground – Tonalite   |                        |                           |                    | 10,676                 | 1.6                       | 554,100            | 10,676                 | 1.6                       | 554,100            |
| Two Mile Hill Underground – BIF  | 48                     | 6.8                       | 10,400             | 105                    | 2.8                       | 9,400              | 153                    | 2.8                       | 19,800             |
| <b>Underground Subtotal</b>  | <b>48</b>              | <b>6.8</b>                | <b>10,400</b>      | <b>10,782</b>          | <b>1.6</b>                | <b>563,500</b>     | <b>10,829</b>          | <b>1.6</b>                | <b>573,900</b>     |
| <b>Central Sandstone Total</b>   | <b>5,446</b>           | <b>1.3</b>                | <b>228,000</b>     | <b>13,005</b>          | <b>1.6</b>                | <b>653,300</b>     | <b>18,451</b>          | <b>1.5</b>                | <b>881,300</b>     |
| <b>Johnson Range^</b>  |                        |                           |                    |                        |                           |                    |                        |                           |                    |
| <b>Johnson Range Open Pit Deposits – Summary Mineral Resource Estimates (2012 JORC Code) at 1.0g/t cut-off</b> |                        |                           |                    |                        |                           |                    |                        |                           |                    |
| Gwendolyn  |                        |                           |                    | 803                    | 2.51                      | 64,700             | 803                    | 2.51                      | 64,700             |
| <b>Sandstone Operations Total</b>  | <b>5,446</b>           | <b>1.3</b>                | <b>228,000</b>     | <b>13,808</b>          | <b>1.6</b>                | <b>718,100</b>     | <b>37,705</b>          | <b>1.5</b>                | <b>946,000</b>     |

\*Data has been rounded to the nearest 1,000 tonnes, 0.1g/t and 100 ounces. Rounding variations may occur.

^Data has been rounded to the nearest 1,000 tonnes, 0.01g/t and 100 ounces. Rounding variations may occur.

## **SHILLINGTON – TWO MILE HILL GEOLOGICAL COMPLEX**

Shillington and Two Mile Hill have been modelled as separate zones within a single geological complex (see Figure 1). The precise timing of, and the relationship between, the mineralising events at Two Mile Hill and Shillington remains unresolved; however, the deposits share stratigraphy and structural linkages, and evidence suggests that shared mineralisation and controls on mineralisation impact both deposits.

The Two Mile Hill -Shillington complex includes a late-stage, near vertical, intrusive tonalite stock, which cuts a local stratigraphy of mafic volcanics and Banded Iron Formation (BIF). Gold mineralisation is developed in the tonalite, the enveloping pillow and komatiitic basalts, the BIF and the overlying laterite.

At Two Mile Hill the majority of mineralisation is hosted within the tonalite body, with sub-horizontal to shallow dipping sheeted quartz veins forming broad, gradational packages of mineralisation. Gold mineralisation within the basalts is accompanied by silica-sericite-carbonate-pyrite alteration.

At Two Mile Hill, the BIF hosted mineralisation occurs adjacent to the contact between the tonalite and the BIF unit, hosting localised high-grade mineralisation. The structure hosting the tonalite is interpreted to project through the Shillington BIF sequence and may have acted as a structural focus for the mineralisation within the Shillington system, highlighting the potential for mineralised positions linking the two adjacent deposits.

The Shillington open pit is located approximately 400m to the south of the Two Mile Hill deposit and historical open pit. Gold mineralisation is associated with zones of brecciation and quartz veining within a series of stacked, northwest trending and shallow northeast dipping banded iron formation (BIF) units, known as the Shillington BIF package.

At Shillington, the BIF hosting mineralisation comprises an upper and middle unit and is about 45m thick, thought to be tapering to 25m thick towards the Two Mile Hill tonalite contact. Mineralisation occurs as semi-continuous lenses within the Shillington BIF package.

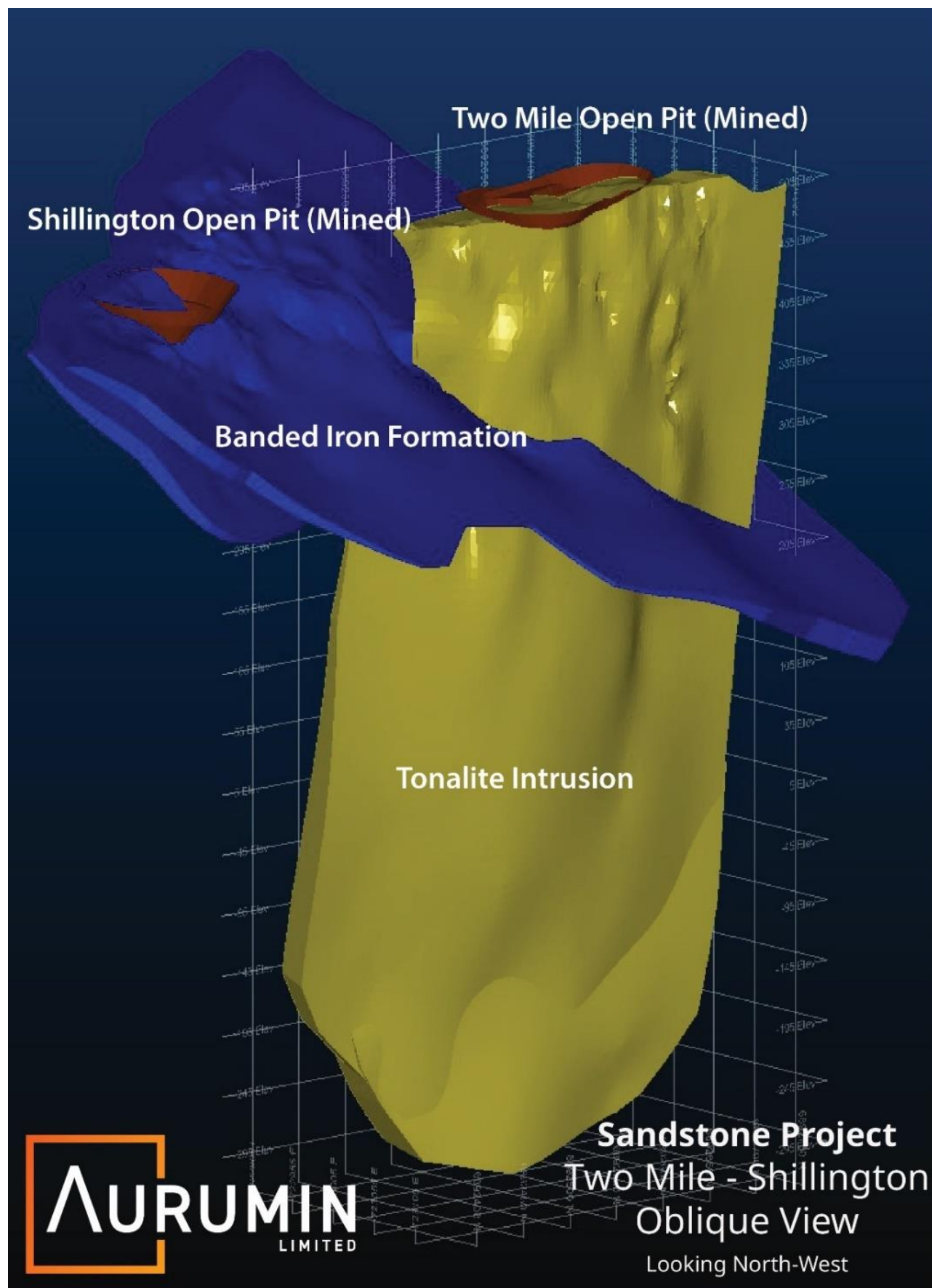


Figure 1 – Oblique view toward the North-west showing major geological units within the Shillington- Two Mile hill complex. The blue wireframe is the Banded Iron Formation unit and the yellow wireframe is the tonalite intrusion.



## RESOURCE IMAGES

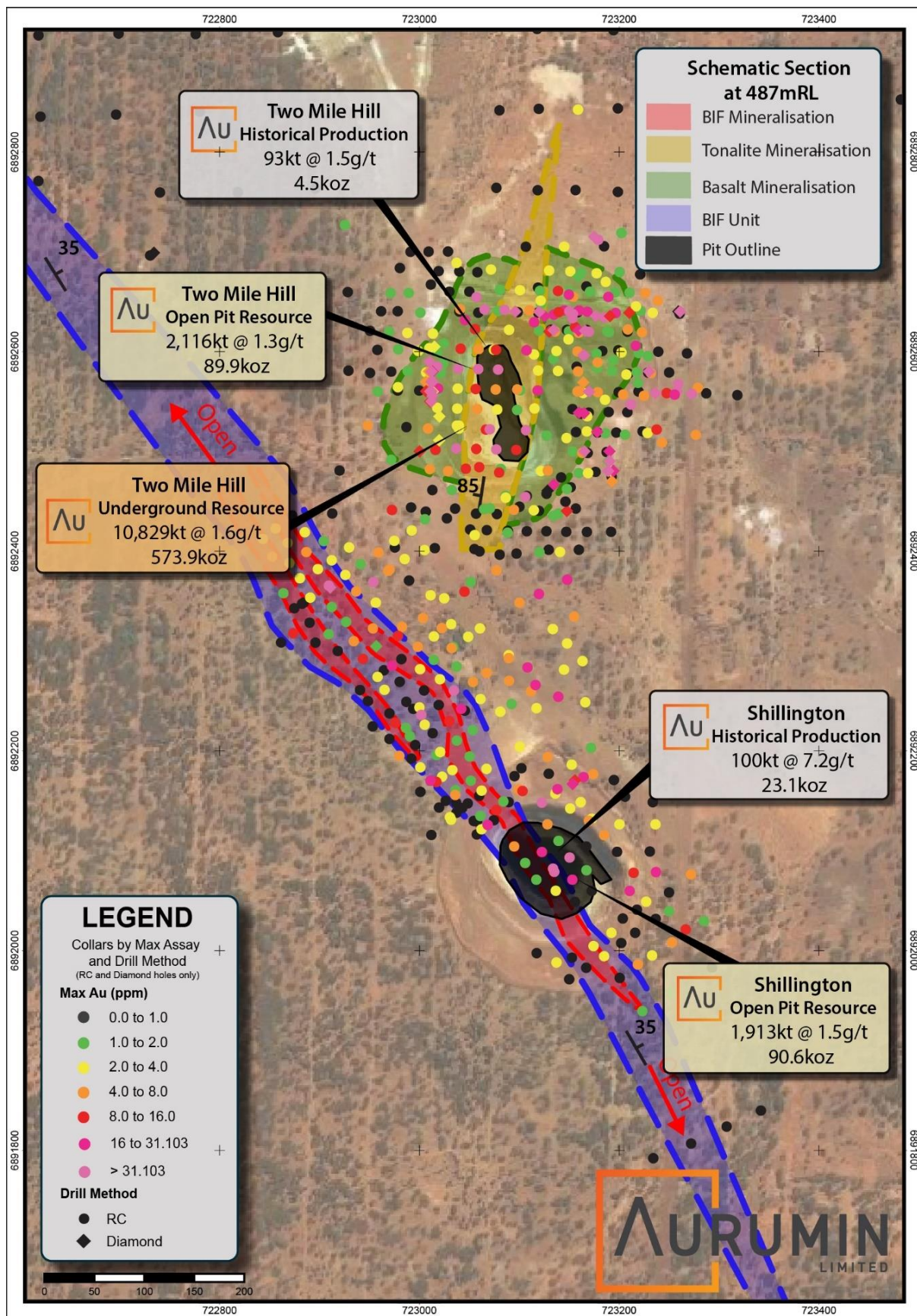


Figure 2 – Shillington and Two Mile Hill Plan View showing collars and max Au assay values

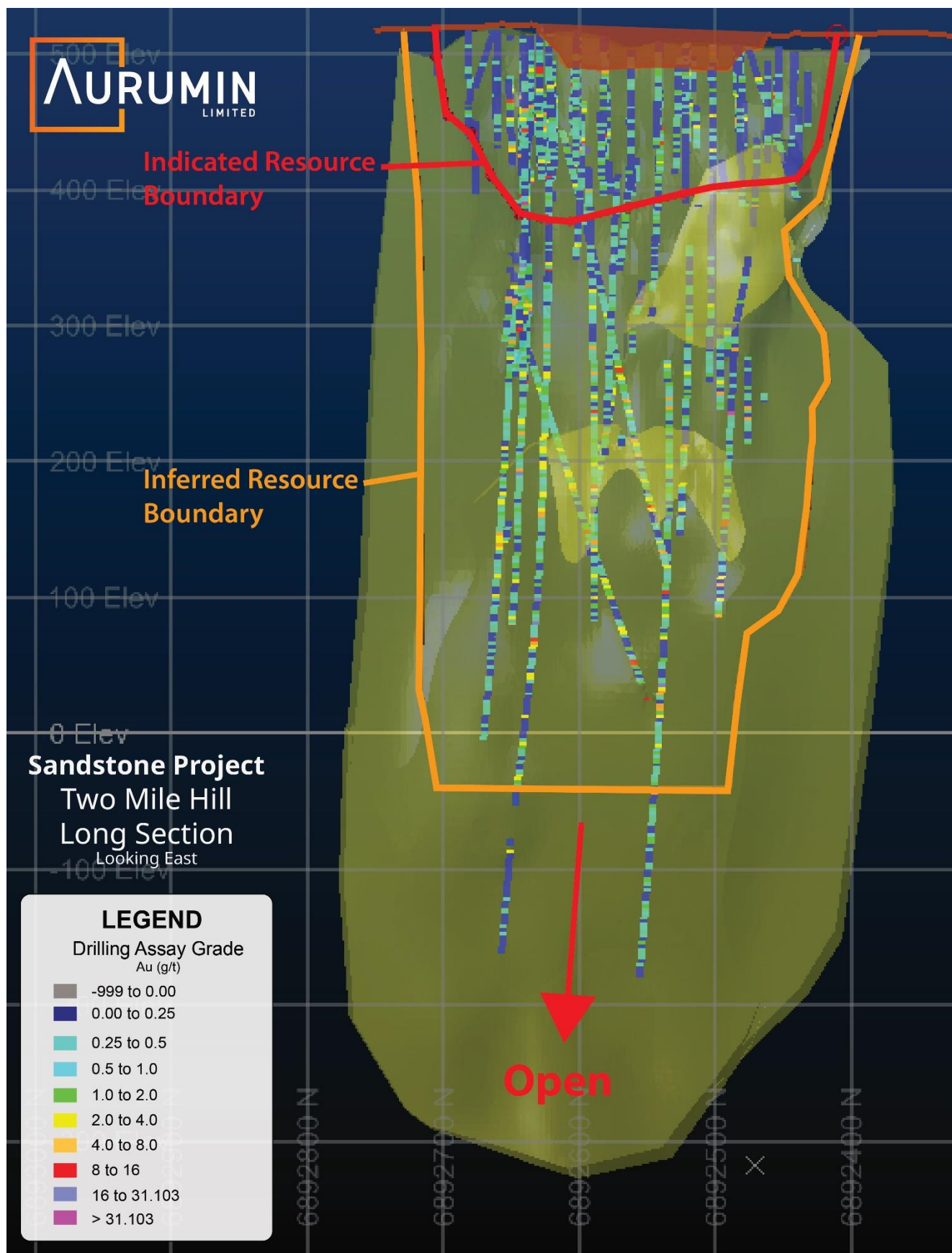


Figure 3 – Two Mile Hill Long Section showing indicated and inferred mineralisation boundaries



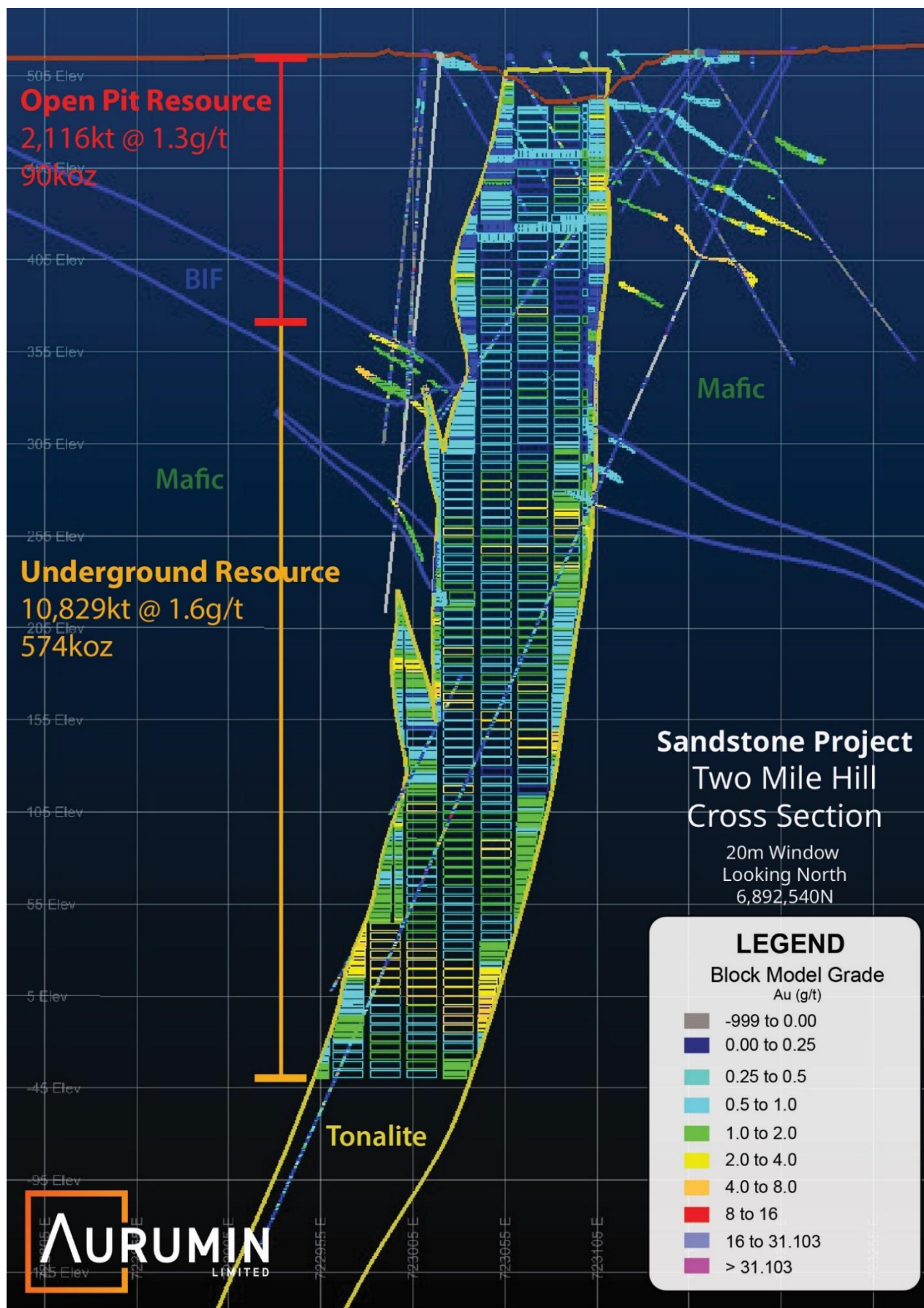


Figure 4 – Two Mile Hill mineralisation interpretation indicative cross section, showing block model and drilling. Looking north on 6,892,540N

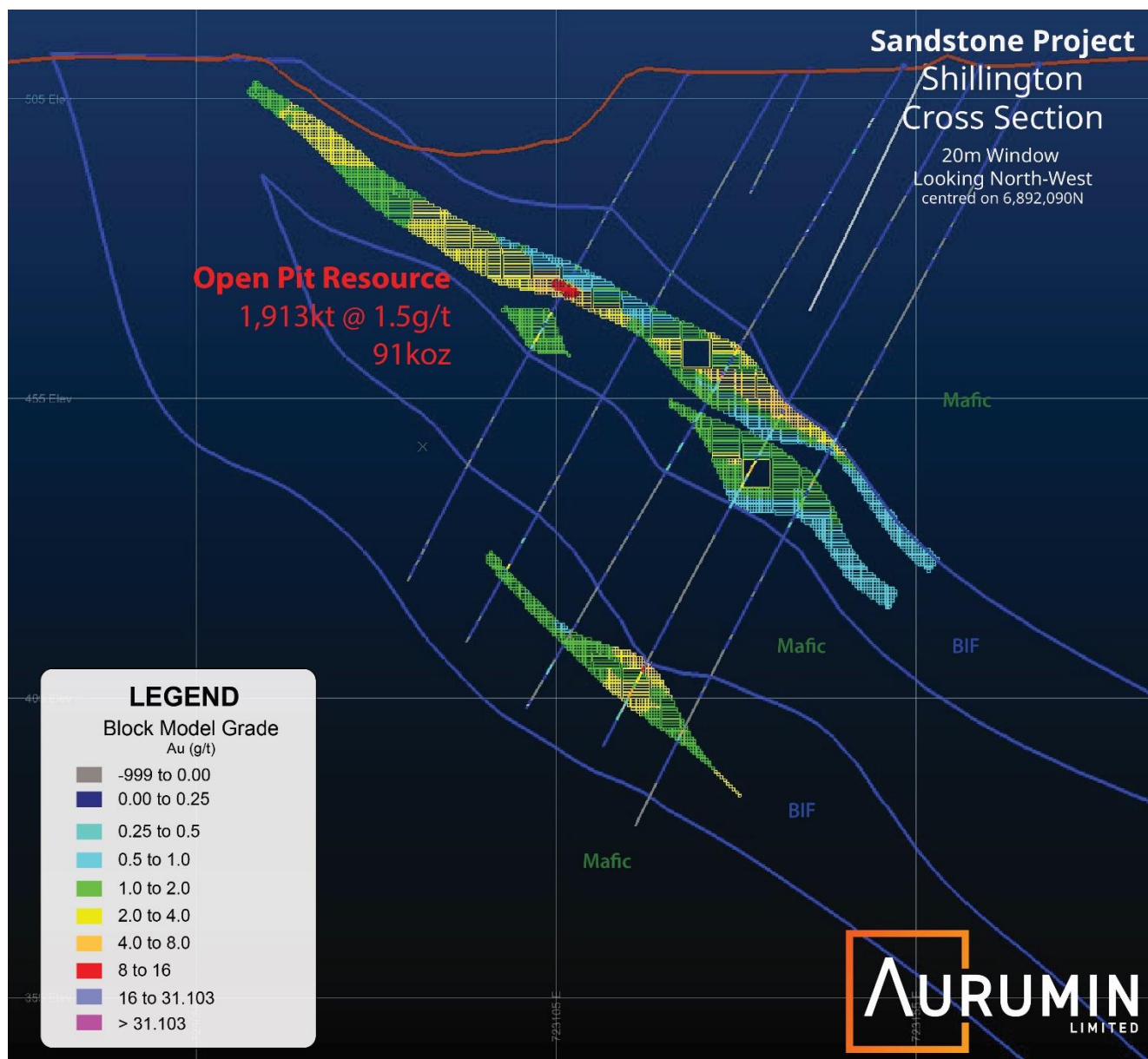


Figure 5 – Shillington mineralisation interpretation indicative cross section, showing block model and drilling. Looking north-west, centred on 6,892,090N



## MINERAL RESOURCE SUMMARY

The following information is provided to meet the requirements under listing rule 5.8.1. This information is provided in greater detail in the attached JORC Table 1 (Annexure A).

Modern testing and sampling at the Central Sandstone Project has been completed since 1984 by several companies starting with Black Hill Minerals Limited/Sundowner Minerals NL (BHM) and moving through Herald Resources Limited (HRL), Troy Resources NL (TYR), Middle Island Resources Limited (MDI) and Aurumin Limited (AUN).

### *Geology and Geological Interpretation*

#### **Regional Geology**

The Two Mile Hill and Shillington deposits are located in the Sandstone greenstone belt (SSGB). The SSGB is a triangular belt, interpreted as a north-plunging antiform, located at the northern end of the Southern Cross province, which forms the central spine of the Archaean Yilgarn block. The SSGB sits at the northern end of the Diemals dome, at the conjunction of the major transcratonic Youanmi and Edale faults. The geology of the Sandstone greenstone belt is controlled by the Sandstone syncline.

The SSGB consists of mafic volcanic and intrusive rocks with subordinate ultramafic BIF and siliciclastic sediments. Granitoid plutons associated with the Diemals dome intrude the southern margin of the belt. The metamorphic grade is greenschist facies, although amphibolite facies assemblages are locally developed along the flanks of the belt. A mafic-dominated succession containing BIF, chert and schist is located on the limbs of the Sandstone syncline.

Gold deposits within the Project are typical Archaean mesothermal types that are hosted in the regional structural corridors that bound the greenstone belt on the east and west.

#### **Shillington – Two Mile Hill complex**

The Two Mile Hill - Shillington complex consists of late stage, near vertical intrusive tonalite stock which cuts the local stratigraphy of mafic volcanics and BIF. Gold mineralisation is developed in the tonalite, enveloping pillow and komatiitic basalts and the overlying laterite.

Weathering surfaces (base of complete oxidation (BOCO) and top of fresh rock (TOFR)) and laterites have been interpreted and constructed using geologically guided implicit modelling within Datamine RM software for the whole complex to ensure continuity between the two areas.

Multiple as-built wireframes (open pit shapes) were constructed from surface and drone surveys. There are no known underground workings. Mineralisation within open pits has been depleted from the Mineral Resource estimate.

#### **Shillington Deposit**

The primary gold mineralisation in the Shillington deposit is hosted by a folded BIF units with minor lateritic and oxide zone within the surrounding basalts. The base of complete oxidation is higher at Shillington, due to the higher resistance to weathering of the BIF units, however the majority of gold mineralisation does occur in the transitional zone. The BIF units and gold mineralisation strike approximately 320° and have a shallow dip of approximately 30° to the northeast.

The Shillington Mineral Resource has a total strike length of 650m, is 60m wide, and extends to approximately 120m depth based on current drilling.

A total of 31 mineralisation wireframes have been constructed.

### **Two Mile Hill Deposit**

Mineralisation at Two Mile Hill is hosted in three geological domains. The majority of the Two Mile Hill resource occurs within a tonalite intrusion. Mineralisation also occurs within BIF beds, and within the basalts that host the tonalite intrusion. The tonalite intrusion is broadly oblate in plan, elongate generally north to south (010°) and dipping steeply (~78°) towards 281°. The tonalite hosted mineralisation occurs predominantly as discrete free gold occurrences within a sheeted/stockwork array of narrow quartz veins. Coarse free gold is frequently evident in quartz veins, often associated with galena. Quartz veining is associated with pervasive sericite-carbonate alteration, frequently accompanied by disseminated pyrite. Typical mineralised tonalite core is pictured Figure 7 and Figure 8 below.

A total of 26 mineralisation wireframes, have been constructed.

#### Two Mile Hill Tonalite Mineralisation

The primary Two Mile Hill Mineral Resource has a total strike length of approximately 400m, and is approximately 100m wide. The body remains open at depth with current drilling defining mineralised tonalite beyond 725m below surface.

The orientation of the sheeted vein array is variable but is on average orthogonal to the estimated axis of the tonalite, with the axis of the tonalite plunging approximately 80° towards 280°. Analysis of drill core structural observations from recent and historical drilling demonstrates an average plane for all quartz veining in tonalite dipping 25° towards 138°; however, structural observations recorded for veins returning grades above 1g/t Au show a dominant shallow to moderate dip towards the east to northeast (29°->049°), see Figure 6. This northeasterly dip conforms with the visually observed break in grade within the tonalite of 31°->052°.

Veins range from 2mm to 900mm but are typically in the order of 20-80mm width. Through the tonalite there is subtly partitioned zones of more and less intense veining (vein frequency changes). As gold in the tonalite is almost exclusively hosted within the quartz vein set the combination of zones of veining and the orientation of mineralised set informs an overarching shallow northeast dipping control on grade.

In addition to the tonalite ore zone, there is a number of narrow shallow east dipping ore zones within the basalt country rock, predominately on the eastern side of the tonalite, which are included in the Two Mile Hill resource.

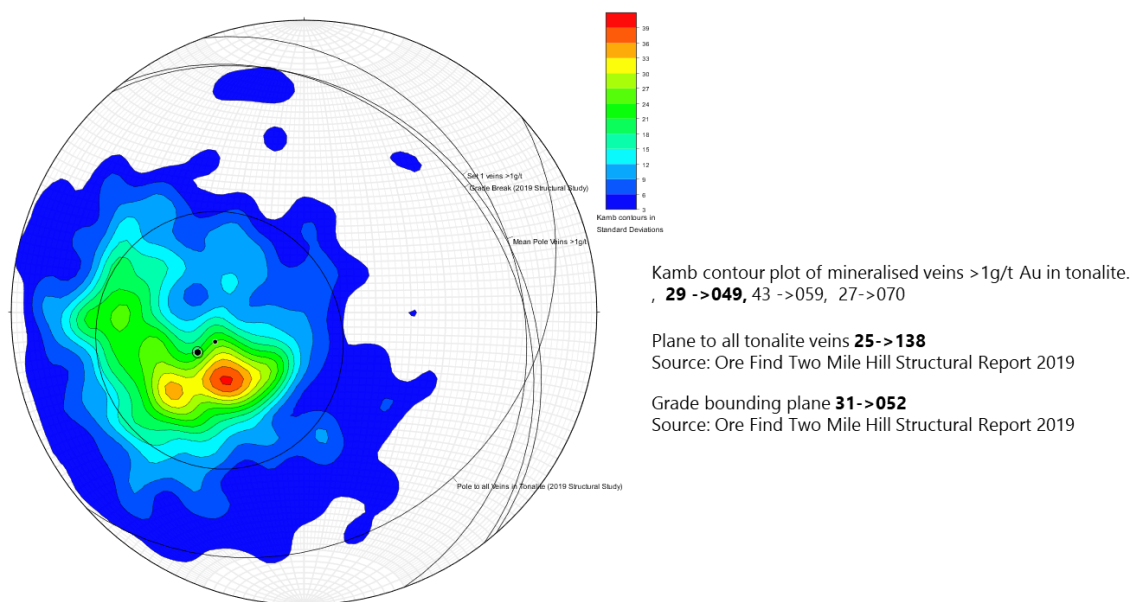


Figure 6 – Lower Hemisphere Equal Area Plot. Kamb Contour structural measurement taken on veins >1g/t Au in tonalite.

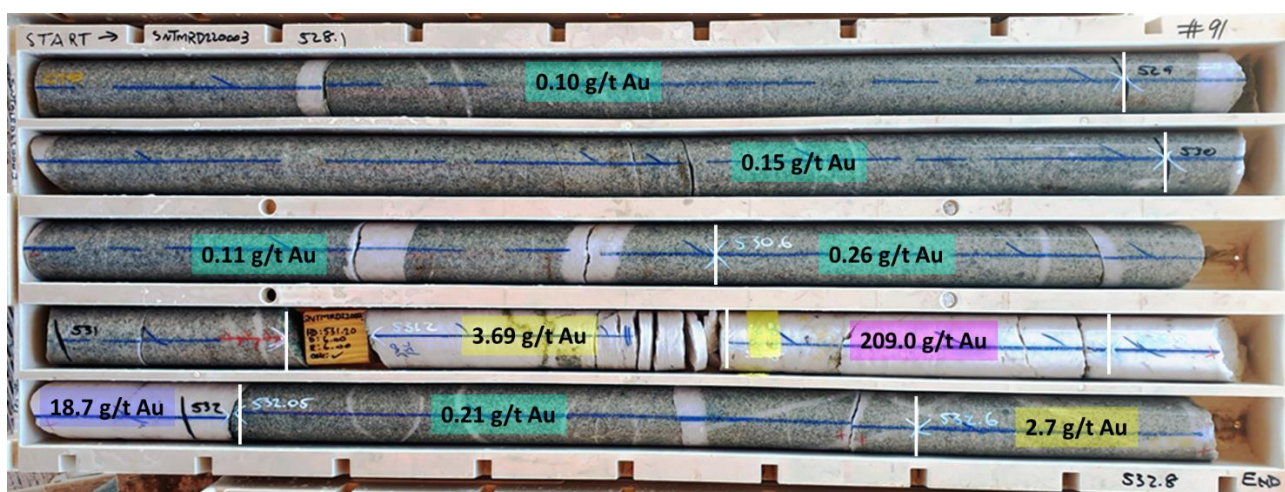


Figure 7 – Sheeted veins in Two Mile Hill Tonalite. Hole SN-TM\_RD\_22\_0003. 528.1m-532.8m. Key assay results: 531.2m to 531.5m 3.69g/t Au, 531.5m to 531.8m 209g/t Au and 531.8m to 532.05m 18.7g/t Au.

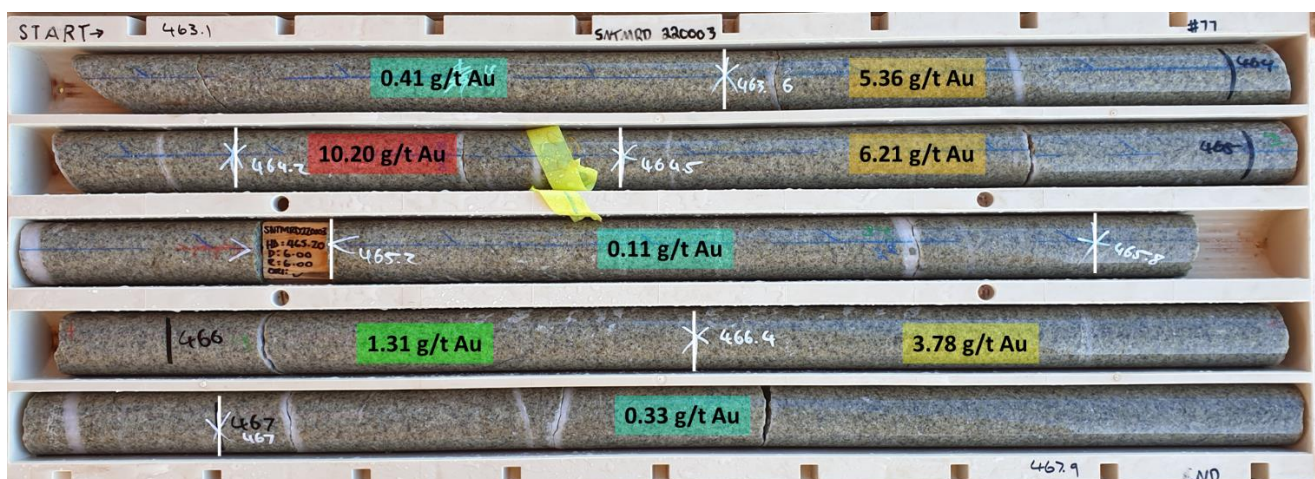


Figure 8 – Sheeted veins in Two Mile Hill Tonalite. Hole SN-TM\_RD\_22\_0003. 463.1m-467.9m. Key assay results: 463.6m to 464.2m 5.36g/t Au, 464.2m to 464.5m 10.2g/t Au (VG) and 464.5m to 465.2m 6.21g/t Au.



### Two Mile Hill BIF Mineralisation

Gold mineralisation at the Two Mile Hill BIF deposit is hosted within a series of stacked BIF units comprising the Shillington BIF package, which dip at approximately 40° towards the northeast, and are intruded by the Two Mile Hill Tonalite Underground deposit. Gold mineralisation is associated with massive to semi-massive pyrite replacement of magnetite horizons within the BIF units, commonly proximal to zones of oblique quartz veining and/or brecciation often associated with interfingering narrow tonalite and/or granodiorite dykes. Although rarely visible, petrographic evidence indicates that the gold is relatively coarse and is developed along fractures within pyrite grains or along pyrite grain boundaries.

The deposition of thick, higher-grade gold intervals within the BIF appears to be primarily controlled by proximity to the intrusive contact with the Two Mile Hill tonalite, with a subordinate control being the density of quartz veining that appears to extend from the tonalite. The balance of evidence suggests that the gold mineralising fluids were sourced from or through the adjacent tonalite.

The BIF underground deposit is situated at approximately 200m vertical depth, lying immediately adjacent to the tonalite margins, possibly better developed along the axes of subtle northeast plunging fold hinges. Typical mineralised BIF core is pictured in Figure 9 and Figure 10.



Figure 9 – Mineralised BIF core from Two Mile BIF domain. Historical TRY hole TRCD825 196.5m to 202.2m

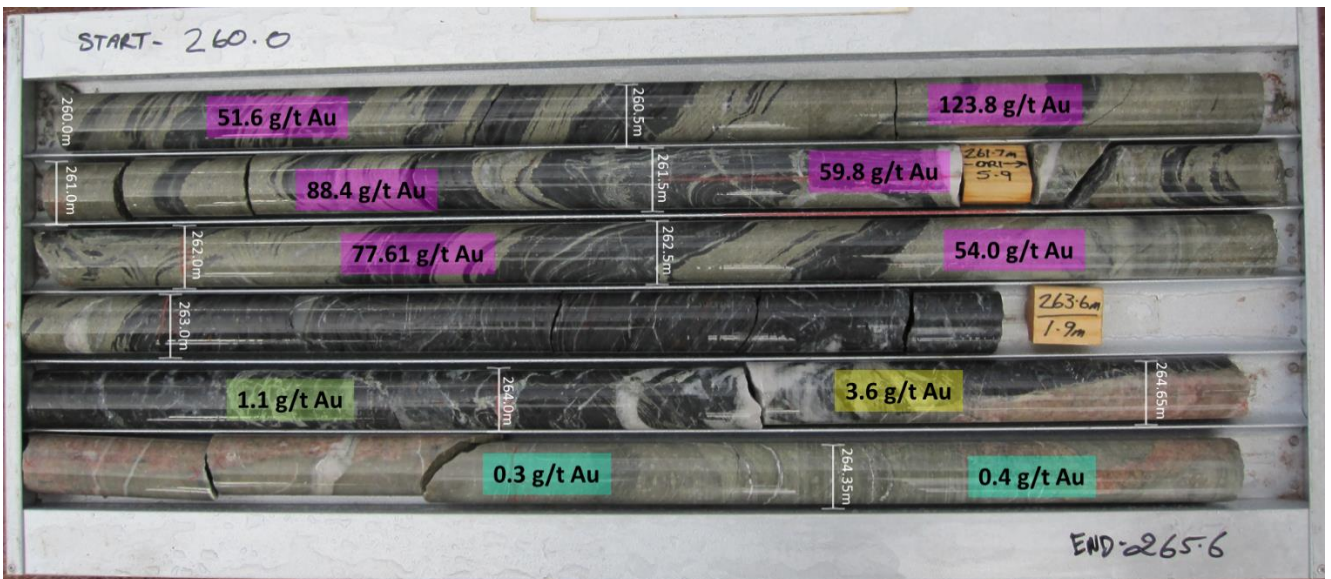


Figure 10 – Mineralised BIF core from Two Mile BIF domain. Historical TRY hole TRCD733 260m to 265.6m

### Two Mile Hill Mafic Domain Mineralisation

The mafic volcanic / basalt domains are interpreted as shallow dipping (approximately 5° to 30°), broadly conformable to the overall trend of bedding described by the BIF units, although local variations and geometry are interpreted. Mineralisation occurs within zones of increased quartz veining within a sequence of pillow basalts. Mineralisation is also observed to occur on narrow sedimentary beds and chert horizons interrupting the basalt beds. In the near surface better grades occur in the mafic domain to the east of the tonalite with only minor anomalous intercepts are noted in the western zones.

Diamond holes drilled in 2022 by Aurumin have identified numerous narrow moderate to high grade intercepts in the mafic rocks adjacent to the tonalite body on both the eastern footwall and western hanging wall positions. Mineralisation in these positions have typically been associated with sericite, carbonate, albite alteration surrounding narrow quartz and quartz—carbonate veins. The vein style and orientation are like that occurring in the tonalite suggesting a relationship to the mineralising event and strain regime under which tonalite mineralisation has formed. Rare bonanza grades have been observed on the contact with the mafic and tonalite geology.



Figure 11 - SN\_TM\_RD\_22\_0004: 447.15m to 451.9m Mineralised veins in mafic contact zone western hanging wall to tonalite.



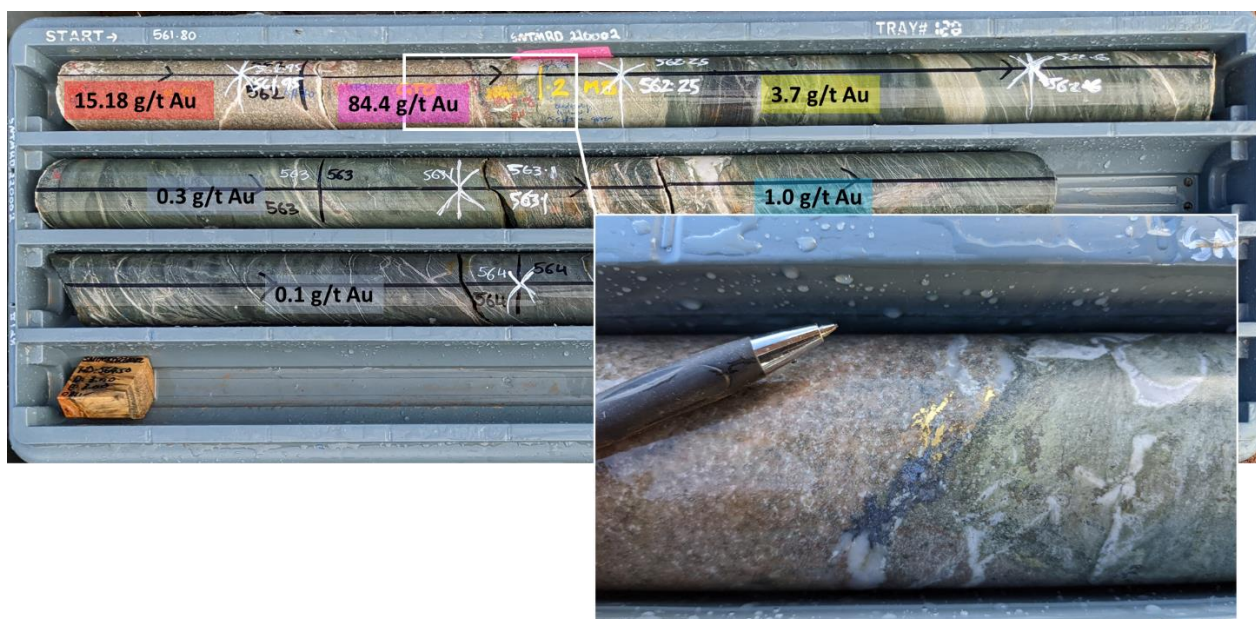


Figure 12 - SN\_TM\_RD\_22\_0004. 562.1m, high grade coarse gold on contact between tonalite and mafic domain, western hanging wall position. Note that interval returned assay of 84.4g/t Au however all visible gold remained on the non-sampled archive half core.

### Drilling Techniques

A number of drilling methods have been used throughout the project's history including Reverse Circulation (RC), Diamond Drilling (DD), Air Core (AC), Rotary Air Blast (RAB), Auger Drilling (AG) and Vacuum (VC). However, only RC and DD have been used for estimation. Much metadata and documentation surrounding the drilling at the Central Sandstone Project exists and all drilling used for estimation is assumed to have been completed to industry standard practices current at the time of drilling and is given equal weighting.

Grade control data for the historical pits is available and has been sighted but not used in estimation.

Table 2 - All drillhole used in Shillington and Two Mile Hill

| Drill Type   | Count      |
|--------------|------------|
| Diamond      | 65         |
| RC           | 566        |
| <b>Total</b> | <b>631</b> |

The Two Mile Hill tonalite deposit is defined by 38 RC pre-collared diamond drill holes (predominantly NQ and some HQ core size) representing 13,383m and 103 RC holes representing 10,333m, or 141 drill holes comprising 23,716m in aggregate.

The Two Mile Hill BIF deposit is defined by 34 RC pre-collared diamond drill holes (predominantly NQ and some HQ core size) representing 10,452m and 1 RC hole representing 209m, or 35 drill holes comprising 10,661m in aggregate.

The Shillington ore zones are defined by 186 RC holes representing 15652m, and 3 diamond holes (HQ3) representing 255.63m or 189 drill holes comprising 15,907m in aggregate.

Aurumin and MDI pre-collars were drilled with 5¼ inch face sampling hammer from surface, while the HRL and TRY RC drilling was drilled at an unknown size to return a 1m sample. The diamond cored component was



completed with HQ (63.5mm) core, in one instance HQ3 (61.1mm), otherwise NQ2 (50.6mm) tails. Core was oriented using a Reflex ACT orientation tool or the Boart Longyear TRUCORE device (AUN).

Aurumin RC and Diamond holes were surveyed using the Axis Champ north seeking gyro survey tool.

RC and diamond logging included, where practicable, but not is limited to, lithology, alteration, mineralogy, vein quantification and description, and orientation information of selected geological or structural features. Logging was carried out according to internal Company standards at the time of drilling. All core was marked with depth, orientation lines, key geological logging and sample intervals and the photographed before being cut and/or sampled. Core was photographed wet and dry within each core tray. Each metre of all drillholes was qualitatively logged from start to finish of the drillhole.

### ***Sampling and Sub Sampling Techniques***

Aurumin diamond core was sampled to intervals defined by the geologist to honour geological/mineralised features. Through areas of uniform mineralisation or sheet work/stockwork type veining samples were taken at a uniform interval 0.6 to 1.0m intervals. For diamond core the minimum sample length was 0.2m and the maximum sample length of 1.2m. HQ core samples comprised half core whereas NQ2 core was whole core sampled. Where whole core sampling was employed sample length was restricted to 0.6m to reduce sample volume split at coarse fractions during sample preparation. MDI Diamond drill core was sampled at 1m intervals and comprised half NQ2 core. Diamond core and RC chip recovery data were measured for each drill run/drillhole and captured in a digital logging software package. The data has been reviewed and the core recovery was effectively 100% throughout. Core was re-aligned prior to splitting and the right-hand side half core section (looking down the hole) was consistently sampled for assay.

HQ and NQ diamond core drilling was also completed by HRL and TRY. TRY diamond holes triple tube coring was used due to the friable nature of the oxide zone lithologies being drilled. The angled core holes were orientated where possible using a crayon marker spear tool and the holes were regularly surveyed using an Eastman downhole camera. TRY core samples were marked on the core by the geologist according to geological intervals. The core was cut in half by TRY field technicians, with half being placed in a pre-numbered calico bag and the other half returned to the core tray. For duplicate samples the core to be submitted for analysis was quartered.

HRL sampled half core, the core was sampled mostly in metre intervals however some varied in length according to alteration, mineralisation and lithological boundaries.

AUN and MDI RC sampling involved the collection of 2-3kg of RC chips off the drill rig's cone splitter at 1m intervals. In some cases, composite samples were created using a PVC spear to collect sample from the reject 1m intervals. These were placed into pre-numbered calico bags. Where composite samples returned anomalous results, the initial 1m samples collected from the cone splitter were submitted for the interval. The primary RC sample was taken from the same splitter chute for all programmes.

HRL and TRY RC sampling was by collecting 2-3kg of RC chips via a three-tier Jones riffle splitter at 1m intervals. Composite samples of varying length were collected using a scoop and where anomalous values were returned the original 1m interval samples were submitted for analysis.

### ***Sample recoveries***

For Aurumin diamond drilling, recovery of core was recorded by drillers on core blocks. This was checked and compared to the measurements of the core by the geologist. Areas of diamond core loss were marked on core blocks; all logging and sampling intervals honour intervals of core loss. AUN monitored RC recoveries visually and through sample weights. MDI diamond core and RC chip recovery data were measured for each drill run/drillhole and captured in a digital logging software package. The data has been reviewed and the core recovery was

effectively 100% throughout drilling. Aurumin and MDI RC recoveries were excellent, with dry samples being a consistent weight of 2-3kg.

No sample recovery information has been found for TRY or HRL drilling, however TRY reported that there were no known drilling, sampling or recovery factors that could materially impact the accuracy and reliability of the results.

The water table was intersected at 40–60m depth down-hole. AUN and MDI had no issues in keeping the sample dry. HRL and TRY drilling also intersected the water table at 40–60m. While some wet material was sampled, this accounts for less than 1% of their total sampling.

There is no known relationship between recovery and grade in RC or DD sampling.

### ***Classification***

All mineralisation has been classified as a combination of Indicated and Inferred Resource based on input data quality, confidence in the geological understanding and modelling, grade estimation parameters and economic parameters.

The grade estimation parameters include the number of data points informing the estimate, the distance the data points are apart and review and validation post estimation.

Mineral Resource wireframes constructed with less than two informing drill holes, have been deemed unclassified have not been reported.

### ***Sample Analysis Method***

All AUN samples were submitted to ALS laboratories in Perth, WA for sample preparation, a portion of samples were redirected to ALS Adelaide, SA for sample preparation due to laboratory congestion. Pulps and reject material were returned to Perth. All analyses were conducted at ALS Perth, WA. Sample preparation for drill samples involved drying the whole sample and pulverising to 75 microns. HQ and NQ diamond core samples were sent to the laboratory and crushed. Samples weighing less than 3kg were crushed to (-10mm) then full sample pulverised to a 300g pulp, with a 50g charge sub-sampled for fire assay analysis. Samples weighing greater than 3kg were fine crushed to (-2mm) then split using a Boyd Rotary Splitter to produce a 3kg sample which is then pulverised to 95% passing 75 microns to produce a 300g pulp, with a 50g charge sub-sampled for fire assay analysis. A 50g sample charge was then used for the fire assay (AAS finish); the detection limit was 0.005ppm.

A fire assay fusion-gravimetric analysis was used for gold analysis in samples that returned a greater than 100ppm result using the standard fire analysis technique. These methods are considered an estimation of total gold content.

MDI used a fire assay (FA) method with either an ICP-OES or an ICP-AAS finish for gold analysis. Analysis by Intertek was a 50g FA/ICP-OES, analysis by Nagrom was FA/ICP-OES by and Analysis by SGS was FA/AAS. Sample preparation was completed by Intertek, Nagrom and SGS laboratories. The samples were dried and crushed to -10mm before being split and a 300g subsample pulverised to 95% passing 75 micron. This fraction was then split again to a 50g sample charge for fire assay.

TRY samples were assayed by SGS Australia Pty Ltd in Perth, Western Australia. The samples were dried and crushed to -10mm before being split and a 300g subsample pulverized to 95% passing 75 micron. This fraction was then split again to a 50g sample charge for fire assay with an AAS finish.

HRL samples were sent to Analabs in Mt Magnet for 50g fire assay, however, the precise preparation procedure is not documented.

Aurumin QAQC procedures collect field duplicates (for RC samples) and insert certified reference materials (CRMs). Standards were inserted at a rate of 1:20 while blanks were inserted at 1:50. Duplicate samples in RC samples are taken every 1:20. MDI collected RC field duplicates at a rate of 1:18 samples and inserted CRMs at a rate of 1:9. A quartz flush was inserted after every batch processed. QAQC samples were assessed on a batch by batch basis.

TRY QAQC procedures inserted a minimum of 1 CRM sample with each batch of samples for all exploration work. The grade of the standard used was routinely varied according to expected results. For RC and DD resource evaluation drilling an average of 1 field duplicate, 1 blank and 1 standard was submitted for every 50 samples. QC samples were inserted randomly throughout the sample sequence. TRY's exploration drilling results of QC samples were assessed by TRY on a batch by batch basis and a periodic audit of the exploration QC data was carried out by Data consultants Maxwell Geoservices (Maxwell). Details surrounding the specifics of HRL QAQC protocols has not been found.

In all cases, sample size and assay charge size are considered appropriate for the style of mineralisation.

### ***Estimation Methodology (Mineral Resource Estimate)***

#### **Shillington Resource Estimation**

Three-dimensional wireframes (geological and mineralised) were constructed using geologically guided implicit modelling within Datamine RM software. These wireframes were used in the construction of a rotated block model with parent block sizes of 5m (x) by 10m (y) by 5m (z). The model was sub-blocked to 0.5m x 1m x 0.5m to ensure block model representation of constructed wireframes volumes.

Statistical analysis of the mineralised intervals determined that 1m was an appropriate composite length for top cut, variogram modelling and estimation.

Analysis on grade outliers was conducted for each domain and used to determine appropriate top cut values. These top cut values (ranging from 4-10g/t) were applied to the composite file before estimation.

Variogram modelling was completed with Snowden's Supervisor software, with good correlation between calculated directions and geological observations. The parameters determined from this analysis were used in the estimation interpolation process.

The block model grades were estimated using Ordinary Kriging (OK) grade interpolation techniques constrained within the mineralisation wireframes, with Inverse Distance (ID1.5 and ID2) and Nearest Neighbour (NN) also estimated for validation and comparison purposes.

A three-pass estimation strategy was employed for all domains as shown below. After these three passes, all un-estimated blocks were assigned a nearest neighbour estimate value using a seam composite.



Table 3 – Block model estimation parameters used per pass for the Shillington deposit

|        | Domain | Rotation |    |      | Search Range |      |      | Min Samples | Max Samples | Max Samples/drillhole |
|--------|--------|----------|----|------|--------------|------|------|-------------|-------------|-----------------------|
|        |        | Z        | X  | Z    | X            | Y    | Z    |             |             |                       |
| Pass 1 | 1      | 55       | 30 | -40  | 17.5         | 13   | 12.5 | 12          | 24          | 3                     |
|        | 2      | 70       | 55 | -45  | 15           | 7.5  | 7.5  |             |             |                       |
|        | 3      | -140     | 40 | -90  | 12.5         | 12.5 | 12.5 |             |             |                       |
|        | 4      | 0        | 0  | -120 | 12.5         | 10   | 12.5 |             |             |                       |

|        | Domain | Rotation |    |      | Search Range |    |    | Min Samples | Max Samples | Max Samples/drillhole |
|--------|--------|----------|----|------|--------------|----|----|-------------|-------------|-----------------------|
|        |        | Z        | X  | Z    | X            | Y  | Z  |             |             |                       |
| Pass 2 | 1      | 55       | 30 | -40  | 35           | 26 | 25 | 12          | 24          | 3                     |
|        | 2      | 70       | 55 | -45  | 30           | 15 | 15 |             |             |                       |
|        | 3      | -140     | 40 | -90  | 25           | 25 | 25 |             |             |                       |
|        | 4      | 0        | 0  | -120 | 25           | 20 | 25 |             |             |                       |

|        | Domain | Rotation |    |      | Search Range |    |    | Min Samples | Max Samples | Max Samples/drillhole |
|--------|--------|----------|----|------|--------------|----|----|-------------|-------------|-----------------------|
|        |        | Z        | X  | Z    | X            | Y  | Z  |             |             |                       |
| Pass 3 | 1      | 55       | 30 | -40  | 70           | 52 | 50 | 5           | 24          | 3                     |
|        | 2      | 70       | 55 | -45  | 60           | 30 | 30 |             |             |                       |
|        | 3      | -140     | 40 | -90  | 50           | 50 | 50 |             |             |                       |
|        | 4      | 0        | 0  | -120 | 50           | 40 | 50 |             |             |                       |

## Two Mile Hill Resource Estimation

Three-dimensional wireframes (geological and mineralised) were constructed using geologically guided implicit modelling within Datamine RM. These wireframes were used in the construction of an un-rotated block model with parent block sizes of 20m (x) by 20m (y) by 5m (z). The model was sub-blocked to 1m x 1m x 1m to ensure block model representation of constructed wireframes volumes.

The estimates of the tonalite and non-tonalite (Basalt, Banded Iron and Laterite) ore zone was conducted separately and combined at the end for reporting.

### Tonalite

Statistical analysis of the mineralised intervals determined that 3m was an appropriate composite length for top cut, variogram modelling and estimation.

Analysis on grade outliers was conducted to determine appropriate top cut values. The top cut value (20g/t) was applied to the composite file before estimation.

Variogram modelling was completed with Snowden's Supervisor software, with good correlation between calculated directions and geological observations (quartz vein direction). The parameters determined from this analysis were used in the estimation interpolation process.

The block model grades were estimated using Ordinary Kriging (OK), Inverse Distance (ID1.5 and ID2) and Nearest Neighbour (using 4m seam composites) grade interpolation techniques constrained within the tonalite geological wireframes.

A four Pass estimation strategy was employed (refer to table 2). After these four passes, all un-estimated blocks

were assigned a nearest neighbour estimate value using a 4m composite with heavy top cut (at 90% grade percentile).

*Non-Tonalite (Two Mile Hill)*

Statistical analysis of the mineralised intervals determined that 1m was an appropriate composite length for top cut, variogram modelling and estimation.

Analysis on grade outliers was conducted for each domain and used to determine appropriate top cut values. These top cuts values (ranging from 2-20g/t) were applied to the composite file before estimation.

Variogram modelling was completed with Snowden's Supervisor software, with good correlation between calculated directions and geological observations. The parameters determined from this analysis were used in the estimation interpolation process.

The block model grades were estimated using Ordinary Kriging (OK), Inverse Distance (ID1.5 and ID2) and Nearest Neighbour grade interpolation techniques constrained within the mineralisation wireframes. Final estimating technique was chosen after complete validation and review.

A three-pass estimation strategy was employed for all domains as shown below. After these three passes, all un-estimated blocks were assigned a nearest neighbour estimate value using a seam composite.

Table 4 – Block model estimation parameters used per pass for the Two Mile Hill resource estimate

|        | Domain    | Rotation |     |      | Search Range |      |     | Min Samples | Max Samples | Max Samples/drillhole |
|--------|-----------|----------|-----|------|--------------|------|-----|-------------|-------------|-----------------------|
|        |           | Z        | X   | Z    | X            | Y    | Z   |             |             |                       |
| Pass 1 | Basalt_mz | -115     | 150 | -20  | 12.5         | 8    | 7.5 | 15          | 45          | 5                     |
|        | HG_BIF    | -130     | 140 | -110 | 11.5         | 9.5  | 9.5 |             |             |                       |
|        | 9505_bif  | -105     | 120 | -35  | 16.5         | 5.5  | 5.5 |             |             |                       |
|        | laterite  | 0        | 0   | -170 | 24.5         | 18.5 | 5   | 3           | 6           | NA                    |
|        | TONALITE  | -130     | 150 | -70  | 25           | 22.5 | 5   | 5           | 15          | 2                     |

|        | Domain    | Rotation |     |      | Search Range |    |    | Min Samples | Max Samples | Max Samples/drillhole |
|--------|-----------|----------|-----|------|--------------|----|----|-------------|-------------|-----------------------|
|        |           | Z        | X   | Z    | X            | Y  | Z  |             |             |                       |
| Pass 2 | Basalt_mz | -115     | 150 | -20  | 25           | 16 | 15 | 15          | 45          | 5                     |
|        | HG_BIF    | -130     | 140 | -110 | 23           | 19 | 19 |             |             |                       |
|        | 9505_bif  | -105     | 120 | -35  | 33           | 11 | 11 |             |             |                       |
|        | laterite  | 0        | 0   | -170 | 49           | 37 | 10 | 3           | 6           | NA                    |
|        | TONALITE  | -130     | 150 | -70  | 50           | 45 | 10 | 5           | 15          | 2                     |

|        | Domain    | Rotation |     |      | Search Range |    |    | Min Samples | Max Samples | Max Samples/drillhole |
|--------|-----------|----------|-----|------|--------------|----|----|-------------|-------------|-----------------------|
|        |           | Z        | X   | Z    | X            | Y  | Z  |             |             |                       |
| Pass 3 | Basalt_mz | -115     | 150 | -20  | 50           | 32 | 30 | 5           | 24          | 5                     |
|        | HG_BIF    | -130     | 140 | -110 | 46           | 38 | 38 |             |             |                       |
|        | 9505_bif  | -105     | 120 | -35  | 66           | 22 | 22 |             |             |                       |
|        | laterite  | 0        | 0   | -170 | 98           | 74 | 20 | 3           | 6           | NA                    |
|        | TONALITE  | -130     | 150 | -70  | 50           | 45 | 10 | 5           | 15          | NA                    |

|        | Domain   | Rotation |     |     | Search Range |    |    | Min Samples | Max Samples | Max Samples/drillhole |
|--------|----------|----------|-----|-----|--------------|----|----|-------------|-------------|-----------------------|
|        |          | Z        | X   | Z   | X            | Y  | Z  |             |             |                       |
| Pass 4 | TONALITE | -130     | 150 | -70 | 100          | 90 | 20 | 5           | 15          | NA                    |

The bulk density has been assigned based on weathering and lithology groupings of the available data and using knowledge of the project based on previous studies (production and resource/reserve investigations). Where insufficient bulk density data exist, the density was assumed based on like lithology and weathering.

The bulk density values were derived from 178 measurements taken on the core comprising 46 immersion test of core billets and 132 core tray weight determinations. Very limited documentation is available about the collection method and quality of core tray weight data. The core billet immersion determinations have been completed by independent laboratory ALS using wax coating where applicable. Bulk densities used for the Shillington and Two Mile Hill resource models are presented in Table 5.

Table 5 - Bulk densities used for the both the Shillington and Two Mile Hill resource estimates

| Lithology                   | Weathering   | Density |
|-----------------------------|--------------|---------|
| Laterite                    |              | 2.21    |
| Basalt                      | Oxide        | 1.83    |
|                             | Transitional | 2.42    |
|                             | Fresh        | 2.91    |
| Banded Iron Formation (BIF) | Oxide        | 2.00    |
|                             | Transitional | 2.80    |
|                             | Fresh        | 3.00    |
| Tonalite                    | Oxide        | 2.21    |
|                             | Transitional | 2.54    |
|                             | Fresh        | 2.71    |

Block model validation was completed to ensure modelling and estimation techniques were appropriate for the deposit. These methods include:

- visual validation,
- swath plots,
- model/volume checks and
- composite vs model grades analysis.

### **Cut-off Grades**

For Shillington the Mineral Resource is reported at a 0.5g/t Au cut-off grade, to allow for potential mining, haulage and processing costs.

For the Two Mile Hill Open Pit (above 370mRL) the Mineral Resource is reported at a 0.5g/t Au cut-off grade, to allow for potential Mining, haulage, and processing costs.

For the Two Mile Hill Underground the Mineral Resource is reported at a 0.73g/t Au cut-off grade, to allow for potential mining haulage and processing costs as below.

Table 6 - Cost assumptions used to determine cut-off grade for Two Mile Hill resource estimates

| Operating Costs                |                |
|--------------------------------|----------------|
| Item:                          |                |
| Mining (A\$/t):                | \$30.00        |
| Overheads (A\$/t):             | \$10.00        |
| Surface Haulage (A\$/t):       | \$1.40         |
| Processing (A\$/t)             | \$30.00        |
| <b>Total Cost (A\$/t):</b>     | <b>\$71.40</b> |
| Revenue and Revenue Deductions |                |
| Item:                          |                |
| Gold Price (A\$/oz):           | \$3,250        |
| Processing Recovery            | 96%            |
| WASG Royalty                   | 2.50%          |
| <b>Net Revenue (A\$/g):</b>    | <b>\$97.80</b> |



***Mining and Metallurgical Methods and Parameters (Modifying Factors)***

Mining at the Shillington deposit is assumed to be by conventional open pit methods. The maximum depth reported has been limited to 140m as a conceptual maximum open pit mining depth.

Mining of the Two Mile Hill open pit resource (above 370mRL) is assumed to be by conventional open pit mining methods. The maximum depth reported has been limited to 150m as a conceptual maximum open pit mining depth.

Open pit optimisations have not been completed and no modifying factors (mining dilution and recovery or processing recovery) have been applied to the reported Mineral Resource.

The Two Mile Hill Underground deposit is assumed to be mined using bulk underground mining techniques. No stope optimization has occurred. No modifying factors (mining dilution and recovery or processing recovery) have been applied to the reported Mineral Resource.

Metallurgical test work was undertaken by ALS laboratories on the Shillington and Two Mile Hill Deposits in 2016 with further work was completed on Two Mile Hill Underground material in 2017 and 2020.

Two Mile Hill composites contained significant free gold with a minimum 20% gravity recovered gold (GRG) recovered across the 9 tests undertaken in 2016, 2017 and 2020. The tonalite underground material contained the largest amount of GRG of all (>60%) and is due to significant occurrence of coarse gold noted in the intervals making up the composite. A gold recovery of approximately 96% has been determined by metallurgical test work on the primary tonalite mineralisation utilising site process water.

For Shillington the GRG test work confirms the presence of coarse gold in the Shillington composites. The average GRG was 14% obtained for Shillington. The gold extraction obtained for Shillington (92.3% at 106µm) is comparable to recoveries obtained historically through the plant in the late 1990's. An estimated target recovery of 92.0% should be achievable for Shillington for the head grade proposed.

**Significant Model and Interpretation Changes**

The recent 2,470m diamond drilling campaign at Two Mile Hill has provided important new geological and assay data. This has allowed for more definition in the geological interpretation of the Two Mile Hill Tonalite, the abutting Two Mile BIF units and mineralised volumes in the eastern mafic domain. The refined geological models have resulted in a comparatively tighter tonalite interpretation and less extrapolated volume at depth.

Aurumin's diamond drilling programme at Two Mile Hill was planned to improve the data density in the area of sparser drilling between 250m and 500m below surface. This area had been relatively under-drilled, however, the drilling that existed showed good vein frequency and high-grades typical of the tonalite style mineralisation at Two Mile Hill. Drilling was designed to partially infill the poorly defined areas between isolated zones of higher grades and vein frequency in an interpreted shallow to moderately northeast dipping orientation. The overarching goal being to determine broad higher-grade intervals of mineralisation that could be linked into continuous zones.

The nine-hole RC programme drilled at Shillington sought to test for geological linkages between the Shillington and Two Mile Hill deposits and the potential for higher-grade mineralisation along a structurally controlled corridor to both improve and extend the existing Shillington Resource. The positions targeted correspond to the interpreted intersection of the structure into which the Two Mile Hill Tonalite has intruded. Drilling at the margin and beyond the previous resource at Shillington identified high-grade mineralisation in this position and has contributed to the change in Shillington resource.

A synthesis of a historical technical reports, review of drill core, pit observations and analysis of historical and newly acquired drill hole structural data has informed the search parameters and modelling approach taken in the

Two Mile Hill Tonalite model. A significant result has been the recognition and confirmation of the dominant shallowly east to northeast dipping vein sets as reflecting the general orientation of gradational zones or packages of mineralisation. This orientation conforms to visual observations of the apparent and inferred geological controls on emplacement of the extension vein sets in the tonalite plug. Using these geological observations as a line of evidence informing statistical analysis of assay data has resulted in increased continuity of grade within the tonalite hosted mineralisation.

Minor (increases) have been applied to costs for cut-off grade determination. Similarly, despite several trials supporting the efficacy of ore sorting technology at Aurumin's Sandstone deposits and Two Mile Hill in particular, ore sorting has been removed as an economic consideration in this evaluation.

### **Authorisation for release**

The Aurumin Board has authorised this announcement for release.

### **For further information please contact**

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### **Competent Person Statements**

The information in this announcement that relates to exploration results, data quality, geological interpretations and mineral resources for the Central Sandstone Project and Greater Sandstone Project were first released in the Company's announcements 16 December 2021, 25 March 2022, 28 April 2022, 2 May 2022, 9 June 2022, 21 June 2022, 11 July 2022, 11 August 2022, 26 August 2022, 5 September 2022, 12 September 2022 and 6 October 2022. The Company confirms that it is not aware of any new information or data that materially affects the information included in the announcements and confirms that all material assumptions and technical parameters underpinning the estimates in the relevant market announcements continue to apply and have not materially changed, except as updated in this announcement.

The information in this announcement that relates to exploration results and data quality for the Shillington (open pit) and Two Mile Hill (open pit and underground) deposits is based on information compiled by Peter Aldridge, a Competent Person who is a Member of the Australian Institute of Geoscientists and a full-time employee of Aurumin Limited. Mr Aldridge has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Aldridge consents to the inclusion in this announcement of the matters based on this information in the form and context in which it appears

The information in this announcement that relates to geological interpretations and Mineral Resource estimations for the Shillington (open pit) and Two Mile Hill (open pit and underground) deposits is based on information compiled by Graeme Bland, a Competent Person who is a Member of the Australian Institute of Geoscientists and a full-time employee of Aurumin Limited. Mr Bland has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Bland consents to the inclusion in this announcement of the matters based on this information in the form and context in which it appears

The information in this announcement that relates to exploration results, data quality, geological interpretations and mineral resources for the Johnson Range Project were first released in the Company's announcement dated 25 August 2021. The Company confirms that it is not aware of any new information or data that materially affects the information included in the announcement and confirms that all material assumptions and technical parameters underpinning the estimates in the relevant market announcement continue to apply and have not materially changed.

## About Aurumin Limited

Aurumin Limited is an ASX-listed mineral exploration company focused on two project areas in Western Australia.

The **Sandstone Gold Operations** were cornerstone by the acquisition of the **Central Sandstone Project** by the Company in early 2022.

- The **Central Sandstone Project** comprises an **881,300 ounce gold mineral resource** and significant project infrastructure that the Company aims to use to support a gold mining operation in the future.
- The Company's **Johnson Range Project** has a Mineral Resource of **64,700 ounces at a grade of 2.51g/t Au**, located midway between Southern Cross and Sandstone.

In addition to the Sandstone Gold Operations, the Company has a significant landholding at its **Southern Cross Operations**, including two historical high-grade production centres, Mt Dimer and Mt Palmer.

- The **Mt Dimer Project** produced over 125,000 ounces of gold from open pit and underground production of approximately 600,000 tonnes @ 6.4 g/t, and has a substantial tenure footprint.
- The historical **Mt Palmer Project** produced via open pit and underground methods, generating approximately 158,000 ounces of gold at an average grade of 15.9 g/t.

The Company is actively exploring its tenements and pursuing further acquisitions that complement its existing focus and create additional Shareholder value.

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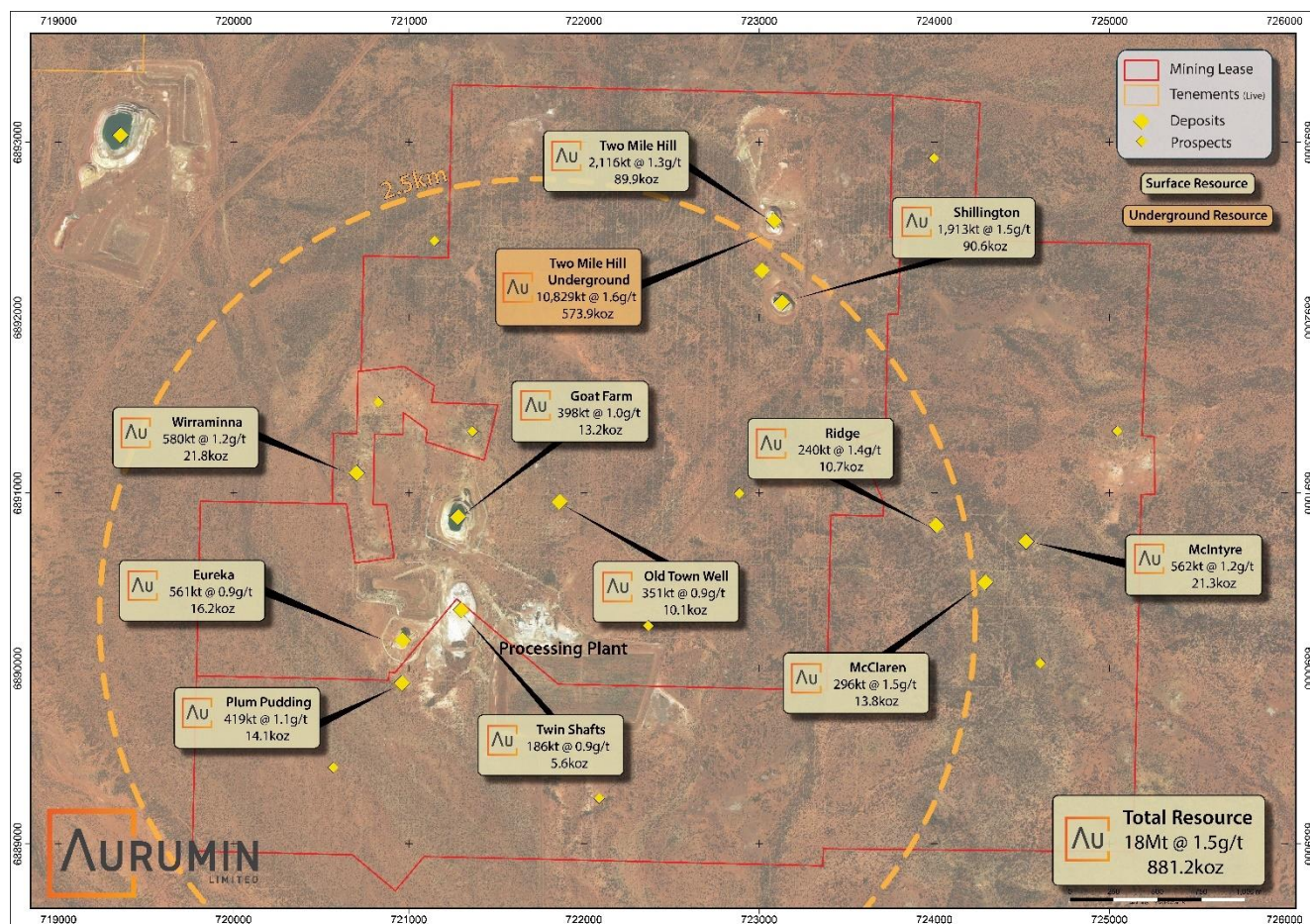
To keep abreast of the Company's latest announcements and developments available to investors please subscribe to our mailing list at <https://aurumin.com.au/contact/>.

## Previous ASX Announcements

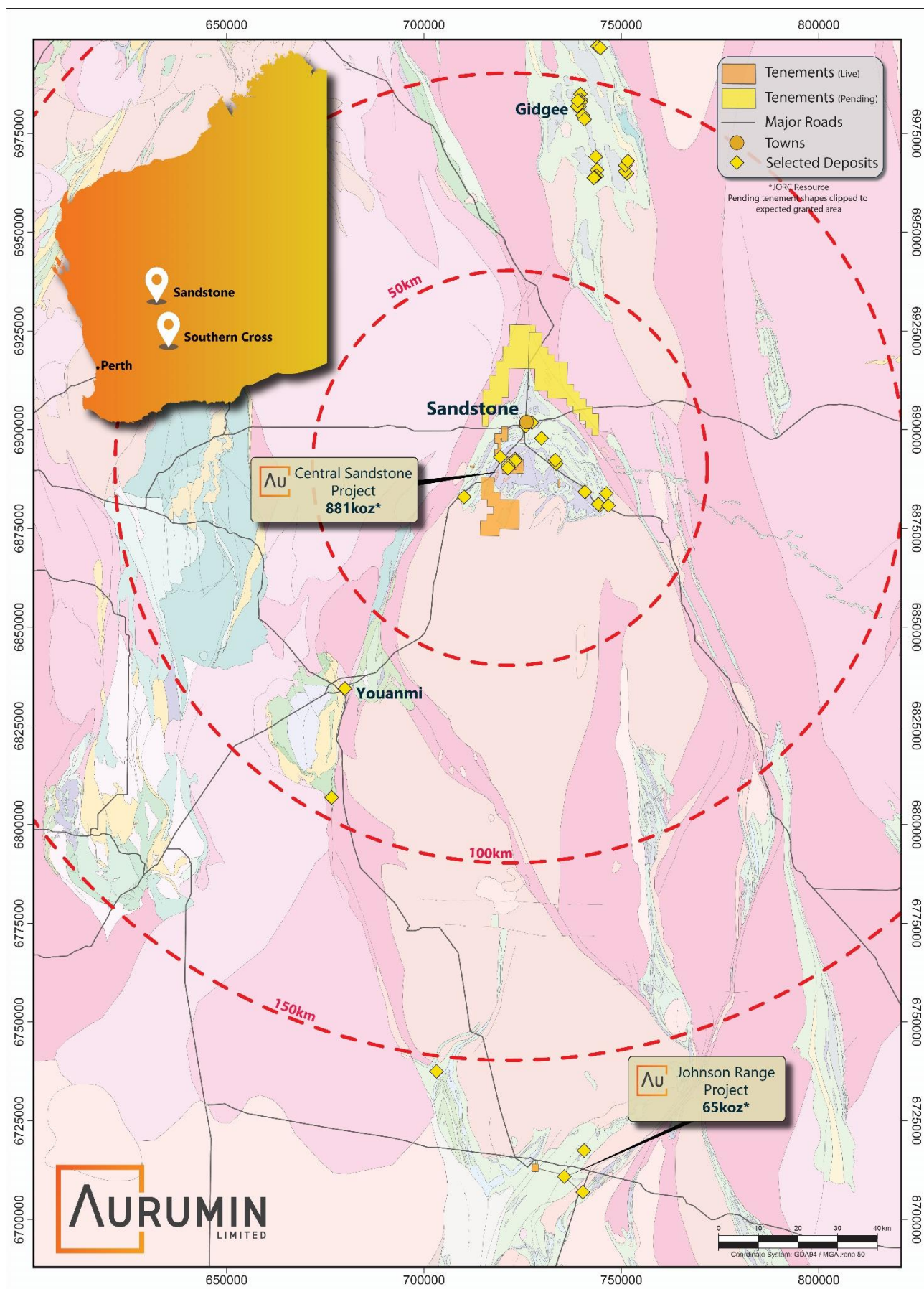
|   |            |  |
|---|------------|--|
| 1 | 15-Dec-21  | Aurumin To Acquire 784,000oz Au Sandstone Gold Project           |
| 2 | 25-Aug-21  | 64,700oz Johnson Range Mineral Resource Estimate                 |
| 3 | 11-Jul-22  | 344m @ 1.29g/t Au in first Aurumin Diamond Hole at Two Mile Hill |
| 4 | 11-Aug-22  | 224.0m @ 1.5g/t Au at Two Mile Hill from Second Hole Assayed     |
| 5 | 26-Aug-22  | Shillington RC Drill Results Returned                            |
| 6 | 05- Sep-22 | 352.8m @ 1.5g/t Au at Two Mile Hill, from Third Hole             |
| 7 | 12-Sep-22  | 242.7m @ 1.20g/t Au at Two Mile Hill, from final assays          |



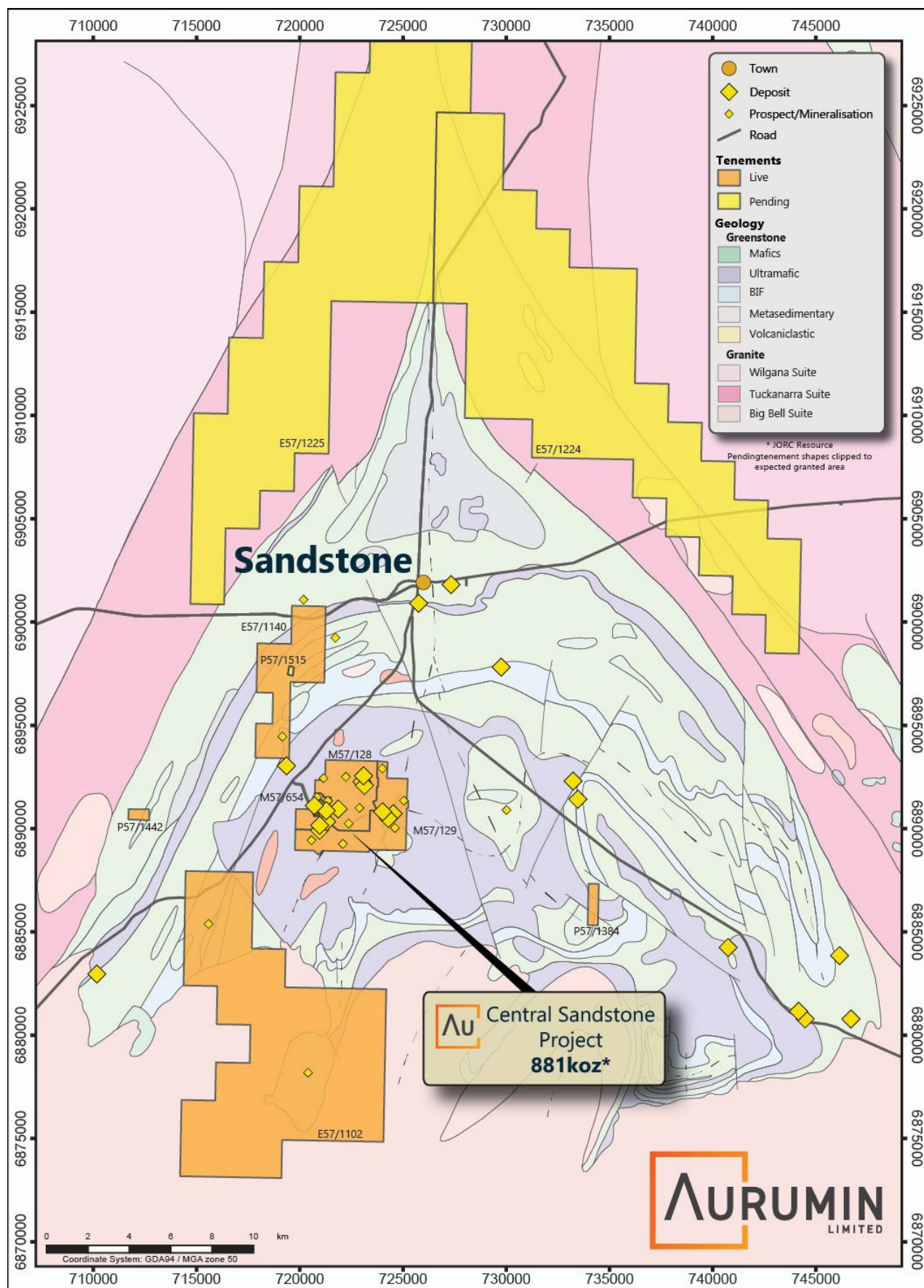
## Annexure A – Central Sandstone Project Map and Resources





**Annexure B – Sandstone Operations Location Map**


## Annexure C – Sandstone Region Project Map





## Annexure D – JORC Tables

### Sandstone Project Shillington and Two Mile Hill Resources

#### Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

| Criteria                   | JORC Code explanation  | Commentary  |
|----------------------------|--|---|
| <b>Sampling techniques</b> | <p><i>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg' reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</i></p> | <ul style="list-style-type: none"> <li>Sampling details, procedures and analytical results have been compiled from a number of sources for the historical drilling; a large portion of this information was captured and stored in the database at the time of work by the operators of the project at the time. Additionally, historical results and assays are generally found to be consistent with the more recent Aurumin (AUN) and Middle Island Resources (MDI) work, and to fit the overall geological model. This has allowed AUN to time use all results with equal confidence in the resource estimation work.</li> <li>A number of drilling methods have been used throughout the project's history including Reverse Circulation (RC), Diamond Drilling (DD), Air Core (AC), Rotary Air Blast (RAB), Auger Drilling (AG) and Vacuum (VC). See Section 2 for project history.</li> <li>Only RC and DD have been used for estimation.</li> </ul> <p><u>RC Drilling</u></p> <ul style="list-style-type: none"> <li>The vast majority of sampling at the deposits fall within this category.</li> <li>AUN RC drilling samples were collected as 1m intervals. The 1m samples were collected from a cone splitter via the cyclone directly into pre-numbered calico bags, creating a nominal 2.5kg sample. RC Sample rejects were also placed on the ground in sequence at 1m intervals to indicate metres drilled for the hole, for geological logging, and for composite sampling.</li> <li>Samples were subsequently collected as 1m intervals and 4m composites at the designation of the geologist onsite and submitted to ALS Laboratories in Perth for drying and pulverising to produce a nominal 50g charge for gold by fire assay analysis. Most samples were dry with some moisture present at depth in some holes.</li> <li>Composite samples were created using a PVC spear to collect sample from the reject 1m intervals. These were placed into pre-numbered calico bags. Where composite samples returned anomalous results, the initial 1m samples collected from the cone splitter were submitted for the interval.</li> <li>MDI RC drilling sampling was undertaken by collecting 2-3kg of RC chips from the drill rig's cone splitter at 1m intervals. Intervals of expected mineralisation were analysed at 1m intervals immediately. Other intervals were composited to 4m intervals from the 1m with a</li> </ul> |

| Criteria | JORC Code explanation | Commentary  |
|----------|-----------------------|---|
|          |                       | <p>single-tier riffle splitter. Where 4m composites returned assays greater than 0.2g/t Au, the 1m bulk samples were split down to 2-3kg sub-samples using a single-tier riffle splitter and submitted for analysis.</p> <ul style="list-style-type: none"> <li>Troy Resources (TRY) RC drilling, samples were passed directly from the in-line cyclone through a rig mounted multi-tier riffle splitter. Samples were collected in 1m intervals into bulk plastic bags and 1m calico splits. From the bulk sample, a 5m composite sample was collected using a split PVC scoop and then submitted to the laboratory for analysis. The 1m calico splits were submitted to the laboratory if the composite sample returned assay values equal to or greater than 0.2 g/t Au. In certain cases selected samples from some holes were passed from the cyclone through a rig mounted multi-tier riffle splitter, and samples collected into calico bags at 1m intervals were submitted directly for analyses. The remaining bulk sample was placed on the ground in 1m intervals.</li> <li>Herald Resources (HRL) sample collection during RC drilling was carried out over 1m intervals via a cyclone and riffle splitter. A mix of 5 1/4" and 5 3/8" bits were used. All dry RC samples were split at 1m intervals using a 3-tier riffle splitter, with the excess collected in plastic bags and left on-site. Wet samples were generally 'grabbed' and of a lesser quality.</li> </ul> <p><u>Diamond Drilling</u></p> <ul style="list-style-type: none"> <li>In all cases, after drilling, the core was placed for storage in labelled core trays. Core was then logged by a geologist and sampled. Sample lengths over the course of the project have varied from 0.1m to over 3m in places where no grade was expected.</li> <li>AUN diamond drilling (DD) samples are HQ, HQ3 or NQ2 core with sample intervals defined by the geologist to honour geological boundaries, ranging from 0.3 to 1.2m in length. DD core was aligned and measured by tape, comparing back to down hole core blocks consistent with industry practice. Core was sampled as either half core in HQ core, or as whole core in NQ2 core. Where whole core was sampled a maximum sample length of 0.6m was adhered to so as to keep sample size around 3kg and minimise reduction in sample volumes at larger particle sizes prior to pulverisation to 75 microns.</li> <li>Core samples were submitted at intervals defined by the geologist for drying and pulverising to produce a nominal 50g charge for gold by fire assay analysis. Core sample width was decided with relation to the width of the geological/mineralised features. Through areas of uniform mineralisation or sheet work/stockwork type veining samples were taken at a uniform interval 0.6 to 1.0m intervals. Visible gold was occasionally encountered in core. Where visible gold was observed a flush was passed through the core saw and a barren flush inserted</li> </ul> |

| Criteria                   | JORC Code explanation  | Commentary   |
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|                            |  | <p>in the sample sequence. Core was consistently sampled from the same side. All core was photographed within each core tray.</p> <ul style="list-style-type: none"> <li>MDI DD drilling was completed by various drilling contractors using a variety of drill rigs. HQ, NQ3, and NQ diamond core drilling was completed. The diamond drill core was sampled as half HQ and NQ core. For intervals selected for metallurgical test work, a quarter core sample was taken for assay, with the other quarter retained, and half-core submitted to a designated metallurgical laboratory. The diamond core was re-aligned prior to splitting and the right-hand side half core section was consistently sampled. The diamond core was cut by diamond saw and half core was left in the core trays for reference purposes. Half or quarter core samples were bagged in 1m intervals, or as per geological boundaries, with a minimum sample length of 0.2m and maximum 1.3m. All core was photographed within each core tray.</li> <li>HQ and NQ diamond core drilling was also completed by HRL and TRY.</li> <li>TRY diamond holes used triple tube coring due to the friable nature of the oxide zone lithologies being drilled. TRY core samples were marked on the core by the geologist according to geological intervals. The core was cut in half by TRY field technicians, with half being placed in a pre-numbered calico bag and the other half returned to the core tray. For duplicate samples the core to be submitted for analysis was quartered.</li> <li>HRL sampled half core, the core was sampled mostly in metre intervals however some varied in length according to alteration, mineralisation and lithological boundaries.</li> </ul> |
| <b>Drilling techniques</b> | <i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i> | <ul style="list-style-type: none"> <li>Only RC and DD drilling samples have been used estimation.</li> <li>Grade control data has been sighted and used for validation purposes</li> </ul> <p><u>RC Drilling</u></p> <ul style="list-style-type: none"> <li>RC drill testing and sampling has been the dominant method of exploration and resource definition at Shillington and Two Mile Hill.</li> <li>AUN RC Drilling was completed by JDC drilling of Southern Cross using a Hydco RC70 rig mounted on an 8x4 Mitsubishi truck with an onboard auxiliary air 1800 cfm by 700psi and a Hurricane 900x600 Hurricane booster. Drilling was conducted using a 5¼ inch face sampling hammer. Holes were surveyed downhole using an Axis Champ Gyro north seeking survey tool at 15m intervals.</li> <li>MDI RC holes were drilled with a variety of drilling companies and rigs. A 5¼ inch face sampling bit was used to collect 1m samples.</li> </ul>   |

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|                              |  | <ul style="list-style-type: none"> <li>RC holes drilled prior to this were drilled with a variety of drilling companies and rigs and used an unknown bit size to collect samples at 1m intervals. HRL notes that the majority of rigs used onsite were Schramm rigs.</li> </ul> <p><u>Diamond Drilling</u></p> <ul style="list-style-type: none"> <li>All DD has been surface drilling.</li> <li>AUN DD was completed by Terra Drilling Pty Ltd. using a KWL1600 diamond drill rig. Drilling used a combination of HQ2, HQ3 (triple tube) and NQ2 wireline techniques depending on the drilling circumstances. Core was routinely orientated using the Boart Longyear TRUCORE device. Diamond holes were surveyed using the Axis Champ north seeking gyro survey tool.</li> <li>MDI used DDH1 and Orlando Drilling to obtain HQ3 core (triple tube). TRY used Mt Magnet Drilling and HRL used Ausdrill and Bostech to collect core of an unknown diameter. Attempts were made to orientate core using a variety of techniques including modern orientation devices and a crayon marker spear tool.</li> </ul>   |
| <b>Drill sample recovery</b> | <p><i>Method of recording and assessing core and chip sample recoveries and results assessed.</i></p> <p><i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i></p> <p><i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i></p> | <p><u>RC Drilling</u></p> <ul style="list-style-type: none"> <li>AUN monitored recovery of RC drill cutting material via sample bag and reject pile size. Recoveries were considered adequate. The cyclone was regularly checked and cleaned. No issues with wet samples were recorded. Based on the sampling method and sample weight no bias in the sampling process has been identified.</li> <li>MDI recorded RC chip recovery for many of their drill programmes in a digital logging software package. Recovery was considered to be excellent with minor exceptions in some sheared/faulted intervals. Samples were at a consistent weight of 2–3 kg and consistently dry. In some isolated cases (&lt;1% of the MDI samples), wet samples were produced when faults/shear zones with higher water flows were intercepted. A limited amount of wet drilling is noted for previous operators of the project, representing less than 1% of the total sampling database. Wet RC sampling and potential downhole smearing does not appear to be an issue.</li> <li>No sample recovery information has been found for TRY or HRL drilling, however TRY reported that there were no known drilling, sampling or recovery factors that could materially impact the accuracy and reliability of the results.</li> </ul> <p><u>Diamond Drilling</u></p> <ul style="list-style-type: none"> <li>AUN Recovery of diamond drilling core was recorded by drillers on core blocks. This was checked and compared to the measurements of the core by the geologist. Areas of diamond core loss were marked on core blocks; all logging and sampling intervals honour intervals of core loss.</li> </ul> |



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|   |   | <ul style="list-style-type: none"> <li>Core recovery was reported by MDI as excellent. DD core was measured for each drill run and captured in a digital logging software package. Core recovery was reported as 94% on average. Some core loss was observed in softer ground in the oxide profile as well as in the case of cavities in the more competent transitional and fresh zones.</li> <li>There is no known relationship between recovery and grade in RC or DD sampling.</li> </ul>   |
| <b>Logging</b>  | <p><i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i></p> <p><i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. The total length and percentage of the relevant intersections logged.</i></p>  | <ul style="list-style-type: none"> <li>All RC and DD drilling was geologically logged by a qualified geologist at the time of drilling.</li> <li>RC and Diamond logging included, where practicable, but not is limited to lithology, alteration, mineralogy, vein quantification and description, and orientation information of selected geological or structural features</li> <li>All core was marked with depth, orientation lines, key geological logging and sample.</li> <li>Logging was qualitative in nature.</li> <li>Logged geology variation between project operators is considered to be within acceptable limits.</li> <li>Geotechnical logging has not been carried out.</li> <li>AUN considers the geological logging to be at a standard appropriate to support Mineral Resource estimation.</li> </ul>  |
| <b>Sub-sampling techniques and sample preparation</b> | <p><i>If core, whether cut or sawn and whether quarter, half or all core taken.</i></p> <p><i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i></p> <p><i>For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i></p> <p><i>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</i></p> <p><i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i></p> | <ul style="list-style-type: none"> <li>AUN RC drilling samples were collected as 1m intervals. The 1m samples were collected from a cone splitter via the cyclone directly into pre-numbered calico bags, creating a nominal 2.5kg sample. RC Sample rejects were also placed on the ground in sequence at 1m intervals to indicate metres drilled for the hole.</li> <li>Samples were subsequently collected as 1m intervals and 4m composites at the designation of the geologist onsite and submitted to ALS Laboratories in Perth for drying and pulverising to produce a nominal 50g charge for gold by fire assay analysis.</li> <li>The 4m composite samples were created using a PVC spear to collect sample from the reject 1m intervals. These were placed into pre-numbered calico bags. Where composite samples returned anomalous results, the initial 1m samples collected from the cone splitter were submitted for the interval.</li> <li>AUN diamond drilling (DD) samples are HQ, HQ3 or NQ2 core with sample intervals defined by the geologist to honour geological boundaries, ranging from 0.3 to 1.2m in length. DD core was aligned and measured by tape, comparing back to down hole core blocks consistent with industry practice. Core was sampled as either half core in HQ core, or as whole core in NQ2 core. Where whole core was sampled a maximum sample length of 0.6m was adhered to so as to keep sample size around 3kg and minimise reduction in</li> </ul> |

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|          |                       | <p>sample volumes at larger particle sizes prior to pulverisation to 75 microns.</p> <ul style="list-style-type: none"> <li>Core samples were submitted at intervals defined by the geologist for drying and pulverising to produce a nominal 50g charge for gold by fire assay analysis. Core sample width was decided with relation to the width of the geological/mineralised features. Through areas of uniform mineralisation or sheet work/stockwork type veining samples were taken at a uniform interval 0.6 to 1.0m intervals. Visible gold was occasionally encountered in core. Where visible gold was observed a flush was passed through the core saw and a barren flush inserted in the sample sequence. Core was consistently sampled from the same side. All core was photographed within each core tray.</li> <li>AUN inserted CRM standards at a rate of 1:20 while blanks were inserted at 1:50. Duplicates were collected at 1:20 as per Aurumin QAQC procedures using the same method of collection as the original samples. QC samples were assessed on a batch by batch basis and no major issues were found.</li> <li>MDI RC drilling sampling was undertaken by collecting 2-3kg of RC chips from the drill rig's cone splitter at 1m intervals. Intervals of expected mineralisation were analysed at 1m intervals immediately. Other intervals were composited to 4m intervals from the 1m with a single-tier riffle splitter. Where 4m composites returned assays greater than 0.2g/t Au, the 1m bulk samples were split down to 2-3kg sub-samples using a single-tier riffle splitter and submitted for analysis.</li> <li>MDI DD drilling was completed by various drilling contractors using a variety of drill rigs. HQ, NQ3, and NQ diamond core drilling was completed. The diamond drill core was sampled as half HQ and NQ core. For intervals selected for metallurgical test work, a quarter core sample was taken for assay, with the other quarter retained, and half-core submitted to a designated metallurgical laboratory. The diamond core was re-aligned prior to splitting and the right-hand side half core section was consistently sampled. The diamond core was cut by diamond saw and half core was left in the core trays for reference purposes. Half or quarter core samples were bagged in 1m intervals, or as per geological boundaries, with a minimum sample length of 0.2m and maximum 1.3m. All core was photographed within each core tray.</li> <li>MDI collected RC field duplicates at a rate of 1:18 samples and inserted CRMs at a rate of 1:9. A quartz flush was inserted after every batch processed. QAQC samples were assessed on a batch by batch basis. On several occasions during MDI's 2020 drilling programmes QC failures were detected. Re-assays of the affected standards and a sequence of 10 samples</li> </ul> |

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|          |                       | <p>straddling the QC failure were carried out in such cases.</p> <ul style="list-style-type: none"> <li>TRY RC drilling samples were passed directly from the in-line cyclone through a rig mounted multi-tier riffle splitter. Samples were collected in 1m intervals into bulk plastic bags and 1m calico splits. From the bulk sample, a 5m composite sample was collected using a split PVC scoop and then submitted to the laboratory for analysis. The 1m calico splits were submitted to the laboratory if the composite sample returned assay values equal to or greater than 0.2 g/t Au. In certain cases selected samples from some holes were passed from the cyclone through a rig mounted multi-tier riffle splitter, and samples collected into calico bags at 1m intervals were submitted directly for analyses. The remaining bulk sample was placed on the ground in 1m intervals.</li> <li>TRY diamond holes used triple tube coring due to the friable nature of the oxide zone lithologies being drilled. TRY core samples were marked on the core by the geologist according to geological intervals. The core was cut in half by TRY field technicians, with half being placed in a pre-numbered calico bag and the other half returned to the core tray. For duplicate samples the core to be submitted for analysis was quartered.</li> <li>TRY inserted a minimum of 1 CRM sample with each batch of samples for all exploration work. The actual standard used was dependant on the expected assay results and type of sample being taken (i.e. oxide, transitional or fresh rock). The grade of the standard used was also routinely varied. For RC and DD resource evaluation drilling an average of 1 field duplicate, 1 blank and 1 standard was submitted for every 50 samples. QC samples were inserted randomly throughout the sample sequence.</li> <li>TRY's exploration drilling results of QC samples were assessed by TRY on a batch by batch basis. Batches of samples where the results of the submitted standards differed from the expected value by more than 10% were re-analysed by the laboratory. A periodic audit of the exploration QC data was carried out by Data consultants Maxwell Geoservices (Maxwell).</li> <li>TRY's Resource definition drilling results of QC standards were assessed by TRY on a batch by batch basis. Where results of the submitted standards differed from the expected value by more than 10% samples were re-analysed by the laboratory. TRY had independent checking of all QC sample results carried out by Maxwell on a monthly basis. Maxwell monitored the laboratory performance over longer period and liaised with the laboratory TRY when QC problems were detected. Maxwell reported that all standards and blanks fall within the expected limits. The field duplicate results had 20 to 25% of the repeat samples are outside of +/- 10% compared to the original sample values with no</li> </ul> |

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|   |  | <p>apparent bias. This is to be expected given the style of mineralisation.</p> <ul style="list-style-type: none"> <li>HRL sample collection during RC drilling was carried out over 1m intervals via a cyclone and riffle splitter. A mix of 5 1/4" and 5 3/8" bits were used. All dry RC samples were split at 1m intervals using a 3 tier riffle splitter, with the excess collected in plastic bags and left on-site. Wet samples were generally 'grabbed' and of a lesser quality.</li> <li>HRL sampled half core, the core was sampled mostly in metre intervals however some varied in length according to alteration, mineralisation and lithological boundaries.</li> <li>Details surrounding the specifics of HRL QAQC protocols has not been found.</li> <li>To date there are no known drilling, sampling or recovery factors that could materially impact the accuracy and reliability of the results of samples.</li> <li>All sample sizes and sampling methodologies are appropriate to the grain size and style mineralisation being sampled.</li> </ul>   |
| <b>Quality of assay data and laboratory tests</b> | <p><i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i></p> <p><i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i></p> | <ul style="list-style-type: none"> <li>All AUN samples were submitted to ALS Laboratories for sample preparation and analysis. Sample preparation for drill samples involved drying the whole sample, pulverising to 85% passing 75 microns. A 50g sample charge was then used for the fire assay (AAS finish); the detection limit was 0.005ppm. A fire assay fusion-gravimetric analysis was used for gold analysis in samples that returned a greater than 100ppm result using the standard fire analysis technique. These methods are considered an estimation of total gold content. Where visible gold was observed a flush was passed through the core saw and a barren flush inserted in the sample sequence.</li> <li>MDI used a fire assay (FA) method with either an ICP-OES or an ICP-AAS finish for gold analysis. Analysis by Intertek was a 50g FA/ICP-OES, analysis by Nagrom was FA/ICP-OES by and Analysis by SGS was FA/AAS. Sample preparation was completed by Intertek, Nagrom and SGS laboratories. The samples were dried and crushed to -10mm before being split and a 300 g subsample pulverised to 95% passing 75 micron. This fraction was then split again to a 50 g sample charge for fire assay.</li> <li>TRY samples were assayed by SGS Australia Pty Ltd in Perth, Western Australia. The samples were dried and crushed to - 10mm before being split and a 300 g subsample pulverized to 95% passing 75 micron. This fraction was then split again to a 50 g sample charge for FA/AAS.</li> <li>HRL samples were sent to Analabs in Mt Magnet for 50g fire assay, however, the precise preparation procedure is not documented.</li> <li>All companies reported using QAQC procedures (see</li> </ul> |



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|  |  | <p>above). No bias has been reported and all assays are considered suitable for use in mineral estimation.</p> <ul style="list-style-type: none"> <li>No geophysical tools were used in determining element concentrations.</li> </ul>  |
| <b>Verification of sampling and assaying</b> | <p><i>The verification of significant intersections by either independent or alternative company personnel.</i></p> <p><i>The use of twinned holes.</i></p> <p><i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i></p> <p><i>Discuss any adjustment to assay data.</i></p> | <ul style="list-style-type: none"> <li>Significant intersections are part of a data set that include multiple holes and drilling from multiple previous operators. There is no indication that any single data set is not in line with other datasets. Specific twinned holes have not been drilled.</li> <li>AUN acquired a Microsoft SQL Server based database for MDI upon purchase of the project. This database was originally compiled by Troy Resources using historical, more localised, databases from both TRY and HRL work. The SQL data is stored in a modified legacy Gbis / Geobank schema.</li> <li>Geological data consultants Expedio Services Pty Ltd (Expedio) built and supported the original database on behalf of TRY before handing over the database for TRY to self-manage. Subsequent to TRY's work, Expedio has managed the database for MDI and AUN.</li> <li>The continuity of ownership and management of the database gives confidence in the integrity of the data.</li> <li>All sampling and assay data are stored in a secure database with restricted access.</li> <li>All data is stored by Expedio and backed up to a cloud-based storage system.</li> <li>In September 2022 Expedio conducted an audit of drillhole samples and assay results whilst improving database validation techniques. The database had originally allowed duplicate SampleIDs; previous workflows for the assay loading process included some safeguard measures to prevent a mix-up of results, but the process was not foolproof. Expedio determined there was no mix-up of assay results during this process, made several duplicated SampleIDs unique by adding a suffix before enforcing greater database integrity through a unique SampleID key constraint on the sample table.</li> <li>Both AUN and MDI collected field data by logging and validating directly into a customised field logging tool (OCRIS). This allows the capture of accurate data and easy migration of the data into the database.</li> <li>AUN has records of many of the original TRY and HRL drilling and logging sheets. In records checked, no major discrepancies have been found.</li> <li>Significant intersections are part of a data set that include multiple holes and drilling from multiple previous operators. There is no indication that any single data set is not in line with other datasets. Specific twinned holes have not been drilled.</li> </ul> |

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| <b>Location of data points</b> | <p><i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i></p> <p><i>Specification of the grid system used.</i></p> <p><i>Quality and adequacy of topographic control.</i></p> | <ul style="list-style-type: none"> <li>No adjustment to assay values has been completed.</li> <li>Two local grids were used historically at Two Mile Hill and Shillington by HRL and TRY. AUN has received the transformation parameters contemporaneously used for these grids. AUN had Mine Survey Plus complete a review of the grid transformations and create an independent transformation from local grid to MGA94, zone 50. Results are within error and the historical survey work is considered to be of good quality.</li> <li>TRY moved away from using local coordinates and moved to AMG84, zone 50. MDI and Aurumin have used MGA94, zone 50.</li> <li>AUN Drill collars were located using a Differential GPS by Mine Survey Plus. Accuracy is sub 10cm. The grid system used is GDA94/MGA94 Zone 50.</li> <li>All MDI holes were surveyed using a DGPS system by either a contract surveyor or prior to 2020, trained MDI staff. MDI also completed a programme of resurveying historical holes onsite with a DGPS and concluded survey control was accurate.</li> <li>Prior to MDI's work specific information to collar survey methods are not uniformly recorded. TRY and HRL make reference to surveying collar locations and routinely had surveyors onsite. This, coupled with MDI's resurveying programme allows for confidence in collar locations.</li> <li>During AUN's resource work, seven holes were found with incorrect RL values. The collars for these holes were corrected to a topographic surface appropriate for the time they were drilled.</li> <li>All AUN holes were downhole surveyed using an Axis Champ Gyro north seeking survey tool at 15m intervals. Core was routinely orientated using the Boart Longyear TRUCORE device.</li> <li>Not all holes were surveyed downhole prior to AUN taking control of the project. For the more recent drilling programmes since 2020 the majority of holes were downhole surveyed utilizing Gyro tools – Reflex and Axis Champ instruments at 10–25 m intervals.</li> <li>MDI diamond drillholes were surveyed by gyro survey instruments at 10- 20m increments. Prior to 2020 most MDI RC drilling was surveyed by a downhole camera tool, with adjustments made for magnetic intensity where readings were out of specification for the tool.</li> <li>Holes prior to MDI are variably surveyed, both TRY and HRL recorded the use of single shot surveys. Many of these holes have also had downhole surveys adjusted for high magnetic readings within the BIF, although the method of shot and magnetic intensity has not been recorded in the database. Some historical RC drilling is surveyed only for dip with no change or precision noted</li> </ul> |

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|                                      |   | <p>for the azimuth.</p> <ul style="list-style-type: none"> <li>The incomplete downhole survey data was highlighted by the Mineral Resources consultants (ERGM and Ashmore) as a potential material issue. During 2020, an effort was made to survey all drilled non-vertical holes where practicable.</li> <li>With most of all drilling by MDI being completed in 2020, and AUN in 2022 using north seeking gyros the percentage of surveyed drill holes has greatly improved.</li> <li>The survey data is considered sufficiently robust to estimate mineral resources.</li> <li>The difference between magnetic north (MN) and true north (TN) is 0.53°. The difference between TN and GDA is 1.07°.</li> <li>All resource work has been completed in MGA94 zone 50.</li> </ul>   |
| <b>Data spacing and distribution</b> | <p><i>Data spacing for reporting of Exploration Results.</i></p> <p><i>Whether the data spacing, and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i></p> <p><i>Whether sample compositing has been applied.</i></p> | <p><u>Shillington</u></p> <ul style="list-style-type: none"> <li>The majority of drilling profiles were oriented across the strike of the mineralised body at a bearing of 236° with a dip of -60° to best test the orientation of the mineralisation.</li> <li>Several of the earlier exploration holes are orientated at different azimuths to the normal grid; these are a minority of holes.</li> <li>Diamond holes are orientated at varying angles depending on the structures and/or mineralisation they were specifically targeting.</li> <li>Data spacing of holes reported is variable. Almost all of the deposit is drilled with collar spacings of at least 20x20m. Much of the deposit is drilled to a greater resolution and wider spacings occur on the peripheries away from the area of estimation.</li> <li>The drilling density is considered sufficient for an Indicated and Inferred Mineral Resource.</li> <li>Samples were composited to 1m prior to estimation</li> </ul> <p><u>Two Mile Hill</u></p> <ul style="list-style-type: none"> <li>The majority of drilling profiles were oriented across the strike of the mineralised body at a bearing of 270° or 090° with a dip of -60° to best test the orientation of the mineralisation. A number of earlier drillholes are drilled vertically.</li> <li>Several of the earlier exploration holes are orientated at different azimuths to the normal grid; these are a minority of holes.</li> <li>Diamond holes are orientated at varying angles depending on the structures and/or mineralisation they were specifically targeting.</li> </ul> |

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|  |   | <ul style="list-style-type: none"> <li>Data spacing of holes reported is variable. Almost all of the upper part of the deposit is drilled with collar spacings of at least 20x20m. Much of the deposit is drilled to a greater resolution and wider spacings occur on the peripheries away from the area of estimation.</li> <li>The drilling density is considered sufficient for Indicated and Inferred Mineral Resources.</li> <li>Samples use for the tonalite estimation were composited to 3m. Sample used in the non-tonalite sections used 1m composites.</li> </ul>  |
| <b>Orientation of data in relation to geological structure</b> | <p><i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i></p> | <p><u>Shillington</u></p> <ul style="list-style-type: none"> <li>At Shillington the mineralisation is modelled as broadly bedding conformable although local heterogeneities exist due to the folded and deformed nature of the stratigraphy.</li> <li>The orientation of drilling is generally on a high angle to the dominant stratigraphic control bedding in BIF (~dipping 35° towards 052°)</li> <li>No sampling bias from the orientation of the drilling is believed to exist</li> </ul> <p><u>Two Mile Hill</u></p> <ul style="list-style-type: none"> <li>At Two Mile Hill mineralisation in the tonalite body occurs within shallowly dipping sheeted vein sets oriented approximately orthogonal to the orientation of the of the tonalite intrusive that dips ~78° towards 281°.</li> <li>Structural measurements on drill core in the tonalite show a range of orientations. However the contoured mean of mineralised veins (&gt;1g/t Au) shows a plane to the mean of the poles dipping 29° towards 049°</li> <li>The orientation of drilling is generally on a high angle to the dominant vein set and the dominant stratigraphy, banded iron formation ~dipping 35° towards 052°).</li> <li>No sampling bias from the orientation of the drilling is believed to exist.</li> </ul> |
| <b>Sample security</b>   | <p><i>The measures taken to ensure sample security.</i></p>   | <ul style="list-style-type: none"> <li>All AUN samples were collected and stored onsite in a secure location before being transported to Perth by consignment in sealed bags. Upon receipt by the laboratory Sample IDs and total number of samples were checked, a sample receipt was issued and AUN was notified of any discrepancies. Results were sent to Aurumin personnel by the assay laboratory.</li> <li>MDI Chain of custody was managed by MDI geological personnel. Samples were stored on site until collected for transport to the laboratory in Perth WA. MDI personnel had no contact with the samples once they are picked up for transport. Tracking sheets were set up to track the progress of samples.</li> <li>TRY samples were placed in a labelled and tied calico bag. After wet samples had been dried, six bags were</li> </ul>  |



| Criteria                 | JORC Code explanation  | Commentary  |
|--------------------------|--|---|
|                          |  | <p>placed in a larger plastic polyweave bag that was labelled with the laboratory address and sender details and tied with wire. Samples were dispatched three times per week. On each occasion, a sample submission form was completed which listed the sample IDs, the total number of samples and analyses to be conducted. This form was faxed to the laboratory and to the database technician in TRY's Perth office. Samples were picked up by a courier firm, who counted the total number of polyweave bags before taking them to the Mt Magnet depot 250km to the west of Sandstone. Here the samples were picked up by the courier's road train and taken to the Perth depot before being dispatched to the lab. Upon receipt of the samples, the lab checked the sample IDs and total number of samples and notified TRY of any differences from the sample submission form. After the analysis of the samples was completed, results were sent to the senior geologist and database technician in both digital and paper format.</p> <ul style="list-style-type: none"> <li>Chain of custody and sample security is not documented by earlier explorers.</li> </ul> |
| <b>Audits or reviews</b> | <i>The results of any audits or reviews of sampling techniques and data.</i> | <ul style="list-style-type: none"> <li>AUN has reviewed sampling procedures and associated QAQC data as part of the mineral estimation process. No fatal flaws were noted, and it is believed that industry standard practices have been adhered to throughout the project life.</li> <li>Expedio audited the database for sample mix-up errors (described above) and found no issues.</li> </ul>   |

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

| Criteria                                       | JORC Code explanation   | Commentary   |
|--|---|--|
| <b>Mineral tenement and land tenure status</b> | <p><i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i></p> <p><i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</i></p> | <ul style="list-style-type: none"> <li>The Sandstone Projects are located on granted tenements M57/128, M57/129, M57/654, E57/1140, E57/1102, P57/1442, and P57/1384.</li> <li>Resources reported are on M57/128.</li> <li>These tenements are wholly owned by Aurumin.</li> <li>The project is located in the Sandstone Shire, centred approximately 10 kilometres south of the Town of Sandstone.</li> <li>The historical town site of Nungarra is located on M57/128 but does not impede or encroach on any known resources.</li> <li>No impediments are known at the time of reporting.</li> </ul> |

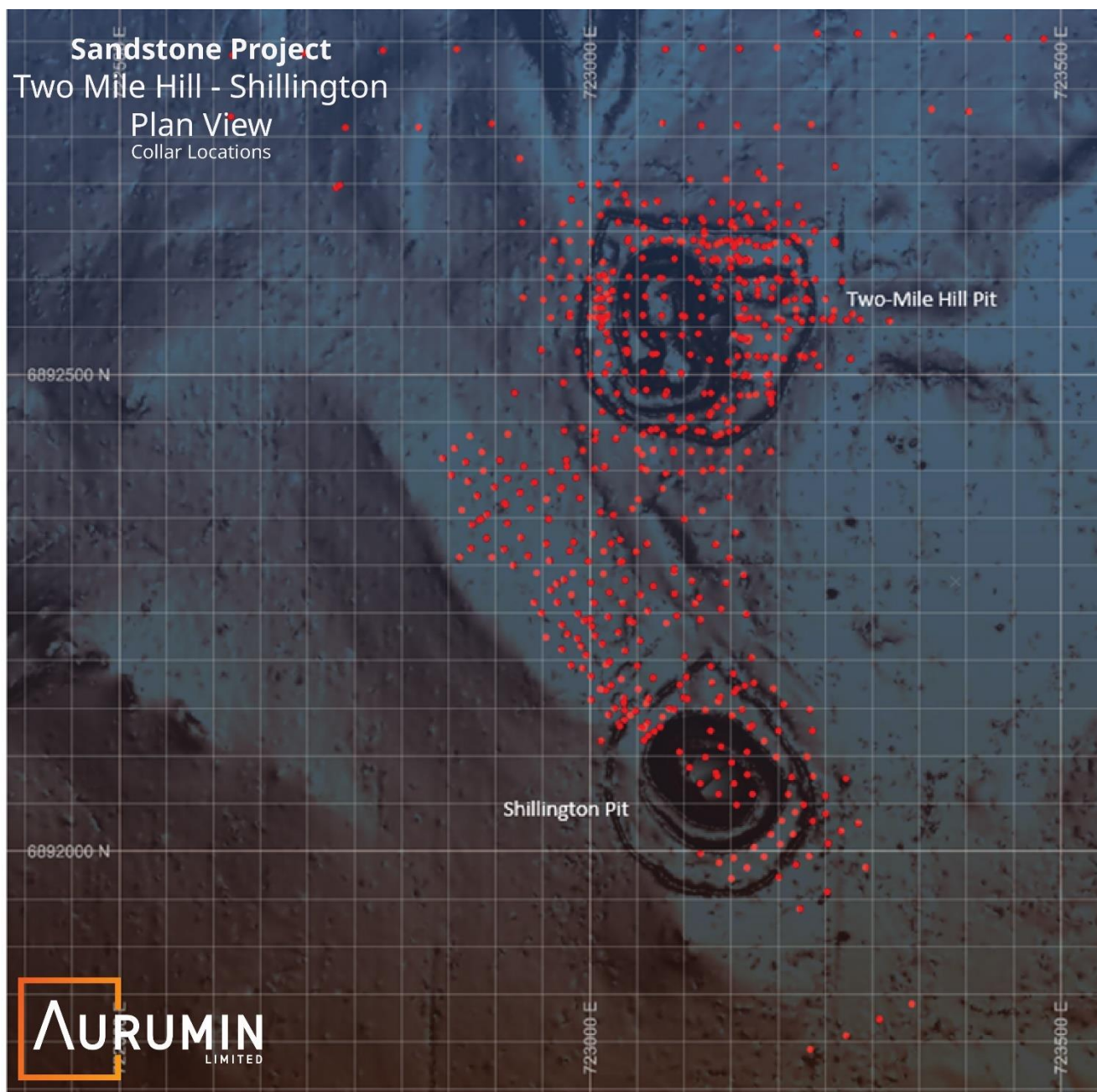
| Criteria                                 | JORC Code explanation  | Commentary   |
|--|--|--|
| <b>Exploration done by other parties</b> | <i>Acknowledgment and appraisal of exploration by other parties.</i> | <ul style="list-style-type: none"> <li>Gold exploration in the Sandstone area has occurred since the late 1800s</li> <li>Modern production commenced in 1993 from laterite material. Subsequently, in 1994, HRL constructed a CIP processing plant and began open pit mining.</li> <li>TRY acquired the project in 1999 and mining continued at various deposits until 2010</li> <li>MDI acquired the project in 2016 and completed substantial exploration drilling, resource drilling and mining pre-feasibility work.</li> <li>AUN acquired the project in 2022 and has started exploration and mineral resource estimation.</li> </ul>   |
| <b>Geology</b>                           | Deposit type, geological setting and style of mineralisation.        | <ul style="list-style-type: none"> <li>Shillington and Two Mile Hill are located within the Sandstone Greenstone Belt (SSGB).</li> <li>The SSGB is a triangular shaped Archean greenstone belt located towards the northern end of the Southern Cross Province, the central spine of the Archean Yilgarn Block. The SSGB sits at the northern end of the Diemals Dome, at the juncture of the Youanmi Fault and Edale Fault, two major trans-cratonic faults which bound the west and east sides of the belt respectively.</li> <li>The southern half and core of the belt, dominated by ultramafic and high magnesian mafic volcanics with numerous interflows of oxide-facies Banded Iron Formation ("BIF"). Along the southern margin of the belt these rocks are in direct contact with the Diemals Dome.</li> <li>The northern part and flanks of the belt, dominated by mafic volcanics and syn-volcanic mafic sills, BIF interflow units are common. Ultramafic volcanics and/or intrusives are rare. • Siliciclastic sediments other than BIF are restricted to a small tear drop-shaped basin at the northern apex of the belt. A variety of felsic rocks intrude the greenstones, ranging from granite, granodiorite, to various quartz-eye and feldspar-phyric porphyries.</li> <li>Deposits of the SSGB exhibit strong structural controls indicative of sub-horizontal east-west compression hosted by major shear zones at the intersection of two regional shear zones.</li> <li>High-grade gold mineralisation in SSGB deposits is associated with thin quartz veins, stacked or sheeted quartz vein arrays, or stockworks.</li> <li>Mineralisation is generally 'free' gold within quartz veins, with only refractory ore, hosted by sulfidic shale recorded at Bell Chambers.</li> <li>Gold has been mined from all stratigraphic domains and most lithological units of the SSGB.</li> </ul> <p><u>Shillington</u></p> <ul style="list-style-type: none"> <li>Gold mineralisation at Shillington is associated with zones of brecciation and quartz veining within a series of</li> </ul> |

| Criteria                        | JORC Code explanation   | Commentary   |
|---------------------------------|---|--|
|                                 |   | <p>stacked, northwest trending and shallow northeast dipping banded iron formation (BIF) units. The BIF units are hosted within a sequence of tholeiitic and komatiitic basalts, with minor sediment and chert. Intensive folding is evident at all scales of observation in the Shillington BIF, parasitic folds are common as is tight, recumbent, isoclinal folding. The general bedding planes observed in the Shillington BIF are mostly orientated northwest - southeast and west northwest – east southeast with a moderate easterly dip. The BIF hosting mineralisation comprises an upper and middle unit and is about 45m thick, thought to be tapering to 25m thick towards the Two Mile Hill tonalite contact. Mineralisation is modelled as semi continuous lenses within the Shillington BIF package</p> <p><u>Two Mile Hill</u></p> <ul style="list-style-type: none"> <li>The mineralisation at Two Mile Hill is hosted in three geological domains. The majority of the Two Mile Hill resource occurs within a tonalite intrusion. Mineralisation also occurs within banded iron formation (BIF) beds, and within the basalts that host the tonalite intrusion. The tonalite intrusion is approximately oblate in plan, dipping ~78° towards 281°. Tonalite hosted mineralisation occurs predominantly as fine free gold within a sheeted/stockwork quartz vein array.</li> </ul> |
| <b>Drill hole Information</b>   | <p><i>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:</i></p> <p><i>easting and northing of the drill hole collar</i></p> <p><i>elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</i></p> <p><i>dip and azimuth of the hole</i></p> <p><i>down hole length and</i></p> <p><i>interception depth</i></p> <p><i>hole length.</i></p> <p><i>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</i></p> | <ul style="list-style-type: none"> <li>A plan of drill hole locations for holes used in estimation is available at the end of section 2 and in the document.</li> <li>All relevant drill hole information has been released previously. Please refer to AUN ASX Announcements released on:             <ul style="list-style-type: none"> <li>16<sup>th</sup> December 2021,</li> <li>11<sup>th</sup> July 2022,</li> <li>11<sup>th</sup> August 2022,</li> <li>26<sup>th</sup> August 2022,</li> <li>5<sup>th</sup> September 2022 and,</li> <li>12<sup>th</sup> September 2022</li> </ul> </li> </ul>  |
| <b>Data aggregation methods</b> | <p><i>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should</i></p>   | <ul style="list-style-type: none"> <li>Not applicable for reporting of Mineral Resources.</li> <li>No metal equivalents have been used.</li> </ul>   |

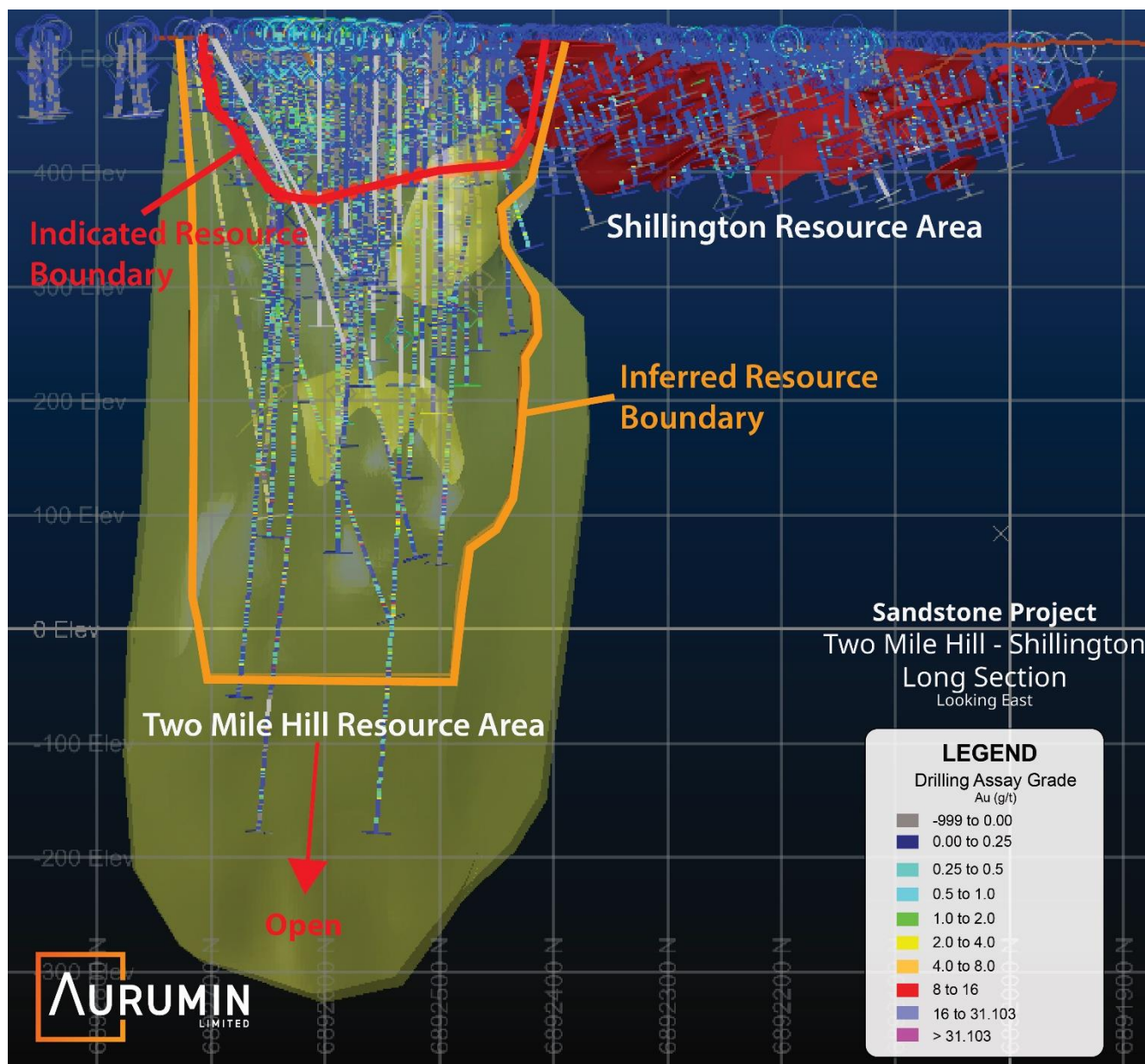
| Criteria  | JORC Code explanation  | Commentary   |
|---|--|--|
|   | <p>be stated.</p> <p>Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</p> <p>The assumptions used for any reporting of metal equivalent values should be clearly stated.</p> |  |
| <b>Relationship between mineralisation widths and intercept lengths</b> | <p>These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').</p> | <p><u>Shillington</u></p> <ul style="list-style-type: none"> <li>The majority of holes were drilled perpendicular to bedding in order to orthogonally intercept the BIF units. As such the majority of reported mineralised intercepts are effectively true widths.</li> </ul> <p><u>Two Mile Hill</u></p> <ul style="list-style-type: none"> <li>The majority of holes were drilled perpendicular to the long axis of the tonalite body in order to orthogonally intercept both the BIF units in the hanging wall and the dominant vein orientation within the tonalite. As such the majority of reported mineralised intercepts are effectively true widths.</li> <li>Gold mineralisation within the vertically oriented Two Mile Hill tonalite intrusive is associated with sub-horizontal quartz veins. The drilling is therefore oriented to ensure both adequate definition the tonalite contacts and an optimum angle of intersection on the mineralised quartz veins.</li> </ul> |
| <b>Diagrams</b>   | <p>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</p>  | <ul style="list-style-type: none"> <li>Plan views and long sections of the resources are attached in the body of the text and at the end of Section 2.</li> </ul>  |
| <b>Balanced reporting</b>   | <p>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</p>   | <ul style="list-style-type: none"> <li>Not applicable for reporting of mineral resources.</li> </ul>   |
| <b>Other substantive exploration data</b>                               | <p>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey</p>  | <ul style="list-style-type: none"> <li>No other information is considered material for this presentation.</li> </ul>   |

| Criteria            | JORC Code explanation   | Commentary   |
|---------------------|---|--|
|                     | <p>results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</p>   |  |
| <b>Further work</b> | <p>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</p> | <ul style="list-style-type: none"> <li>• Further extensional and definition drilling in both the Shillington and Two Mile Hill resource 2022/23 financial year.</li> <li>• Re-logging of historical diamond drill holes to standardise vein frequency and type.</li> <li>• Additional density data from historical and new drilling recommended.</li> <li>• Open pit and underground optimisations and assessments.</li> </ul> |





*Plan View of Drillhole collars used in the Shillington and Two Mile Hill resource models*



Long-section of drillholes used and modelled mineralisation, for both the Shillington and Two Mile Hill resource areas.  
Section facing East.

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

| Criteria                         | JORC Code explanation   | Commentary  |
|----------------------------------|---|---|
| <b>Database integrity</b>        | <i>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. Data validation procedures used.</i> | <ul style="list-style-type: none"> <li>The historical database and current database were validated and audited by Expedio database consultants. Expedio manage the current database on behalf of AUN.</li> <li>All geological and field data is currently entered using data-loggers and software developed by OCRIS, that includes lookup tables and fixed formatting (and protected from modification) thus only allowing data to be entered using the AUN geological code system and sample protocol.</li> <li>Historical logging was carried out according to MDI, HRL and TRYs internal protocols at the time of drilling.</li> <li>The database is yet to be fully rationalised and therefore the different logging schemes persist in the database to a limited extent.</li> <li>Data is loaded and managed by independent database consultants, Expedio.</li> <li>Checks between the current database and the original logging spreadsheets and assay certificates have been completed. No material discrepancies have been found.</li> <li>AUN technical personnel validated the database using Datamine software.</li> <li>Following importation the data goes through a series of digital checks for duplication and non-conformity, followed by validation by the relevant project geologist who manually checks the collar, survey, assay and geology for errors against the original field data and final paper copies of the assays.</li> <li>Drill holes that are missing critical information have been excluded from work.</li> <li>Data has been checked for: <ul style="list-style-type: none"> <li>Overlapping sample intervals</li> <li>Duplicate Hole IDs</li> <li>Duplicate Sample IDs</li> <li>Duplicate/erroneous collar locations</li> </ul> </li> </ul> |
| <b>Site visits</b>               | <i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.<br/>If no site visits have been undertaken indicate why this is the case.</i>   | <ul style="list-style-type: none"> <li>The competent person has undertaken multiple site visits to the Sandstone Gold Project which included extensive time at the Shillington and Two Mile Hill resource area.</li> </ul>  |
| <b>Geological interpretation</b> | <i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i>  | <ul style="list-style-type: none"> <li>The geological interpretation of the Shillington and Two Mile Hill complex was carried out using a systematic approach to ensure continuity of the geology and estimated mineral resource. All wireframes were</li> </ul>  |

| Criteria                                   | JORC Code explanation  | Commentary  |
|--|--|---|
|  | <p><i>Nature of the data used and of any assumptions made.</i></p> <p><i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i></p> <p><i>The use of geology in guiding and controlling Mineral Resource estimation.</i></p> <p><i>The factors affecting continuity both of grade and geology.</i></p> | <p>constructed using geological guided implicit modelling techniques in Datamine RM software on approximately 20m spacing sections. Checks were made to ensure that the wireframed volume agreed with the true ore widths of drillhole intersections. There is a medium to high level of confidence in the geological interpretation and this due to the lack of confidence in the historical drilling</p> <ul style="list-style-type: none"> <li>Validated RC and DD drillholes have been utilised in the creation of the wireframes.</li> <li>The confidence in the geological interpretation is considered high, based on the majority of the resource area being drill tested to at least 20m by 20m drill spacing and knowledge gained through mining by previous operators.</li> <li>All available geological data was used in the interpretation including mapping, drill hole logs and previous interpretations.</li> <li>No alternative interpretations were completed for either the Shillington or Two Mile Hill resource areas</li> <li>Geological controls and relationships are used to define and orientate mineralised domains. A 0.5g/t Au was also used as a guide to model the mineralised envelopes for the resources.</li> <li>On a deposit scale the primary gold mineralisation at Shillington is hosted in a folded banded iron formation (BIF) dipping moderately towards the North-East. A shallow weathering profile especially around the BIF units had resulted in significant mineralisation occurring above fresh rock.</li> <li>On a deposit scale the primary coarse gold mineralisation at Two Mile Hill is hosted by a package of sheeted flat lying narrow quartz vein in a tonalite plug. Grade can be modelled across vein packages.</li> </ul> |
| <b>Dimensions</b>                          | <p><i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i></p>   | <ul style="list-style-type: none"> <li>The mineralised portion of the Shillington resource extend over 650m strike and 60m width, up to a depth of 140m.</li> <li>Primary mineralisation at Shillington strikes 320 degrees (NW)</li> <li>The primary mineralised portion of the Two Mile Hill Tonalite resource extend over 400m strike and 100m width, up to a depth of 725m. A broad laterite blanket is also evident over a significant portion of the deposit and can measure up to 5</li> </ul>   |
| <b>Estimation and modelling techniques</b> | <p><i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and</i></p>  | <ul style="list-style-type: none"> <li>Geological modelling using hanging wall and footwall points derived from the drill hole database were used to create both geological and mineralisation wireframes utilising the Datamine RM implicit modelling module in a sectional environment.</li> <li>These wireframes showed a strong correlation between</li> </ul>  |



| Criteria | JORC Code explanation  | Commentary   |
|----------|--|--|
|          | <p><i>maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i></p> <p><i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i></p> <p><i>The assumptions made regarding recovery of by-products.</i></p> <p><i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i></p> <p><i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i></p> <p><i>Any assumptions behind modelling of selective mining units.</i></p> <p><i>Any assumptions about correlation between variables.</i></p> <p><i>Description of how the geological interpretation was used to control the resource estimates.</i></p> <p><i>Discussion of basis for using or not using grade cutting or capping.</i></p> <p><i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i></p> | <p>the modelled mineralised domain and interpreted geology.</p> <ul style="list-style-type: none"> <li>• A statistical analysis using Snowden's Supervisor software was undertaken to determine the appropriate composite length and grade outliers with each domain and determine appropriate top cut values.</li> <li>• The Top cutting strategy used and applied includes:             <ul style="list-style-type: none"> <li>- Disintegration analysis of log Histogram</li> <li>- Log probability plot, histogram data and coefficient of variation</li> <li>- Outlier analysis: removal of outliers and</li> <li>- analysis of impact on the CV of domain.</li> </ul> </li> <li>• Top cuts were applied to the composite data, before any estimate was conducted</li> <li>• Variogram modelling was completed with Snowden's Supervisor software, with good correlation between those directions and geological observations. The parameters determined from this analysis were used in the interpolation process.</li> <li>• Search distances used for estimation is based on variogram ranges and vary by domain.</li> <li>• Ordinary Kriging, inverse distance (ID1.5 and ID2) and Nearest Neighbour block estimation techniques employed on all domains using Datamine RM software.</li> <li>• Estimation to sub-cells was employed.</li> <li>• No assumptions have been made with respect to the recovery of by-products.</li> <li>• No estimate of deleterious elements has been done on this deposit.</li> <li>• No assumptions were made on selective mining units.</li> <li>• No assumptions have been made.</li> </ul> <p><u>Shillington</u></p> <ul style="list-style-type: none"> <li>• For the Shillington resource area, ordinary kriging and Inverse Distance estimation methods used a 1m composite, while the Nearest Neighbour uses a seam composite.</li> <li>• A three pass search strategy was employed for all estimated domains use the Shillington search parameters below. After these passes, un-estimated blocks area assigned a nearest neighbour estimate value.</li> <li>• Shillington Search Parameters:</li> </ul> |

## Criteria

JORC Code  
explanation

## Commentary

|        | Domain | Rotation |    |      | Search Range |      |      | Min Samples | Max Samples | Max Samples /drillhole | Octant Search |         |         |
|--------|--------|----------|----|------|--------------|------|------|-------------|-------------|------------------------|---------------|---------|---------|
|        |        | Z        | X  | Z    | X            | Y    | Z    |             |             |                        | No. Octants   | Min Sam | Max Sam |
| Pass 1 | 1      | 55       | 30 | -40  | 17.5         | 13   | 12.5 | 12          | 24          | 3                      | NA            |         |         |
|        | 2      | 70       | 55 | -45  | 15           | 7.5  | 7.5  |             |             |                        |               |         |         |
|        | 3      | -140     | 40 | -90  | 12.5         | 12.5 | 12.5 |             |             |                        |               |         |         |
|        | 4      | 0        | 0  | -120 | 12.5         | 10   | 12.5 |             |             |                        |               |         |         |
| Pass 2 | 1      | 55       | 30 | -40  | 35           | 26   | 25   | 12          | 24          | 3                      | NA            |         |         |
|        | 2      | 70       | 55 | -45  | 30           | 15   | 15   |             |             |                        |               |         |         |
|        | 3      | -140     | 40 | -90  | 25           | 25   | 25   |             |             |                        |               |         |         |
|        | 4      | 0        | 0  | -120 | 25           | 20   | 25   |             |             |                        |               |         |         |
| Pass 3 | 1      | 55       | 30 | -40  | 70           | 52   | 50   | 5           | 24          | 3                      | NA            |         |         |
|        | 2      | 70       | 55 | -45  | 60           | 30   | 30   |             |             |                        |               |         |         |
|        | 3      | -140     | 40 | -90  | 50           | 50   | 50   |             |             |                        |               |         |         |
|        | 4      | 0        | 0  | -120 | 50           | 40   | 50   |             |             |                        |               |         |         |

Two Mile Hill

- For the Two Mile Hill resource area, the geological defined tonalite intrusion was estimated using Ordinary Kriging and Inverse Distance estimation methods using 3m composite. The Nearest Neighbour uses a 4m heavy top cut composite.
- The non-tonalite Two Mile Hill resources (including deep BIF mineralisation) used a 1m composite, while the Nearest Neighbour estimate uses a seam composite.
- For the Two Mile Hill tonalite resource, a four pass search strategy was employed. After these pass, un-estimated blocks were assigned a nearest neighbour estimate valve. For the non-tonalite resources a 3 pass search strategy was employed as below
- Two Mile Hill Search Parameters:

|        | Domain    | Rotation |     |      | Search Range |      |     | Min Samples | Max Samples | Max Samples/drill hole | Octant Search |         |         |
|--------|-----------|----------|-----|------|--------------|------|-----|-------------|-------------|------------------------|---------------|---------|---------|
|        |           | Z        | X   | Z    | X            | Y    | Z   |             |             |                        | No. Octants   | Min Sam | Max Sam |
| Pass 1 | Basalt_mz | -115     | 150 | -20  | 12.5         | 8    | 7.5 | 15          | 45          | 5                      | NA            |         |         |
|        | Hg_BIF    | -130     | 140 | -110 | 11.5         | 9.5  | 9.5 |             |             |                        |               |         |         |
|        | 9505_bif  | -105     | 120 | -35  | 16.5         | 5.5  | 5.5 |             |             |                        |               |         |         |
|        | laterite  | 0        | 0   | -170 | 24.5         | 18.5 | 5   |             |             |                        |               |         |         |
|        | TONALITE  | -130     | 150 | -70  | 25           | 22.5 | 5   |             |             |                        |               |         |         |
| Pass 2 | Basalt_mz | -115     | 150 | -20  | 25           | 16   | 15  | 15          | 45          | 5                      | NA            |         |         |
|        | Hg_BIF    | -130     | 140 | -110 | 23           | 19   | 19  |             |             |                        |               |         |         |
|        | 9505_bif  | -105     | 120 | -35  | 33           | 11   | 11  |             |             |                        |               |         |         |
|        | laterite  | 0        | 0   | -170 | 49           | 37   | 10  |             |             |                        |               |         |         |
|        | TONALITE  | -130     | 150 | -70  | 50           | 45   | 10  |             |             |                        |               |         |         |
| Pass 3 | Basalt_mz | -115     | 150 | -20  | 50           | 32   | 30  | 5           | 24          | 5                      | NA            |         |         |
|        | Hg_BIF    | -130     | 140 | -110 | 46           | 38   | 38  |             |             |                        |               |         |         |
|        | 9505_bif  | -105     | 120 | -35  | 66           | 22   | 22  |             |             |                        |               |         |         |
|        | laterite  | 0        | 0   | -170 | 98           | 74   | 20  |             |             |                        |               |         |         |
|        | TONALITE  | -130     | 150 | -70  | 50           | 45   | 10  |             |             |                        |               |         |         |
| Pass 4 | Basalt_mz | -115     | 150 | -20  | 100          | 62   | 60  | 5           | 24          | 5                      | NA            |         |         |
|        | Hg_BIF    | -130     | 140 | -110 | 98           | 60   | 60  |             |             |                        |               |         |         |
|        | 9505_bif  | -105     | 120 | -35  | 166          | 44   | 44  |             |             |                        |               |         |         |
|        | laterite  | 0        | 0   | -170 | 398          | 316  | 100 |             |             |                        |               |         |         |
|        | TONALITE  | -130     | 150 | -70  | 100          | 90   | 20  |             |             |                        |               |         |         |

- A number of block model validations were completed to ensure the block modelling and estimation techniques employed were appropriate for the deposit. These methods include:
  - Visual validation methods comparing blocks against raw and composited drill hole data, in section and 3D
  - Numerical validation methods, such as histogram, log-probability and swath plots as way a block/composite comparison of different estimation techniques.
  - Block model/wireframe volume checks
- The validation showed the block model estimates appropriately reflect the composites, showing a

| Criteria                             | JORC Code explanation   | Commentary  |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
|--------------------------------------|---|---|-----------------|--|-------|--|-----------------|---------|--------------------|---------|--------------------------|--------|--------------------|---------|----------------------------|----------------|--------------------------------|--|-------|--|----------------------|---------|---------------------|-----|--------------|-------|-----------------------------|----------------|
|                                      |   | reasonable global estimate  |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| <b>Moisture</b>                      | <i>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</i>   | <ul style="list-style-type: none"><li>Tonnages are estimated on a dry basis. Moisture content within the ore is expected to be moderate to low</li></ul>  |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| <b>Cut-off parameters</b>            | <i>The basis of the adopted cut-off grade(s) or quality parameters applied.</i>   | <ul style="list-style-type: none"><li>The Mineral Resource has been reported within optimised wireframes.</li><li>The cut-off grade has been determined using the Mining and Processing information detailed below.</li><li>The Shillington Mineral Resource is reported at a 0.5g/t cut-off grade and a depth of 140m.</li><li>The Two Mile Hill open pit resource (above 370mRL) is reported at a 0.5g/t cut-off grade and depth of 150m</li><li>The Two Mile Hill underground resource (below the 370mRL) is reported at the 0.73g/t Au cut-off grade</li></ul>  |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| <b>Mining factors or assumptions</b> | <i>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</i> | <ul style="list-style-type: none"><li>Mining at Shillington is assumed to be by open pit mining methods.</li><li>The Two Mile Hill resource is assumed to be mined by open pit and underground mining methods</li><li>Maximum depth for the open pits at Shillington is assumed to be approximately 140m while the Two Mile Hill pit is assumed to be 115m below original surface base on knowledge from other deposits.</li><li>No mining dilution or recovery have been applied</li><li>Ore sorting methods have been successfully trialled on Two Mile Hill ore, but no benefaction has been assumed in this analysis.</li><li>Cost and revenue assumptions for Two Mile Hill are as follows:<table><tr><th colspan="2">Operating Costs</th></tr><tr><th colspan="2">Item:</th></tr><tr><td>Mining (A\$/t):</td><td>\$30.00</td></tr><tr><td>Overheads (A\$/t):</td><td>\$10.00</td></tr><tr><td>Surface Haulage (A\$/t):</td><td>\$1.40</td></tr><tr><td>Processing (A\$/t)</td><td>\$30.00</td></tr><tr><td><b>Total Cost (A\$/t):</b></td><td><b>\$71.40</b></td></tr><tr><th colspan="2">Revenue and Revenue Deductions</th></tr><tr><th colspan="2">Item:</th></tr><tr><td>Gold Price (A\$/oz):</td><td>\$3,250</td></tr><tr><td>Processing Recovery</td><td>96%</td></tr><tr><td>WASG Royalty</td><td>2.50%</td></tr><tr><td><b>Net Revenue (A\$/g):</b></td><td><b>\$97.80</b></td></tr></table></li><li>This work calculated a cut-off grade of 0.73 g/t Au as meeting the criteria for reasonable prospects for</li></ul> | Operating Costs |  | Item: |  | Mining (A\$/t): | \$30.00 | Overheads (A\$/t): | \$10.00 | Surface Haulage (A\$/t): | \$1.40 | Processing (A\$/t) | \$30.00 | <b>Total Cost (A\$/t):</b> | <b>\$71.40</b> | Revenue and Revenue Deductions |  | Item: |  | Gold Price (A\$/oz): | \$3,250 | Processing Recovery | 96% | WASG Royalty | 2.50% | <b>Net Revenue (A\$/g):</b> | <b>\$97.80</b> |
| Operating Costs                      |   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| Item:                                |   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| Mining (A\$/t):                      | \$30.00   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| Overheads (A\$/t):                   | \$10.00   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| Surface Haulage (A\$/t):             | \$1.40  |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| Processing (A\$/t)                   | \$30.00   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| <b>Total Cost (A\$/t):</b>           | <b>\$71.40</b>  |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| Revenue and Revenue Deductions       |   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| Item:                                |   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| Gold Price (A\$/oz):                 | \$3,250   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| Processing Recovery                  | 96%   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| WASG Royalty                         | 2.50%   |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |
| <b>Net Revenue (A\$/g):</b>          | <b>\$97.80</b>  |   |                 |  |       |  |                 |         |                    |         |                          |        |                    |         |                            |                |                                |  |       |  |                      |         |                     |     |              |       |                             |                |

| Criteria                                    | JORC Code explanation   | Commentary   |
|---|---|--|
|   |   | economic extraction defined by the JORC Code.  |
| <b>Metallurgical factors or assumptions</b> | <i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i>   | <ul style="list-style-type: none"> <li>The metallurgical assumptions/parameters applied to the optimisation are:               <ul style="list-style-type: none"> <li>- 96% processing recovery, Two Mile Hill</li> <li>- 92% processing recovery, Shillington.</li> <li>- Processing costs – A\$30/tonne,</li> <li>- No ore sorting beneficiation factor has been applied although test programmes have demonstrated Two Mile Hill mineralised material is amendable to ore sorting.</li> </ul> </li> </ul> <p><u>Shillington</u></p> <ul style="list-style-type: none"> <li>For Shillington the gravity recoverable gold (GRG) test work completed by ALS in 2017 confirms the presence of coarse gold in Shillington composites. The average GRG was 14% obtained for Shillington. The gold extraction obtained for Shillington (92.3% at 106µm) is comparable to recoveries obtained historically through the plant in the late 1990's. An estimated target recovery of 92.0% should be achievable for Shillington.</li> </ul> <p><u>Two Mile Hill</u></p> <ul style="list-style-type: none"> <li>Historic production records from the Two Mile Hill open pit deposits have been reviewed in detail. Sandstone Operations have also undertaken further metallurgical test work on samples derived from archived and new diamond drill core. The average metallurgical gold recoveries determined from test work conducted in 2016, 2017 and 2020 at the Two Mile Hill deposit is consistent with historical recoveries, is 95.3% at a 106 micron grind size. The metallurgical recoveries and conceptual operating costs have been incorporated in estimation to determine an appropriate range of cut-off grades for estimation and resource reporting purposes.</li> </ul> |
| <b>Environmental factors or assumptions</b> | <i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this</i> | <ul style="list-style-type: none"> <li>No environmental factors or assumptions have been applied.</li> <li>Deposits are located within existing mining area and no issues are anticipated.</li> </ul>  |



| Criteria                    | JORC Code explanation  | Commentary  |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
|-----------------------------|--|---|-----------|------------|---------|----------|--|------|--------|-------|------|--------------|------|-------|------|-----------------------------|-------|---|--------------|-----|-------|---|----------|-------|------|--------------|------|-------|------|
|                             | <i>should be reported with an explanation of the environmental assumptions made.</i>   |   |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
| <b>Bulk density</b>         | <p><i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i></p> <p><i>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit. Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i></p> | <ul style="list-style-type: none"> <li>Bulk density values have been calculated from 178 measurements. Data has been separated into lithological and weathering datasets for analysis.</li> <li>46 immersion test of core billets and 132 core tray weight determinations. Very limited documentation is available about the collection method and quality of core tray weight data.</li> <li>The core billet immersion determinations have been completed by independent laboratory ALS using wax coating where applicable.</li> <li>Bulk densities have been assigned to the block model on the basis of lithology and weathering state.</li> <li>The bulk densities assigned to the block model are:</li> </ul> <table border="1"> <thead> <tr> <th>Lithology</th><th>Weathering</th><th>Density</th></tr> </thead> <tbody> <tr> <td colspan="2">Laterite</td><td>2.21</td></tr> <tr> <td rowspan="3">Basalt</td><td>Oxide</td><td>1.83</td></tr> <tr> <td>Transitional</td><td>2.42</td></tr> <tr> <td>Fresh</td><td>2.91</td></tr> <tr> <td rowspan="3">Banded Iron Formation (BIF)</td><td>Oxide</td><td>2</td></tr> <tr> <td>Transitional</td><td>2.8</td></tr> <tr> <td>Fresh</td><td>3</td></tr> <tr> <td rowspan="3">Tonalite</td><td>Oxide</td><td>2.21</td></tr> <tr> <td>Transitional</td><td>2.54</td></tr> <tr> <td>Fresh</td><td>2.71</td></tr> </tbody> </table> | Lithology | Weathering | Density | Laterite |  | 2.21 | Basalt | Oxide | 1.83 | Transitional | 2.42 | Fresh | 2.91 | Banded Iron Formation (BIF) | Oxide | 2 | Transitional | 2.8 | Fresh | 3 | Tonalite | Oxide | 2.21 | Transitional | 2.54 | Fresh | 2.71 |
| Lithology                   | Weathering   | Density   |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
| Laterite                    |  | 2.21  |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
| Basalt                      | Oxide  | 1.83  |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
|                             | Transitional   | 2.42  |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
|                             | Fresh  | 2.91  |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
| Banded Iron Formation (BIF) | Oxide  | 2   |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
|                             | Transitional   | 2.8   |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
|                             | Fresh  | 3   |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
| Tonalite                    | Oxide  | 2.21  |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
|                             | Transitional   | 2.54  |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
|                             | Fresh  | 2.71  |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |
| <b>Classification</b>       | <p><i>The basis for the classification of the Mineral Resources into varying confidence categories. Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i></p> <p><i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i></p>   | <ul style="list-style-type: none"> <li>Definitions for Mineral Resource categories are consistent with those defined by JORC (2012). The classifications were determined based on geological confidence and continuity, drill spacing and search volume (pass).</li> <li>Indicated resource category are modelled blocks which lie inside the modelled mineralisation wireframes and display coherent continuity in strike and down dip extension, based on the current borehole intersections. All these blocks have been estimated within an early search volume and therefore require minimal infill drilling to improve the quality of the geological interpretation and grade estimate.</li> <li>Inferred resource category are model blocks which lie inside the modelled mineralisation wireframes, which still display reasonable strike continuity and down dip extension, based on the current borehole intersections. All these blocks have been estimated within search volume and therefore require infill drilling to improve the quality of the geological interpretation and grade estimate.</li> <li>There were no Measured resources estimated in either the Shillington or Two Mile Hill deposits.</li> <li>The results appropriately reflect the Competent Persons</li> </ul>   |           |            |         |          |  |      |        |       |      |              |      |       |      |                             |       |   |              |     |       |   |          |       |      |              |      |       |      |

| Criteria  | JORC Code explanation   | Commentary  |
|---|---|---|
|   |   | view of the deposit.  |
| <b>Audits or reviews</b>                          | <i>The results of any audits or reviews of Mineral Resource estimates.</i>  | <ul style="list-style-type: none"> <li>Internal and external peer reviews have been conducted for this resource estimate. These concluded that the procedures used to estimate and classify the mineral resource are appropriate.</li> </ul>  |
| <b>Discussion of relative accuracy/confidence</b> | <p><i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate. The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i></p> <p><i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i></p> | <ul style="list-style-type: none"> <li>The mineral resource for Shillington and Two Mile Hill deposits have been reported in accordance with the guidelines established in the 2012 edition of the JORC code. The resource estimates have undergone validation processes, and as such, the competent person is satisfied that the resources estimated in the block model are a true representation of the in-situ resources on a global scale.</li> <li>The statements relate to a global estimate of tonnes and grade for Shillington and Two Mile Hill deposits.</li> </ul> |