ASX/LSE: CCZ

28 February 2023

CASTILLO COPPER

Exploration with Purpose

Encouraging REE metallurgy test-work from Broken Hill

Highlights

- **Preliminary metallurgical test-work on a 20m composite sample from the Fence Gossan Prospect (FG_003RC) delivered encouraging results, with clays – subjected to froth flotation – obtaining up to 2-3 times rare earth element (REE) enrichment from the head grade at up to 70% recovery:**
  - **These findings confirm REEs can be readily separated from clay within the East Zone discovery area and potentially beneficiated to a higher grade concentrate**
- **To acquire a deeper understanding of the potential to extract REE-mineralisation from clays in the East Zone discovery area, the Board has approved appointing a specialist consultancy to conduct an in-depth metallurgy test-work program:**
  - **Once completed and interpreted, the results from this program will be key to securing interest from potential off-take partners and providing a path to market**
- **Further, 1m re-assays for Reefs Tank were received for all four drill-holes (RT_001-4RC), which further verified there is an extensive, shallow REE system apparent across the central part of the East Zone – the best intercept comprised:**

  3m @ 2,587ppm TREO from 14m (RT_001RC)
- **Reconciling all assays from the recent drilling and auger campaigns across the Fence Gossan, Tors & Reefs Tanks Prospects, the geology team has created heat maps which identify zones of high Total and Magnetic Rare Earth Oxides (TREO/MREO):**
  - **These areas will be subject to further surface sampling and geophysical surveys then potentially drill-testing to extend known mineralisation**

Castillo Copper's Chairman Ged Hall commented: *"On a holistic basis, the Board is delighted with results from the drilling, surface sampling and metallurgical test-work at Broken Hill as they collectively demonstrate the forward value creating potential of the BHA Project's East Zone. In short, the underlying REE system is shallow, extends over at least 4.5km^2, delivered results up to 3,491ppm TREO and produced up to 38.9% MREO in diamond core[1]. Moreover, the metallurgy test-work proves REE mineralisation readily separates from clay and can potentially be beneficiated to a higher-grade concentrate. By all accounts, this is an excellent report card ahead of exploratory work ramping up."*

ENCOURAGING METALLURGICAL TEST-WORK RESULTS

Castillo Copper Limited's ("CCZ") Board is delighted with the initial REE metallurgical test-work results from a 20m composite sample (FG_003RC) from the Fence Gossan Prospect (Appendix A). The sample, which comprised clays – was subjected to froth flotation – delivered up to 2-3 times REE enrichment from the head grade at up to 70% recovery (refer Figure 1 and Appendix B for full details). Moreover, these findings verify that REEs can be readily separated from clay within the East Zone discovery area and potentially beneficiated to a higher-grade concentrate.

FIGURE A1: HEAD ASSAY / IMPROVEMENT

ANALYTE	ALS Adelaide REE ME-MS81 %	ALS Perth HEAD GRADE REE COMP %	Times Improvement
Ce (%)	0.045	0.05	1.6
La (%)	0.038	0.03	2.3
Nd (%)	0.021	0.02	2.0
Pr (%)	0.006	0.01	1.3
Y (%)	0.009	0.01	1.1

Source: ALS

To follow up on these excellent results, the Board has now approved the appointment of a specialist metallurgy consultancy with extensive experience in how REE mineralisation liberates from various host rocks (including clays). The Board wants a deeper understanding of the potential to extract REE mineralisation from the East Zone discovery area, as this information will be key to securing interest from potential off-take partners that can provide a clear path to market.

Reefs Tank Assays

All 1m re-assays for Reefs Tank were received for the four drill-holes (RT_001-4RC), with up to 2,587ppm TREO recorded (Figure 1). On a holistic basis, the Reefs Tank results provide incremental evidence there is an extensive, shallow REE system apparent across the central part of the BHA Project's East Zone (Appendix A).

FIGURE 1: REEFS TANK 1M ASSAYS

Hole	From (m)	To (m)	Width (m)	Ag (g/t)	Th (ppm)	U (ppm)	TREO (ppm)	TREO-Ce (ppm)	LREO (ppm)	HREO (ppm)	CREO (%)	MREO (%)
RT_001RC	11	13	2	0.05	17.0	5.4	631	313.08	490.55	140.69	27.3%	20.6%
RT_001RC	14	17	3	0.96	29.9	9.4	2,587	2187.30	1105.24	1481.70	55.7%	24.7%
RT_001RC	54	55	1	0.15	70.2	9.2	796	429.43	746.15	49.34	20.8%	29.1%
RT_001RC	55	56	1	0.08	80.5	6.2	896	487.84	838.19	57.49	21.2%	29.9%
RT_001RC	64	65	1	0.12	121.0	9.0	1,236	658.75	1196.01	40.09	19.0%	29.3%
RT_002RC	0	1	1	0.06	19.8	2.5	367	241.55	272.76	94.70	34.1%	28.2%
RT_002RC	1	4	3	0.11	24.7	2.5	449	285.00	350.63	98.36	31.5%	27.6%
RT_002RC	28	32	4	0.12	54.6	3.5	601	343.27	541.76	59.48	24.1%	30.9%
RT_002RC	64	68	4	0.05	27.6	3.2	430	267.15	339.41	90.36	30.7%	27.5%
RT_003RC	0	4	4	nd	14.6	6.2	247	165.15	183.62	63.40	34.5%	29.8%
RT_003RC	8	16	8	nd	27.5	4.5	424	258.35	352.12	71.76	28.4%	28.5%
RT_003RC	56	64	8	nd	23.8	3.8	389	237.70	313.43	75.97	29.6%	27.6%
RT_003RC	72	76	4	nd	28.6	6.9	450	272.82	366.14	83.72	29.1%	27.3%
RT_004RC	52	56	4	0.25	44.4	4.1	567	344.40	465.92	101.13	29.1%	29.2%
RT_004RC	84	92	8	1.78	25.6	8.5	525	314.92	433.13	92.23	28.4%	27.7%

Source: CCZ geology team

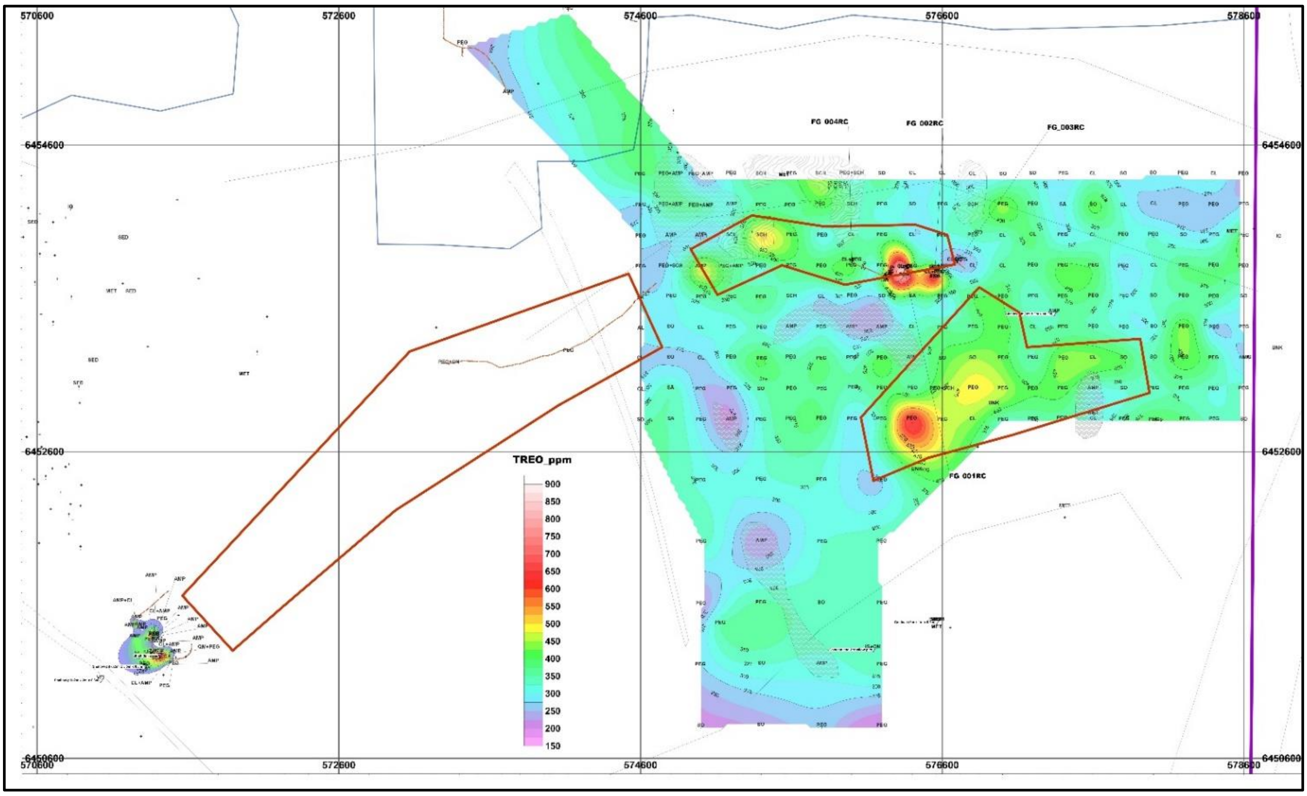
TREO / MREO Contours

After reconciling all assays from the recent drilling and auger campaigns across the Fence Gossan, Tors & Reefs Tanks Prospects (Appendix B), the geology team has created heat maps which identify zones of high TREO and MREO (Figure 2 & 3).

These areas will be subject to further surface sampling and geophysical campaigns (including trial transects of ground radiometric and EM surveys) then potentially drill-testing (red zones in Figure 2) to extend known mineralisation.

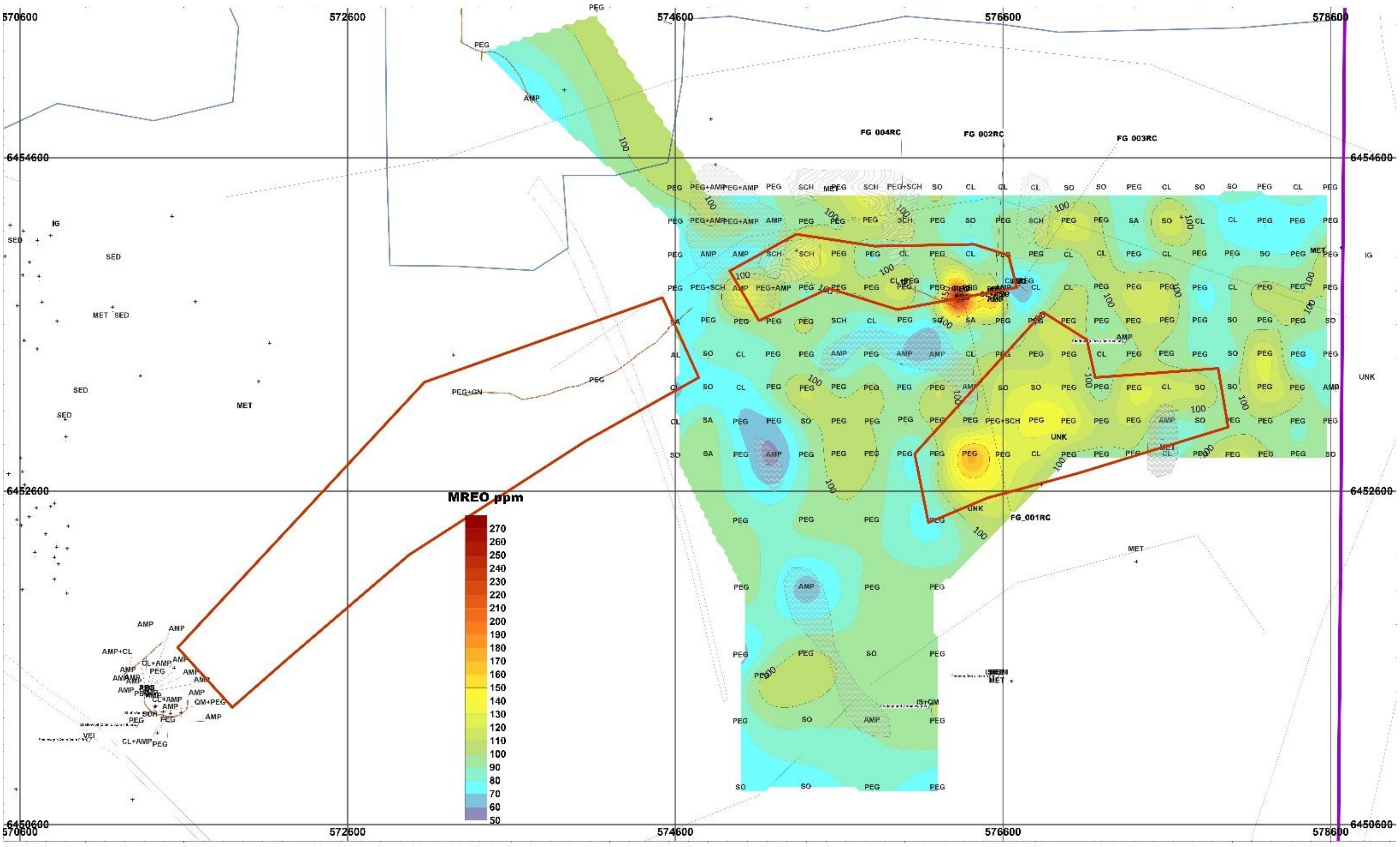
Note, the TREO is the sum of REEs in ppm, calculated from ME-MS81 method, converted to their stoichiometric equivalent i.e., Ce converted to CeO_2 and so forth. The high-value Magnetic REO comprise Nd+Pr+Dy+Tb and generally command premium pricing to other REEs as they are in strong demand. Refer to Appendix C for a full explanation and TREO calculation.

FIGURE 2: FENCE GOSSAN AND SURROUNDS SURFACE SAMPLING – TREO IN PPM



Source: CCZ geology team

FIGURE 3: FENCE GOSSAN AND SURROUNDS SURFACE SAMPLING – MREO ppm



Notes: All coordinates in MGA94-Z54S Source: CCZ Geology team

The Board of Castillo Copper Limited authorised the release of this announcement to the ASX.

Dr Dennis Jensen

Managing Director

Competent Person's Statement

The information in this report that relates to Exploration Results and Mineral Resource Estimates for "BHA Project, East Zone" is based on information compiled or reviewed by Mr Mark Biggs. Mr Biggs is a director of ROM Resources, a company which is a shareholder of Castillo Copper Limited. ROM Resources provides ad hoc geological consultancy services to Castillo Copper Limited. Mr Biggs is a member of the Australian Institute of Mining and Metallurgy (member #107188) and has sufficient experience of relevance to the styles of mineralisation and types of deposits under consideration, and to the activities undertaken, to qualify as a Competent Person as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, and Mineral Resources. Mr Biggs holds an AusIMM Online Course Certificate in 2012 JORC Code Reporting. Mr Biggs also consents to the inclusion in this report of the matters based on information in the form and context in which it appears.

The Australian Securities Exchange has not reviewed and does not accept responsibility for the accuracy or adequacy of this release.

References

1) CCZ ASX Release – 15 February 2023

About Castillo Copper

Castillo Copper Limited is an Australian-based explorer primarily focused on copper across Australia and Zambia. The group is embarking on a strategic transformation to morph into a mid-tier copper group underpinned by its
core projects:

A large footprint in the in the Mt Isa copper-belt district, north-west Queensland, which delivers significant exploration upside through having several high-grade targets and a sizeable untested anomaly within its boundaries in a copper rich region.

Four high-quality prospective assets across Zambia's copper-belt which is the second largest copper producer in Africa.

A large tenure footprint proximal to Broken Hill's world-class deposit that is prospective for cobalt-zinc-silver-lead-copper-gold and platinoids.

Cangai Copper Mine in northern New South Wales, which is one of Australia's highest grading historic copper mines.

The group is listed on the LSE and ASX under the ticker "CCZ."

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ASX/LSE Symbol

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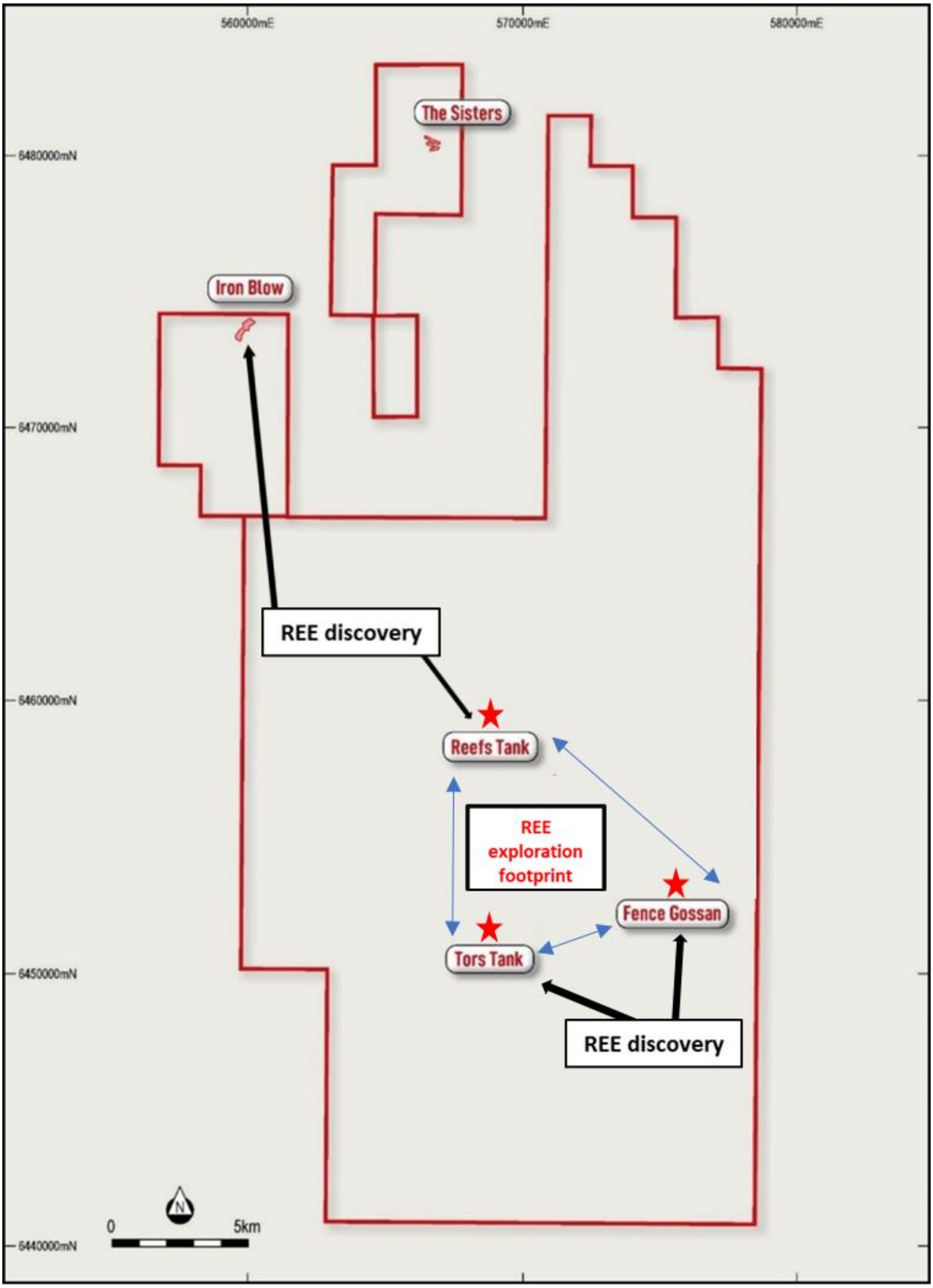
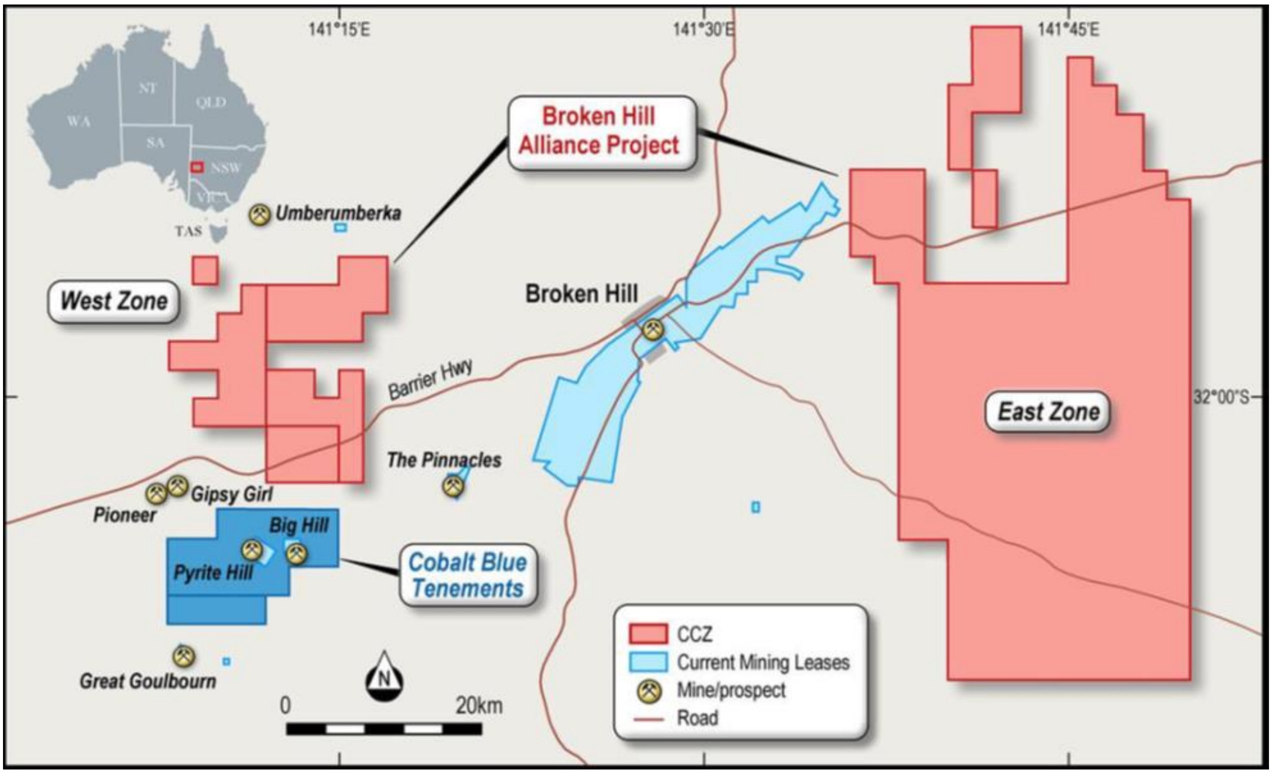
APPENDIX A: BHA PROJECT'S EAST ZONE

FIGURE A1: BHA PROJECT's EAST ZONE - REE EXPLORATION FOOTPRINT



Source: CCZ geology team

FIGURE A2: BHA PROJECT



Source: CCZ geology team

APPENDIX B: PRELIMINARY METALLURGY TESTWORK

Background and Scope

A composite sample of RC chips from Fence Gossan drill-hole FG_003RC was constructed over the interval from 0-20m. The material reported over that interval had lithology logged as clay, haematite, goethite, and extremely weathered pegmatite. The main rare-containing minerals are thought to be monazite, allanite, xenotime, and possibly baryte or celsian (to account for the high barium contents of some samples). Note, these assumptions need to be tested by XRD and/or QEM-SEM testing.

The composite was made up of 1m samples tested using ME-MS81 analysis method (the results for which are provided in Figure A1).

The process methodology followed by ALS Perth was as follows:

- Rotary Blending & Splitting (12x1kg, reserve)
- PPS - Head Assay Submission
- Assay - Head Assay (Ce, La, Nd, Pr, SiO_2, Y)
- 1kg Grind Establishment (P80 53µm assumed)
- Rougher Flotation (6 con, 1 Tail)
- PPS - Float Products
- Assay - Head Assay (Ce, La, Nd, Pr, SiO_2, and Y)

Results

The head grade and froth flotation improvement are shown in Figure A1.

FIGURE A1: HEAD ASSAY / IMPROVEMENT

ANALYTE	ALS Adelaide REE ME-MS81 %	ALS Perth HEAD GRADE REE COMP %	Times Improvement
Ce (%)	0.045	0.05	1.6
La (%)	0.038	0.03	2.3
Nd (%)	0.021	0.02	2.0
Pr (%)	0.006	0.01	1.3
SiO2 (%)	NT	64.3	-
Y (%)	0.009	0.01	1.1

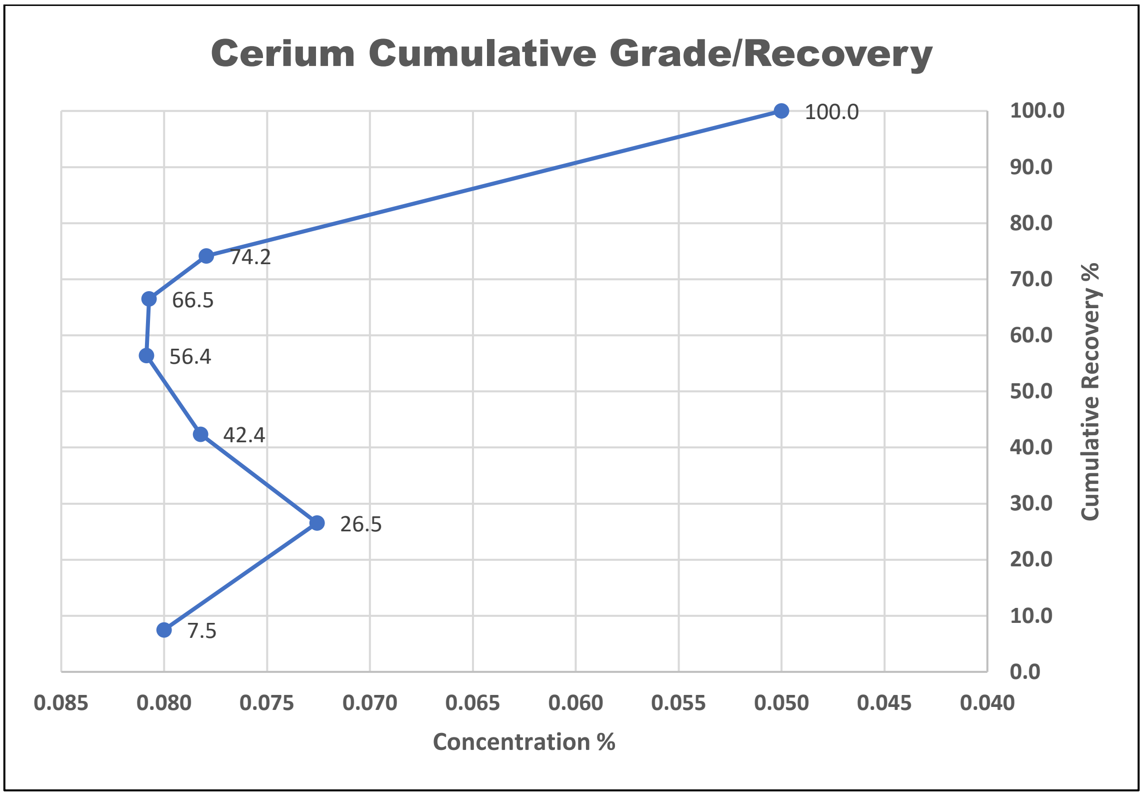
Source: ALS

Overall main laboratory observations of note are:

- Slurry was highly viscous after ALS Perth added lime that changed the target pH down to 9.5. The process was changed to soda ash in the second test.
- By end of float, ALS Perth saw froth instability, which indicates what material wanted to float.
- There was a colour trend in the concentrate progressing through the stages.

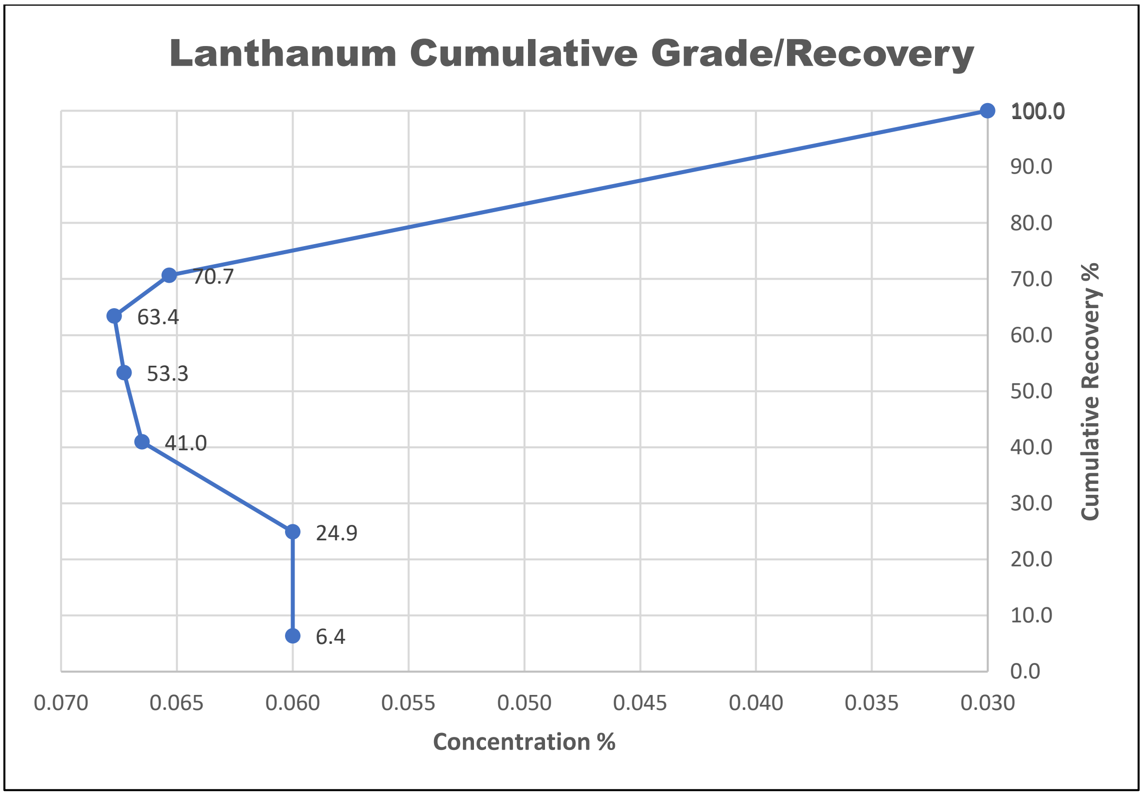
Figures A2 to A5 show cumulative recovery versus grade for the Ce, La, Nd, and Pr components.

FIGURE A1: CERIUM CUMULATIVE GRADE / RECOVERY



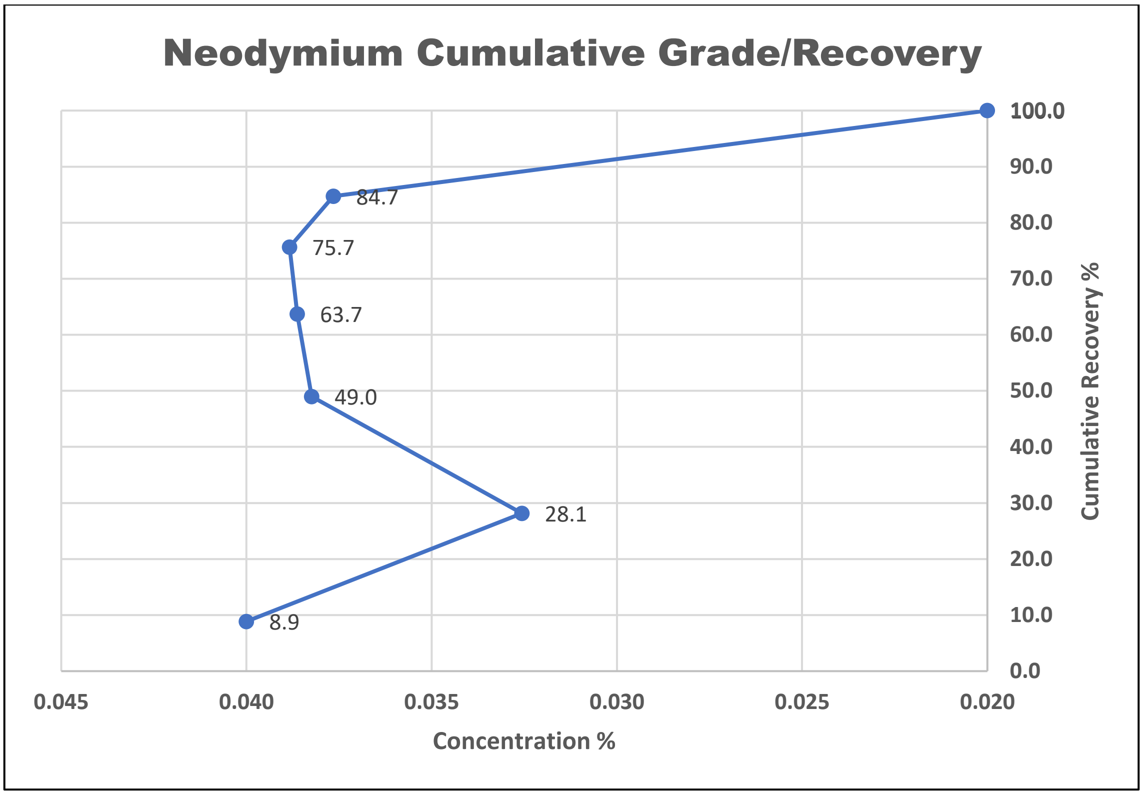
Source: ALS

FIGURE A1: LANTHANUM CUMULATIVE GRADE / RECOVERY



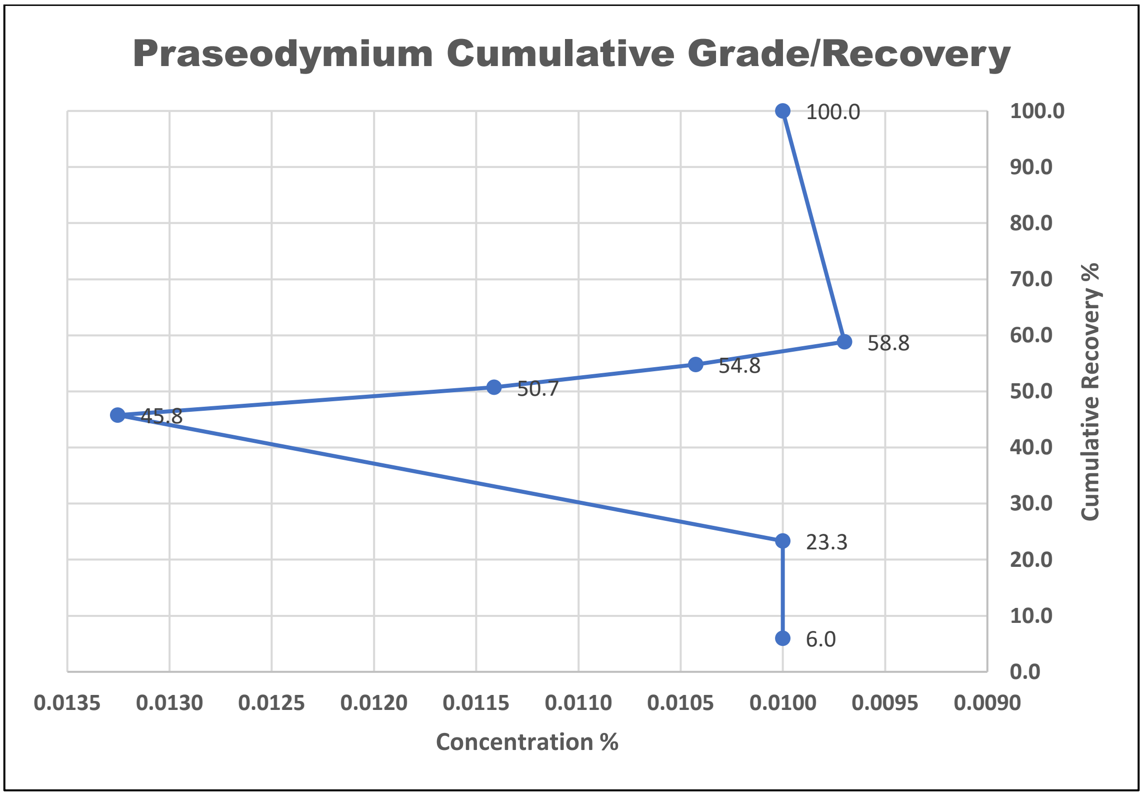
Source: ALS

FIGURE A1: NEODYMIUM UMULATIVE GRADE / RECOVERY



Source: ALS

FIGURE A5: PRASEODYMIUM CUMULATIVE GRADE / RECOVERY



Source: ALS

FIGURE A6: FLOWTATION FLOWSHEET

ALS

Flotation Flowsheet , Reagent Scheme & Results - **Test : BF2364**

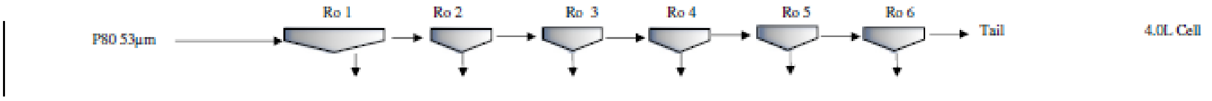
Metallurgy

TEST DETAILS :

PROJECT	A24090 - Castillo REE Evaluation Program
COMPOSITE	REE Comp
TEST No	BF2364
WATER TYPE	Perth Tap Water 2018"
GRIND SIZE	P80 53µm
PULP DENSITY	Cond ~ 18% Float 35% 4.0L Cell / 1000g Charge
TECHNICIAN/DATE	JS 13-Jan-23

Test 2
Soda Ash, extra reagent (dilution implimented)

FLOWSHEET :



REAGENT SCHEME :

CELL rpm =1200 conditioning, 750 flotation

Agitar Slope-Back Cell

Operation	Reagent	Dose	pH	mV Plat	Temp C	Air (L/min)	MIBC Frother (drops)	Float Time (mins)
Mill			7.95	+266.4	22.0			
Conditioning 1	Na2SiO3 (g/t) Sylfat FA2 (g/t) Soda Ash (g)	500 150 11.34						
Ro Con 1			9.83		41.4			1
Conditioning 2	Na2SiO3 (g/t) Sylfat FA2 (g/t) Soda Ash (g)	100 150						
Ro Con 2			9.73		40.8			2
Conditioning 3	Na2SiO3 (g/t) Sylfat FA2 (g/t) Soda Ash (g)	100 150						
Ro Con 3			9.67		40.6			2
Conditioning 4	Na2SiO3 (g/t) Sylfat FA2 (g/t) Soda Ash (g)	100 150						
Ro Con 4			9.62		41.2			2
Conditioning 5	Na2SiO3 (g/t) Sylfat FA2 (g/t) Soda Ash (g)	100 150						
Ro Con 5			9.58		41.2			2
Conditioning 6	Na2SiO3 (g/t) Sylfat FA2 (g/t) Soda Ash (g)	100 150						
Ro Con 6			9.49	+99.8	42.6			2

Notes:
Soda ash resulted in high viscosity,
Moved to a 4L cell for flotation

RESULTS

Below Detection
Half of detection limit used

PRODUCT	WEIGHT		Ce		La		Nd		Pr		SiO2		Y	
	Gram	%	%	%dist	%	%dist	%	%dist	%	%dist	%	%dist	%	%dist
Ro Con 1	60.95	6.09	0.07	10.0	0.05	9.67	0.03	7.76	0.005	5.36	63.4	5.99	0.005	4.28
Ro Con 2	79.63	7.96	0.10	18.8	0.07	17.7	0.05	16.9	0.005	7.01	61.0	7.53	0.02	22.4
Ro Con 3	120.78	12.1	0.08	22.8	0.06	23.0	0.04	20.5	0.005	10.6	61.6	11.5	0.005	8.48
Ro Con 4	74.38	7.44	0.08	14.0	0.05	11.8	0.04	12.6	0.01	13.1	61.7	7.11	0.005	5.22
Ro Con 5	61.59	6.16	0.08	11.6	0.06	11.7	0.04	10.4	0.01	10.8	62.4	5.95	0.02	17.3
Ro Con 6	73.42	7.34	0.06	10.4	0.04	9.32	0.03	9.34	0.005	6.46	65.4	7.44	0.005	5.16
Scav Tail	529.38	52.9	0.01	12.5	0.01	16.8	0.01	22.5	0.005	46.6	66.4	54.5	0.005	37.2
Calc'd Head	1000.13	100.0	**0.04**	**100.0**	**0.03**	**100.0**	**0.02**	**100.0**	**0.01**	**100.0**	**64.5**	**100.0**	**0.01**	**100.0**
Assay Head			**0.05**		**0.03**		**0.02**		**0.01**		**64.3**		**0.01**	
Ro Con 1		6.09	0.07	10.0	0.05	9.67	0.03	7.76	0.01	5.36	63.4	5.99	0.01	4.28
Ro Con 1-2		14.1	0.09	28.8	0.06	27.4	0.04	24.6	0.01	12.4	62.0	13.5	0.01	26.7
Ro Con 1-3		26.1	0.08	51.5	0.06	50.4	0.04	45.1	0.01	23.0	61.8	25.0	0.01	35.1
Ro Con 1-4		33.6	0.08	65.6	0.06	62.2	0.04	57.8	0.01	36.1	61.8	32.1	0.01	40.4
Ro Con 1-5		39.7	0.08	77.2	0.06	73.9	0.04	68.2	0.01	46.9	61.9	38.1	0.01	57.7
Ro Con 1-6		47.1	0.08	87.5	0.06	83.2	0.04	77.5	0.01	53.4	62.4	45.5	0.01	62.8

Source: ALS

FIGURE A7: DRILLHOLE FG_003RC – 0 TO 20M COMPOSITE USED FOR ALS PERTH METALLURGICAL TESTING, 1M ANALYSIS (A-P)

Sample Number	From	To	Length	PGM-MS23	PGM-MS23	PGM-MS23	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81
				Au	Pt	Pd	Ba	Ce	Cr	Cs	Dy	Er	Eu	Ga	Gd	Hf	Ho	La	Lu	Nb	Nd	Pr
	m	m	m	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm
CCZ04511	0	1	1	0.002	0.001	0.002	297	131	61	3.13	6.48	3.92	1.71	23.5	7.17	5.56	1.35	70	0.58	10.85	54.8	16.1
CCZ04512	1	2	1	0.006	0.0013	0.003	910	172.5	73	2.58	7.57	4.05	2.16	38.1	8.71	4.09	1.52	97.5	0.46	10.55	74.2	21
CCZ04513	2	3	1	0.004	0.0011	0.002	648	696	71	2.64	20.9	9.3	9.12	46.2	34.4	4.18	3.6	409	0.93	12.75	347	94.2
CCZ04514	3	4	1	0.002	0.0007	0.001	166.5	580	72	5.2	17.85	6.75	7.5	55.9	28.5	3.02	2.76	369	0.54	10.4	276	74.4
CCZ04515	4	5	1	0.002	0.0007	0.001	143	511	80	5.01	16.35	6.43	6.46	51.2	25.9	3.39	2.67	336	0.63	13.85	252	67.4
CCZ04516	5	6	1	0.001	0.0008	0.001	98.4	376	75	3.04	10.5	3.86	3.91	53.5	17.5	3.05	1.62	229	0.36	12.8	175.5	46.6
CCZ04517	6	7	1	<0.001	0.0008	0.001	91.9	480	76	3.89	13.75	4.51	5.55	54.5	22.4	3.37	2.03	293	0.47	11.9	221	59.8
CCZ04518	7	8	1	<0.001	0.0007	0.001	59.1	332	90	3.2	8.64	3.14	3.43	60.5	14.3	3.18	1.33	204	0.28	15.4	142.5	39.3
CCZ04519	8	9	1	<0.001	0.0007	0.001	87.2	422	88	5.13	12.5	5.17	4.67	53.4	19	2.97	2.05	258	0.6	12.55	184.5	49.7
CCZ04520	9	10	1	<0.001	0.0008	0.001	94.5	287	78	5.62	7.68	3.76	2.49	56.5	10.55	2.62	1.37	175	0.49	13.2	116.5	31.3
CCZ04521	10	11	1	0.001	0.0007	0.001	110.5	366	81	6.57	8.9	4.09	3.31	48.3	14.05	2.56	1.69	231	0.55	10.95	145.5	42.6
CCZ04522	11	12	1	<0.001	0.0007	0.001	118.5	384	90	6.47	12.3	6.33	3.66	58.3	16.7	2.95	2.2	258	0.92	13.1	158.5	43.4
CCZ04523	12	13	1	<0.001	0.0007	0.001	88.6	292	85	3.63	9.33	5.15	2.71	57.2	12.45	3.51	1.79	202	0.61	12.7	117	32.1
CCZ04524	13	14	1	<0.001	0.0007	0.001	98.8	318	81	5.38	12.6	5.77	4.14	56.9	17.65	2.9	2.28	233	0.68	13.15	145.5	38.3
CCZ04525	14	15	1	<0.001	0.0009	0.001	45.7	486	91	4.58	17.9	6.78	5.7	63	28.4	3.06	2.93	341	0.61	12.45	222	59.1
CCZ04526	15	16	1	<0.001	0.0008	0.001	69.4	577	71	9.24	29	13.5	7.19	61.2	38.1	3.58	5.31	427	1.5	11.4	266	68.9
CCZ04527	16	17	1	0.001	0.0025	0.002	53.4	453	67	5.76	23.3	11.35	5.34	47.1	28	4.04	4.32	322	1.29	10.1	195	50.9
CCZ04528	17	18	1	0.003	0.0017	0.002	118	698	53	17.75	30.3	14.65	7.91	48.2	40.5	1.46	5.72	466	1.5	5.57	303	81.5
CCZ04529	18	19	1	0.045	0.002	0.002	109	774	54	6.11	42.4	16.05	12.35	40.3	60.8	1.61	6.9	644	1.36	6.51	425	106.5
CCZ04530	19	20	1	0.005	0.0011	0.001	193	661	60	2.69	104.5	69.3	15.6	25.8	100	2.98	23.8	597	8.34	7	403	94.2
Average							180.0	449.8	74.9	5.4	20.6	10.2	5.7	50.0	27.3	3.2	3.9	308.1	1.1	11.4	211.2	55.9

Source: ALS Adelaide methods ME-MS81 and PGM-MS23 used. Drillhole FG_003RC drilled October 2022.

FIGURE A7: DRILLHOLE FG_003RC – 0 TO 20M COMPOSITE USED FOR ALS PERTH METALLURGICAL TESTING, 1M ANALYSIS (CONT)

Sample Number	From	To	Length	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81	ME-MS81
				Rb	Sc	Sm	Sn	Sr	Ta	Tb	Th	Ti	Tm	U	V	W	Y	Yb	Zr
	m	m	m	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm
CCZ04511	0	1	1	67.5	16.4	10.3	3.2	128	0.9	1.18	12.85	0.49	0.59	4.02	190	3.1	37	3.69	223
CCZ04512	1	2	1	51.2	20	12.35	2.4	180	0.8	1.28	13.65	0.41	0.55	7.54	247	4	35.3	3.39	134
CCZ04513	2	3	1	51.7	19.4	52.8	3.2	126	1	4.53	14.55	0.38	1.18	15.65	191	4.4	76.9	7.01	137
CCZ04514	3	4	1	92.2	37.5	41.8	3.5	129.5	1	3.79	16.3	0.33	0.84	13.85	171	2.8	50.3	5.02	109
CCZ04515	4	5	1	89.1	27.5	38.7	4.3	109.5	1.2	3.52	14.95	0.4	0.78	12.5	178	2.8	53.6	5.09	110
CCZ04516	5	6	1	51.2	14.7	25.9	3.5	91.3	1.1	2.28	16.25	0.38	0.55	7.46	129	3.7	30.9	2.88	100
CCZ04517	6	7	1	78.9	14.7	33.2	2.6	99.1	1	2.98	16.35	0.34	0.57	9.41	106	4.3	35.8	3.23	110
CCZ04518	7	8	1	79.8	11.6	22.6	3.2	101	1.2	1.88	18.25	0.38	0.38	7.65	102	6.3	25.5	2.31	107
CCZ04519	8	9	1	121	16.7	29	3.6	100	1.2	2.58	14.9	0.35	0.71	10.7	140	3	43.1	4.57	99
CCZ04520	9	10	1	160.5	19.6	16.3	3.5	84.7	1.1	1.5	14.3	0.32	0.55	8.74	150	2.2	28.2	4.08	87
CCZ04521	10	11	1	196	20.4	21.6	4.1	89.8	0.9	1.96	14.5	0.31	0.59	12.1	149	1.7	33.6	3.97	87
CCZ04522	11	12	1	171.5	20.2	24	3.7	117	1.1	2.28	19.6	0.34	0.96	15.85	149	3.5	50.9	6.62	99
CCZ04523	12	13	1	108.5	21.4	16.55	3.1	98.9	1.1	1.79	17.65	0.34	0.73	11.2	101	6.3	38.4	4.72	116
CCZ04524	13	14	1	131	20.4	22.3	5	103.5	1	2.28	17.3	0.33	0.79	12.5	136	4	49	4.78	97
CCZ04525	14	15	1	98.8	15.7	35.2	4.3	88.2	1.1	3.64	18.45	0.36	0.81	14.2	170	3.5	57	5	95
CCZ04526	15	16	1	143.5	19.2	41.5	4.3	81.2	1	5.56	18.25	0.31	1.78	20.7	184	2.7	115.5	11.75	113
CCZ04527	16	17	1	84.4	17.6	30.9	3.5	64.9	0.9	4.24	12.7	0.27	1.54	19.1	147	3.6	95.8	9.92	142
CCZ04528	17	18	1	139.5	17.8	47	3.8	51.4	0.4	5.61	6.91	0.15	1.98	38.1	498	4.2	137	12.55	53
CCZ04529	18	19	1	52	38.5	66	5.7	110	0.4	8.47	4.76	0.74	1.94	73.4	580	3	128	11.6	50
CCZ04530	19	20	1	32.7	41.9	72.2	1.5	146	0.4	16	1.57	1.11	9.13	48.7	442	1.1	722	57.8	94
Average				100.1	21.6	33.0	3.6	105.0	0.9	3.9	14.2	0.4	1.3	18.2	208.0	3.5	92.2	8.5	108.1

Source: ALS Adelaide methods ME-MS81 and PGM-MS23 used. Drillhole FG_003RC drilled October 2022.

APPENDIX C: REE RESULTS / TREO CONVERSION FACTOR

FIGURE B1: FENCE GOSSAN SURFACE SAMPLING – ALS METHOD ME-MS81 LABORATORY RESULTS

HoleID	Sampid	Easting	Northing	from	to	thickness	Th	U	Ce	La	Y	Dy	Er	Eu	Gd	Ho	Lu	Nd	Pr	Sm	Tb	Tm	Yb	TREO (ppm)	TREO-Ce (ppm)	LREO (ppm)	HREO (ppm)	CREO %	MREO %	MREO_%
FG_SM_T12	CCZ05627	574597.0	6454393.0	0	0.3	0.3	16.0	2.5	113.5	53.6	41.3	7.49	4.33	1.6	8.57	1.49	0.54	49.3	12.95	9.54	1.31	0.59	4.04	373.4	233.9	286.5	86.9	0.33	0.28	27.9
FG_SM_T13	CCZ05628	574601.0	6454194.0	0	0.3	0.3	12.9	2.1	77.7	37.2	36.6	5.95	3.91	1.33	6.33	1.36	0.54	34.9	8.87	6.74	1.03	0.58	3.7	273.2	177.7	198.3	74.9	0.35	0.27	27.3
FG_SM_T14	CCZ05629	574600.0	6453990.0	0	0.3	0.3	14.9	2.2	88.6	43.1	31.1	5.25	3.28	1.11	6.03	1.12	0.46	37.7	10.15	7.22	0.95	0.46	3.05	288.4	179.6	224.0	64.4	0.32	0.27	27.3
FG_SM_T15	CCZ05630	574600.0	6453791.0	0	0.3	0.3	12.8	1.8	73.9	36.2	30.4	5.16	3.17	1.21	6.01	1.09	0.4	33.4	8.87	6.81	0.91	0.48	3.01	254.0	163.3	190.8	63.2	0.34	0.28	28.1
FG_SM_T16	CCZ05631	574599.0	6453588.0	0	0.3	0.3	13.8	1.9	83.5	39.9	32.1	5.65	3.17	1.31	6.31	1.2	0.41	37.7	9.93	7.66	0.99	0.45	2.94	280.8	178.2	214.2	66.5	0.33	0.28	28.4
FG_SM_T17	CCZ05632	574602.0	6453389.0	0	0.3	0.3	14.4	2.0	85.2	41.1	33.3	5.52	3.58	1.19	6.08	1.19	0.55	37.4	9.9	6.89	0.92	0.55	3.7	285.5	180.8	216.4	69.0	0.33	0.27	27.3
FG_SM_T18	CCZ05633	574598.0	6453194.0	0	0.3	0.3	12.1	1.8	84.4	35.7	29	4.93	3.07	1.22	5.79	1.09	0.41	32.2	8.45	6.07	0.92	0.46	2.89	261.0	157.4	200.4	60.7	0.32	0.26	26.1
FG_SM_T19	CCZ05634	574601.0	6452990.0	0	0.3	0.3	13.7	1.9	84.5	41.5	34.6	5.92	3.95	1.34	6.61	1.24	0.48	38.1	9.89	7.45	1.01	0.55	3.64	289.8	186.0	217.5	72.3	0.34	0.28	27.8
FG_SM_T20	CCZ05635	574600.0	6452790.0	0	0.3	0.3	18.3	2.6	104.5	51.5	36.1	6.3	3.94	1.32	7.3	1.31	0.46	46.2	12	9.12	1.06	0.53	3.63	343.3	214.9	267.7	75.5	0.32	0.28	27.9
FG_SM_U12	CCZ05636	574800.0	6454396.0	0	0.3	0.3	17.9	2.4	108.5	51.6	37.6	6.73	3.74	1.49	7.61	1.33	0.51	46.7	12.8	9.28	1.15	0.58	3.54	352.9	219.6	274.5	78.4	0.32	0.28	27.9
FG_SM_U13	CCZ05637	574799.0	6454196.0	0	0.3	0.3	16.6	2.3	98.9	48.7	49.7	8.11	5.28	1.5	9.26	1.82	0.75	46.1	11.95	9.47	1.45	0.8	5.15	360.1	238.6	257.8	102.3	0.36	0.28	28.0
FG_SM_U14	CCZ05638	574802.0	6453995.0	0	0.3	0.3	12.5	2.0	75.1	37.5	42.2	6.24	4.31	1.12	6.31	1.49	0.59	33.9	8.91	6.78	0.99	0.71	4.43	278.0	185.8	194.4	83.6	0.37	0.27	26.5
FG_SM_U15	CCZ05639	574800.0	6453795.0	0	0.3	0.3	14.8	2.3	79.5	37.4	42	6.89	4.58	1.24	6.76	1.57	0.61	35.5	9.28	7.26	1.15	0.71	4.48	288.0	190.4	202.6	85.5	0.37	0.27	27.1
FG_SM_U16	CCZ05640	574803.0	6453599.0	0	0.3	0.3	14.5	2.1	84.8	42.7	37.9	6.2	3.87	1.33	6.34	1.3	0.56	37.9	10.05	7.54	1.06	0.58	3.72	296.1	192.0	219.3	76.8	0.35	0.27	27.3
FG_SM_U17	CCZ05641	574800.0	6453399.0	0	0.3	0.3	14.5	2.2	88.7	44.5	32.5	5.49	3.37	1.23	6.04	1.17	0.49	38.8	10.6	7.47	0.98	0.52	3.1	294.9	185.9	227.9	67.0	0.32	0.28	27.5
FG_SM_U18	CCZ05642	574800.0	6453199.0	0	0.3	0.3	13.4	2.1	78.3	38.8	32.3	5.35	3.28	1.2	5.69	1.09	0.46	35.1	9.27	7.11	0.86	0.45	3.09	267.7	171.6	202.1	65.7	0.34	0.28	27.7
FG_SM_U19	CCZ05643	574799.0	6453000.0	0	0.3	0.3	17.1	2.3	104.5	51	38.2	6.25	3.78	1.44	7.53	1.33	0.6	45.3	12.3	9.02	1.11	0.61	3.63	345.0	216.7	266.3	78.7	0.32	0.28	27.6
FG_SM_U20	CCZ05644	574801.0	6452798.0	0	0.3	0.3	18.4	2.9	105.5	50.5	38.3	6.25	3.97	1.39	7.23	1.35	0.57	45.7	12.2	8.94	1.1	0.57	3.64	345.8	216.2	267.2	78.6	0.32	0.28	27.5
FG_SM_V12	CCZ05645	574999.0	6454394.0	0	0.3	0.3	12.1	1.6	71.3	36.2	27.8	4.74	2.82	1.11	5.23	0.93	0.41	31.8	8.52	6.49	0.83	0.42	2.58	242.2	154.6	185.0	57.2	0.33	0.28	27.8
FG_SM_V13	CCZ05646	575001.0	6454190.0	0	0.3	0.3	15.0	2.2	105	50.3	44.2	7.19	4.65	1.25	7.83	1.55	0.67	45.2	12.1	8.95	1.24	0.66	4.09	355.3	226.3	265.7	89.6	0.34	0.27	27.1
FG_SM_V14	CCZ05647	574999.0	6453995.0	0	0.3	0.3	12.7	1.9	72.8	37.3	38.3	6.21	3.82	1.32	6.08	1.32	0.56	32.9	9.01	6.89	0.99	0.57	3.78	267.4	177.9	190.4	76.9	0.36	0.27	27.1
FG_SM_V15	CCZ05648	574999.0	6453792.0	0	0.3	0.3	15.8	3.3	130.5	64.6	63	10.85	6.35	2.31	11.9	2.23	0.88	62	16.3	13.05	1.84	0.97	5.99	473.0	312.7	343.2	129.8	0.36	0.29	28.6
FG_SM_V16	CCZ05649	575004.0	6453591.0	0	0.3	0.3	16.2	2.7	100	49.9	39.1	6.6	4.1	1.33	7.36	1.37	0.62	43.5	11.6	8.71	1.1	0.61	3.81	336.8	213.9	256.2	80.5	0.33	0.27	27.4
FG_SM_V17	CCZ05650	575000.0	6453393.0	0	0.3	0.3	14.5	2.3	88.5	45.1	36.8	6.15	3.83	1.35	6.56	1.32	0.55	40.8	10.6	7.87	1.02	0.55	3.52	306.4	197.7	231.1	75.3	0.34	0.28	27.9
FG_SM_V18	CCZ05651	575001.0	6453195.0	0	0.3	0.3	14.5	2.4	80	40	31.4	5.28	3.21	1.23	5.69	1.09	0.46	34.6	9.37	7.09	0.9	0.49	3.18	269.7	171.4	205.1	64.6	0.33	0.27	27.3
FG_SM_V19	CCZ05652	574999.0	6452991.0	0	0.3	0.3	13.1	2.2	73.9	36.6	31.2	5.23	3.23	1.04	5.29	1.08	0.49	32	8.7	6.42	0.88	0.49	3.14	252.6	161.8	189.0	63.6	0.34	0.27	27.1
FG_SM_V20	CCZ05653	575001.0	6452793.0	0	0.3	0.3	15.2	2.2	82.2	41.6	34.3	5.31	3.46	1.07	5.99	1.13	0.49	36.5	9.89	7.19	0.86	0.5	3.22	281.5	180.5	212.6	68.9	0.34	0.27	27.3
FG_SM_W12	CCZ05654	575202.0	6454400.0	0	0.3	0.3	16.3	2.3	93.7	45.8	39.4	6.58	4.06	1.37	7.54	1.43	0.57	42.3	11.35	8.53	1.16	0.61	3.97	323.1	208.0	241.8	81.4	0.34	0.28	28.0
FG_SM_W13	CCZ05655	575203.0	6454197.0	0	0.3	0.3	19.5	2.4	91.8	43.7	41.6	6.6	4.21	1.24	7.31	1.43	0.63	39.8	10.8	8.39	1.1	0.64	4.12	317.4	204.6	233.2	84.1	0.35	0.27	27.3
FG_SM_W14	CCZ05656	575203.0	6453997.0	0	0.3	0.3	13.2	2.3	93.2	46.2	40	6.6	4.11	1.41	7.1	1.44	0.58	41.3	11.05	8.3	1.1	0.58	3.75	321.2	206.8	239.8	81.4	0.34	0.27	27.5
FG_SM_W15	CCZ05657	575200.0	6453793.0	0	0.3	0.3	12.5	2.4	106	50.7	49	8.36	4.86	1.79	9.19	1.71	0.71	47.7	12.05	10.15	1.45	0.73	4.46	372.1	241.9	271.6	100.4	0.35	0.28	27.9
FG_SM_W16	CCZ05658	575203.0	6453593.0	0	0.3	0.3	15.8	2.7	102.5	52.5	42.6	6.76	4.16	1.46	7.46	1.4	0.67	44.8	12.2	9.06	1.2	0.67	4.17	351.2	225.3	265.0	86.2	0.33	0.27	27.1
FG_SM_W17	CCZ05659	575198.0	6453396.0	0	0.3	0.3	14.6	2.1	90.2	47.8	30.3	5.44	3.08	1.5	6.4	1.08	0.43	42.7	11.85	8.4	0.94	0.47	2.71	304.5	193.7	240.7	63.8	0.32	0.29	29.1
FG_SM_W18	CCZ05660	575201.0	6453200.0	0	0.3	0.3	15.7	3.0	98.4	52.8	38.7	6.24	4	1.44	7.08	1.36	0.58	43.3	11.8	8.71	1.06	0.61	3.95	337.0	216.2	257.7	79.4	0.33	0.27	27.1
FG_SM_W19	CCZ05661	575204.0	6452996.0	0	0.3	0.3	12.4	1.9	69.2	35.5	34	5.23	3.68	1.21	5.16	1.15	0.61	32.4	8.49	6.17	0.81	0.59	3.75	250.5	165.5	181.8	68.6	0.36	0.27	27.2
FG_SM_W20	CCZ05662	575202.0	6452795.0	0	0.3	0.3	13.7	2.4	58.2	32	28.9	4.49	3.02	0.95	4.72	0.96	0.47	26.4	7.33	5.19	0.7	0.45	3.13	213.1	141.6	154.7	58.4	0.35	0.27	26.8
FG_SM_X12	CCZ05663	575399.0	6454396.0	0	0.3	0.3	19.3	2.3	109	52.7	54.8	8.73	6.03	1.34	8.22	1.9	0.84	45.7	12.4	9.23	1.34	0.92	5.47	384.2	250.3	274.7	109.5	0.35	0.26	26.0
FG_SM_X13	CCZ05664	575400.0	6454192.0	0	0.3	0.3	15.4	3.0	99	48	51.2	8.67	5.28	1.3	8.88	1.83	0.74	44.1	11.7	9.48	1.51	0.81	4.8	358.3	236.7	254.5	103.9	0.36	0.27	27.5
FG_SM_X14	CCZ05665	575402.0	6453996.0	0	0.3	0.3	20.7	3.3	153	82.7	56.1	9.61	5.75	1.85	9.91	2.06	0.86	62.8	17.2	12.25	1.62	0.83	5.35	507.9	319.9	393.2	114.7	0.31	0.26	26.1
FG_SM_X15	CCZ05666	575400.0	6453795.0	0	0.3	0.3	15.6	2.6	98.8	50.4	34.2	5.79	3.24	1.36	6.92	1.18	0.47	42.2	11.35	8.32	1	0.49	3.09	323.5	202.2	253.1	70.5	0.32	0.27	27.3
FG_SM_X16	CCZ05667	575399.0	6453591.0	0	0.3	0.3	15.1	2.8	112.5	59.4	42.4	7.17	4.39	1.72	8.12	1.48	0.62	49.2	13.3	9.16	1.21	0.66	4.07	379.6	241.4	291.9	87.7	0.32	0.27	27.2
FG_SM_X17	CCZ05668	575402.0	6453394.0	0	0.3	0.3	13.7	2.3	98.5	49.7	32.3	5.61	3.28	1.55	6.79	1.16	0.49	43.3	11.75	8.75	1.01	0.47	3.27	322.3	201.3	254.1	68.2	0.31	0.28	28.0
FG_SM_X18	CCZ05669	575404.0	6453192.0	0	0.3	0.3	13.9	2.5	126.5	53.2	45.3	7.54	5	1.95	8.49	1.59	0.76	53.9	13.7	11	1.3	0.74	4.77	404.4	249.0	310.0	94.4	0.33	0.28	27.7
FG_SM_X19	CCZ05670	575398.0	6452993.0	0	0.3	0.3	17.1	2.7	106.5	50.9	37.6	6.32	3.96	1.52	7.16	1.28	0.56	44.9	12.25	8.79	1.07	0.54	3.71	345.6	214.8	267.9	77.7	0.32	0.27	27.2
FG_SM_X20	CCZ05671	575400.0	6452792.0	0	0.3	0.3	14.7	2.5	96.4	47.4	37.4	5.94	3.85	1.5	6.75	1.28	0.58	41.6	11.45	8.28	1.03	0.59	3.64	322.4	203.9	246.0	76.4	0.33	0.27	27.2
FG_SM_Y12	CCZ05672	575600.0	6454397.0	0	0.3	0.3	18.1	2.5	111.5	57.8	45.3	8.02	4.8	1.54	8.88	1.63	0.63	52.8	14.2	10.35	1.36	0.71	4.23	389.5	252.6	295.5	94.0	0.34	0.29	28.7
FG_SM_Y13	CCZ05673	575592.0	6454191.0	0	0.3	0.3	11.1	2.5	102	51.6	42.3	7.62	4.41	1.46	8.1	1.51	0.65	46.3	11.95	9.22	1.26	0.69	4.13	352.9	227.6	264.9	88.0	0.34	0.28	28.0

FG_SM_Y14	CCZ05674	575600.0	6453999.0	0	0.3	0.3	18.3	2.9	125.5	63.1	50.9	8.5	5.34	1.58	8.97	1.79	0.83	52.2	14.55	10.6	1.46	0.78	4.88	422.8	268.6	318.9	103.8	0.33	0.27	26.6
FG_SM_Y15	CCZ05675	575599.0	6453797.0	0	0.3	0.3	14.3	2.7	112	59.1	41.9	6.45	4.12	1.5	7.47	1.36	0.62	49.2	13.3	9.14	1.18	0.62	3.87	375.4	237.8	290.9	84.4	0.32	0.27	27.0
FG_SM_Y16	CCZ05676	575600.0	6453598.0	0	0.3	0.3	16.2	2.6	100.5	52.4	29.2	4.77	2.82	1.26	5.89	0.98	0.4	43.1	12.1	8	0.89	0.45	2.73	319.4	195.9	259.1	60.3	0.30	0.27	27.4
FG_SM_Y17	CCZ05677	575600.0	6453400.0	0	0.3	0.3	12.7	2.2	77.4	40.6	35.4	5.79	3.5	1.33	6.34	1.18	0.49	36.2	9.73	7.52	0.96	0.53	3.45	277.4	182.3	205.4	72.0	0.35	0.28	28.0
FG_SM_Y18	CCZ05678	575598.0	6453200.0	0	0.3	0.3	17.8	2.8	107.5	53.5	36.4	6.05	3.51	1.59	7.03	1.28	0.51	47.6	12.55	8.92	1.08	0.55	3.43	350.8	218.7	275.8	75.0	0.32	0.28	27.7
FG_SM_Y19	CCZ05679	575600.0	6452995.0	0	0.3	0.3	18.4	2.8	105	55.9	40.4	6.74	3.94	1.53	7.72	1.38	0.6	49.9	13.7	9.87	1.14	0.63	3.8	363.6	234.6	280.7	82.9	0.33	0.29	28.7
FG_SM_Y20	CCZ05680	575598.0	6452799.0	0	0.3	0.3	19.3	2.8	115	56	37.4	6.46	3.52	1.33	7.56	1.26	0.52	51.4	13.65	9.9	1.14	0.55	3.27	371.8	230.5	294.9	76.9	0.32	0.28	28.3
FG_SM_Z12	CCZ05681	575795.0	6454397.0	0	0.3	0.3	17.7	2.8	126.5	65.3	61.7	9.72	5.93	1.61	10.45	2.09	0.82	58.5	15.85	11.7	1.71	0.88	5.55	455.8	300.4	332.9	122.9	0.35	0.28	27.7
FG_SM_Z13	CCZ05682	575791.0	6454200.0	0	0.3	0.3	14.1	2.8	113.5	58.9	52.5	8.7	5.3	1.83	9.14	1.89	0.75	52.3	13.75	10.15	1.5	0.82	4.83	404.5	265.1	297.9	106.6	0.35	0.28	27.6
FG_SM_Z14	CCZ05683	575806.0	6453995.0	0	0.3	0.3	14.3	2.0	85.7	43.9	36.2	6.8	3.96	1.48	6.8	1.34	0.5	41.2	11	8.07	1.16	0.59	3.6	303.6	198.3	227.5	76.1	0.35	0.29	28.9
FG_SM_Z15	CCZ05684	575799.0	6453795.0	0	0.3	0.3	13.1	2.9	129	66.4	32.1	5.82	3.12	1.54	7.34	1.11	0.4	51.4	15.1	9.37	1.12	0.43	2.8	393.4	234.9	325.4	68.0	0.28	0.27	26.8
FG_SM_Z16	CCZ05685	575799.0	6453594.0	0	0.3	0.3	12.9	2.5	78.7	39.8	30.8	5.46	3.33	1.33	5.92	1.2	0.46	36.5	9.66	7.18	0.96	0.48	3.1	270.6	173.9	205.9	64.7	0.33	0.28	28.4
FG_SM_Z17	CCZ05686	575797.0	6453396.0	0	0.3	0.3	12.4	2.3	83.3	45.3	44.8	6.7	4.24	1.61	7.39	1.49	0.62	41.2	10.75	8.02	1.18	0.61	3.91	314.6	212.2	225.8	88.8	0.37	0.28	28.0
FG_SM_Z18	CCZ05687	575798.0	6453193.0	0	0.3	0.3	17.2	2.7	111.5	54	49	7.87	5	1.77	8.66	1.69	0.72	48.5	13	9.51	1.33	0.76	4.85	383.3	246.4	283.6	99.7	0.34	0.27	27.1
FG_SM_Z19	CCZ05688	575802.0	6452992.0	0	0.3	0.3	18.1	3.0	108	55.1	45.8	7.17	4.48	1.29	7.39	1.53	0.65	47.6	13.1	8.86	1.26	0.72	4.4	370.2	237.6	278.9	91.3	0.34	0.27	27.0
FG_SM_Z20	CCZ05689	575800.0	6452800.0	0	0.3	0.3	17.3	2.7	118.5	60.5	35.5	6	3.5	1.42	7.06	1.2	0.49	50.2	14.25	9.27	1.07	0.53	3.32	376.4	230.8	303.0	73.3	0.30	0.27	27.3
FG_SM_AA12	CCZ05690	576000.0	6454400.0	0	0.3	0.3	13.0	2.0	86.6	44.2	42.2	6.77	4.39	1.26	7.2	1.49	0.59	40.6	10.5	8.41	1.22	0.64	3.95	313.2	206.8	228.0	85.2	0.36	0.28	27.9
FG_SM_AA13	CCZ05691	576002.0	6454198.0	0	0.3	0.3	13.7	2.0	100.5	54.3	41.8	7.15	4.24	1.64	7.97	1.53	0.59	49.3	13.35	9.68	1.32	0.63	3.93	358.4	234.9	272.0	86.4	0.34	0.29	29.0
FG_SM_AA14	CCZ05692	575997.0	6453998.0	0	0.3	0.3	15.0	2.9	107.5	53.9	36.6	6.55	4.24	1.34	7.24	1.42	0.55	46.4	12.65	9.51	1.18	0.56	4.08	353.4	221.3	275.7	77.7	0.31	0.28	27.6
FG_SM_AA15	CCZ05693	575999.0	6453799.0	0	0.3	0.3	10.4	3.3	130.5	65.2	39.8	7.79	4.09	1.94	8.2	1.51	0.47	57.6	15.4	9.7	1.21	0.66	3.95	418.6	258.3	333.8	84.8	0.31	0.28	27.9
FG_SM_AA16	CCZ05694	576003.0	6453601.0	0	0.3	0.3	13.7	2.1	85	44.6	30.6	5.37	3.05	1.38	6.23	1.06	0.44	38.5	10.5	7.5	0.93	0.46	2.89	286.9	182.5	223.0	63.9	0.32	0.28	28.1
FG_SM_AA17	CCZ05695	575999.0	6453398.0	0	0.3	0.3	12.0	2.1	72.6	38	29.7	5.09	2.99	1.14	5.74	1.04	0.46	33.4	8.92	6.18	0.89	0.44	2.79	252.0	162.8	190.7	61.4	0.34	0.28	27.9
FG_SM_AA18	CCZ05696	575999.0	6453197.0	0	0.3	0.3	15.3	2.6	92.9	48.1	40.7	6.28	3.88	1.33	6.74	1.32	0.63	42.6	11.5	8.04	1.12	0.63	4.03	324.9	210.8	243.4	81.5	0.34	0.27	27.5
FG_SM_AA19	CCZ05697	576006.0	6453003.0	0	0.3	0.3	17.3	2.8	106.5	54.2	33.3	5.53	3.12	1.39	7.01	1.13	0.45	46.4	12.75	8.77	1.07	0.49	2.93	342.9	212.1	274.1	68.9	0.31	0.28	27.8
FG_SM_AA20	CCZ05698	576002.0	6452797.0	0	0.3	0.3	13.4	2.2	84.2	44.4	28.4	4.58	2.85	1.46	5.98	0.94	0.41	38.6	10.65	7.17	0.9	0.42	2.63	280.9	177.5	221.7	59.2	0.32	0.28	28.3
FG_SM_AB12	CCZ05699	576200.0	6454398.0	0	0.3	0.3	17.9	2.6	107.5	54	45.8	7.49	4.82	1.27	8.23	1.52	0.63	49	13.4	9.79	1.36	0.72	4.47	373.3	241.2	280.1	93.2	0.34	0.28	28.0
FG_SM_AB13	CCZ05700	576202.0	6454197.0	0	0.3	0.3	14.8	2.1	91.3	48	37.5	6.21	3.66	1.42	7.19	1.33	0.54	42.5	11.3	8.53	1.1	0.56	3.45	318.4	206.3	241.6	76.9	0.34	0.28	28.2
FG_SM_AB14	CCZ05701	576201.0	6453998.0	0	0.3	0.3	13.8	2.4	105.5	57.5	37.7	6.32	3.64	1.68	7.73	1.29	0.48	48.3	13.15	9.83	1.18	0.53	3.27	358.5	228.9	280.7	77.9	0.32	0.28	28.2
FG_SM_AB15	CCZ05702	576201.0	6453797.0	0	0.3	0.3	11.2	3.4	105	62.5	39.9	6.13	3.61	1.51	7.17	1.28	0.54	45.7	12.75	8.12	1.1	0.54	3.39	360.1	231.1	280.4	79.7	0.32	0.26	26.3
FG_SM_AB16	CCZ05703	576200.0	6453598.0	0	0.3	0.3	14.0	2.5	87.8	45.4	27.4	4.54	2.82	1.2	5.8	0.96	0.4	39	10.7	6.88	0.9	0.45	2.7	285.0	177.1	227.5	57.5	0.31	0.28	27.8
FG_SM_AB17	CCZ05704	576199.0	6453396.0	0	0.3	0.3	12.5	2.2	71.6	37.4	32	5.21	3.4	1.12	5.66	1.09	0.44	33.6	8.73	6.47	0.87	0.46	3.05	254.2	166.2	189.1	65.1	0.35	0.28	27.8
FG_SM_AB18	CCZ05705	576200.0	6453195.0	0	0.3	0.3	18.8	3.2	117.5	60.1	58.4	9.2	5.97	1.63	8.77	1.98	0.92	51.2	14.25	9.62	1.54	0.96	5.71	419.2	274.8	302.9	116.3	0.35	0.26	26.4
FG_SM_AB19	CCZ05706	576200.0	6452999.0	0	0.3	0.3	19.1	3.2	116	59.6	38	6.34	3.74	1.43	7.55	1.28	0.52	50.3	14.1	9.61	1.16	0.58	3.57	377.6	235.1	299.2	78.3	0.31	0.28	27.6
FG_SM_AB20	CCZ05707	576198.0	6452797.0	0	0.3	0.3	18.3	3.2	109.5	56.5	36.6	5.95	3.55	1.43	7.49	1.22	0.52	47.2	12.85	8.51	1.09	0.55	3.5	356.8	222.3	281.2	75.5	0.31	0.27	27.2
FG_SM_AC12	CCZ05708	576403.0	6454399.0	0	0.3	0.3	14.6	2.0	78.2	40.5	34.7	5.59	3.5	1.21	5.74	1.18	0.5	36.2	9.62	7.25	0.95	0.56	3.4	275.9	179.8	205.8	70.0	0.35	0.28	27.7
FG_SM_AC13	CCZ05709	576402.0	6454197.0	0	0.3	0.3	11.2	1.8	89.1	46	31	5.27	3.16	1.63	6.34	1.08	0.43	40.6	11.25	8.08	0.99	0.5	2.87	298.7	189.2	233.7	65.0	0.32	0.28	28.4
FG_SM_AC14	CCZ05710	576402.0	6453998.0	0	0.3	0.3	14.2	2.2	86.4	44.4	30.5	5.04	2.81	1.28	5.56	1.07	0.44	38.9	10.45	7.4	0.88	0.42	2.72	286.7	180.6	224.8	62.0	0.32	0.28	27.8
FG_SM_AC15	CCZ05711	576400.0	6453794.0	0	0.3	0.3	11.8	3.9	143.5	72.2	43.3	7.85	4.42	1.94	9.23	1.61	0.6	60.7	15.65	11.2	1.38	0.63	4.12	455.1	278.9	363.6	91.5	0.30	0.27	27.2
FG_SM_AC16	CCZ05712	576403.0	6453599.0	0	0.3	0.3	16.2	2.6	113	55.1	32.2	5.92	3.02	1.45	6.86	1.17	0.44	48.9	13	8.85	0.99	0.44	2.95	354.0	215.2	286.4	67.6	0.30	0.28	27.9
FG_SM_AC17	CCZ05713	576402.0	6453397.0	0	0.3	0.3	15.8	2.3	101	50.8	36.2	6.39	3.55	1.56	7.35	1.33	0.48	46.8	12.2	8.94	1.09	0.51	3.34	338.7	214.7	263.3	75.4	0.33	0.29	28.6
FG_SM_AC18	CCZ05714	576401.0	6453199.0	0	0.3	0.3	15.7	2.7	102	50.8	44.5	7.27	4.54	1.28	7.67	1.57	0.67	46.5	11.85	8.65	1.16	0.65	4.42	353.5	228.2	263.5	90.1	0.34	0.27	27.5
FG_SM_AC19	CCZ05715	576402.0	6452999.0	0	0.3	0.3	18.9	3.1	116.5	56.5	32.5	6.02	3.33	1.42	7.73	1.2	0.44	51.5	13.9	9.53	1.11	0.44	3.09	367.0	223.9	297.3	69.7	0.30	0.29	28.6
FG_SM_AC20	CCZ05716	576398.0	6452800.0	0	0.3	0.3	20.2	3.7	229	115	38.4	7.22	3.71	2.02	9.82	1.41	0.5	89.7	25.5	14.7	1.4	0.49	3.34	651.8	370.5	568.7	83.1	0.25	0.27	26.7
FG_SM_AD12	CCZ05717	576600.0	6454399.0	0	0.3	0.3	13.3	2.4	93.4	45.4	33.6	5.62	3.4	1.24	6.4	1.25	0.48	40.3	10.5	6.98	0.96	0.5	3.37	305.1	190.4	235.8	69.3	0.32	0.27	27.1
FG_SM_AD13	CCZ05718	576602.0	6454197.0	0	0.3	0.3	11.7	2.0	87.8	44.2	37.8	7.21	4.01	1.62	7.6	1.36	0.48	44.6	11.75	8.29	1.22	0.58	3.58	315.3	207.4	235.5	79.8	0.35	0.30	29.9
FG_SM_AD14	CCZ05719	576601.0	6453992.0	0	0.3	0.3	14.1	2.3	89.4	46	37.3	6.8	4.11	1.7	6.92	1.4	0.57	45	11.7	8.21	1.12	0.59	3.97	318.5	208.7	239.9	78.6	0.35	0.29	29.3
FG_SM_AD15	CCZ05720	576602.0	6453794.0	0	0.3	0.3	12.3	3.9	93	52.4	28.1	5.2	3.25	1.34	6.16	1.06	0.39	40.9	11.2	7.4	0.93	0.46	2.88	306.1	191.9	245.5	60.6	0.30	0.27	27.4
FG_SM_AD16	CCZ05721	576601.0	6453596.0	0	0.3	0.3	15.0	2.7	93	45.2	32.1	6.16	3.42	1.46	6.65	1.26	0.47	43.6	11.5	7.9	1.06	0.48	3.09	309.6	195.3	241.2	68.4	0.33	0.29	29.0
FG_SM_AD17	CCZ05722	576600.0	6453393.0	0	0.3	0.3	17.1	2.9	114	53.6	40.4	7.1	4.41	1.6	7.79	1.38	0.59	50.8	13.4	9.16	1.17	0.59	3.78	372.9	232.9	289.0	83.9	0.33	0.28	28.0
FG_SM_AD18	CCZ05723	576602.0	6453193.0	0	0.3	0.3	20.1	3.3	124.5	61.3	42.1	7.57	4.49	1.58	8.14	1.46	0.61	56.6	15.75	10.35	1.38	0.6	3.94	409.5	256.6	321.9	87.7	0.32	0.29	28.5
FG_SM_AD19	CCZ05724	576599.0	6452995.0	0	0.3	0.3	21.3	3.8	145	70.6	40.8	7.01	3.87	1.61	8.29	1.41	0.52	62.1	16.6	11.4	1.24	0.57	3.85	451.0	272.9	366.6	84.4	0.30	0.28	27.7
FG_SM_AD20	CCZ05725	576600.0	6452793.0	0	0.3	0.3	20.7	3.8	153.5	75.7	41	7.44	4.05	1.77	8.8	1.48	0.59	65.1	17.5	11.25	1.32	0.57	3.67	473.6	285.1	387.5	86.2	0.30	0.28	27.5
FG_SM_AE12	CCZ05726	576799.0	6454395.0	0	0.3	0.3	13.5	1.8	78.4	39.5	30.4	5.28	3.17	1.22	6.08	1.09	0.44	38.1	9.65	6.89	0.87	0.44	3	270.1	173.8	206.7	63.4	0.34	0.29	28.9

FG_SM_AE13	CCZ05727	576803.0	6454195.0	0	0.3	0.3	15.4	2.3	104	51.4	37.5	6.69	3.86	1.52	7.17	1.38	0.51	47.9	12.55	9.12	1.14	0.54	3.49	347.5	219.7	269.6	77.8	0.33	0.28	28.5
FG_SM_AE14	CCZ05728	576803.0	6453996.0	0	0.3	0.3	15.1	2.4	101.5	51.5	34.7	6.15	3.59	1.4	7.13	1.27	0.54	46.3	11.9	8.5	1.09	0.51	3.35	336.1	211.5	263.3	72.8	0.32	0.28	28.2
FG_SM_AE15	CCZ05729	576802.0	6453796.0	0	0.3	0.3	12.4	2.2	78.4	40.3	28.3	4.86	2.88	1.16	5.53	1.01	0.39	35.6	9.42	6.97	0.84	0.42	2.64	263.2	166.9	204.6	58.6	0.32	0.28	28.1
FG_SM_AE16	CCZ05730	576800.0	6453594.0	0	0.3	0.3	14.1	2.7	120	55.6	48.3	7.72	4.79	1.66	7.99	1.76	0.74	52	13.45	9.33	1.3	0.73	4.79	397.8	250.4	300.3	97.5	0.34	0.27	27.0
FG_SM_AE17	CCZ05731	576803.0	6453397.0	0	0.3	0.3	15.1	2.6	119.5	55.8	35.6	6.22	3.66	1.52	7.33	1.29	0.46	52.1	13.55	9.36	1.1	0.49	3.29	374.6	227.8	300.2	74.3	0.31	0.28	28.0
FG_SM_AE18	CCZ05732	576802.0	6453196.0	0	0.3	0.3	22.1	3.4	147	69.4	40.2	7.46	3.9	1.6	8.73	1.42	0.53	62.3	16.6	11.25	1.28	0.56	3.7	452.3	271.7	367.7	84.6	0.30	0.28	27.8
FG_SM_AE19	CCZ05733	576805.0	6453000.0	0	0.3	0.3	20.1	3.5	167	77.4	37.6	6.71	3.65	1.68	8.65	1.4	0.5	68	18.4	11.75	1.26	0.55	3.6	491.0	285.9	411.1	79.9	0.28	0.27	27.4
FG_SM_AE20	CCZ05734	576803.0	6452797.0	0	0.3	0.3	20.9	3.7	134	64.4	48.5	8	4.98	1.55	8.49	1.66	0.76	58.8	15.4	10.15	1.26	0.79	5.08	438.1	273.5	339.1	99.0	0.33	0.27	27.3
FG_SM_AF12	CCZ05735	577004.0	6454394.0	0	0.3	0.3	15.0	2.1	88.3	42.7	38	6.3	3.83	1.2	6.62	1.36	0.53	40.4	10.45	7.3	1.02	0.57	3.83	304.0	195.6	226.8	77.3	0.35	0.28	27.7
FG_SM_AF13	CCZ05736	577002.0	6454198.0	0	0.3	0.3	16.7	2.8	138	64.4	42.6	7.64	4.23	1.67	8.67	1.56	0.66	60.7	16.05	10.9	1.32	0.63	3.9	436.8	267.2	347.9	88.9	0.31	0.28	28.2
FG_SM_AF14	CCZ05737	577001.0	6453993.0	0	0.3	0.3	15.2	2.9	105	51.5	29.8	5.56	3.04	1.26	6.42	1.15	0.41	44.9	11.95	7.82	0.97	0.45	2.77	328.4	199.4	265.3	63.2	0.30	0.28	27.6
FG_SM_AF15	CCZ05738	577001.0	6453795.0	0	0.3	0.3	15.6	2.6	113	57.1	34	6.15	3.24	1.44	7.25	1.18	0.44	51.2	13.5	9.06	1.07	0.45	3.08	363.4	224.6	292.3	71.1	0.31	0.28	28.4
FG_SM_AF16	CCZ05739	577001.0	6453595.0	0	0.3	0.3	16.9	2.7	125.5	61.7	36.8	6.77	3.87	1.66	8.06	1.36	0.46	55.8	14.7	10.05	1.24	0.5	3.42	399.2	245.0	321.0	78.1	0.31	0.28	28.3
FG_SM_AF17	CCZ05740	577003.0	6453394.0	0	0.3	0.3	18.6	3.6	122.5	60	53.5	8.35	5.75	1.37	8.18	1.88	0.82	53.1	14	9.46	1.32	0.87	5.57	417.8	267.3	310.7	107.1	0.34	0.26	26.4
FG_SM_AF18	CCZ05741	577004.0	6453196.0	0	0.3	0.3	20.0	3.2	135	66.3	37.2	6.58	3.71	1.51	8.01	1.35	0.48	59	15.85	10.6	1.22	0.5	3.22	421.6	255.8	343.9	77.8	0.30	0.28	28.1
FG_SM_AF19	CCZ05742	577001.0	6452996.0	0	0.3	0.3	21.8	3.9	146.5	72.1	42.6	7.7	4.28	1.8	9.27	1.55	0.58	64	17.05	12.05	1.33	0.63	4.03	463.6	283.7	373.7	89.9	0.30	0.28	28.1
FG_SM_AF20	CCZ05743	577004.0	6452793.0	0	0.3	0.3	16.9	3.0	106	51.8	33.3	6.01	3.13	1.43	6.8	1.17	0.42	46.6	12.35	8.63	1	0.44	3.03	339.5	209.2	270.2	69.2	0.31	0.28	28.0
FG_SM_AG12	CCZ05744	577200.0	6454399.0	0	0.3	0.3	12.5	2.0	93.3	44.8	41.4	7.32	4.16	1.34	7.5	1.49	0.58	42.9	11.15	8.26	1.2	0.59	3.84	325.0	210.4	240.2	84.8	0.35	0.28	28.2
FG_SM_AG13	CCZ05745	577200.0	6454200.0	0	0.3	0.3	19.0	2.7	106	52.9	37.7	6.73	4.23	1.4	7.36	1.36	0.55	48.9	12.5	9.34	1.26	0.57	3.82	354.4	224.2	275.2	79.2	0.33	0.28	28.4
FG_SM_AG14	CCZ05746	577201.0	6454000.0	0	0.3	0.3	17.9	3.0	123.5	60.3	33.9	5.78	3.42	1.59	7.59	1.26	0.47	53	13.9	9.17	1.12	0.48	3.33	383.5	231.8	311.7	71.8	0.30	0.28	27.6
FG_SM_AG15	CCZ05747	577201.0	6453800.0	0	0.3	0.3	16.7	2.8	112	53.8	35.5	6.35	3.73	1.46	7.36	1.3	0.51	47.3	12.75	9.41	1.14	0.57	3.71	357.3	219.7	282.2	75.1	0.31	0.28	27.6
FG_SM_AG16	CCZ05748	577203.0	6453597.0	0	0.3	0.3	15.6	2.4	101	49	32.4	5.78	3.45	1.27	6.2	1.2	0.47	43.6	11.6	8.09	1.03	0.51	3.23	323.5	199.4	255.8	67.7	0.31	0.28	27.6
FG_SM_AG17	CCZ05749	577202.0	6453396.0	0	0.3	0.3	15.7	2.8	101	50.3	47.5	7.56	5.04	1.53	7.37	1.7	0.71	45	11.95	8.97	1.18	0.76	4.88	356.0	231.9	260.4	95.6	0.35	0.27	26.9
FG_SM_AG18	CCZ05750	577202.0	6453199.0	0	0.3	0.3	15.5	2.9	106	53.2	37.3	6.15	3.85	1.48	6.86	1.32	0.62	45.7	12.15	8.25	1.08	0.6	3.96	347.3	217.1	270.2	77.1	0.32	0.27	27.0
FG_SM_AG19	CCZ05751	577202.0	6452995.0	0	0.3	0.3	19.1	3.3	121	58.9	47.8	7.8	4.7	1.52	7.97	1.6	0.72	51.9	14.1	9.84	1.28	0.72	4.65	402.9	254.3	306.7	96.2	0.33	0.27	27.0
FG_SM_AG20	CCZ05752	577203.0	6452796.0	0	0.3	0.3	17.9	3.3	104.5	50.2	38.9	6.49	3.94	1.37	6.88	1.37	0.62	45.4	11.9	8.61	1.14	0.58	3.79	344.0	215.7	264.6	79.5	0.33	0.27	27.3
FG_SM_AH12	CCZ05753	577402.0	6454398.0	0	0.3	0.3	13.2	1.9	80.5	40	29.1	5.13	3.13	1.28	5.87	1.06	0.44	37	9.63	7.38	0.88	0.45	2.83	270.3	171.4	209.1	61.2	0.33	0.29	28.5
FG_SM_AH13	CCZ05754	577399.0	6454196.0	0	0.3	0.3	14.3	2.7	89.2	43.9	32.5	5.66	3.52	1.31	5.73	1.14	0.47	39.3	10.4	7.56	0.98	0.5	3.41	295.6	186.0	228.2	67.4	0.33	0.28	27.5
FG_SM_AH14	CCZ05755	577399.0	6453998.0	0	0.3	0.3	16.4	2.7	93.3	46.3	28.9	5.21	2.92	1.28	6	1.04	0.39	41.4	10.5	7.77	0.9	0.45	2.69	299.6	185.0	238.9	60.7	0.31	0.28	28.0
FG_SM_AH15	CCZ05756	577400.0	6453799.0	0	0.3	0.3	15.7	3.7	131.5	64.8	37	6.96	3.87	1.75	8.12	1.38	0.52	57.6	15.35	10.4	1.17	0.53	3.41	414.1	252.6	335.3	78.8	0.30	0.28	28.1
FG_SM_AH16	CCZ05757	577397.0	6453596.0	0	0.3	0.3	17.1	2.9	111	55.6	42.8	7.15	4.25	1.6	8.05	1.5	0.66	50.7	13.15	9.63	1.22	0.67	4.37	375.9	239.6	287.8	88.2	0.33	0.28	28.0
FG_SM_AH17	CCZ05758	577401.0	6453397.0	0	0.3	0.3	14.4	2.4	110	54.2	36.7	6.4	3.71	1.53	7.31	1.32	0.53	48.7	12.8	9.22	1.1	0.53	3.48	358.0	222.9	281.7	76.4	0.32	0.28	27.9
FG_SM_AH18	CCZ05759	577402.0	6453194.0	0	0.3	0.3	18.9	3.2	149	70.6	34.4	6.46	3.47	1.69	8.13	1.3	0.46	61.7	16.6	11.2	1.15	0.51	3.18	444.8	261.8	370.8	74.0	0.28	0.28	27.7
FG_SM_AH19	CCZ05760	577398.0	6452998.0	0	0.3	0.3	19.6	3.8	121	58.9	51.7	8.19	5.42	1.56	8.45	1.84	0.84	52.4	13.9	10.55	1.36	0.81	5.43	412.4	263.8	307.9	104.6	0.34	0.27	26.9
FG_SM_AH20	CCZ05761	577395.0	6452801.0	0	0.3	0.3	17.9	2.9	107.5	52.7	38.1	6.63	3.9	1.54	7.3	1.34	0.52	47	12.25	8.94	1.16	0.6	3.78	353.0	220.9	273.8	79.1	0.32	0.28	27.6
FG_SM_AI12	CCZ05762	577600.0	6454397.0	0	0.3	0.3	16.3	2.1	101	49	35.8	6.42	3.8	1.46	6.99	1.34	0.52	45.3	11.8	9.08	1.08	0.58	3.61	334.3	210.2	259.2	75.1	0.32	0.28	28.2
FG_SM_AI13	CCZ05763	577601.0	6454195.0	0	0.3	0.3	16.5	2.7	117.5	64.2	46.1	8.03	4.82	1.69	9.28	1.67	0.76	57.9	15.25	11	1.4	0.73	4.63	414.8	270.5	318.3	96.5	0.33	0.29	29.0
FG_SM_AI14	CCZ05764	577601.0	6453997.0	0	0.3	0.3	16.4	2.8	99.7	48.7	33.6	6.19	3.34	1.35	6.59	1.18	0.49	43.1	11.5	8.36	0.98	0.49	3.54	323.9	201.4	253.4	70.4	0.32	0.28	27.7
FG_SM_AI15	CCZ05765	577603.0	6453799.0	0	0.3	0.3	15.5	3.0	125.5	60.9	34.6	6.23	3.5	1.64	7.49	1.22	0.48	56.5	14.85	10.25	1.12	0.55	3.45	394.8	240.6	321.3	73.4	0.30	0.29	28.6
FG_SM_AI16	CCZ05766	577602.0	6453600.0	0	0.3	0.3	18.7	2.8	108.5	56.2	38.2	6.75	3.89	1.6	7.58	1.42	0.58	51.3	13.6	9.96	1.15	0.61	3.84	367.0	233.7	287.0	80.0	0.33	0.29	28.8
FG_SM_AI17	CCZ05767	577600.0	6453400.0	0	0.3	0.3	17.0	2.7	109.5	53.1	32.8	5.93	3.35	1.52	7.01	1.24	0.51	46.3	12.4	9.23	1.01	0.51	3.32	346.2	211.6	276.5	69.7	0.30	0.28	27.7
FG_SM_AI18	CCZ05768	577599.0	6453198.0	0	0.3	0.3	18.6	3.6	139	67.9	42.5	7.56	4.35	1.67	8.37	1.62	0.63	56.9	15	10.5	1.28	0.63	4.26	435.9	265.2	347.0	88.9	0.30	0.27	26.7
FG_SM_AI19	CCZ05769	577601.0	6452999.0	0	0.3	0.3	14.6	2.3	90.8	45.1	33.9	5.96	3.34	1.33	6.26	1.2	0.47	41.9	10.8	8.2	0.98	0.51	3.4	305.8	194.3	235.9	70.0	0.33	0.28	28.3
FG_SM_AI20	CCZ05770	577602.0	6452799.0	0	0.3	0.3	16.0	2.7	97.8	47.2	34.2	5.84	3.35	1.3	6.31	1.18	0.5	41.9	11.2	8.54	0.98	0.51	3.08	317.7	197.6	247.8	69.9	0.32	0.28	27.5
FG_SM_AJ12	CCZ05771	577802.0	6454397.0	0	0.3	0.3	12.6	2.0	78.9	38.9	33.8	5.67	3.39	1.29	5.94	1.19	0.53	36.9	9.32	7.25	0.94	0.5	3.31	274.3	177.4	205.3	69.1	0.35	0.28	28.1
FG_SM_AJ13	CCZ05772	577802.0	6454194.0	0	0.3	0.3	13.8	2.2	93.2	45.9	32.7	6.14	3.36	1.36	6.75	1.16	0.46	44.2	11.55	8.74	1	0.5	3.29	313.1	198.6	244.0	69.1	0.33	0.29	29.3
FG_SM_AJ14	CCZ05773	577800.0	6454000.0	0	0.3	0.3	14.8	2.9	98.6	50	35	6.17	3.66	1.3	6.43	1.29	0.48	44.3	11.7	8.41	0.99	0.56	3.49	327.8	206.6	255.3	72.4	0.32	0.28	27.8
FG_SM_AJ15	CCZ05774	577802.0	6453794.0	0	0.3	0.3	13.9	2.5	81.6	40.2	31.3	5.21	3.2	1.19	5.8	1.1	0.45	37	9.52	6.72	0.88	0.46	3.14	274.2	174.0	209.8	64.4	0.33	0.28	27.8
FG_SM_AJ16	CCZ05775	577803.0	6453599.0	0	0.3	0.3	14.5	2.5	88.9	44.6	36.4	6.13	3.65	1.32	6.35	1.25	0.57	39.9	10.15	7.7	0.95	0.57	3.85	303.8	194.6	229.2	74.5	0.34	0.27	27.4
FG_SM_AJ17	CCZ05776	577803.0	6453395.0	0	0.3	0.3	14.8	2.3	96.4	47	33	5.82	3.31	1.39	6.5	1.2	0.44	42.4	11	8.65	1.05	0.5	3.26	315.2	196.8	246.3	68.9	0.32	0.28	28.0
FG_SM_AJ18	CCZ05777	577803.0	6453196.0	0	0.3	0.3	18.7	3.1	132.5	64.1	35.3	6.35	3.33	1.52	7.66	1.26	0.46	56	15.05	10.3	1.12	0.55	3.26	407.5	244.8	333.4	74.1	0.30	0.28	27.7
FG_SM_AJ19	CCZ05778	577804.0	6452998.0	0	0.3	0.3	15.4	2.6	97.9	46.9	36.8	6.15	3.87	1.35	6.76	1.26	0.63	42.8	11.1	7.96	1.06	0.61	3.84	323.9	203.6	247.8	76.0	0.33	0.27	27.4
FG_SM_AJ20	CCZ05779	577806.0	6452797.0	0	0.3	0.3	19.0	2.7	109	52.8	35.3	6.32	3.35	1.48	7.78	1.26	0.52	48.7	12.7	9.08	1.08	0.49	3.26	352.7	218.8	278.5	74.2	0.32	0.28	28.4

FG_SM_AK12	CCZ05780	577999.0	6454401.0	0	0.3	0.3	15.1	2.5	89.1	43.1	34.2	5.45	3.5	1.28	6.25	1.21	0.51	40.5	10.8	8.19	0.93	0.5	3.46	299.7	190.3	229.8	69.9	0.33	0.28	28.1
FG_SM_AK13	CCZ05781	578003.0	6454202.0	0	0.3	0.3	12.2	2.1	76.3	37.2	29.2	5.03	2.85	1.3	5.37	1.01	0.45	34.7	9.07	7.09	0.86	0.45	2.97	257.4	163.7	197.0	60.4	0.33	0.28	28.2
FG_SM_AK14	CCZ05782	578000.0	6454000.0	0	0.3	0.3	14.0	2.6	94.4	46	42.1	6.87	4.39	1.4	6.2	1.49	0.69	41.3	10.95	7.87	1.08	0.67	4.71	325.5	209.5	240.4	85.0	0.35	0.27	26.7
FG_SM_AK15	CCZ05783	578003.0	6453798.0	0	0.3	0.3	14.9	2.4	96.6	47.6	34.8	6.12	3.56	1.52	6.82	1.25	0.57	43.5	11.6	8.91	1.04	0.51	3.39	322.2	203.6	249.6	72.7	0.33	0.28	28.3
FG_SM_AK16	CCZ05784	578001.0	6453601.0	0	0.3	0.3	14.9	2.4	99.5	48.8	37	6.11	3.69	1.48	6.92	1.27	0.54	44.1	11.9	8.58	1.06	0.55	3.53	331.1	208.9	255.2	75.9	0.33	0.28	27.8
FG_SM_AK17	CCZ05785	578003.0	6453400.0	0	0.3	0.3	14.8	2.4	90.3	44.7	35.8	5.99	3.79	1.5	6.32	1.29	0.6	40.6	10.75	7.96	0.97	0.57	3.98	307.1	196.2	232.9	74.2	0.33	0.28	27.6
FG_SM_AK18	CCZ05786	578001.0	6453200.0	0	0.3	0.3	16.7	2.8	105.5	54.8	37.9	6.53	3.83	1.45	6.98	1.32	0.59	45.5	12.2	8.79	1.06	0.56	3.87	350.1	220.5	271.9	78.2	0.32	0.27	27.1
FG_SM_AK19	CCZ05787	578003.0	6452998.0	0	0.3	0.3	16.6	2.5	102.5	49.2	34.9	6.03	3.59	1.42	7.02	1.27	0.46	46	12.3	8.74	1.02	0.48	3.33	334.9	209.0	262.3	72.6	0.32	0.28	28.3
FG_SM_AK20	CCZ05788	578003.0	6452793.0	0	0.3	0.3	19.2	3.0	127.5	61.5	36.4	6.41	3.46	1.84	8.02	1.28	0.48	58.3	15.7	10.95	1.2	0.48	3.32	405.1	248.5	328.4	76.7	0.31	0.29	29.1
FG_SM_AL12	CCZ05789	578197.0	6454400.0	0	0.3	0.3	14.4	2.0	84.5	42	31.5	5.59	3.19	1.43	6.39	1.17	0.45	38.5	10.2	7.81	0.96	0.47	3.08	285.5	181.7	219.3	66.1	0.33	0.28	28.4
FG_SM_AL13	CCZ05790	578199.0	6454196.0	0	0.3	0.3	11.6	1.9	74.2	38	31.9	4.89	3.09	1.28	5.46	1.06	0.48	34.2	8.88	6.49	0.85	0.44	3.02	258.0	166.8	193.9	64.1	0.34	0.28	27.5
FG_SM_AL14	CCZ05791	578199.0	6453998.0	0	0.3	0.3	12.6	2.1	86.3	42.5	33.8	5.73	3.48	1.34	6.02	1.22	0.49	39.9	10.65	7.84	0.99	0.49	3.53	294.0	188.0	224.4	69.7	0.34	0.28	28.3
FG_SM_AL15	CCZ05792	578199.0	6453798.0	0	0.3	0.3	15.0	2.3	121.5	63.4	33.6	5.58	3.26	1.5	6.53	1.14	0.47	51.9	14.9	8.81	0.98	0.48	3.21	381.6	232.4	312.4	69.3	0.29	0.27	27.2
FG_SM_AL16	CCZ05793	578200.0	6453600.0	0	0.3	0.3	13.2	2.7	107	55.9	33.4	5.83	3.31	1.46	7	1.19	0.47	47.4	13.1	8.9	1.03	0.48	3.22	348.4	217.0	278.4	70.0	0.31	0.28	28.0
FG_SM_AL17	CCZ05794	578200.0	6453400.0	0	0.3	0.3	20.1	3.3	137.5	66.9	39.3	7.07	4.07	1.83	8.71	1.44	0.55	62	16.95	11.85	1.22	0.56	3.56	437.1	268.2	353.9	83.2	0.31	0.29	28.9
FG_SM_AL18	CCZ05795	578198.0	6453200.0	0	0.3	0.3	21.6	3.5	130.5	62.6	44	7.35	4.67	1.63	8.11	1.51	0.72	57.9	15.4	10.75	1.22	0.69	4.59	423.2	262.9	332.3	90.9	0.32	0.28	27.8
FG_SM_AL19	CCZ05796	578202.0	6452996.0	0	0.3	0.3	16.5	2.5	97.6	50.1	42.7	6.97	4.4	1.62	7.35	1.48	0.64	46.6	11.95	9.15	1.2	0.63	4.2	345.0	225.1	258.1	86.9	0.35	0.28	28.2
FG_SM_AL20	CCZ05797	578206.0	6452796.0	0	0.3	0.3	18.4	3.4	125.5	59.4	33.7	5.89	3.37	1.42	6.8	1.18	0.52	51.5	14.1	9.62	1.03	0.52	3.39	382.6	228.4	312.1	70.5	0.29	0.27	27.2
FG_SM_AM12	CCZ05798	578401.0	6454397.0	0	0.3	0.3	14.3	2.3	91.7	45.1	35	5.9	3.43	1.44	6.43	1.18	0.52	41.8	11.05	8	0.97	0.52	3.44	308.7	196.1	236.9	71.8	0.33	0.28	28.1
FG_SM_AM13	CCZ05799	578398.0	6454195.0	0	0.3	0.3	13.4	1.9	74.9	37	28.8	4.96	2.98	1.35	5.42	1.01	0.42	34.4	9.21	7.06	0.86	0.43	3	254.9	162.9	194.8	60.0	0.33	0.28	28.4
FG_SM_AM14	CCZ05800	578402.0	6453997.0	0	0.3	0.3	16.9	2.1	90.1	42.7	33.7	5.48	3.28	1.24	5.89	1.14	0.45	40.9	10.65	8.18	0.92	0.42	3.12	298.8	188.1	230.8	68.0	0.33	0.28	28.2
FG_SM_AM15	CCZ05801	578400.0	6453800.0	0	0.3	0.3	13.7	2.3	117	57	41.3	6.92	4	1.44	7.23	1.43	0.55	47.7	12.9	9.4	1.15	0.58	3.99	376.5	232.8	292.7	83.8	0.32	0.26	26.5
FG_SM_AM16	CCZ05802	578401.0	6453596.0	0	0.3	0.3	22.6	3.6	115	56.6	31.1	5.8	3.28	1.22	6.9	1.15	0.46	48.4	13.55	9.59	1.06	0.46	3.14	358.0	216.8	291.6	66.5	0.29	0.28	27.9
FG_SM_AM17	CCZ05803	578402.0	6453395.0	0	0.3	0.3	12.3	2.6	82.5	40.1	29.7	5.05	2.97	1.19	5.54	1.1	0.47	36.3	9.76	7.47	0.84	0.46	2.98	272.5	171.2	211.2	61.4	0.32	0.28	27.9
FG_SM_AM18	CCZ05804	578398.0	6453196.0	0	0.3	0.3	16.4	3.5	106	53.1	41.4	7.04	4.2	1.7	7.76	1.47	0.62	49.9	12.95	9.76	1.2	0.61	3.82	362.9	232.7	277.7	85.2	0.34	0.29	28.6
FG_SM_AM19	CCZ05805	578400.0	6452994.0	0	0.3	0.3	14.9	3.1	96.6	48.1	34.7	5.77	3.49	1.35	6.24	1.21	0.5	43.3	11.25	8.36	1.02	0.53	3.3	319.8	201.2	248.9	71.0	0.33	0.28	27.8
FG_SM_AM20	CCZ05806	578402.0	6452797.0	0	0.3	0.3	16.6	2.6	99.9	53	37.1	6	3.63	1.5	7.02	1.29	0.51	45	12.15	8.79	1.08	0.49	3.37	337.9	215.2	262.2	75.7	0.32	0.28	27.7
FG_SM_AN12	CCZ05807	578598.0	6454396.0	0	0.3	0.3	13.9	2.2	76.5	37.8	36.7	5.74	3.64	1.16	6.03	1.27	0.59	35.5	9.45	7.17	0.95	0.56	3.72	273.2	179.2	199.4	73.8	0.36	0.28	27.7
FG_SM_AN13	CCZ05808	578600.0	6454197.0	0	0.3	0.3	15.2	2.3	84.9	43	37.1	6.28	3.82	1.22	6.42	1.35	0.57	40.3	10.6	7.92	0.99	0.57	3.97	299.8	195.5	223.7	76.0	0.35	0.28	28.3
FG_SM_AN14	CCZ05809	578600.0	6453994.0	0	0.3	0.3	16.9	3.0	113	58.1	51	8.69	5.24	1.28	8.76	1.82	0.75	53.6	14.2	10.2	1.36	0.78	5.27	402.2	263.4	298.5	103.7	0.35	0.28	28.1
FG_SM_AN15	CCZ05810	578599.0	6453795.0	0	0.3	0.3	19.5	5.5	113.5	55.4	43.2	7.4	4.41	1.47	7.3	1.47	0.73	49	12.95	9.25	1.19	0.71	4.8	376.6	237.2	287.9	88.7	0.33	0.27	27.0
FG_SM_AN16	CCZ05811	578599.0	6453597.0	0	0.3	0.3	13.3	2.8	100.5	49.8	31.7	5.53	3.12	1.32	6.13	1.08	0.52	44	11.85	8.22	0.95	0.45	3.34	323.1	199.6	257.0	66.0	0.31	0.28	27.8
FG_SM_AN17	CCZ05812	578600.0	6453397.0	0	0.3	0.3	13.5	2.6	94	44.6	37.6	6.16	3.54	1.58	7.17	1.35	0.54	42.3	10.85	8.36	1.06	0.59	3.81	317.3	201.8	239.9	77.4	0.34	0.28	28.0
FG_SM_AN18	CCZ05813	578603.0	6453197.0	0	0.3	0.3	14.2	2.4	87	42.6	34.8	5.73	3.57	1.2	6.32	1.22	0.54	39.2	10.35	7.64	0.99	0.54	3.42	295.1	188.3	223.9	71.2	0.34	0.28	27.8
FG_SM_AN19	CCZ05814	578599.0	6452996.0	0	0.3	0.3	15.2	3.3	104	51.5	38.7	6.83	4.15	1.64	7.36	1.44	0.55	46.9	12.55	9.19	1.18	0.58	3.59	349.2	221.4	268.7	80.5	0.33	0.28	28.1
FG_SM_AN20	CCZ05815	578600.0	6452794.0	0	0.3	0.3	16.9	3.0	99.3	50.4	38.9	6.37	4.14	1.46	7.01	1.42	0.57	46	12.35	8.75	1.14	0.62	3.75	339.6	217.6	259.8	79.8	0.33	0.28	28.1
FG_SM_V22	CCZ05816	574999.0	6452396.0	0	0.3	0.3	15.9	2.3	95.6	46.8	32.9	5.6	3.69	1.25	6.19	1.17	0.47	45.5	11.35	8.64	0.93	0.55	2.95	317.1	199.7	249.1	68.0	0.33	0.29	28.8
FG_SM_V24	CCZ05817	575004.0	6451998.0	0	0.3	0.3	19.3	2.8	104	50.8	30.7	5.76	3.46	1.34	6.99	1.15	0.44	47.8	12	9.51	1.04	0.42	2.64	334.3	206.5	268.6	65.7	0.31	0.29	29.1
FG_SM_V26	CCZ05818	575000.0	6451593.0	0	0.3	0.3	12.9	1.9	65.3	33.9	23.7	4.3	2.71	0.91	4.61	0.89	0.37	32.1	7.83	6.3	0.71	0.37	2.31	224.0	143.8	174.2	49.8	0.33	0.29	29.1
FG_SM_V28	CCZ05819	574997.0	6451196.0	0	0.3	0.3	14.2	2.2	77.7	39.1	32.1	5.26	3.59	1.14	5.92	1.16	0.53	38.6	9.68	7.32	0.89	0.55	3.13	272.7	177.3	206.5	66.2	0.35	0.29	29.0
FG_SM_V30	CCZ05820	575000.0	6450798.0	0	0.3	0.3	12.8	1.9	71.5	35.7	27.9	4.76	3.18	1.12	5.29	1.02	0.44	35	8.7	6.8	0.79	0.44	2.79	247.1	159.3	188.9	58.2	0.34	0.29	29.0
FG_SM_X22	CCZ05821	575400.0	6452404.0	0	0.3	0.3	14.9	2.4	99.5	46.8	28.5	5.07	3.07	1.56	6.69	1.03	0.38	46.6	11.7	9.41	0.93	0.4	2.41	317.5	195.2	256.5	60.9	0.31	0.30	29.6
FG_SM_X24	CCZ05822	575401.0	6452002.0	0	0.3	0.3	16.4	1.9	65.9	33.5	26	4.08	2.73	1.01	5.02	0.94	0.39	32.6	8	6.02	0.76	0.36	2.36	228.2	147.3	174.9	53.3	0.34	0.29	28.9
FG_SM_X26	CCZ05823	575398.0	6451601.0	0	0.3	0.3	15.6	2.6	112	50.7	35.2	6.31	4.16	1.68	7.48	1.37	0.53	51.2	13.2	9.88	1.11	0.59	3.22	359.3	221.7	284.2	75.1	0.32	0.29	29.0
FG_SM_X28	CCZ05824	575404.0	6451203.0	0	0.3	0.3	17.5	2.9	97.4	46.5	33.8	5.53	3.97	1.16	6.63	1.26	0.54	44	11.5	8.69	0.99	0.51	3.46	320.0	200.4	249.5	70.5	0.32	0.28	28.3
FG_SM_X30	CCZ05825	575398.0	6450803.0	0	0.3	0.3	15.4	2.4	77.4	37.5	31.4	5.02	3.39	1.04	5.51	1.06	0.45	36	9.23	6.81	0.87	0.48	2.88	263.7	168.7	200.1	63.6	0.34	0.28	28.1
FG_SM_Z22	CCZ05826	575800.0	6452401.0	0	0.3	0.3	17.0	2.8	101	48.3	30.1	5.37	3.15	1.25	6.53	1.14	0.43	45.6	11.75	9.2	0.97	0.43	2.76	322.3	198.2	258.8	63.5	0.31	0.29	28.8
FG_SM_Z24	CCZ05827	575803.0	6451997.0	0	0.3	0.3	14.6	2.3	100	48.8	29.9	5.33	3.53	1.5	6.65	1.12	0.42	47.2	12.35	9.19	0.94	0.44	2.64	324.6	201.8	260.7	63.9	0.31	0.29	29.4
FG_SM_Z26	CCZ05828	575798.0	6451599.0	0	0.3	0.3	17.2	2.8	100.5	47.7	36.9	6.12	4.45	1.28	6.65	1.38	0.59	46.4	11.75	8.64	1.03	0.57	3.63	334.1	210.6	257.7	76.4	0.33	0.28	28.2
FG_SM_Z28	CCZ05829	575801.0	6451202.0	0	0.3	0.3	15.7	2.4	91.7	45.4	34	5.77	3.97	1.2	6.48	1.2	0.5	45	11.25	8.5	0.97	0.51	3.35	312.5	199.9	241.8	70.7	0.34	0.29	29.2
FG_SM_Z30	CCZ05830	575802.0	6450799.0	0	0.3	0.3	15.3	2.4	80.9	41.4	33.2	5.66	3.83	1.3	6.33	1.24	0.49	40.3	10	7.73	0.98	0.51	3.41	285.4	186.0	216.0	69.4	0.34	0.29	29.1
FG_SM_AB22	CCZ05831	576199.0	6452399.0	0	0.3	0.3	13.0	2.4	82.9	41.2	28	5	3.17	1.41	5.57	0.97	0.33	38.6	9.6	7.18	0.8	0.41	2.45	273.8	171.9	215.1	58.7	0.32	0.29	28.5
FG_SM_AB24	CCZ05832	576198.0	6451999.0	0	0.3	0.3	18.0	3.1	108	50.8	34.6	6.03	3.64	1.4	6.95	1.2	0.51	48	12.2	9.16	1.07	0.49	3.33	345.8	213.1	273.6	72.2	0.32	0.28	28.2

FG_SM_AB26	CCZ05833	576201.0	6451598.0	0	0.3	0.3	16.8	2.5	96.5	49.3	33.3	5.83	3.78	1.32	6.93	1.2	0.51	48.7	12.1	8.73	1	0.53	2.99	327.9	209.3	257.9	70.0	0.33	0.30	29.7
FG_SM_AB28	CCZ05834	576201.0	6451197.0	0	0.3	0.3	15.6	2.6	106.5	50.7	32.6	5.7	3.71	1.51	6.67	1.18	0.43	49.6	12.35	9.57	1.03	0.49	2.94	342.7	211.9	274.2	68.6	0.32	0.29	29.0
FG_SM_AB30	CCZ05835	576201.0	6450798.0	0	0.3	0.3	12.4	1.9	66.5	32	29.4	4.62	3.41	1.12	5.22	1.02	0.39	33.1	7.8	6.39	0.86	0.46	2.71	234.7	153.1	174.7	60.1	0.36	0.29	28.9
FG_SM_POC	CCZ05836	575129.0	6451468.0	0	0.3	0.3	18.0	2.9	103.5	52.2	36.1	5.57	4.15	1.5	7.31	1.28	0.6	49.9	12.8	9.52	1.06	0.61	3.64	348.4	221.3	273.1	75.4	0.33	0.29	28.9

Notes:

1. Verification has been undertaken by CCZ Geology team personnel.
2. Sample results from ALS method ME-ICP81.

Source: ALS Adelaide.

APPENDIX D: JORC CODE, 2012 EDITION – TABLE 1 – FENCE GOSSAN SURFACE SAMPLING

Section 1: Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	*Nature and quality of sampling (e.g., cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.* *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* *Aspects of the determination of mineralisation that are Material to the Public Report.* *In cases where 'industry standard' work has been done this would be relatively simple (e.g., 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	**Diamond Drilling (DDH)** Diamond drilling of HQ diameter (TT_005DD) was completed to 137.7m recently in the completed program and was located 5m away from a RC hole already drilled (TT_003RC). **Reverse Circulation ('RC') Drilling** RC drilling at Fence Gossan was used to obtain a representative sample by means of riffle splitting with samples submitted for analysis using the above-mentioned methodologies. Four (4) reverse circulation (RC) holes for a total of 516m have been completed at the Fence Gossan Prospect. Four (4) RC holes were completed at Reefs Tank for a total of 564m. At Tors Tank, four (4) RC holes for a total of 625.7m (including the cored hole) were completed. The RC drilling technique was used to obtain a representative sample by means of a cone or riffle splitter with samples submitted for assay by mixed acid digestion and analysis via ICP-MS + ICP-AES with anticipated reporting a suite of 48 elements (sulphur >10% by LECO) **Surface Sampling** Two large surface sampling programs were conducted on grids based about the drilling at Tors Tank and Fence Gossan. The sampling was by using hand auger to take soil samples from depth varying between

		0.1-0.5m. Original samples were between 0.5-2kg in weight, reduced to 200g for crushing and pulverizing. The Stage 1 program consisted of 189 sampling stations, spaced at 200m intervals across a total survey area measuring 6.4km^2 The first area was based about the centre of the grid, closest to the known points of observations (drill holes FG001RC-4RC). Stations extended east of the Resource Mask to the EL8434 lease boundary. Stations also extended west to identify extension of REEs into the Reef Tank Resource Area. Station numbers are based on a wider grid that incorporates Reef Tank and Tors Tank. A Stage 2 second area at a larger spacing (400m) was completed slighter later in December 2022, which managed to collect another 21 samples over mainly pegmatite outcrop.
Drilling techniques	*Drill type (e.g., core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g., core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	Historical drilling consisted of auger, rotary air blast, reverse circulation, and NQ, BQ, and HQ diamond coring. One cored hole of HQ (61mm) diameter was completed at Tors Tank after all the RC holes had been completed. Diamond drilling was completed with standard diameter, conventional HQ, with historical holes typically utilizing RC and percussion pre-collars to an average 30 metres (see drillhole information for further details).
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.* *Measures taken to maximise sample recovery and ensure representative nature of the samples.* *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	Reverse Circulation ('RC') Drilling - Reverse circulation sample recoveries were visually estimated during drilling programs. Where the estimated sample recovery was below 100% this was recorded in field logs by means of qualitative observation. Reverse circulation drilling employed sufficient air (using a compressor and booster) to maximise sample recovery. Historical cored drillholes by North Broken Hill, CRA , and Pasminco were well documented and generally have >90% core recovery.

		No relationship between sample recovery and grade has been observed.
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* *The total length and percentage of the relevant intersections logged.*	The drilling that did occur was completed to modern-day standards. The preferred exploration strategy in the eighties and early nineties was to drill shallow auger holes to negate the influence of any Quaternary and Tertiary sedimentary cover, and then return to sites where anomalous Cu or Zn were assayed. In this program at all three areas holes were completed to varying depths ranging from 100-160m. No downhole geophysical logging took place; however, measurements of magnetic susceptibility were taken at the same 1m intervals as the PXRF readings were taken.
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.* *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* *For all sample types, the nature, quality, and appropriateness of the sample preparation technique.* *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* *Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.* *Whether sample sizes are appropriate to the grain size of the material being sampled.*	Core samples will be hand-split or sawn with re-logging of available historical core indicating a 70:30 (retained: assayed) split was typical. The variation of sample ratios noted are considered consistent with the sub-sampling technique (hand-splitting). No second half samples will be submitted for analysis, but duplicates have been taken at a frequency of 1:20 in samples collected. It is considered water planned to be used for core cutting is unprocessed and unlikely to have introduced sample contamination. Procedures relating to the definition of the line of cutting or splitting are not available. It is expected that 'standard industry practice' for the period was applied to maximize sample representivity. Quarter core will be submitted to ALS for chemical analysis using industry standard sample preparation and analytical techniques. The sample interval details and grades quoted for cored intervals described in various maps in the main section are given in previous ASX releases (Castillo Copper 2022a, b, c, d, e, f, g).

Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	The following rare earth elements were analysed using ME-MS61R Sample Decomposition is by HF-HNO_3-$HClO_4$ acid digestion, HCl leach (GEO-4A01). The Analytical Method for Silver is shown below: **Element** | **Symbol** | **Units** | **Lower Limit** | **Upper Limit** **Silver** | Ag | ppm | 0.01 | 100 **Inductively Coupled Plasma - Atomic Emission Spectroscopy (ICP - AES) Inductively Coupled Plasma - Mass Spectrometry (ICP-MS)** A prepared sample (0.25 g) is digested with perchloric, nitric, hydrofluoric, and hydrochloric acids. The residue is topped up with dilute hydrochloric acid and analysed by inductively coupled plasma atomic emission spectrometry. Following this analysis, the results are reviewed for high concentrations of bismuth, mercury, molybdenum, silver, and tungsten and diluted accordingly. Samples meeting this criterion are then analysed by inductively coupled plasma-mass spectrometry. Results are corrected for spectral interelement interferences. Four acid digestions can dissolve most minerals: however, although the term “near total” is used, depending on the sample matrix, not all elements are quantitatively extracted. Results for the additional rare earth elements will represent the acid leachable portion of the rare earth elements and as such, cannot be used, for instance to do a chondrite plot. **Geochemical Procedure** Element geochemical procedure reporting units and limits are listed below:

Element	Symb	Units	Lower Limit	Upper Limit
Aluminum	Al	%	0.01	50
Arsenic	As	ppm	0.2	10 000
Barium	Ba	ppm	10	10 000
Beryllium	Be	ppm	0.05	1 000
Bismuth	Bi	ppm	0.01	10 000
Calcium	Ca	%	0.01	50
Cadmium	Cd	ppm	0.02	1 000
Cerium	Ce	ppm	0.01	500
Cobalt	Co	ppm	0.1	10 000
Chromium	Cr	ppm	1	10 000
Cesium	Cs	ppm	0.05	500
Copper	Cu	ppm	0.2	10 000
Iron	Fe	%	0.01	50
Gallium	Ga	ppm	0.05	10 000
Germanium	Ge	ppm	0.05	500
Hafnium	Hf	ppm	0.1	500
Indium	In	ppm	0.005	500
Potassium	K	%	0.01	10
Lanthanum	La	ppm	0.5	10 000
Lithium	Li	ppm	0.2	10 000

Magnesium	Mg	%	0.01	50

Element	Symbol	Units	Lower Limit	Upper Limit
Molybdenum	Mo	ppm	0.05	10 000
Sodium	Na	%	0.01	10
Niobium	Nb	ppm	0.1	500
Nickel	Ni	ppm	0.2	10 000
Phosphorous	P	ppm	10	10 000
Lead	Pb	ppm	0.5	10 000
Rubidium	Rb	ppm	0.1	10 000
Rhenium	Re	ppm	0.002	50
Sulphur	S	%	0.01	10
Antimony	Sb	ppm	0.05	10 000
Scandium	Sc	ppm	0.1	10 000
Selenium	Se	ppm	1	1 000
Tin	Sn	ppm	0.2	500
Strontium	Sr	ppm	0.2	10 000
Tantalum	Ta	ppm	0.05	100
Tellurium	Te	ppm	0.05	500
Thorium	Th	ppm	0.2	10 000
Titanium	Ti	%	0.005	10
Thallium	Tl	ppm	0.02	10 000
Uranium	U	ppm	0.1	10 000
Vanadium	V	ppm	1	10 000
Tungsten	W	ppm	0.1	10 000

Method ME-MS81

This method involves a lithium borate fusion prior to acid dissolution and ICP- MS analysis provides the most quantitative analytical approach for a broad suite of trace elements. Options for adding the whole rock elements from an |CP - AES analysis on the same fusion, or base metals from a separate four acid digestion, are available.

Lower and upper detection limits are given below:

Element	Symbol	Units	Lower Limit	Upper Limit
Yttrium	Y	ppm	0.1	500
Zinc	Zn	ppm	2	10 000
Zirconium	Zr	ppm	0.5	500
Dysprosium	Dy	ppm	0.05	1 000
Erbium	Er	ppm	0.03	1 000
Europium	Eu	ppm	0.03	1 000
Gadolinium	Gd	ppm	0.05	1 000
Holmium	Ho	ppm	0.01	1 000
Lutetium	Lu	ppm	0.01	1 000
Neodymium	Nd	ppm	0.1	1 000
Praseodymium	Pr	ppm	0.03	1 000
Samarium	Sm	ppm	0.03	1 000
Terbium	Tb	ppm	0.01	1 000
Thulium	Tm	ppm	0.01	1 000
Ytterbium	Yb	ppm	0.03	1 000

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- Laboratory inserted standards, blanks and duplicates were analysed per industry standard practice. There was no evidence of bias from these results.

</td>
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<tr>
<td>Verification of sampling and assaying</td>
<td>

The verification of significant intersections by either independent or alternative company personnel.

The use of twinned holes.

Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.

Discuss any adjustment to assay data.

</td>
<td>

- Two of the drillholes have been twinned, at Tors Tank where TT_005DD was drilled next to TT_003RC.
- Conversion of elemental analysis (REE parts per million) to stoichiometric oxide (REO parts per million) was undertaken by ROM geological staff using the below element to stoichiometric oxide conversion factors (https://www.jcu.edu.au/news/releases/2020/march/rare-earth-metals-an-untapped-resource)

Table C1-1: Element -Conversion Factor -Oxide Form

<table>
<tr><th></th><th></th><th></th></tr>
<tr><td>Ce</td><td>1.2284</td><td>CeO_2</td></tr>
<tr><td>Dy</td><td>1.1477</td><td>Dy_2O_3</td></tr>
<tr><td>Er</td><td>1.1435</td><td>Er_2O_3</td></tr>
<tr><td>Eu</td><td>1.1579</td><td>Eu_2O_3</td></tr>
<tr><td>Gd</td><td>1.1526</td><td>Gd_2O_3</td></tr>
<tr><td>Ho</td><td>1.1455</td><td>Ho_2O_3</td></tr>
<tr><td>La</td><td>1.1728</td><td>La_2O_3</td></tr>
<tr><td>Lu</td><td>1.1371</td><td>Lu_2O_3</td></tr>
<tr><td>Nd</td><td>1.1664</td><td>Nd_2O_3</td></tr>
<tr><td>Pr</td><td>1.2083</td><td>Pr_6O_{11}</td></tr>
<tr><td>Sm</td><td>1.1596</td><td>Sm_2O_3</td></tr>
<tr><td>Tb</td><td>1.1762</td><td>Tb_4O_7</td></tr>
<tr><td>Tm</td><td>1.1421</td><td>Tm_2O_3</td></tr>
<tr><td>Y</td><td>1.2699</td><td>Y_2O_3</td></tr>
<tr><td>Yb</td><td>1.1387</td><td>Yb_2O_3</td></tr>
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		Rare earth oxide is the industry accepted form for reporting rare earths. The following calculations are used for compiling REO into their reporting and evaluation groups: TREO (Total Rare Earth Oxide) = La_2O_3 + CeO_2 + Pr_6O_{11} + Nd_2O_3 + Sm_2O_3 + Eu_2O_3 + Gd_2O_3 + Tb_4O_7 + Dy_2O_3 + Ho_2O_3 + Er_2O_3 + Tm_2O_3 + Yb_2O_3 + Y_2O_3 + Lu_2O_3. TREO-Ce = TREO – CeO_2 LREO (Light Rare Earth Oxide) = La_2O_3 + CeO_2 + Pr_6O_{11} + Nd_2O_3 + Sm_2O_3 HREO (Heavy Rare Earth Oxide) = Eu_2O_3 + Gd_2O_3 + Tb_4O_7 + Dy_2O_3 + Ho_2O_3 + Er_2O_3 + Tm2O3 + Yb2O3 + Y2O3 + Lu2O3 CREO (Critical Rare Earth Oxide) = Nd_2O_3 + Eu_2O_3 + Tb_4O_7 + Dy_2O_3 + Y_2O_3 MREO (Magnetic Rare Earth Oxide) = Pr_6O_{11} + Nd_2O_3 + Sm_2O_3 + Gd_2O_3 + Tb_4O_7 + Dy_2O_3. **Total Rare Earth Oxides (TREO):** To calculate TREO an oxide conversion “factor” is applied to each rare-earth element assay. The “factor” equates an elemental assay to an oxide concentration for each element. Below is an example of the factor calculation for Lanthanum (La): ○ Relative Atomic Mass (La) = 138.9055 ○ Relative Atomic Mass (O) = 15.9994 ○ Oxide Formula = La_2O_3 ○ Oxide Conversion Factor = 1/ ((2x 138.9055)/(2x 138.9055 + 3x 15.9994)) Oxide Conversion Factor = 1.173 (3dp) None of the historical data has been adjusted.
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* *Specification of the grid system used.* *Quality and adequacy of topographic control.*	In general, locational accuracy does vary, depending upon whether the historical surface and drillhole samples were digitised off plans or had their coordinated tabulated. Many samples were originally reported to AGD66 or AMG84 and have been converted to MGA94 (Zone 54) The holes are currently surveyed with handheld GPS, awaiting more accurate DGPS survey. It is thus estimated that locational accuracy therefore varies between 2-4m until the more accurate

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<td>surveying is completed. This assessment was confirmed once the holes were surveyed by DGPS from GMC Surveying.

The quality of topographic control (GSNSW 1 sec DEM) is deemed adequate for the purposes of the exploration drilling program.</td>
</tr>
<tr>
<td>Data spacing and distribution</td>
<td>Data spacing for reporting of Exploration Results.

Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.

Whether sample compositing has been applied.</td>
<td>The average sample spacing from the current drilling program across the tenure varies per prospect, and sample type, as listed in Table C1-2, below:

Table C1-2: EL 8434 Drillhole Spacing
<table>
<tr><th>Prospect</th><th>Drillholes Completed</th><th>RMS Drillhole Spacing (m)</th></tr>
<tr><td>The Sisters</td><td>Not yet</td><td></td></tr>
<tr><td>Iron Blow</td><td>Not Yet</td><td></td></tr>
<tr><td>Tors Tank</td><td>4</td><td>127</td></tr>
<tr><td>Fence Gossan</td><td>4</td><td>208</td></tr>
<tr><td>Ziggy’s Hill</td><td>n/a</td><td>n/a</td></tr>
<tr><td>Reefs Tank</td><td>4</td><td>221</td></tr>
</table>

The Datamine software allows creation of fixed length samples from the original database given a set of stringent rules.

Sample location is shown in Figure C1.

Figure C1: Location of Stage 1 Fence Gossan Surface Samples</td>
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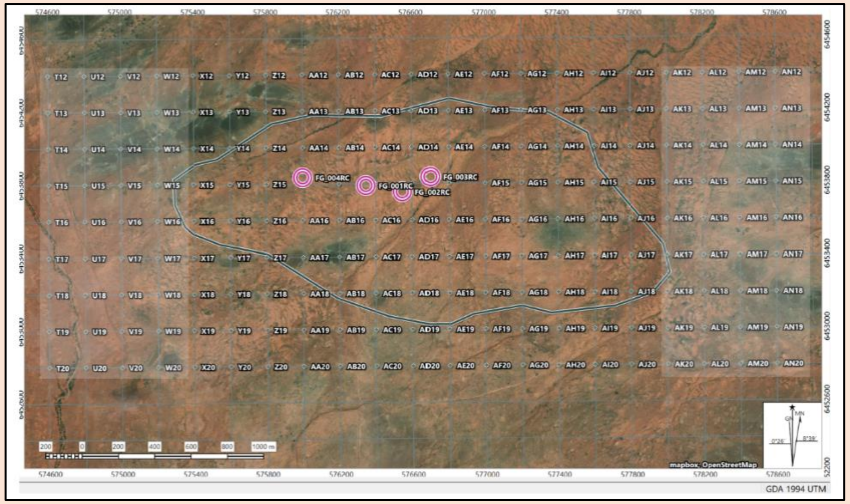
</table>

		
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	Historical drill holes at the BHAE are typically drilled vertically for auger and RAB types (drilled along section lines) and angled at -55˚ or -60˚ to the horizontal and drilled perpendicular to the mineralised trend for RC and DDH. Drilling orientations are adjusted along strike to accommodate folded geological sequences. All Fence Gossan holes were designed to drill toward grid south at an inclination of 60 degrees from horizontal. The drilling orientation is not considered to have introduced a sampling bias on assessment of the current geological interpretation. Geological mapping by various companies has reinforced that the strata dips variously between 5 and 65 degrees.
Sample security	*The measures taken to ensure sample security.*	Sample security procedures are considered 'industry standard' for the current period.

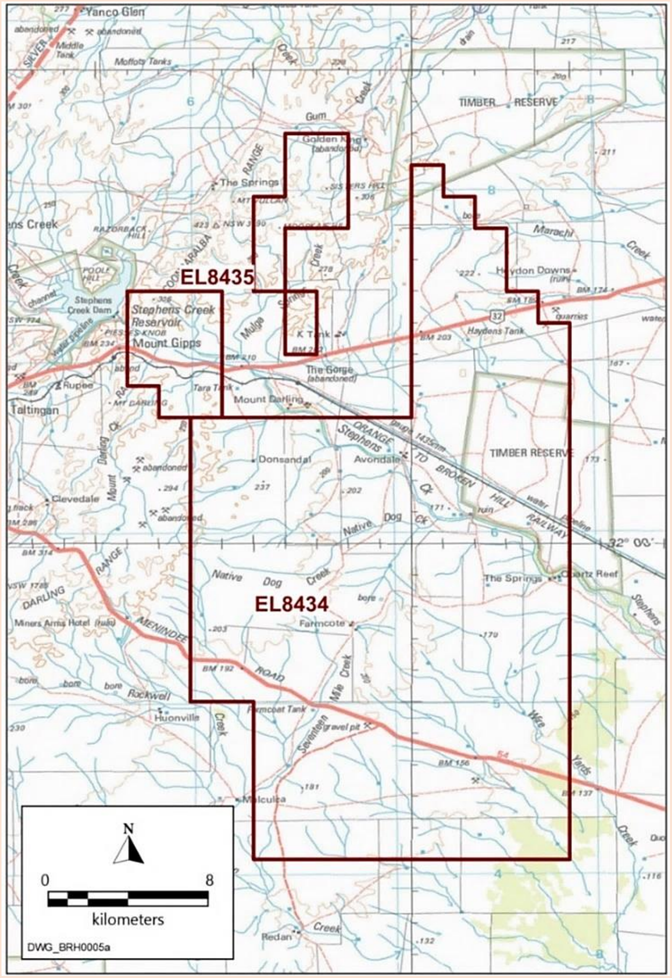
		Samples obtained during drilling completed between 4/10/22 to the 10/10/22 were transported by exploration employees or an independent courier directly from Broken Hill to ALS Laboratory, Adelaide. The Company considers that risks associated with sample security are limited given the nature of the targeted mineralisation.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	No external audits or reviews have yet been undertaken.

SECTION 2: REPORTING OF EXPLORATION RESULTS

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	EL 8434 is located about 28km east of Broken Hill whilst EL 8435 is 16km east of Broken Hill. Both tenures are approximately 900km northwest of Sydney in far western New South Wales (Figures C2-1 and C2-2 in Appendix A &B, above). EL 8434 and EL 8435 were both granted on the $2^{nd\ of}$ June 2016 to Squadron Resources for a term of five (5) years for Group One Minerals. On the $25^{th\ of}$ May 2020, Squadron Resources changed its name to Wyloo Metals Pty Ltd (Wyloo). In December 2020 the tenure was transferred from Wyloo Metals to Broken Hill Alliance Pty Ltd a 100% subsidiary company of Castillo Copper Limited. Both tenures were renewed on the $12^{th\ of}$ August 2021 for a further six (6) years and are due to expire on the $2^{nd\ of}$ June 2027. EL 8434 lies across two (2) 1:100,000 geology map sheets Redan 7233 and Taltingan 7234, and two (2) 1:250,000 geology map sheets, SI54-3 Menindee, and SH54-15 Broken Hill in the county of Yancowinna. EL 8434 consists of one hundred and eighty-six (186) units) in the Adelaide and Broken Hill 1:1,000,000 Blocks covering an area of approximately $580km^2$. EL 8435 is located on the 1:100,000 geology map sheet Taltingan 7234, and the 1:250,000 geology map sheet SH/54-15 Broken Hill in the county of Yancowinna. EL 8435 consists of twenty-two (22) units (Table 1) in the Broken Hill 1:1,000,000 Blocks covering an area of approximately $68km^2$. Access to the tenures from Broken Hill is via the sealed Barrier Highway. This road runs north-east to south-west through the northern portion of the EL 8434, passes the southern tip of EL 8435 eastern section and through the middle of the western section of EL 8435. Access is also

available via the Menindee Road which runs north-west to south-east through the southern section of the EL 8434. The Orange to Broken Hill Rail line also dissects EL 8435 western section the middle and then travels north-west to south-east slicing through the eastern arm of EL 8434 (Figure C2-1).

Figure C2-1: EL 8434 and EL 8435 General Location Map



Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	Explorers who were actively involved over longer historical periods in various parts of EL8434 were: - North Broken Hill Ltd, CRAE Exploration, Major Mining Ltd and Broken Hill Metals NL, Pasminco Exploration Ltd, Normandy Exploration Ltd, PlatSearch NL/Inco Ltd/ EGC Pty Ltd JV and the Western Plains Gold Ltd/PlatSearch/EGC Pty Ltd JV. A comprehensive summary of work by previous explorers was presented in Leyh (2009). However, more recently, follow-up field reconnaissance of areas of geological interest, including most of the prospective zones was carried out by EGC Pty Ltd over the various licenses. This work, in conjunction with a detailed interpretation of aeromagnetic, gravity plus RAB / RC drill hole logging originally led to the identification of at least sixteen higher priority prospect areas. All these prospects were summarized in considerable detail in Leyh (2008). Future work programs were then also proposed for each area. Since then, further compilation work plus detailed geological reconnaissance mapping and sampling of gossans and lode rocks has been carried out. A total of 22 prospects were then recognised on the exploration licence with at least 12 occurring in and around the tenure. With less than 45% outcropping Proterozoic terrain within the licence, this makes it very difficult to explore and is in the main very effectively screened from the easy application of more conventional exploration methodologies due to a predominance of extensive Cainozoic cover sequences. These include recent to young Quaternary soils, sands, clays and older more resistant, only partially dissected, Tertiary duricrust regolith covered areas. Depth of cover ranges from a few metres in the north to over 60 metres in some areas on the southern and central license. Exploration by EGC Pty Ltd carried out in the field in the first instance has therefore been heavily reliant upon time consuming systematic geological reconnaissance mapping and relatable geochemical sampling. These involve a slow systematic search over low outcropping areas, poorly exposed subcrops and float areas as well as the

		progressive development of effective regolith mapping and sampling tools. This work has been combined with a vast amount of intermittently acquired past exploration data. The recent data compilation includes an insufficiently detailed NSWGS regional mapping scale given the problems involved, plus some regionally extensive, highly variable, low-level stream and soil BLEG geochemical data sets over much of the area. There are also a few useful local detailed mapping grids at the higher priority prospects, and many more numerous widespread regional augers, RAB, and percussion grid drilling data sets. Geophysical data sets including ground magnetics, IP and EM over some prospect areas have also been integrated into the exploration models. These are located mainly in former areas of moderate interest and most of the electrical survey methods to date in this type of terrain continue to be of limited application due to the high degree of weathering and the often prevailing and complex regolith cover constraints. Between 2007 and 2014 Eaglehawk Geological Consulting has carried out detailed research, plus compilation and interpretation of a very large volume of historic exploration data sourced from numerous previous explorers and dating back to the early 1970's. Most of this data is in non-digital scanned form. Many hard copy exploration reports (see references) plus several hundred plans have been acquired from various sources, hard copy printed as well as downloaded as scans from the Geological Survey of NSW DIGS system. They also conducted field mapping, costean mapping and sampling, and rock chip sampling and analysis. **Work Carried out by Squadron Resources and Whyloo Metals 2016-2020** Research during Year 1 by Squadron Resources revealed that the PGE-rich, sulphide-bearing ultramafic rocks in the Broken Hill region have a demonstrably alkaline affinity. This indicates a poor prospectivity for economic accumulations of sulphide on an empirical basis (e.g., in comparison to all known economic magmatic nickel sulphide deposits,

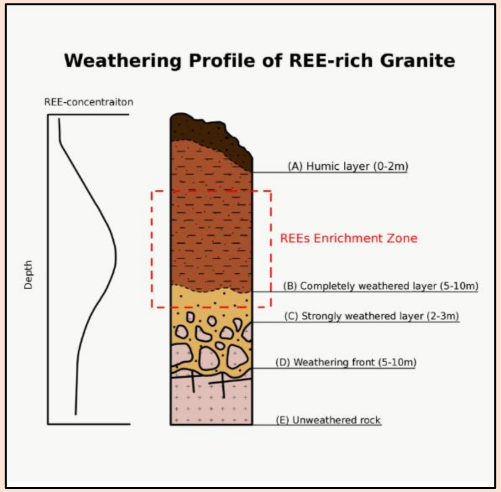
		which have a dominantly tholeiitic affinity). Squadron instead directed efforts toward detecting new Broken Hill-Type (BHT) deposits that are synchronous with basin formation. Supporting this modified exploration rationale are the EL's stratigraphic position, proximity to the Broken Hill line of lode, abundant mapped alteration (e.g., gahnite and/or garnet bearing exhalative units) and known occurrences such as the "Sisters" and "Iron Blow" prospects. The area overlies a potential magmatic Ni-Cu-PGE source region of metasomatised sub-continental lithospheric mantle (SCLM) identified from a regional targeting geophysical data base. The exploration model at the time proposed involved remobilization of Ni-Cu-PGE in SCLM and incorporation into low degree mafic-ultramafic partial melts during a post-Paleoproterozoic plume event and emplacement higher in the crust as chonoliths/small intrusives - Voisey's Bay type model. Programs were devised to use geophysics and geological mapping to locate secondary structures likely to control and localise emplacement of Ni-Cu-PGE bearing chonoliths. Since EL8434 was granted, the following has been completed: • Airborne EM survey. • Soil and chip sampling. • Data compilation. • Geological and logistical reconnaissance. • Community consultations; and • Execution of land access agreements. **Airborne EM Survey** Geotech Airborne Limited was engaged to conduct an airborne EM survey using their proprietary VTEM system in 2017. A total of 648.92-

		line kilometres were flown on a nominal 200m line spacing over a portion of the project area. Several areas were infilled to 100m line spacing. The VTEM data was interpreted by Southern Geoscience Consultants Pty Ltd, who identified a series of anomalies, which were classified as high or low priority based on anomaly strength (i.e., does the anomaly persist into the latest channels). Additionally, a cluster of VTEM anomalies at the "Sisters" prospect have been classified separate due to strong IP effects observed in the data. Geotech Airborne have provided an IP corrected data and interpretation of the data has since been undertaken. **Soil and Chip sampling** The VTEM anomalies were followed up by a reconnaissance soil sampling programme. Spatially clustered VTEM anomalies were grouped, and follow-up soil lines were designed. Two (2) VTEM anomalies were found to be related to culture and consequently no soils were collected. Two (2) other anomalies were sampled which were located above thick alluvium of Stephens Creek and were therefore not sampled. A line of soil samples was collected over a relatively undisturbed section at Iron Blow workings and the Sisters Prospect. One hundred and sixty-six (166) soil samples were collected at a nominal 20cm depth using a 2mm aluminum sieve. Two (2) rock chips were also collected during this program. The samples were collected at either 20m or 40m spacing over selected VTEM anomalies. The samples were pulverised and analysed by portal XRF at ALS laboratories in Perth. Each site was annotated with a "Regolith Regime" such that samples from a depositional environment could be distinguished from those on exposed Proterozoic bedrock, which were classified as an erosional environment. The Regolith Regime groups were used for statistical analysis and levelling of the results. The levelled data reveals strong relative anomalies in zinc at VTEM anomaly clusters 10, 12 and 14 plus strong anomalous copper at VTEM 17.

<table>
<tr>
<td>Geology</td>
<td>Deposit type, geological setting, and style of mineralisation.</td>
<td>
As the strata is tightly folded, the intersected cobalt-rich layers are overstated in terms of apparent thickness, however the modelling software calculates a true, vertical thickness. Cobalt mineralisation is commonly associated with shears, faults, amphibolites, and a quartz-magnetite rock within the shears, or on or adjacent to the boundaries of the Himalaya Formation. In general, most of the cobalt and rare earth element - rich layers have a north-northwest to north strike.

REE enrichment generally occurs as a 5 to 10-metre-thick zone between the completely weathered layer and strongly weathered layer and it is targeted for commercial mining (Figure D2-2). Compared to other REE deposits, regolith-hosted rare earth element deposits are substantially low-moderate grade (containing 0.05-0.3 wt.% extractable REEs). Nevertheless, due to its easy extraction method, low processing costs and large abundance, the orebodies are generally economic to be extracted (Duuring, (2020); Kanazawa and Kamitani (2006); and Murakami, H.; Ishihara (2008)).

Figure C2-2: Weathering Profile over REE – Rich Granite



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		https://en.wikipedia.org/wiki/Regolith-hosted_rare_earth_element_deposits Weathering profile of regolith hosted REE deposits shown above, the legend is: (A) Humic layer. (B) Completely weathered layer. (C) Strongly weathered layer. (D) Weathering front. (E) Unweathered rock. Most of the REE found in cerium monazite (Ce (PO_4)) which always contains major to minor amounts of other REE (Nd, La, Pr, Sm etc) replacing Ce. Also, the mineral often contains trace amounts of U and Th (coupled with Ca). This will be collaborated with XRD and or SEM analysis.
Drill hole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.* *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	Header information about all drillholes and surface samples completed at Tors Tank and Fence Gossan have been tabulated in this release in Appendix B.
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations*	No metal equivalents have been reported. Rare earth element results have been converted to rare earth oxides as per standard industry practice (Castillo Copper 2022f).

	(e.g., cutting of high grades) and cut-off grades are usually Material and should be stated. *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	No compositing of assay results has taken place, but rather menu options within the Datamine GDB module have been used to create fixed length 1m assay intervals from the original sampling lengths. The rules follow very similarly to those used by the Leapfrog Geo software in creating fixed length samples.
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.* *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g., 'down hole length, true width not known').*	A database of all the historical borehole sampling has been compiled and validated. It is uncertain if there is a strong relationship between the surface sample anomalies to any subsurface anomalous intersections due to the possible masking by variable Quaternary and Tertiary overburden that varies in depth from 0-15m. The mineralisation appears to be secondary enrichment in the regolith clays and extremely weathered material derived from quartzo-feldspathic pegmatites.
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Current surface anomalies are shown on maps released on the ASX (Castillo Copper 2022d, 2022e, 2022f and 2022g). All historical surface sampling has had their coordinates converted to MGA94, Zone 54.
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	All recent laboratory analytical results have been recently reported (see Castillo Copper 2022a, b, c, d, e, f, and g) for assay results. Regarding the surface and sampling, no results other than duplicates, blanks or reference standard assays have been omitted.

Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Historical explorers have also conducted airborne and ground gravity, magnetic, EM, and IP resistivity surveys over parts of the tenure area but this is yet to be fully georeferenced (especially the ground IP surveys). Squadron Resources conducted an airborne EM survey in 2017 that covers Iron Blow and The Sisters, but not the southern cobalt and REE prospects.
Further work	*The nature and scale of planned further work (e.g., tests for lateral extensions or depth extensions or large-scale step-out drilling).* *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	It is recommended that: • Complete rehabilitation of the 2022 BHAE drilling campaign that comprised mostly RC drilling. An application supporting an ESF2 lodgment is yet to be approved by the NSW Resource Regulator • The remaining non-sampled zones within the Core Library drillholes, BH1, BH2, and DD90-IB3 in the north of the tenure group be relogged and sampled. DD90-IB3 had 21-87m retested recently and is a good candidate for hyperspectral logging. • A program of field mapping and ground magnetic, IP or radiometric surveys be planned and executed at Fence Gossan. Mapping of pegmatite outcrops is a high priority. • Generate an Exploration Target for Fence Gossan to the standard of Clause 17 of the 2012 JORC Code. • Depending upon the results of the proposed geophysical surveys and Exploration Target noted above, the next drilling program will specifically target the air coring technique over the known cobalt and REE mineralisation downdip to at least 30m depth at all three prospects. That proposed drilling program is also designed to increase the resource confidence of the REE to Inferred Resources to the standard of the 2012 JORC Code.

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